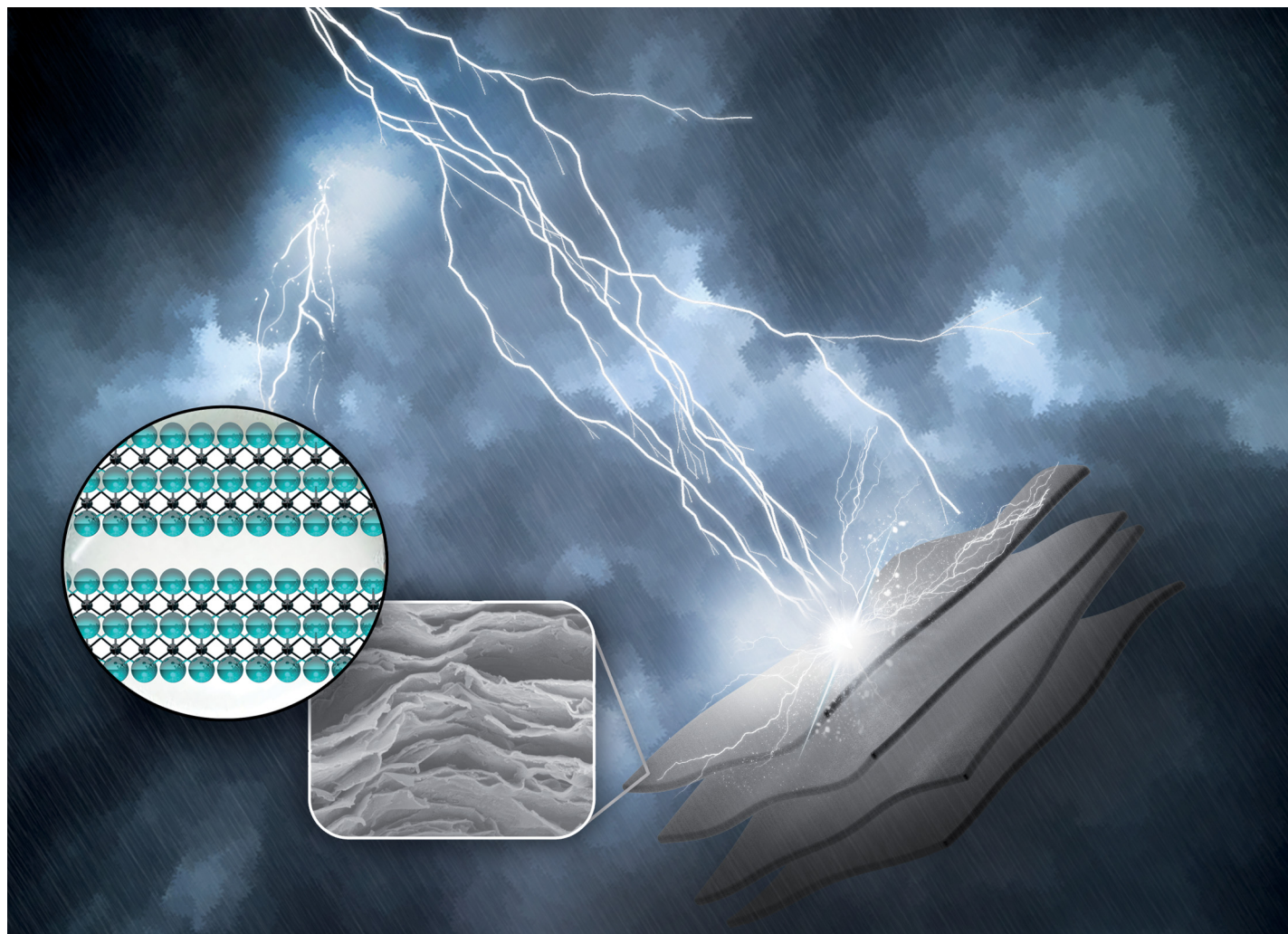


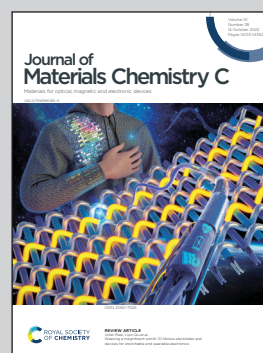


Lin's group from Guangxi University reports a time-difference blow-spinning technology to fabricate a dual-scale multilayer MXene/PAN fabric for high-efficiency EMI shielding.

Time-difference blow-spinning to a flexible dual-scale multilayer fabric for highly efficient electromagnetic interference shielding

A dual-scale multilayer fabric consisting of PAN fibers and MXene prepared by time-difference blow-spinning exhibits remarkable EMI shielding property.

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Time-difference blow-spinning to a flexible dual-scale multilayer fabric for highly efficient electromagnetic interference shielding†

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A new kind of pollution known as electromagnetic interference (EMI) caused by the ubiquitous usage of integrated electronic devices and communication systems is attracting increasing attention. The design and mass-production of functional materials for large-scale, flexible, and curved surface EMI shielding remains a challenge. In this study, we have developed a time-difference blow-spinning technology to continuously fabricate multilayer polyacrylonitrile (MLPAN) nanofibers; on combining with roll-to-roll dip-coating post-processing, a flexible $\text{Ti}_3\text{C}_2\text{T}_x$ /MLPAN hybrid fabric was obtained. It shows a special dual-scale multilayer structure, including a primary multilayer structure from MLPAN, and a secondary nanoscale multilayer structure from $\text{Ti}_3\text{C}_2\text{T}_x$. The hybrid fabric is lightweight (639.0 mg cm^{-3}), with high conductivity ($23327.40 \text{ S m}^{-1}$) and good mechanical stability. Moreover, this hybrid fabric exhibits a remarkable EMI shielding property with a shielding efficiency of 61.8 dB, which is attributed to the synergistic effect of surface reflection, internal multiple scattering and multiple reflections.

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Introduction

The rapid development of multidisciplinary technologies has enabled modern electronic devices to become smaller, lighter, more integrated and smarter. Nowadays, various portable and wearable electronic products, such as wireless communication devices, photographic equipment, and functional sensors, are effectively improving our daily lives.^{1,2} A new form of pollution known as electromagnetic interference (EMI) accordingly occurs by radioactive rays from high-power electromagnetic equipment, massive signal crosstalk from communication systems, or military special facilities like radar.^{3,4} Such electronic pollution, if ignored, will interfere with the normal operation of various electronic devices, threaten the information security of communication equipment, and even lead to some potential

security risks (e.g., eye problems and cancer) for human health.^{5–7} A consensus has been formed that the mitigation and shielding of EMI is not only the key issue of integrated circuits, the modern electronic industry and flexible electronics but also a topic of significance to human society.

According to Schelkunoff theory, total EMI shielding effectiveness (SE_{Total}) on the decibel scale can be described in the sum of reflection loss (SE_{R}), absorption loss (SE_{A}), and multiple reflection loss (SE_{M}). Further, SE_{R} as a primary EMI shielding mechanism for conductive materials can be quantified *via* the Fresnel's equation:⁸

$$\text{SE}_{\text{T}} (\text{dB}) = \text{SE}_{\text{R}} + \text{SE}_{\text{A}} + \text{SE}_{\text{M}} \quad (1)$$

$$\text{SE}_{\text{R}} (\text{dB}) = 20 \log \frac{(\eta + \eta_0)^2}{4\eta\eta_0} \quad (2)$$

where η and η_0 are the characteristic impedance of the shielding medium and air, respectively. In the transmission line theory, characteristic impedance η is defined as follows:⁹

$$\eta = \sqrt{\frac{j\omega\mu}{\sigma + j\omega\varepsilon}} \quad (3)$$

where μ , σ , and ε are the permeability, conductivity, and permittivity, respectively, and $\omega = 2\pi f$ is the angular frequency of the incident electromagnetic waves. Therefore, good conductors such as metal blocks and metal meshes are generally

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chosen for traditional EMI shielding due to their high reflection loss. However, the intrinsic physical characteristics including high density, brittleness, and poor flexibility co-constrain their applications in portable devices and new generation flexible or wearable electronics.¹⁰

Novel structural design is one of the effective ways to optimize the EMI shielding properties of materials. Dense packing is no longer considered to be an effective strategy for EMI shielding because the shielding ability can be greatly improved by introducing additional interfaces within the medium.¹¹ Increasing interfaces with mismatching impedance characteristics can contribute to additional internal scattering, also referred to as internal multiple scattering, and consequently, enhance absorption loss.¹² In recent years, layer structural materials have attracted increasing attention in many fields due to their special physicochemical properties (anisotropic binding force, interlayer electron transport path, large specific surface area, *etc.*). A new family of two-dimensional transition metal carbides and nitrides referred to as MXenes is one of the research hotspots in electromagnetism, materials science, chemistry, *etc.*,^{13,14} due to their special microscopic layered structure and unique physicochemical properties.¹⁵ For example, a high EMI shielding effectiveness (EMI SE) of $\text{Ti}_3\text{C}_2\text{T}_x$ synthesized by etching Ti_3AlC_2 in an acidic etchant has been reported by Y. Gogotsi *et al.*, offering an SE_{Total} value of about 85.0 dB in the X-band frequency range (8.2 to 12.4 GHz).¹⁶ Such an impressive EMI shielding property for $\text{Ti}_3\text{C}_2\text{T}_x$ is mainly due to the enhanced internal scattering effect that comes from its multilayered structure. However, it is prone to self-accumulation into a compact structure due to the aggregation effect during mass manufacturing or the process of being used, which seriously affects its intrinsic characteristics.¹⁷ In addition, free-standing MXene-based materials like $\text{Ti}_3\text{C}_2\text{T}_x$ thin films, in most situations, show suboptimal mechanical strength (brittleness). This deficiency puts them at risk for damage during long-term storage, transport, and some kinds of post-assembly processes such as bending, rolling, and folding.^{18,19} Therefore, a lightweight, large-scale, flexible, stable, and morphologically controllable structural reinforcement substrate is highly desired to support the MXene functional material's further use in portable and flexible EMI shielding.^{20–22}

Macro-scale internal multiple scattering is also an important factor affecting the total electromagnetic wave loss. In order to make the most of this characteristic, researchers have developed macro-porous and multilayered conductive materials for high-performance EMI shielding; for example, porous graphene foams,²³ flexible waterborne polyurethane (WPU)/silver nanowire (AgNW) nanocomposites with unidirectionally aligned micrometer-sized pores,²⁴ and graphene-hybridized CuNW (CuNW@G) core-shell aerogels.²⁵ Although all these materials show good EMI SE, their practical application remains challenging due to the following. (i) Weak in mass-production. The manufacturing processes of those macro-porous or multiple-layer materials often require stringent conditions, *e.g.*, foaming, freeze-drying, or high-temperature

calcination, which severely limit their continuous manufacturing and large-scale application.^{26,27} (ii) Lack of superior flexibility. Their mechanical properties tend to be rigid, due to Young's modulus being too high to meet the requirements of various curved surface application scenarios. (iii) Low utilization of functional materials.^{28,29}

In this work, we propose a time-difference blow-spinning technology to continuously fabricate the multilayer polyacrylonitrile (MLPAN) nanofiber film with adjustable thickness and layer number in one step. By further conducting modifications with the as-prepared $\text{Ti}_3\text{C}_2\text{T}_x$ solution *via* dip-coating, an ultralight and flexible hybrid fabric (named $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$) was obtained. It contained a multilayer nanofiber-network primary structure from MLPAN and a secondary nanoscale multilayer structure from $\text{Ti}_3\text{C}_2\text{T}_x$, verified *via* a series of micromorphological characterization methods. The hybrid fabric exhibited a low density of 639.0 mg cm^{-3} and good electrical properties including $23327.40 \text{ S m}^{-1}$ of conductivity and $0.39 \text{ } \Omega \text{ sq}^{-1}$ of sheet resistance. Due to its special dual-scale multilayer structure, the hybrid fabric exhibited a high EMI SE_{Total} of up to 61.8 dB and a superior special EMI SE (thickness normalized SE, SSE/d) of $8535.9 \text{ dB cm}^2 \text{ g}^{-1}$, which was considered the synergistic EMI shielding effect of multiple reflections and internal scattering. Moreover, benefits from the inherent mechanical advantages of the nanofiber substrate, $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ exhibited remarkable flexibility, illuminating only a slight change in the EMI SE after 5000 cycles of bending. The synergistic effects of internal reflection, internal multiple scattering and multiple reflections from dual-scale multilayer EMI shielding materials provide the possibility of applying the structurally designed advanced fabric in large-scale, portable, flexible and curved-surface EMI shielding and electromagnetic protection.

Results and discussion

We designed and proposed a time-difference blow-spinning technology to directly separate the deposited nanofibers in both space and time, aiming to manufacture a morphologically adjustable multilayer fiber film in one step. The time-difference blow-spinning contains two main components, namely, a spinning module including two aspectant jets with staggered turn-on times, and a rotating speed-controlled porous cylinder as the fiber collector (Fig. 1a). The internal pressure of the collector was adjusted to negative by an air pump to assist fiber deposition. During the blow-spinning process, compressed air drives the precursor solution with a certain viscosity to form a high-speed jet (Fig. 1b and Fig. S1, ESI†). After solvent volatilization, the precursor fiber was obtained (Fig. 1c). In this method, the size of the product fiber mainly depends on the shape and surface area of the collector. Therefore, in order to scale up the product fiber size, the collector can be further designed on a large scale as a conveyor belt. Fig. 1d shows a typical time-difference blow-spinning process, wherein, the primary and the secondary spinning modules (red and green,

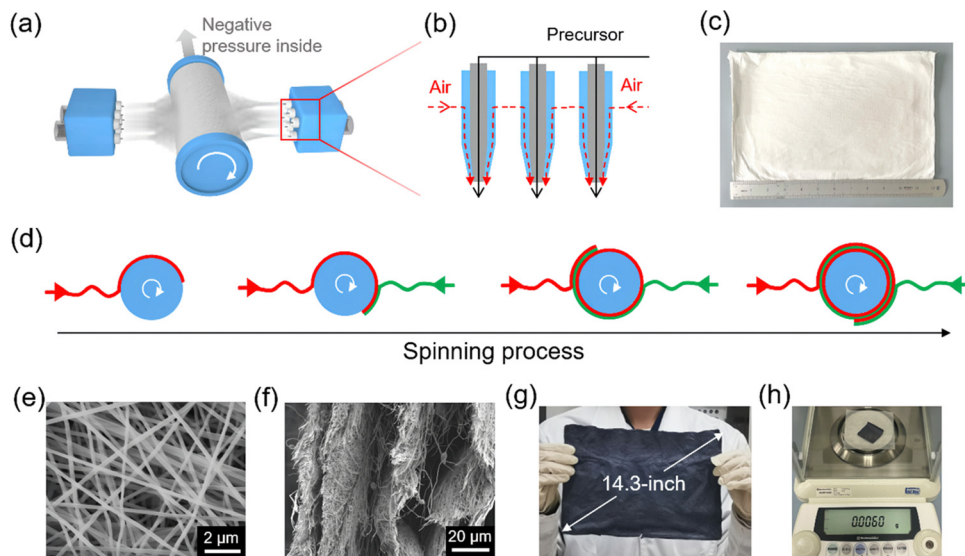


Fig. 1 The time-difference blow-spinning production. (a) Schematic of the spinning module and fiber collector. (b) Details of the airflow and precursor flow paths on spinning needles. (c) Photograph of a 14.3-inch (A4 scale) MLPAN. (d) Working diagram of the primary (red), secondary (green) spinning modules, and the rotating collector during time-difference blow-spinning. (e) Surface and (f) cross-sectional SEM images of the four-layer MLPAN. (g) Photograph of an A4-scale $\text{Ti}_3\text{C}_2\text{T}_x$ /MLPAN, (h) and its ultralow density demonstration.

respectively) turn on in sequence with a time difference while the collector rotated by 180 degrees. The thickness of the fiber film can be adjusted by controlling the solution injection speed, the airflow speed and the rotating speed of the cylindrical collector. Particularly, the rotating speed of the collector was set as 2 degrees per second in this work. As the rotating number increases, different layers of fiber can be obtained. In this work, a typical four-layer PAN fiber film with a network surface structure was fabricated as the substrate material (primary multilayer structure) for further EMI shielding application (Fig. 1e, f and Fig. S2, ESI[†]). The secondary multilayer structure material, $\text{Ti}_3\text{C}_2\text{T}_x$, was made by etching Ti_3AlC_2 using HCl/LiF etchant (Fig. S3, ESI[†]). In this process, Al layers were selectively etched after 24 h of continuous stirring. Previous studies illuminated that a certain amount of PVB can enhance the mechanical stability of a material, therefore, 0.1 wt% PVB was employed in this work to form a dip-coating precursor solution.¹¹ By a subsequent facile dip-coating process, the $\text{Ti}_3\text{C}_2\text{T}_x$ /MLPAN hybrid fabric with specific dimensions can be obtained (Fig. S4 and S5, ESI[†]). Such a dip-coating method is easy to scale up for industrial production (Fig. 1g). Benefiting from the multilayer structure and spatial network structure of MLPAN, the hybrid fabric exhibited an ultralow density, which is highly desired in modern portable and flexible electronics (Fig. 1h).

After etching the Al layers, the obtained $\text{Ti}_3\text{C}_2\text{T}_x$ presented a layered accordion-like structure (Fig. 2a). The transmission electron microscope (TEM) image exhibited a two-dimensional nanosheet structure of few-layered $\text{Ti}_3\text{C}_2\text{T}_x$ (Fig. 2b). The high-resolution TEM (HRTEM) showed an ~ 0.26 nm lattice spacing, corresponding to the $(\bar{1}010)$ lattice plane, which is consistent with that of the parent MAX phase (Fig. S6, ESI[†]).³⁰ The selected area electron diffraction (SAED) exhibits

a typical sixfold symmetric diffraction pattern, indicating the high crystallinity of the as-prepared $\text{Ti}_3\text{C}_2\text{T}_x$ (Fig. 2b, inset). The thickness of the monolayer $\text{Ti}_3\text{C}_2\text{T}_x$ was verified by atomic force microscopy (AFM) as ~ 1.39 nm (Fig. 2c and d). The fine-adjusting of the mass ratio of $\text{Ti}_3\text{C}_2\text{T}_x$ during the dip-coating process led to a series of $\text{Ti}_3\text{C}_2\text{T}_x$ /MLPAN hybrid fabrics with different surface microstructures. As shown in Fig. 2e, the mesh structures of the MLPAN nanofiber substrates were gradually filled and covered with the increase in the mass ratio of $\text{Ti}_3\text{C}_2\text{T}_x$, which was further proved by X-ray photoelectron spectroscopy (XPS) results (Fig. 2f and Fig. S7, ESI[†]). As the mass percentage of $\text{Ti}_3\text{C}_2\text{T}_x$ reached 63.6 wt%, the surface of $\text{Ti}_3\text{C}_2\text{T}_x$ /MLPAN became uniform (Fig. S8, ESI[†]). After dip-coating, $\text{Ti}_3\text{C}_2\text{T}_x$ /MLPAN exhibited strong diffraction peaks in the X-ray diffraction (XRD) spectrum at 2θ of about 7 degrees (Fig. 2g), which corresponds to the (002) lattice plane of $\text{Ti}_3\text{C}_2\text{T}_x$, indicating that the crystal structure of $\text{Ti}_3\text{C}_2\text{T}_x$ remained unchanged. In addition, the slight shift of the (002) lattice plane peak position of the hybrid fabric can be attributed to the interlayer spacing variation of $\text{Ti}_3\text{C}_2\text{T}_x$ after dip-coating.³¹ The cross-section SEM image and corresponding energy dispersive spectroscopy (EDS, element mapping) of $\text{Ti}_3\text{C}_2\text{T}_x$ /MLPAN illuminated the rich deposition of $\text{Ti}_3\text{C}_2\text{T}_x$ on both sides of the fiber substrate, owing to the filtering effect from the surface network structure of blow-spun MLPAN nanofiber film (Fig. 2h and Fig. S9, ESI[†]). However, there was also a certain amount of $\text{Ti}_3\text{C}_2\text{T}_x$ nanosheets inside the MLPAN, forming a secondary multilayer structure on each layer of PAN fiber (Fig. S10, ESI[†]). During thermogravimetric analysis (TGA) testing, a mass decrement was observed around 317 °C, representing the removal of water molecules and other functional groups (such as $-\text{OH}$ and $=\text{O}$) in $\text{Ti}_3\text{C}_2\text{T}_x$. As the temperature increased over 320 °C, the MLPAN started to thermally decompose and $\text{Ti}_3\text{C}_2\text{T}_x$

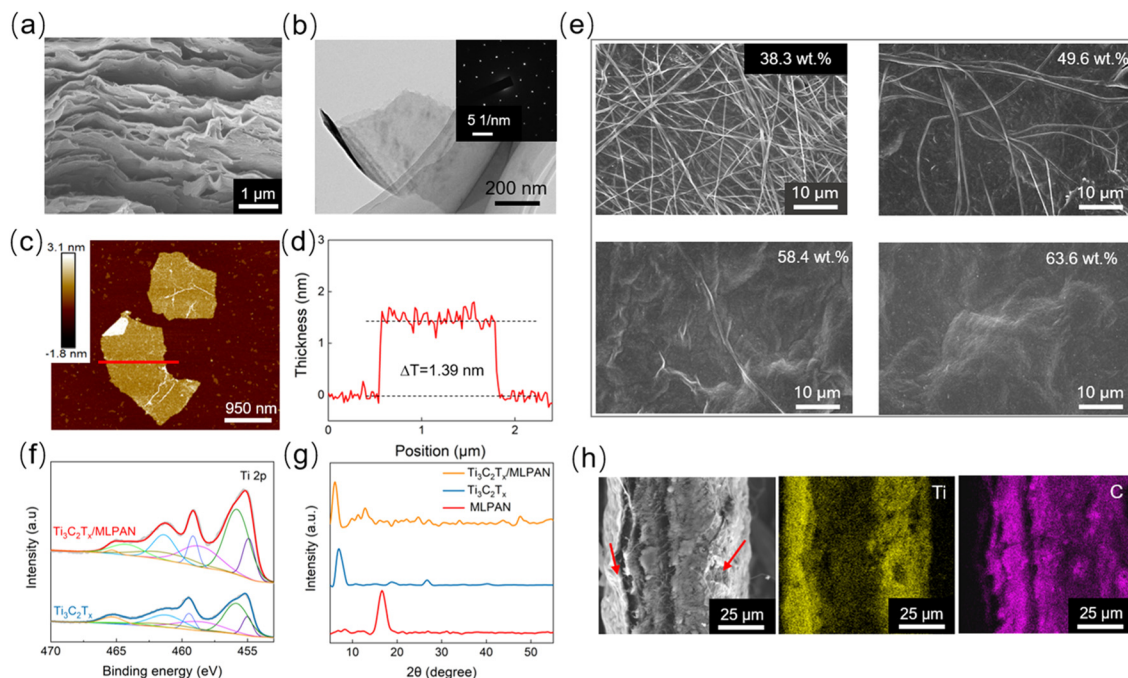


Fig. 2 Micromorphological, crystallographic, and chemical characteristics. (a) Cross-section SEM image of multilayer $\text{Ti}_3\text{C}_2\text{T}_x$. (b) TEM image of the $\text{Ti}_3\text{C}_2\text{T}_x$ nanosheet, the inset shows the corresponding SAED pattern. (c) AFM image of the $\text{Ti}_3\text{C}_2\text{T}_x$ nanosheet after a five-minute ultrasonic dispersion, (d) and its thickness measurement. (e) Surface SEM images of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ with different $\text{Ti}_3\text{C}_2\text{T}_x$ contents of 38.3 wt%, 49.6 wt%, 58.4 wt% and 63.6 wt%. (f) XPS peak differentiation imitating the analysis of Ti 2p. (g) XRD spectra of MLPAN, $\text{Ti}_3\text{C}_2\text{T}_x$, and $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$. (h) Cross-sectional SEM image, and EDS element mapping of Ti and C.

was slightly affected (Fig. S11, ESI†), indicating the high thermal stability of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ below 317 °C.

The electrical properties, including conductivity and sheet resistance, are the main parameters that affect a material's EMI shielding property. We first measured the electrical properties of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ with different $\text{Ti}_3\text{C}_2\text{T}_x$ contents of 38.3 wt%, 49.6 wt%, 58.4 wt% and 63.6 wt%. As the mass ratio of $\text{Ti}_3\text{C}_2\text{T}_x$ increased to 63.6 wt%, the conductivity and sheet resistance of the hybrid fabric were $23327.40 \text{ S m}^{-1}$ and $0.38 \text{ } \Omega \text{ sq}^{-1}$, respectively (Fig. 3a). Such good electrical properties of the hybrid fabric mainly arise from the high electron density of states near the Fermi level $[N(E_F)]$ of $\text{Ti}_3\text{C}_2\text{T}_x$.³² EMI SE is a key indicator of EMI shielding associated fields, which can be expressed using S -parameters:

$$SE_{\text{Total}} = SE_R + SE_A = 10 \log \left(\frac{1}{|S_{21}|^2} \right) \quad (4)$$

$$SE_R = 10 \log \left(\frac{1}{1 - |S_{11}|^2} \right) \quad (5)$$

$$SE_A = 10 \log \left(\frac{1 - |S_{11}|^2}{|S_{21}|^2} \right) \quad (6)$$

As shown in Fig. S12 (ESI†), SE_A and SE_R of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ with different $\text{Ti}_3\text{C}_2\text{T}_x$ contents were calculated from S_{11} and S_{21} . $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ enables efficient EMI shielding in the X-band with high EMI SE_{Total} . The SE_{Total} of the hybrid fabric

reached $\sim 61.8 \text{ dB}$ as the mass ratio of $\text{Ti}_3\text{C}_2\text{T}_x$ increased to 63.6 wt% (Fig. 3b), wherein SE_A reached $\sim 56.7 \text{ dB}$ and SE_R reached $\sim 5.1 \text{ dB}$ (Fig. 3c and Fig. S13, ESI†). This result indicates an ultrahigh shielding efficiency of over 99.9999%, enabling an almost complete blocking of the incident electromagnetic waves (Fig. 3d). Compared with the EMI SE obtained when the same mass of $\text{Ti}_3\text{C}_2\text{T}_x$ was filtered into the membrane alone (Fig. S14, ESI†), the SE_{Total} of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ increased by 35.8%. Fig. S15 (ESI†) shows that the EMI SE of MLPAN was almost zero. The type of EMI shielding can be determined by the power coefficients, including the reflection coefficient (R), absorption coefficient (A), and transmission coefficient (T).⁸ As shown in Table S1 (ESI†), the low A and low R of MLPAN led to an extremely low EMI shielding performance ($T = 0.988$). The results indicate that MLPAN is electromagnetically insensitive and only acts as a flexible multilayer substrate to separate $\text{Ti}_3\text{C}_2\text{T}_x$ at the first scale (20 μm). On the other hand, the A value of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ (63.6 wt%) reached 0.318, which is 75.7% higher than that of the $\text{Ti}_3\text{C}_2\text{T}_x$ film with the same $\text{Ti}_3\text{C}_2\text{T}_x$ mass ($A = 0.181$). This result can be attributed to the enhanced EM wave absorption for $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ caused by the dual-scale multilayer structure that increases both internal scattering and multiple reflections. As a proof-of-concept, a normal printing paper (Fig. 3e, left) and a $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ hybrid fabric (Fig. 3e, right) were placed successively between a wireless charging pad and a smartphone. As shown in Fig. 3e, the normal printing paper did not affect the wireless charging process. On the contrary, the wireless charging was successfully

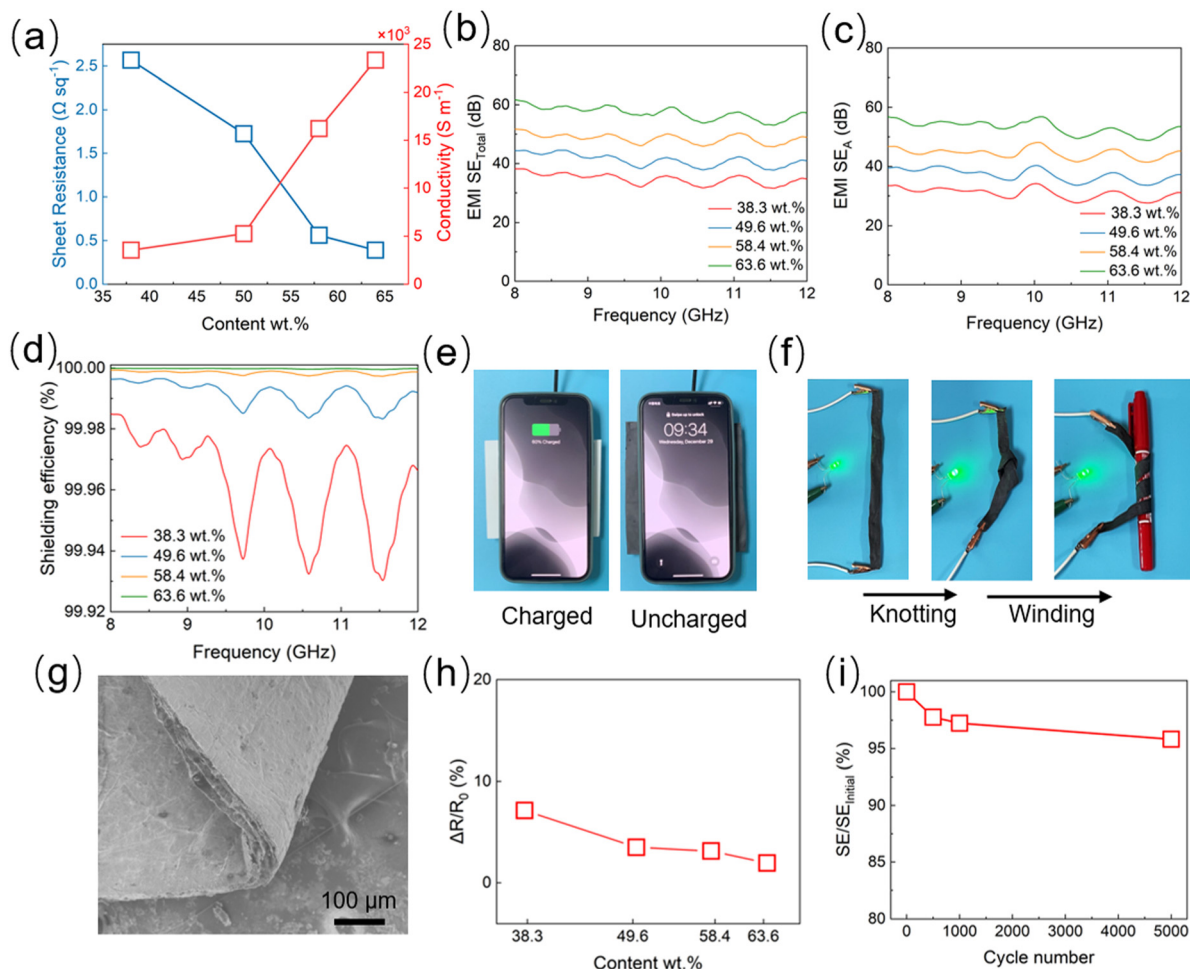


Fig. 3 Electrical, electromagnetic and mechanical properties. (a) Sheet resistance and conductivity of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ with $\text{Ti}_3\text{C}_2\text{T}_x$ content of 38.3 wt%, 49.6 wt%, 58.4 wt% and 63.6 wt%. (b) EMI SE_{Total} , (c) EMI SE_A , and shielding efficiency (%) of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ with different $\text{Ti}_3\text{C}_2\text{T}_x$ contents. (e) A proof-of-concept of the wireless charging blocking with $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ (right) and a printing paper control group. (f) An intuitionistic exhibition of the mechanical properties of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ as it is knotting and winding. (g) SEM image of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ in the bending state. (h) The rate of resistance change of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ with different $\text{Ti}_3\text{C}_2\text{T}_x$ contents of 38.3 wt%, 49.6 wt%, 58.4 wt% and 63.6 wt% after 1000 cycles of bending. (i) Changes in EMI SE for $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ after 500, 1000, and 5000 cycles of bending.

interrupted by the $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ hybrid fabric, indicating the great EMI shielding property of the latter. Flexibility and mechanical stability are two other important factors for cambered and deformable devices. We used $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ as a conducting wire to light an LED in different forms to visually verify its flexibility. As shown in Fig. 3f, the LED was always on, even when the $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ was knotted and winding, indicating the shape-independent electrical conductivity of the hybrid fabric. In terms of micromorphology, $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ showed no cracks or creases after folding and coiling (Fig. 3g and Fig. S16, S17, ESI[†]), mainly due to the nano-size effect of one-dimensional PAN fibers. Cyclic bending experiments were further performed on $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ with different $\text{Ti}_3\text{C}_2\text{T}_x$ contents of 38.3 wt%, 49.6 wt%, 58.4 wt% and 63.6 wt%. The results only showed a slight change in the resistances of those samples after 1000-cycle bending (Fig. 3h). Real-time resistance changes of the samples were also recorded *via* a computer-controlled electrochemical workstation as shown in

Fig. S18 (ESI[†]); the results indicated a steady variation trend and low loss of conductivity. To further demonstrate the microstructure stability, we collected SEM images of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ with different $\text{Ti}_3\text{C}_2\text{T}_x$ contents of 38.3 wt%, 49.6 wt%, 58.4 wt% and 63.6 wt% before and after 1000-cycle bending (Fig. S19, ESI[†]). By comparing the SEM images before and after bending, it was found that the microstructure of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ remained almost the same, indicating a high mechanical stability of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ under deformation conditions. Moreover, $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ retained $\sim 93\%$ of its initial EMI SE after over 5000 cycles of bending, indicating both remarkable flexibility and outstanding mechanical stability (Fig. 3i). A 24 hour soaking experiment was further performed to prove the waterproof property of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$. As shown in Fig. S20 (ESI[†]), the average resistance of the sample before and after soaking remained broadly unchanged, indicating the high stability of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ in water. A comprehensive consideration of thickness, density, usability, flexibility, mechanical

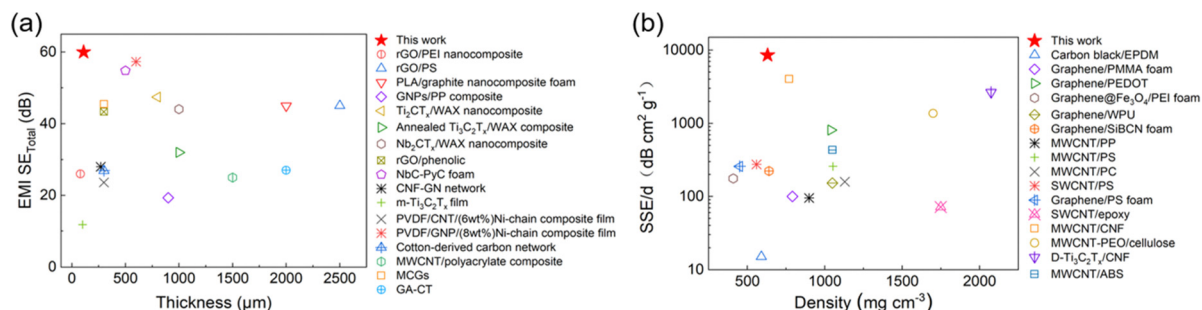


Fig. 4 Comparison of the EMI shielding performance. (a) EMI SE_{Total} versus the thickness of Ti₃C₂T_x/MLPAN and other EMI shielding materials from the references. (b) Thickness-normalized specific SE (SSE/d) of Ti₃C₂T_x/MLPAN with a density of 639.0 mg cm⁻³ and other EMI shielding materials from the references.

stability and EMI shielding property indicated that the Ti₃C₂T_x/MLPAN hybrid fabric is comparable with, and even better than, most reported EMI shielding films and bulk materials (Fig. 4).^{33–63} Detailed data for the comparison of EMI shielding properties including SE_{Total} and thickness-normalized specific SE (SSE/d) are shown in Tables 1 and 2.

The dual-scale multilayer structure of Ti₃C₂T_x/MLPAN leads to enhanced electromagnetic wave dissipation *via* internal reflection, multiple scattering and multiple reflections (Fig. 5a). When the incident electromagnetic wave reaches the first layer of Ti₃C₂T_x, partial energy is immediately reflected and the rest passes through Ti₃C₂T_x. The same process happens when the transmitted wave reaches the next layer of Ti₃C₂T_x, until it passes through one layer of the PAN substrate. A similar process occurs when the electromagnetic wave reaches the next layer of the PAN substrate, during which, both internal scattering and multiple reflections are significantly increased, resulting in a higher A value. This result proves that such a dual-scale multilayer structure of Ti₃C₂T_x/MLPAN contributes to the effective attenuation and elimination of EM waves.⁶⁴ It is generally considered that the multiple reflections inside a conducting medium occur only when the material's thickness is lower than the corresponding skin depth. The skin depth of Ti₃C₂T_x was

calculated as 154.6 μm, which is much bigger than the thickness of monolayer Ti₃C₂T_x (1.39 nm), leading to the multiple reflections occurring in Ti₃C₂T_x (Fig. 5b). For each layer of Ti₃C₂T_x, the total transmitted wave is the sum of all the partial waves (Fig. 5b, green arrows) transmitted past the Z₂-Z₁ interface:⁶⁵

$$E_t = \frac{(1 - \Gamma_1^2)e^{-\gamma t}}{1 - \Gamma_1^2e^{-2\gamma t}} E_i \quad (7)$$

where E_t is the total transmission wave, E_i is the incident wave, Γ_1 is the reflection coefficient, γ is the propagation constant, and t is the thickness of the conducting medium. The total transmission wave for a medium with N layers (E_{tN}) can be described as follows:

$$E_{tN} = \beta^N E_i \quad (8)$$

$$\beta = \frac{(1 - \Gamma_1^2)e^{-\gamma t}}{1 - \Gamma_1^2e^{-2\gamma t}} \quad (9)$$

It was observed that the intensity of the incident electromagnetic wave exponentially decreases by attenuation coefficient β as the layer number increases. This is mainly due to the impedance mismatch between free space and the conducting medium. Therefore, adequate surface exposure for conducting

Table 1 Fill rate, SE_{Total} and thickness of Ti₃C₂T_x/MLPAN and other EMI shielding materials

Materials	Fill rate [wt%]	SE _{Total} [dB]	Thickness [mm]	Ref.
Ti ₃ C ₂ T _x /MLPAN	63.6	61.8	0.11	This work
MWCNT/polyacrylate composites	10	25	1.5	33
rGo/PEI nanocomposites	2.5	26	0.08	34
rGo/ps	7	45.1	2.5	35
PLA/graphite nanocomposite foam	2.5	45	2	36
GNPs/PP composites	10	19.3	0.9	37
Ti ₂ CT _x /WAX	80	47.5	0.8	38
Annealed Ti ₃ C ₂ T _x /WAX composite	90	32	1	39
Nb ₂ CT _x /WAX nanocomposites	80	44.09	1	40
rGo/phenolic	70	43.4	0.3	41
NbC-PyC foam	37.2	54.8	0.5	42
CNF-GN networks	17.2 (GN)	28	0.27	43
m-Ti ₃ C ₂ T _x film	15	11.8	0.1	44
PVDF/CNT/6 wt% Ni-chain composite films	6	23.6	0.3	45
PVDF/GNP/8 wt% Ni-chain composite films	8	57.3	0.6	45
Cotton-derived carbon network	—	26.9	0.3	46
MCGs	—	45.5	0.3	47
GA-CT	—	27	2	48

Table 2 Fill rate, density, SE_{Total} and thickness-normalized specific SE (SSE/d) of $Ti_3C_2T_x$ /MLPAN and other EMI shielding materials

Materials	Fill rate [wt%]	Density [$mg\ cm^{-3}$]	SE_{Total} [dB]	SSE/d [$dB\ cm^2\ g^{-1}$]	Ref.
$Ti_3C_2T_x$ /MLPAN	63.6	639.0	61.8	8535.9	This work
MWCNT/ABS	15	1050.4	50	432.7	49
Carbon black/EPDM	—	590	—	15.1	50
Graphene/PMMA foam	5	791.6	19	100	51
Graphene/PEDOT	25	1040	70	814	52
Graphene@ Fe_3O_4 /PEI foam	10	409	18.2	176	53
Graphene/WPU	7.7	1049.18	32	152.5	54
Graphene/SiBCN foam	0.5	640	18.56	223	55
MWCNT/PP	5 (vol%)	898.88	24	95.4	56
MWCNT/PS	20	1052.6	60	285	57
MWCNT/PC	20	1130	39	159.7	58
SWCNT/PS	7	560	18.56	275	59
Graphene/ps foam	30	450.3	29	257.6	60
SWCNT/epoxy	15	1748.25	25	71.5	3
MWCNT/CNF	75	770	46.4	4017.3	61
MWCNT-PEO/cellulose	40	1700	35	1372	62
D- $Ti_3C_2T_x$ /CNF	80	2073.95	25.8	2647	63

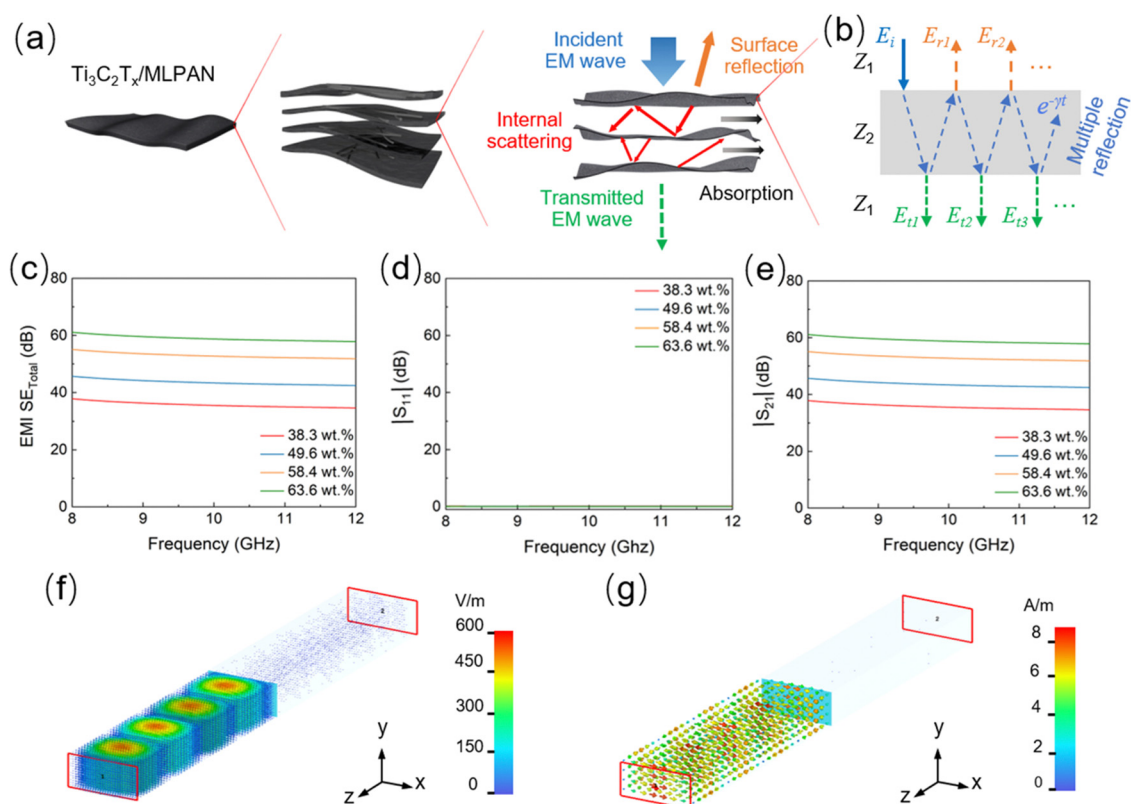


Fig. 5 Principle and electromagnetic simulations. (a) Schematic of the EMI shielding principle of the dual-scale multilayer $Ti_3C_2T_x$ /MLPAN hybrid fabric. (b) Multiple reflections occurred inside monolayer $Ti_3C_2T_x$ when the material thickness was lower than the corresponding skin depth, where γ is the propagation constant and t is the thickness of the material. Simulation results of (c) SE_{Total} , and the corresponding S -parameters include (d) $|S_{11}|$ and (e) $|S_{21}|$. Field distribution simulation results for electromagnetic waves including the (f) electric field and (g) magnetic field.

materials can be considered as an effective method to improve EMI shielding properties.

We further performed time domain simulation to verify the EMI shielding principle of $Ti_3C_2T_x$ /MLPAN and the electromagnetic field behavior during the penetration of plane electromagnetic waves *via* the computer simulation technology microwave studio (CST MWS 2019) software. A four-layer

sandwich structure approximate model (Fig. S21, ESI[†]) was used to simulate as-prepared $Ti_3C_2T_x$ /MLPAN (details in ESI[†]). Particularly, the conductivity of the external $Ti_3C_2T_x$ was set to be different from the internal one because the coating densities of $Ti_3C_2T_x$ were different as mentioned before. Simulation results showed conductivity-dependent properties including high $|S_{21}|$, low $|S_{11}|$, as well as SE_{Total} from 38.2 dB to 61.8 dB,

which are consistent with the test results from VNA (Fig. 5c–e). The field distribution simulation of electromagnetic waves including electric and magnetic fields was also performed. It was found that the electric field intensity rapidly attenuated to $\sim 0.07\%$ of its initial value as it passed through $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ (Fig. 5f and Fig. S22, ESI†), which agrees well with experimental data. A similar situation was also found in the magnetic field distribution results (Fig. 5g and Fig. S23, ESI†), which corroborated the test results from VNA and illuminated the application potential for the flexible and dual-scale multilayer $\text{Ti}_3\text{C}_2\text{T}_x/\text{PAN}$ fabric in EMI shielding and electromagnetic protection.

Conclusions

In this work, we have proposed a time-difference blow-spinning technology and fabricated an MLPAN nanofiber substrate in one step. By further conducting modification with the as-prepared MXene ($\text{Ti}_3\text{C}_2\text{T}_x$) solution *via* dip-coating, an ultra-light and flexible hybrid fabric ($\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$) was obtained. The primary multilayer nanofiber-network structure from MLPAN and a secondary nanoscale multilayer structure from $\text{Ti}_3\text{C}_2\text{T}_x$ were verified *via* a series of micromorphological characterization methods. Due to the network structure of the PAN fiber, the density of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ was measured to be as low as 639.0 mg cm^{-3} . By coating with a highly conductive MXene, $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ exhibited good electrical properties including a conductivity of $23327.40 \text{ S m}^{-1}$ and sheet resistance of $0.39 \Omega \text{ sq}^{-1}$. By VNA testing, the hybrid fabric exhibited a high EMI SE up to 61.8 dB and a superior SSE/d of $8535.9 \text{ dB cm}^2 \text{ g}^{-1}$, which is considered the synergistic EMI shielding effect of multiple reflections and internal scattering. Moreover, $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ showed both remarkable flexibility and mechanical stability, enabling it to be bent for five thousand cycles. This work developed a mass-production strategy for morphologically adjustable multilayer nanofibers and provided the possibility of applying structurally designed advanced fabric in large-scale, portable, flexible and curved-surface EMI shielding and electromagnetic protection.

Experimental

Materials

Polyacrylonitrile (PAN, $M_w = 150\,000$), dimethyl sulfoxide (DMSO, 99.8%), TiH_2 (400 mesh, 99%), Al (5–6 μm , 99.8%), and TiC (400 mesh, 98%) were purchased from Shanghai Aladdin Bio-Chem Technology Co. Ltd. Fluorocarbon surfactant (FS-3100) was purchased from DuPont Research & Development and Management Co. Ltd. All reagents were used without further purification.

Fabrication of PAN fiber substrates

First, 0.14 g of PAN ($M_w = 150\,000$) was dispersed in 100.00 g of DMSO and stirred for 2 h at 70 °C. Then, 30–50 μL of FS-3100 can be selected to add to the precursor solution depending on the actual ambient temperature and humidity. To perform

time-difference blow-spinning, the solution was injected into two integrated blow-spinning apparatus with a liquid-gas two-channel six-needle module and a rotating fiber collector. The internal pressure of the collector was adjusted to negative by an air pump to assist fiber deposition. During blow spinning, the airflow velocity was set to $4.5 \text{ m}^3 \text{ h}^{-1}$, and the injection speed of the solution was kept at a value of 2.0 mL h^{-1} .

Synthesis of Ti_3AlC_2 powder

Ti_3AlC_2 was synthesized as described in our previous work.³⁰ Typically, TiH_2 , Al, and TiC powders were mixed in a 1:1.2:2 mole ratio, followed by ball-milling for 18 h. The mixture was then sintered in a tube oven at 1450 °C for 2 h in a flowing Ar atmosphere. On crushing and sieving the resulting compact powder, Ti_3AlC_2 powder with a size of $< 38 \mu\text{m}$ was obtained.

Preparation of $\text{Ti}_3\text{C}_2\text{T}_x$ suspension

The few-layer $\text{Ti}_3\text{C}_2\text{T}_x$ suspension was synthesized by etching the Ti_3AlC_2 MAX phase in LiF/HCl hybrid etchant according to the previously reported route.¹⁶ Typically, a total of 3.0 g of Ti_3AlC_2 powder was gradually added (over the course of 3 min) to the LiF (4.8 g)/HCl (60 mL, 9 M) mixture. Then, the mixture was left under continuous stirring at room temperature for 24 h. Afterward, the resultant acidic mixture was washed repeatedly with deionized water *via* centrifugation at 3500 rpm for 5 min per cycle until the pH of the supernatant reached 6. The stable dark-green supernatant was collected to obtain the few-layer $\text{Ti}_3\text{C}_2\text{T}_x$ suspension with a concentration of $\sim 2.0 \times 10^{-3} \text{ g mL}^{-1}$, which was determined by filtering a known volume of the suspension and measuring the weight of the film after vacuum drying.

Preparation of $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ films

In a typical dip-coating process, the as-prepared MLPAN was immersed in the solution of the coating material ($\text{Ti}_3\text{C}_2\text{T}_x$) at a constant speed. PVB/ethanol was mixed into the $\text{Ti}_3\text{C}_2\text{T}_x$ aqueous solution, forming a 0.1 wt% PVB precursor solution for dip-coating. The $\text{Ti}_3\text{C}_2\text{T}_x$ thin layer was deposited on the MLPAN substrate and the solvent evaporated from the liquid while the substrate was pulled up, forming the $\text{Ti}_3\text{C}_2\text{T}_x/\text{MLPAN}$ hybrid fabric.

Dip coating processing. The rolling dip coating equipment consisted of three parts: one transmission shaft (radius = 2 cm), four squeezing shafts (radius = 1 cm, wheel base is adjustable), and one electrically driven collecting shaft (radius = 2 cm). Particularly, the squeezing shafts inside the precursor solution can help to eliminate the air inside the MLPAN; the squeezing shafts outside the precursor solution were used to extrude the excess solvent to accelerate the evaporation and forming process.

Materials characterization

X-ray powder diffraction data were collected using an XRD diffractometer (D/max 2500, Rigaku, Japan) in Cu K α radiation ($\lambda = 1.54178 \text{ \AA}$). The micromorphological analysis was performed by means of a field emission scanning electron microscope (FE-SEM, LEO-1530, Zeiss, Germany) with an EDS

attachment module and a transmission electron microscope (TEM, JEM-F200_TFEG, JEOL, Japan). The thickness of the as-prepared sample was measured by an atomic force microscope (AFM, Dimension ICON, Bruker, Germany). Thermogravimetric analysis (TGA) was performed using a thermogravimetric analyzer (STA 449 F3, Jupiter, Germany). The electrical properties of the as-prepared samples were examined on an IV/CV probe installation (PRECISION SYSTEMS INDUSTRIAL LIMITED, HK, China), including an EPS4 probe station, a PCA1000 LCR instrument, and PPTS-CV IV/CV test software. The IV/CV probe test system was linked to an electrochemical workstation (Metrohm Multi Autlab M204, Switzerland) for accurate data recording.

Author contributions

Wei Song: Validation, methodology, writing – original draft, formal analysis. Shuang Hu: writing – review & editing. Jiaxiang Lu: writing – review & editing. Liang Su: writing – review & editing. Zhemin Li: writing – review & editing. Junchen Liu: formal analysis. Yufeng Wu: formal analysis. Jianan Song: writing – review & editing. Zhenglian Liu: writing – review & editing. Shuaikai Xu: conceptualization, writing – review & editing, project administration, funding acquisition. Sen Lin: conceptualization, validation, writing – review & editing, project administration, funding acquisition.

Conflicts of interest

There are no conflicts to declare.

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