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## 2D WS<sub>2</sub> embedded PVDF nanocomposites for photosensitive piezoelectric nanogenerators with a colossal energy conversion efficiency of ~25.6%†

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Benefiting from the advantages of low cost, light weight and mechanical flexibility, piezoelectric nanogenerators have the potential for application in renewable energy harvesting from various unexplored sources. Here, we report the demonstration of the record efficiency of flexible piezoelectric nanogenerators (PENG) using composites of polyvinylidene fluoride (PVDF) and chemically exfoliated tungsten disulfide (WS<sub>2</sub>) nanosheets, which are found to be strongly photosensitive, making them attractive for self-powered optical devices. The presence of two-dimensional (2D) WS<sub>2</sub> nanosheets in the PVDF matrix plays a dual role in enhancing the nucleation of the electroactive  $\beta$ -phase as well as inducing strong photosensitivity in the nanocomposite. The PVDF-WS<sub>2</sub> composed flexible device is able to produce an enormously high output voltage of ~116 V (for an impact of 105 kPa) and a piezoelectric energy conversion efficiency of ~25.6%, which is the highest among the reported values for PVDF-2D material based self-poled piezoelectric nanogenerators. This self-poled piezo-phototronic device exhibits strain-dependent photocurrent at zero bias and exhibits a responsivity of  $6.98 \times 10^{-3} \text{ A W}^{-1}$  at 0.75% strain under the illumination of 410 nm. The fabricated PENG is also able to harvest energy from routine human activities (finger tapping, writing on paper, mouse clicking, etc.) and movement of human body parts. These results open up a new horizon in piezo-phototronic materials through the realization of photosensitive multi-functional PENGs, which can be scaled up for fabricating compact, high performance, portable and self-powered wearable electronic devices for smart sensor applications.

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## Introduction

Due to the increasing demand for sensors and IoT based application in recent years, miniaturized nanogenerator (piezoelectric, triboelectric, thermoelectric, etc.) devices for driving low power systems are studied with immense interest. The advantage of the nanogenerator devices is that they can convert mechanical, optical, and thermal energy into electrical energy and their abundant resources are available, and apart from those, regular human activities are also huge sources of bio-mechanical energy. Amongst different types of nanogenerators, piezoelectric nanogenerators are quite promising in energy harvesting owing to their efficacy towards portable and wearable electronic systems. Following the first demonstration

of ZnO nanowire array based piezoelectric nanogenerators by Wang *et al.*,<sup>1</sup> several piezoelectric materials such as GaN, PZT, BaTiO<sub>3</sub>, NaNbO<sub>3</sub>, LiNbO<sub>3</sub>, etc. have evolved.<sup>2–9</sup> Amongst them, inorganic perovskites have high piezoelectric coefficients but are less selective for applications in the flexible nanogenerator domain due to the lack of bio-compatibility, durability, complex synthesis procedure and high toxicity. Some other materials with high piezo-coefficients possess complicated structures coupled with high fabrication cost and hence are not suitable for commercial applications. In contrast, piezoelectric polymers and copolymers, *viz.*, poly(vinylidene fluoride) (PVDF), are attractive for energy harvesting as they possess high piezoelectric coefficient, chemical and thermal stability, bio-compatibility and light weight.<sup>9–12</sup> This semi-crystalline polar polymer generally exhibits active crystalline phases ( $\alpha$ ,  $\beta$ ,  $\gamma$ , and  $\delta$  (polar version of ( $\alpha$ )) depending on their chain configurations.<sup>10,13</sup> Amongst them, the  $\alpha$ -phase (TGTTG conformation) is not electroactive and the  $\gamma$ -phase (T<sub>3</sub>GT<sub>3</sub>G conformation) has a weak piezoelectric coefficient, while the  $\beta$ -phase (TTTT conformation) is the most desirable, as it possesses the highest dipole moment per unit volume. Commercially available PVDF is mostly found in the  $\alpha$ -phase; hence, it is not suit-

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able for piezoelectric nanogenerators. Previous studies have revealed that the presence of the  $\beta$ -phase has a massive impact on the piezoelectricity of PVDF.<sup>11,14–16</sup> The dominance of the  $\beta$ -phase can be achieved through preferential orientation of  $-\text{CH}_2/-\text{CF}_2$  dipoles in the direction normal to the chain axis of PVDF and several protocols such as mechanical stretching, electrospinning, electrical poling, and high temperature annealing have been performed for achieving the  $\beta$ -phase.<sup>17–20</sup>

Recent studies have reported that the introduction of fillers in the PVDF matrix is another effective way for achieving the  $\beta$ -phase. The piezo-characteristics of hybrid structures obtained by introducing fillers such as metal nanoparticles, perovskites, semiconductors and 2D materials in the PVDF matrix have been studied widely because of their easy fabrication process, compatibility and mechanical flexibility.<sup>10,11,14,21–26</sup> Furthermore, it has been found that hybrid devices are sensitive to various environmental conditions such as temperature, light, *etc.*<sup>16,17,27–33</sup> In this regard, the introduction of optically active fillers in PVDF is extremely interesting as it can make the hybrid system suitable for application in next generation photo-piezotronic devices.<sup>13,34–37</sup> To date, most of the aforementioned devices demonstrating piezotronic and photo-piezotronic effects have been realized by coupling semiconducting and perovskite nanostructures with piezoelectric films. Here, we report the piezoelectric and photosensing properties of two dimensional (2D) transition metal dichalcogenide incorporated PVDF nanocomposites on flexible substrates. We have demonstrated that 2D semiconductor tungsten disulphide ( $\text{WS}_2$ ) nanosheets, with a broadband absorption spectrum, can serve as efficient fillers into the PVDF matrix to develop nanogenerators as well as self-powered optical sensors. Chemically exfoliated  $\text{WS}_2$  nanosheet in DMF solvent has good dispersity in the PVDF

matrix, forming a homogeneous, uniformly distributed PVDF- $\text{WS}_2$  nanocomposite. Therefore, the crystallinity and optical properties of  $\text{WS}_2$  remain unchanged in the PVDF matrix. The uniform distribution of  $\text{WS}_2$  nanosheets in the PVDF matrix and their good interfacial properties in nanocomposites result in a superior piezoelectric response. Fabricated self-poled PVDF- $\text{WS}_2$  nanogenerator devices yield an enormously high piezoelectric output voltage of  $\sim 116.0$  V for an stress of only 105 kPa and  $\sim 4$  V by a simple mechanical bending induced strain of  $\sim 0.75\%$ . The device exhibits a record energy conversion efficiency of  $\sim 25.6\%$  using 2D materials with a photo-responsivity of  $\sim 6.98 \times 10^{-3} \text{ A W}^{-1}$  at zero bias at 0.75% strain.

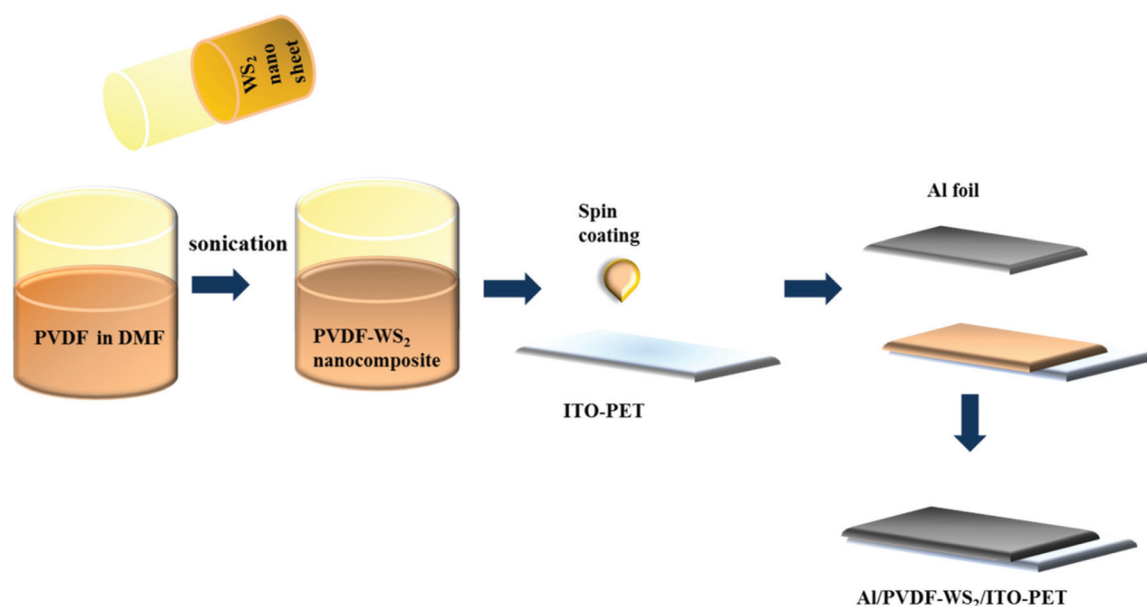
## Experimental section

### Materials and methods

All the chemicals ( $\text{WS}_2$  powder, PVDF powder) and solvents (hexane, DMF) were purchased from Sigma-Aldrich and used without further purification.

### Synthesis of the PVDF- $\text{WS}_2$ nanocomposite

Commercially available PVDF powder (0.25 g) was added to chemically exfoliated  $\text{WS}_2$  nanosheets dispersed in DMF (see ESI Synthesis of  $\text{WS}_2$  nanosheet<sup>†</sup>), and PVDF- $\text{WS}_2$  nanocomposites of different filler ratios (0.037%, 0.075%, 0.125%, 0.187% and 0.262%) were prepared. To get a homogeneous mixture of PVDF- $\text{WS}_2$ , the solution was sonicated for 4 h. This mixture was then used for further measurements and device fabrication purposes (Scheme 1). To synthesize the control PVDF based nanogenerator, bare PVDF powder was added into DMF solvent in the absence of  $\text{WS}_2$  nanosheets using a similar procedure.



**Scheme 1** Schematic of the fabrication process of the PVDF- $\text{WS}_2$  composed piezoelectric nanocomposite device.

### Device fabrication

The homogeneous solution of the PVDF-WS<sub>2</sub> nanocomposite was spin-coated at 1000 rpm for 10 s on an ITO coated PET substrate. Aluminum (Al) foil was attached on the top of the spin coated films so that the PVDF-WS<sub>2</sub> composite was sandwiched between the top Al electrode and ITO coated PET substrate (bottom electrode). Thereafter, the device was kept for drying at 60 °C for 1.5 h to obtain the final device in the Al/PVDF-WS<sub>2</sub>/ITO-PET configuration (Scheme 1).

### Characterization methods

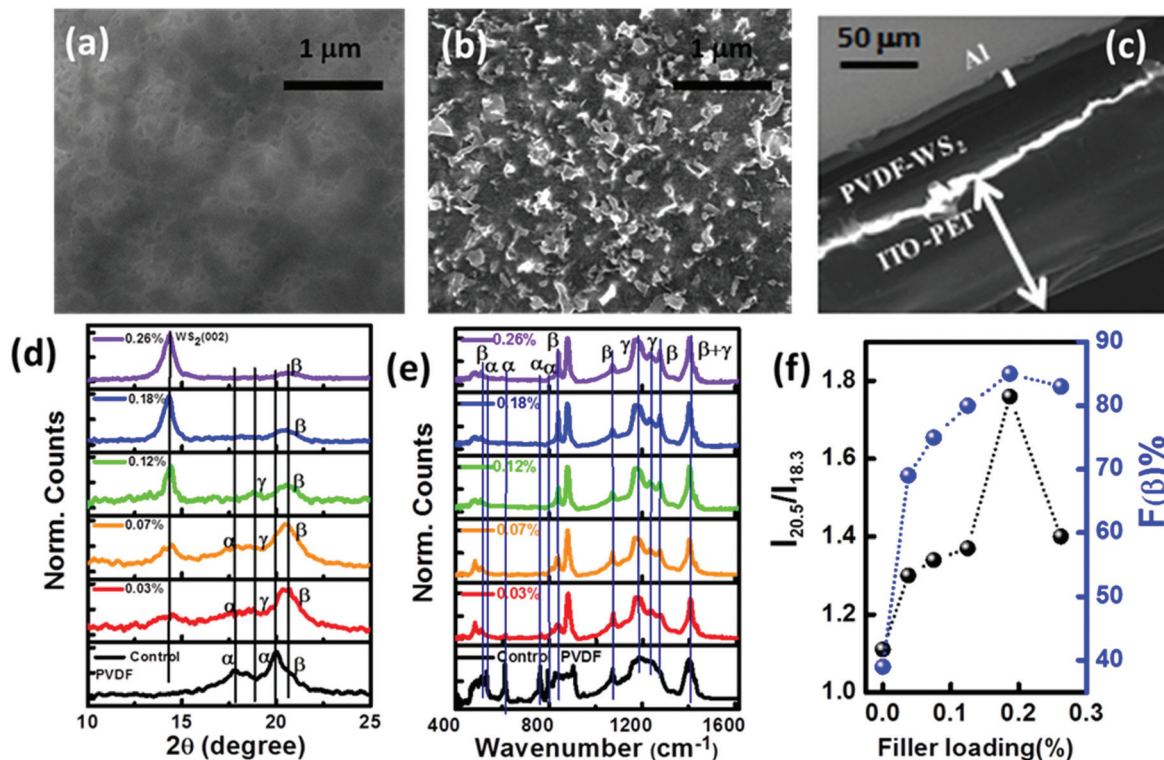
The phase and crystallinity of control PVDF and PVDF-WS<sub>2</sub> nanocomposites were investigated by X-ray diffraction (Rigaku MiniFlex with Cu-K<sub>α</sub>, 1.54 Å). Fourier transform infrared (FTIR) spectroscopy was carried out using a Jasco FTIR-6300 spectrometer. Surface profiles of the nanocomposites and device structure were examined using a field-emission scanning electron microscope (FESEM) equipped with an energy-dispersive X-ray (EDX) spectrometer, with an electron energy of 20 keV. The morphology of chemically exfoliated WS<sub>2</sub> nanosheets was investigated using a high-resolution transmission electron microscope (FEI-TECNAI G2 20ST, energy 200 keV) and an atomic force microscope (di INNOVA). The absorption spectrum of the chemically exfoliated WS<sub>2</sub> nanosheets was measured using a UV-Vis spectrometer (Shimadzu-UV-Vis 2600

Spectrophotometer) and Raman spectra were recorded using a spectrometer (LabRam HR Evolution; HORIBA France SAS-532 nm laser). A Keithley 2450 source meter and a digital oscilloscope (SMO702 (scientific)) were used for the electrical measurements.

## Results and discussion

Scanning electron micrographs (SEM) showing the morphology of PVDF and PVDF-WS<sub>2</sub> nanocomposites are presented in Fig. 1(a–c). The surface of control PVDF (without any WS<sub>2</sub>) nanosheets is shown in Fig. 1(a), and is relatively smoother as compared to that of the nanocomposite presented in Fig. 1(b), and nanosheets are found to be well dispersed in the PVDF matrix. From the cross-sectional SEM image (Fig. 1(c)), the thickness of the PVDF-WS<sub>2</sub> nanocomposite film is estimated to be  $\sim 40 \pm 3 \mu\text{m}$  and that of the composed device including the electrodes is  $\sim 150 \pm 5 \mu\text{m}$ .

PVDF-WS<sub>2</sub> nanocomposites with a higher fraction of the  $\beta$ -phase are attractive because of their improved piezoelectric response. Here, XRD and FTIR analyses have been used to investigate the influence of the WS<sub>2</sub> nanosheet filler on the crystalline structures of PVDF. (The SEM images of nanocomposites with different filler ratios are presented in Fig. S3†.) Fig. 1(d) shows the XRD pattern of control PVDF and



**Fig. 1** Typical SEM images of (a) control PVDF and (b) the PVDF-WS<sub>2</sub> nanocomposite. (c) Cross-sectional view of a PVDF-WS<sub>2</sub> nanogenerator device. (d) X-ray diffraction patterns and (e) Fourier transform infrared spectra of control PVDF and PVDF-WS<sub>2</sub> nanocomposite films at various WS<sub>2</sub> filler loadings, (f) variation of intensity ratio  $\frac{I_{20.5}}{I_{18.3}}$  from the XRD pattern and relative  $\beta$ -phase content from FTIR spectra as a function of the WS<sub>2</sub> filler content.

PVDF-WS<sub>2</sub> nanocomposites. For control PVDF, the characteristic nonpolar  $\alpha$ -phase peaks are observed at 17.6° (100), 18.3° (202) and 19.9° (110).<sup>13,38,39</sup> On the other hand, PVDF-WS<sub>2</sub> shows a characteristic sharp peak at 14.4° demonstrating the crystalline phase of WS<sub>2</sub> (002).<sup>40,41</sup> Furthermore, the XRD pattern of the bare nanosheet exhibits the characteristic diffraction peak at 14.4° (002) of WS<sub>2</sub> (Fig. S2(c)†). All the above results reveal the existence of the semiconducting WS<sub>2</sub> phase in the nanocomposite without any degradation. In the PVDF-WS<sub>2</sub> nanocomposite, the dominant XRD peak observed at 20.5° (200) emanates from the electroactive crystalline  $\beta$ -phase of PVDF,<sup>21,27</sup> which appears for all filler concentrations. We observe that the diffraction peak intensities for the  $\alpha$ -phase at 17.6°, 18.3°, and 19.9° diminish gradually with increasing filler concentration (Fig. 1(d)). The HRTEM and selected area electron diffraction (SAED) pattern of bare WS<sub>2</sub> nanosheets (Fig. S1(b), (c) and (d)†) also indicate the existence of the (002) plane. Thus, the dominance of the  $\beta$ -phase peak and the diminishing nature of the  $\alpha$ -phase peak of PVDF indicate the WS<sub>2</sub> mediated reorientation of functional groups in PVDF. To validate this premise by studying the existence of functional groups, FTIR measurements have been performed (Fig. 1(e)). In control PVDF, the vibrational bands appearing at 614, 763, 794 and 975 cm<sup>-1</sup> are attributed to the non-polar  $\alpha$ -phase<sup>21,42</sup> and they are related to the mixed CF<sub>2</sub> bending, CCC skeletal vibration, the in plane bending or rocking vibration and CH<sub>2</sub> rocking vibration, respectively.<sup>21</sup> On the other hand, the bands appearing at 510 and 1074 cm<sup>-1</sup> correspond to the  $\beta$ -phase and features observed at 1234 and 1177 cm<sup>-1</sup><sup>42</sup> are the signatures of  $\gamma$ -phases. The absorption observed at 1401 cm<sup>-1</sup> is considered to be a contribution from both  $\beta$  and  $\gamma$  phases.<sup>42</sup> The appearance of two new sharp peaks at 839 and 1274 cm<sup>-1</sup> in the FTIR spectra of the nanocomposites is the signature of intense electroactive  $\beta$ -phase formation<sup>16,17,42</sup> and the peak at 839 cm<sup>-1</sup> is due to mixed CF<sub>2</sub> asymmetric stretching and CF<sub>2</sub> rocking vibration and the peak at 1274 cm<sup>-1</sup> is related to C-F stretching vibrations. The vibrational band at 1074 cm<sup>-1</sup> is related to the linear dependency on the thickness of the film and independent of its crystallinity. From the FTIR measurements, it is observed that the nucleation of the electroactive  $\beta$ -phase and the reduction of the non-polar  $\alpha$ -phase take place due to the addition of WS<sub>2</sub> in the PVDF matrix, as shown in Fig. 1(e). The relative fraction of the  $\beta$ -phase,  $F(\beta)$ , present in the samples can be calculated by using

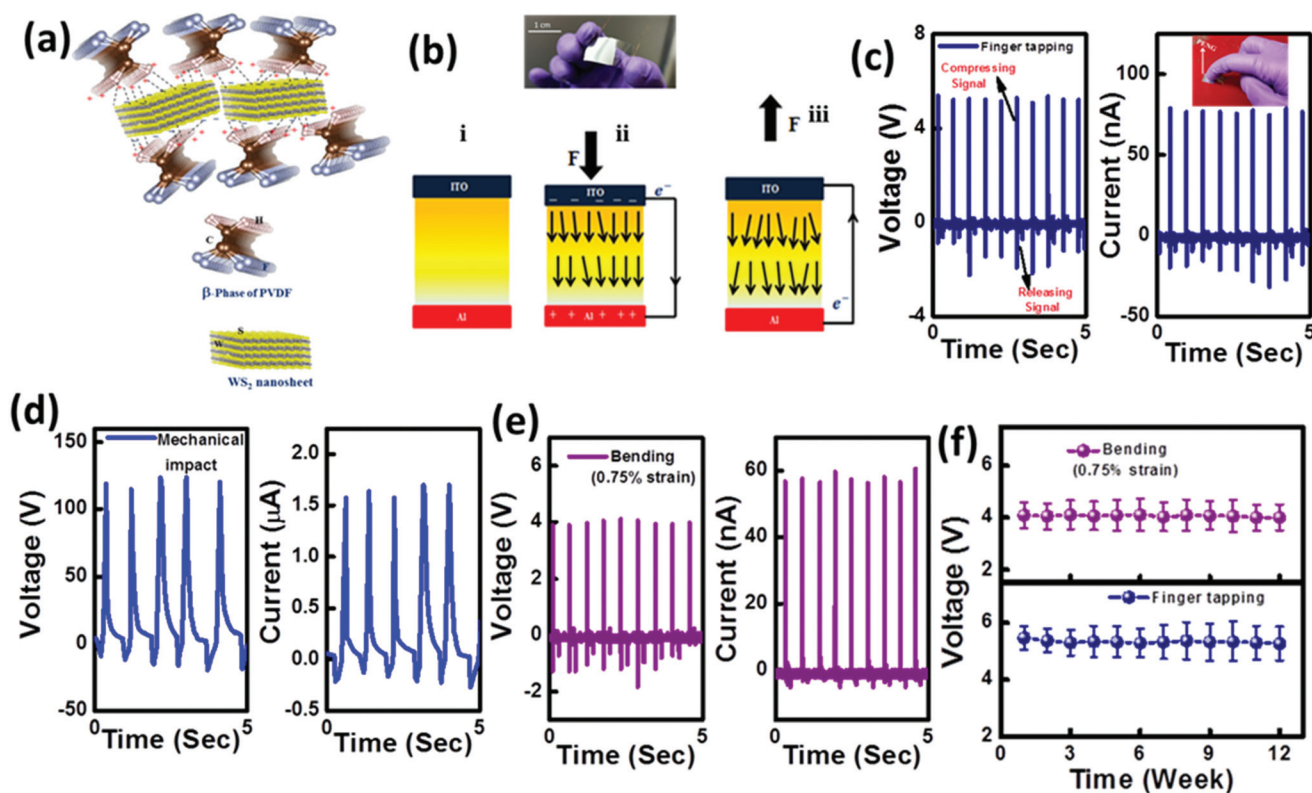
$$F(\beta) = \frac{A_{\beta}}{\left(\frac{K_{\beta}}{K_{\alpha}}\right)A_{\alpha} + A_{\beta}} \quad (1)$$

where  $A_{\alpha}$  and  $A_{\beta}$  are the absorbance (as measured using FTIR spectroscopy) of the bands at 763 and 839 cm<sup>-1</sup> corresponding to the  $\alpha$ - and  $\beta$ -phases, respectively, and  $K_{\alpha}$  and  $K_{\beta}$  are the absorption coefficients at the respective wave number, which are  $6.1 \times 10^4$  and  $7.7 \times 10^4$  cm<sup>2</sup> mol<sup>-1</sup>, respectively.<sup>10,43</sup> From the above estimation, the electroactive  $\beta$ -phase fraction,

responsible for piezoelectric response, is plotted as a function of the WS<sub>2</sub> concentration in Fig. 1(f). It is observed that  $F(\beta)$  increases initially with increasing WS<sub>2</sub> content and attains the highest value of ~85% for a WS<sub>2</sub> filler loading of 0.187% beyond which it decreases. Such a decrease in  $F(\beta)$  beyond a critical loading could be explained by taking into consideration the possibility of WS<sub>2</sub> nanosheet agglomeration within the PVDF polymer matrix, as the filler loading concentration beyond 0.187% may lower the surface charge interaction of WS<sub>2</sub> with PVDF. From the XRD pattern, the ratio of the intensity of the peaks at 20.5° and 18.3°  $\left(\frac{I_{20.5}}{I_{18.3}}\right)$  has been calculated, which provides a qualitative idea about the relative content of the  $\beta$ -phase and  $\alpha$ -phase,<sup>44</sup> as shown in Fig. 1(f). It is observed that this ratio attains its highest value at 0.187% filler content, in corroboration with the FTIR results.<sup>10,21,43,44</sup>

The working mechanism of the hybrid nanogenerator can be explained in terms of the combined effect of the PVDF dipoles and the surface charges of WS<sub>2</sub>. The opposite polarity surface charges on WS<sub>2</sub> interact with the dipoles (-CF<sub>2</sub>-/-CH<sub>2</sub>-) of PVDF, which results in the development of charge density over the nanocomposite, leading to the formation of the piezoelectrically active  $\beta$ -phase through the surface charge induced electrostatic interactions (Fig. 2(a)).<sup>45,46</sup> The (-CH<sub>2</sub>-CF<sub>2</sub>) bond stretching vibration, dipole-dipole interaction between WS<sub>2</sub> nanosheets and PVDF and the stress induced polarization are the main reasons behind the conversion from the nonpolar  $\alpha$ -phase to the electroactive  $\beta$ -phase<sup>13</sup> in the nanocomposite. WS<sub>2</sub> nanosheets act here as a nucleating agent to form the polar crystalline  $\beta$ -phase in the PVDF-WS<sub>2</sub> nanocomposite. The working mechanism of this PVDF-WS<sub>2</sub> composite is schematically presented in Fig. 2(b), where the attraction between the surface charge of WS<sub>2</sub> and the dipoles of PVDF is highlighted. In the absence of any external mechanical impact, all the dipoles within the hybrid nanocomposite film are oriented randomly, resulting in a zero net dipole moment (Fig. 2(b)(i)). The application of an external mechanical force aligns the dipoles in the direction of the applied force through stress induced polarization. When the piezoelectric nanogenerator PENG is subjected to vertical compressive stress, the crystal structure of the nanocomposite is deformed, *i.e.*, the dipolar distribution within the nanocomposite is altered, which consequently produces positive and negative potential on the two electrodes (Fig. 2(b)(ii)). The potential difference between the top and the bottom electrodes generates a piezoelectric potential which drives the flow of electrons from one electrode to the other through an external circuit. As the compressive strain is released, the piezoelectric potential vanishes immediately (Fig. 2(b)(iii)) and to compensate for that, the electrons accumulated near the electrode flow back to the other one through the external circuit, leading to an electric signal in the opposite direction. So, an alternating voltage signal is obtained during this continuous vertical compression and release. Piezoelectric outputs from the PVDF-WS<sub>2</sub> composite nanogenerator, as obtained under vertical repetitive com-





**Fig. 2** Schematic mechanisms of (a) interactions between  $\text{WS}_2$  and PVDF and (b) operation of a piezo-electric nanogenerator and the device image is shown in the inset. Open-circuit output voltage and current from the PVDF- $\text{WS}_2$  PENG for 0.187% filler loading for repeated (c) finger tapping, (d) mechanical impact ( $\sim 105$  kPa) and (e) bend/release action, (f) long-term stability performance of the PVDF- $\text{WS}_2$  PENG in laboratory atmosphere for 12 weeks on repeated mechanical tapping and bending.

pression and release of manual human finger tapping ( $\sim 3.1$  kPa pressure), are depicted in Fig. 2(c). Polarity switching tests have been carried out to verify whether the output voltage originates from the piezoelectric phenomenon or not. As expected, we observe output voltages with an opposite sign from the nanogenerators when they are connected in the reverse configuration, confirming that the piezoelectric signals are reversible in nature (Fig. S4 (a) and (b)†). To study the effect of the filler concentration on the piezoelectric response, we have studied nanogenerators with different  $\text{WS}_2$  nanosheet concentrations (0.037%, 0.07%, 0.12%, 0.18% and 0.26%). The mechanical energy-harvesting features of these self-poled devices are examined without any electrical poling treatment. The piezo-response of all the nanogenerators is analyzed by applying repeated finger tapping with identical frequency (2 Hz) and the open circuit piezoelectric output voltages are recorded. From Fig. S4(c)† it is observed that the open-circuit piezoelectric voltage from the PVDF- $\text{WS}_2$  PENG increases initially with increasing  $\text{WS}_2$  filler loading and the PENG device with 0.187% filler concentration produces the highest piezoelectric open circuit output voltage of  $\sim 5.3$  V. So, from this above result, it can be claimed that the best performance is delivered by the device with 0.187% filler concentration, in corroboration with the XRD and FTIR results.<sup>10,13</sup> The nanogenerator has been subjected to varying external mechanical forces (7.55, 9.05 and

11.33 kPa at 2 Hz) and it is observed that the generated piezo-potential increases with increasing external mechanical impact, as depicted in Fig. S4(d)†. The increase of piezo-potential can be ascribed to the preferential orientation of the electric dipoles in the nanohybrids in a particular direction due to the external stress induced effect.<sup>47</sup> Under a periodic applied stress of  $\sim 105$  kPa, the average output voltage from the self-powered nanogenerator is  $\sim 116$  V under open circuit conditions, which is depicted in Fig. 2(d). The output performance of this PENG is found to be superior to those of other reported PVDF-2D and perovskite based devices presented in Table 1. In the PVDF- $\text{WS}_2$  system, the polymer PVDF matrix interacts with the filler by electrostatic dipole-dipole interaction. For comparison, we can discuss the mechanism in the graphene-PVDF nano-composite: in the case of the graphene or functionalized graphene-PVDF interface, H atoms of  $-\text{CH}_2/-\text{CF}_2$  dipoles tend to approach the graphene surface and electrostatic interactions between the  $\text{sp}^2$  hybridization take place between the C atoms of graphene and the low electronegativity H atoms in the PVDF chain. This interfacial interaction affects the motion of PVDF, resulting in the formation of the  $\beta$ -phase.<sup>10</sup> A similar mechanism is also responsible for other well-known semiconductors (ZnO,  $\text{TiO}_2$ , etc.) and perovskites ( $\text{CsPbBr}_3$ ,  $\text{MAPbI}_3$ ,  $\text{FAPbBr}_3$ ,  $\text{BaTiO}_3$ ).<sup>10,13,14,34</sup> In our study, we have used chemically exfoliated two dimensional  $\text{WS}_2$  nanosheets as a filler in PVDF. With the  $\text{WS}_2$  nanosheets being

**Table 1** Comparison of the piezoelectric performance of the fabricated PVDF-WS<sub>2</sub> PENG with reported 2D and perovskite-PVDF based devices

Name of sample	Poling	Output voltage	Power density & efficiency	Photoactivity	Ref.
PVDF-AIO/rGO	Self-poled	36 V at 31.19 kPa	3.63 μW cm <sup>-2</sup> 12.47%	No	16
Ce <sup>3+</sup> doped-graphene/PVDF	Electrospinning	11 V at 6.6 kPa	0.052 μW cm <sup>-2</sup>	No	17
PVDF-functionalized GO	Electrospinning	62 V at 40 kPa	48.3 μW cm <sup>-2</sup>	No	27
PVDF-graphene	Electromagnetic punch	18 V at 0.45 N	—	No	18
rGO-Ag/PVDF	External electric field of 148 kV cm <sup>-1</sup>	18 V	14.72 μW cm <sup>-2</sup> 0.65%	No	39
PVDF-graphene-silver	Self-poled	0.1 V at 5.2 kPa	0.75 nW cm <sup>-2</sup> 15%	Yes	56
FAPbBr <sub>3</sub> /PVDF	Self-poled	26.2 V at 0.5 MPa	22.88 μW cm <sup>-2</sup>	Yes	14
PVDF-MAPI	Self-poled	1.5 V at 2 kPa	2.5 μW cm <sup>-2</sup>	Yes	29
hBN-PVDF NF	Electrospinning	68 V at 24.5 kPa	53.2 μW cm <sup>-2</sup>	No	25
Graphene-BT NP-PVDF	Electrospinning	11 V under mechanical strain	0.656 μW cm <sup>-2</sup>	No	10
PVDF NF-MoS <sub>2</sub>	Electrospinning	9 V at 8.8 kPa	16 nW cm <sup>-2</sup>	No	26
GO-PVDF NF	Electrospinning	7 V at 8.8 kPa	0.62 μW cm <sup>-2</sup>	No	15
<b>PVDF-WS<sub>2</sub></b>	<b>Self-poled</b>	<b>116 V at 105 kPa</b>	<b>48.5 μW cm<sup>-2</sup> (3.1 kPa) 25.6%</b>	<b>Yes</b>	<b>This study</b>

intrinsically negatively charged and the constituent S atoms having higher electronegativity compared to Zn, Ti, Cs, Ba, C, B *etc.*, the intrinsic polar WS<sub>2</sub> surface can easily interact with CF<sub>2</sub> or CH<sub>2</sub> groups of PVDF and initiate the β-phase nucleation. As a result of this, the PVDF-WS<sub>2</sub> nanocomposite offers a higher value of β-phase fraction ( $F(\beta)$ ) leading to a higher piezoelectric output voltage. In contrast, many fillers having high intrinsic conductivity (graphene, some perovskites, *etc.*) cause unwanted carrier recombination in the polymer matrix and result in higher leakage current within the nanocomposite, which deteriorates the piezoelectric performance of the nanogenerator.<sup>13</sup> In addition, the semiconducting nature of WS<sub>2</sub> may enhance the local electric field to generate induced charges, resulting in a stronger Coulomb force which is helpful to obtain a higher fraction of the β-phase. Besides, good dispersivity of chemically exfoliated WS<sub>2</sub> (in DMF solvent) in the PVDF matrix offers homogeneity and leads to a uniform distribution of WS<sub>2</sub> throughout the nanocomposite without agglomeration. This aggregation-free filler-matrix composition is very important for enhanced nanogenerator performance. The uniform distribution of WS<sub>2</sub> nanosheets in the PVDF matrix accelerates the nucleation of the piezoelectric polar β-phase in the PVDF-WS<sub>2</sub> nanocomposite. Consequently, the piezoelectric performance of the PVDF-WS<sub>2</sub> based PENG is enhanced and is found to be superior to that of the other reported systems.

The fabricated PENG is also capable of generating piezoelectric output under repeated bending and releasing at a low strain (~0.75% based on the calculation presented in the ESI†), which is shown in Fig. 2(e). The piezoelectric output voltage from this composite PVDF-WS<sub>2</sub> nanogenerator is found to be higher, ~44 times for finger tapping and 40 times in the case of a mechanical impact (~11.33 kPa) than that of the control PVDF sample, as presented in Fig. S5(a) and (b).† This is attributed to the interfacial or Maxwell-Wagner-Sillars polarization,<sup>48–50</sup> which induces a change in the dielectric constant of the samples leading to the enhancement of the piezoelectric output<sup>13,51,52</sup> of the PVDF-WS<sub>2</sub> nanogenerator device. The reproducibility of this PVDF-WS<sub>2</sub> device has been tested by measuring under the same external compressive force (finger tapping, 0.75% mechanical

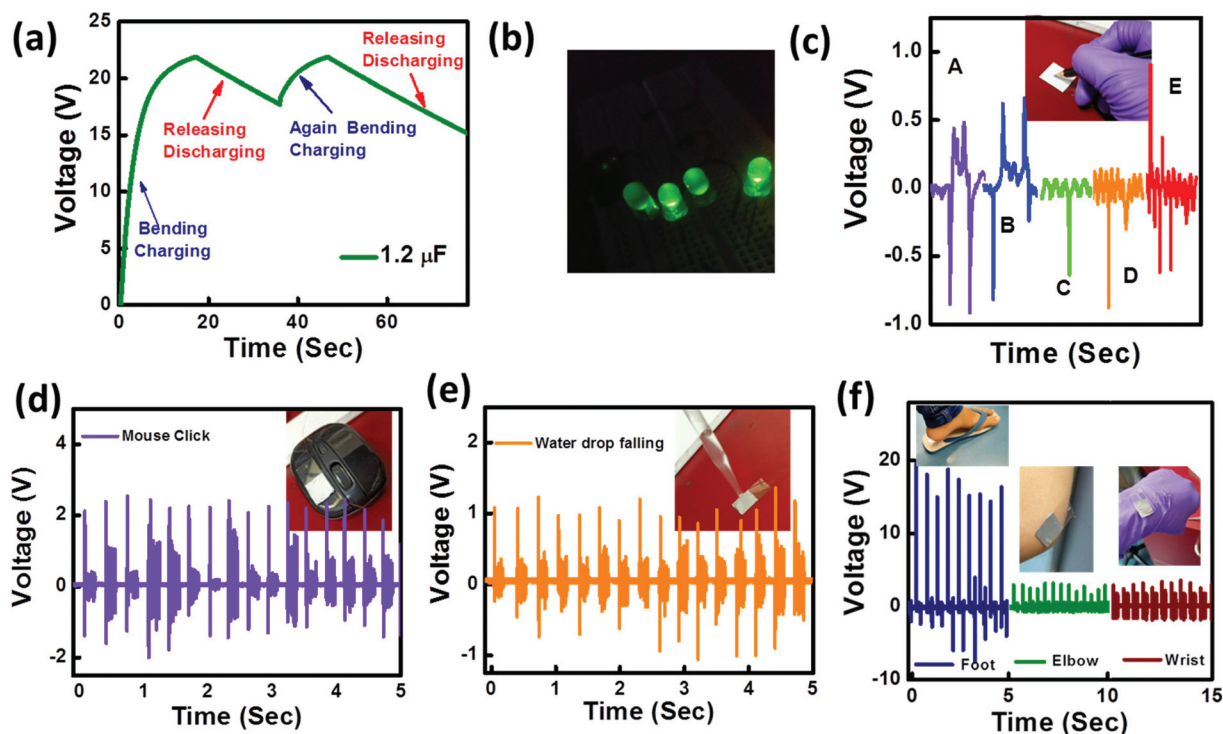
strain) in a weekly interval. The absence of any noticeable degradation in the output voltage over a prolonged period of 12 weeks unambiguously confirms the stability of the fabricated device under ambient conditions (Fig. 2(f)). Again, during repetitive operation, the PENG is found to be operative even after ~50 bending cycles (0.75% strain, 2 Hz) with no significant degradation (Fig. S5(c)†).

The PVDF-WS<sub>2</sub> based piezoelectric nanogenerator exhibits an excellent output performance without applying any electrical poling, which is attractive for practical applications. To investigate the driving capability of the PENG, a capacitor (~1.2 μF) has been charged through a full wave bridge rectifier circuit consisting of four diodes (Fig. S6(a)†), which converts the generated AC signal to a DC signal. The rectified output voltage from the nanogenerator can charge the capacitor up to ~21.8 V only in ~17 s, as shown in Fig. 3(a). The cyclic charging and discharging behavior of the capacitor shows high energy drive capability and the reproducibility of the PENG. The stored energy in the capacitor has been used to drive commercial LEDs (four green, output power ~110 mW (max.) each at a forward current of ~25 mA (max.)) revealing the practical use of the device (Fig. 3(b)). Based on the charging capacity, we can calculate the stored energy across the capacitor using,

$E_e = \frac{CV^2}{2}$ , where  $C$  is the capacitance and  $V$  is the voltage under the steady state conditions after a definite time. On the other hand, the mechanical strain energy  $E_s$  can be calculated

as,  $E_s = \frac{YAL\sigma^2}{2}$ , where  $A$  is the active area (~1.0 × 1.0 cm<sup>2</sup>),  $L$  is the thickness of the composite (~150 μm) including electrodes,  $\sigma$  is the strain (~0.75%) and  $Y$  is the Young's modulus of the nanocomposite, which has been estimated to be about ~2.66 GPa using the rule of mixtures (as presented in the ESI†).<sup>53,54</sup> The mechanical energy is calculated to be ~1.12 × 10<sup>-3</sup> J and the generated output electrical energy is found to be ~2.85 × 10<sup>-4</sup> J, yielding the energy conversion efficiency,  $\eta = \frac{E_e}{E_s}$  of this fabricated PENG to be ~25.6%. This extracted

efficiency value is found to be the highest among the previously reported piezoelectric nanogenerators<sup>16,38,55</sup> using 2D



**Fig. 3** (a) Charging–discharging behavior of a capacitor of 1.2  $\mu\text{F}$  using the PENG device, (b) glowing of four green commercial LEDs ( $I_{\text{power}} = 110 \text{ mW}$  (max)). The output voltage from the PENG device due to (c) writing on paper, (d) clicking of a computer mouse, (e) falling water drops and (f) different human body movements and the images are shown in insets.

and perovskite materials (Table 1). We have also performed the charging of capacitors with different values of capacitance (Fig. S6(b)†). The energy conversion efficiency is estimated to be  $\sim 25.0\%$ ,  $24.5\%$ , and  $25.1\%$  for the three different capacitance values 1.4  $\mu\text{F}$ , 1.7  $\mu\text{F}$  and 2.2  $\mu\text{F}$ , respectively, which also indicates the high energy conversion efficiency of the fabricated PENG. To demonstrate the energy harvesting performance from a routine activity like writing on paper, which acts as a source of mechanical stress, two ends of a PENG are connected to an oscilloscope (schematic circuit diagram is shown in Fig. S6(c)†). During the drawing of lines and writing of different alphabets using a simple pencil, a piezoelectric output voltage of  $\sim 0.5\text{--}0.8 \text{ V}$  is generated as shown in Fig. 3(c), demonstrating that the device can be used as a smart writing board. Furthermore, when the PENG is attached to a computer mouse, an instantaneous piezo-voltage ( $\sim 2.1 \text{ V}$ ) is generated (Fig. 3(d)) for each click of the mouse. Thus, the PVDF-WS<sub>2</sub> nanocomposite device can generate piezoelectric voltage by simple human activities (finger tapping, writing, mouse clicking, etc.), making it a potential candidate for bio-mechanical energy harvesting. This PVDF-WS<sub>2</sub> composed PENG can also produce output voltage due to the impact of a water droplet falling onto it, as presented in Fig. 3(e). An output voltage of  $\sim 1.0 \text{ V}$  for impacting water droplets with a velocity of  $\sim 0.92 \text{ m s}^{-1}$  reveals that the device can also be used as an energy harvester from rainwater. In addition, the PVDF-WS<sub>2</sub> based PENG is able to produce output voltage under a minute strain pro-

duced due to the movement of different parts of the human body with an average magnitude of  $\sim 17.0$ ,  $3.0$  and  $2.7 \text{ V}$  for foot, elbow and wrist movements, respectively, as depicted in Fig. 3(f). Hence, the fabricated nanogenerator is very effective to harvest energy from regular biomechanical activities. The piezoelectric characteristics with record output voltage and superior energy conversion efficiency under mechanical as well as biomechanical actions confer the novelty of the PVDF-WS<sub>2</sub> hybrid compared to the other materials reported in the literature.

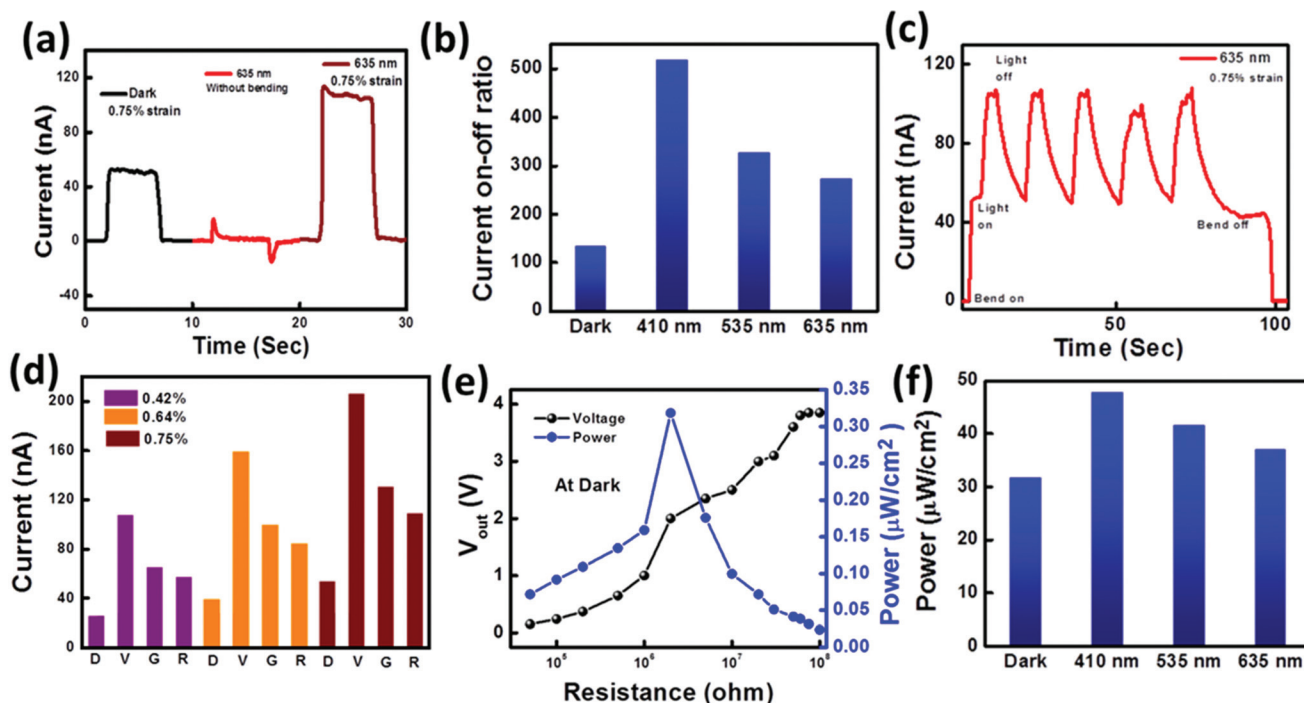
### Photo-sensors

To study the piezo-phototronic based characteristics of the samples, the temporal response of the PVDF-WS<sub>2</sub> nanocomposite device has been studied under repetitive application of strain. The output currents of the control PVDF (Fig. S7(a)†) and PVDF-WS<sub>2</sub> (Fig. 4(a)) nanogenerators are monitored under an identical strain ( $\sim 0.75\%$ ) condition and the relative increase ( $\Delta I$ ) in the output current is expressed as<sup>56</sup>

$$\frac{\Delta I}{I_0} = \frac{I_{\text{strain}} - I_0}{I_0} \quad (2)$$

where  $I_{\text{strain}}$  and  $I_0$  are the output currents in the presence and absence of external strain, respectively. It is observed that the ratio  $\frac{\Delta I}{I_0}$  is  $\sim 22$  (Fig. S7(a)†) for control PVDF, which is enhanced to  $\sim 134$  for the PVDF-WS<sub>2</sub> PENG, as shown in





**Fig. 4** (a)  $I-t$  characteristics of the PVDF-WS<sub>2</sub> PENG at zero bias with bending–releasing in the dark, without bending under 635 nm illumination and bending–releasing under 635 nm illumination, (b) bent-to-relaxed current on–off ratio for  $\sim 0.75\%$  strain in the dark and under illumination of different wavelengths, (c)  $I-t$  characteristics at zero bias with 0.75% strain and 635 nm illumination, (d) variation of currents in the dark and illuminated conditions under application of different strains. D, V, G and R represent dark, violet, green and red illumination respectively, (e) dependence of piezoelectric power–voltage on load resistance in the dark and (f) comparison of power under dark and illuminated conditions in the finger tapping mode.

Fig. 4(a). This remarkable enhancement in piezoelectric response of the PVDF-WS<sub>2</sub> nanocomposite can be attributed to the higher density of piezo-charges in the nanocomposite under an applied mechanical stress. Interaction between semiconducting WS<sub>2</sub> nanosheets and PVDF dipoles induces polarization charges that can enhance the electrical transport under external stress even at a zero bias.<sup>15,34</sup> The time-dependent ( $I-t$ ) characteristics of the PVDF-WS<sub>2</sub> device at zero bias have also been studied (Fig. 4(a)). The absence of photocurrent in control PVDF even in the bent condition (Fig. S7(b)†), reveals that the photo-response is contributed by semiconducting WS<sub>2</sub> nanosheets only. To confirm the piezo-phototronic effect of the PVDF-WS<sub>2</sub> nanocomposite, output currents have been measured by applying an identical external compressive stress under illumination (635 nm) and darkness (Fig. 4(a)). The stressed-to-relaxed current ratio (for  $\sim 0.75\%$  strain) increases under illumination, as compared to that in the dark (Fig. 4(b)). The above ratio is found to be 519, 329 and 274 under violet (0.49 mW cm<sup>-2</sup>), green (0.36 mW cm<sup>-2</sup>) and red (0.4 mW cm<sup>-2</sup>) illumination, respectively which are higher than the dark value of  $\sim 134$ , due to the strong optical absorption of WS<sub>2</sub> nanosheets.

Further measurements have been performed to confirm the piezo-photoresponse of the PVDF-WS<sub>2</sub> nanocomposite device, first by applying compressive stress through mechanical bending followed by periodical illumination. Under illumination at 635 nm (0.4 mW cm<sup>-2</sup>), a measurable photocurrent is

observed and is depicted in Fig. 4(c). Under the application of a compressive strain, piezo-polarization charges are developed within the nanocomposite, which assist the efficient transport of photogenerated e–h pairs by reducing the recombination probability of the charge carriers. The photogenerated e–h pairs can be separated by the polarization induced built-in-field and an enhancement of photocurrent is observed. The photocurrent response under each cycle is consistent and repeatable with no observable decay. A bending test has been performed to explore the mechanical stability, which is very important for flexible photodetector applications. Here, a good switching behavior of the current is observed in Fig. 4(c) under periodic illumination of light at zero bias with rise and decay times of 1.4 s and 5.4 s, respectively which are faster than the previously reported PVDF based photosensitive PENG.<sup>28,36,37</sup> The rise and decay times are defined as the time required for the photocurrent to increase from 10% to 90% and to decrease from 90% to 10% of its maximum value, respectively and most importantly this photocurrent remains almost invariable even after several bending cycles. Under bent conditions in the self-powered mode, the current change depends on both the applied strain and the optical illumination. To understand the effect of the external mechanical stress, this measurement has been performed under variable compressive strain. For a higher strain, the built-in electric field is stronger across the electrodes and under illumination the reduced recombination



of photogenerated e–h pairs contributes to the increase in the current up to a strain magnitude of  $\sim 0.8\%$ , which is depicted in Fig. 4(d).

We can estimate the relative change of photocurrent under strained conditions<sup>56</sup> by using

$$\frac{\Delta I_p}{I_{p,o}} = \frac{I_{ps} - I_{p,o}}{I_{p,o}} \quad (3)$$

where  $I_{ps}$  and  $I_{p,o}$  are the photocurrent with and without external stress under light illumination, respectively. The photosensing behavior of PVDF-WS<sub>2</sub> nanocomposites has been investigated without the application of any external bias and external bending strain, which is depicted in Fig. S8(a).† These results show that the values of  $\frac{\Delta I_p}{I_{p,o}}$  under illumination of 410 nm

( $\sim 91$ ), 535 nm ( $\sim 72$ ) and 635 nm ( $\sim 65$ ) are lower than the  $\frac{\Delta I}{I_o}$  value under dark conditions ( $\sim 134$ ) for the same strain configuration ( $\sim 0.75\%$ ) at zero bias. This difference is attributed to the piezoelectric screening effect from photogenerated carriers. Under irradiation, photogenerated carriers partially screen the piezo-polarization charges, the mechanism of which is schematically depicted in Fig. S8(b).† As indicated in the band diagram, the piezo-potential may facilitate the charge carrier separation due to the reduction of barrier height. The screening of piezo-potential reduces the open circuit output voltage under illuminated conditions compared with in the dark (Fig. S8(c)†). Thus, the piezo-polarization screening effect reduces the relative increase of the photocurrent under a strained condition, as compared to the current without any illumination. The photo-responsivity ( $R_\lambda$ ) and external quantum efficiency (EQE) of the PVDF-WS<sub>2</sub> PENG at zero bias are calculated as,

$$R_\lambda = \frac{I_L - I_D}{P_L \times S} \text{ and EQE} = \frac{1240R_\lambda}{\lambda},$$

where  $I_L$  and  $I_D$  are the current under illuminated and dark conditions, respectively,  $P_L$  is the power of illumination light and  $\lambda$  is the wavelength of illumination.<sup>36</sup> Both the responsivity and EQE are found to be higher under bent conditions when compared to the control sample in the relaxed state (Table 2), which indicates that the strain indeed controls the performance of the photodetector. Both the photocurrent and the photoresponsivity of the device depend strongly upon the applied mechanical strain and this self-poled device exhibits a high photoresponsivity ( $6.98 \times 10^{-3} \text{ A W}^{-1}$ ) and superior detectivity ( $8.61 \times 10^{10} \text{ cm H}^{1/2} \text{ W}^{-1}$ ) under 0.75% strain at zero bias

at 410 nm illumination. It is noticed that the photo-responsivity increases from  $6.98 \times 10^{-5} \text{ A W}^{-1}$  (unstrained) to  $6.98 \times 10^{-3} \text{ A W}^{-1}$  (for 0.75% strain), and higher values of responsivity and EQE are attributed to the strain induced piezo-polarization charges, as they induce enhanced transport of photogenerated e–h pairs with reduced recombination of charge carriers.<sup>36</sup> In practice, the level of electrical power of the system depends on the external load resistance and therefore, the performance of the device can be checked by measuring the output voltages across varying load resistance. The generated output voltage from the PENG across a load resistor gradually increases with increasing load resistance as shown in Fig. 4(e) and reaches a saturation value at higher resistance which almost corresponds to the open circuit condition. The instantaneous power density can be estimated as  $P = \frac{V_{out}^2}{A \times R_L}$ , where  $A$  is the effective contact area and  $V_{out}$  is the effective output voltage considering the internal resistance ( $R_{int}$ ) of the PENG and can be calculated as

$$V_{out} = \frac{R_L}{R_{int} + R_L} V = \frac{1}{1 + \frac{R_{int}}{R_L}} V. \quad (4)$$

If  $R_L \ll R_{int}$ , then with increasing  $R_L$ , the increment of  $V_{out}$  is low. However, whenever  $R_L$  is comparable to  $R_{int}$ ,  $V_{out}$  increases monotonically with increasing  $R_L$ . Finally, at  $R_L \gg R_{int}$ , it provides an open circuit condition, in this regime with changing  $R$ ,  $V_{out}$  does not change substantially. It can be observed that the PENG attains a maximum value ( $\sim 30 \mu\text{W cm}^{-2}$ ) under 2.0 M $\Omega$  load resistance in the dark (Fig. 4(e)). These results are comparable with the other piezoelectric material based PVDF devices.<sup>51,55</sup> Under illuminated conditions, photocarriers are generated inside this PENG which enhance the conductivity and reduce the internal resistance of the PENG under illuminated conditions as compared to the dark ones (Fig. S8(d)†). It is estimated that the internal resistance of the PENG is  $\sim 2.0 \text{ M}\Omega$  under dark conditions and 0.76, 1.08 and 1.3 M $\Omega$  under illumination of 410 nm, 535 nm and 635 nm, respectively. As a result of the photoactivity of the PVDF-WS<sub>2</sub> nanocomposite, the piezoelectric output power density is found to be higher under illumination and exhibits a maximum value of  $\sim 48.5 \mu\text{W cm}^{-2}$  under 410 nm illumination, as depicted in Fig. 4(f). The piezoelectric power density is higher for the violet light (410 nm) than for the green (535 nm) and red (635 nm) illumination following the absorption pattern of WS<sub>2</sub> nanosheets. This result indicates that the fabricated PVDF-WS<sub>2</sub> composed PENG is able to generate

**Table 2** Variation of responsivity and EQE with varying strains

	Without strain		Strain (0.50%)		Strain (0.64%)		Strain (0.75%)	
	$R_\lambda$ ( $\text{A W}^{-1}$ )	EQE	$R_\lambda$ ( $\text{A W}^{-1}$ )	EQE	$R_\lambda$ ( $\text{A W}^{-1}$ )	EQE	$R_\lambda$ ( $\text{A W}^{-1}$ )	EQE
Violet (410 nm)	$6.98 \times 10^{-5}$	$2.11 \times 10^{-4}$	$3.584 \times 10^{-3}$	$10.8 \times 10^{-3}$	$5.316 \times 10^{-3}$	0.016	$6.98 \times 10^{-3}$	0.0211
Green (535 nm)	$5.12 \times 10^{-5}$	$1.186 \times 10^{-4}$	$2.615 \times 10^{-3}$	$6.049 \times 10^{-3}$	$3.97 \times 10^{-3}$	$9.2 \times 10^{-3}$	$5.16 \times 10^{-3}$	0.0119
Red (635 nm)	$4.24 \times 10^{-5}$	$8.345 \times 10^{-5}$	$2.02 \times 10^{-3}$	$3.975 \times 10^{-3}$	$2.99 \times 10^{-3}$	$5.885 \times 10^{-3}$	$3.876 \times 10^{-3}$	$7.636 \times 10^{-3}$

enhanced piezoelectric output power under illuminated conditions and exhibits wavelength selectivity, with the highest energy harvesting efficiency at  $\sim 410$  nm. Thus, the fabricated 2D material based PVDF-WS<sub>2</sub> hybrid nanogenerator can act as a high performance electrical power source as well as a self-powered flexible broadband visible light photodetector driven by a novel piezo-phototronic effect and is capable of harvesting enhanced energy under illumination with potential applications in future wearable and portable self-powered sensor systems.

## Conclusions

Self-poled PVDF-WS<sub>2</sub> nanocomposites have been synthesized by using chemically exfoliated two-dimensional WS<sub>2</sub> nanosheets and PVDF polymers using a low cost, eco-friendly technique. The exfoliated WS<sub>2</sub> nanosheets with an optimized concentration of  $\sim 0.187\%$  not only enhance the piezoelectric output voltage but also induce photo-activity in the nanocomposite devices compared with the pristine PVDF. A colossal piezoelectric voltage of  $\sim 116$  V (for  $\sim 105$  kPa) with a power density ( $\sim 48.5 \mu\text{W cm}^{-2}$  for  $\sim 3.1$  kPa) and a record energy conversion efficiency of  $\sim 25.6\%$  among 2D material based nanocomposites have been demonstrated. Apart from mechanical impacts, the hybrid PENG is also very sensitive to human bio-mechanical movements and thus paves a promising route to drive IoT based portable devices. Furthermore, the piezo-coupled photocurrent ratio in the mechanically stressed (strain  $\sim 0.75\%$ ) to relaxed configuration is enhanced by 287% under illumination ( $\sim 410$  nm), producing a high photoresponsivity ( $6.98 \times 10^{-3} \text{ A W}^{-1}$ ) and detectivity ( $8.61 \times 10^{10} \text{ cm H}^{1/2} \text{ W}^{-1}$ ). A high output power of  $\sim 48.5 \mu\text{W cm}^{-2}$  generated under violet light irradiation makes the system promising for extracting power under illuminated conditions. The excellent stability and capability of producing electrical power from the surrounding environment and routine activities make the PVDF-WS<sub>2</sub> system attractive for application in future wearable, stretchable and portable electronic devices.

## Conflicts of interest

There are no conflicts to declare.

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