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High stress-driven voltages in net-like  
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Hybrid organo-metal halide perovskites (OMHPs) have been extensively explored for photo or photo-enhanced applications, which are time, location or light-limited. Unlike in other works, herein, methylammonium lead iodide (MAPbI<sub>3</sub>) perovskite was employed as a small area (<1 cm<sup>2</sup>) stress-driven energy converter. Briefly, MAPbI<sub>3</sub> was infiltrated into a net-like composite scaffold, having three constituents; polyvinylidene fluoride (PVDF), polylactic acid (PLA) and tin dioxide (SnO<sub>2</sub>) electrospun nanofibres. A systematic vertical ultrasonic vibration was optimized and applied to each sample, followed by ice quenching. Addition of MAPbI<sub>3</sub> and vertical vibration altered the morphotropic phase nature of the composite towards desirable electroactive forms, without further poling, revealed by XRD, FTIR, and Raman studies. When the device was subjected to bending/compression-release forces, high output voltage of 4.82 V and current of 29.7 nA were obtained over an area of 0.0625 cm<sup>2</sup>. The champion device also registered high piezoelectric strain coefficients ( $d_{33}$ ) of 123.93 pC N<sup>-1</sup> and 118.85 pC N<sup>-1</sup> (with and without a SnO<sub>2</sub> nanoparticle underlayer, respectively). We further elucidate the mechano-electrical outputs of MAPbI<sub>3</sub> devices grown on other distinctive underlayers. This work advances the drive towards all-day–all-night energy harvesting using OMHPs, the force being applied from ubiquitous motions or artificial movements.

Driven by a skyrocketing demand for both handy and miniaturized smart, healthcare, and info/edutainment electronics, military and wearable devices and sensor systems, there has been tremendous interest in small area energy devices that have the potential to harness electrical output from several omnipresent processes.<sup>1,2</sup> Similar to thermoelectrics and photovoltaics, piezoelectrics which convert mechanical energy to electrical energy and *vice versa* have also attracted researchers' attention lately.<sup>3–5</sup> Piezoelectrics have a non-centrosymmetric crystal morphology that facilitates displacement of dipoles on application of stress. In the years from the first discovery of piezoelectricity in 1880,<sup>6</sup> enormous efforts have been commissioned towards improving this scientific marvel to performance levels supportive of ever-intricating user devices and systems. For instance, lower piezoelectric coefficients ( $d_{33} < 100$  pC N<sup>-1</sup>) initially discovered in barium titanate, BaTiO<sub>3</sub> – a perovskite structured ceramic<sup>7</sup> have been tuned by over sixfold in Ba(Ti<sub>0.8</sub>Zr<sub>0.2</sub>)O<sub>3</sub>–(Ba<sub>0.7</sub>Ca<sub>0.3</sub>)TiO<sub>3</sub> ( $d_{33} = 620$  pC N<sup>-1</sup>).<sup>8</sup> Many Pb-containing perovskite ceramics like lead zirconate titanate (PZT) have similarly been tuned using various intrinsic and extrinsic techniques presenting high piezoelectric coefficients.<sup>9,10</sup> However, most of the present devices typically necessitate the piezoelectric material to be thin, soft, flexible and sturdy (to sustain many mechanical stress cycles). This is in addition to them having distinctive domains and domain walls. Conventional inorganic piezoelectrics (ceramics) are characteristically multidomain but grow at elevated temperatures in the paraelectric phase, and thus require additional high voltage poling and expensive processing steps to impart most of these properties.<sup>9</sup> Although, hybrid organic–inorganic piezoelectric materials tend to change phases at certain pressures and temperatures, they combine the valuable properties of organic molecules and advantages of crystalline inorganic solids at a molecular level.<sup>5</sup>

Most of the organo-metal halide perovskites (OMHPs) such as CH<sub>3</sub>NH<sub>3</sub>PbI<sub>3</sub>, CH<sub>3</sub>NH<sub>3</sub>PbBr<sub>3</sub> and HC(NH<sub>2</sub>)<sub>2</sub>PbI<sub>3</sub> are efficient for solar cells, but this property is impaired in the dark mode, and thus requires conditional (directional) light exposure.<sup>11</sup>

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Furthermore, some of the most important causes of instabilities in perovskite solar cells have been reported as accumulation of light and the consequent thermal effect.<sup>12–15</sup> Therefore, enhancement of the piezo/ferroelectric properties of the comprising materials is of paramount importance and averts frustrations arising from sole dependence on their photon harvesting function. Piezo/ferroelectric qualities of OMHPs arise due to the dipole moments of their non-centrosymmetric organic cations or the intrinsic lattice distortions, which break the crystal centrosymmetry.<sup>16,17</sup> Hu *et al.*<sup>18</sup> and Frost *et al.*<sup>19</sup> calculated the electronic dipole of the organic cation in halide perovskites and showed that hybrid perovskites exhibit spontaneous electric polarization, though other reports contend that MAPbI<sub>3</sub> is anti-ferromagnetic.<sup>20</sup> By substituting AMX<sub>3</sub> atomic constituents of their generic orthogonal unit cell, it is feasible to tune the structural, electronic, optical, and magnetic properties. Also, interstices formed in the large structure can accommodate different elements, thus adopting various orthogonal crystalline conformations: the cubic, the tetragonal and the orthorhombic.<sup>21,22</sup> Summarily, amongst others, OMHPs give abundance of composition and geometric alterations, and printability on both sturdy and bendable substrates, but register lower piezoelectric constants to be trusted for many real-use applications.<sup>22–24</sup> Consequently, the main research exertions in this field focus on designing better materials and device fabrication strategies, optimizing the perovskite configuration, and the creation of new device constructions for improved and stable performance piezoelectrics.

One particular approach has been combining these hybrid perovskites with piezoelectric polymers. A better piezoelectric polymer shows the presence of permanent molecular dipoles, ability to orient or align the molecular dipoles, ability to sustain the dipole alignment once it is achieved and the ability to undergo large strains when mechanically stressed. Poly(vinylidene fluoride) (PVDF) has been used overly in sensors and actuators owing to its lightweight, flexibility, biocompatibility, sustainable structure, high ferroelectric potential and environmental friendliness.<sup>25</sup> PVDF – a semicrystalline polymer shows  $\alpha$ -,  $\beta$ -,  $\gamma$ -, and  $\delta$ -polymorphs, the  $\beta$ -(TTTT conformation) and  $\gamma$ -(T<sub>3</sub>G<sup>+</sup>T<sub>3</sub>G<sup>-</sup> conformation) phases being electro-active while the  $\beta$ -phase is as well ferroelectric due to the antagonistic electro-behavior of the hydrogen atoms and fluorine atoms within the polymer (-CH<sub>2</sub>-CF<sub>2</sub>-).<sup>25,26</sup> In terms of piezoelectric relevance, the  $\beta$ -phase shows higher dipolar moments per unit and exhibits piezo responses in the  $d_{15}$ ,  $d_{24}$ ,  $d_{31}$ ,  $d_{32}$ , and  $d_{33}$  directions.<sup>27</sup> It is, therefore the most suitable for piezoelectric actuators and sensors. Though high  $\beta$ -phase ferroelectric poly(vinylidene fluoride-co-trifluoroethylene) (PVDF-TrFE) exists, it is expensive and possesses a narrow scope of operating temperature.<sup>28</sup> Therefore, other techniques have been attempted to enhance the  $\beta$ -phase nucleation in the polymer; for example, mechanical stretching, electrical poling, addition of hydrated salts and nanoparticle fillers (Al(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O, ZnO, MgO, Al<sub>2</sub>O<sub>3</sub>, BaTiO<sub>3</sub>, and carbon nanotubes) and melting at high pressure.<sup>26</sup> Most of these processes involve multiple steps which require more energy consumption and result in loss of efficiency. Consequently, there has not been tremendous change in the

relative efficiencies of piezoelectric coefficients following most of these modification methods.

As an alternative approach, Ghosh *et al.*<sup>29</sup> recently used an erbium infrared ion to synthesize a mechanically robust high  $\beta$ -phase PVDF mesoporous film. This improved the piezoelectricity as well as the mechano-sensitivity of the device prominently. In the same line, Sultana *et al.*<sup>30</sup> designed a three-in-one (photodetection, piezoelectricity and hybrid photo-active piezoelectricity) energy harvester system composed of CH<sub>3</sub>NH<sub>3</sub>PbI<sub>3</sub> and  $\beta$ -PVDF. Dipole induction from PbI<sub>3</sub> cage corners in the MAPbI<sub>3</sub> forces the -CH<sub>2</sub>-CF<sub>2</sub> groups in PVDF to align normally, forming strongly electroactive  $\beta$ -phases, especially in the vicinity of perovskites. Interestingly, with an optimal polymer composition, MAPbI<sub>3</sub> partly dissociates into its gaseous phases, CH<sub>3</sub>NH<sub>2</sub> and HI, which discharge leaving a porous matrix, with augmented strain performance. More so, the hydrophobic PVDF polymer provides supplementary encapsulation to the CH<sub>3</sub>NH<sub>3</sub>PbI<sub>3</sub> against oxygen and moisture, making it adaptive to more stress cycles.<sup>31</sup> It is worth noting that although direct solution mixing of the PVDF and MAPbI<sub>3</sub> perovskite enhances the ferroelectric  $\beta$ -phase content of the polymer and improves the piezoelectric performance of the devices,<sup>32</sup> this could potentially enhance oxidation and distort the continuous MAPbI<sub>3</sub> film structure, thus antagonizing the other photoelectric functions of MAPbI<sub>3</sub>.<sup>5,12,33,34</sup> Therefore, device designs that enable coexistence of the two functionalities are apposite. Relatedly, blends of semicrystalline PVDF and chiral piezoelectric poly(L-lactic acid) (PLLA) polymers have been reported which formed porous piezoelectric structures with added performance.<sup>35,36</sup> The addition of PLLA further imparts great potentialities to electronics, robotics and bionics due to its sensibility, pliability and biocompatibility. The properties of PLLA depend on its constituent isomers, processing temperature, annealing time and its molecular weight.<sup>35</sup>

Although less reported, introduction of controlled amounts of SnO<sub>2</sub> to a piezoelectric material enhances mechano-electrical and optoelectronic performance properties, like dielectric constant, strain constants, mechanical quality factor, and conversion efficiencies.<sup>37–39</sup> With the universality of preparation recipes, lower temperature sinterability (compared to other metal oxide semiconductors), and compatibility with polymer matrices, SnO<sub>2</sub> nanomaterials also show optical transparency and high electron mobility, and possess suitable band alignment when used with OMHPs.

Centered on these concepts, we aim to synthesize a material with: a porous polymeric framework to realize maximum mechano-electrical conversion, high ferroelectric  $\beta$ -phase content, and a pure hybrid OMHP film deposition to achieve advanced and stable piezoelectric activity.

Here, we present a highly flexible piezoelectric net-like film composed of PVDF, PLLA and SnO<sub>2</sub> nanofibers (NFs) (expressed as PPS-Co hereinafter) on a bendable PET/ITO substrate. MAPbI<sub>3</sub> perovskite is deposited and infiltrated into this mesoporous netlike composite layer. This typical interfacing enlarges the contact area between MAPbI<sub>3</sub> and the PPS-Co layer, and differs from a simple polymer conjugation. We strategically applied an



**Scheme 1** Experimental procedure. Step by step PPS-Co composite processing approach, together with the cross-sectional structure of the fully fabricated PPS-Co/MAPbI<sub>3</sub> device (not drawn to scale). The device is finally covered by a thin PDMS layer to enhance mechanical perseverance.

ultrasonic vibration post treatment (for simplicity denoted UVPT) on the wet-spun films, using a custom-designed vertical ultrasonic vibrator to achieve the following: (1) to form a net/electret-like (mesoporous) polymeric composite with predominant  $\beta$ -phase, (2) to uniformly combine the composite elements, and (3) to efficiently infiltrate part of the perovskite into the mesopore composite. A fully fabricated perovskite device based on this PPS-Co/MAPbI<sub>3</sub> bilayer (Scheme 1) generated great output voltage on periodic bending, without additional poling induction. This can be attributed to the synergistic piezo and ferroelectric effect presented by the polarizable material constituents in the composite, increased crystal order as well as enhanced polarity along the device thickness (rendered by interfacing of perovskite, SnO<sub>2</sub> NF and the highly polar polymers). Scheme 1 shows PPS-Co processing steps. The mechano-electrical outputs of the perovskite device containing PPS-Co are compared with a counterpart, in which MAPbI<sub>3</sub> was grown on a layer of SnO<sub>2</sub> NFs in lieu of PPS-Co composite, still *via* UVPT. To enhance the anchorage of the SnO<sub>2</sub> NFs or PSS-Co on the conductive flexible substrate, improve the dielectric permittivity and reduce probable shunting especially during mechanical bending tests, a very thin layer of compact SnO<sub>2</sub> nanoparticles (NPs) was spun onto the conductive substrate, and the piezoelectric response of the ensuing device compared in the presence and absence of this thin SnO<sub>2</sub> NP layer. All different models of devices were assessed at analogous intermittent bending and on application of normal compression-release forces to the device's top surface. These revelations present an exciting basis for advancing the lobby into self-powered miniaturized electronics with potential to harness energy from mechanical motions regardless of illumination, for a flexible electronics market that is presently worth about USD 310 million and is expected to rise to USD 645.8 million by 2023.<sup>40</sup>

For proper depiction and comparison of the effects of different underlayers (SnO<sub>2</sub> NFs and PPS-Co) on the electrical yield of the fabricated device, we elaborate first, the characteristic properties of each of these individual thin layers before discussing the observed performance variations between the devices.

## SnO<sub>2</sub> nanofiber thin film layer

Images in Fig. 1a show the top surface SEM micrographs of the densely deposited SnO<sub>2</sub> films (NF and NP) on PET/ITO. The SEM images of the original SnO<sub>2</sub> nanofiber film achieved from electrospinning and after sintering are also provided. From the images, the longer electrospun nanofibres are broken up due to brisk supersonic agitation and magnetic stirring during dispersion in acetone. Dispersing the nanofibres before deposition, and cutting them into shorter pieces, improved their surface area, surface coverage, mechanical endurance against bending, electrical function and close packing on the substrate as can be further affirmed by the presence of intense peaks of SnO<sub>2</sub> in the XRD pattern (Fig. 1b). A lower magnification SEM surface micrograph of the deposited SnO<sub>2</sub> NF film is shown in the ESI,<sup>†</sup> Fig. S1a revealing the uniform dense structure of the formed film.

The XRD pattern revealed the formation of SnO<sub>2</sub> NFs with noticeable peaks located at  $2\theta$  degree values of *ca.* 26.6°, 33.8°, 37.8° and 51.7°, corresponding to reflections in the (110), (101), (200) and (211) lattice planes, respectively, which are characteristic of the tetragonal rutile phase of SnO<sub>2</sub> (JCPDS 41-1445). Fig. 1c shows a Raman spectrum for sintered SnO<sub>2</sub> NFs, recorded at room temperature. The peak at 635 cm<sup>-1</sup> is the



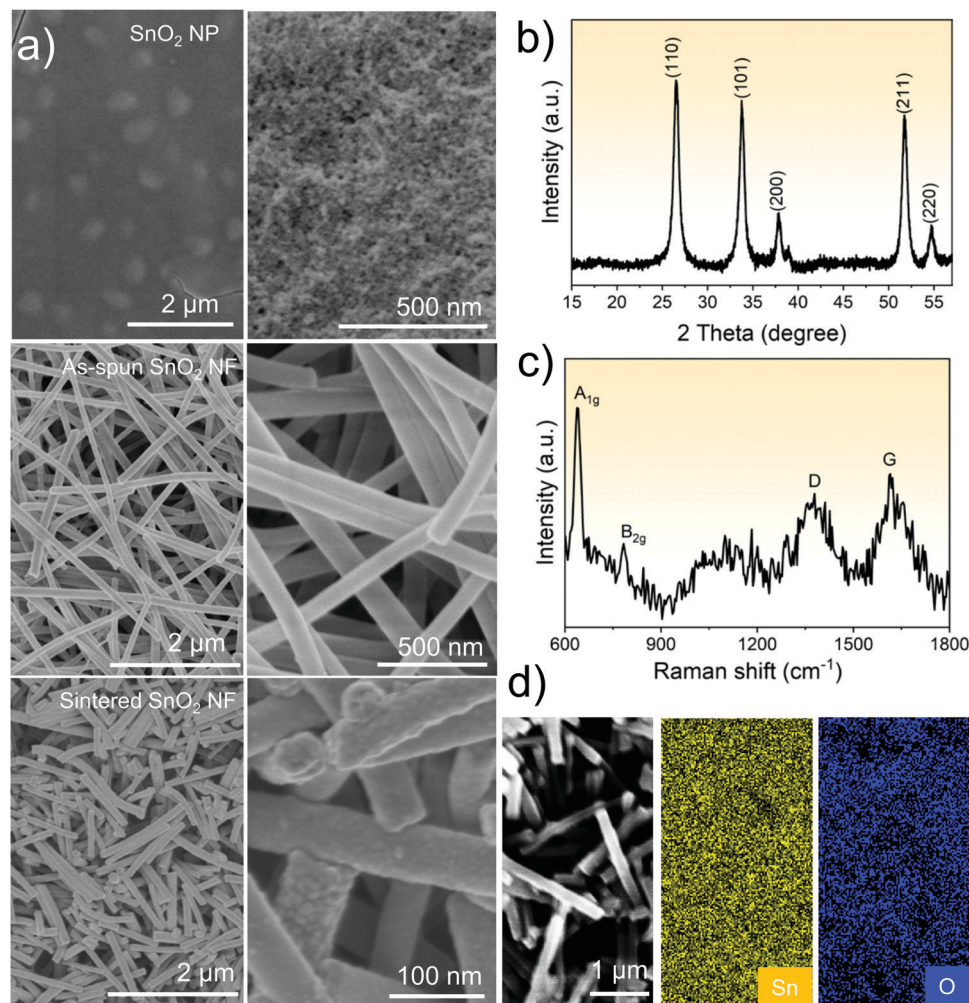


Fig. 1 Characterization of the SnO<sub>2</sub> film. (a) Surface SEM images of the SnO<sub>2</sub> NP film (underlayer), as-electrospun NF membrane and sintered film. (b) XRD pattern, (c) Raman spectrum and (d) EDS maps of SnO<sub>2</sub> NF film.

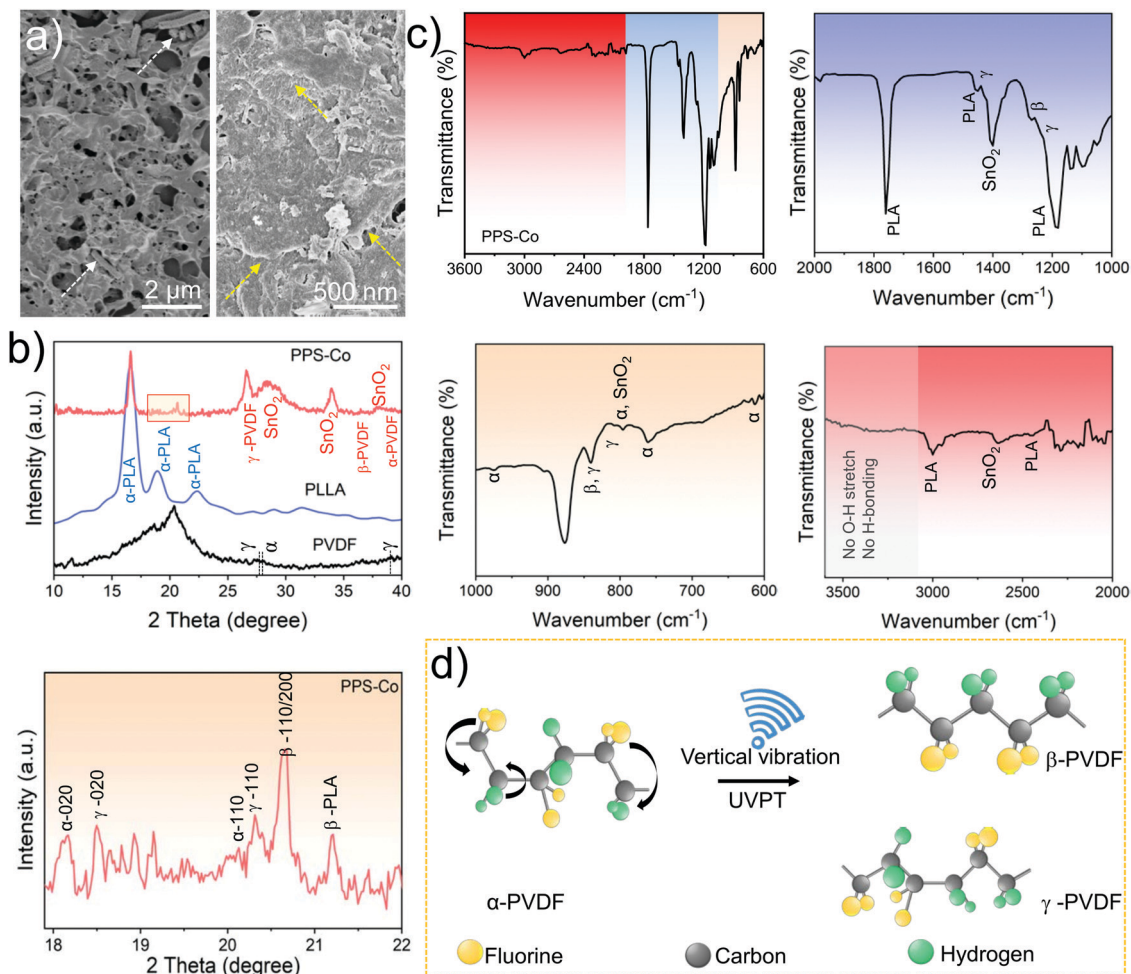
normal lattice vibration of the A<sub>1g</sub> mode of the D<sub>4h</sub> space group, to which the rutile crystalline structure of SnO<sub>2</sub> belongs. Other peaks at *ca.* 778, 1370, and 1650 cm<sup>-1</sup> are indexed to the B<sub>2g</sub>, D band, and G band, respectively, as found in Raman surveys.<sup>41</sup> The obtained EDS maps depicted in Fig. 1d further show that the nanofibers are indeed composed of Sn and O, a result which confirms that the calcined product is the pure tetragonal rutile phase of SnO<sub>2</sub> nanofibers, in line with XRD and Raman surveys.

## PPS–Co composite

SEM surface micrographs of PPS–Co are shown in Fig. 2a and Fig. S1b (ESI†). The microscale appearance of the composite after ultrasonic vibration demonstrates a kind of porous (net-like) structure. Also, higher magnifications revealed different boundaries in the form of phases as depicted by arrows. Before any prejudgment, we attribute this biphasic feature to immiscibility of PVDF and the L-enantiomer of PLLA (hence forth referred to as PLA). A similar effect was discussed by others, who related the piezoelectric behavior to proliferation of the discrete phase

and propagation boundaries in the composite.<sup>30,36</sup> Here, we assign this pattern of dispersion to the contentious molecular motion during polymerization and deposition, under uniformly imparted ultrasonic energy. The scenario which perhaps governs the formation of the porous configuration is the self-assembly of the nano-fibers within the co-polymer, under the ultrasonic field. It is plausible that the background polymer tends to be disintegrated by the ultrasonic energy, during deposition. In the meantime, the SnO<sub>2</sub> NFs, which are trapped in the polymer matrix, act as reinforcements which pin them locally, rendering a net-type or electret-like feature to the composite. Later in this work we discuss improving the role of the PLLA/PVDF electret in piezoelectric yield of the perovskite thin film device. Fig. S2 (ESI†) demonstrates the thermal condition of the ultrasonic energy delivering platform, measured by a remote infrared thermometer within the operating conditions of this work. The thermal effect of the ultrasonic vibration process at ≤5 W for ≤4 minutes (maximum device fabrication parameters) is seen to be less than 1.5 °C, and thus inconsequential.

To prove the micro-structure and track each component in the PPS–Co, we applied crystallography and fundamental



**Fig. 2** PPS-Co net-like layer: (a) low and higher magnification SEM images of PPS-Co. The higher magnification depicts the phase boundaries between the PVDF/PLA and the polymer/SnO<sub>2</sub> NF (see arrows). (b) XRD spectra of the PPS-Co composite and the individual constituents. The region 18.0°–21.5° has been zoomed out to show the major PVDF phases obtained. (c) FTIR spectrum of PPS-Co stored in a vacuum atmosphere overnight together with the corresponding zoomed out regions. (d) Suggested mechanism for the influence of vertical ultrasonic vibration on formation of electroactive PVDF crystalline phases.

chemical analysis. Fig. 2b and c depict the XRD patterns (compared for PSS-Co, pure PLA and pure PVDF) and FTIR spectra of PPS-Co, respectively. In Fig. 2b, the XRD patterns of the pristine PLA and PVDF are also provided. The characteristic peaks in the composite spectrum reveal the existence of all three components (PLA, PVDF, and SnO<sub>2</sub>). The main peaks in the pristine PLA are observed at around  $2\theta$  values of 16.6°, 18.9° and 22.5°, corresponding to (110)/(200), (203), and (015), reflections of the orthorhombic  $\alpha$ -PLA, similar to the reported findings from other works.<sup>42</sup> In the composite however, the peaks at 16.6°, 18.9° and 22.5° reveal a shift to higher  $2\theta$  values of *ca.* 16.7°, 19.1° and 22.8°, respectively, (see magnified pattern in Fig. 2b), which reflects possible chemical interaction, and likely bridging of the polymeric chains by SnO<sub>2</sub> nanofibers. There is emergence of new peaks at 10.3° and 21.2°. These new peaks correlate with the characteristic reflections of the orthogonal  $\beta$ -form of PLA.<sup>42–44</sup> This phenomenon might be linked to the abrupt quenching of the composite during spin coating, distortion due to ultrasonic energy and the high

annealing temperature, right away, that must have combined to instigate a morphotropic stretching-like transformation of the stable  $\alpha$ -form to the metastable  $\beta$ -form of PLA. This polymorphism and phase instability creates inter-domain interactions and domain wall effects which are in part responsible for the piezoelectric behavior of the ensuing composite.<sup>45</sup> As further supported by the high resolution XRD spectrum, a significant amount of the more stable  $\alpha$ -PLA is still detectable. The index peaks of the PLA phase have slightly right-shifted, which implies chemical interactions with the SnO<sub>2</sub> nanofibers, as already stated. A reduction in crystallite size but above a certain optimum enhances the piezoelectric efficiency of thin films, supposedly due to high activity and mobility of the domain walls, as well as suppression of external forces at narrower grain boundaries.<sup>46,47</sup> The FTIR spectrum (Fig. 2c) reveals bands corresponding to the symmetric and asymmetric vibrations of C–H from methyl(ene) groups in the polymers, at 2754 and 2766 cm<sup>-1</sup>, respectively. Other bands (all in cm<sup>-1</sup>) are indexed to C=O stretching (1760), CH<sub>3</sub> bending vibration (1458),

and C–O–C asymmetric and symmetric valence vibrations (1250 and 1193), as well as the small band at 2998  $\text{cm}^{-1}$  that is also assigned to the stretching of the C–H group. These findings correlate with XRD results and also infrared descriptions of PLA in related works.<sup>48</sup>

Similarly, the XRD pattern exposes peaks reminiscent of reflections in the (110), (101), and (200) planes of tetragonal rutile  $\text{SnO}_2$ , at around 26.6°, 33.7°, and 37.9°, respectively, as described earlier. However, just like the case with PLA, the peak positions of reflection in the  $\text{SnO}_2$  crystal planes are all slightly shifted to the right in the composite (Fig. 2b), and thus a further reflection of an envisaged interaction between the polymeric content and  $\text{SnO}_2$  NF, which enhances the piezoelectric response of the nanogenerator. To ascertain the change in crystallite size between the composited and free  $\text{SnO}_2$  NFs, we follow the Scherrer equation (see eqn (S1), ESI†). The average crystallite sizes of free  $\text{SnO}_2$  NFs (12.74 nm) and  $\text{SnO}_2$  NFs in the PPS–Co (11.49 nm) show a slight difference of 1.25 nm as seen in Table S1 in the ESI.† Nonetheless, the scientific rationale behind this phenomenon should be further addressed. Other reports have defined an enhancement in the piezoelectric performance of devices with reduction in crystallite and grain sizes.<sup>46,47</sup> Moreover, the proliferating band at 797  $\text{cm}^{-1}$  in the FTIR spectrum (Fig. 2c) is attributed to the O–Sn–O asymmetric vibration mode,<sup>49</sup> typical of wet processed films and this further cements the claimed interaction between the  $\text{SnO}_2$  NFs and the polymeric content, as deduced from XRD. Similarly, the bands at 1455  $\text{cm}^{-1}$ , and 1242  $\text{cm}^{-1}$  are also characteristic of  $\text{SnO}_2$  nanomaterials, with reference to the literature.<sup>50</sup>

From Fig. 2b, there are other noticeable peaks positioned at  $2\theta = 18.2^\circ$ ,  $20.3^\circ$ , and  $20.7^\circ$  (also Fig. S3, ESI†). Related peaks have been previously reported<sup>31,35,51,52</sup> as exclusive for the reflections in the polymorphic crystal planes of the  $\alpha$ - (020),  $\gamma$ - (110/101), and  $\beta$ - (110/200) forms of PVDF, respectively. The existence of these different crystalline and amorphous phases is further indicated by FTIR spectra in Fig. 2c. In line with the literature, the vibrational band at 841  $\text{cm}^{-1}$  should show the presence of the electroactive  $\gamma$  and/or  $\beta$  forms of PVDF. The bands in the spectra obtained show unique features at around (811  $\text{cm}^{-1}$ , 1235  $\text{cm}^{-1}$ , and 1429  $\text{cm}^{-1}$ ) and 1274  $\text{cm}^{-1}$ , which are correspondingly characteristic of  $\gamma$ - and  $\beta$ - phases.<sup>25,30,31,51</sup> On the other hand, the bands at *ca.* 613, 762, 795, and 975  $\text{cm}^{-1}$ , are prominent with the absorption bands of the  $\alpha$ -crystal phase. This gives support to the deductions from the XRD findings that reveal the existence of the three alternative PVDF forms and also the well-claimed revelation that UVPT solution-borne PVDF contains significant amounts of the  $\beta$  crystal form.

**Table 1** PVDF phase contents in the PPS–Co calculated from FTIR results. The high percentage of electroactive phase content ( $\beta$  and  $\gamma$ ) relative to the  $\alpha$ -crystal phase owing to UVPT is revealed

PPS–Co film	Electroactive phase content ( $F_{\beta\gamma}$ )	$\beta$ -Phase content ( $F_\beta$ )	$\gamma$ -Phase content ( $F_\gamma$ )
Unvibrated	52.29	27.44	24.85
Vibrated	82.47	49.56	32.91

To ascertain the PVDF electroactive/ferroelectric phase content ( $\beta$  and  $\gamma$ , and  $F_{\beta\gamma}$ ) in the composite (since the 841  $\text{cm}^{-1}$  can be indexed to both polar phases), we use the following equations according to Beer–Lambert's law:<sup>30,47</sup>

$$F_{\beta\gamma} = \frac{I_{841}}{\left[\frac{K_{841}}{K_{763}}\right] I_{763} + I_{841}} \quad (1)$$

$$F_\beta = F_{\beta\gamma} \times \left[\frac{X_\beta}{X_\beta + X_\gamma}\right] \quad (2)$$

$$F_\gamma = F_{\beta\gamma} \left[\frac{X_\gamma}{X_\beta + X_\gamma}\right] \quad (3)$$

where  $I_{841}$  and  $I_{763}$  are the absorbances at 841  $\text{cm}^{-1}$  and 763  $\text{cm}^{-1}$ , respectively, whereas  $K_{841}$  ( $7.7 \times 10^4 \text{ cm}^2 \text{ mol}^{-1}$ ) and  $K_{763}$  ( $6.1 \times 10^4 \text{ cm}^2 \text{ mol}^{-1}$ ) are the corresponding absorption coefficients. Relatedly, the relative contents of  $\beta$  ( $F_\beta$ ) and  $\gamma$  ( $F_\gamma$ ) forms of PVDF in the composite are obtained using equations (eqn (1)–(3)).  $X_\beta$  and  $X_\gamma$  are the absorbance values at bands 1275  $\text{cm}^{-1}$  and 1231  $\text{cm}^{-1}$  one-to-one, and the results are indicated in Table 1. To establish the efficacy of our film synthesis approach and for comparison purposes, we gauged the phase content in the UVPT treated against the unvibrated composite. Using FTIR data, we find that the percentage of the electroactive phase increased by ~58% (from 52.29% to 82.47%) with the  $\beta$ -phase content rising by 80.61% (27.44% to 49.56%) and the  $\gamma$ -phase increasing by ~33% (24.85% to 32.91%) following UVPT exposure of the composite.

The increase in the share of the polar domain in the composite owing to ultrasonic assisted vibration (also supported by the above XRD studies) seems imperative in explaining the consequently enhanced piezoelectric performance obtained from the devices. Since to the best of our knowledge, there was no particularly detailed literature on the phase change of polymers tailing from ultrasonic vibration, we plan to do a wholistic examination of this exciting phenomenon in our subsequent works. Here, the most possible mechanism revealing the PVDF phase alignment under ultrasonic fields is suggested as follows: in a normal deposition condition  $\alpha$ -PVDF basically predominates because the atomic size of fluorine mismatches the space provided by the C–H chain. This defect makes F–C–F groups tilt relative to the normal axis and form hetero-directional dipoles.<sup>30</sup> The  $\beta$ -phase is enhanced by rearrangement of dipoles to a unidirectional alignment using stretching or poling in the electrical field.<sup>28,30</sup> In this work for the first time, crystalline transition was driven by a vertical-oscillating ultrasonic field, delivered from the surface of the ultrasonicing element. This vertically vibrating energy also partly transforms the TGTG  $\alpha$ -phase to T3GT3G'  $\gamma$ -phase, as detected by FTIR and XRD. Fig. 2d depicts the mechanism of PVDF phase change under a mild ultrasonic field as predicted in this work.

For the PPS–Co, we predict additional PVDF reorientation towards the  $\beta$ -phase at the PVDF/MAPbI<sub>3</sub> interface where a dielectric layer formed. This rises due to the electrostatic interaction of the iodine atom ( $\text{PbI}_3^-$  anion) induced negative

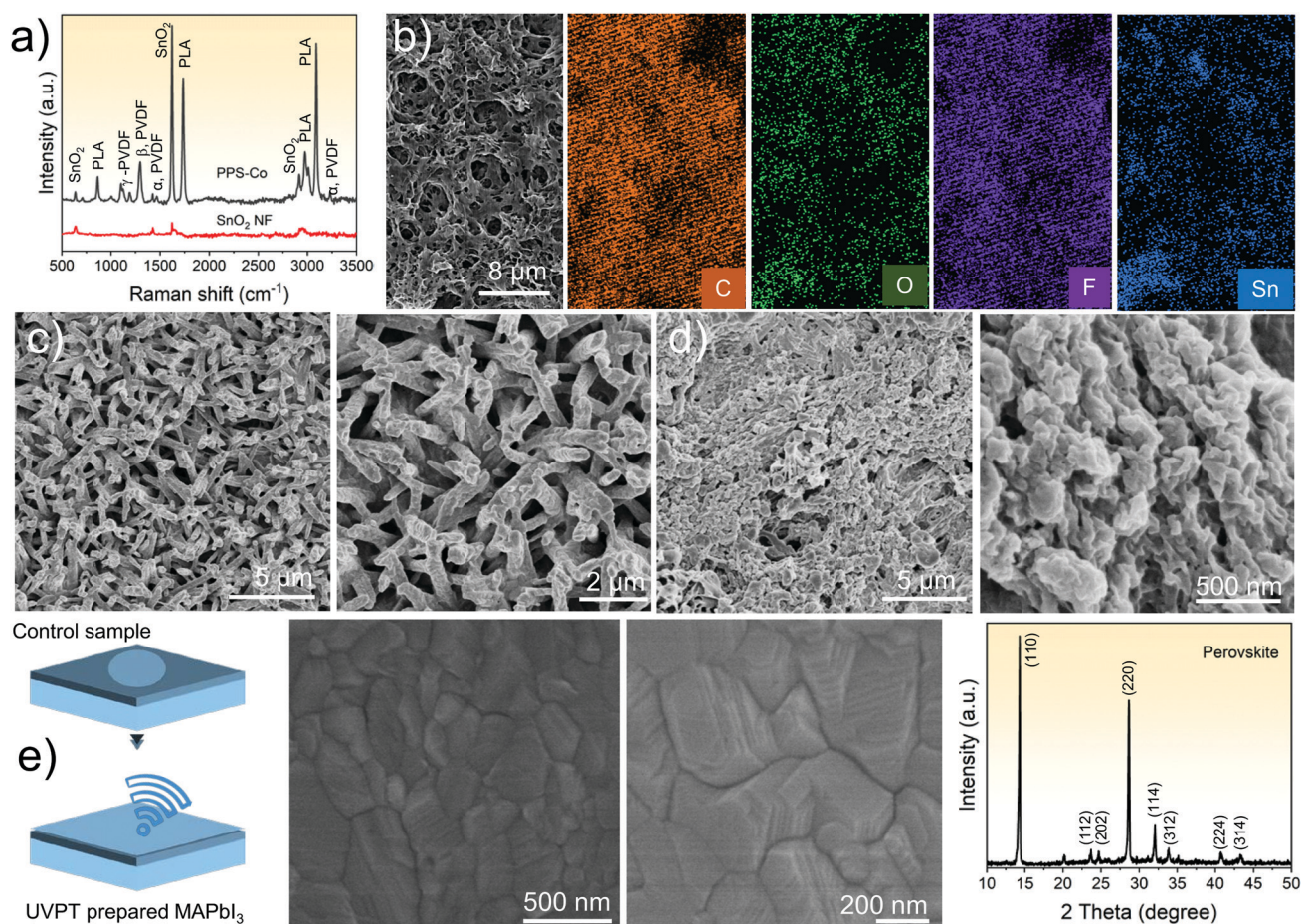


charge density on the MAPbI<sub>3</sub> surface and the –CH<sub>2</sub> dipole on the PVDF surface (effect further illustrated in Fig. S4 (ESI†) and mechanism in Fig. 5d). This explains why the induced β-PVDF content in the composite is higher than the γ-phase, despite UVPT tending to cause both transitions (Table 1), and also credits the high piezoelectric performance of the PPS-Co. A similar occurrence has been reported in related works featuring PVDF.<sup>30</sup> Consequently, the piezoelectric trait of PVDF and thus the composite is brought about by the action of both UVPT and MAPbI<sub>3</sub>-PVDF interactions.

From the FTIR spectrum, there is no strong O–H stretching band in the composite for vacuum preserved films. Nevertheless, from Fig. S5 (ESI†), there is more broadening of bands between 3200–3800 cm<sup>-1</sup> in the films maintained for more than seven days in the ambient environment. This can be attributed to degradative hydrogen bonding between the polar groups of the composite constituents and atmospheric moisture, and thus a justification for encapsulation of the device when in longer use. Generally, the spectra obtained for the overnight vacuum-stored and non-vacuumed films show overly similar characteristics, other than the hydrogen bonding bands.

This confirms the relative stability of the PPS-Co composite and films synthesized.

Fig. 3a and b expound the chemical characteristics of the PPS-Co found from the Raman spectrum (in comparison with the SnO<sub>2</sub> NF spectrum) and SEM-EDS mappings. The Raman spectra (Fig. 3a), in line with previous XRD and FTIR characterizations, show the successful preparation of a multiphase PPS-Co composite including a substantial amount of the electroactive materials, PLA, γ/β-PVDF and SnO<sub>2</sub>. The EDS spectrum reveals high approximate content of each majority element in the composite. The carbon content is the uppermost due to the dual presence of organic polymers, whereas the typical SnO<sub>2</sub> nanomaterial spectrum confirms the presence of the unbound SnO<sub>2</sub> NF material. This ratifies further our earlier postulation that some SnO<sub>2</sub> nanofibers act as mechanical linkages between adjacent polymeric phases of the composite to constitute the fascinating net-like morphology, so observed. From the EDS maps, the uniform mesh structure and the Sn, O, F and C atomic dispersions properly confirm the desired distribution of SnO<sub>2</sub> NFs in the co-polymer matrix, which is predominantly owing to the efficient molecular-scale mass



**Fig. 3** Further characterization of the PPS-Co net-like layer and after it is infiltrated with the organic–inorganic MAPbI<sub>3</sub> perovskite. (a) Raman and (b) SEM EDS maps of PPS-Co composite. The respective EDS maps shown are for C, O, F, and Sn (from PVDF, PLLA and SnO<sub>2</sub> NFs). MAPbI<sub>3</sub> perovskite infiltrated into (c) SnO<sub>2</sub> NFs, and (d) PSS-Co and (e) deposited on PET/ITO (control sample), using single step spin coating followed by 1 min ultrasonication at 2.5 W. The XRD of the perovskite in (e) is also shown.



transfer during post-deposition treatment by ultrasonic field (UVPT). Overall, the bulk properties of the composite can be believed to largely emanate from the expanded individual electro/ferro/piezoactive polymorphic phases of the PLA, PVDF and SnO<sub>2</sub> NF components, besides the mutual polymer–SnO<sub>2</sub> NF interactions that create structures which impart advanced mechanical and electrical agility to the PPS–Co.

## MAPbI<sub>3</sub> perovskite layer

One main purpose of our study is to realize an enhanced mechanical energy conversion function of the organic inorganic perovskite (MAPbI<sub>3</sub>) containing devices. To this end, we have suggested flexible and stable scaffolds for growing perovskite layers, which will potentially be high-level for piezo/photoelectric double-functions. The surface morphology, together with the level of contact and infiltration of perovskite into the under layers of SnO<sub>2</sub> NFs (Fig. 3c) and PSS–Co (Fig. 3d), promotes the piezoelectric yield and the stability of the whole resultant device. A bare perovskite layer was prepared on PET/ITO (Fig. 3e) for comparison purposes. In all cases the deposition of perovskite was conducted *via* a single step solution deposition, followed by UVPT. A brown colored film appeared after 1 minute of ultrasonic vibration and further turned into a stable dark brown MAPbI<sub>3</sub> perovskite layer within 5–7 minutes of annealing at 90 °C. For each sample the same steps were repeated without ultrasonic treatment and the dark MAPbI<sub>3</sub> layer was obtained after at least 15 minutes of thermal annealing at 90 °C. This is consistent with earlier reports that proved a reduction in optimal post-annealing time, thermal-free annealing, and reduced annealing temperature, subsequent to vibration of wet films.<sup>53</sup>

From Fig. 3e, the XRD pattern reveals the occurrence of (211) and (213) Bragg reflections at  $2\theta$  values of *ca.* 23.7° and 31.1°, respectively. This is a characteristic of a tetragonal CH<sub>3</sub>NH<sub>3</sub>PbI<sub>3</sub> polymorph as hitherto reported.<sup>53,54</sup> As a result of the optimization, the film subjected to UVPT at 2.5 W reflected the most prominent perovskite indicative signs, at 14.3° (110) and 23.6° (211).<sup>13</sup> Henceforth, we applied these conditions to prepare the perovskite layer in the piezoelectric devices, as stated earlier. Fig. S6 (ESI†) shows XRD patterns of different MAPbI<sub>3</sub> films under various UVPT power and exposure times.

As can be seen in Fig. 3c and d, the PPS–Co and SnO<sub>2</sub> NF films act as scaffolds into which some MAPbI<sub>3</sub> crystals percolate filling and covering their porous morphology, aided more by the high frequency ultrasonic vibration. It is also clear from these images that there is more perovskite coverage on the composite film than the SnO<sub>2</sub> NF layer. This can be attributed to the smoother surface morphology and smaller pores of the PPS–Co than the SnO<sub>2</sub> NFs as well as the perpendicular orientation of the SnO<sub>2</sub> NFs on the substrate, relative to UVPT, as seen from Fig. 4c and cross-section (Fig. S7, ESI†). This contravenes free growth of a continuous MAPbI<sub>3</sub> film, increasing lattice distortion and the wall domain effect,<sup>55</sup> whose consequences we will elucidate later. In essence, this reflects one distinguishing property of the resultant devices. For the case of

PSS–Co, a more compact MAPbI<sub>3</sub> layer remains on the composite surface whereas a significant part of the perovskite percolates through, increasing the surface interaction between the functional components in the mesoporous composite and the perovskite layer, which is believed to enhance the piezoelectricity as well as the mechanical properties of the films.<sup>30</sup> Also, for both cases application of UVPT during perovskite deposition enhances their adherence to the underlayer, which is consistent with the postulations by Ahmadian and Eslamian.<sup>53</sup> There was no recognizable peeling off of the films from the substrate after the several cycles of bending during device tests.

## Device performance

To evaluate the mechano-electrical yield potential, standard equipment (Fig. 4a) was employed in which the devices were intermittently bent and relaxed as their energy harvesting potential was being recorded. The perovskite multi-layers (Fig. 4b) based on PPS–Co and SnO<sub>2</sub> NF thin films (with and without SnO<sub>2</sub> NP under layer) were fabricated pursuant to the procedures explained in the Experimental section, then subjected to horizontal bending motions of varying frequencies until the winner devices were identified. In order to ensure that a more homogeneous load is provided to the device active area, the device was fabricated on the mid part of the substrate, leaving equal distances between the device mask taped edge and the attachments to either side of the equipment. 10 devices were tested for each sample set and the average values are accordingly reported. The registered champion output voltages and currents are shown in Fig. 4c and d.

As shown, optimum output voltages of 4.82 V and 1.04 V as well as the direct output currents of ~29.7 nA and 10.32 nA were obtained from the 0.0625 cm<sup>2</sup> device area, respectively, containing the PPS–Co composite film and the SnO<sub>2</sub> NF films (without SnO<sub>2</sub> NP under layer). This high voltage and current generated by the device made on PSS–Co can be attributed to the synergistic contribution of the vertical ultrasonic vibration-induced high electroactive PVDF and PLLA phases, the apparent dipolar interaction between the SnO<sub>2</sub> NFs/MAPbI<sub>3</sub> and a large contact area between PPS–Co and MAPbI<sub>3</sub>, which all resulted in stronger dipoles. As stated earlier, metastable phases of PVDF can convert to  $\beta$ -phases in the vicinity of its border with CH<sub>3</sub>NH<sub>3</sub>PbI<sub>3</sub>, which enhances the piezoelectric potential of the fabricated composite film. When the device is subjected to a bending motion, the electroactive parts of the composite (PLA, and PVDF) and the MAPbI<sub>3</sub> phase undergo dipole relocation and possible ionic migration (strain induced charges), specifically in their domain walls.<sup>11,16,54,56</sup> The electrical charges are released normal to the plane, in which the stress is applied, injected to the circuit, and revealed as a voltage signal.<sup>22,57</sup> Additionally, we postulate that the 1D fibrous SnO<sub>2</sub> in contact with MAPbI<sub>3</sub> and PVDF/PLLA generates an additional polarization by encouraging charge concentration along their surfaces, thus creating charged spaces/voids and consequently electret dipoles. A similar effect was reported in other PVDF–nanofibre

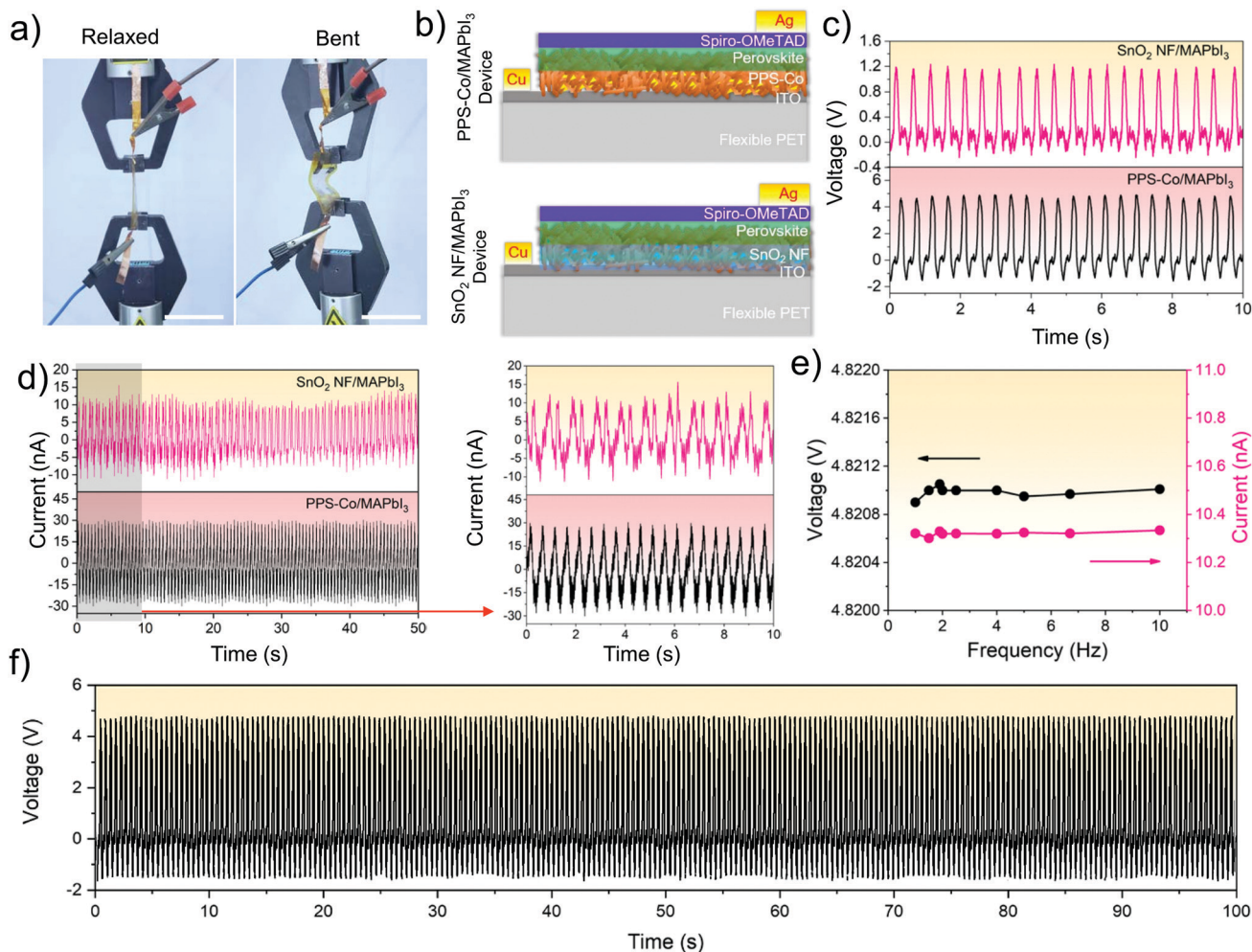


Fig. 4 Variation of output voltage and current of piezoelectric perovskite devices based on PPS-Co and pure SnO<sub>2</sub> NFs, for application of stress over a 10 s time period. (a) Digital images of the device during repetitive bending and release motions generating electrical output (scale bar 3 cm). (b) Schematics showing the layers and nature of stacking in the tested devices (not to scale). (c) Output voltage, and (d) output current, both at a frequency of 2 Hz and the corresponding zoomed-in view of the PPS-Co/MAPbI<sub>3</sub> and SnO<sub>2</sub> NF/MAPbI<sub>3</sub> devices. (e) Variation of output voltage and current with bending frequency of the PPS-Co/MAPbI<sub>3</sub> device. (f) Voltage harvesting stability from PPS-Co/MAPbI<sub>3</sub> for over 100 s at a frequency of 2 Hz.

nanogenerators.<sup>28,39</sup> The same device structure made on pure SnO<sub>2</sub> NF film also generated good output voltage and current (champion device, 1.04 V, and 10.32 nA, as mentioned above). This property most likely arises from the concentration and propagation of space charges due to the presence of MAPbI<sub>3</sub>, as well as lattice distortions which are possible due to the interaction between MAPbI<sub>3</sub> and SnO<sub>2</sub> NFs as seen in Fig. 3c and cross section in Fig. S7b (ESI<sup>†</sup>). Induced lattice defects can pivotally control ionic polarizations culminating in a piezoelectric potential in MAPbI<sub>3</sub>.<sup>55</sup> However, this latter device still performed behind the former made on PSS-Co/MAPbI<sub>3</sub>, owing to the higher polarizability of the composite as stated already. A schematic of the proposed charge generating mechanism in the PPS-Co and SnO<sub>2</sub> NFs is depicted in Fig. S7 (ESI<sup>†</sup>), whereas a comparison of the piezoelectric output from some other related devices is presented in Table 2. Taking notice of the smaller functional area and no extra poling treatment, our device has great output performance.

Fig. 4e shows the variation of output voltage and current with bending frequency. It is seen that as long as the bending angle is maintained, the applied low bending frequencies have no significant effect on the output voltage and current signals, within the testing conditions. It is universal that at low testing frequencies, the dielectric constants of active materials remain constant unless intrigued by other factors like temperature variations, and pressure changes.<sup>22,54</sup> In this study, we determined the dielectric constants at room temperature for the PPS-Co, pure MAPbI<sub>3</sub> and SnO<sub>2</sub> NF layers at 1 kHz as 63.4, 7.6 and 31.8. The higher PPS-Co dielectric constant can be ascribed to the high polarization ability of the composite, which is characterized by both strong dipolar and interfacial polarizations, as explained already.

SnO<sub>2</sub> NFs form a dense network structure that could generate a high space charge concentration, and high dielectric constant,<sup>39</sup> but also have a predictable high dielectric loss due to easy conduction of current (leakage current) and charge trapping.

Table 2 Piezoelectric performance of some MAPbI<sub>3</sub> nanogenerator devices

Composite (electrical poled/unpoled)	Applied force/pressure	Output voltage [V]	Output current/current density	Functional/electrode area [cm <sup>2</sup> ]	Ref.
MAPbI <sub>3</sub> -PVDF (unpoled)	Finger tap	1.8	37.5 [nA]	1 × 1	30
MAPbBr <sub>3</sub> -PVDF	Finger tap	5	60 [nA]	2.4 × 1.5	69
MAPbI <sub>3</sub> -PVDF (poled, drop-casted)	Finger tap (~97.7 μm thickness)	18.5	1.5 [μA]	1 × 1	70
MAPbI <sub>3</sub> -PVDF (poled, spin-coated)	Finger tap (~6 μm thickness)	6.5	0.43 [μA]	1 × 1	70
MASnI <sub>3</sub> -PVDF (poled)	Bending	1.96	0.135 [μA cm <sup>-2</sup> ]	1 × 1	34
SnO <sub>2</sub> NF-MAPbI <sub>3</sub> , 500 nm	0.5 MPa	2.7	0.14 [nA cm <sup>-2</sup> ]	1.6 × 2.5	22
FAPbBr <sub>3</sub> -PDMS (poled)	0.5 MPa	8.5	3.8 [μA cm <sup>-2</sup> ]	1 × 1	71
PVDF-PLLA-SnO <sub>2</sub> NF-MAPbI <sub>3</sub> (unpoled, spin-coated)	Bending	4.82	29.7 [nA]	0.0625 (0.25 × 0.25)	This work
PVDF-PLLA-SnO <sub>2</sub> NF (unpoled, spin-coated)	Bending	2.03	21.8 [nA]	0.0625	This work
SnO <sub>2</sub> NF-MAPbI <sub>3</sub> (unpoled, spin-coated)	Bending	1.02	10.32 [nA]	0.0625	This work

This supports the observation that the PPS-Co generated more piezoelectric output than the SnO<sub>2</sub> NF film device. Dielectric performance is dependent on the rotational dielectric polarization and surface charge polarization.<sup>39</sup> SnO<sub>2</sub> NFs owing to their n-type semiconducting nature have huge interfacial oxygen vacancies that act as donors. Negative oxygen ions and positive oxygen vacancies attract at these interfaces, creating huge dipole moments. This results in a rotational dielectric polarization at the interface on application of a sufficient force/field. Equally, the positive and negative interfacial space charges are attracted to the antagonistic poles of the electric field, where they are trapped resulting in more dipolar activity. These surface charge dipoles are more in these nanomaterials due to higher interfaces and are the major origins of the higher dielectric constant for the SnO<sub>2</sub> NF device. The presence of SnO<sub>2</sub> nanomaterials in the PPS-Co implies added dipolar moments as already stated. This as well distinguishes the high dielectric constant of the PPS-Co compared to that of the SnO<sub>2</sub> NF film. The other dielectric constants determined are revealed in Table S2 (ESI†) and are all in agreement with similar reports.

The stability of output at low frequencies is an indication of the great reliability and prospective deployment of the device for a variety of applications where frequency-dependent fluctuations in output voltages and current could potentially have corresponding detrimental repercussions, for example in medical appliances. This finding rhymes with a related discovery by He *et al.*<sup>56</sup> In addition, a steady output voltage was registered for a longer period from the PPS-Co device, as seen in Fig. 4f over 100 s repetitive bending cycles, which further corroborates the stability of output and endurance of the device against bending. This great mechanical resistance might be rendered from the ultra-flexible PPS-Co net structure which offers the dual function of augmented mechanical robustness and increased electroactive fields. Correspondingly, this agrees with reports that the presence of suitable polymeric phases offers extended operational stability to MAPbI<sub>3</sub> perovskites.<sup>15,58</sup>

To obtain wide-screen knowledge about the stress-to-voltage conversion by the developed perovskite devices, both PPS-Co based and SnO<sub>2</sub> NF based samples were decorated with an additional SnO<sub>2</sub> NP layer, deposited right atop the conductive

flexible electrode (PET/ITO). The major basis for the inclusion of SnO<sub>2</sub> NPs was to enhance the overall dielectric performance, improve underlayer anchorage onto the substrate and prevent probable shunting (as already discussed in previous paragraphs) which has been reported especially for perovskite incorporating devices.<sup>21</sup> The piezoelectric yield and the sheet resistance ( $R_s$ ) of four devices have been compared, in Fig. 5. Each device was tested under lateral bending (Fig. 5a and b). Also, they were subjected to a dark conductivity test (Fig. 5e), and direct normal pressing by a horizontally moving load that delivered an impact force of 0.2 N. The latest test was applied for measurement of the normal dielectric constant ( $d_{33}$ ). Fig. 5a and b show the mechano-electrical output voltage and current registered over 10 minutes from each of the four devices under bending motions. It is interesting to note that the trends of output voltage and current are similar, for all the devices at a uniform bending frequency. The yield order indicates that either in the absence or presence of the SnO<sub>2</sub> NPs the device assembled on PSS-Co outperforms the one on pure SnO<sub>2</sub> NFs. Also, in both PSS-Co and SnO<sub>2</sub> NF devices, the presence of SnO<sub>2</sub> NPs significantly disturbs the time-resolved output voltage and current. We attribute this to the increased number of SnO<sub>2</sub> nanomaterials (Fig. 1a) that might on the contrary lead to growth of a larger leakage current, and excessive MAPbI<sub>3</sub> defects, which work against the required insulating function for higher piezoelectric energy generation. Table 3 shows the optimum voltage and current outputs recorded from each of the devices with distinguished underlayers. For additional disclosure of the effect of the PPS-Co and SnO<sub>2</sub> NP underlayers on the bulk mechano-electrical output of the devices, we explored the electrical output of devices composed of MAPbI<sub>3</sub> on PET/ITO (shown as MAPbI<sub>3</sub> in the table), then one more on PET/ITO/SnO<sub>2</sub> NPs (denoted as SnO<sub>2</sub> NPs in Table 3) when subjected to recurring bending tests. Both voltage and current outputs recorded from the device on PPS-Co (without SnO<sub>2</sub> NPs) give the highest values (4.82 V, and 29.7 nA) amongst all. On the other side, the control samples in which perovskite was grown on PET/ITO/SnO<sub>2</sub> produced the lowest voltage (0.143 V), 60.8% drop than that prepared on PET/ITO only (0.23 V). These results perfectly support the above-mentioned analysis and theories, and finally the idea behind this research.



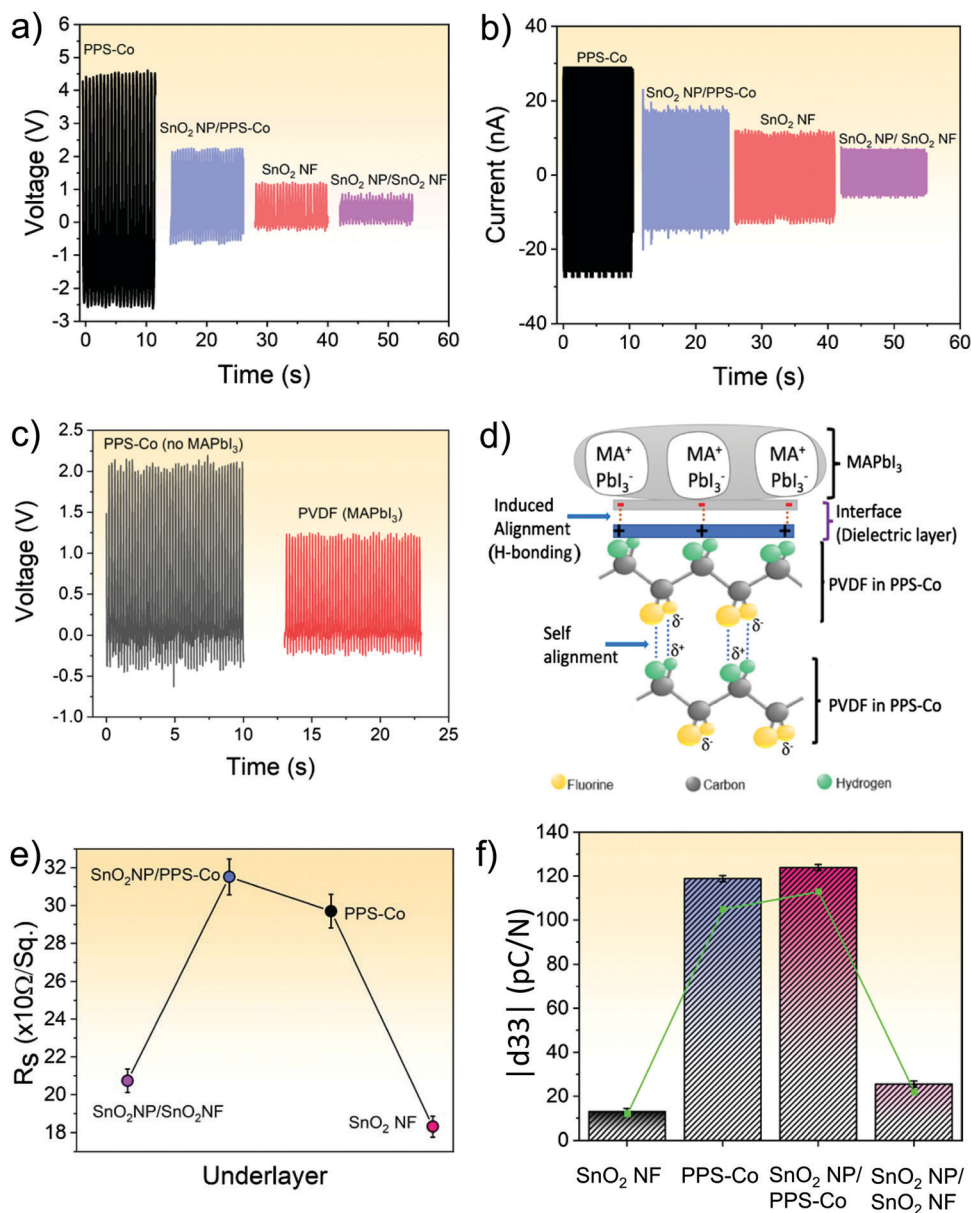


Fig. 5 Comparison of mechano-electrical output of devices, containing different underlayers exposed to repeat bending (compression): (a) output voltage, and (b) current. (c) Output voltage of the PPS-Co and PVDF films prepared by UVPT but without MAPbI<sub>3</sub> perovskite. (d) A schematic diagram showing the interaction between MAPbI<sub>3</sub> and PVDF. (e) Sheet resistance values measured for the different underlayers. (f) Piezoelectric strain constants ( $d_{33}$ ) of CH<sub>3</sub>NH<sub>3</sub>PbI<sub>3</sub> grown on various underlayers: SnO<sub>2</sub> NFs, PPS-Co, SnO<sub>2</sub> NP/PPS-Co, and SnO<sub>2</sub> NP/SnO<sub>2</sub> NFs, measured by the direct method and by piezometer (green line graph).

In order to confirm the effect of both compositing and introduction of MAPbI<sub>3</sub> to the device, the output voltages obtained from a pristine PVDF film as well as PPS-Co composite without MAPbI<sub>3</sub> are shown in Fig. 5c. Both films were prepared using UVPT processes and subjected to the same bending test. Voltage outputs of 1.24 V and 2.03 V, respectively, were obtained as revealed by the wave forms. It is seen that although the PPS-Co without MAPbI<sub>3</sub> generated high voltage, this still lags behind the values generated from PPS-Co devices incorporating the perovskite. Therefore, compositing with PLLA, UVPT and addition of MAPbI<sub>3</sub> provided a synergistic basis for the

greater performance of the composite. The suggested mechanism by which MAPbI<sub>3</sub> enhances and improves the  $\beta$ -phase content of PVDF is schematically illustrated in Fig. 5d, as earlier explained.

The electrical output of the device is greatly influenced by the electrical properties of each layer and their interfaces. Therefore, for each device we surveyed the dark-mode sheet resistance ( $R_s$ ) values, in straight status (without stress), as represented in Fig. 5e. Devices possessing SnO<sub>2</sub> NPs show higher overall sheet resistance values than those without. Additionally, the sheet resistances of the composite films are higher than those of the corresponding bare SnO<sub>2</sub> NF films.



**Table 3** The voltage and current outputs registered for four devices in which perovskite was grown on different underjunctions, as well as the results of the control devices

Underjunction	Output voltage [V]	Standard deviation	Output current [nA]	Standard deviation
PPS-Co	4.82	0.15	29.70	1.75
SnO <sub>2</sub> NP/PPS-Co	2.29	0.11	16.79	1.94
SnO <sub>2</sub> NFs	1.04	0.04	10.32	1.52
SnO <sub>2</sub> NP/SnO <sub>2</sub> NFs	0.6	0.05	6.78	0.34
None (only MAPbI <sub>3</sub> )	0.23	0.08	8.32	0.72
SnO <sub>2</sub> NPs	0.143	0.043	5.24	0.28

These sheet resistance values follow the trend: SnO<sub>2</sub> NP/PPS-Co > SnO<sub>2</sub> NP/SnO<sub>2</sub> NFs and PPS-Co > SnO<sub>2</sub> NFs. From the relationship,  $R_s = \frac{\rho}{t}$  where  $R_s$  is sheet resistance ( $\Omega \text{ sq}^{-1}$ ),  $\rho$  is electrical resistivity, an intrinsic property of the material, and  $t$  is film thickness, it can be concluded that in a similar materials system, a thicker film induces a higher series electrical resistivity to the system. However, an ultra-thin film like the SnO<sub>2</sub> NPs applied in the present study ( $\approx 30 \text{ nm}$ ), might possess plenty of pin-holes and defects in the crystalline lattice, particularly since it was made by solution processing. Defective structures of SnO<sub>2</sub> NP films constrain the mobility of the electrons and free charges, and consequently disturb the polarization performance of the whole device. As well, subjected to a lateral stress, an additional layer, especially of a metal oxide (*e.g.* of the SnO<sub>2</sub> NPs in this work) can decrease the maximum potential bending radii for the whole device, and mitigate polarization due to strain. On the other hand, the sheet resistivity of the PPS-Co is higher than that of corresponding SnO<sub>2</sub> NFs, with or without the ultrathin SnO<sub>2</sub> NPs. Back to the theoretical expression ( $R_s = \frac{\rho}{t}$ ), this might be due to the intrinsic high resistivity of the polymer matrix and the discontinuous (net-like) structure of the composite (Fig. 2a), which make it a better dielectric, leading to higher stress-driven voltage and current outputs as seen from the trend in Fig. 5a and b (and in Table 3).

In a further survey, we determined the piezoelectric strain constant,  $d_{33}$ , for the perovskite films grown on the four distinctive junctions (PPS-Co, SnO<sub>2</sub> NP/PPS-Co, SnO<sub>2</sub> NFs, and SnO<sub>2</sub> NP/SnO<sub>2</sub> NFs), from eqn (4).<sup>59</sup>

$$q = d_{33}F \quad (4)$$

where  $q$  is the charge magnitude,  $d_{33}$  is the piezoelectric strain constant and  $F$  is the applied mechanical force. We obtained the average charge magnitude from the time resolved data measured by the high input resistance electrical analyzer (Keithley-6517) in charge mode, when the devices were repetitively pressed and released (normal stress-release) at a constant frequency by a loading force of 0.2 N. The  $d_{33}$  values are represented in Fig. 5f. This method derives the  $d_{33}$  from first principal data. Whereas piezoresponsive force microscopy (PFM) measurements have been used to determine the  $d_{33}$  values, it is not recommended especially for very thin and

highly flexible films and substrates. Difficulty in applying a uniform local electric field, the anonymous substrate bending effect and the possible ionic lattice distortions caused by applied electrical bias at the tip of the PFM probe are the most cited negatives.<sup>59,60</sup> Related experimental works and reports have shown our method to give good repeatability of measurements and an accuracy of findings.<sup>59</sup> The PPS-Co composite films show higher  $d_{33}$  values compared to those of SnO<sub>2</sub> NFs. SnO<sub>2</sub> NP/PPS-Co showed a  $d_{33}$  value of  $123.93 \text{ pC N}^{-1}$ , slightly superior to the one without SnO<sub>2</sub> NPs with  $d_{33}$  of  $118.85 \text{ pC N}^{-1}$ . These values are some of the highest ever recorded for a PVDF-MAPbI<sub>3</sub> containing thin film and are en route to the theoretical maximum possible estimated value of  $186.3 \text{ pC N}^{-1}$  (for PVDF).<sup>28,61</sup>

To credit and quantify the obtained  $d_{33}$  values, we also tested the films using a commercial Berlincourt piezometer (Piezotest P300). The samples were mounted on the meter and intermittently pressed by the meter's top head producing a direct reading.<sup>59</sup> The resultant  $d_{33}$  values for the PPS-Co/MAPbI<sub>3</sub> under clamping with and without SnO<sub>2</sub> NPs were *ca.* 113 and  $105 \text{ pC N}^{-1}$ , respectively. These are closer to those obtained using the first technique, and reveal the high piezoelectric potential of the devices. Fig. 5f includes some recorded  $d_{33}$  values using the piezometer. Additionally, PPS-Co/MAPbI<sub>3</sub> was prepared on glass/ITO substrates and measured by the piezometer. Maximum  $d_{33}$  values of  $\sim 109$  and  $103 \text{ pC N}^{-1}$  (respectively, with and without SnO<sub>2</sub> NPs) are well in synch with those obtained using PET/ITO substrates. Therefore, we believe that the obtained results arise from the greatly enhanced piezoelectric potential of our composites and there was no significant contribution from the triboelectric charge generation or other similar phenomena arising from nanopatterning as reported for some PET containing films.<sup>62</sup> A comparison of effective  $d_{33}$  values obtained for various PVDF containing energy generators is displayed in Fig. 6. These outstanding values are ascribed to the synergistic internal piezoelectric contribution of the three components (particularly the intrinsic  $d_{33}$  of PVDF is  $-31.5 \text{ pC N}^{-1}$ , though the theoretical maximum is predicted at *ca.*  $-186 \text{ pC N}^{-1}$ ),<sup>28</sup> the large polar phases and strong dipole moments due to coexistence of SnO<sub>2</sub> NFs, PLLA,  $\beta$ -PVDF, and MAPbI<sub>3</sub>. There is potential accumulation of charged dipoles at the SnO<sub>2</sub> NF surfaces that could link to form charged-pores and electret dipoles between the nanofibers (space charges).<sup>63</sup> Furthermore, the highly directional dipoles and more uniform distribution of components in the composite matrix, which are all enhanced by vertical ultrasonic vibration,<sup>13,36,64</sup> are the most important rationales for the desired mechano-electrical response of these devices. SnO<sub>2</sub> NP/SnO<sub>2</sub> NF/MAPbI<sub>3</sub> and SnO<sub>2</sub> NF/MAPbI<sub>3</sub> films show lower  $d_{33}$  values of  $25.56 \text{ pC N}^{-1}$  and  $17.02 \text{ pC N}^{-1}$ , respectively. Moreover, it is seen that in both composite and NF based devices, the presence of the ultrathin SnO<sub>2</sub> NP underlayer slightly favors the normal piezoelectric strain constant ( $d_{33}$ ). Supported by eqn (4), we inferred that the SnO<sub>2</sub> NP ultrathin film assists the charge displacement along the thickness of the device. In summary, the favorite architecture of the perovskite

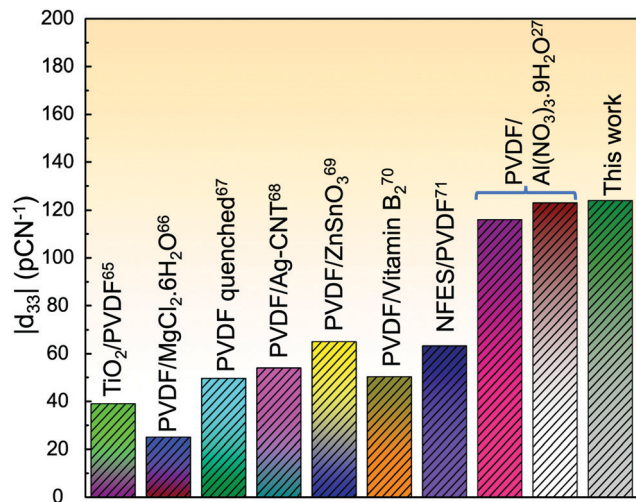


Fig. 6 Comparison of the various effective piezoelectric strain coefficients,  $d_{33}$  of PVDF reported after modification using different approaches.

piezoelectric device is practically dependent on direction of applied forces. Fig. S8 (ESI<sup>†</sup>) shows the waveforms of output voltages and currents consequential to direct press-release on the top surface and under rhythmic bending of the control samples. The  $d_{33}$  values obtained from the control films having MAPbI<sub>3</sub> grown on SnO<sub>2</sub> NPs and PET/ITO, are, respectively, 16.44 pC N<sup>-1</sup> and 13.48 pC N<sup>-1</sup>. Thus, the presence of the SnO<sub>2</sub> NPs enhances the effective  $d_{33}$  value, in accordance with the explanation stated herein before.

We believe that in the case of stretching, the geometry of the net-like structure of the composite and consequently the interfacial phenomena between the PPS-Co/MAPbI<sub>3</sub> would markedly change, presenting important alterations in the general device performance. This is an interesting approach for consideration in subsequent works. Also, owing to the high sheet resistance values ( $R_s$ ) of the PPS-Co composite, a tradeoff between the mechano-electric and photovoltaic functions would materialize following a standard photovoltaic test.

## Conclusions

To expand the application scope of MAPbI<sub>3</sub> perovskite centered devices beyond photovoltaic functions, we innovatively fabricated devices based on both thin PVDF/PLLA/SnO<sub>2</sub> NF composites (PPS-Co) and SnO<sub>2</sub> nanofibrous membranes. The assembly process involved instant vertical ultrasonic vibration of the wet films after spin coating. This vertical displacement induced by ultrasonic fields reduces/eliminates the need for a post-annealing process (which is thus economical) and interestingly boosted the transformation of the electroactive PVDF phase content of the composite by a significant 57.72%. The polar phase contents  $\beta$  and  $\gamma$  individually rose by 80.61% and 32.44%, respectively. We also contend that the synergy between MAPbI<sub>3</sub> and PPS-Co increased the output performance by creating strong interfacial dipoles with the PPS-Co composite (increased polar  $\beta$ -phase content of PVDF). Additionally, there

was an induced transformation of poly(L-lactic acid) from the  $\alpha$ - to the looser  $\beta$ -phase as deduced from XRD studies, a factor that presumably enhances the flexibility and thus mechanical performance of the device. The high surface area 1D SnO<sub>2</sub> NFs in the composite connected the two polymers to form a more desirable flexible net-like structure. This resulted in an amplified mechano-electrical output without extra poling. Output performance of different thin film devices was examined through bending and then application of direct press-release forces onto the device's top surface. Some intrinsic factors that affect the performance of the device *vis-à-vis* its mechano-electrical output such as sheet resistivity and dielectric permittivity have been traced. Generally, both devices with high sheet/film resistances and dielectric constants produced higher output voltages and *vice versa*. Our special PPS-Co composite, produced an average voltage of 4.82 V from an area of 0.0625 cm<sup>2</sup> and a large efficient piezoelectric strain constant,  $d_{33}$  between 118.85 pC N<sup>-1</sup> and 123.93 pC N<sup>-1</sup>, depending on the underjunction layer. We envisage the near-future realization of less than 1 cm<sup>2</sup> light-independent MAPbI<sub>3</sub> products for various mechano-electrical processes including in energy harvesters and transducers or for integrated piezo/photo-electric systems.

## Experimental

### Materials

*N,N*-Dimethylformamide (DMF,  $\geq 99.8\%$ , Sigma-Aldrich), isopropyl alcohol (IPA), ethanol (analytical grade), acetone, dimethyl sulfoxide (DMSO), poly(vinyl pyrrolidone) (PVP), tin (ii) chloride dihydrate (SnCl<sub>2</sub>·2H<sub>2</sub>O,  $\geq 98\%$ , Sigma-Aldrich), PVDF ( $M_w$  ca. 275 000 g mol<sup>-1</sup>) and PLLA pellets (nominal size  $\approx 5$  mm), methyl ammonium iodide (MAI) and lead iodide (PbI<sub>2</sub>) were used in the material synthesis as received from chemical suppliers without additional refinement, unless otherwise stated. Only commercially patterned PET/ITO substrates (0.05 mm thickness, 6  $\Omega$  sq<sup>-1</sup>) were used in all cases without any pre-treatment.

### SnO<sub>2</sub> nano-fiber membrane (NF) preparation

SnO<sub>2</sub> nanofibers were prepared by electrospinning. The precursor solution was made of SnCl<sub>2</sub>·2H<sub>2</sub>O (0.7 g) and PVP (0.4 g) in 6 mL of DMF and ethanol (1:1). For the electrospinning process a stainless-steel capillary needle connected to a 10 mL syringe was used to eject the solution under a 15 kV direct electrical voltage, while the injection system was set to provide a 5.33  $\mu$ L min<sup>-1</sup> flow rate. A sample collection rotor was placed 12 cm horizontally from the needle nozzle tip. After continuous spinning, the as-electrospun nanofiber mat was heated in a furnace for 4 hours at 600 °C to eliminate the organic components and enhance nucleation of SnO<sub>2</sub> nanocrystals. SnO<sub>2</sub> nanofibres were dispersed in acetone (1% w/v), stirred overnight and dispensed on substrates (PET/ITO or PET/ITO/SnO<sub>2</sub> NP) with spinning at 2500 rpm for 40 s, before being subjected to UVPT for 4 minutes at a constant power of 5 W,

as adapted from ref. 65 and 66. Briefly, for the UVPT process, the wet-spun samples were immediately placed atop a vibrating steel box inside which a Langevin transducer was installed. The transducer is actuated by a signal generator, operating at 40 kHz and 5 W, generating a maximum vertical displacement of 4 nm on the surface of the steel box. Finally, the sample was heated on a hotplate at 80 °C for 2 hours. Before deposition of any layers, the edges of the PET/ITO substrate were masked with tape so as to protect the electrode and prevent possible short circuits during device testing.

### SnO<sub>2</sub> nanoparticle (NP) layer fabrication

SnCl<sub>2</sub>·2H<sub>2</sub>O was dissolved in IPA (0.01 mol L<sup>-1</sup>, 98%) stirred for 1 hour, aged for 6 hours at room temperature, and subjected to spin coating on PET/ITO substrates at 4000 rpm for 30 s to enable completion of the sol-gel process. The formed gel films were then heated for 30 s at 120 °C, and cooled down, to form a SnO<sub>2</sub> NP foundation structure.

### PVDF/PLLA/SnO<sub>2</sub> composite film preparation

12% w/v solutions of each of PVDF and PLLA (L-enantiomer of the PLA) in acetone were magnetically stirred for 2 hours on a hot plate at 65 °C to dissolve. The SnO<sub>2</sub> NF dispersion (as prepared above) was added to the polymeric mixture, in a ternary ratio of 2 : 1 : 4 (PVDF : PLLA : SnO<sub>2</sub> NF) and continuously stirred for 4 hours until a uniform composite mixture was obtained. The composite was spin-coated on PET/ITO or PET/ITO/SnO<sub>2</sub> NPs at 2500 rpm for 30 s followed by UVPT for 2 minutes at 5 W, then annealing for 1 hours at 80 °C. The annealed films were finally quenched in ice for 30 minutes, giving PVDF/PLLA/SnO<sub>2</sub> NF composites (PPS-Co).

### Perovskite layer deposition

The MAPbI<sub>3</sub> perovskite film was also prepared using single step solution deposition, followed by UVPT as mentioned above. Precisely, 158.9 mg MAI and 461 mg PbI<sub>2</sub> were dissolved in a 1 mL solvent mixture of DMF and DMSO (4 : 1, respectively), and magnetically stirred overnight at 60 °C. 100 μL volumes were spin coated at 4000 rpm for 20 s on PPS-Co or SnO<sub>2</sub> NF films (on PET/ITO or PET/ITO/SnO<sub>2</sub> NPs for the control samples), followed by immediate UVPT treatment of the wet films at 2.5 W for 1 minute. The films were finally annealed at 100 °C for 10 minutes conferring a dark perovskite layer onto each surface.

### Device fabrication

A thin layer of 2,2',7,7'-tetrakis-(*N,N*-di-4-methoxy phenylamino)-9,9',9'-spirobifluorene (spiro-OMeTAD) was cast on top of the perovskite, following the procedure adapted from ref. 67. Spiro-OMeTAD has the ability to act as a dielectric<sup>68</sup> with a dielectric constant of ~3 for a 400 nm thin film. After settling for 12 hours, a silver layer (counter electrodes) was coated using a patterned paper mask. The device was then covered with a thin layer of polydimethylsiloxane (PDMS) to complete its fabrication. PDMS was envisaged to offer protection to the device layers while spiro-OMeTAD additionally abates surface

reaction between the Ag electrode deposit and the perovskite film. The proceeding deposition steps of MAPbI<sub>3</sub> perovskite, spiro-OMeTAD and silver layers were all carried out in a customized glove box under N<sub>2</sub> atmosphere. The intersection of the coated Ag with ITO formed the active area of the device. Four silver contacts each of area *ca.* 0.0625 cm<sup>2</sup> were deposited on every top layer.

### Material characterization

Surface morphology of the films was observed by field emission scanning electron microscopy (FE-SEM) arrayed with energy dispersive X-ray diffraction (EDS). A Shimadzu XRD 6000 diffractometer with Ni filtered Cu K $\alpha$  radiation ( $\lambda = 0.15406$  nm),  $2\theta$  ranging between 10° to 60°, was employed for the structural characterization. Fourier-transform infrared (FTIR, a Nicolet™ 6700, 4000–400 cm<sup>-1</sup> range system) in attenuated total reflection (ATR) mode and Raman (Renishaw inVia micro-Raman Spectrometer, England, 514 nm argon ion laser) spectra were recorded, in order to predict the chemical interactions of materials within the PPS-Co composite system.

### Device testing

The electrical output of the device was measured over time by a Keithley 6517 electrical probe station which was linked to the device *via* connective wires. The equipment is powered by an electric motor and produces lateral motions of varying frequency values between two adjacent bars (one fixed and one movable). During bending tests, the device was taped between the two adjacent bars of maximum separation 3.0 cm, and the movable bar periodically pushed the device through 2.5 cm towards the fixed bar and back at a constant frequency for a definite time period. For tests across the thickness (also termed normal load method here), the device was taped onto the fixed bar and periodically pressed by the lateral impacts of the movable bar. Throughout each set of experiments, the maximum separation between the bars was maintained. For piezometer (Berlincourt meter) measurements, results were read off directly and average values recorded. Sheet resistance values of the underlayer films were measured using a Jandel-4 four-point probe analyzer.

### Conflicts of interest

There are no conflicts to declare.

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