


RESEARCH ARTICLE

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2017, 1, 1995***In situ* polymerized hyperbranched polymer reinforced poly(acrylic acid) hydrogels**Nazila Dehbari,^{†a} Javad Tavakoli,^{†b} Simranjeet Singh Khatrao^{ab} and
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Hydrogels have been extensively investigated for use in various applications. Poly acrylic acid (PAA) is a common example, which has been widely used due to its super hydrophilicity properties, biocompatibility and biodegradability characteristics. However its poor mechanical properties, which have been addressed in many research studies, are known as a drawback that limits its applications. So, enhancing PAA mechanical properties using a hyperbranched polymer (HB) is the key question to be addressed in this research. Investigations of the mechanical properties of the PAA-HB hydrogel revealed 130% improvement in the ultimate tensile strength, indicating a two times enhancement compared to that of PAA. Statistical analysis showed that the overall effect of introducing notches (with different depths) on the selected mechanical properties of both PAA and PAA-HB was significant. Mechanical characterization of PAA-HB networks showed that significant improvement in the mechanical properties was achieved as the capability of water uptake increased by 20%. Characterization of the physical properties confirmed that participation of HB may form a PAA based hybrid material with good swelling properties. Those findings are attributed to the supramolecular structure of the HB, which can introduce physical entanglement between the PAA network structure and increase the crystallinity of the final hydrogel as compared to those from the PAA hydrogel.

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Introduction

Hydrogels are three-dimensional cross-linked, water-swollen and hydrophilic polymers whose properties are highly dependent on the environmental conditions.^{1–3} As enviro-sensitive materials, hydrogels have been widely used for industrial and biomedical applications due to their unique structure and capabilities.^{4–6} The properties of a specific hydrogel are extremely important in selecting which materials are suitable for a given application. The suitability of a hydrogel for a given application depends on the mechanical properties that are affected by the environmental conditions such as temperature, pH level and ionic strength, magnetic and electric fields as well as the monomer type and crosslinking agents.^{7–9}

Among various types of hydrogels, poly acrylate polymers such as poly acrylic acid (PAA), with distinctive absorptivity properties, have the most versatile structure to enhance their practical utility in everyday life applications such as filtration, water remediation, diapers and hygiene products, cosmetics,

wound dressings, medical waste solidification and metal ion removal.^{10–14} From extensive studies evaluating different properties of PAA hydrogels, such as swelling,¹⁵ adhesion,¹⁶ diffusion,¹⁷ physico-chemical¹⁸ and mechanical¹⁹ properties, it has been revealed that the greatest concern about these types of hydrogels is their poor mechanical properties.^{11,20–22} The poor mechanical properties of PAA hydrogels, which relate closely to their large volume change subsequent to swelling, count as a marked weakness in consideration for adoption for high-tech applications, and have limited their specific applications.^{23,24} Typically, PAA hydrogels exhibit a low Young's modulus (<200 kPa) and low fracture energy (<20 J m⁻²), and possess a low tensile strength (<0.2 MPa).^{25,26} Therefore, there has been an urgent focus on improving the mechanical properties of PAA hydrogels *via* toughening methods by mixing different types of crosslinked polymers or introducing energy-dissipating mechanisms.^{27–29} Various methods of producing multi-functional cross-linked hydrogels,³⁰ nanocomposite hydrogels,³¹ hybrid interpenetrating networks,³² slip-link networks³³ and homogeneous hydrogels³⁴ have been introduced to toughen PAA hydrogels, resulting in improved mechanical properties. To the best of our knowledge, toughening hydrogels using chemical methods may limit their biomedical application as unreacted components adversely affect the biocompatibility.^{35,36} On the other hand although other methods were reported to enhance the mechanical properties of the hydrogels, some inherent disadvantages such as weak-self

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recovery and poor fatigue resistance still existed.²⁹ Contribution of hyperbranched polymers to hydrogels' toughening performance physically leads to unconventional assemblies and complex structures with responsive properties.^{37,38}

Recently, among the most extensively used nanoparticles, hyperbranched (HB) polymers, with a structure of highly branched tree-like dendritic material containing numerous –OH end groups, have been used in hydrogels.^{39–41} In a hydrogel crosslinked with HB polymers, polymeric chains have been held together by directionally discrete supramolecular binding sites to enhance the mechanical properties of the resultant composite.^{42,43} Evidence has suggested the potential for using HB polymers as a reinforcement agent in PAA based hydrogels.^{44,45}

The aim of this study was to toughen PAA hydrogels with a combination of covalent and physical crosslinking by introducing HB polymers, without sacrificing the swelling ratio of the final product. This was achieved through *in situ* polymerisation, which is an easy process, and a cost-effective and environmentally friendly method. The structure–property relationship of the hydrogels was evaluated and a possible mechanism was also proposed.

Material preparation and characterisation

Material preparation

Acrylic acid monomer (AA), hyperbranched bis-MPA polyester-64-hydroxyl (HB), ammonium persulfate (APS), the initiator, and *N,N'*-methylenebis (acrylamide) (MBA), the crosslinking agent, were purchased of an analytical grade from Sigma Aldrich (Australia) and used without any further purification. Sodium hydroxide (NaOH) was supplied by Chem-Supply (Australia). All aqueous solutions were prepared using Milli-Q water at room temperature.

Synthesis of the PAA-HB solution was done by following the method used in previous work.³¹ Briefly, 3.7 g of acrylic acid was dispersed in 3.5 cm³ of distilled water at 5 °C. A 0.45 g cm⁻³ NaOH solution was prepared by dissolving 1.63 g of sodium hydroxide powder in 3.62 g of distilled water followed by cooling in an ice-water bath for 10 min. The NaOH solution was then added to the acrylic acid solution dropwise with magnetic stirring at 5 °C for 20 min. Finally, 0.025 g of MBA and 0.08 g of APS powder were added to the mixture, followed by vigorous shaking using an IKA Vortex 3 shaker to ensure homogeneity. The mixture was poured into a glass mould and placed in an oven (preset at 60 °C) for 30 min with the temperature being increased from 60 to 80 °C at a rate of 1 °C min⁻¹. After the overall heating duration of 30 min, the prepared hydrogels were cooled to room temperature for 2 h, and kept in the oven. The synthesized PAA samples were peeled off from the mould and stored in sealed bags at 4 °C for testing. For the PAA-HB sample, 3.5 cm³ of distilled water was first mixed with 0.6 g of HB powder and 3.7 g of acrylic acid was added to the suspension, which was then shaken vigorously using an IKA Vortex 3 shaker. The rest of the procedure was the same as above.

Material characterisation

Spectroscopic analysis. To investigate the possible interaction between the PAA and HB in the hybrid samples in terms of their functional groups, Fourier transform infrared (FTIR) spectroscopy (PerkinElmer Spectrum 400 spectrometer equipped with an attenuated total reflectance (ATR, top-plate type)) was performed. Each sample was mounted in turn onto the central crystal of the ATR plate, and air was used as a background reference before each scan. FTIR spectra were then recorded using 64 scans from 4000 to 550 cm⁻¹ with a resolution of 4 cm⁻¹ in absorbance mode with background subtraction.

Thermal analysis. The thermal behaviour of the hydrogels was studied using a differential scanning calorimeter (DSC) (TA instruments, USA). Samples were heated in a sealed aluminium crucible with another empty aluminium crucible as a reference, over the temperature range of –30–300 °C at a rate of 10 °C min⁻¹ in a N₂ atmosphere.

Morphology characterization. The surface morphology of the PAA and PAA-HB hydrogels was characterized using scanning electron microscopy (SEM) (CamScan MX2500). Dried specimens were mounted on aluminium stubs with double adhesive tape, then sputter coated with platinum at 2 nm thickness. The high voltage was set at 10 kV and the distance from the sample to the beam source was kept constant for all the tests performed. To investigate the distribution of HB particles in the PAA hydrogel, a transmission electron microscope (TEM) (Philips CM200, the Netherlands) was employed. For preparation of the TEM specimens, all the hydrogel samples were completely dried in a vacuum oven overnight at 50 °C. Then, the samples were ultramicrotomed using glass knives on an ultra-cut microtome (Leica Ultra cut-R ultramicrotome, Germany) to produce thin sections with a nominal thickness of 100 nm.

Swelling behaviour. The swelling behaviour of the PAA and PAA-HB samples was tested by measuring the initial weight of the dry samples and subsequently the weight after they had been immersed in distilled water until equilibrium. Each test was repeated three times. Before measurement of the weight of the swollen samples, excess surface water was removed using filter paper. The swelling ratio was calculated using the equation:

$$SR = \frac{m_t - m_0}{m_0} \times 100 \quad (1)$$

where m_0 and m_t are the weight of the sample in the initial dry and the swollen state, respectively.

Also, swelling kinetics of PAA and PAA-HB hydrogels for pH sensor applications were conducted in solutions at different pH values, *i.e.* 2, 7 and 10, attuned by sodium hydroxide and hydrochloric acid in deionized water. The dynamic swelling kinetics of both samples were explored by soaking and alternating them between solutions of pH 10 and 2 every two hours, 3 times.

Mechanical properties. The mechanical properties of PAA and PAA-HB were measured for intact and notch-induced samples, using an Instron universal testing machine. All the samples were cut into a square shape with the dimensions 3.0 mm × 3.0 mm. Each sample's thickness was measured as



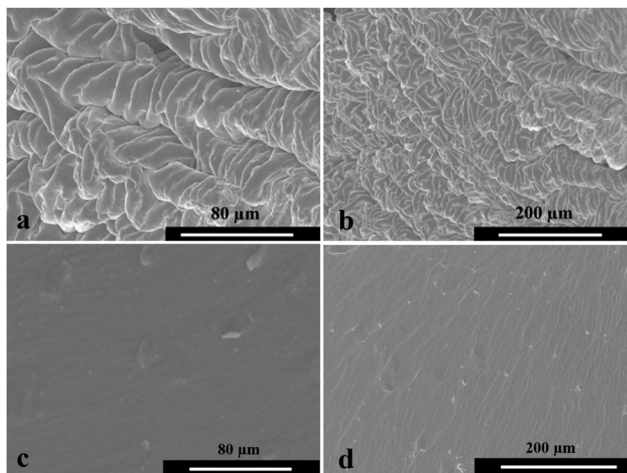


Fig. 3 SEM images of (a) and (b) PAA-HB surfaces and (c) and (d) PAA surfaces.

distributed into the PAA structure, as shown in Fig. 3. The rough surface of the PAA-HB also suggested good dispersion of the HB within the PAA. A change in surface morphology of the PAA-HB samples, as compared to the smooth surface of a PAA sample, is consistent with FTIR results that suggest the possibility of hyperbranched polymer contribution to the structural organization of PAA molecules. Also TEM images suggest good dispersion of HB inside the PAA, as shown below.

TEM images of PAA-HB samples are shown in Fig. 4. The aggregated nanospheres in the range of 10–200 nm in diameter are attributed to the HB polymer binders which are dispersed well in the PAA matrix. Due to the numerous hydroxyl groups at the ends of the HB, the particles tend to aggregate. Meanwhile, the hydrophilic character of these hydroxyl groups could help to enhance the compatibility of HB with PAA during *in situ* polymerisation.³¹

Water swelling behaviours

The swelling behaviours of PAA and PAA-HB hydrogels immersed in water at 25 °C are shown in Fig. 5. The addition of HB into the PAA solution caused increased water uptake by the hydrogel. In the first 15 minutes, the water uptake of both hydrogels was extremely fast, followed by constant increments, finally reaching equilibrium within 150 min. In the PAA sample, the swelling ratio (SR) at the equilibrium stage was about 86k % of its initial weight. With the introduction of HB, however, this amount increased to a higher value of 9.6k %, which was about 1.12 times higher than that of the PAA. This increase was attributed to the availability of a large

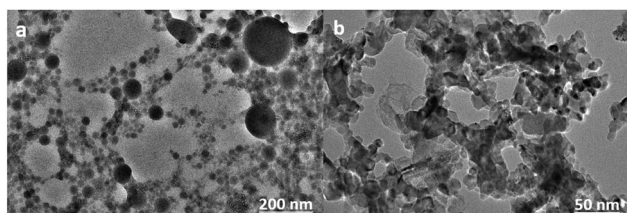


Fig. 4 TEM images of the PAA-HB hydrogel.

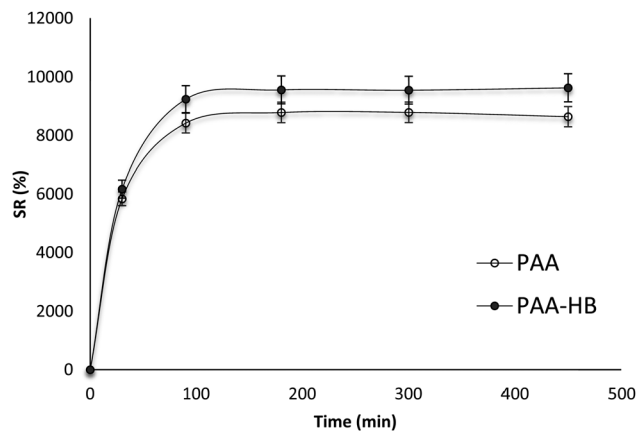


Fig. 5 Swelling ratios of PAA and PAA-HB hydrogels immersed in water.

number of hydrophilic hydroxyl groups in the HB particles, which could bind to water and increase the absorption capacity of the hydrogel. The slopes of SR *versus* immersion duration of both PAA and PAA-HB samples had similar trends. Once the time exceeded 150 min, the SR of samples reached a plateau, indicating excellent water retention by the PAA and PAA-HB hydrogels.

Mechanical behaviours of hydrogels

The effects of adding HB to the PAA structure on the mechanical properties of the PAA-HB hydrogel are shown in Fig. 6. As shown, the ultimate tensile strength of the PAA-HB hydrogel improved by 130% (1.15 ± 0.10 MPa) compared to the PAA hydrogel with an ultimate strength of approximately 0.50 ± 0.04 MPa. Also, elongation at break is doubled, from $340 \pm 12\%$ for PAA to $650 \pm 35\%$ for PAA-HB. Thus, the fracture energy of the PAA-HB hydrogel, measured as 4483 ± 39 kJ m⁻³, is approximately four times greater than that of the PAA hydrogel, which was 1020 ± 29 kJ m⁻³.

Stress–strain curves for the PAA-HB samples at different stretch ratios are presented in Fig. 7. The stretch ratio (λ) was defined as the ratio of final to initial length. As is evident, the stress–strain relationship for all stretch ratios is linear for strain less than 50%. As λ increases, the ultimate tensile stress and the corresponding strain both increase. Table 1 shows the change in ultimate stress, the Young's modulus and toughness at different stretch ratios.



Fig. 6 Mechanical properties of PAA and PAA-HB hydrogels.



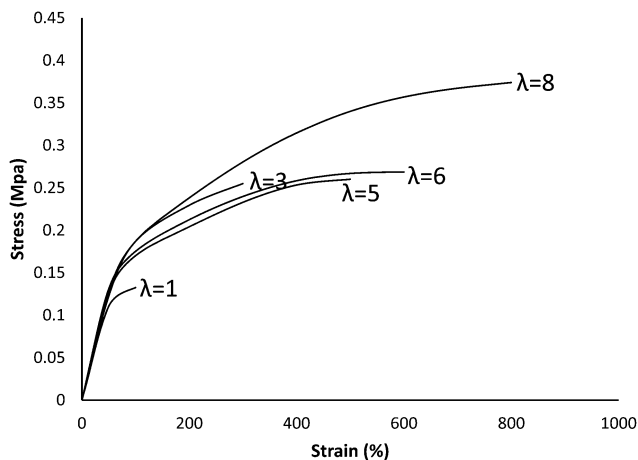


Fig. 7 Stress-strain relationship for PAA-HB hydrogels at different stretch ratios.

A comparison of the mechanical properties of PAA and PAA-HB at different notch depths is presented in Fig. 8. The stretchability of PAA-HB samples with selected notches of 0 and 14 mm is also shown in Fig. 8.

As shown, the unnotched samples display greater toughness, elongation at break and ultimate strength than the notched samples. Also the PAA-HB samples have significantly enhanced mechanical properties compared to the PAA samples. Surprisingly, the ultimate tensile strength for the PAA-HB samples with notch depths of 3, 5 and 8 mm remains constant at approximately 0.10 ± 0.02 MPa. A similar trend is found for the samples with 11 and 14 mm notches, as shown in Fig. 8(a). Generally, the elongation of the unnotched PAA-HB samples is about twice that of the intact PAA samples. The stretchability of the PAA-HB and PAA samples for different notch depths is about 20% and 50% lower than those of the corresponding intact samples, respectively, and remains constant for all notch depths, as shown in Fig. 8(b). Fig. 8(c) shows that both intact and notched PAA-HB samples with different depths have significant improvement in fracture toughness compared with the corresponding PAA samples. The PAA samples with notch depths greater than 5 mm have negligible toughness.

Statistical analysis revealed that the overall effect of introducing different notches on the selected mechanical properties of stiffness, elongation at break and ultimate strength of both PAA and PAA-HB was significant ($P < 0.01$). Due to the marked decrease in these mechanical properties of PAA after notch insertion, changes in notch depth showed no significant effect on the ultimate strength ($P = 0.99$), whereas in the PAA-HB samples, introducing a notch with depth greater than 11 mm resulted in a significant change in ultimate strength ($p = 0.004$).

Meanwhile, it was found that a change in notch depth from 1 to 5 mm had a significant effect on the PAA samples' elongation at break ($P = 0.003$), but not when the notch was greater than 5 mm ($P = 1.00$). In contrast, the addition of HB into the PAA structure improved the elongation at break property. It was shown that the change was negligible for samples with notch depth difference less than 6 mm ($P = 0.593$). For PAA samples with notch depth greater than 2 mm, the change in fracture toughness was significant ($P = 0.021$). However, notches of at least 6 mm or greater needed to be introduced to the PAA-HB samples to significantly affect toughness ($P = 0.004$).

Fig. 9 shows the results of dynamic tests that were performed on intact PAA-HB samples. As shown, the hysteresis effect for the first loading to a stretch of $\lambda = 4$ and the subsequent unloading to zero is huge in comparison to that of samples with a second loading. The PAA-HB hydrogels dissipated energy effectively and their hysteresis loop was reduced for the second loading at different time intervals after the first loading. It seems that the change in maximum stress at a stretch ratio of 4 was negligible for all second tests for a given sample, indicating the effect of hyperbranching on the mechanical properties of the PAA due to increasing physical interaction or internal friction.

Proposed mechanism

Hydrogels of PAA and PAA-HB were successfully synthesized through a one-step, cost-effective and environmentally friendly method. From the above investigations, the mechanism for the PAA-HB network structure can be proposed. Fig. 10 illustrates the structure of the PAA hydrogel with HB particles. Numerous $-COOH$ groups of PAA result in the formation of hydrogen bonding. These hydrogen bond formations are increased in the presence of water. On the other hand, HB experiences some physical entanglement in PAA networks due to its high molecular weight and star shape. Meanwhile, the $-OH$ groups of HB can effectively connect with the $-COOH$ groups of PAA, resulting in the formation of hydrogen bonding. After MBA and APS were added during *in situ* polymerisation, PAA networks were constructed tightly around the HB molecules. Therefore, PAA-HB hydrogels are expected to have higher mechanical properties compared to those of PAA hydrogels.

To compare our study with other research studies relevant information is presented in Table 2, more details have to be noticed during the comparison as mechanical characterisation was performed under different conditions. As it can be seen from the table, different toughening agents/methods, *i.e.* graphene oxide, branched polymers, hyper-branched polymers, IPN, etc., may improve some mechanical properties while their negative effects on other properties, such as swelling ability need to be addressed.

Table 1 Change in the selected mechanical properties of PAA-HB at different stretch ratios

Mechanical properties	Unit	Stretch ratio (λ)				
		1	3	5	6	8
Ultimate stress	MPa	0.13 ± 0.21	0.25 ± 0.18	0.26 ± 0.27	0.27 ± 0.15	0.37 ± 0.14
Young's modulus	MPa	2.21 ± 0.18	2.55 ± 0.12	2.55 ± 0.08	2.55 ± 0.16	2.55 ± 0.21
Toughness	kJ m^{-3}	97 ± 11	459 ± 32	835 ± 49	1094 ± 69	2124 ± 51



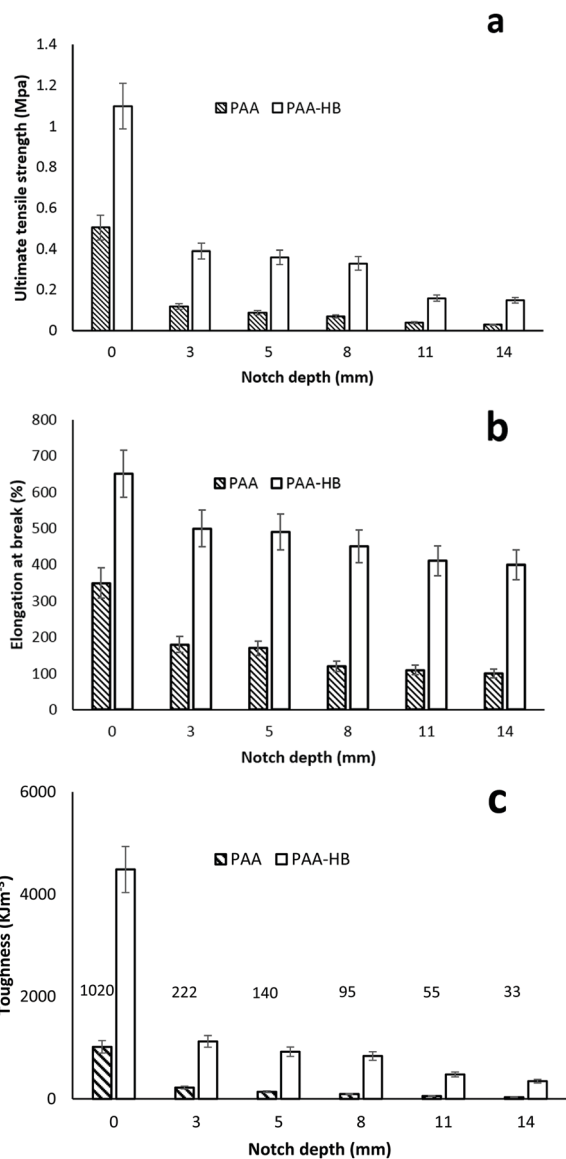


Fig. 8 Comparison of the mechanical properties of PAA with PAA-HB hydrogel for different notch depths. (a) Ultimate tensile strength, (b) elongation at break and (c) toughness. Figure (d) shows the stretchability of the intact sample (un-notched) versus the notched sample (14 mm) for both PAA and PAA-HB hydrogels.

Sensor application

To investigate the possibility of utilizing the toughened PAA-HB hydrogel as a pH-sensitive sensor, its enviro-responsive and dynamic swelling properties were investigated here. Measuring the swelling ratio as a function of time in solutions at different



Fig. 9 Hysteresis effect of loading to a certain stretch ($\lambda = 4$) and unloading to zero for first and second loadings with different time intervals. All dynamic tests were performed at 50 mm min^{-1} strain rate.

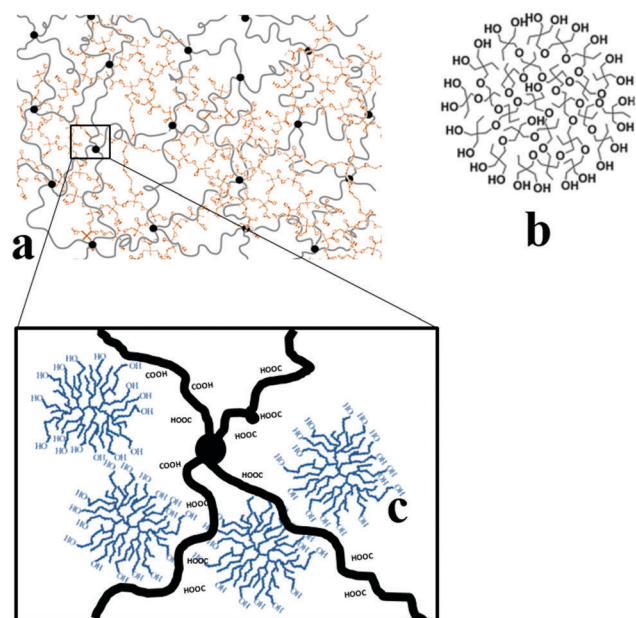


Fig. 10 (a) Interpenetrating networks of PAA-HB; (b) schematic structure of a HB molecule; and (c) schematic illustration of the possible physical interaction and hydrogen bond formation mechanism between PAA chains and HB molecules.

pH values of 2, 7 and 10 revealed that the overall trend of swelling kinetic curves for PAA-HB samples are consistent with those without HB. Below the pK_a , both PAA and PAA-HB samples swelled significantly less than those above the pK_a ($P = 0.041$). However, the increase of the pH value resulted in a higher swelling ratio for PAA-HB samples compared to that of PAA samples (Fig. 11a). As it is shown in Fig. 11b, despite a negligible change in the equilibrium swelling ratio (ESR) for PAA and PAA-HB samples at pH = 3, increasing the pH value from 7 to 10 resulted in 10% and 23% ESR increases for PAA-HB compared to those of PAA, respectively.

Dynamic swelling behavior, with the pH value alternating between 2 and 10, was examined to confirm the reversibility of



Table 2 Different PAA hydrogel toughening methods with selected mechanical and swelling properties

Method	UTS (MPa)	EAB (%)	SR (%)	T (MJ m ⁻³)	Ref.
PAA hydrogel	0.07	115	300	0.5	50
	0.06	78	8000	N/A	31
Dually cross-linked single network	1	2000	1800	13.5	50
Micellar copolymerization of acrylic acid	1.7	800	500	N/A	51
Incorporating nanosilica and branched polymer	0.15	1200	250	N/A	52
PAA-chitosan IPN	6	10	70	N/A	53
PAA-PVA IPN	0.5	200	35	N/A	54
PAA-graphene oxide	0.03	300	100	N/A	55
	0.2	450	12000	N/A	31
PAA-guar gum membrane	40	60	N/A	N/A	56
PAA-cellulose nanocomposite	0.35	400	350	N/A	57
PAA-hyper-branched nanocomposite	1.25	650	10 000	2.124	Our study

the swelling process and the ability of the samples to maintain their swelling capacity during cycling deformation. All cycles were performed in two-hour time intervals as swelling kinetics showed that samples approximately approached their equilibrium state after two hours. The ratio of samples' swelling ratio at pH 10 and 2 (mentioned as SR10/SR2 and called the reversibility factor (RF)) was calculated and compared for three cycles. As shown in Fig. 12a, comparing the 2nd and 3rd cycles to the 1st cycle, changes in RF for PAA-HB samples were significantly lower than those of PAA samples ($P = 0.046$). It means that differences between the swelling ratio at pH 10 and 2 were less for PAA-HB samples as compared to those of PAA samples.

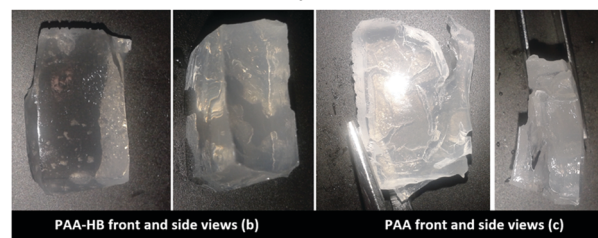
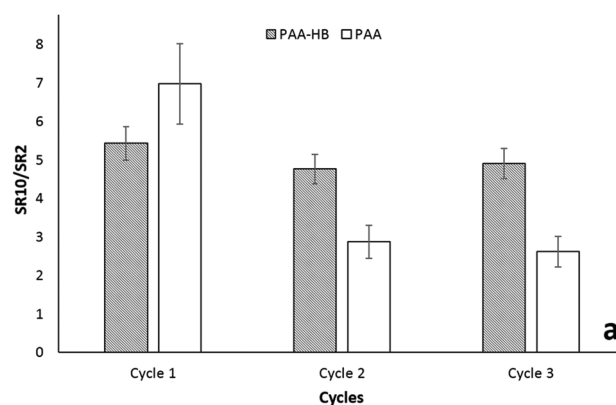


Fig. 12 (a) Change in the SR10/SR2 ratio during three cycles of dynamic swelling revealed higher pH sensitivity of PAA-HB hydrogels compared to that of PAA samples. After 3 cycles, the better dimensional stability of (b) PAA-HB samples compared to that of (c) PAA samples was in general agreement with the enhanced mechanical properties from HB.

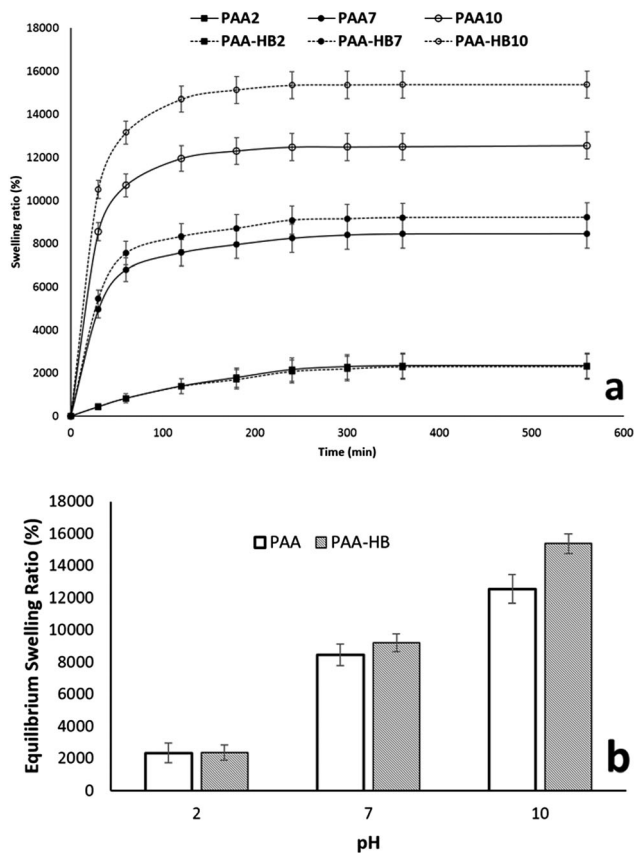


Fig. 11 Effect of pH values on the (a) swelling kinetics and (b) equilibrium swelling ratio (ESR) of PAA and PAA-HB samples.

Meanwhile, after performing 3 cycles of dynamic swelling, PAA-HB samples were more structurally stable than PAA hydrogels. Deep cracks and dimensional instability were observed in PAA samples after the alternative swelling/de-swelling process. HB addition provides improved mechanical properties to the hydrogel, enhances the pH sensitivity of PAA hydrogels and improves the swelling properties with a positive impact on dimensional stability.

Conclusions

In this study, by introducing a HB polymer into PAA using *in situ* polymerisation, a hydrogel network was formed with the mechanical entanglement of HB into the PAA structure and a possible hydrogen bond between the active group of HB and $-COOH$ groups of PAA. TEM results showed that spherical HB



particles were well dispersed in the PAA matrix, indicating good compatibility of PAA with HB. Significant improvements in the mechanical properties were achieved when the capability of water uptake was increased by approximately 20%. With the introduction of notches in the PAA and PAA-HB samples, the effects on selected mechanical properties were significant; but notches of at least 6 mm or greater had to be introduced to significantly affect the toughness of the PAA-HB samples. It is worth mentioning the possibility of their application in sensors, where the simultaneous enviro-responsive and mechanical properties of hydrogels are important.

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