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Current development, optimisation strategies and future perspectives for lead-free dielectric ceramics in high field and high energy density capacitors

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To meet the United Nations' sustainable development goal of affordable and clean energy, there has been a growing need for low-cost, green, and safe energy storage technologies. High-field and energy-density capacitors have gained substantial attention from academics and industry, particularly for power electronics, where they will play a key role in optimising the performance of management systems in electric vehicles. The key figure of merit, energy density (W_{rec}), for high-field applications has dramatically increased year-on-year from 2020 to 2024, as evidenced by over 250 papers, demonstrating ever larger W_{rec} values. This review briefly introduces the background and principles of high energy density ceramics, but its focus is to provide constructive and comprehensive insight into the evaluation of W_{rec} , E_{max} , ΔP , and η , and more importantly, the normalised metrics, $W_{\text{rec}}/E_{\text{max}}$ and $W_{\text{rec}}/\Delta P$ in lead-free dielectric ceramics. We also present several optimisation strategies for materials modification and process innovation that have been recently proposed before providing perspectives for the further development of high-field and high-energy density capacitors.

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1. Introduction

Global energy demand has been increasing rapidly due to industrialisation, technological advancements, and the expanding economies of countries. According to a recent International Energy Agency (IEA) report,¹ global energy consumption is expected to rise by 3.4% per year until 2026. To minimise global CO₂ emissions, renewable, smart, and clean energy systems with high energy storage performance must be rapidly deployed to achieve the United Nation's sustainability goal.² The energy density of electrostatic or dielectric capacitors is far smaller than in batteries and fuel cells.^{3–5} However, they possess the highest power density due to ultra-fast charge–

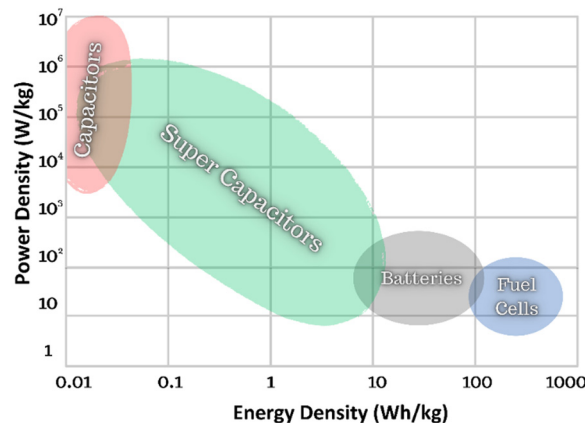


Fig. 1 Power density vs. energy density (Ragone Plot) for different energy storage technologies.



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discharge, as shown in the Ragone Plot (Fig. 1)^{6–8} and form an integral part of the power management of battery systems.

BaTiO₃-based multilayer ceramic capacitors are commonly employed as filters and de-couplers in the consumer electronics industry, with a market valued at USD ~ 3 billion in 2023, with a 4.9% compound annual growth rate in the US market (2024–2032).⁷ Ceramic dielectrics are popular due to their temperature stability (e.g. X7R MLCCs),⁹ fast charge–discharge speed (ms or ns), strong mechanical and fatigue resistance, and low manufacturing costs compared to polymer dielectrics.¹⁰ However, BaTiO₃-based dielectrics break down at relatively low fields (<350 kV cm^{–1}), limiting their energy density, and above 130 °C their permittivity declines markedly.¹⁰ Developing



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including electroceramics, solid-state electrolytes and high entropy perovskite oxides, using skillset ranging from crystal chemistry and crystallography to advanced processing of ceramics and prototype devices. He published 40+ peer-reviewed articles with a H-index of 24 and >3800 citations (Google Scholar). He is currently the deputy research lead for Nano and Functional Materials at the Department of Materials, a member of the early career editorial board for the Journal of Advanced Dielectric (JAD), and a professional member (MIMMM) of IOM3 and the Royal Society of Chemistry (MRSC).



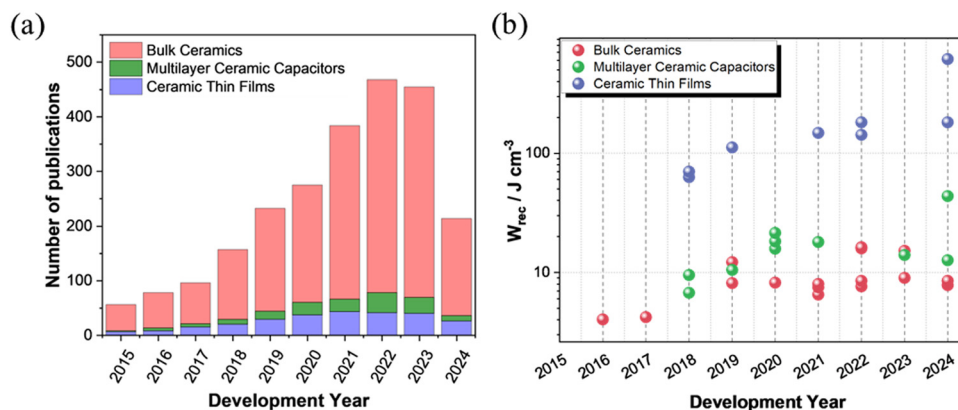


Fig. 2 (a) Number of publications, Web of Science (keywords of high energy density ceramics, multilayer ceramic capacitors, and ceramic thin films, excluding glass, polymer, and composite). (b) Development of W_{rec} in bulk ceramics, ceramic multilayers, and ceramic thin films for energy storage applications from 2015 to 2024.

next-generation dielectric ceramics with higher energy density for high-field/voltage and high temperature ($> 200\text{ }^{\circ}\text{C}$) capacitor applications has therefore drawn increasing interest, particularly for power electronics in the automotive sector.

Lead (Pb) based dielectric ceramics, such as La-doped Pb (Zr, Ti) O_3 ,^{11,12} have been used in pulsed capacitor applications for a number of years due to their exceptional power density and efficiency. However, researchers have been favouring Pb-free alternatives in the past decade due to legislation that restricts the use of Pb in consumer electronics. Fig. 2(a) illustrates the increase in publications on lead-free high-energy density ceramics from 2015 (~ 50 papers) to 2023 (~ 500 papers). Bulk ceramics based on BaTiO₃(BT), Na_{0.5}Bi_{0.5}TiO₃ (NBT), BiFeO₃ (BF), AgNbO₃ (AN) and NaNbO₃(NN)-based ceramics, account for 80% of the publications, with multilayer ceramic capacitors (MLCCs) 8% and ceramic thin films 12%.

The highest energy densities reported in the past 10 years for Pb-free bulk ceramics, MLCCs, and ceramic thin films are 16.3 J cm^{-3} , 43.5 J cm^{-3} , and 182 J cm^{-3} , respectively. These values are achieved with approximate thicknesses of $50\text{--}150\text{ }\mu\text{m}$ for bulk ceramics, $5\text{--}20\text{ }\mu\text{m}$ for MLCCs, and $0.1\text{--}0.6\text{ }\mu\text{m}$ for ceramic thin films, and electrode areas typically ranging from 0.075 to 0.12 cm^2 . Bulk ceramics and MLCCs are prepared by solid-state sintering, with energy density influenced by factors such as electrode area and thickness. In contrast, ceramic thin films are formed using different techniques, where factors like substrate choice (strain), electrode area and thickness play a crucial role. However, further research in Pb-free dielectric ceramics is still required to offer high energy density ($W_{\text{rec}} > 20\text{ J cm}^{-3}$) with efficiency ($\eta > 90\%$), wide frequency range ($1\text{--}1000\text{ Hz}$), large temperature range (-50 to $250\text{ }^{\circ}\text{C}$), low dielectric loss ($\tan \delta < 2.5\%$), fast charge-discharge time ($\tau_{0.9} < 100\text{ ns}$), co-fire compatibility with cost-effective internal electrodes and greater volumetric efficiency.

In the realm of energy storage capacitors, many companies such as Skelton Technologies, TDK, Taiyo Yuden, Panasonic Corporations, Maxwell Technologies (now part of Tesla, Inc.), Kyocera Corporation, Murata Manufacturing Co. Ltd, Knowles

Capacitors, and Ioxus, offer bulk ceramics and MLCCs tailored to specific applications. For instance, Knowles Precision Devices manufactures a wide selection of MLCCs, including AEC-Q200, Tandem and Open Mode, X8R and EMI filters, to meet the needs of electric and hybrid electric vehicle systems with a maximum voltage rating of 1 kV .¹³ Ceramic capacitor technology is expected to advance further with the MLCC market forecast to reach $\sim\text{USD } 16.77$ billion by 2030.¹⁴ High energy density and high voltage capacitors will be used in many applications¹⁵ as shown in Fig. 3, including but not limited to power electronics in electrical transportation, electronics, aerospace, pulse power applications and solar plants due to their high voltage tolerance, low loss, greater temperature and frequency stability and volumetric efficiency.⁹

2. Principles of energy storage performance in lead-free dielectric ceramics

Understanding the principles of energy storage performance is crucial for designing and optimising materials for specific applications. The chapter covers three main topics: energy storage density evaluation, polarisation, and dielectric breakdown strength.

2.1. Energy density evaluation of dielectric ceramics

The typical representation of a capacitor consists of two parallel electrodes with a dielectric between them, as shown in Fig. 4(a and b). In dielectric capacitors, an external electric field is applied to induce polarisation in the dielectric, allowing for the storage of electrical energy (Fig. 4a). When the electric field is removed, the capacitor releases the stored energy, and the dipoles return to their initial state (Fig. 4b). This ability to store and release energy rapidly makes electrostatic capacitors suitable for applications requiring high power density (P_D) for applications requiring ultrafast charge-discharge ($\tau_{0.9}$) cycles.





Fig. 3 Schematic diagram of MLCCs with key properties in developing the high energy performance and their different applications.

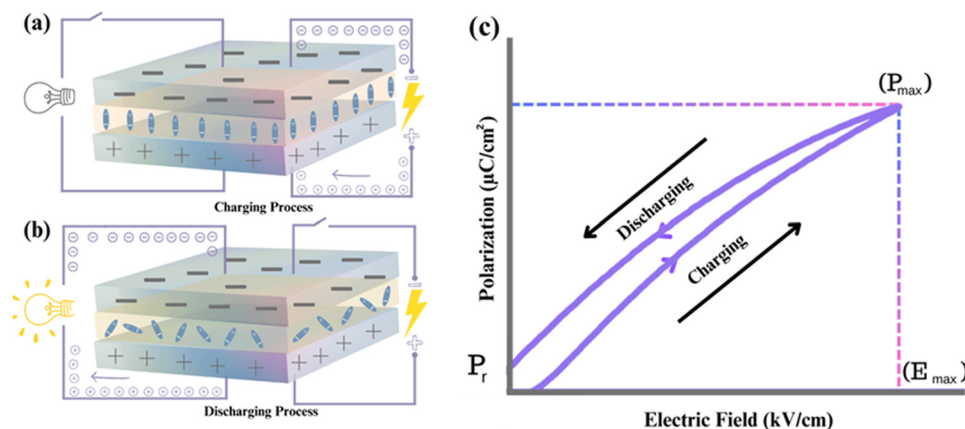


Fig. 4 (a) Charging process (b) discharging process (c) P - E loop of evaluating energy storage performance of the dielectric capacitors.

The energy storage of dielectric capacitors is related to capacitance (C), which is defined as the charge (dQ) induced by an external electric field (dV), as illustrated in Fig. 4c. The capacitance is calculated using the permittivity and geometry, as shown in eqn (1):

$$C = \frac{dQ}{dV} = \epsilon_0 \epsilon_r \frac{A}{t} \quad (1)$$

where ϵ_0 is the permittivity of the vacuum, ϵ_r is the relative permittivity, t is the thickness of the dielectric medium, and A is the area of the dielectric capacitors.

The energy storage density depends on ϵ_r and the applied electric field for all dielectrics. Due to energy dissipation *via* Joule heat loss, particularly in nonlinear dielectrics, the recoverable energy storage density (W_{rec}) is used to quantify the energy that can be recovered during the discharge cycle. W_{rec} is calculated as an integral of maximum polarisation ($P_{\max}$) and remnant polarisation (P_r), as shown in eqn (2):

$$W_{\text{rec}} = \int_{P_r}^{P_{\max}} E dP \quad (2)$$



Achieving high energy density in dielectrics involves a combination of high $P_{\max}$, low P_r , high breakdown strength, and low dielectric loss. Understanding and controlling these nonlinear effects is essential in various applications, as they may limit the W_{rec} . Moreover, energy efficiency (η) is an important indicator for dielectric capacitors, alongside W_{rec} , particularly in practical applications. Energy efficiency is expressed by eqn (3):

$$\eta = \frac{W_{\text{rec}}}{W_{\text{rec}} + W_{\text{loss}}} \quad (3)$$

where W_{loss} is the unrecoverable or lost energy density during discharging. High η is desirable for practical applications, ideally exceeding 90%, to minimise self-heating during operation.

2.2. Polarisation

Polarisation–electric (P – E) loops, obtained from ferroelectric hysteresis measurements, demonstrate characteristics such as $P_{\max}$ and P_r , coercive electric field (E_c), and $E_{\max}$. These loops are typically obtained by measuring charge with a classical sawyer-tower circuit,¹⁶ which provides a preliminary estimate of energy storage performance. In this context, it's important to note that the electric displacement–electric field (D – E) loops may maybe more theoretically accurate to evaluate the energy storage performance of a ceramic capacitor since W_{rec} values are evaluated under the application of electric field. However, most of the studies assess their materials using P – E instead of

D – E (based on ferroelectric hysteresis loops) because polarisation is closely related to the electric displacement based on the equation below:

$$D = \epsilon_0 E + P \quad (4)$$

where ϵ_0 , E and P are the vacuum permittivity, applied electric field and polarisation.

Based on the form features of P – E loops shown in Fig. 5, dielectrics are categorised into four specific groups: ferroelectric (FE), antiferroelectric (AFE), relaxor (RFE), and linear dielectric (LD).¹⁷ FEs, as shown in Fig. 5(a), exhibit high $P_{\max}$ and P_r , which collectively lead to nonlinear P – E loops, resulting in low $E_{\max}$ (less than 100 kV cm^{−1}), W_{rec} and η , making them unsuitable for energy storage capacitor applications. AFEs, Fig. 5(b), exhibit dual hysteresis characteristics, with linear behaviour and FE loops positioned before and after, respectively, the critical switching field, making them desirable for energy storage applications. RFEs, obtained through the process of chemical doping, exhibit slim polarisation hysteresis loops as shown in Fig. 5(c), high $P_{\max}$ and low P_r , ideal for high W_{rec} . LDs, in Fig. 5(d), on the other hand, typically exhibit low $P_{\max}$ and P_r due to their low ϵ_r but can theoretically achieve high efficiency ($\eta > 90\%$). The low energy storage density due to low $P_{\max}$ and ϵ_r ensures a low volumetric efficiency for any device but linear dielectrics with higher values of $P_{\max}$ and permittivity (> 500) would constitute a breakthrough in dielectric technology.¹⁸

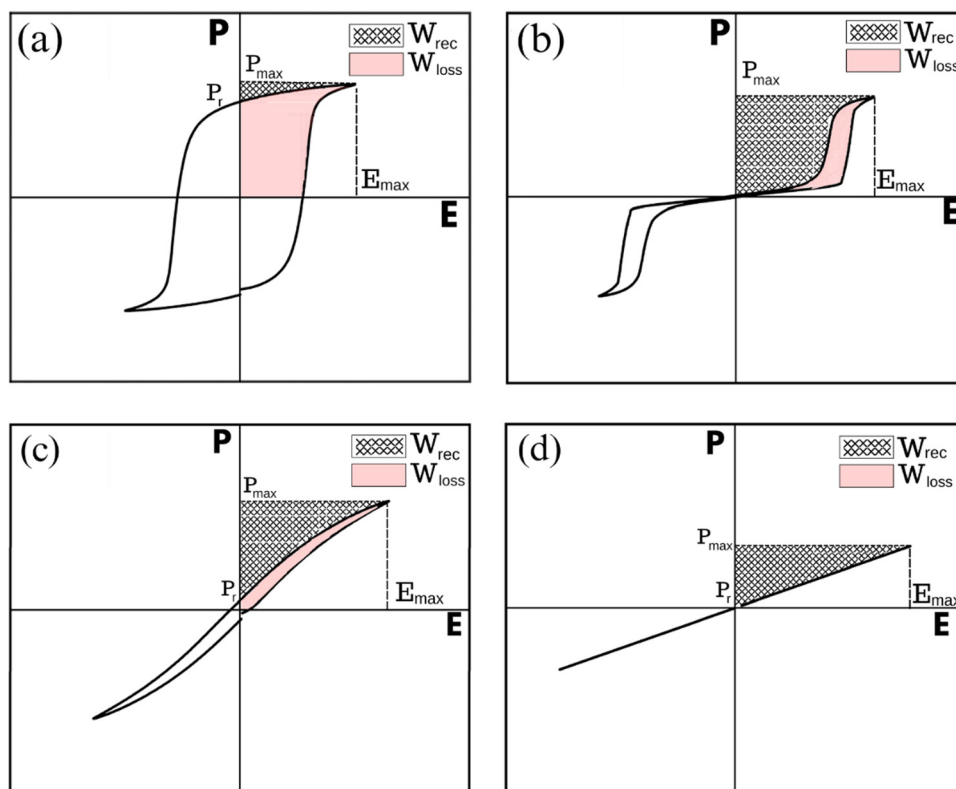


Fig. 5 Typical P – E loops for (a) ferroelectrics – FE (b) antiferroelectrics – AFE (c) relaxor ferroelectrics – RFE (d) linear dielectrics – LD.



Delta polarisation, $\Delta P (P_{\max} - P_r)$, is crucial for assessing the energy storage capabilities of dielectric materials and depends on many factors such as grain size, microstructure, core-shell morphology, and electrode area. Moreover, minimising P_r is essential for efficient energy storage, allowing for effective energy release with minimal losses. These parameters can be optimised through material design, processing, and other strategies to enhance energy storage performance. Understanding and maximising ΔP are imperative for designing materials with favourable P - E loop characteristics, ultimately enhancing energy storage performance.¹⁸

It is also critical to understand the origin of polarisation for the lead-free dielectric/ferroelectric ceramics since some ultra-high polarisation values ($> 50 \mu\text{C cm}^{-2}$, see Table 6 below) have been reported for dielectric thin films. It is impossible to get measured polarisation higher than spontaneous polarisation (P_s) which is a fixed value for a conventional ferroelectric (except the case for additional field-induced transition to produce higher P_s). P_s of ferroelectric ceramic systems can be calculated based on neutron diffraction, as proposed by Shimakawa *et al.*¹⁹ Then spontaneous polarisation caused by displacements can be calculated using Shima Kawa's model as follows:

$$P_s = \sum_i \frac{m_i \Delta x_i Q_i e}{V} \quad (5)$$

where m_i is the site multiplicity, Δx_i is the atomic displacement along the a -axis from the corresponding position in the tetragonal structure, $Q_i e$ is the ionic charge of the i th constitute ion, and V is the volume of the unit cell. For example, the P_s of NBT-based ceramics, 0.8NBT-0.2($\text{Ba}_{0.4}\text{Sr}_{0.6}\text{TiO}_3$), has been reported using eqn 5 above, resulting in $4.5 \mu\text{C cm}^{-2}$.²⁰ Therefore, there is an urgent required to investigate further the contribution of such high polarisation, either by intrinsic (*e.g.*, electric field-induced phase transition) or extrinsic effects.

2.3. Dielectric breakdown strength

Dielectric breakdown (E_{BD}) is an undesirable physical phenomenon where materials ionise, causing an electrical current to flow instantly through capacitors at excessive voltage. $E_{\max}$ is the maximum electric field a material can withstand before breakdown, while the maximum applied electric field is the highest applied field for effective energy storage at which the material breaks. $E_{\max}$ is influenced by internal factors (band gap, activation energy, electrical microstructure) and external factors (defects, porosity). The pulse electric field (E_{pulse}) refers to short-duration, high-intensity fields that materials can endure in AC-pulsed conditions without breaking down. Most of the studies assess the energy storage performance of their materials using an E_{pulse} of 1 to 20 Hz (based on P - E loops). Moreover, Yan's group proposed a new concept for assessing energy storage materials, termed recoverable energy storage intensity (ρ). This metric is defined as the W_{rec} per unit electric field difference (ΔE), where ΔE is the difference between the breakdown field and the starting electric field. This approach provides a refined method for evaluating the

efficiency of energy storage materials under specific electric field conditions.²¹

Several mechanisms have been proposed to explain dielectric capacitor failure, including thermal runaway, electromechanical breakdown, electric puncture, and partial discharge. A wider band gap (E_g) or activation energy (E_a) is considered a good indicator of higher $E_{\max}$ for dielectric materials. Chemical doping is an effective method for tailoring $E_{\max}$ by manipulating the electrical microstructure. Additionally, the thickness of ceramic specimens influences $E_{\max}$ during high-voltage electrical measurements (discussed later with respect to Fig. 19). Achieving high $E_{\max}$ is essential for high W_{rec} and reliable energy storage performance. Overall, a high-density, single-phase ceramic with high $E_{\max}$, high resistivity and homogeneous electrical microstructure is ideal for delivering high-energy storage.

3. State-of-art lead-free dielectric ceramics for high energy density capacitors

State-of-the-art lead-free dielectric ceramics (bulk ceramics, multilayer ceramic capacitors, and ceramic thin films) are discussed along with how energy storage performance may be normalised to take into account the effect of thickness and electrode area.

3.1. Bulk ceramics

3.1.1. NaNbO_3 . Sodium niobate (NaNbO_3 , NN), a lead-free AFE,²² undergoes a series of phase transitions upon heating as shown in Fig. 6.^{23–27} Under the application of an electric field, the room-temperature AFE P phase is irreversibly transformed to the FE Q phase ($P2_1ma$), resulting in an FE-like square hysteresis loop with large polarisation values ($P_r = 30 \mu\text{C cm}^{-2}$ at 150 kV cm^{-1}),^{28,29} Fig. 6. The volume fraction of the P vs. Q phase in the unpoled state depends on many factors such as impurity concentration and grain size. NN has a comparatively large intrinsic band gap ($E_g \sim 3.58 \text{ eV}$)³⁰ among lead-free perovskite dielectrics, thus it is considered a promising candidate for sustaining a high $E_{\max}$ ^{31,32} and therefore W_{rec} .

Recent studies on NN-based dielectric ceramics have been summarised in Table 1, which are primarily focused on (i) A-site chemical dopants (Na),³⁴ (ii) B-site chemical dopants (Sr, Sn, Zr, Hf, W, Mn),^{35–37} (iii) A and B-site co-doping (Bi/Ta, Bi/Mg, Ca/Zr)^{38–40} and (iv) formation binary (NN- CaHfO_3 , CaTiO_3 (CT), BT, BiScO_3 , SrTiO_3 (ST), AN, and CaZrO_3 (CZ))^{41–45} and ternary solid solution.^{22,33,35–37,40,45–54} NN-based systems have a dominant room temperature AFE structure with anti-parallel cation displacements normal to the long (b) axis.^{25,55} The AFE phase has a similar free energy to the FE Q phase and transforms irreversibly to the latter on the application of an electric field.²⁵ However, the AFE structure may be stabilised using dopants that decrease the Goldschmidt perovskite (general



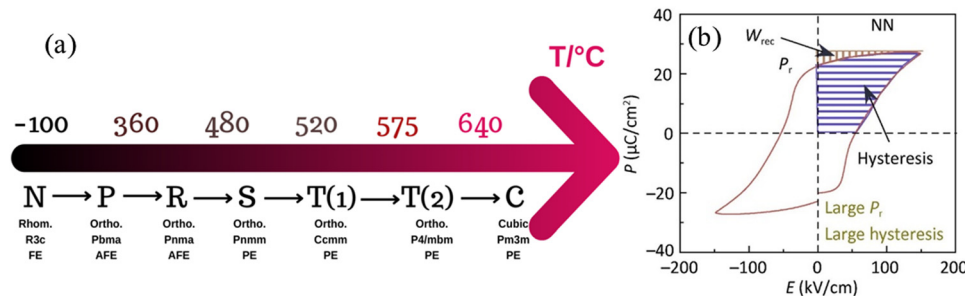


Fig. 6 (a) Phase transition of NN ceramics as a function of temperature (b) PE Loop of NN.³³ Reprinted (adapted) with permission from ref. 33 under the terms of the Creative Commons CC BY license, Elsevier.

Table 1 Summary of energy storage performance of NN-based ceramics from the literature

Composition	W_{rec} (J cm ⁻³)	η (%)	E (kV cm ⁻¹)	ΔP (μC cm ⁻²)	$\tau_{0.9}$ (ns)	P_D (MW cm ⁻³)	ϵ_r (RT)	$\tan \delta$ (RT)	t (mm)	Ref.
0.69NN-0.06BT-0.25Ca _{0.7} La _{0.2} TiO ₃	3.1	91	360	18	—	154	412	0.013	0.10	58
0.90(0.88NN-0.12Bi(Ni _{0.5} Zr _{0.5} O ₃)-0.10CT	5.1	83	580	12	35	75	383	0.010	0.10	59
0.85NN-0.15CZ	5.4	82	680	32	—	—	545	—	0.10	48
0.8(0.92NN-0.08Bi(Mg _{0.5} Ti _{0.5} O ₃)-0.2 CT	5.7	86	475	31	28	48	373	0.003	0.10	31
0.96(0.8NN-0.2 ST)-0.04 Bi(Zn _{0.5} Sn _{0.5} O ₃	5.8	92	573	11	—	—	712	0.009	0.10	60
0.85(0.92NN-0.08 Bi(Mg _{0.5} Ti _{0.5} O ₃)-0.15 ST	6.0	81	590	19	990	96	620	0.002	0.15	51
0.84NN-0.16CT	6.6	93	520	15	700	350	730	0.009	0.10	42
Na _{0.9} Bi _{0.1} Nb _{0.9} Ta _{0.1} O ₃	7.3	87	530	30	60	320	1450	0.002	0.15	38
0.75[0.90NN-0.10Bi(Mg _{0.5} Ta _{0.5} O ₃)-0.25(Bi _{0.5} Na _{0.5} O ₃)-0.7Sr _{0.3} TiO ₃	8.0	90	800	23	32	49	620	0.005	0.15	61
0.88NNTa _{0.1} -0.10ST-0.02La(Mg,Ti)O ₃	8.7	80	580	37	—	—	515	0.008	0.20	18
0.85 NN-0.15 Ca _{0.7} Sm _{0.2} TiO ₃	9.1	80	800	31	80	157	605	0.007	0.035	62
(Na _{0.91} Bi _{0.09})(Nb _{0.94} Mg _{0.06})O ₃	10.9	83	820	30	19	—	920	0.002	0.06–0.08	63
0.76NN-0.24(Bi _{0.5} Nb _{0.5})TiO ₃	12.2	69	620	59	—	—	1320	—	0.15	64
0.88 NN-0.12(Bi _{0.9} Na _{0.1})(Fe _{0.8} Ti _{0.2})O ₃	12.7	83	873	27	5000	200	650	0.002	0.05	65
0.88 NN-0.12(0.7BF-0.3BT)	14.5	84	930	55	4500	233	780	0.002	0.05	66
0.12 NN-0.12(0.55BF-0.45 ST)	16.2	82	970	61	4800	178	910	0.004	0.05	55

formula, ABO₃) tolerance factor, t .⁵⁶

$$t = \frac{r_A + r_O}{\sqrt{2}(r_B + r_O)} \quad (6)$$

where r_A , r_B and r_O are the ionic radii of the A-, B-, and O-sites, respectively. Besides t , the average electronegativity (X) difference between the ions also plays a role, where X_{BO} is the electronegativity difference between the B cation and the oxygen anion while X_{AO} is the electronegativity difference between the A cation and the oxygen anion, respectively,⁵⁷

$$\Delta X = \frac{X_{BO} + X_{AO}}{2} \quad (7)$$

For example, t for the conventional lead-based AFE PbZrO₃ is 0.964, lower than NN with a similar ΔX of 2.25 to ST and BT. Thus, NN's AFE may be stabilised by lowering its t value while holding ΔX constant.⁵⁷ Recently, FE Q phase NN was stabilised in 0.9NN-0.1ST, which is further modified to a short-range relaxor 0.88NN-0.10ST-0.02La(Mg, Ti)O₃ and then to an incipient/paraelectric for 0.88NaNb_{0.9}Ta_{0.1}O₃-0.10ST-0.02La(Mg, Ti)O₃ that exhibits quasi-linear dielectric (QLD) behaviour, where $\tan \delta$ remained <0.01 between -143 to 290 °C (130 to

563 K) for NNTa_{0.10}-10ST-2LMT (Fig. 7a). The polarisation increment, dP/dE , for QLD was found to be near constant (0.008 μC cm⁻¹ kV⁻¹) up to $E > 500$ kV cm⁻¹, giving rise to excellent $W_{\text{rec}} = 8.7$ J cm⁻³ with $\eta = 80\%$ (Fig. 7b–d).¹⁸ To date, a 50 μm-thick 0.88NN-0.12(0.55BF-0.45ST) ceramic has been reported with the highest $W_{\text{rec}} \sim 16.2$ J cm⁻³ with $\eta \sim 82\%$.

3.1.2. AgNbO₃. AgNbO₃ (AN) has emerged as a promising candidate, demonstrating substantial potential for energy storage due to its high polarisation, 52 μC cm⁻².⁶⁷ In the ideal cases, the P_r value of AFE materials is zero, but undoped AFE AN co-exists with a ferroelectric AFE/FE phase resulting in non-zero P_r (~ 7 μC cm⁻²) and low E_{max} at room temperature.⁶⁸ There are three principal strategies to enhance the energy density of AN-based ceramics.²⁹ The first entails the incorporation of MnO₂, a technique inspired by lead-based materials, to mitigate leakage current.^{68,69} In addition to pinning V_O and inhibiting their movement, MnO₂ refines the grain size which also decreases electrical conductivity, resulting from the refractory nature of the dopants and the elevated sintering temperatures needed for doped AN ceramic, advantageous for achieving higher E_{max} .⁷⁰ The second strategy, the most widely adopted, involves aliovalent doping at the A-site and replacing Nb with Ta.^{69,71–75} Notably, the substitution of Nb with Ta has garnered



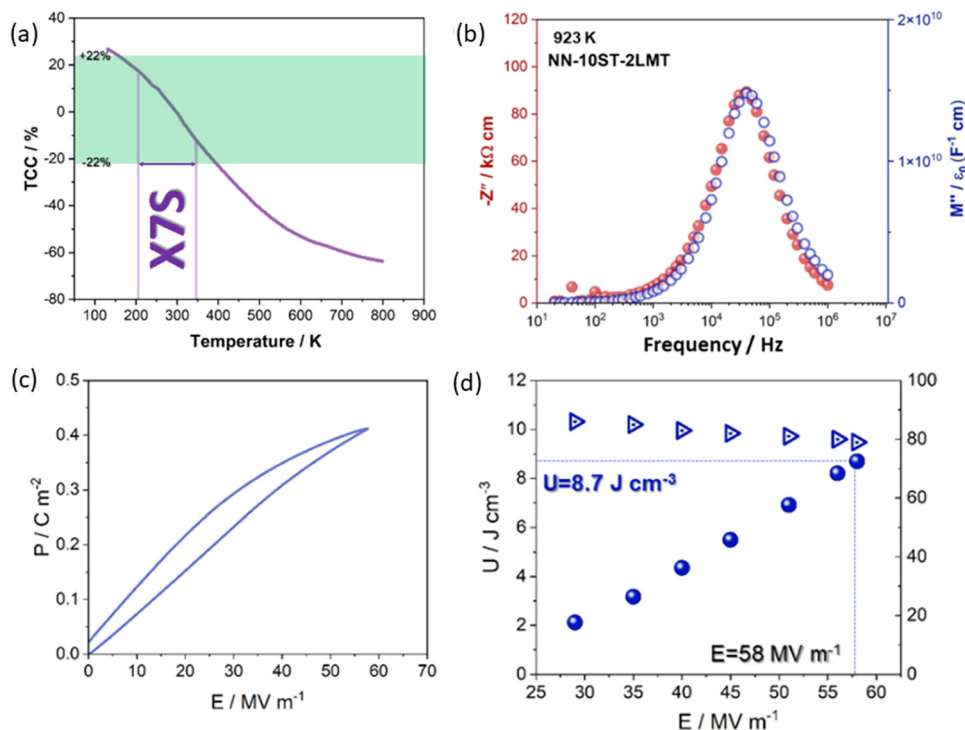


Fig. 7 (a) Temperature-coefficient of capacitance (TCC) values of NN-Ta_{0.10}-10ST-2LMT across the temperature range from 800 K, (b) temperature-dependent M'' spectroscopic plots for NN-Ta_{0.10}-10ST-2LMT, (c) P - E loops of NN-Ta_{0.10}-10ST-2LMT bulk ceramics, and (d) Calculated discharge energy density (U) and energy conversion efficiency (η) at various electric fields.¹⁸ Reprinted with permission from ref. 18, the John Wiley and Sons., under the terms of the Creative Commons CC BY license.

considerable attention in recent AN-based research. Ta is known to stabilise the AFE phase by regulating the M2 or M3 transitions, evident from the shift in temperature of the dielectric anomalies and disruption of long-range antipolar AFE order which reduces the scale of AFE domains. Ultimately for the AgTaO₃ end member, an incipient FE response is observed.⁷⁶ Before the onset of incipient behaviour, the field required to promote the AFE/FE transition is increased. Within the field-induced FE phase, polar coupling is also reduced, and the loop is slimmer, simultaneously increasing η and W_{rec} . A-site substitutions with RE and Bi ions enhance this effect due to the difference in ionic radius with Ag which also affects the correlation length of antipolar order in the AFE and polar coupling in the induced FE phase.^{77,78} Therefore, to enhance

energy storage properties, AN-based materials sacrifice P_{max} , leading to an increase in E_g and E_a , thus contributing to higher η , lower strain, and enhanced E_{max} , ultimately leading to higher W_{rec} .

The third strategy involves the formation of a solid solution with other compounds, such as (Sr_{0.7}Bi_{0.2})HfO₃ and Ca(Hf_{0.2}Ti_{0.8})O₃^{79,80} to induce relaxor rather than AFE/FE switching behaviour. Recently, a significant milestone has been the successful development of AN-based MLCCs by several research groups,^{71,72} which have achieved high W_{rec} , principally due to a reduction in thickness of the dielectric layer in relaxor-based systems (third strategy). Fig. 8 shows a TEM image of Ag_{0.64}Bi_{0.12}NbO₃ + 0.10 wt% MnO₂ revealing lamellar domains, with Fig. 8b demonstrating the highest W_{rec} to date

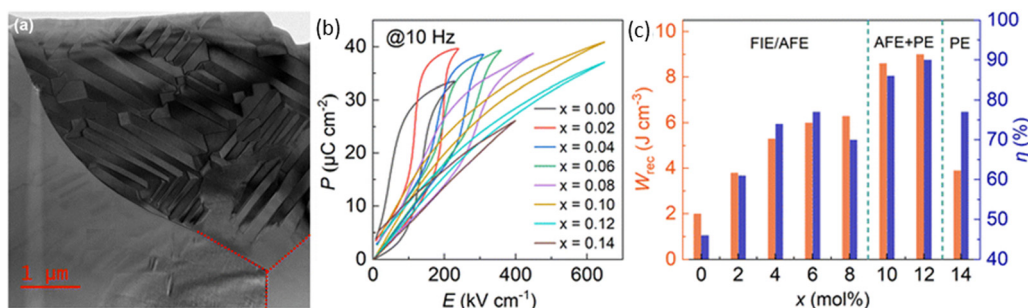


Fig. 8 (a) Overview of bright-field TEM image displaying three grains of the Ag_{0.64}Bi_{0.12}NbO₃ + 0.10 wt% MnO₂ ceramic (b) unipolar P - E loops measured at 10 Hz, and (c) W_{rec} and η of AN- x Bi ceramics at room temperature.⁷⁷ Reproduced from ref. 77 with permission from the Royal Society of Chemistry.

Table 2 Functional properties of the AN-based Ceramics from the literature

Composition	W_{rec} (J cm ⁻³)	η (%)	E (kV cm ⁻¹)	ΔP ($\mu\text{C cm}^{-2}$)	$\tau_{0.9}$ (ns)	P_{D} (MW cm ⁻³)	ε_{r} (RT)	$\tan \delta$ (RT)	t (mm)	Ref.
Ag _{0.99} Nd _{0.01} Nb _{0.796} Ta _{0.2} O ₃	4.5	68	290	36	—	—	520	0.030	—	81
0.94 AN-0.06 CaHf _{0.2} Ti _{0.8} O ₃ + 0.2wt% Mn	5.4	66	300	38	—	—	400	0.003	—	80
Ag _{0.92} Sr _{0.04} Nb _{0.78} Ta _{0.22} O ₃	5.6	70	300	36	137	132	600	0.007	—	82
Ag _{0.80} Na _{0.20} Nb _{0.80} Ta _{0.20} O ₃ + 0.1% MnO ₂	5.8	62	260	46	160	—	431	0.005	0.08	73
AN@SiO ₂ + 0.10 wt% MnO ₂ -doped + 4 mol% Bi ₂ O ₃ and Sc ₂ O ₃	5.9	71	322	42	160	273	813	0.001	0.06	83
0.945AN-0.055Sr _{0.7} Bi _{0.2} HfO ₃ + 1 mol% BaCu(B ₂ O ₅)	6.1	73	330	40	—	—	600	0.002	0.15	79
Ag _{0.94} La _{0.02} Nb _{0.8} Ta _{0.2} O ₃	6.7	74	540	33	—	—	550	—	0.12	84
Ag _{0.76} La _{0.08} NbO ₃	7.0	77	476	35	—	—	660	0.003	0.15	78
Ag _{0.96} Ce _{0.01} Nb _{0.7} Ta _{0.3} O ₃	7.4	76	377	41	23	294	580	—	0.13	85
0.90AN-0.10Bi _{0.2} Sr _{0.7} TiO ₃	7.8	56	580	45	310	—	950	0.180	0.05	69
Ag _{0.80} Bi _{0.04} Sr _{0.04} NbO ₃ + 0.1 wt%MnO ₂	7.9	75	702	37	—	—	844	0.009	0.05	70
Ag _{0.80} Bi _{0.04} Sr _{0.04} Nb _{0.85} Ta _{0.15} O ₃ + 0.30 wt% MnO ₂	8.5	76	729	33	300	—	687	0.003	0.05	74
Ag _{0.64} Bi _{0.12} NbO ₃ + 0.10 wt%MnO ₂	9.0	90	651	39	—	—	1100	—	0.05	77

for AN-based materials.⁷⁷ The energy storage properties of AN-based materials are summarised in Table 2.

3.1.3. Na_{0.5}Bi_{0.5}TiO₃. Na_{0.5}Bi_{0.5}TiO₃ (NBT) is one of the most studied lead-free electroceramics. The properties of modified compositions include large electro-strain,⁸⁶ oxygen ion conduction,⁸⁷ and large electrostatic energy storage.^{29,63,88,89} Undoped NBT exhibits a FE *P*-*E* loop with $P_{\text{max}} \sim 40 \mu\text{C cm}^{-2}$,⁹⁰ $P_{\text{r}} \sim 38 \mu\text{C cm}^{-3}$ and E_{c} of 73 kV cm⁻¹.⁹¹ NBT was thought to have an average rhombohedral *R3c* structure but more recent studies have identified the room temperature phase as monoclinic with *Cc* symmetry,^{87,92} as reported by Jones.⁹³ For high-field applications, the leakage in undoped NBT is caused by defects relating to Bi³⁺ volatilisation^{94,95} during calcination and densification, however, excess Bi₂O₃ to the stoichiometric composition improves the total resistivity. Early studies focused on A, B or A/B site (co-) doping, promoting relaxor behaviour, such as Na, Bi, Sr, or Ba on A-site⁹⁶⁻¹¹⁶ or Nb, Mg, Fe, Mn, or Ti on B-site^{96,115-123} sites, and Na/Nb, Ba/Mg, Bi/Na, and Sr/Mg, Nb co-doped^{29,92,124-157} yielding W_{rec} up to 4 J cm⁻³ for bulk ceramics.

As with AN, there are several strategies employed to optimise energy density in NBT-based ceramics. NBT is often combined with end members that have a large E_{g} , such as ST, Sr_{0.7}Bi_{0.2}TiO₃ (SBT) and Ca_{0.7}La_{0.2}TiO₃¹⁵⁸ to form a relaxor phase (pseudo-cubic) with polar nano regions (PNRs). A high $W_{\text{rec}} \sim 10.3 \text{ J cm}^{-3}$ with $\eta \sim 97\%$ ¹⁵⁹ was reported by Zhou *et al.*, in 0.85 (Bi_{0.5}Na_{0.5})_{0.7}Sr_{0.3}TiO₃ (BNST)-0.15 Bi(Mg_{1/3}Ta_{2/3})O₃ (BMT) in which Sr²⁺, Mg and Ta ions promote the formation of PNRs, due to their larger ionic radius leading to lattice strain which not only disrupts polar coupling (Fig. 9)¹⁶⁰ but locally enhances polarisation.¹⁶¹ The low tolerance factor associated with NBT-based ceramics ensures that not only is their chemical and displacive cation disorder but also of the O²⁻ octahedral framework in which the amplitude and type of rotation (in-phase *vs.* antiphase) varies over a short range. Liu and co-authors¹⁶² utilised these strategies albeit expressed in different terms and reported 0.88 (0.75 NBT-0.25BT)-0.12NN ceramics with $W_{\text{rec}} \sim 15.2 \text{ J cm}^{-3}$, $\eta \sim 91\%$, $E_{\text{max}} \sim 730 \text{ kV cm}^{-1}$, $\tau_{0.9} \sim 38 \text{ ns}$, temperature stability from 30-120 °C, frequency stability from 10-200 Hz and cyclic fatigue resistance (up to 10⁷ cycles, with less than 1% changes).¹⁶² Energy density performance for a

wide range of NBT-based compositions is summarised in Table 3.

3.1.4. BiFeO₃. Bismuth ferrite, BiFeO₃ (BF)-based lead-free ceramics are considered promising candidates for high energy density capacitors due to the large spontaneous polarisation and high Curie temperature (T_{c}) of the BiFeO₃ end member.^{172,173} Bi³⁺ has a similar electronic configuration to Pb²⁺ with a lone electron pair contributing to higher T_{c} .¹⁷⁴ BF is both an antiferromagnetic and FE material at room temperature (RT) which has attracted attention in the field of multiferroics.¹⁷⁵ However, the properties of undoped BF generally are very poor, with large leakage current, high $\tan \delta$, and low W_{rec} . Most research has adopted chemical dopants to overcome these issues which arise mainly due to the multiple and unstable valence of the Fe ions coupled with Bi volatilisation during processing.¹⁷⁶ Therefore, BF-based dielectric ceramics are modified by doping at A- and/or B-site *e.g.* Nd,¹⁷⁷ alloying with a third compound *e.g.* Bi(Zn_{2/3}Nb_{1/3})¹⁷⁸ or both, *e.g.* 0.61BF-0.33(Ba_{0.8}Sr_{0.2})TiO₃-0.06La (Mg_{2/3}Nb_{1/3})O₃ to improve electrical properties.¹⁷⁹ The BF-BT solid solution was the first solid solution to exhibit large W_{rec} ^{177,180,181} but the highest (16.3 J cm⁻³) with $\eta \sim 86\%$ at $E_{\text{max}} \sim 690 \text{ kV cm}^{-1}$ was reported for a 50 μm -thick 0.62Bi_{0.9}La_{0.1}FeO₃ (BLF)-0.3Ba_{0.7}Sr_{0.3}TiO₃ (BST)-0.08 K_{0.5}Na_{0.5}NbO₃ (KNN) bulk ceramic,¹⁸² Fig. 10a. Other BF-based binary solid solutions include BF-K_{0.5}Bi_{0.5}TiO₃ (BF-KBT)¹⁸³ and BF-ST¹⁸⁴ and are summarised in Table 4. Wang and co-authors¹⁸³ reported a 0.5KBT-0.42BF-0.08Sm(Mg_{2/3}Nb_{1/3})O₃ (SMN) ceramics with the formation of lamellar nanodomains (Fig. 10b), giving $W_{\text{rec}} \sim 6.1 \text{ J cm}^{-3}$ with η of 72% at $E = 410 \text{ kV cm}^{-1}$,¹⁸³ along with good temperature stability from 25 to 150 °C (<15% variation). 0.35BF-0.65ST ceramics have also been reported with $W_{\text{rec}} = 8.4 \text{ J cm}^{-3}$ with $\eta \sim 90\%$ at $E_{\text{max}} = 750 \text{ kV cm}^{-1}$ after a two-step sintering method (TSSM) which improved grain size, E_{max} , and W_{rec} , with less than 10% variation from 1-100 Hz and from 10-120 °C when compared to one-step sintering methods (OSSM), Fig. 10(c and d).¹⁸⁴

One of the key factors to improve E_{max} and W_{rec} in BF-based dielectrics is the optimisation of the electrical microstructure, as proposed by Wang *et al.*¹⁸¹ For example, adding a third



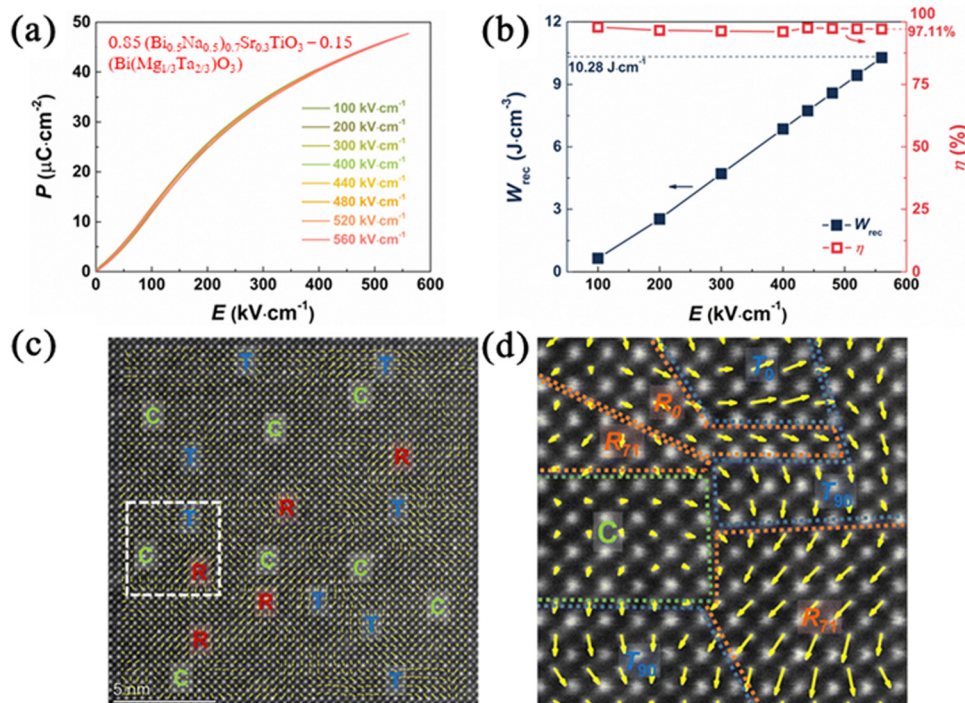


Fig. 9 Properties of 0.85 (Bi_{0.5}Na_{0.5})_{0.7}Sr_{0.3}TiO₃–0.15 (Bi(Mg_{1/3}Ta_{2/3})O₃) ceramics (a) *P*–*E* Loops (b) *W*_{rec} and *η* values (c) HRDP STEM polarisation vector image along [100]_c (d) enlarged image from the white frame.¹⁶⁰ Reproduced from ref. 160 with permission from the Royal Society of Chemistry.

Table 3 Functional properties of the NBT-based Ceramics from the literature

Composition	<i>W</i> _{rec} (J cm ^{−3})	<i>η</i> (%)	<i>E</i> (kV cm ^{−1})	ΔP (μC cm ^{−2})	$\tau_{0.9}$ (ns)	<i>P</i> _D (MW/cm ³)	ϵ_r at RT	tan(δ) at RT	<i>t</i> (mm)	Ref.
0.465NBT–0.035CaSnO ₃ –0.5Sr _{0.7} B _{0.2} TiO ₃	4.0	80	415	38	116	107	2600	0.013	0.15	163
0.94Bi _{0.4867} Sm _{0.0133} Na _{0.4601} Sm _{0.0133} TiO ₃ –0.06BaTiO ₃	4.4	84	230	42	—	—	990	0.035	0.11	21
0.75 NBT–0.25(Bi(Mg _{0.5} Hf _{0.5} Mg _{0.5} Hf _{0.5})O ₃)	4.6	75	310	21	110	39.1	430	0.023	0.12	164
0.62NBT–0.3Sr _{0.7} Bi _{0.2} TiO ₃ –0.08BiMg _{2/3} Nb _{1/3} O ₃	7.5	92	470	48	—	—	1230	0.061	0.15	89
0.85(0.94NBT–0.06BT)–0.15 BiMg _{0.5} Hf _{0.5} O ₃	7.8	76	370	35	—	—	1600	0.230	0.20	90
0.85 Bi _{0.47} Na _{0.47} Ba _{0.06} TiO ₃ –0.15 Sr(Al _{0.5} Ta _{0.5})O ₃	8.3	91	555	39	97	—	1460	—	0.05	165
0.90(Bi _{0.5} Na _{0.5})0.65 Sr _{0.35} TiO ₃ –0.10 Bi(Mg _{0.5} Zr _{0.5})O ₃	8.5	86	522	59	—	—	1320	0.165	0.10	166
0.92(0.6NBT–0.4Sr _{0.7} Bi _{0.2} TiO ₃)–0.08 BMT	8.6	93	565	45	—	—	1350	0.090	0.60	167
NBT–Bi _{0.5} K _{0.5} TiO ₃ –Sr(Sc _{0.5} Nb _{0.5})O ₃	9.2	96	385	46	244	—	750	0.014	0.05	168
0.76(0.94NBT–0.06BT)–0.24 CaTi _{0.75} Ta _{0.25} O ₃	9.6	88	410	60	—	117	789	0.020	0.11	169
0.85 BNST–0.15 BMT	10.3	97	420	54	1350	—	615	0.045	0.05	159
0.50(0.75NBT–0.25BT)–0.50 BaZrO ₃	13.6	91	660	63	35	313	455	0.070	0.08	170
(Bi _{0.5} Na _{0.5})(Ti _{0.33} Fe _{0.33} Nb _{0.33})O ₃	13.8	82	640	53	35	136	480	0.019	0.05	171
0.62(0.94NBT–0.06BT)–0.38 Ca _{0.7} La _{0.2} TiO ₃	15.1	82	640	61	32	212	710	0.001	0.12	158
0.88(0.75 NBT–0.25BT)–0.12 NN	15.2	91	730	30	38	—	1896	0.003	0.05	162

compound SMN into BF–KBT resulted in lower conductivity, higher *E*_a and electrical homogeneity,¹⁸³ favouring high *E*_{max} as well as *W*_{rec}. In impedance complex plots such as Fig. 11(a), there are two *M*'' (*M*'' = 1/2*C* where *C* is capacitance) peaks at each temperature, indicating heterogeneous electrical microstructure (two-component) of the undoped BF–KBT ceramic. Instead, only one *M*'' peak was identified for BF–KBT–0.08SMN ceramics, as shown in Fig. 11(b), whereas Fig. 11(c and d) shows the overlap of the *Z*' over *M*''. Another example, 0.6BF–0.4ST–0.08BiMg_{2/3}Nb_{1/3}O₃ (BMN)–0.01Nb ceramics, as reported by Lu and co-authors,¹⁹² also demonstrates that achieving electrical

homogeneity even at the weak field with a highly resistive and large *E*_a is key to achieving high *E*_{max} as well as *W*_{rec}.

3.2. Multilayer ceramic capacitors (MLCCs)

MLCCs are composed of co-fired multiple layers of ceramic and internal electrodes. The fabrication involves slurry preparation, tape-casting, screen printing, lamination, co-sintering and termination, Fig. 12.¹⁹⁴ By 2022, the market of ceramics MLCCs was ~10.9 billion USD and is expected to be ~16.77 billion by 2030.¹⁹⁵ There are different demands for MLCCs as they are used in many different areas of electronics such as electric



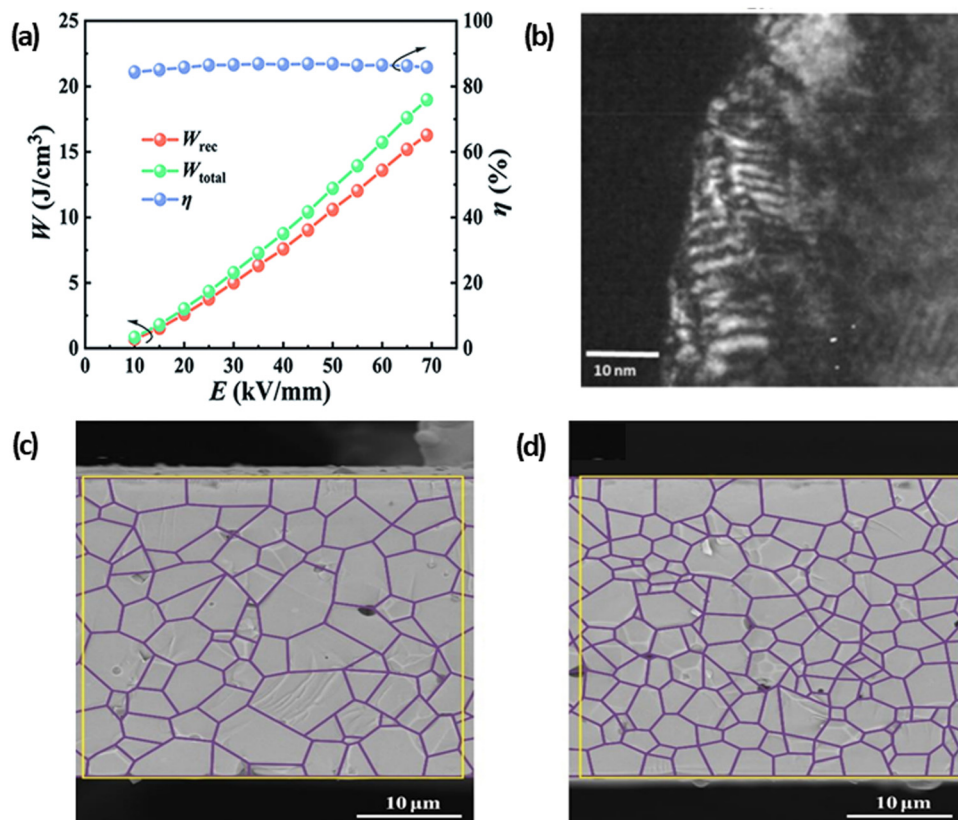


Fig. 10 (a) W_{rec} and η values of 0.62 BLF–0.3 BST–0.08 KNN ceramics.¹⁸² (b) TEM image of grain with lamellar nanodomains for 0.5 KBT–0.42 BF–0.08 SMN.¹⁸³ SEM images for (c) OSSM and (d) TSSM 0.35BF–0.65ST ceramics.¹⁸⁴ Reproduced with permission ref. 182 from the Royal Society of Chemistry. Reprinted with permission ref. 183 from Elsevier under the terms of the Creative Commons CC-BY license. Reprinted with permission from ref. 184, the John Wiley and Sons.

Table 4 Functional properties of BF-based ceramics from the literature

Composition	W_{rec} (J cm ⁻³)	η (%)	E (kV cm ⁻¹)	ΔP (μC cm ⁻²)	$\tau_{0.9}$ (ns)	P_D (MW cm ⁻³)	ε_r at RT	$\tan(\delta)$ at RT	t (mm)	Ref.
0.65BF–0.3 BT–0.05Bi (Zn _{2/3} Nb _{1/3}) O ₃ + 0.1 wt% Mn ₂ O ₃	2.1	53	180	33	100	—	450	0.010	—	178
0.56BF–0.30BT–0.14AN + 5% mol CuO	2.1	84	195	26	—	—	620	0.020	0.30	185
0.7(Bi _{0.97} Nd _{0.03}) [Fe _{0.95} (Li _{0.5} Nb _{0.5}) _{0.05}] O ₃ –0.3BT + 0.1 wt% MnO ₂	3.2	74	290	28	—	—	500	—	—	186
0.61BF–0.33(Ba _{0.8} Sr _{0.2})TiO ₃ –0.06La(Mg _{2/3} Nb _{1/3})O ₃ + 0.1 wt% MnO ₂ + 2 wt% BaCu(B ₂ O ₅)	3.4	59	230	27	—	—	380	—	0.30	187
0.5Bi _{1.02} FeO ₃ –0.37BT–0.13Bi(Zn _{2/3} (Nb _{0.85} Ta _{0.15}) _{1/3})O ₃	4.8	80	410	25	—	—	125	—	0.08	188
0.88(0.67BF–0.33BT)–0.12Na _{0.73} Bi _{0.09} NbO ₃	5.6	84	410	14	—	—	700	0.090	—	189
0.5 KBT–0.42BF–0.08 SMN	6.1	72	410	15	—	—	500	0.100	0.20	183
0.35BF–0.65ST	7.5	93	626	33	166	280	430	—	0.04	184
0.85(0.7BF–0.3BT)–0.15NN	8.2	70	275	65	—	—	1000	—	0.10	190,191
0.5BF–0.4 ST–0.03Nb–0.1BMN	8.2	74	460	49	—	—	485	—	0.15	192
0.55BF–0.33BT–0.12NaTaO ₃	13.4	90	580	62	6	158	750	—	0.05	176
0.62 BLF–0.3 BST–0.08 NaNb _{0.85} Ta _{0.15} O ₃	15.9	88	680	57	6	192	590	—	0.05	193
0.62 BLF–0.3 BST–0.08 KNN	16.3	86	690	64	6	181	550	—	0.05	182

vehicles, medical implants, servers, robotics, and bypass capacitors.^{196,197} The leading companies for fabricating MLCCs include Murata Manufacturing and TDK Taiyo Yuden. The energy density performance of MLCCs is summarised in Table 5.

Lead-free RFE-type MLCCs have been reported in the literature with promising energy storage performance and reliability,

Table 5. For example, Lu and co-authors reported a 0.5BF–0.4 ST–0.03Nb–0.1BMN MLCC¹⁹² with high W_{rec} of 15.8 J cm⁻³ with $\eta = 75.2\%$ under $E_{\text{max}} \sim 1000$ kV cm⁻¹, as shown in Fig. 13. Nb⁵⁺ donor doping was used to enhance resistivity with a third end-member (BMN) promoting relaxor behaviour.

More recently, the energy storage performance (evaluated from P – E measurements) of the QLD MLCCs,



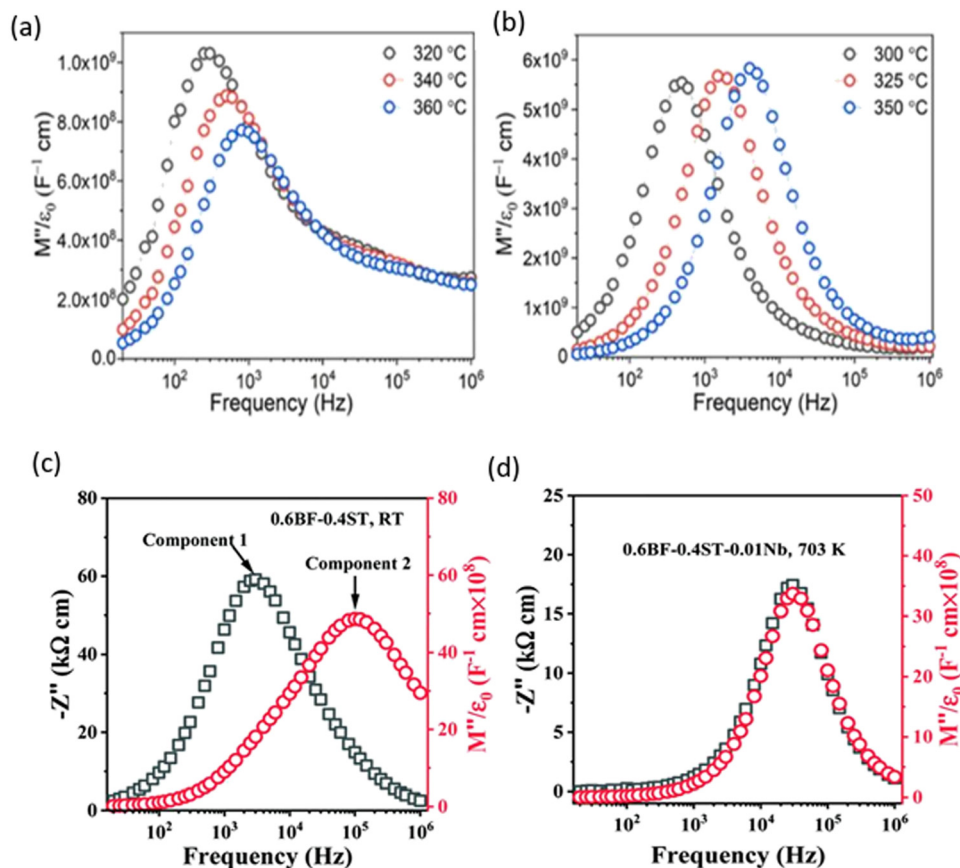


Fig. 11 Temperature-dependent M'' spectroscopic plots for KBT-BF- x SMN ceramics¹⁸³ (a) $x = 0.00$ and (b) $x = 0.08$. (c) Z'' and M'' spectroscopic plot for 0.6BF-0.4 ST ceramics at RT (d) Z'' and M'' spectroscopic plot for 0.6BF-0.4 ST-0.01Nb ceramics at 703 K.¹⁹² Reprinted (adapted) with permission from ref. 183 under the terms of the Creative Commons CC BY license, Elsevier. Reprinted (adapted) with permission from ref. 192 under the terms of the Creative Commons Attribution 3.0 Unported Licence, Royal Society of Chemistry.

0.88NaNb_{0.90}Ta_{0.10}O₃ (NNT)-0.10ST-0.02La(Mg, Ti)O₃ (LMT), was $W_{\text{rec}} = 43.5 (\pm 2.6) \text{ J cm}^{-3}$ with $\eta = 85 (\pm 3) \%$, Fig. 14, at least twice that of all reported MLCCs to date.¹⁸ The ultrahigh W_{rec} obtained in the QLD type MLCCs not only depends on its ability to withstand high E_{max} (associated with homogenous physical and electrical microstructure), low leakage conductivity and high activation energy) but also the QLD behaviour in which dP/dE is constant of $0.0013 (\pm 0.0002) \mu\text{C cm}^{-1} \text{ kV}^{-1}$ from low-field (750 kV cm^{-1}) to high-field (2800 kV cm^{-1}). The origin of near constant dP/dE still requires further investigation but is highly likely to be associated with weakly coupled polar displacements with random polarisation vectors (Fig. 14d).

Additionally, NBT-based MLCCs have demonstrated significant improvements in energy storage performance. For instance, (111)-textured NBT-Sr_{0.7}Bi_{0.2}TiO₃ (NBT-SBT) multi-layer ceramics (discussed in section 4.4) achieved a remarkable W_{rec} of 21.5 J cm^{-3} with $\eta \sim 80\%$ at $E_{\text{max}} \sim 103 \text{ MV m}^{-1}$. This enhancement in performance is attributed to the controlled grain orientation, which reduces the strain induced by the E and improves E_{max} .²⁰⁵ Priya and co-authors investigated AFE-type MLCCs with Ag(Nb_{0.85}Ta_{0.15})O₃ + 0.25 wt.% MnO₂ (ANT + Mn) as the dielectric.⁸¹ The AFE-FE transition was observed

around 250 kV cm^{-1} , resulting in a decrease in η from over 95% to approximately 70% (Fig. 15). These MLCCs exhibited a W_{rec} of 7.9 J cm^{-3} with η measured at 71% at $E_{\text{max}} \sim 1020 \text{ kV cm}^{-1}$, demonstrating lower performance compared to other lead-free REF-type MLCCs.

3.3. Ceramic thin films

Substantial progress in the development of lead-free thin films, e.g., BT, NBT and BF, has been achieved through various synthesis methods, such as sputtering, pulsed laser deposition and chemical solution deposition^{206–208} allowing precise control over composition and thickness.^{209–215} Although thin films may have applications in electrostatic energy storage devices for highly miniaturised electronics requiring high voltage and high temperature, the technology cannot compete on cost with powder-based MLCC fabrication technology.

For dielectric thin films, both $E_{\text{max}} (> 2000 \text{ kV cm}^{-1})$ and $W_{\text{rec}} (> 40 \text{ J cm}^{-3})$ are significantly higher than bulk ceramic and MLCCs due to fewer defects and pores, as summarised in Table 6. Most research into lead-free ceramic thin films has focused on perovskite-type BT and BF-based compositions. High $W_{\text{rec}} \sim 112 \text{ J cm}^{-3}$ with $\eta \sim 80\%$, along with good temperature stabilities between -100 to 150°C , was reported



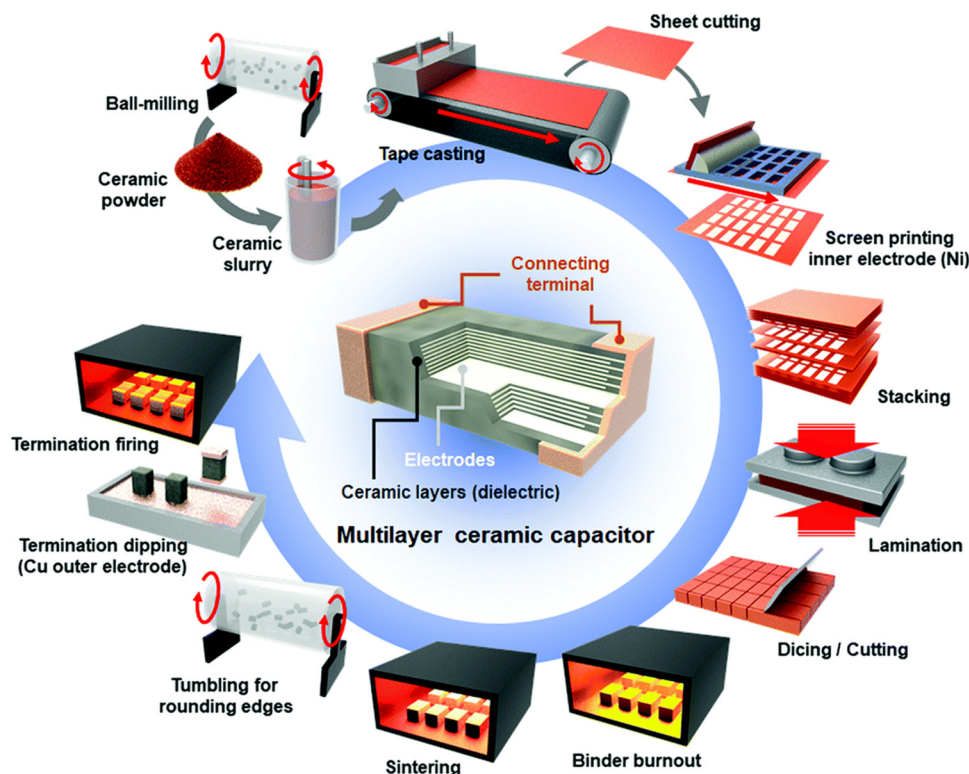


Fig. 12 Schematics of the fabrication process with its construction.¹⁹⁴ Reproduced from ref. 194 with permission from the Royal Society of Chemistry.

Table 5 Functional properties of the MLCCs from the literature

Composition	W_{rec} (J cm ⁻³)	η (%)	E (kV cm ⁻¹)	ΔP ($\mu\text{C cm}^{-2}$)	$\tau_{0.9}$ (ns)	P_D (MW cm ⁻³)	ϵ_r at RT	t (μm)	Electrode	Ref.
0.88BT–0.12 Bi (Li _{0.5} Ta _{0.5}) O ₃	4.1	95	466	25	—	—	—	30	Pt	198
Ag (Nb _{0.85} Ta _{0.15}) O ₃ + 0.25 wt.% MnO ₂	7.9	71	1020	44	—	—	—	15	Pt	199
0.67NN–0.18NBT–0.15Bi (Mg _{0.5} Hf _{0.5}) O ₃	12.7	88	1100	29	900	44	550	100	70 Ag/30Pd	200
0.57BF–0.3BT–0.13 Bi (Li _{0.5} Nb _{0.5}) O ₃	13.8	81	950	54	—	—	—	10	Pt	201
Sm _{0.05} Ag _{0.85} Nb _{0.7} Ta _{0.3} O ₃	14.0	85	1450	20	900	103	440	10	Pt	71
0.87BT–0.13Bi [Zn _{2/3} (Nb _{0.85} Ta _{0.15}) _{1/3}] O ₃	14.1	70	1500	35	—	—	900	5	Pt	202
0.5BF–0.4 ST–0.03Nb–0.1BMN	15.8	75	1000	50	—	—	510	8	Pt	192
0.62NBT–0.3Sr _{0.7} Bi _{0.2} TiO ₃ –0.08BMN	18.0	93	1013	54	—	—	1280	150	Pt	89
0.87BT–0.13Bi [Zn _{2/3} (Nb _{0.85} Ta _{0.15}) _{1/3}] O ₃ + SiO ₂	18.2	94	1755	35	450	—	920	10	60 Ag/40Pd	203
(Ba _{0.33} Bi _{0.32} Ca _{0.11} Sm _{0.07} Na _{0.07} Sr _{0.1})(Ti _{0.63} Fe _{0.32} Zr _{0.05})O ₃	20.8	97	1094	49	11000	—	480	10	70Ag/30Pd	204
(111)-textured 0.65NBT–0.35(Sr _{0.7} Bi _{0.2}) TiO ₃	21.5	80	1030	65	—	—	2000	20	Pt	205
0.88NaNb _{0.90} Ta _{0.10} O ₃ –0.10ST–0.02La(Mg, Ti)O ₃	43.5	85	2800	35	—	—	515	6	Pt	18

in a 450 nm-thick 0.25BF–0.3BT–0.45 ST thin film at $E_{\text{max}} \sim 4900$ kV cm⁻¹, which the authors explained through the presence of a disordered crystal structure with mixed polymorphic nanodomains.²⁰⁹ Non-perovskite-type dielectric thin films have also been reported with promising energy storage performance. A 350 nm-thick Aurivillius-type Bi_{3.15}Nd_{0.85}Ti_{2.8}Zr_{0.2}O₁₂ thin film was optimised to deliver a high $\Delta P \sim 103$ $\mu\text{C cm}^{-2}$ and $W_{\text{rec}} \sim 124$ J cm⁻³ with $\eta \sim 80\%$ at $E_{\text{max}} \sim 3000$ kV cm⁻¹ ref. 207 with fatigue-resistant up to 10⁹ charge/discharge cycles and a wide temperature range of –100 to 200 °C. The best electrostatic energy storage performance to date, $W_{\text{rec}} \sim 182$ J cm⁻³ with $\eta \sim 78\%$ at $E_{\text{max}} \sim 6200$ kV cm⁻¹, was reported in 2022 by Lin *et al.* in a pyrochlore-type dielectric

thin film, Fig. 16(a and b).²¹⁰ The authors proposed this huge response was due to the growth of a high-entropy stabilised Bi₂Ti₂O₇-based dielectric film with the coexistence of multiple lattice distortions. The large W_{rec} was attributed to the large E_{max} (increased resistivity and breakdown properties) correlated with the presence of nano-crystalline grains and amorphous-like phases in the microstructure, as displayed in Fig. 16(c and d).

However, it is important to note that the mechanisms underlying the high polarisation values observed in thin films have not been fully evaluated. There is an urgent need for further investigation to understand why these thin films exhibit such large polarisation responses, as this could significantly

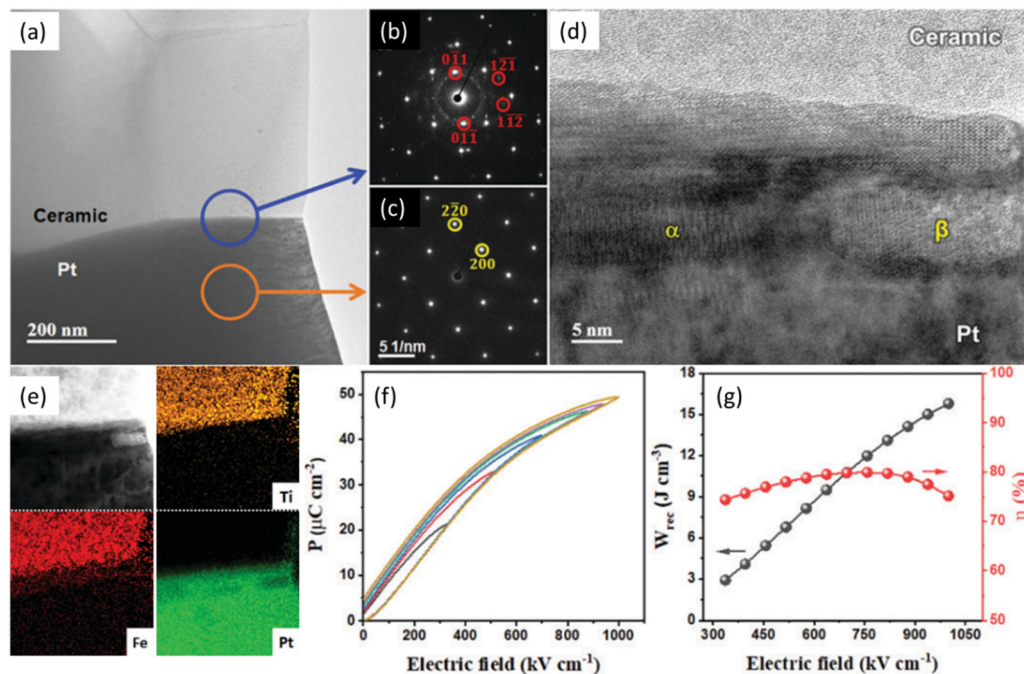


Fig. 13 (a) TEM micrograph of BF-ST-Nb-0.1BMN/Pt interface. (b) SAD pattern highlighting BF-ST-Nb-0.1BMN reflections. (c) SAD pattern from Pt area in (a). (d) High-resolution TEM micrograph showing different phases at ceramic/Pt interface. (e) Bright-field STEM image and EDS elemental maps of ceramic/Pt interface. (f) Unipolar P - E loops. (g) Energy storage properties (W_{rec} and η) for BF-ST-Nb-0.1BMN multilayer.¹⁹² Reprinted (adapted) with permission from ref. 192 under the terms of the Creative Commons Attribution 3.0 Unported Licence, Royal Society of Chemistry.

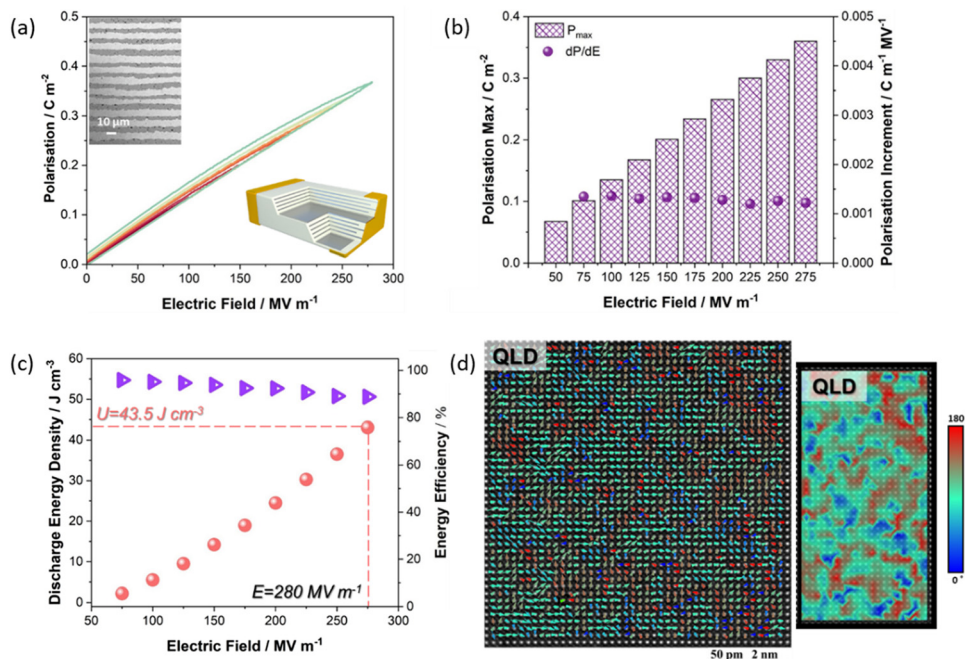


Fig. 14 QLD type MLCCs performance. (a) Unipolar P - E curves of NNTa_{0.10}-10ST-2LMT MLCCs up to the maximum field. (b) Polarisation maximum and increment as a function of electric field up to 280 MV m⁻¹. (c) Energy storage performance up to the maximum field. (d) The [001]-oriented atomic resolution HADDF-STEM images for NNTa_{0.10}-10ST-2LMT (QLD) with the projected polarisation angle. Individual arrows show B-site cation displacement vectors in individual unit cells with different vector angles.¹⁸ Reprinted with permission from ref. 18, the John Wiley and Sons., under the terms of the Creative Commons CC BY license.



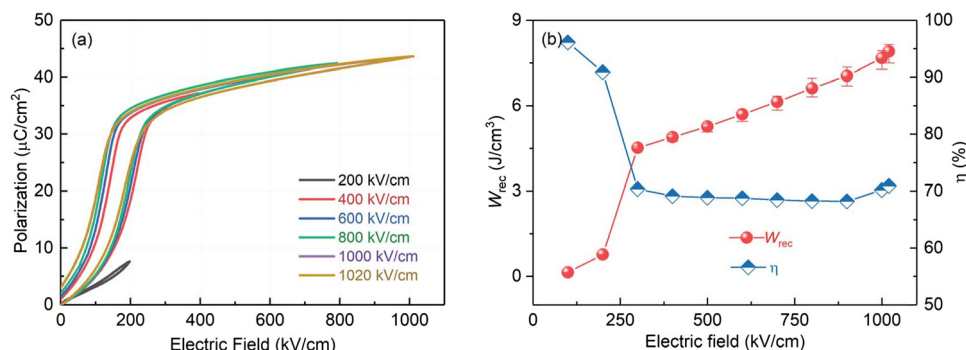


Fig. 15 Energy storage of ANT + Mn multilayer capacitors. (a) Unipolar P - E loops and (b) W_{rec} and η measured at different electric fields from 200 kV cm^{-1} to 1020 kV cm^{-1} .⁸¹ Reproduced from ref. 81 with permission from the Royal Society of Chemistry.

Table 6 Functional properties of thin film ceramics from the literature

Composition	Substrate	W_{rec} (J cm^{-3})	η (%)	E (kV cm^{-1})	ΔP ($\mu\text{C cm}^{-2}$)	ϵ_r at RT	t (nm)	Ref.
BaZr _{0.35} Ti _{0.65} O ₃	ITO layer	40.6	69	4230	22	86	130	211
Ag (Nb _{0.45} Ta _{0.55})O ₃	Si (100)	46.4	80	3300	34	130	300	212
0.4BF-0.6ST	Nb: STO	51.0	60	3600	40	225	500	213
Ba (Zr _{0.35} Ti _{0.65})O ₃	LSMO + STO + F-Mica	65.1	73	6150	28	141	130	214
0.88Ba _{0.55} Sr _{0.45} TiO ₃ -0.12BMN	Nb: STO	86.0	73	5000	51	240	400	216
Ba _{0.3} Sr _{0.7} Zr _{0.18} Ti _{0.82} O ₃	Pt-coated Si	89.4	65	6300	38	151	610	217
Ba(Zr _{0.35} Ti _{0.65})O ₃	Si	93.5	71	8500	30	57	415	218
Ba _{0.95} Sr _{0.05} Zr _{0.2} Ti _{0.8} O ₃	Pt/Ti/SiO ₂ /Si	102.0	87	6200	30	65	100	219
0.25BF-0.3BT-0.45 ST	(001)-oriented Nb: STO	112.0	80	4900	57	250	450	209
(Ba _{0.95} , Sr _{0.05})(Zr _{0.2} , Ti _{0.8})O ₃	Pt (111)/Ti/(100)Si	148.0	91	6600	49	—	300	220
(Bi _{3.25} La _{0.75})(Ti _{1.8} Zr _{0.4} Hf _{0.4} Sn _{0.4})O ₁₂	Pt (111)/Ti/SiO ₂ /Si	182.0	78	6200	55	80	620	210

impact the future design and optimisation of high-performance dielectric materials.

3.4. Summary of state-of-the-art lead-free ceramics for high energy density capacitors

The development of lead-free dielectric ceramics for high-energy-density capacitors has seen significant progress over the past five years, as evidenced by the increasing number of publications (Fig. 2). The figure-of-merit (W_{rec} and η) of these lead-free candidates is either equivalent to or outperforms their lead-based counterparts, although we note that much less research and optimisation have been performed on lead-based systems. Class-II capacitors for consumer electronics rely on BT but it offers lower W_{rec} than competitor compositions.^{14,15,221–225} Instead, there has been an explosion of lead-free candidates based on AFEs (NN and AN) and FEs (NBT and BF). Several promising bulk ceramic compositions based on NN and AN have successfully transitioned into MLCCs using powder-based synthesis methods (tape-casting). This success highlights the potential for larger-scale manufacturing of new lead-free high-energy-density capacitors. Comparatively, the W_{rec} of ceramic thin films ($t < 1 \mu\text{m}$) surpasses that of bulk ceramics and MLCCs but this is attributed in the main to their higher breakdown strengths with E_{max} an order of magnitude greater than in MLCCs.

3.4.1. Comparison between lead-free bulk ceramics. The energy storage performance metrics (E_{max} , ΔP , W_{rec} and η) of

lead-free bulk ceramics are summarised and depicted in Fig. 17. W_{rec} vs. η (Fig. 17a) NN and NBT-based bulk ceramics currently demonstrate superior performance, exhibiting $W_{\text{rec}} > 8 \text{ J cm}^{-3}$ and $\eta > 80\%$. AN-based bulk ceramics present lower W_{rec} ($< 8 \text{ J cm}^{-3}$) and lower η ($< 80\%$). The W_{rec} for BF-based bulk ceramics displays variable values, with a few instances below 5 J cm^{-3} with $\eta < 60\%$, attributed to the opening of the P - E loop (potentially indicating a high leakage). In Fig. 17b, a comparison of W_{rec} vs. E_{max} reveals that NN-based bulk ceramics currently offer the highest E_{max} (up to 980 kV cm^{-1}), partially due to their large intrinsic bandgap, followed by NBT, AN, and BF which along with a homogeneous electrical micro-structure yields a high E_{max} . Lead-free dielectric ceramics for high energy density capacitors can be categorised based on the required voltage, with NN being the preferred choice for high voltage (equivalent to electric field $> 800 \text{ kV cm}^{-1}$) capacitors, while NBT is the optimal candidate for intermediate voltage (equivalent to electric field between 400 to 800 kV cm^{-1}) capacitors. Additionally, we note that E_{max} is closely associated with thickness, which may affect the comparison between each lead-free candidate. Fig. 17c illustrates the comparison between W_{rec} and ΔP for lead-free bulk ceramics. NBT-based bulk ceramics exhibit the highest ΔP (up to $62 \mu\text{C cm}^{-2}$), followed by AN, BF and NN. The high W_{rec} of NBT-based materials is influenced by their substantial ΔP which is influenced by the electrode area. It is therefore important to consider such information for an accurate comparison. Fig. 17d illustrates



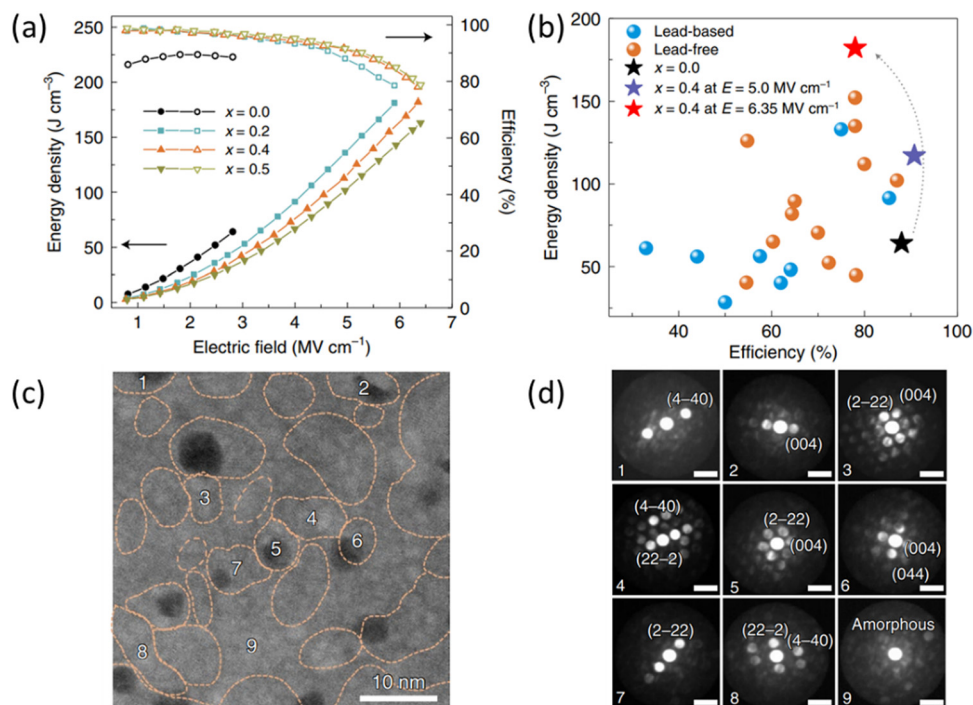


Fig. 16 (a) Energy density and efficiency as functions of electric field up to breakdown strength. (b) Comparison of the energy density and efficiency of our films with representative dielectrics. (c) Low-magnification HAADF image of the ceramic thin film, showing the coexistence of nano-crystalline grains (numbered 1–8) and an amorphous-like phase (no. 9). (d) Nano-beam electron diffraction patterns of the nano-crystalline grains and amorphous-like phase labelled by 1–9 in (c).²¹⁰ Reproduced from ref. 210 with permission from Springer Nature.

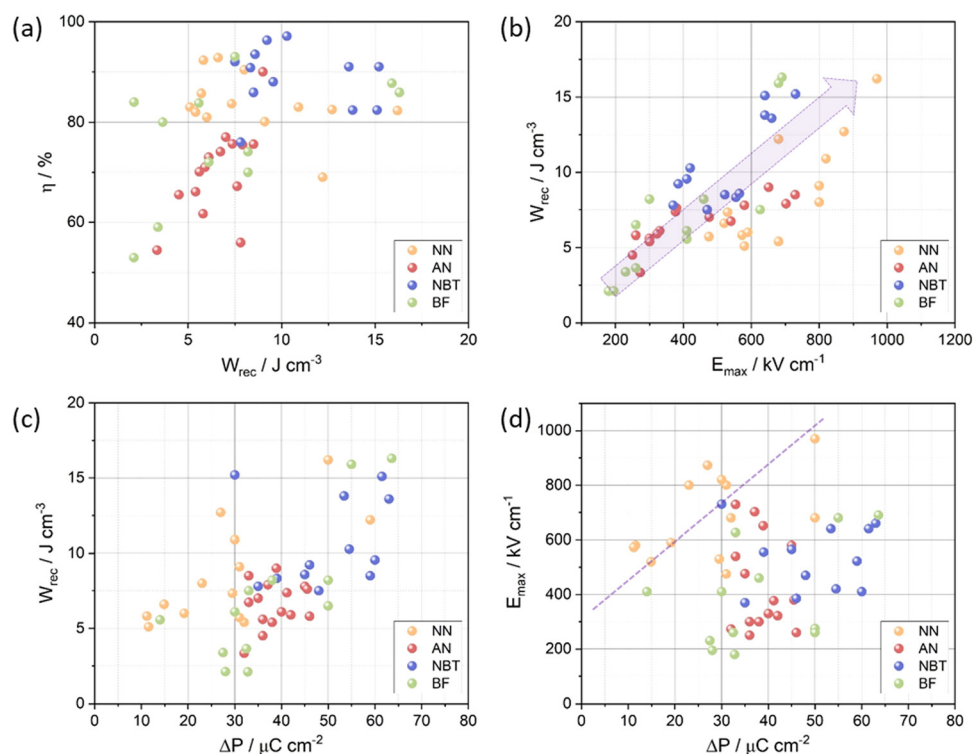


Fig. 17 Comparison between (a) W_{rec} vs. η (b) W_{rec} vs. E_{max} (c) W_{rec} and ΔP (d) E_{max} vs. ΔP in different bulk ceramics.



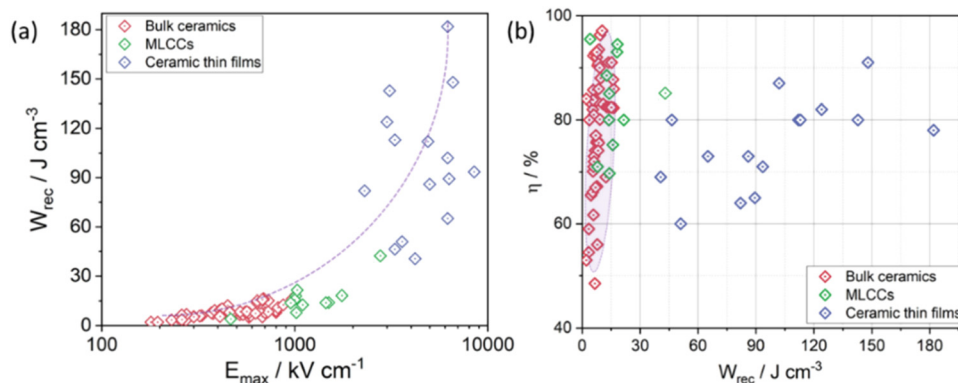


Fig. 18 The comparison between (a) $E_{\max}$ and W_{rec} and (b) W_{rec} and η in terms of thickness.

$E_{\max}$ vs. ΔP for a wide range of compositions. NN-based bulk ceramics cluster above the diagonal line due to their high $E_{\max}$ and low ΔP , whereas NBT, BF, and AN-based bulk ceramics are primarily situated below the diagonal line signifying high ΔP and low $E_{\max}$.

3.4.2. Comparison between bulk ceramics, MLCCs and ceramic thin films. The current state-of-the-art values for W_{rec} in bulk ceramics, multilayer ceramic capacitors (MLCCs), and ceramic thin films are reported as 16 J cm^{-3} , 43.5 J cm^{-3} , and 182 J cm^{-3} , respectively. As of 2024, the W_{rec} for bulk ceramics and MLCCs has witnessed a remarkable improvement but the W_{rec} for ceramic thin films surpasses that of both bulk ceramics and MLCCs by $>5\times$. This significant difference is primarily

attributed to the larger $E_{\max}$ (Fig. 18a) which is enhanced by the reduced thickness (different fabrication techniques). The thickness of bulk ceramics, MLCCs, and ceramic thin films is approximately $50\text{--}150 \mu\text{m}$, $5\text{--}20 \mu\text{m}$, and $0.1\text{--}0.6 \mu\text{m}$, respectively. Consequently, it becomes imperative to normalise W_{rec} with respect to thickness for a more appropriate comparison across different lead-free ceramics (including bulk ceramics, MLCCs, and thin films).

3.4.3. The effect of thickness on energy storage performance. The impact of thickness on $E_{\max}$ and W_{rec} among lead-free bulk ceramics is presented in Fig. 19a. As the thickness of bulk ceramics decreases from 200 to $50 \mu\text{m}$, $E_{\max}$ increases fourfold, ranging from approximately 250 to

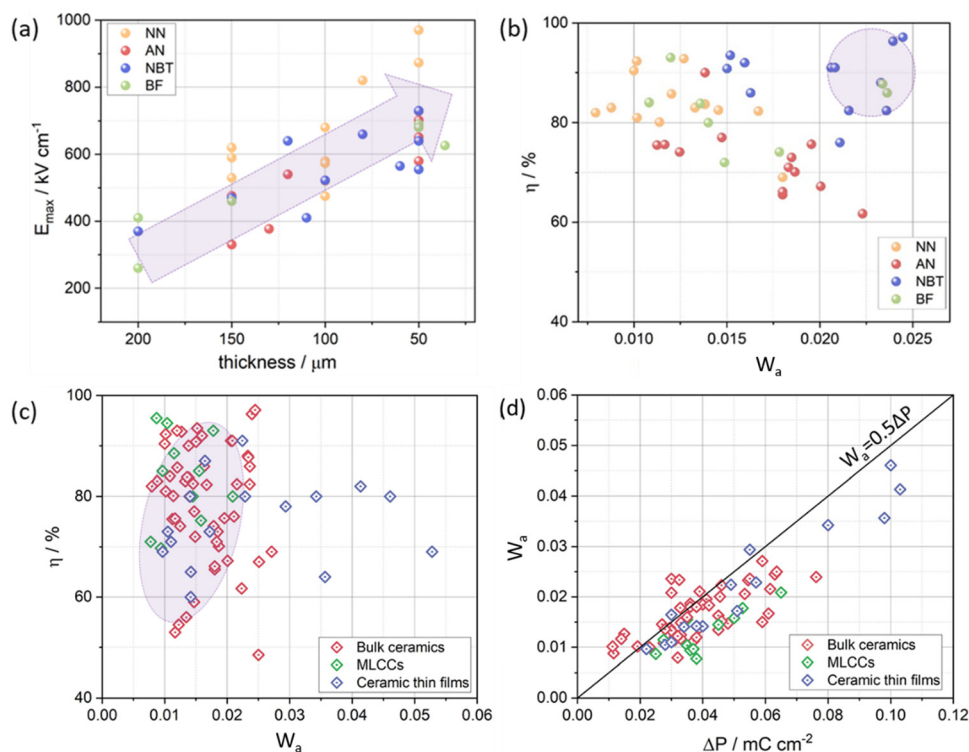


Fig. 19 Impact of thickness on (a) $E_{\max}$ (b) normalised $W_a = W_{\text{rec}}/E_{\max}$ and η in NN, AN, NBT, and BF-based ceramics (c) normalised W_a with η (d) normalised W_a with ΔP in bulk ceramics, MLCCs, and thin films.



1000 kV cm⁻¹. To mitigate the thickness effect, W_{rec} is normalised by E_{max} ($W_{\text{a}} = W_{\text{rec}}/E_{\text{max}}$), as depicted in Fig. 19b. NBT-based bulk ceramics, situated in the top right corner (high W_{a} and η), currently exhibit the best-normalised W_{a} (up to 0.025) and η (> 80%) due to the higher ΔP under the same electric field for NBT-based bulk ceramics. The comparison of normalised W_{a} with η and ΔP is illustrated in Fig. 19c and d. The normalised W_{a} values are concentrated in a range from 0.01 to 0.025. From Fig. 4, the W_{rec} (area to the left of unipolar P - E loop) is equal to half of the product between E_{max} and ΔP . W_{a} thus exhibits a linear relationship to the ΔP ($W_{\text{a}} = 0.5 \times \Delta P$), as displayed in the black solid line in Fig. 19d. The majority of the reported AFE and RFE dielectrics, regardless of the thickness, follow this line with slope $k < 0.5$, mainly due to the energy loss and curve of the P - E loop during electrical charging and discharging.

3.4.4. The effect of electrode area on energy storage performance. Zhang and co-authors²⁰ proposed in 2023 that the size of the electrode area has a significant impact on ΔP as well as W_{rec} . The influence of electrode area on ΔP and W_{rec} is examined among bulk ceramics, MLCCs and ceramic thin films. The relationship between electrode area and ΔP is displayed in Fig. 20a. As the electrode area decreases from 0.12 to 0.075 cm², ΔP doubles from 20 to 40 $\mu\text{C cm}^{-2}$ on average. The W_{rec} is again normalised by ΔP , $W_{\text{b}} = W_{\text{rec}}/\Delta P$, to account for the electrode area effect. Fig. 20b shows that NN-based bulk ceramics, situated in the top right corner

(high W_{b} and η), currently offer the best-normalised W_{b} (up to 0.47) and η (> 80%). The comparison of normalised W_{b} with η and ΔP is illustrated in Fig. 20c and d. W_{b} is 0.1 to 0.5 (Fig. 20c) across all bulk ceramics, MLCCs as well as some ceramic thin films. W_{b} is also found to demonstrate a linear relationship with E_{max} ($W_{\text{b}} = 0.5 \times E_{\text{max}}$), as shown by the black solid line in Fig. 20d. The majority of the non-linear AFE and RFE dielectrics demonstrate a linear relationship between W_{b} and E_{max} with slope $k < 0.5$.

The electrode area information is commonly provided in recent studies on bulk ceramics, as it influences polarisation during electrical P - E measurements. However, this crucial parameter is often ignored or unreported in ceramic thin film and MLCC studies. The determination of the effective dielectric layer thickness in MLCCs and ceramic thin films commonly relies on direct measurements from SEM images. However, discrepancies may arise when estimating electrode areas, often leading to calculation errors in energy storage assessments. From this perspective, we propose that evaluating electrode area is equally important as ceramic thickness and is critical for electrical measurements to accurately assess energy storage.

4. Strategies for optimising energy storage performance

Achieving an optimal balance among various parameters is essential for improving energy storage. The enhancement of

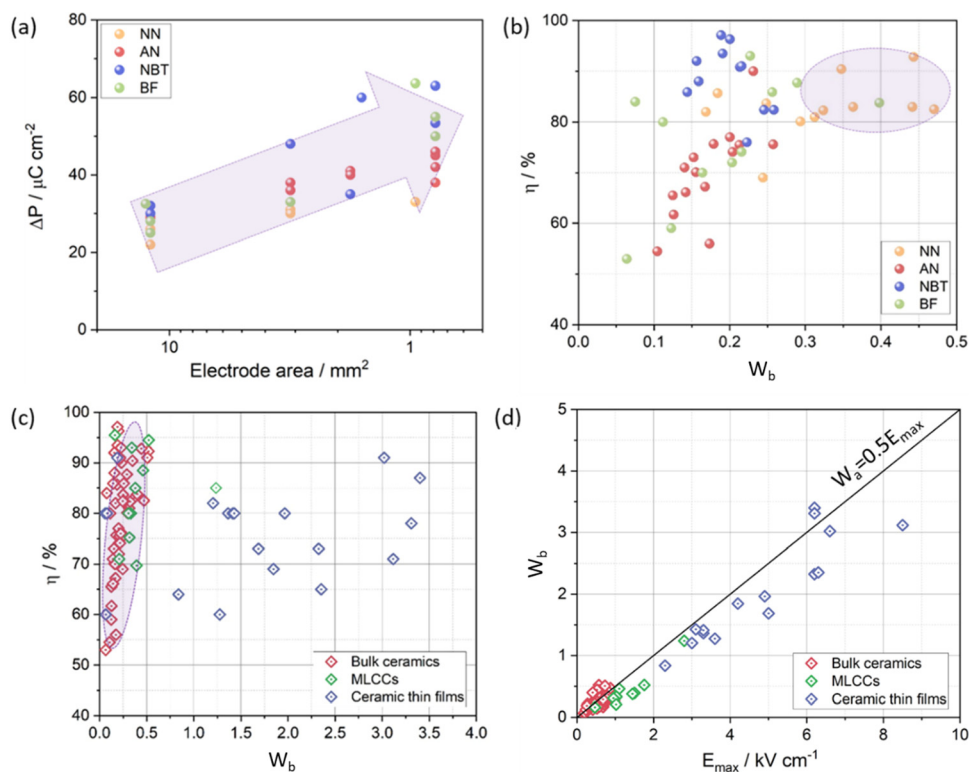


Fig. 20 The relationship between (a) electrode area and ΔP in NN, AN, NBT, and BF-based ceramics (b) normalised W_{b} and η in NN, AN, NBT, and BF-based ceramics (c) normalised W_{b} and η in bulk ceramics, MLCCs, and thin films (d) normalised W_{b} and E_{max} in bulk ceramics, MLCCs, and thin films.



Chem. Soc. Rev., 2024, 53, 10761-10790 | 10779

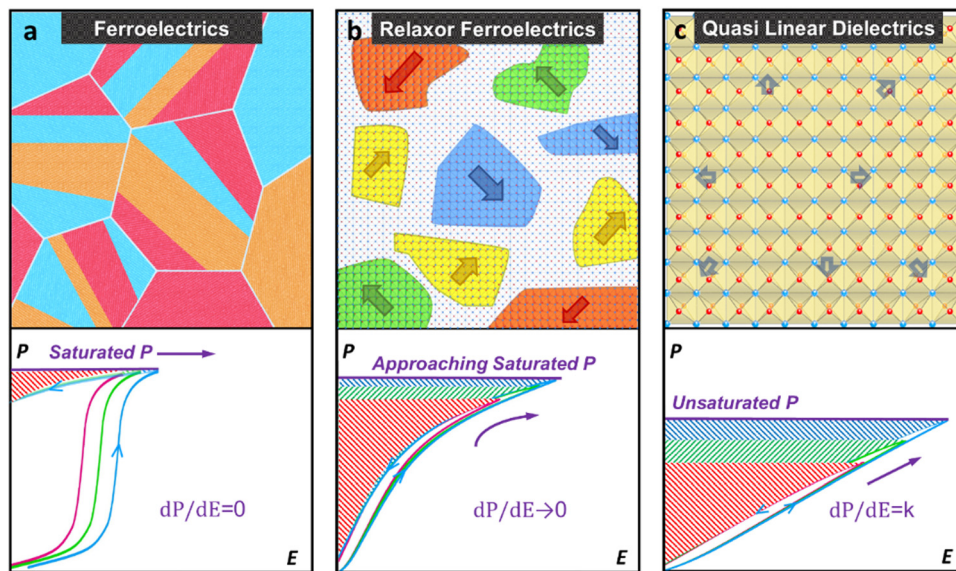


Fig. 22 Schematic microstructure and unipolar P - E loops (with the same internal electric between red, green, and blue) of different dielectrics for electrostatic energy storage (evaluated by the area of red, green and blue) (a) FE with macroscopic domains ($dP/dE = 0$) (b) RFE with multiple polar nanoregions ($dP/dE \rightarrow 0$). (c) QLD behaviour with lattice distortions ($dP/dE = \text{constant}, k$).¹⁸ Reprinted with permission from ref. 18, the John Wiley and Sons., under the terms of the Creative Commons CC BY license.

by the large coercive field (E_C). By combining a FE component with significant structural distortion (δ) and a paraelectric (PE) component to create an RFE with a t close to 1, it is possible to achieve exceptionally high W_{rec} and high η simultaneously.¹⁶¹ Additionally, doping with ions of varying valence, electronegativity, and ionic radii may induce significant local lattice disorder, leading to the disruption of long-range polar order and the formation of PNRs, thereby substantially reducing P_r .¹⁸²

4.3. High entropy enhancement

Since 2004, the concept of disordered multicomponent systems emerged, aiming to maximise configurational entropy and stabilise equimolar mixtures, leading to the development of high-entropy materials. Initially explored in metal alloys and nitride films, entropy stabilisation was later demonstrated in oxides in 2015, spurring the rapid development of high-entropy disordered ceramics. Highly disordered, multi-component systems benefit from high entropy, leading to preferred single-phase solid solutions, sluggish kinetics, lattice distortions, and superior properties. This versatility enables the enhancement of properties by tailoring the compositions of the ceramics in the field of high-energy dielectric ceramic capacitors.

Derived from the Gibbs free energy, the relationship between the atomic fraction of elements and entropy of mixing is shown below, where ΔS_{mix} is the entropy of mixing, R is the gas constant, and N is the total number of elements, yielding the results for single phase materials usually.²³⁸

$$\Delta S_{\text{mix}} = R \ln N \quad (8)$$

S_{mix} reaches a maximum when all elements are present in an equiatomic 5-cation system, the maximum S_{mix} value that can

be achieved is 1.61 R . As per empirical classification, based on its configurational entropy introduced by Murty *et al.*,²³⁹ <https://onlinelibrary.wiley.com/doi/full/10.1002/adma.201806236-adma201806236-bib-0012> materials with $S_{\text{mix}} \geq 1.5 R$ can be classified as “high entropy”, materials with $1.5 R > S_{\text{mix}} \geq 1 R$ as “medium entropy” and materials with $S_{\text{mix}} < 1 R$ as “low entropy” systems. When $S_{\text{mix}} \geq 1.5 R$, a single phase is often attained, as the magnitude of $T\Delta S_{\text{mix}}$ becomes significant enough to surpass enthalpy, ΔH_{mix} , which is dependent on the free energy of the system (ΔG_{mix}) particularly at elevated temperatures (T), as shown in eqn (9). This underscores the importance of high temperatures in facilitating the formation of high or medium entropy (single-phase) systems; however, many of these systems are deemed metastable at room temperature.²³⁸

$$\Delta G_{\text{mix}} = \Delta H_{\text{mix}} + T\Delta S_{\text{mix}} \quad (9)$$

In bulk materials, notable successes using a ‘high-entropy’ approach are exemplified in KNN- and NBT-based ceramics, and recently a BT-based MLCC²⁰⁴ which exhibits relaxor behaviour. In KNN-based ceramics, combining the high-entropy strategy with meticulous preparation optimisation yields rhombohedral-orthorhombic-tetragonal-cubic multiphase nanoclusters, as depicted in Fig. 23. These nanoclusters host ultra-small polar nanoregions (PNRs), resulting in an unprecedented $W_{\text{rec}} \sim 10.06 \text{ J cm}^{-3}$ and an ultra-high η of approximately 90.8%.²⁴⁰ Conversely, in NBT-based ceramics, the high-entropy approach vacates multiple oxygen octahedron tilts, enhancing the random field and significantly delaying polarisation saturation. This facilitates easier polarisation reorientation under external electric fields, reducing heat generation and enhancing thermal breakdown strength,



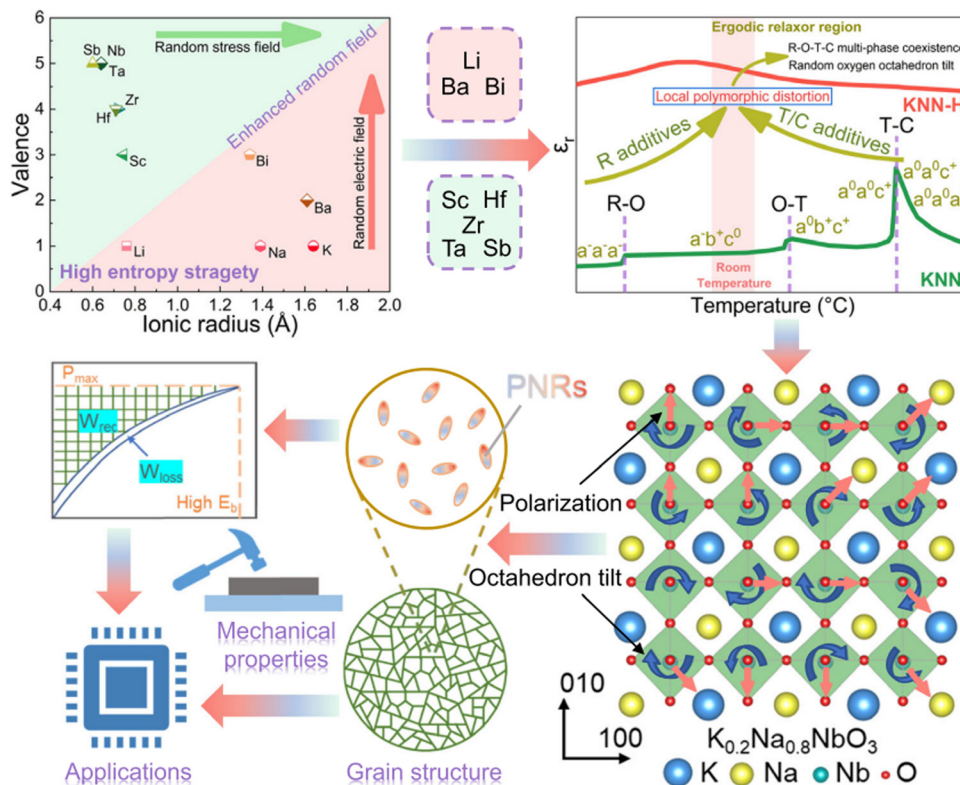


Fig. 23 Schematic overview of high-entropy design approach for KNN-based ceramics.²⁴⁰ Reprinted (adapted) with permission from ref. 240 under the terms of the Creative Commons CC BY license, Springer Nature.

leading to an exceptional $W_{\text{rec}} \sim 13.8 \text{ J cm}^{-3}$ and a high efficiency ($\eta \sim 82.4\%$).¹⁷¹ Extending beyond bulk ceramics, the high-entropy strategy has been applied to thin films based on bismuth titanate ($\text{Bi}_2\text{Ti}_2\text{O}_7$, Fig. 16) and MLCC-based on $(\text{Ba}_{0.33}\text{Bi}_{0.32}\text{Ca}_{0.11}\text{Sm}_{0.07}\text{Na}_{0.07}\text{Sr}_{0.1})(\text{Ti}_{0.63}\text{Fe}_{0.32}\text{Zr}_{0.05})\text{O}_3$ with entropy $> 2.38R$ providing high W_{rec} value of 20.8 J cm^{-3} with an ultrahigh η of 97.5%.

High entropy compositions have multiple components occupying the A or B-site which is the same effective approach used in the formation of many relaxors. The characteristics of multiple polar clusters at the local scale reported in 'high-entropy' bulk ceramics, MLCCs and ceramic thin film are comparable to PNRs in relaxor which can be induced through multiple occupancy of A and B- sites of the perovskite structure. Therefore, the comprehensive implementation of the high-entropy strategy across different material systems does require further clarification and investigation. Although it has been claimed to be an optimisation strategy for energy density performance, it appears to be qualitatively similar to approaches in the literature reported over the last decade which are often described as pseudo-ternary, quaternary and quinary (or more) perovskite solid solutions,^{241–244} rather than as a single formula unit.

4.4. Processing innovation

High electro-strain in AFEs and REFs is considered a potential threat for practical applications for high field/energy density

capacitors during AC/DC cycling and may cause mechanical failure along the interface between internal electrodes and ceramic layers, leading to poor MLCC reliability and early breakdown. Li and co-authors²⁰⁵ fabricated grain-orientated NBT-SBT MLCCs using an ST template, Fig. 24(a and b). The textured MLCCs exhibited reduced electro strain ($< 0.2\%$) in comparison to $> 0.5\%$ in untextured samples, Fig. 24(c and d), realising enhanced $W_{\text{rec}} \sim 21.5 \text{ J cm}^{-3}$ at $E_{\text{max}} \sim 1030 \text{ kV cm}^{-1}$.

Low η not only leads to a high W_{loss} but may also generate self-heating during charge-discharge, leading to electrical breakdown.²⁴⁵ A 'sandwich' MLCC structure, designed to optimise η composed of mixed layers of 0.35BF–0.65 ST and BNST has been reported by Yan and co-authors,²⁴⁶ realising improved $W_{\text{rec}} \sim 9.05 \text{ J cm}^{-3}$ with high $\eta = 97\%$ at 710 kV cm^{-1} , Fig. 25.

5. Current challenges and future perspectives

5.1. Materials challenge for temperature stability

The thermal stability of dielectric materials exhibiting high energy/power density is a crucial factor for practical applications in portable electronics, electric vehicles, and pulsed power systems. Polymer-based dielectric materials offer high power/energy density at ambient temperatures, but above 100°C , they become unreliable and susceptible to dielectric breakdown. Consequently, ceramic-based dielectric materials are prioritised and receiving increased attention due to their



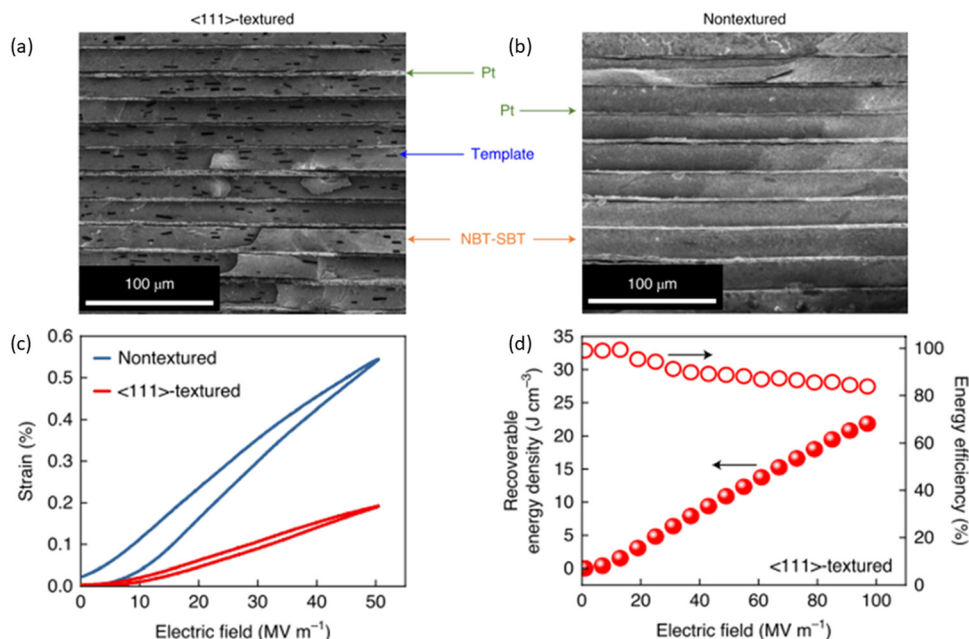


Fig. 24 SEM cross-section of (a) textured and (b) untextured NBT-SBT MLCCs. (c) *S*–*E* Loops of textured and nontextured MLCCs. (d) The energy storage performance of textured NBT-SBT MLCCs.²⁰⁵ Reproduced from ref. 205 with permission from Springer Nature.

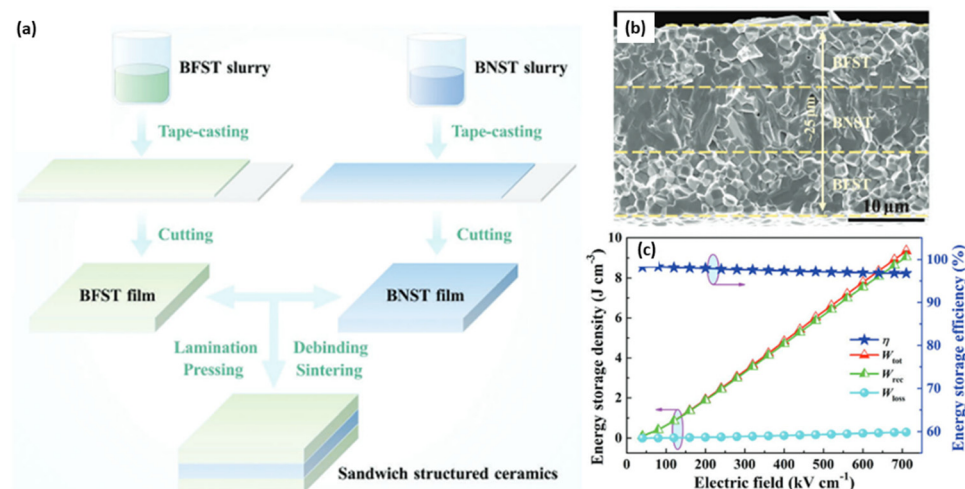


Fig. 25 (a) Schematic illustration for preparing the sandwich BFST/BNST/BFST ceramics by tape-casting method; (b) SEM cross-section image of sandwiched structured ceramics; (c) energy storage performance of sandwiched structured ceramics.²⁴⁶ Reproduced from ref. 246 with permission from the John Wiley and Sons.

high polarisation, rapid charge–discharge speed (<ns), and superior thermal stability.

The temperature stability of high energy density ceramics is often evaluated by performing temperature-dependent *P*–*E* measurements, simulating the environmental conditions in high-voltage capacitors. The applied electric field during temperature studies is approximately 1/4 to 1/2 of the maximum field ($E_{\max}$), and the stability benchmark refers to a variation in W_{rec} of less than 15%. Temperature stability performance for bulk ceramics has been summarised and plotted in Fig. 26.

Currently, the maximum operating temperature is 200 °C in a few NN and NBT-based bulk ceramics which offer the best average temperature stability of 160 ± 40 °C, compared to $\sim 110 \pm 30$ °C found in BF and AN-based ceramics. Recently, broad temperature stability (<10%) has also been reported in a NN based MLCCs, $0.88\text{Na}(\text{Nb}_{0.90}\text{Ta}_{0.10})\text{O}_3$ – 0.1ST – $0.02\text{La}(\text{Mg},\text{Ti})\text{O}_3$, up to 200 °C with $W_{\text{rec}} \sim 15 \text{ J cm}^{-3}$.¹⁸

Two significant challenges have been identified for high-temperature operation: (i) premature mechanical/dielectric breakdown and (ii) low charge–discharge energy efficiency



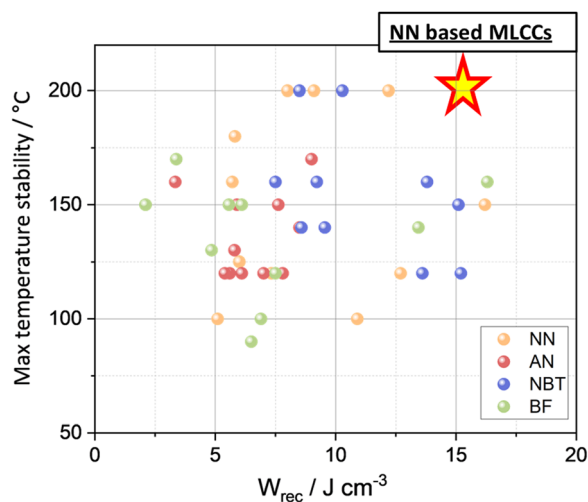


Fig. 26 Correlation between max temperature stability and W_{rec} among four lead-free dielectric candidates.

($\eta < 60\%$). W_{rec} often decreases at elevated temperatures, as evidenced by the opening of the P - E loops (reduced η) or electrical breakdown (reduced E_{max}). Premature dielectric/mechanical breakdown can be attributed to the electric field-induced phase switching between AFE/RFE to FE phases. Substantial electrostrain is often developed during domain reorientation and/or structural transformation from PNRs to long-range orders during high field/voltage charge-discharge electrical cycling, leading to microcrack formation along the interface between electrodes and ceramics. The decrease in η may be associated with changes in the correlation length (e.g. from short-range to meso-range) or to the motion of oxygen vacancies V_{O} . (Under combined high voltage and temperature conditions, both electrical and thermal breakdown mechanisms may occur simultaneously when dielectric ceramics can no longer maintain electrical insulation. However, there is a lack of in-depth studies, such as *in situ* poling diffraction/scattering with pair distribution function (PDF) analysis and high-resolution scanning transmission electron microscopy (STEM), to reveal such features under combined thermal (up to 200 °C) and electrical loading at high electric field levels (up to 400 kV cm⁻¹).

5.2. Process challenge on the co-fire compatibilities between dielectric ceramics with cost-effective inner electrodes

Precious metal electrodes (PMEs) like Pt or Ag/Pd (high level of Pd) are currently used as internal electrodes in most of the MLCCs reported in the literature (Table 5 above) whereas, base metal electrodes (BMEs) such as Ni or Cu, are employed in 99% of Class II high-permittivity commercial capacitors. An issue of incompatibility of BMEs with all current high energy density/voltage capacitors poses a serious challenge to achieving scalable manufacturing and system integration. Although PMEs offer robustness and long-term reliability, BMEs present a cost-effective solution for mass production.

Most lead-free dielectric ceramics can be sintered with a selection of PME in the air without any reaction. However, Pt is too expensive for industrial manufacturing and the recent spike in Pd price, from approximately \$14.3 per gram in 2012 to \$30.7 per gram in 2024,²⁴⁵ also brings significant cost concerns for MLCC manufacturing. In contrast, the overall price trend for BMEs (Ni) between 2012 and 2021 has remained stable, approximately \$0.02 per gram,²⁴⁷ making them a more sensible option for MLCC mass production. The high melting point of Ni (~1455 °C) allows co-firing capability with dielectric ceramics requiring high sintering temperatures (*i.e.* >1200 °C for BT).²⁴⁸ To date, none of the reported high-energy density MLCCs have used Ni as internal electrodes. The reaction between the Ni electrode and Bi-contained dielectric materials, *e.g.*, BF and NBT, at high temperatures results in the formation of low-resistivity and high-loss impurities. Although controlling both temperature and atmosphere ($p\text{O}_2$) is highly complicated and dependent on the specific dielectric ceramic material, exploring co-fire compatibilities with BMEs is still the prioritised research focus to overcome this challenge, particularly for those Bi-free MLCCs cases (NN/AN-based). Co-firing of KNN-based piezoelectric multilayers with Cu internal electrodes has however been reported by Randall and co-authors.²⁴⁹

In addition to exploring the processing conditions with BMEs, a secondary research focus is to reduce the sintering temperature to <950 °C, allowing co-firing with Ag/10%Pd internal electrodes. Incorporating sintering aids such as glass, dopants, and/or alloying with other members encourages ceramic densification at lower temperatures by forming liquid phases.²⁵⁰ For example, adding a third component of Bi(Li_{0.5}Nb_{0.5})O₃ into BF-BT effectively reduces the sintering temperature to 890 °C, allowing the possibility to co-fire with Ag or Ag/10%Pd. CuO was also reported to lower the sintering temperature of KNN-based piezoelectric ceramics to approximately 940 °C.²⁵¹

6. Summary and perspectives

6.1. E_{max} and equivalent voltage

E_{max} has been frequently reported for various dielectric ceramics, including bulk, MLCCs and thin films while an assessment of the equivalent voltage has not received adequate attention. Bulk ceramics offer the highest voltage range for capacitors, averaging between 3 to 5 kV, followed by MLCCs (1.0 to 1.6 kV). Ceramic thin films, on the other hand, provide the lowest voltage range (0.05 to 0.20 V) due to their reduced thickness. Presently, commercial high-voltage capacitors offer a range of 400 to 800 V. State-of-the-art MLCCs now meet future voltage requirements for many high voltage/energy density applications but are limited by either the use of PME internal electrodes or their temperature stability is insufficient. In contrast, the PVD routes required to fabricate ceramic thin films are expensive and may only experience exploitation when directly integrated into Si technology.



6.2. Temperature stability

NN and NBT-based bulk ceramics currently offer the best average temperature stabilities of 160 ± 40 °C, while AN and BF-based bulk ceramics experience $>15\%$ drops in W_{rec} at temperatures above 150 °C. The electric field applied in almost every temperature study reaches only 1/4 to 1/2 of the E_{max} , equivalent to 1–2 kV for bulk ceramics and 0.4–0.8 kV in MLCCs, which is too low for practical applications. To enhance temperature stability, further research is required to understand field-induced AFE/FE and short- to long-range phase transitions. Most importantly, the defect chemistry which controls the conductivity at higher fields and temperatures requires further investigation.

Currently, there is a lack of *in situ* structural and electrical microstructural analysis under high field and temperature which modifies the operating conditions of a capacitor. More advanced structural analysis techniques, *e.g.*, synchrotron X-ray/neutron scattering, high-resolution STEM, *in situ* Raman spectroscopy, and local probe atomic force microscopy, as well as advanced electrical microstructural analysis techniques *e.g.*, local probe impedance, are desirable for further understanding temperature instabilities and dielectric/mechanical breakdown mechanism(s) under high fields and high temperatures. Additionally, there is a critical need to investigate the intrinsic polarisation mechanisms in lead-free dielectric/ferroelectric ceramics to better understand the origins of ultrahigh polarisation values reported in some materials.

6.3. Charge–discharge efficiency (η)

Low η implies high energy consumption during electrical charging and discharging, which is not ideal for AC/DC cycles. NBT currently offers the highest η of $\sim 89\%$, followed by NN ($\sim 84\%$), BF ($\sim 75\%$), and AN ($\sim 71\%$). Recent studies have focused more on RFE-type dielectrics, *e.g.*, NBT, realising high η over AFE-type dielectrics (*e.g.*, AN and NN). To understand the origin of low η at room or elevated temperatures, the local structural analysis and electrical microstructure of dielectric ceramics must be closely examined. Possible reasons include electric field-induced phase transition(s), motion of oxygen vacancies, changes in resistivity, capacitance, activated energy and electrical homogeneity.

6.4. MLCC development

The chemical reaction between Bi-based dielectrics and low-cost internal electrodes, such as Ag and Ni (under a controlled atmosphere), significantly restricts their potential for large-scale manufacture. AN and NN-based dielectrics offer the possibility of co-firing with cost-effective (BME) electrodes, although Ag/30Pd and Pt were still used in the literature. For AN and NN-based ceramics, glass additions could be used to reduce the sintering temperature, increasing compatibility with cost-effective electrodes. This would also decrease resistivity in grain boundaries, increase density and create a more uniform microstructure, all of which enhance the breakdown strength of the ceramic layers.²⁴⁹ Similar strategies have been successfully employed in BT MLCCs. Recent developments in

academia and industry have focused on improving the volumetric efficiency and reliability of MLCCs, driven by the demand for advanced electronics and electric vehicles. Notable companies leading these advancements include Murata Manufacturing, TDK Corporation, and Samsung Electro-Mechanics.

Data availability

No primary research results, software or code have been included and no new data were generated or analysed as part of this review.

Conflicts of interest

There is no conflict of interest related to this publication

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