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Low-cost microarray thin-film electrodes with ionic liquid gel-polymer electrolytes for miniaturised oxygen sensing

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A robust, miniaturised electrochemical gas sensor for oxygen (O_2) has been constructed using a commercially available Pt microarray thin-film electrode (MATFE) with a gellified electrolyte containing the room temperature ionic liquid (RTIL) 1-ethyl-3-methylimidazolium bis(trifluoromethylsulfonyl)imide ([C_2mim][NTf_2]) and poly(methyl methacrylate) (PMMA) in a 50 : 50 mass ratio. Diffusion coefficients and solubilities for oxygen in mixtures of PMMA/RTIL at different PMMA doping concentrations (0–50% mass) were derived from potential step chronoamperometry (PSCA) on a Pt microdisk electrode. The MATFE was then used with both the neat RTIL and 50% (by mass) PMMA/RTIL gel, to study the analytical behavior over a wide concentration range (0.1 to 100 vol% O_2). Cyclic voltammetry (CV) and long-term chronoamperometry (LTCA) techniques were employed and it was determined that the gentler CV technique is better at higher O_2 concentrations (above 60 vol%), but LTCA is more reliable and accurate at lower concentrations (especially below 0.5% O_2). In particular, there was much less potential shifting (from the unstable Pt quasi-reference electrode) evident in the 50% PMMA/RTIL gel than in the neat RTIL, making this a much more suitable electrolyte for long-term continuous oxygen monitoring. The mass production and low-cost of the electrode array, along with the minimal amounts of RTIL/PMMA required, make this a viable sensing device for oxygen detection on a bulk scale in a wide range of environmental conditions.

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1. Introduction

The detection and monitoring of gases is important for industrial, medicinal, security and health and safety applications.[1] Various techniques are used to detect gases, but those based on electrochemical methods are often the most widely employed.[1] Amperometric gas sensors (AGSs) based on "Clark electrodes" have been around for several decades and are available to purchase commercially from a range of companies.[2] They typically consist of three electrodes connected by an electrolyte (usually water/H_2SO_4 mixture) and covered by a gas permeable membrane.[1–3] Room temperature ionic liquids (RTILs) have been investigated significantly as a replacement solvent in AGSs due to their non-volatile nature (eliminating the need for a membrane),[3] in addition to other advantageous properties such as wide electrochemical windows, good intrinsic conductivity, good solvating abilities and high chemical and thermal stability.[4–7] A number of reviews on gas sensing in RTILs are available.[2,8–11]

The gas that appears to be the most widely investigated in RTILs so far is oxygen (O_2).[11] Various studies on oxygen reduction in RTILs have used microdisc electrodes for the obvious advantages of higher current densities and lower ohmic drop effects.[12–16] From an analytical point of view, employing an array of microdiscs can increase currents, whilst maintaining the benefits of a single microelectrode.[17] However, due to the relatively expensive fabrication processes, there have only been limited investigations with microelectrode arrays, particularly for gas sensing in RTILs. Huang *et al.*[18] proposed a membrane-free oxygen gas sensor consisting of a thin layer of the RTIL tris(*n*-hexyl)tetradecylphosphonium trifluorotris(pentafluoroethyl)phosphate ([$P_{14,6,6,6}$][FAP]) dropcast onto an electrode array with 80 microdiscs in a square pattern (10 by 8). The microdiscs were patterned by photolithography onto a silicon wafer, and were 12 μm in diameter, recessed by *ca.* 1.6 μm and separated by 150 μm (centre-to-centre distance). Oxygen concentrations from 2–13 vol% O_2 were studied, and linear calibration graphs were obtained (current *vs.* vol% O_2) from continuous cyclic voltammograms. However, concentrations of O_2 higher than 13 vol% were not investigated. The electrolyte was also a pure RTIL in the liquid state, so there are limitations on how such a "membrane-free" electrode can be employed in certain situations *e.g.* movement,

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shaking or tilting of the electrode, where loss of the RTIL might occur.

To overcome this, in our recent work,[19] we mixed a pure RTIL with increasing amounts of poly(methyl methacrylate) (PMMA) to make a gel polymer electrolyte (GPE) that is mechanically stable (*i.e.* does not flow). At 50% mass of PMMA relative to the total mass (PMMA and RTIL), defined as 50% $m_{PMMA}/m_{Tot.}$ GPE, no electrolyte flow was evident. Oxygen reduction currents on 1 mm diameter Pt thin film electrodes (TFEs) were linear *vs.* concentration over the range 10–100 vol% O_2 using cyclic voltammetry (CV), but suffered from some ohmic drop effects on the macro-sized electrode. The robustness of the electrode was demonstrated by the observation of identical CVs on the electrode at different geometries (*e.g.* upright, sideways, upside down), whereas CVs in the neat RTIL were significantly altered.[19]

In this work, we have employed the same GPE with a Pt microarray thin film electrode (MATFE) as a robust sensor for long-term continuous monitoring of oxygen. The microarray TFE has obvious advantages over the TFE, such as higher current density and lower ohmic drop contributions. Importantly, the MATFEs are commercially available, mass produced and low cost (just over 4 EURO per device), making the possibility of commercializing such oxygen sensors highly favourable. The results will show that good analytical responses can be obtained on these devices, and that more stable and reproducible results are obtained in the GPE compared to the neat RTIL. Ultimately, these cheap, robust, miniaturised electrodes, when used in conjunction with a layer of PMMA–RTIL GPE, could be employed in a range of applications for oxygen monitoring, even at high O_2 concentrations and while being subjected to agitation, acceleration or positioned at different orientations during operation.

2. Experimental

2.1 Chemical reagents

The RTIL 1-ethyl-3-methylimidazolium bis(trifluoromethylsulfonyl)imide ($[C_2mim][NTf_2]$) was purchased from Merck (Kilsyth, Vic, Australia) at ultra-high purity electrochemical grade, and used as received. Poly(methyl methacrylate) (PMMA, average MW *ca.* 15 000, Sigma-Aldrich Pty Ltd, NSW, Australia), tetra-*N*-butylammonium perchlorate (TBAP, >99.0%, Sigma-Aldrich) and ferrocene (Fc, 98%, Sigma-Aldrich) were also used as received. Acetone (≥99.9%, Sigma-Aldrich), acetonitrile (MeCN, 99.8%, Sigma-Aldrich), ethanol (EtOH, Sigma-Aldrich, 99%), and ultrapure water (with a resistivity of 18.5 MΩ cm prepared by a Milli-Q laboratory water purification system (Millipore Pty Ltd, North Ryde, NSW, Australia) were used for rinsing the microdisk electrode after polishing. High-purity oxygen gas (O_2, >99.5%) and high-purity nitrogen gas (N_2, 99.99%) were purchased from BOC gases (North Ryde, NSW, Australia). Aqueous solutions of 0.5 M sulfuric acid (H_2SO_4, 95–98 wt%, Ajax Finechem, WA, Australia) for activating electrodes were prepared in ultrapure water.

2.2 Preparation of gel polymer electrolytes

For the platinum microdisk electrode experiments, mixtures of PMMA–$[C_2mim][NTf_2]$ (10–50% $m_{PMMA}/m_{Tot.}$) were prepared using acetone as a carrier solvent, following the procedure detailed in our previous work.[19] 30 μL of neat RTIL or PMMA–RTIL mixture (in acetone, see explanation below) was employed, giving an estimated electrolyte thickness above the electrode of *ca.* 1.5 mm. This was the minimum volume required to ensure good connection of the working electrode with the Ag wire counter/reference electrode at all PMMA doping concentrations. For the Pt microarray thin-film electrodes (MATFEs) the 50% $m_{PMMA}/m_{Tot.}$ mixture was prepared in the same way. 5 μL of neat $[C_2mim][NTf_2]$ or 50% $m_{PMMA}/m_{Tot.}$ GPE (in acetone, see below) was dropcast to cover the three electrodes (working, counter and reference). Thicknesses of *ca.* 1 mm (for neat $[C_2mim][NTf_2]$) and *ca.* 0.5 mm (for 50% $m_{PMMA}/m_{Tot.}$ GPE) was estimated based on the volume and spread of the droplet. However, it is noted that the thickness is likely to vary over the layer due to meniscus formation. Note: acetone was added to the 50% $m_{PMMA}/m_{Tot.}$ mixture in a ratio of 4 : 1 GPE : acetone (*i.e.* 20% acetone) in order to be able to dropcast the GPE by pipetting for both the microelectrode and TFE experiments.

2.3 Electrochemical experiments

All electrochemical experiments were performed using a PGSTAT101 potentiostat (Eco-Chemie, Netherlands) interfaced to a PC with NOVA 1.11.2 software. All experiments were carried out inside a custom-made aluminium Faraday cage to reduce ambient electromagnetic interferences, and at temperatures of 294 ± 1 K. A step potential of 2.5 mV and a scan rate of 10 mV s^{-1} was used. Chronoamperometric transients on the microdisk electrode employed a sampling time of 0.01 s. Long-term chronoamperometry (LTCA) measurements were conducted with a sampling interval time of 2.5 s.

The platinum microdisk electrode (radius = 7.44 μm) was kindly made and donated by the group of Professor Richard Compton, University of Oxford, UK. It was polished on soft lapping pads (Buehler, Illinois) in a Figure-8 motion, using alumina powder of decreasing size (3, 1 and 0.5 μm). A micropipette tip (Eppendorf, Australia) was fit at the top of the working electrode to hold the electrolyte (30 μL of neat RTIL or PMMA–RTIL mixture). The electrode was housed in a glass T-cell with a silver wire as a combined reference/counter electrode. The electrolyte was left under a N_2 environment overnight to allow any O_2 and other absorbed gases to be purged, and for any acetone to volatilize before the electrochemical measurements were commenced. After the introduction of O_2 gas, cyclic voltammetry (CV) was conducted at 5-minute intervals to ensure that the gas was fully saturated and that the CVs were stable. *Ca.* 20 minutes was sufficient to saturate 30 μL of neat $[C_2mim][NTf_2]$. However, more than 1 hour was required for the 50% $m_{PMMA}/m_{Tot.}$ mixture, probably due to the slower diffusion of O_2 in the viscous mixture. After experiments, the microdisk electrode was soaked and washed with acetone (to

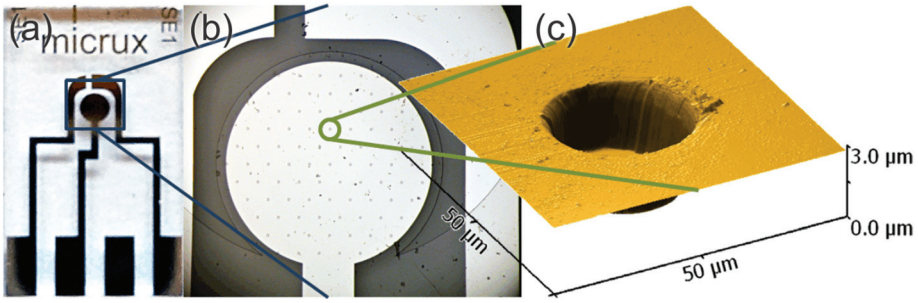

Fig. 1 (a) Photo of the thin-film microarray electrode, (b) optical microscope image of the platinum working electrode, consisting of a platinum disk electrode ($Ø_{Pt\text{-}disk}$ = 1 mm) covered by a (3.0 ± 0.5 µm thick) SU-8 layer and defined by 90 microholes ($Ø_{\mu\text{-}hole}$ = 10 µm, pitch = 100 µm), (c) atomic force microscopy (AFM) mapping of a working electrode microhole.

remove the GPE), re-polished, then rinsed with ethanol and acetone before subsequent experiments.

Platinum microarray thin-film electrodes (MATFEs) (MicruX Technologies, Oviedo, Spain; ED-mSE-10-Pt) were electrochemically activated by cycling for 30 cycles in 0.5 M H_2SO_4 between −0.75 V and 1.25 V. The MATFE has all three Pt electrodes (working, reference and counter) fabricated by thin-film technology and contained within a small area on the glass substrate. The working electrode array consists of 90 recessed Pt disk electrodes in a hexagonal arrangement, 10 µm in diameter with 100 µm between adjacent microholes (see a photo of the device in Fig. 1a, an optical image of the microholes in Fig. 1b and depth profile in Fig. 1c). According to the manufacturer, a layer of SU-8 resin (3.0 ± 0.5 µm thick) is used to define the array. Depth profiles (from atomic force microscopy experiments) from more than five different MATFEs confirmed this thickness, with values between 2.6 and 3.4 µm observed. The thickness was consistent over the whole array for an individual device. 5 µL of either the neat RTIL or 50% $m_{PMMA}/m_{Tot.}$ mixture (plus acetone carrier solvent) was used to cover the working, counter and reference electrodes, before the device was inserted using a rubber bung into a modified glass cell, as described previously.[20] It was flushed with N_2 for a sufficiently long time (*ca*. 1–2 hours in the neat RTIL and overnight in the 50% $m_{PMMA}/m_{Tot.}$ mixture) to remove oxygen and to allow the remaining acetone to volatilize, until stable baselines were obtained. Aluminium wires were soldered onto the electrode connections to allow easy attachment to the potentiostat.

2.4 Gas mixing experiments

Oxygen gas was diluted with nitrogen gas using a gas mixing system detailed in our previous work,[20] based on the ratios of flow rates in the two digital flow meters. Two O_2 concentration ranges were employed in this work, termed "low concentration" (1–20 vol% O_2 for CV and 0.1–20 vol% O_2 for LTCA) and "high concentration" (10–100 vol% O_2 for CV and 1.1–100 vol% O_2 for LTCA). For experiments within the "low concentration" range, the N_2 flow rate was fixed at 180 sccm, and the O_2 flow rate varied. For the "high concentration" range, the N_2 flow rate was fixed at 1000 sccm, while varying the O_2 flow rate. For LTCA, the initial response was allowed to stabilize (under N_2) for *ca.* 30 min before commencing with the introduction of O_2 gas. Adjusting of the flow rates was automated using a computer software controller for the LTCA experiments since the duration of the measurements was *ca.* 14 and up to 35 hours.

3. Results and discussion

The aim of this work is to investigate the electroanalytical behavior of O_2 in a gel polymer electrolyte (GPE) on a commercially available MATFE, as a simple, robust, inexpensive, miniaturized platform for oxygen sensing. The RTIL [C_2mim][NTf_2] was chosen as the solvent as it mixes well with PMMA, and the behavior of O_2 in the mixture has been well characterized in our previous work.[19] The electroanalytical behavior on the MATFE in the neat RTIL and the 50% $m_{PMMA}/m_{Tot.}$ gel polymer electrolyte (GPE) will be investigated. However, in order to obtain information about the physical properties (*e.g.* diffusion coefficient and solubility) of oxygen in the GPE PMMA–RTIL mixtures, the reduction of oxygen will first be studied on a conventional microdisk electrode in PMMA–RTIL mixtures, where the two parameters can be easily resolved from theoretical modeling of the data.[21]

3.1 Diffusion coefficient and solubility values in PMMA–[C_2mim][NTf_2] mixtures

Fig. 2a shows linear sweep voltammetry (LSV) for the reduction of 100 vol% O_2 on a Pt microdisk electrode (diameter 14.88 µm) with various percentages of PMMA mixed with the RTIL. As was observed in our previous work with a working Pt thin film electrode (TFE, 1 mm diameter),[19] the current decreases as the amount of PMMA in the mixture is increased. This is expected due to the higher viscosity of the mixture leading to slower diffusion coefficients of O_2. The shape of the voltammammetry (where a true steady-state plateau is not obtained) is quite similar to that reported by Huang *et al.*[13] in various ionic liquids on a Pt microdisk electrode at similar scan rates (50 mV s^{-1}, lower scan rates were not investigated). Due to the nature of the Ag wire reference electrode, some potential shifting (of up to a few hundred millivolts) was

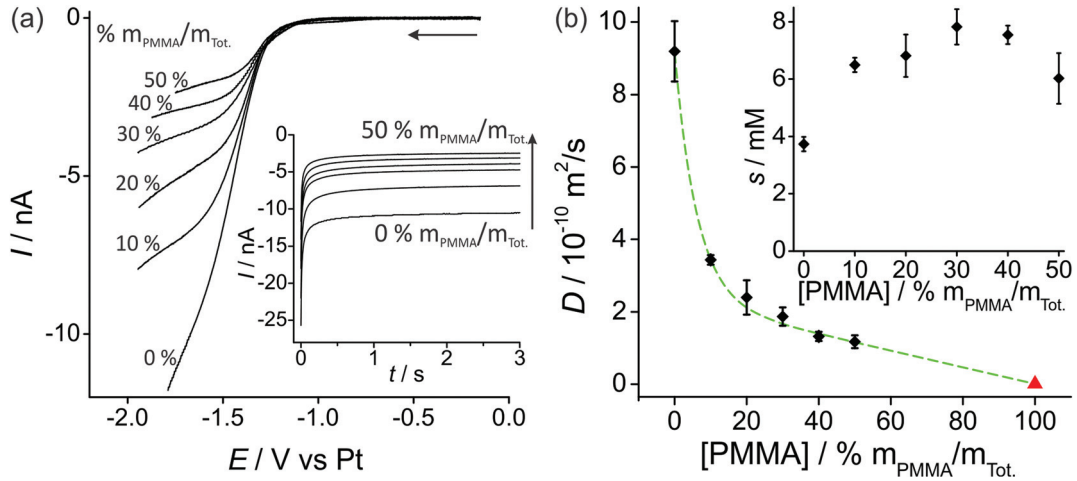

Fig. 2 (a) Linear sweep voltammetry (10 mV s^{-1}) for 100 vol% O_2 in PMMA–[C_2mim][NTf_2] mixtures at 0–50% $m_{PMMA}/m_{Tot.}$, on a platinum microdisk electrode (radius 7.44 μm). The inset shows the corresponding chronoamperometric transients. (b) Plot of diffusion coefficient (D) of O_2 *vs.* [PMMA] (the red triangle for pure PMMA, *i.e.* 100% $m_{PMMA}/m_{Tot.}$ is taken from the literature[22]). The inset shows oxygen solubilities s *vs.* [PMMA]. D and s were obtained by fitting chronoamperometric transients to the Shoup and Szabo equation.[21]

observed during the course of measurements; however, the shape of the voltammetry was ultimately used to determine the end potential of the linear sweep and to determine a suitable biasing potential for the chronomaperometry experiments).

In order to try to obtain diffusion coefficients and solubilities of oxygen in the various RTIL–PMMA mixtures, potential step chronoamperometry (PSCA) was carried for 100 vol% O_2 out at each PMMA doping concentration in the RTIL. The inset to Fig. 2a shows the experimental transients obtained from PSCA where the potential was stepped from 0 V to a chosen potential (on the slanted plateau where oxygen reduction occurs), and monitoring the current over time. The transients were then fitted to the Shoup and Szabo expression:[21]

$$I = -4nFDcr_d f(\tau) \quad (1)$$

$$f(\tau) = 0.7854 + 0.8863\tau^{-1/2} + 0.2146e^{-0.7823\tau^{-1/2}} \quad (2)$$

$$\tau = \frac{4Dt}{r_d^2} \quad (3)$$

where n is the number of electrons transferred (assuming 1 for O_2 in RTILs), F is Faraday's constant, D is the diffusion coefficient, c is the concentration (or solubility) of O_2, r_d is the radius of the microdisk, τ is dimensionless time and t is the time. The results from the fitting (D and solubility) are shown in Table 1, along with the steady-state current, I_{ss}, which was the current value averaged over the last 10 data points of the chronoamperometric transient. In the neat RTIL, the diffusion coefficient (9.2×10^{-10} m^2 s^{-1}) and solubility (3.7 mM) of O_2 agrees relatively well with that reported in the literature (8.3×10^{-10} m^2 s^{-1} and 3.9, respectively)[12] in the same RTIL. Also included in the table is the diffusion coefficient of O_2 in 100% PMMA for comparison, as reported by Vyazovkin *et al.*[22]

Table 1 Calculated properties (diffusion coefficient, D, solubility, s) for O_2 in [C_2mim][NTf_2] on a Pt microdisk electrode (radius = 7.44 μm) doped with 0–50% $m_{GPE}/m_{Tot.}$ concentrations of PMMA, obtained from fitting the chronoamperometry data in Fig. 2a (inset) using the Shoup and Szabo equation.[21] n is the number of different samples measured and I_{ss} is the steady state current, averaged over the last 10 data points of the chronoamperometric transient

[PMMA]/% $m_{GPE}/m_{Tot.}$	N	I_{ss}/nA	$D/10^{-10}$ m^2 s^{-1}	s/mM
0	3	−10.3 ± 0.4	9.2 ± 0.8	3.7 ± 0.3
10	4	−6.8 ± 0.1	3.4 ± 0.1	6.5 ± 0.3
20	5	−5.2 ± 0.1	2.5 ± 0.4	6.5 ± 0.3
30	5	−4.6 ± 0.9	1.9 ± 0.3	7.8 ± 0.6
40	3	−3.4 ± 0.3	1.4 ± 0.1	7.6 ± 0.4
50	5	−2.3 ± 0.2	1.2 ± 0.2	6.0 ± 0.9
100			0.00698 [22]	

Fig. 2b shows a plot of the diffusion coefficients, D, (main figure) and solubilities, s, (inset figure) of oxygen in the RTIL, as a function of increasing concentrations of PMMA. The diffusion coefficient decreases significantly when 10% PMMA is added to the RTIL, and gets systematically smaller as the % of PMMA increases. The triangle on the figure also shows the literature value for 100% PMMA. Attempts were made to fit the data using a range of curves/models (*e.g.* linear, exponential, polynomial) but the best fit (shown as the dashed line) appears to be the Shah model, where $D = 2.39 \times 10^{-10} - 2.38 \times 10^{-12}$[PMMA] + $6.73 \times 10^{-10} \times 0.849^{[PMMA]}$. D has units of m^2 s^{-1} and [PMMA] has units of % $m_{PMMA}/m_{Tot.}$, with R^2 = 0.9985. In this empirical model, an exponential and linear characteristic are both present, as shown in the dashed line in the figure.

The solubility of O_2 (inset to Fig. 2b) appears to almost double from the neat RTIL to 10% PMMA doping (3.7 mM in the neat RTIL compared to 6.6 mM in the 10% mixture), but remains relatively constant (within experimental error) as the

% of PMMA is increased further. This suggests a slightly stronger affinity of oxygen towards PMMA/RTIL mixtures, or an increase in gas permeability compared to the neat RTIL. The higher solubility of O_2 in the GPE (50% $m_{PMMA}/m_{Tot.}$) is advantageous for sensing purposes, however this is overcome by the much slower diffusion coefficient in the GPE compared to the neat RTIL, resulting in lower overall currents. The information on D and solubility of O_2 in the mixtures will be used to calculate expected currents on the microarray thin-film electrode (MATFE) in the next section.

3.2 Analytical utility for oxygen reduction on a MATFE

In order to investigate the feasibility of employing a commercially available microarray thin film electrode (MATFE) for oxygen gas sensing, with the gel-polymer electrolyte (GPE) for robust sensing, both cyclic voltammetry (CV) and long-term chronoamperometry (LTCA) was carried out in the neat RTIL and the 50% $m_{PMMA}/m_{Tot.}$ GPE. Other PMMA doping concentrations were not studied since they are not sufficiently gellified to provide a robust sensing device.

3.2.1 Cyclic voltammetry. Fig. 3 shows CV for the reduction of O_2 on a MATFE in the neat RTIL (a and b) and the 50% $m_{PMMA}/m_{Tot.}$ GPE (c and d). Two concentration ranges are shown, in order to observe the linear behaviour over the whole concentration range, and the detailed behaviour at lower concentrations. Due to the absence of a well-defined plateau current, the current was measured from a suitable fixed value (see Table 2). As can be seen in the insets to Fig. 3, excellent linear responses were observed ($R^2 > 0.99$) in both the neat RTIL and 50% $m_{PMMA}/m_{Tot.}$ GPE at both the low and high concentration ranges, despite the lack of a clear current plateau. The equations of the lines of best fits for the calibration graphs are given in Table 2, along with the LOD and R^2 values. There is not a significant difference in the limit of detection (LOD) for the high concentration range between the neat RTIL and 50% $m_{PMMA}/m_{Tot.}$ GPE. However, at the lower concentration range, the LOD is higher in the 50% $m_{PMMA}/m_{Tot.}$ GPE, which is likely due to the higher viscosity of the PMMA–RTIL mixture, giving rise to lower experimental currents for O_2 reduction. The LODs are significantly better than that reported

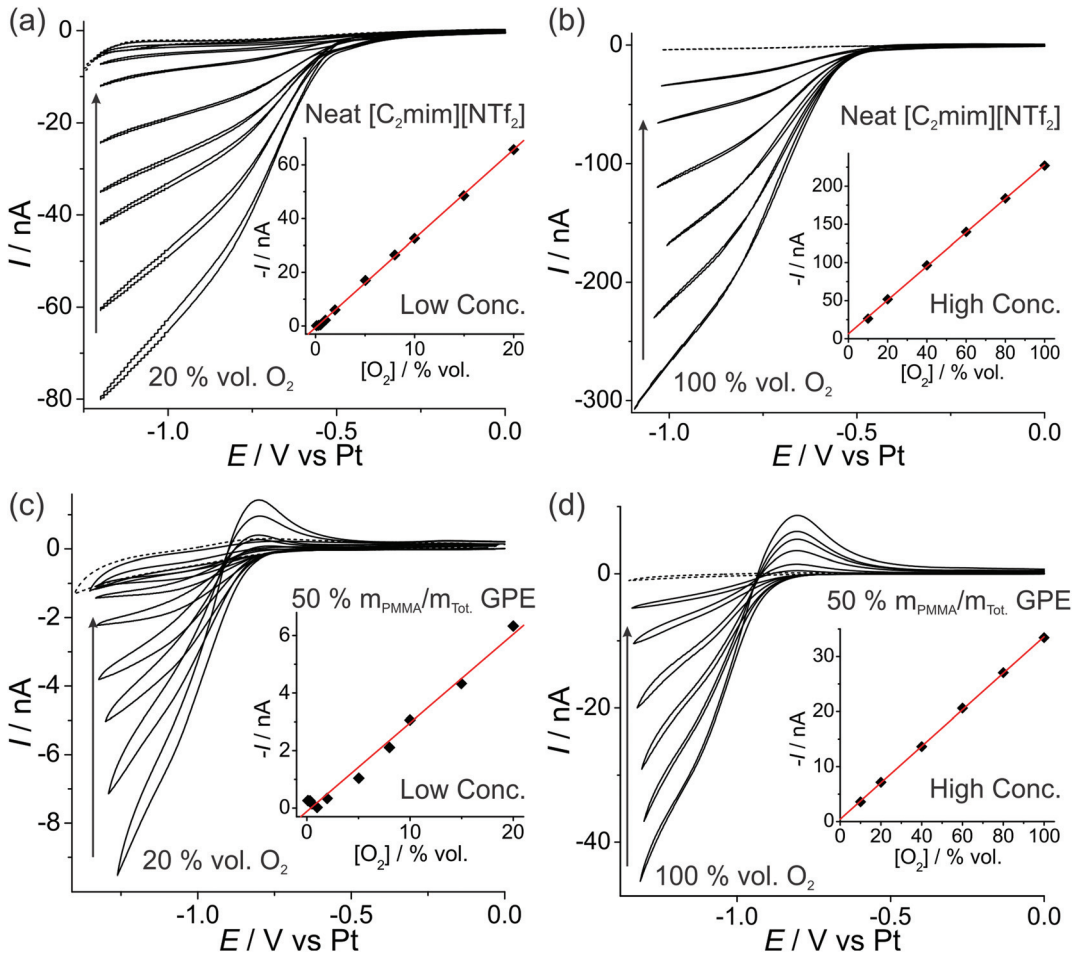

Fig. 3 CV of the $O_2/O_2^{\bullet-}$ redox couple at (a, c) "low concentrations" of 20, 15, 10, 8, 5, 2, 1 vol% O_2, and (b, d) "high concentrations" of 100, 80, 60, 40, 20, 10 vol% O_2 for (a, b) neat $[C_2mim][NTf_2]$ and (c, d) PMMA–$[C_2mim][NTf_2]$ mixture at 50% $m_{PMMA}/m_{Tot.}$ at a scan rate of 10 mV s^{-1}. The dotted lines are the CVs in the absence of oxygen. The insets are corresponding plots of background corrected current (obtained at a fixed potential, see Table 2) *vs.* vol% O_2, and the line of best-fit.

Table 2 Electrochemical data obtained for the reduction of varying oxygen concentrations, $[O_2]$, using cyclic voltammetry (CV) at 10 mV s^{-1} (Fig. 3) and long-term chronoamperometry (LTCA) (Fig. 4), for neat $[C_2mim][NTf_2]$ and 50% $m_{PMMA}/m_{Tot.}$ GPE. The equations of the linear best-fits, R^2 value, and LODs, are presented. The potential at which the currents were extracted from the CVs in Fig. 3 are also listed

	Electrolyte	$[O_2]$ range/vol% O_2	Potential/V	Equation of calibration graph (where I/A and $[O_2]$/vol%)	R^2	LOD/vol% O_2
CV	Neat $[C_2mim][NTf_2]$	1–20	−1.05	$-I = 3.31 \times 10^{-9}\,[O_2] - 5.3 \times 10^{-10}$	0.9995	0.5
		10–100	−0.90	$-I = 2.21 \times 10^{-9}\,[O_2] + 6.5 \times 10^{-9}$	0.9997	2.2
	50% $m_{PMMA}/m_{Tot.}$ GPE	1–20	−1.15	$-I = 3.13 \times 10^{-10}\,[O_2] - 1.8 \times 10^{-10}$	0.9874	2.6
		10–100	−1.20	$-I = 3.32 \times 10^{-10}\,[O_2] + 4.4 \times 10^{-10}$	0.9998	1.8
LTCA			**Order**			
	Neat $[C_2mim][NTf_2]$	0.1–20	Descending	$-I = 3.06 \times 10^{-10}\,[O_2] + 4.2 \times 10^{-10}$	0.9976	5.8
		0.1–20	Ascending	$-I = 3.03 \times 10^{-10}\,[O_2] + 3.3 \times 10^{-10}$	0.9989	4.0
		1.1–100	Ascending	$-I = 2.67 \times 10^{-9}\,[O_2] + 1.4 \times 10^{-8}$	0.9721	21
	50% $m_{PMMA}/m_{Tot.}$ GPE	0.1–20	Descending	$-I = 3.18 \times 10^{-10}\,[O_2] + 6.6 \times 10^{-11}$	0.9989	0.8
		0.1–20	Ascending	$-I = 3.11 \times 10^{-10}\,[O_2] + 6.6 \times 10^{-11}$	0.9991	0.8
		1.1–100	Ascending	$-I = 3.20 \times 10^{-9}\,[O_2] - 2.1 \times 10^{-10}$	0.9959	1.7
		1.1–100	Descending	$-I = 3.92 \times 10^{-9}\,[O_2] - 1.1 \times 10^{-9}$	0.9986	1.0

on a macrosized electrode (1 mm diameter Pt TFE) over the same 10–100 vol% O_2 concentration range in our previous work (4.2% and 5.4 vol% O_2 for neat RTIL and GPE, respectively).[19] This suggests that the MATFE is better than the TFE for analytical purposes, which is expected due to the higher current density at microelectrodes.[17]

The difference in the shape of the reverse sweep of the CV (oxidation of superoxide) in Fig. 3 is most likely due to the significantly lower diffusion coefficient of superoxide in the highly viscous 50% $m_{PMMA}/m_{Tot.}$ GPE compared to the neat RTIL, resulting in a peak-shaped oxidation in Fig. 3c and d (GPE), but a steady-state oxidation in Fig. 3a and d (neat RTIL). This effect has been previously reported for the oxygen/superoxide redox couple in the RTIL hexyltriethylammonium bis(trifluoromethylsulfonyl)imide ($[N_{6,2,2,2}][NTf_2]$) – where a 30× discrepancy in diffusion coefficients of oxygen and superoxide resulted in a voltammogram exhibiting both steady-state and transient (peak-shaped) behaviour on the same cycle.[12]

Using the fitted values for D and solubility of O_2 obtained for the neat RTIL and 50% $m_{PMMA}/m_{Tot.}$ GPE (section 3.1), the expected currents for a recessed disk array electrode is given by the following equation:[23,24]

$$I_{lim} = \frac{4\pi nFcDr_d^2}{4L + \pi r_d} \quad (4)$$

where n is the number of electrons, F is Faraday's constant, D is the diffusion coefficient, c is the concentration, r_d is the radius of the microdisk, and L is the depth of the pore (SU-8 layer). For 100 vol% O_2 on a MATFE with 90 electrodes, 10 μm in diameter and 3.0 ± 0.5 μm depth, the calculated currents in the neat RTIL and 50% $m_{PMMA}/m_{Tot.}$ GPE are 338 nA and 70 nA, respectively. Assuming the average value for the depth of the hole (3 μm), this compares to the experimental currents of 220 nA and 34 nA, representing only 65% and 49% of the theoretical value. Taking an extreme value of 3.5 μm for the depth is still unable to account for the significantly lower experimental currents. This may suggest that the geometry of the pores is not fully optimized for the experimental parameters *e.g.* due to overlapping diffusion layers.[25] It may also indicate that some of the pores could be blocked or not fully active; the SEM image in Fig. 1c shows that some of the SU-8 layer may still be present in the holes. The lower current % (experimental/theoretical value) for the 50% $m_{PMMA}/m_{Tot.}$ GPE (compared to the neat RTIL) could indicate poorer wetting of the surface, suggesting that some holes may not be fully filled by the electrolyte. However, similar currents (*ca.* ± 10%) were observed on repeat experiments on different days (on the same MATFE), showing good reproducibility of the data. This may indicate that wettability is not an issue. Alternatively, the higher resistance of the GPE could result in an increased ohmic drop effect, with a lower current % compared to the neat RTIL.

3.2.2 Chronoamperometry. Long-term chronoamperometry (LTCA) was performed on the MATFE to investigate the ability of the device to continuously monitor oxygen concentrations. This can be considered as quite a harsh technique due to the accumulation of superoxide at the working electrode. Fig. 4 shows the results from the LTCA experiments (for *ca.* 830 min) performed on the MATFE in the neat RTIL and 50% $m_{PMMA}/m_{Tot.}$ GPE at two O_2 concentration ranges (0.1–20 vol% O_2 and 1.1–100 vol% O_2). For LTCA, the current response at 0.1 vol% O_2 was very clearly distinguished from the background, unlike for CV where even measurements conducted for 1% O_2 were hard to discriminate from the background. The zoomed in plots of the lowest concentrations (*i.e.* 0.5, 0.1% O_2) are shown in Fig. 4a and c and the response in the GPE is clearly more stable and distinct than in the neat RTIL. However, in both the neat RTIL and 50% $m_{PMMA}/m_{Tot.}$ GPE, the currents reach a stable plateau above 0.5 vol% O_2, and linear calibration graphs were obtained. The equations of the calibration graphs, their R^2 value and LOD for O_2 for all plots are given in Table 2. There was a higher sensitivity (gradient) on the ascending plot compared to the descending plot for the neat RTIL, but both descending and ascending currents almost overlay for the GPE.

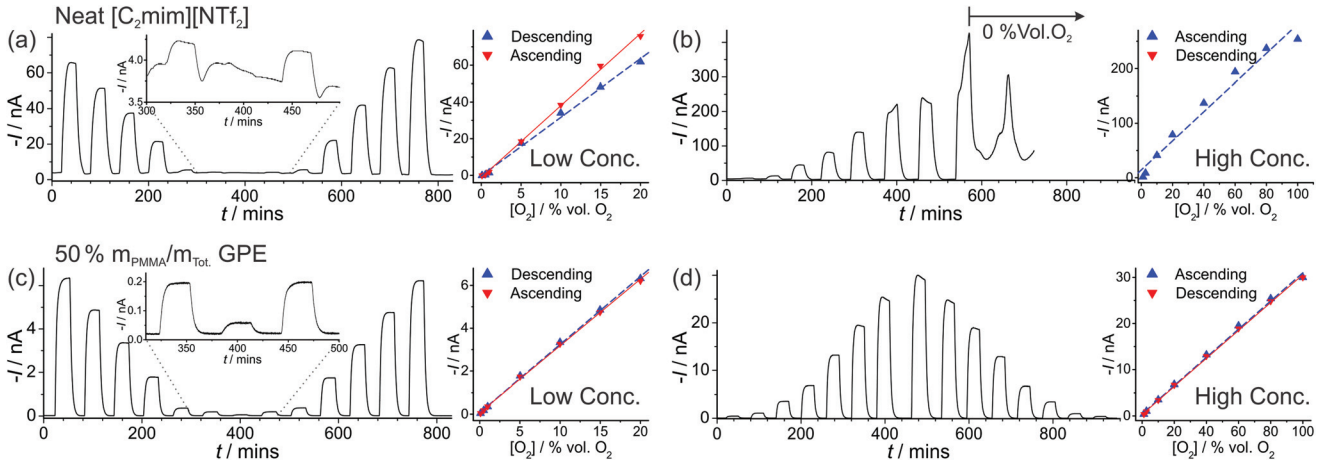

Fig. 4 Long-term chronoamperometry (LTCA) at different O_2 gas concentrations in (a, b) neat $[C_2mim][NTf_2]$ and (c, d) 50% $m_{PMMA}/m_{Tot.}$ PMMA–$[C_2mim][NTf_2]$ mixture. The gas flow was alternated between 100 vol% N_2 and varying O_2 concentrations: "low concentration" (a, c) 20, 15, 10, 5, 1, 0.5, 0.1, 0.5, 1, 5, 10, 15, 20 vol% and "high concentration" (b) 1.1, 2.7, 10, 20, 40, 60, 80, 100 vol% and (d) 1.1, 2.7, 10, 20, 40, 60, 80, 100, 80, 60, 40, 20, 10, 2.7, 1.1 vol% O_2. Background subtracted current *vs.* concentration plots are shown on the right, along with the lines of best fit from the "descending" and "ascending" data sets. The equations of the line of best-fit, R^2 value, and LODs are given in Table 2.

For the high concentration range in Fig. 4b and d, the current response appears to be relatively stable at the starting concentrations (from 1.1–20 vol% O_2). However, at higher concentrations (above 40 vol% O_2), the current response rapidly deteriorates in the neat RTIL (Fig. 4b). This is likely due to the shift in the potential of the pseudo-reference electrode during the course of the LTCA experiment, and proved to be a severe problem in the neat RTIL. Even when N_2 was added in (at *ca.* 570 minutes), a stable baseline could not obtained, and with the appearance of a large current spike at 660 min, despite no oxygen being present. In the GPE, signs of instability were also observed above 60 vol% O_2, where the current drops after reaching a peak, instead of maintaining the expected steady-state. However, the potential shifting that was present in the neat RTIL was insignificant in the 50% $m_{PMMA}/m_{Tot.}$ GPE, and stable and reproducible responses were observed on several repeat experiments. This is probably due to the slower migration of counter electrode products towards the RE in the polymer matrix, or the lower overall currents in the GPE (compared to neat RTIL), generating less superoxide.

The limits of detection (LODs) at the low concentration range in the neat RTIL (Table 2) were much higher from LTCA (5.8 and 4.0 vol% O_2) compared to CV (0.5 vol% O_2). This is probably due to the accumulation of superoxide in the μL volume of electrolyte during LTCA biasing. At the higher concentration range, the LOD in the neat RTIL is substantially poorer (21 vol% O_2) due to the visibly curved calibration plot (Fig. 4b, $R^2 = 0.9721$) as a result of the degradation of the LTCA response. This is likely to be the result of instability of the pseudo-reference electrode, or accumulation of superoxide inhibiting the kinetics of the oxygen reduction reaction. However, for the 50% $m_{PMMA}/m_{Tot.}$ GPE, LODs obtained at the high concentration range from CV (1.8 vol% O_2) and LTCA (1.7 vol% O_2) experiments are comparable, and are actually better at the low concentration range using LTCA (0.8 vol% O_2). Despite there not being a significant difference in LODs for the GPE obtained from LTCA (0.8 vol% O_2) compared to the neat RTIL from CV (0.5 vol% O_2) at the low concentration range, the O_2 current responses are clearly more straight forward to extract from the LTCA data compared to the CV data – where the lack of a current plateau required the current to be extracted at an arbitrarily chosen potential where O_2 reduction occurs (see Table 2). Therefore, it can be concluded that LTCA is the more reliable method, especially for the sensing of lower concentrations (*e.g.* ≤0.5 vol% O_2) where the CV signal-to-background response is poor. Based on the LTCA transients in Fig. 4, a 90% response time, t_{90}, of *ca.* 10 min is estimated in the neat RTIL and *ca.* 7 min in the 50% $m_{PMMA}/m_{Tot.}$ GPE. This is relatively long due to the moderate thickness of the electrolyte layers, and is expected to be smaller if thinner layers are employed. This is the focus of our future work.

Fig. 5a shows LTCA for an extended period of time (*ca.* 2100 min) for different concentrations of O_2 in the 50% $m_{PMMA}/m_{Tot.}$ GPE on a MATFE, and the corresponding plots of current *vs.* O_2 concentration (Fig. 5b). Both the initial ascending and descending plots from 1.1–100 vol% O_2 give very similar currents, as was observed in Fig. 4d. However, on the second ascending concentration set, the currents are slightly smaller (*ca.* 5–10%) suggesting a reduction in the sensitivity over time. When the 100 vol% O_2 was reached (at *ca.* 1480 min), the sensor was tested under extreme conditions by exposing to 100% for *ca.* 350 min. As can be seen in Fig. 5a, after *ca.* 150 min, the current response rapidly deteriorates to around half of the expected current value over prolonged exposure to 100% O_2. After this, N_2 was then added to observe the return of a stable baseline, followed by two more additions of 100 vol% O_2 at *ca.* 1880 min and 2000 min. The current responses are lower than that observed for 100% O_2 in the

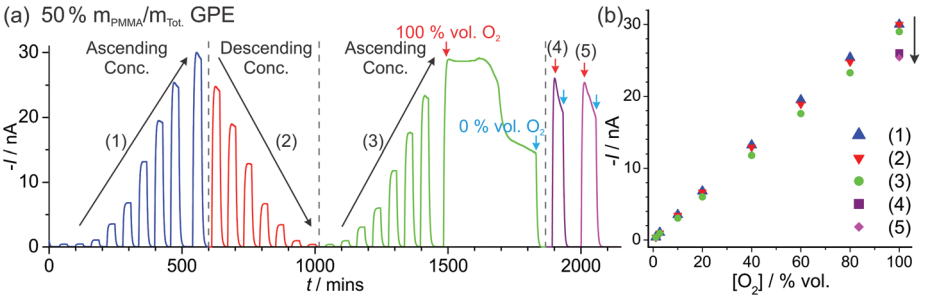

Fig. 5 (a) Long-term chronoamperometry (LTCA) on the MATFE with 50% $m_{PMMA}/m_{Tot.}$ PMMA–$[C_2mim][NTf_2]$ GPE exposed to higher O_2 concentrations (up to 100%) for an extended period of time, showing the impressive robustness of the GPE for O_2 sensing. (b) Plots of maximum current *vs.* concentration for: ascending (1), descending (2), subsequent ascending (3) order of concentrations, followed by two 100% O_2 additions ((4) and (5)) after being exposed to 100% O_2 for ~350 min (last part of green curve).

earlier part of the LTCA transient (see (4) and (5) in Fig. 5b). For these two additions, the current reached a peak but then fell sharply, suggesting that the MATFE is no longer behaving optimally. This could suggest that the surface has become passivated, possibly due to the large build-up of superoxide at the working electrode or other passivating species at the counter electrode that have migrated towards the working or reference electrodes. As a result, continually biasing in the presence of high O_2 concentrations (*e.g.* 60 vol% O_2 and above), even in the 50% $m_{PMMA}/m_{Tot.}$ GPE, is not recommended for the long-term use of these devices.

Although this type of sensor could be regarded as 'disposable' once the surface has been fouled (*e.g.* exposed to 100% O_2), it was actually found that reliable and reproducible current responses could be obtained on the same device if the GPE was rinsed off with acetone and the MATFE surface was re-activated in sulphuric acid. (Note: acetonitrile is not recommended for removal of the GPE for this as the SU-8 layer on the MATFE becomes compromised.) This suggests that even after exposure to high oxygen concentrations, the electrode can be reused provided the rinsing and reactivation steps are followed. However, for the majority of health-and-safety applications, concentrations in the 16–25% range are typically monitored (close to the concentration in air), so these devices have the potential to be easily and cheaply employed for long-term oxygen monitoring for these purposes. The use of a non-volatile RTIL as a gelled electrolyte also means these sensors could be employed in a wide range of conditions where typical membrane-based Clark-electrodes do not perform, such as at high temperatures and pressures, and under shaking, agitation and tilting of the sensor device.

4. Conclusions

The performance of a low-cost commercially-available MATFE was investigated for its response to different concentrations of oxygen at short timescales (CV) and long timescales (LTCA) in a neat RTIL and a RTIL gellified with PMMA. Although the current responses are lower in the gellified RTIL, they are much more stable, reproducible and less prone to shifts in the reference electrode potential. LTCA appears to be the most reliable technique to measure lower concentrations of O_2 (less than 1 vol%) compared to CV (where currents were difficult to determine due to the slanted nature of the voltammetry). However, CV is the better technique at higher O_2 concentrations (above 60 vol%) since it does not involve the continuous build-up of superoxide (as with LTCA). Overall the results look very promising for employing the MATFE for O_2 sensing, particularly when using the 50% $m_{PMMA}/m_{Tot.}$ GPE. The variation in thicknesses of the SU-8 layer on the MATFE (3.0 ± 0.5 μm) could pose a problem if employed for oxygen sensing on a bulk scale. However, if this is taken into account (*e.g.* by calibrating with a gas standard), then it appears that these low-cost MATFE could be easily and cheaply employed in the field for long-term oxygen monitoring.

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