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# Unveiling the role of cobalt in the product regulation for CO<sub>2</sub> hydrogenation to light olefins over alumina-supported Co–Fe catalysts†

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CoFe-based catalysts for CO<sub>2</sub> hydrogenation reactions have been widely studied, but the effects of cobalt on the product regulation remains largely over-looked. In the present study, we report a series of Na-decorated alumina-supported Co–Fe bimetallic catalysts with varying Co/Fe molar ratios for the direct conversion of CO<sub>2</sub> to light olefins. *In situ* XRD and Mössbauer spectroscopy reveal that Co doping significantly promotes the reduction and carburization of Fe species, leading to the formation of active CoFe alloy carbides. Furthermore, the DFT results indicate that cobalt decreases the H<sub>2</sub> adsorption energy, thereby regulating the surface C/H ratio and enhancing the tandem RWGS and Fischer–Tropsch reactions. These effects synergistically improve the formation and desorption of light olefins. As a result, the optimal Co1Fe2 catalyst (Co/Fe = 1/2) achieves a high STY of 315.1 g<sub>cat</sub><sup>-1</sup> h<sup>-1</sup> for light olefins with a CO<sub>2</sub> conversion of 51.9% at 320 °C. This study provides mechanistic insights into cobalt-assisted product selectivity control and offers a promising strategy for designing highly efficient CO<sub>2</sub>-to-light olefins catalytic systems.

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## Introduction

The excessive anthropogenic CO<sub>2</sub> emissions caused by social development have resulted in significant environmental issues, including global warming and ocean acidification.<sup>1–3</sup> In recent decades, the thermal catalytic conversion of CO<sub>2</sub> with green H<sub>2</sub> to produce high-value-added chemicals has attracted considerable interest.<sup>4</sup> Among these, light olefins (including ethylene, propylene, and butene) are widely used in the production of plastics, fibers, and other chemical products. Traditionally, they are obtained by naphtha cracking. As the crisis of non-renewable energy sources has received increasing attention, the efficient catalytic CO<sub>2</sub> hydrogenation to produce light

olefins represents a potential strategy to mitigate the greenhouse effect and alleviate the market demand, given its status as an industrialized method today.

Typically, the hydrogenation of CO<sub>2</sub> to light olefins can be achieved through two distinct routes: a modified Fischer–Tropsch synthesis (CO<sub>2</sub>-FTS) route or a tandem methanol-mediated (MeOH) route.<sup>5,6</sup> The FTS pathway can be divided into a two-stage cascade reaction, comprising a reverse water gas shift (RWGS) reaction and Fischer–Tropsch synthesis. Fe-based catalysts have been extensively investigated due to their cost-effectiveness and strong adaptability to reaction conditions.<sup>7–11</sup> Nevertheless, the carbon efficiency remains low due to the restricted target selectivity of the FTS process and the constrained thermodynamic equilibrium CO<sub>2</sub> conversion rate. To address this case, various strategies have been adopted to regulate the activity and product selectivity over Fe-based catalysts. The doping modification with alkaline promoters, such as Na and K, has been demonstrated to enhance the CO<sub>2</sub> adsorption and facilitate the formation of active phases.<sup>12–14</sup> Wang *et al.*<sup>12</sup> reported that the presence of Na played an important role in regulating the electronic properties of iron carbide and adsorption behaviours of reactant molecules, resulting in a significant increase in total olefin selectivity from 27% to 76%. In addition, the incorporation of a second active metal (*e.g.*, Co, Cu) was also a prevalent strategy to enhance the catalytic performance of Fe-based catalysts.<sup>15–17</sup> Among them, cobalt is

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frequently employed to modify iron-based catalysts due to its high reducibility and the ability to dissociate CO and H<sub>2</sub>. However, the primary products of the individual Co-based catalysts in CO<sub>2</sub> hydrogenation were mainly CH<sub>4</sub> instead of C<sub>2+</sub> hydrocarbons, due to the inability of cobalt in the RWGS reaction.<sup>18</sup> As a result, the key to optimizing iron-based catalysts for efficient CO<sub>2</sub> hydrogenation by cobalt doping lies in understanding how to regulate the structural evolution and surface chemistry properties of the iron species. Therefore, it is imperative to construct a cobalt–iron bimetallic catalyst that combines the high activity and reducibility of cobalt with the high olefin selectivity of iron.

Up to now, considerable efforts have been dedicated to developing efficient cobalt–iron bimetallic catalysts and exploring their synergistic effect for CO<sub>2</sub> hydrogenation.<sup>10,19–24</sup> By modifying the preparation methods, the active components and catalytic performance of catalysts with different composition and structure have been investigated. Zhang *et al.*<sup>19</sup> reported a Na-modified CoFe alloy catalyst utilizing layered double hydroxide precursors that could directly convert CO<sub>2</sub> into jet fuel comprising hydrocarbons. At 240 °C, the catalyst exhibited an unprecedented jet-fuel-range hydrocarbons selectivity of 63.5% with a CO<sub>2</sub> conversion of 10.2%, and a combined selectivity of less than 22% for the unwanted CO and CH<sub>4</sub>. Liu *et al.*<sup>20</sup> prepared a series of Na-promoted Co–Fe bimetallic catalysts with varying compositions or proximity and elucidated the structural evolution that occurred during the reduction and reaction. It was demonstrated that the incorporation of the Co element could enhance the reducibility of the catalyst and facilitate the formation of carbides, thereby exhibiting remarkable improvements for CO<sub>2</sub> hydrogenation to olefins. Even though the doping of Co is believed to play a crucial role in determining the reduction and carburization of Fe-based catalysts and promoting cascade reactions between chain propagation, the current understanding is limited, and the contribution of Co in regulating the product distribution remains largely over-looked.

Herein, we prepared a series of Na-modified alumina-supported Co–Fe bimetallic catalysts with varying Co/Fe molar ratios and tested their catalytic performance for directly synthesis of light olefins from CO<sub>2</sub> hydrogenation. The specific roles of Co doping on the structural evolution and surface chemical properties of iron-based catalysts were investigated by a variety of *ex/in situ* characterization techniques. It was observed that the reduction and carburization of Fe species was facilitated by the cooperation of Co. In addition, the augmented dissociation of H<sub>2</sub> from Co doping helped to regulate the C/H ratio on the catalyst surface, accelerating transfer of reaction intermediates species and thus reinforcing the cascade reactions between RWGS and FTS. As a result, the optimal Co1Fe2 catalyst with the Co/Fe molar ratio of 1/2 exhibited more distinguished catalytic performance for CO<sub>2</sub> hydrogenation to light olefins relative to other catalysts, and demonstrated no evident deactivation during the 100 h stability test. This work is expected to provide a valuable contribution for studying the specific promoting effects of cobalt on Co–Fe bimetallic catalysts.

## Experimental

### Catalyst preparation

Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O, Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O, urea, and Na<sub>2</sub>CO<sub>3</sub> were purchased from Fujifilm Chemical Reagent Co. Ltd. Al(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O was purchased from Sigma-Aldrich Chemical Reagent Co. Ltd. All reagents were of analytical grade and used as received without further purification.

A series of precursor samples were synthesized by a facile hydrothermal method, as described in our previous work with minor modifications.<sup>18</sup> Take the Co1Fe2 catalyst for example, 5 mmol of Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O, 10 mmol of Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O, and 5 mmol of Al(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O were dissolved sequentially in 100 mL of deionized water with magnetic stirring. Subsequently, 0.1 mol of urea was added to aforementioned solution under constantly stirring and then the stirring was continued for 30 min. Subsequently, the suspension was transferred into a Teflon-lined stainless-steel autoclave and subjected to hydrothermal treatment at 120 °C for 10 h under autogenous pressure. The precipitate was filtered and washed three times with deionized water by centrifugation until the pH of the supernatant reached 7. The resulting sample was then dried at 80 °C overnight to obtain the precursor. The mixed metal oxides were obtained by calcining precursors in air at 400 °C for 4 h. Then, the Na-decorated catalyst was prepared by the incipient wetness impregnation method using Na<sub>2</sub>CO<sub>3</sub>. Specifically, a certain amount of Na<sub>2</sub>CO<sub>3</sub> was dissolved in 0.3 mL of deionized water and slowly dropped onto 0.5 g of the calcined sample under ultrasonic conditions and continuously stirred with a glass rod. Once the surface was dry, the container was rinsed with 0.2 mL of water and the process was repeated, ensuring that all sodium ions were impregnated on the catalyst surface. This was followed by drying at 80 °C for 6 h and calcination at 550 °C for 2 h. The resulting product was denoted as Co1Fe2. The synthesis of Co0Fe, Co1Fe4, and Co2Fe1 catalysts was conducted using the same methodology as that employed for Co1Fe2, with the respective molar ratio of Co/Fe in the precursors. The amount of Al was kept constant, with the ratio of  $([\text{Co}]^{2+} + [\text{Fe}]^{3+})/[\text{Al}]^{3+}$  set at 3.

The various Fe-based catalysts doped with typical metals (Cu, Mn, Zn, and Zr) were prepared using the same methodology as that employed for Co1Fe2, with the respective nitrates in the precursors. The obtained samples were denoted as Cu1Fe2, Mn1Fe2, Zn1Fe2, and Zr1Fe2, respectively.

### Characterization

In order to ascertain the precise content of the Na promoter, the calcined samples were measured by inductively coupled plasma optical emission spectrometry (ICP-OES) analysis on a PerkinElmer 8300 instrument. The transmission electron microscope (TEM) and element mapping images were obtained using a FEI Tecnai F20 instrument operating at an accelerating voltage of 200 kV. The samples were dispersed in ethanol and dried on carbon-coated copper grids. The texture properties of the samples were determined by N<sub>2</sub> physisorption



measurements at  $-196\text{ }^{\circ}\text{C}$  using a Micromeritics 3Flex instrument. The samples were first degassed at  $250\text{ }^{\circ}\text{C}$  for 2 h to purify. The pore structures and properties were determined using Brunauer–Emmett–Teller (BET) and Barrett–Joyner–Halenda (BJH) method, respectively.

The crystalline and phase of the samples were determined by X-ray diffraction (XRD) performed on a Rigaku D/MAX2200PC instrument with Cu  $K\alpha$  radiation ( $\lambda = 1.54\text{ \AA}$ ) at 40 kV and 40 mA. The intensity data were recorded over the  $2\theta$  range of  $20\text{--}80^{\circ}$  with a scanning step length of  $5^{\circ}\text{ min}^{-1}$ . The average particle sizes of the samples were calculated according to Scherrer equation. *In situ* XRD measurements were carried out using a Rigaku SmartLab instrument to investigate the phase evolution of catalysts during the reduction (atmospheric pressure and temperature increased from room temperature to  $400\text{ }^{\circ}\text{C}$ ) and reaction (3 MPa and temperature increased from  $50\text{ }^{\circ}\text{C}$  to  $320\text{ }^{\circ}\text{C}$ ) processes. Mo  $K\alpha$  radiation ( $\lambda = 0.71\text{ \AA}$ ) was employed due to its superior penetration through the stainless-steel walls of the *in situ* high-pressure reactor. This higher-energy X-ray source enabled reliable phase identification under *operando* conditions, particularly for catalysts undergoing reduction and reaction at elevated pressure and temperature. Specifically, 50 mg of the sample was placed in the chamber under reducing conditions (high-purity  $\text{H}_2$ ,  $30\text{ mL min}^{-1}$ ) and gradually heated to  $400\text{ }^{\circ}\text{C}$  at a heating rate of  $5\text{ }^{\circ}\text{C min}^{-1}$  and maintained for 2 h. Subsequently, the reaction chamber was cooled to  $50\text{ }^{\circ}\text{C}$  naturally and the feed gas ( $\text{CO}_2/\text{H}_2/\text{Ar} = 27/68/5$ ) was switched to 3 MPa. As the temperature increased to  $320\text{ }^{\circ}\text{C}$ , the XRD spectrum was recorded. The reaction intermediates and mechanism were identified through *in situ* diffuse reflectance infrared Fourier transform (DRIFT) measurement on a Bruker TENSOR II spectrometer. In detail, 50 mg of the 20–40 mesh sample was subjected to a 2 h pretreatment at  $400\text{ }^{\circ}\text{C}$  in a high-purity  $\text{H}_2$ . Subsequently, the chamber was adjusted to the reaction temperature and pressure in an Ar atmosphere and the background spectrum was recorded. Subsequently, the feed gas ( $\text{CO}_2/\text{H}_2/\text{Ar} = 27/68/5$ ) was introduced to 3 MPa, and the infrared signal of the catalyst surface was recorded at 10 min intervals.

$\text{H}_2$  temperature-programmed reduction ( $\text{H}_2$ -TPR) was conducted on an Autochem II 2920 instrument. In a typical process, 50 mg of the catalyst was loaded into a quartz tube and pretreated at  $300\text{ }^{\circ}\text{C}$  for 1 h in pure He flow. After cooling to  $50\text{ }^{\circ}\text{C}$ , a mixture of  $\text{H}_2/\text{He}$  (1/9, v/v) was injected into the reactor with the temperature heated to  $800\text{ }^{\circ}\text{C}$  at a rate of  $10\text{ }^{\circ}\text{C min}^{-1}$ . The hydrogen consumption signal was quantified using TCD. All temperature-programmed experiments were performed on the same instrument as  $\text{H}_2$ -TPR. For  $\text{CO}_2$  temperature-programmed desorption ( $\text{CO}_2$ -TPD) experiment, 50 mg of the sample was pretreated in  $\text{H}_2$  at  $400\text{ }^{\circ}\text{C}$  for 2 h and then cooled to  $50\text{ }^{\circ}\text{C}$ . Subsequently,  $\text{CO}_2/\text{He}$  (1/9, v/v) was passed through for 1 h to saturate the sample with  $\text{CO}_2$ . The sample was then flushed with He for 1 h. Finally, the catalyst was heated to  $700\text{ }^{\circ}\text{C}$  while recording the TCD signal. The  $\text{CO}$ -TPD and  $\text{H}_2$ -TPD experiments were conducted using the same processing steps as  $\text{CO}_2$ -TPD, with the exception of the introduction of alternative adsorption gases. For  $\text{C}_3\text{H}_6$ -TPD

experiment, 50 mg of the spent catalyst was pretreated in He at  $300\text{ }^{\circ}\text{C}$  for 1 h and then cooled to  $50\text{ }^{\circ}\text{C}$ . Subsequently, pure  $\text{C}_3\text{H}_6$  was passed through for 1 h to saturate the sample with  $\text{C}_3\text{H}_6$ . The sample was then flushed with He for 0.5 h. Finally, the catalyst was heated to  $800\text{ }^{\circ}\text{C}$  while recording the TCD signal. The  $^{57}\text{Fe}$  Mössbauer spectroscopy (MES) technique was employed to detect Fe species in spent catalysts. This was achieved by utilizing a MS500 spectrometer at room temperature, with  $^{57}\text{Co}(\text{Rh})$  serving as the irradiation source.

### Catalytic performance test

The catalytic performance of the catalysts was evaluated in a fixed-bed reactor with a 6 mm inner diameter. Firstly, 0.2 g pelletized precursor sample (20–40 mesh) mixed with 0.5 g quartz sand was packed into the reactor and *in situ* reduced at  $400\text{ }^{\circ}\text{C}$  for 8 h using a pure  $\text{H}_2$  flow ( $40\text{ mL min}^{-1}$ , atmospheric pressure) prior to the reaction. After that, the reactor was cooled to reaction temperature and the reaction gas ( $\text{CO}_2/\text{H}_2/\text{Ar} = 27/68/5$ ) was gradually introduced into the reactor until the pressure increased to the target condition. The reaction conditions were  $320\text{ }^{\circ}\text{C}$ , 3 MPa,  $9000\text{ mL g}_{\text{cat}}^{-1}\text{ h}^{-1}$ , and TOS = 8 h unless specified. During the reaction, the effluent gas was quantitatively analyzed utilizing two online gas chromatographs. One was equipped with a thermal conductivity detector (TCD) and an active charcoal column to analyze the inorganic components and  $\text{CH}_4$ ; the other was equipped with a flame ionization detector (FID) and a HP-PLOTQ column to detect light hydrocarbons. The heavy hydrocarbons were collected in a cold trap using 2 g of dodecane as a solvent and analyzed using an off-line gas chromatograph equipped with an FID and a DB-1 capillary column.

The conversion of  $\text{CO}_2$ , selectivity of  $\text{CO}$  and  $\text{C}_i\text{H}_x$  hydrocarbons (excluding  $\text{CO}$ ), STY of  $\text{C}_2\text{--C}_4$ , and the probability of the chain growth value ( $\alpha$ ) were calculated as eqn (1)–(5).

$$\text{CO}_2 \text{ conversion (\%)} = \frac{n_{\text{CO}_2\text{in}} - n_{\text{CO}_2\text{out}}}{n_{\text{CO}_2\text{in}}} \times 100\% \quad (1)$$

$$\text{CO selectivity (\%)} = \frac{n_{\text{CO}}}{n_{\text{CO}_2\text{in}} - n_{\text{CO}_2\text{out}}} \times 100\% \quad (2)$$

$$\text{C}_i\text{H}_x \text{ selectivity (\%)} = \frac{i \times n_{\text{C}_i\text{H}_x}}{\sum_i i \times n_{\text{C}_i\text{H}_x}} \times 100\% \quad (3)$$

$$\text{STY} = \frac{p \times \text{GHSV} \times V_{\text{CO}_2} \times X_{\text{CO}_2} \times (1 - S_{\text{CO}}) \times S^i \times 14}{8.315 \times T} \quad (4)$$

$$\ln \frac{W_n}{n} = n \ln \alpha + \ln \frac{(1 - \alpha)^2}{\alpha} \quad (5)$$

where  $n_{\text{CO}_2\text{in}}$  and  $n_{\text{CO}_2\text{out}}$  are concentrations of  $\text{CO}_2$  in the feed gas and product, respectively;  $n_{\text{CO}}$  and  $n_{\text{C}_i\text{H}_x}$  are concentrations of  $\text{CO}$  and  $\text{C}_i\text{H}_x$  hydrocarbons in the product, respectively;  $X_{\text{CO}_2}$ ,  $S_{\text{CO}}$ , and  $S^i$  represent  $\text{CO}_2$  conversion and selectivity of  $\text{CO}$  and  $\text{C}_2\text{--C}_4$ , respectively;  $i$  and  $W_n$  represent the carbon number and weight fraction of a product containing  $n$  carbon atoms, respectively.



## Results and discussion

### Catalytic activity tests

Fig. 1a illustrated the XRD patterns of the prepared catalysts. After calcination, the diffraction pattern of the calcined Co0Fe catalyst indicated that  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> was supported on amorphous Al<sub>2</sub>O<sub>3</sub> nanosheets.<sup>25</sup> The addition of Co resulted in the appearance of diffraction peaks at  $2\theta = 30.3^\circ$  and  $43.4^\circ$ , which could be attributed to the spinel Co<sub>x</sub>Fe<sub>3-x</sub>O<sub>4</sub> phase.<sup>26</sup> Furthermore, the aforementioned diffraction peaks exhibited a shift towards higher  $2\theta$  with increasing Co addition (Fig. S1a†). This could be attributed to the isomorphous replacement of Fe<sup>3+</sup> at the octahedral position in the Co–Fe bimetallic catalyst by Co<sup>3+</sup>, which had a smaller radius.<sup>20,26,27</sup> This resulted in a contraction of the crystal structure and a shift of the diffraction peaks. Upon increasing the Co/Fe ratio to 1/2, the diffraction peaks belonging to Co<sub>3</sub>O<sub>4</sub> emerged.<sup>28</sup> In addition to its impact on the phase structure of the catalyst, the Co/Fe ratio also influenced the particle size. In accordance with the Scherrer equation, the particle size of the calcined catalyst exhibited a unidirectional decrease, from 22.1 nm for Co0Fe to 15.2 nm for Co2Fe1 (Table 1). In addition, the pore structure and performance of the catalysts were investigated using N<sub>2</sub> physical adsorption measurements. As shown in Fig. 1b, all catalysts exhibited a type IV isotherm according to the IUPAC classification with

a mesoporous structure. At medium relative pressure, the desorption branch rose faster than the adsorption branch due to N<sub>2</sub> capillary condensation, resulting in a hysteresis loop. After the capillary condensation filled the mesopores, the catalyst continued to adsorb to form a multimolecular layer and the desorption isotherm continued to rise. Therefore, an H3 hysteresis loop was observed on the catalyst. The isotherm did not have an obvious saturated adsorption platform, indicating the irregular pore structure. Table 1 showed the specific surface area and pore structure parameters of different catalysts. The incorporation of cobalt increased the specific surface area and pore volume of the catalyst. Combined with the reduction in catalyst particle size after cobalt addition (Table 1), the proximity of cobalt to iron was more conducive to the distribution of iron species.

The catalytic performance of a series of Fe-based catalysts doped with typical metals (Co, Cu, Mn, Zn, Zr, and Co) was investigated, and the results were showed in Fig. S2.† Among all tested catalysts, the Co-doping Co1Fe2 catalyst demonstrated the highest selectivity (44.3%) and STY (315.1 g kg<sub>cat</sub><sup>-1</sup> h<sup>-1</sup>) of light olefins, significantly outperforming the other catalysts. Moreover, it exhibited the lowest selectivity towards undesired by-products, with CO + CH<sub>4</sub> accounting for only 21.4%, signifying a substantial advantage over Fe-based catalysts previously reported for CO<sub>2</sub> hydrogenation to light olefins (Table S1†). This



Fig. 1 (a) XRD patterns and (b) N<sub>2</sub> adsorption–desorption isotherms of the prepared catalysts.

Table 1 Selected physical properties of various catalysts

Catalysts	Crystal size <sup>a</sup> (nm)	Surface area (m <sup>2</sup> g <sup>-1</sup> )	Pore diameter (nm)	Pore volume (cm <sup>3</sup> g <sup>-1</sup> )	Na content <sup>b</sup> (wt%)
Co0Fe	22.1	50.1	9.6	0.20	3.8
Co1Fe4	17.3	108.1	10.3	0.41	3.7
Co1Fe2	16.7	97.7	11.9	0.36	4.1
Co2Fe1	15.2	93.2	14.3	0.46	4.1

<sup>a</sup> Calculated from Fe<sub>2</sub>O<sub>3</sub> (104) plane using the Scherrer equation. <sup>b</sup> Obtained from ICP-OES measurements.



suggested a distinctive role for cobalt in facilitating superior product regulation, favoring the production of light olefins.

Fig. 2 and Table S2† illustrated the catalytic performance of the prepared catalysts with varying Co doping in the CO<sub>2</sub> hydrogenation reactions. At 320 °C and 3 MPa, the Co-free catalyst (Co0Fe) showed a C<sub>5+</sub> selectivity of up to 50.4% with a CO<sub>2</sub> conversion of 36.8% (Fig. 2a). As the Co doping increased, the activity of the catalyst was enhanced, accompanied by a notable alteration in the product distribution towards light hydrocarbons. The CO<sub>2</sub> conversion increased from 36.8% (for the Co0Fe catalyst) to 61.6% (for the Co2Fe1 catalyst), while the selectivity of C<sub>5+</sub> in hydrocarbon products decreased from 50.4% to 25.2% with a marked increase in CH<sub>4</sub> selectivity from 10.1% to 42.3%. Additionally, an increase in the Co/Fe molar ratio resulted in a notable volcano-shaped distribution in the space time yield (STY) of C<sub>2</sub>–C<sub>4</sub>, which initially rose from 163.0 g kg<sub>cat</sub><sup>-1</sup> h<sup>-1</sup> for Co0Fe and reached its maximum of 315.1 g kg<sub>cat</sub><sup>-1</sup> h<sup>-1</sup> for Co1Fe2, then declined precipitously to 36.1 g kg<sub>cat</sub><sup>-1</sup> h<sup>-1</sup> for the Co2Fe1 catalyst.

The chain growth factors of catalysts with varying Co/Fe ratios revealed the alteration in product distribution after Co doping, as demonstrated in Fig. 2b. The Co0Fe catalyst, which lacked Co, exhibited the highest chain growth factor of 0.68. The chain growth factor demonstrated a decline with an increase in Co content, indicating that iron species was more advantageous than Co in promoting C–C coupling to C<sub>2+</sub> hydrocarbons, as opposed to the production of CH<sub>4</sub> in CO<sub>2</sub> hydrogenation (Fig. 2c). Conversely, the Co1Fe2 catalyst exhibited the highest selectivity for C<sub>2</sub>–C<sub>4</sub>. This illustrated that the incorporation of cobalt into the Fe-based catalyst restrained

the expansion of carbon chains, whereas the optimal amount of Co could effectively regulate the termination of carbon chains and enhance the selectivity of the target light olefins.<sup>29,30</sup>

The aforementioned results indicated that the Co1Fe2 catalyst demonstrated superior catalytic performance in comparison to other catalysts with varying Co/Fe ratios. As previously stated, the Na promoter modification has been demonstrated to enhance catalytic performance by modifying the electronic structure and adsorption properties of the catalyst surface.<sup>12,13</sup> However, an excess of Na content may potentially result in the coverage of the catalyst surface. An investigation was conducted into the effect of Na content on the performance of the Co1Fe2 catalyst (Fig. S3†). The results indicated that the optimal Na content of 4% achieved the highest catalytic activity and STY of C<sub>2</sub>–C<sub>4</sub>. Moreover, the sensitivity of the Co1Fe2 catalyst to the reaction conditions, including temperature, pressure, and GHSV, was evaluated, and the results were summarized in Table S3.† As illustrated in Fig. 3a, when the temperature was varied from 280 °C to 320 °C, a notable enhancement in CO<sub>2</sub> conversion was observed, rising from 31.6% to 51.9%. Concurrently, the light olefin selectivity exhibited a marked increase, rising from 35.7% to 44.3%. Jiang *et al.*<sup>31</sup> reported that the addition of Co promoted the consumption of CO in the FT reaction after the RWGS, thereby enhancing the CO<sub>2</sub> conversion of the Fe-based catalyst. It may be postulated that the rise in temperature served to further activate the synergistic effect between iron and cobalt, thereby promoting the efficient hydrogenation of CO<sub>2</sub> to low-carbon olefins. Upon further elevation of the temperature to 380 °C, the performance of the catalyst did not exhibit a notable enhancement. Furthermore, an increase in pressure resulted in

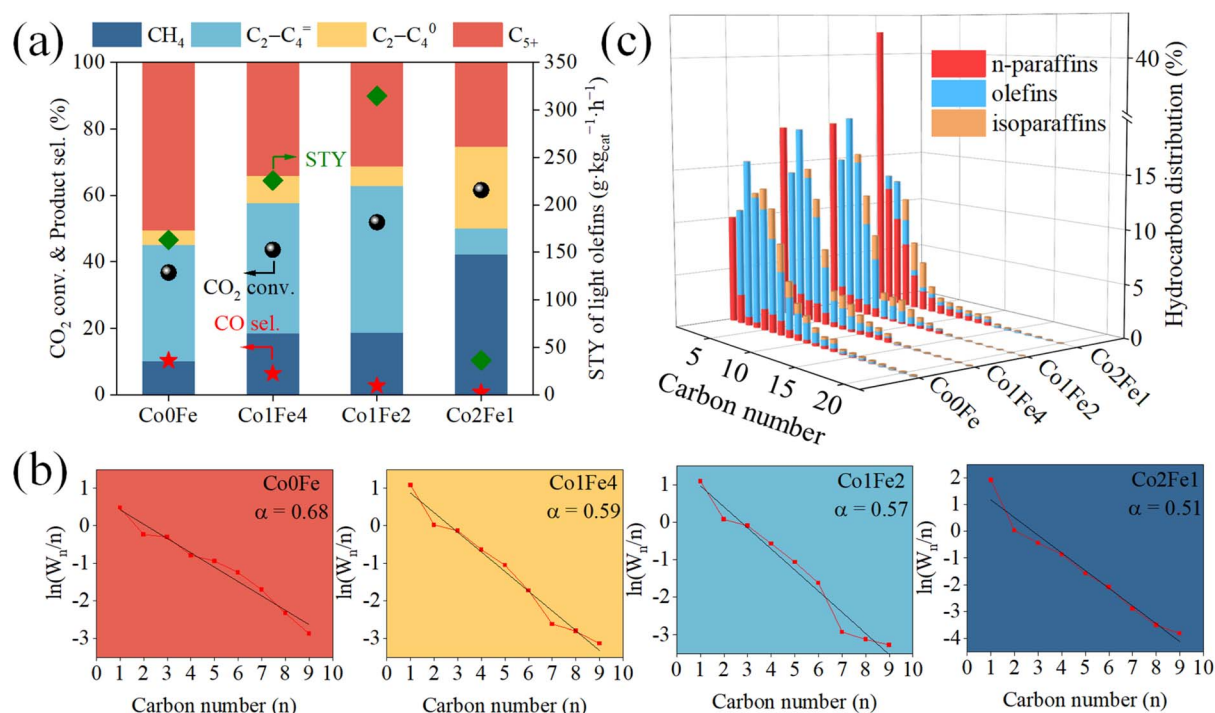


Fig. 2 (a) The catalytic performance of the prepared catalysts. (b) The chain growth factors of the prepared catalysts. (c) The product distribution of the prepared catalysts (reaction conditions: 320 °C, 3 MPa, 9000 mL g<sub>cat</sub><sup>-1</sup> h<sup>-1</sup>, TOS = 8 h).





Fig. 3 Effects of (a) reaction temperature, (b) pressure, and (c) GHSV on the catalytic performance of Co1Fe2. (d) The durability test of CO<sub>2</sub> hydrogenation over the Co1Fe2 catalyst (reaction conditions: 320 °C, 3 MPa, 9000 mL g<sub>cat</sub><sup>-1</sup> h<sup>-1</sup>, TOS = 8 h unless specified).

a slight increase in catalyst activity due to the molecule reduction reaction (Fig. 3b). An increase in space velocity resulted in a reduction of the effective residence time, and an increase in the number of reactant molecules entering the system. Concurrently, the adsorption sites and activation capacity of the catalyst surface were limited, resulting in a considerable portion of reactant molecules not participating in the reaction. Consequently, the CO<sub>2</sub> conversion decreased with an increase in GHSV, while the distribution of catalyst products remained largely unchanged (Fig. 3c). Moreover, the STY of light olefins was sustained above 200 g kg<sub>cat</sub><sup>-1</sup> h<sup>-1</sup> across almost all tested reaction conditions, indicating the stability of the catalysts and their adaptability to varying reaction conditions, which was conducive to large-scale industrial utilization. In addition, the catalytic activity and product distribution of the Co1Fe2 catalyst over a 100 h reaction period were illustrated in Fig. 3d. The catalytic performance of the Co1Fe2 catalyst remained largely stable after the initial few hours of the induction period. The CO<sub>2</sub> conversion exhibited a slight decline, from 51.9% (8 h) to 48.2% (100 h), while the selectivity of light olefins in the hydrocarbons was consistently above 40% across the tested points.

### Structural evolution of the catalysts

The reduction behavior of the catalysts was investigated to monitor the dynamic structural evolution and to evaluate the contribution of Co throughout the reduction process. As

illustrated in Fig. 4a, four reduction peaks were observed at 356, 458, 653 and 750 °C for Co0Fe catalysts. The former three peaks roughly corresponded to a stepwise reduction process from the initial α-Fe<sub>2</sub>O<sub>3</sub> through Fe<sub>3</sub>O<sub>4</sub>, FeO, and then to metallic Fe, respectively, while the last one could be attributed to the reduction of the iron species that interacted strongly with the support.<sup>32</sup> Following the introduction of Co, the position of the reduction peaks exhibited a notable shift towards lower temperatures. Moreover, the hydrogen consumption peak areas at elevated temperature were significantly reduced with increasing Co addition, indicating that the Co element may enhance the reducibility of the Co-Fe bimetallic catalysts. This could be assigned to the fact that Co was more readily reduced, thereby facilitating the dissociation of H<sub>2</sub>.<sup>33</sup>

This promotion effect was also reflected in the *in situ* XRD. As illustrated in Fig. S4a,† the Co0Fe catalysts did not exhibit notable alterations in the phase below 400 °C, remaining in the initial Fe<sub>2</sub>O<sub>3</sub> (PDF # 24-0072) phase. After 0.5 h at 400 °C, the intensity of the diffraction peaks of Fe<sub>2</sub>O<sub>3</sub> exhibited a gradual decline, accompanied by the gradual emergence of metal Fe (PDF # 01-1252). Following 2 h at 400 °C, the metal Fe had become the predominant phase, and the diffraction peaks belonging to iron oxides disappeared. In contrast, the diffraction peaks attributed to the CoFe alloy phase at 2θ = 15.1°, 16.2° and 24.1° appeared immediately at 400 °C in Co1Fe2 (Fig. 4c), which was earlier than that in the Co0Fe catalyst, indicating





Fig. 4 (a)  $H_2$ -TPR profiles of the prepared catalysts; (b) XRD patterns of the spent catalysts; *in situ* XRD patterns for the Co1Fe2 catalyst during the (c) reduction and (d) reaction process. "\*" symbol represents the diffraction peaks of sample holder, which is unavoidable because of supporting the samples.

that the Co1Fe2 catalyst could be reduced to the final alloy phase at a lower temperature and in a shorter time than the Co0Fe catalyst. These results suggested that the incorporation of Co could facilitate the reduction of iron species and accelerate the structural transformations of iron species during the reduction process, which was in accordance with the findings of the  $H_2$ -TPR experiments.

The structural evolution of the catalysts during the reaction process and the formation of active sites were characterized by *in/ex situ* XRD and STEM. Fig. 4c and S4a† illustrated the CoFe alloy and metallic Fe of the reduced Co1Fe2 and Co0Fe catalysts, respectively. Upon exposure to the reaction gas, the formation of carbides was observed at 320 °C in the Co1Fe2 catalyst (Fig. 4d), indicating the carburization of alloy species. As the reaction time increased, the diffraction peaks of the CoFe alloy phase diminished, while those of  $\chi$ -( $Co_xFe_{1-x}$ )<sub>5</sub>C<sub>2</sub> (PDF # 20-0509) became more pronounced. Simultaneously, the characteristic peaks belonging to the FeCo alloy oxides reemerged, and the dual phases collaboratively catalyzed the conversion of CO<sub>2</sub>. In contrast, the formation of carbide peaks was not observed in Co0Fe until 1 h at 320 °C, indicating that the Co0Fe

catalyst exhibited a lower carburization ability than the Co1Fe2 catalyst during the reaction (Fig. S4b†). It is widely acknowledged that metal carbides play a pivotal role in the synthesis of light olefins through CO<sub>2</sub> hydrogenation.<sup>34–36</sup> The presence of a greater number of metal carbides on Co1Fe2 with Co doping facilitated the formation of more active sites, thereby enhancing the overall activity and C<sub>2</sub>–C<sub>4</sub><sup>–</sup> selectivity.

The XRD and TEM were employed to confirm the active phases and structures of the spent catalysts. As illustrated in Fig. 4b, the presence of Fe<sub>3</sub>O<sub>4</sub> and Fe<sub>5</sub>C<sub>2</sub> was observed in the spent Co0Fe catalyst, which were identified as the two crucial active sites for the catalytic CO<sub>2</sub> hydrogenation to light olefins over iron-based catalysts.<sup>37</sup> With the introduction of Co, the diffraction peaks of Fe<sub>5</sub>C<sub>2</sub> shifted to a higher 2θ angle with an increase in the Co/Fe ratio (Fig. S1b†). This was consistent with the XRD patterns of the calcined catalysts. It was attributed to the doping of the Co with a small radius into the Fe<sub>5</sub>C<sub>2</sub> lattice, forming the  $\chi$ -( $Co_xFe_{1-x}$ )<sub>5</sub>C<sub>2</sub> structure, which narrowed the lattice.<sup>20,26,38</sup> Additionally, the peaks of Fe<sub>3</sub>O<sub>4</sub> were significantly weakened, accompanied by an increase in the peak belonging to iron carbide, which indicated that Co doping promoted the





Fig. 5 TEM and HRTEM images of the spent (a and b) Co0Fe and (c and d) Co1Fe2 catalysts; (e) elemental mapping of the spent Co1Fe2 catalyst.

carburization of iron species. Furthermore, the microstructure of the spent catalysts was observed by HRTEM (Fig. 5). For the spent Co0Fe catalyst,  $\text{Fe}_3\text{O}_4$  and  $\text{Fe}_5\text{C}_2$  were distributed on the alumina matrix with fringe spacings of 0.250 and 0.205 nm (Fig. 5b), respectively, which matched well with the (311) and (510) lattice planes of  $\text{Fe}_3\text{O}_4$  and  $\text{Fe}_5\text{C}_2$ , respectively. In the spent Co1Fe2 catalyst, the presence of alumina and metal carbide nanoparticles was evident. Concurrently, the  $d$ -spacing values of the lattice planes of the HRTEM images revealed the formation of the  $\chi\text{-(Co}_x\text{Fe}_{1-x})_2\text{C}_2$  phase with a lattice spacing of 0.202 nm (Fig. 5d). Furthermore, the images with EDS elemental mapping revealed the surface spatial distribution of Fe, Co, and Al elements (Fig. 5e). After the reaction, the distribution of Fe and Co elements was found to be uniform in the same position, confirming that Co penetrated into the  $\text{Fe}_5\text{C}_2$  lattice to form Co-Fe alloy carbides. Concurrently, the crystallized carbides were observed to be surrounded by alumina, suggesting that a structure comprising Co-Fe carbides as the primary phase and alumina support was formed in the spent Co1Fe2 catalyst. Therefore, the addition of Co played a significant role in the structural evolution of iron species during the reduction and reaction of the catalyst. The strong ability of Co to decompose CO and  $\text{H}_2$  led to the promotion of the reduction and carburization of iron species, which in turn generated more active sites for catalytic  $\text{CO}_2$  hydrogenation reactions and promoted the production of light olefins.

### Structure–activity relationship

The traditional concept is that the conversion of  $\text{CO}_2$  to hydrocarbons requires two process pathways: the conversion of  $\text{CO}_2$  to

CO is initiated by the RWGS reaction, followed by the hydrogenation of CO to hydrocarbons, which is a characteristic step of the Fischer–Tropsch process. This pathway requires Fe-based catalysts with bifunctional active sites, including iron oxide sites for RWGS and possibly iron carbide sites that promote C–C coupling to form hydrocarbons. In order to obtain accurate and detailed information about the composition of the iron-containing phase of the spent catalysts after 8 h of  $\text{CO}_2$  hydrogenation,  $^{57}\text{Fe}$  Mössbauer spectra were recorded (Fig. 6). For the spent Co0Fe catalyst, the raw spectra were deconvoluted into one doublet and five sextet subspectra. The sextets with hyperfine field (Hhf) of 187, 217, and 104 kOe were attributed to the typical iron carbide (A, B, and C) phases.<sup>39,40</sup> The presence of sextets with hyperfine fields of 469 and 455 kOe, corresponding to  $\text{Fe}_3\text{O}_4$  components (A and B), was also identified, along with double peaks  $\text{IS} = 0.24 \text{ mm s}^{-1}$  and  $\text{QS} = 1.11 \text{ mm s}^{-1}$ , corresponding to  $\text{Fe}^{3+}$ .<sup>41</sup> This finding confirmed the *in situ* phase restructuring from metal to oxides and carbides as the actual active species during  $\text{CO}_2$  hydrogenation reactions. The detailed Mössbauer parameters exhibited in Table 2 demonstrated the presence of the primary iron phases in the spent Co0Fe1 and Co1Fe2. It was also noteworthy that the Hhf value of iron carbide changed following the addition of cobalt, particularly the Hhf value of iron carbide (III), which underwent a substantial reduction from 104 kOe (Co0Fe) to 93 kOe (Co1Fe2). This deviation indicated that the disorder in the local Fe–Co environment within the particles, proving the formation of mixed iron–cobalt carbides.<sup>20,26</sup>

Despite its high  $\text{Fe}_3\text{O}_4$  content (Table 2), Co0Fe exhibited a low  $\text{CO}_2$  conversion of 36.8%. This suggested that only RWGS reaction could not limit the kinetics of  $\text{CO}_2$  hydrogenation





Fig. 6  $^{57}\text{Fe}$  Mössbauer spectra of the spent (a) Co0Fe and (b) Co1Fe2 catalysts.

Table 2 Detailed Mössbauer parameters of the spent Co0Fe and Co1Fe2 catalysts

Catalysts	Assignment	IS ( $\text{mm s}^{-1}$ )	QS ( $\text{mm s}^{-1}$ )	Hhf (kOe)	Area (%)	
Co0Fe	$\chi\text{-Fe}_5\text{C}_2$ (A)	0.04	0.03	187	11.5	36.0
	$\chi\text{-Fe}_5\text{C}_2$ (B)	0.12	0.04	217	11.5	
	$\chi\text{-Fe}_5\text{C}_2$ (C)	0.29	0.05	104	13.0	
	$\text{Fe}_3\text{O}_4$ (A)	0.08	0.00	469	32.0	59.1
	$\text{Fe}_3\text{O}_4$ (B)	0.56	0.10	455	27.1	
	$\text{Fe}^{3+}$	0.21	1.00	—	4.8	
Co1Fe2	$\chi\text{-(Co}_x\text{Fe}_{1-x})_5\text{C}_2$ (A)	0.09	0.08	192	17.8	68.8
	$\chi\text{-(Co}_x\text{Fe}_{1-x})_5\text{C}_2$ (B)	0.12	0.07	218	23.6	
	$\chi\text{-(Co}_x\text{Fe}_{1-x})_5\text{C}_2$ (C)	0.28	0.08	93	27.4	
	$\text{Fe}_3\text{O}_4$ (A)	0.03	0.15	462	10.4	16.9
	$\text{Fe}_3\text{O}_4$ (B)	0.69	0.04	455	6.5	
	$\text{Fe}^{3+}$ (spm)	0.20	0.86	—	14.2	

reactions. For the second stage Fischer–Tropsch reaction, the CO-TPD results (Fig. S5†) demonstrated that the desorption peak shifted to lower temperatures following the addition of cobalt, indicating that the binding force between CO and the catalyst surface diminished. An increase in the desorption peak area was also observed, which was conducive to the rapid transfer and conversion of CO under reaction conditions. In addition, in order to determine the co-adsorption and reaction of CO and  $\text{H}_2$  on the catalyst surface, the adsorption energy of  $\text{H}_2$  on the carbide surface was calculated. As shown in Fig. S6 and S7,† the optimal configuration for the carbide surface to

adsorb  $\text{H}_2$  after CO pre-adsorbed was determined. In this structure, the total adsorption energy of  $\text{H}_2$  on the  $(\text{Co}_x\text{Fe}_{1-x})_5\text{C}_2$  surface was  $-0.02$  eV (Fig. S8†), which was lower than that on the  $\text{Fe}_5\text{C}_2$  surface of  $0.17$  eV (the positive adsorption energy could be attributed to the energy consumption required for surface reconstruction), suggesting that the surface H atoms were more likely to aggregate on the  $(\text{Co}_x\text{Fe}_{1-x})_5\text{C}_2$  surface. This finding was consistent with the results of  $\text{H}_2$ -TPD (Fig. 7a), which indicated a substantial enhancement in  $\text{H}_2$  adsorption following the incorporation of Co. This might be attributed to the pronounced  $\text{H}_2$  dissociation capacity exhibited by cobalt





Fig. 7 (a) H<sub>2</sub>-TPD and (b) CO<sub>2</sub>-TPD profiles of the prepared catalysts.

species. The lower C/H ratio on the surface of the Co<sub>1</sub>Fe<sub>2</sub> catalyst was more conducive to the hydrogenation of CO. This process had been found to accelerate the transfer and conversion of reaction intermediates, thereby reinforcing cascade reactions between the RWGS reaction and FTS. Therefore, the Co<sub>1</sub>Fe<sub>2</sub> catalyst exhibited higher activity for CO<sub>2</sub> hydrogenation reactions. Furthermore, the H coverage on the catalyst surface might affect the formation of products. C<sub>3</sub>H<sub>6</sub>-TPD was performed using the spent Co<sub>0</sub>Fe and Co<sub>1</sub>Fe<sub>2</sub> catalyst, and the results were shown in Fig. S9.† It was evident that the desorption peak position of C<sub>3</sub>H<sub>6</sub> on the Co<sub>1</sub>Fe<sub>2</sub> catalyst was at lower temperatures, and the peak area was larger. This indicated that light olefin products were more easily desorbed and generated on the Co<sub>1</sub>Fe<sub>2</sub> catalyst without further secondary hydrogenation and coupling reactions. Furthermore, the H<sub>2</sub>/CO<sub>2</sub> ratio of 2.5 in the feed gas was slightly lower than the commonly reported ratio of 3. This lower H<sub>2</sub> partial pressure contributed to the suppression of the secondary hydrogenation of the primary olefin products, thereby enhancing the light olefin selectivity and improving the STY.

### Reaction pathway

*In situ* DRIFTS experiments were conducted on Co<sub>0</sub>Fe and Co<sub>1</sub>Fe<sub>2</sub> catalysts with the objective of elucidating the reaction

intermediates and reaction mechanism (Fig. 8). Following the switching of the reaction gas at 320 °C for 10 min, signals attributable to carbonate (1440 cm<sup>-1</sup>) and bicarbonate (1349 and 1647 cm<sup>-1</sup>) species were observed on Co<sub>1</sub>Fe<sub>2</sub> (Fig. 8b). This was attributed to the adsorption and interaction of CO<sub>2</sub> and H<sub>2</sub> on the catalyst surface. The bands at 1539 and 1774 cm<sup>-1</sup> were attributed to the formate species, which were considered as the important intermediates for the formation of CO. In contrast, these intermediates were not detected until 30 min on Co<sub>0</sub>Fe (Fig. 8a). This finding was verified by the results of CO<sub>2</sub>-TPD (Fig. 7b). With the increase in cobalt doping, a shift in the CO<sub>2</sub> desorption peaks towards higher temperatures was observed, accompanied by an enhancement in CO<sub>2</sub> uptake. This indicated a heightened propensity for CO<sub>2</sub> adsorption, consistent with the augmented initial reaction activity observed in the Co<sub>1</sub>Fe<sub>2</sub> catalyst. Moreover, the signal associated with chemically adsorbed CO\* on the Co<sub>1</sub>Fe<sub>2</sub> catalyst became stronger and remained relatively stable (Fig. 8d), thereby confirming the hypothesis that cobalt doping increased the reaction activity and promoted the cascade reaction. The saturated C–H bond signal at 3014 cm<sup>-1</sup> on the Co<sub>1</sub>Fe<sub>2</sub> catalyst was discovered earlier and with higher intensity. This finding was consistent with the result that after adding cobalt, the selectivity of low-carbon alkanes increased significantly from 14.6% for Co<sub>0</sub>Fe



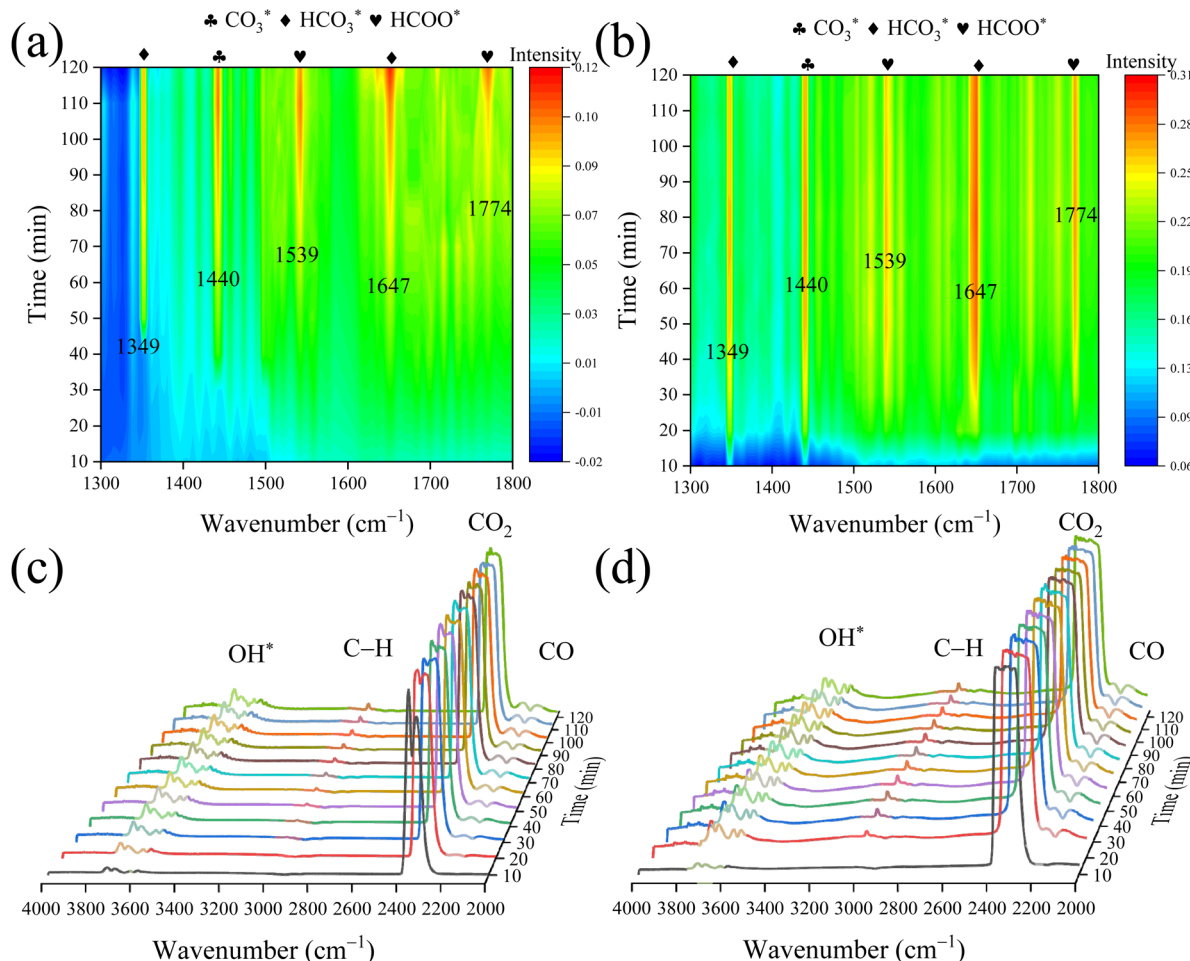


Fig. 8 The *in situ* DRIFT spectra of the spent (a and c) Co<sub>0</sub>Fe and (b and d) Co<sub>1</sub>Fe<sub>2</sub> catalysts.

to 24.6% for Co<sub>1</sub>Fe<sub>2</sub>. Furthermore, it had been demonstrated that the addition of cobalt served to regulate the production of low-carbon products.

## Conclusions

This work systematically studied the role of cobalt in the structural evolution and surface property regulation of Co-Fe bimetallic catalysts for CO<sub>2</sub> hydrogenation to light olefins, and disclosed their structure-activity relationship. The results of *in situ* XRD demonstrated that the iron species in the Co-Fe catalyst was more readily reduced to alloys and further carburized into mixed metal carbides during the reduction and reaction process. The cascade reaction of RWGS and FTS was reinforced by the rapid adsorption and conversion of CO intermediates, thereby facilitating the conversion of CO<sub>2</sub>. Furthermore, the enhanced H coverage after Co doping helped regulate the C/H ratio on the catalyst surface, promoting the production and desorption of primary light olefins products. Consequently, the Co<sub>1</sub>Fe<sub>2</sub> catalyst, with a Co/Fe molar ratio of 1/2, displayed remarkable performance in the CO<sub>2</sub> hydrogenation to light olefins reaction, exhibiting a CO<sub>2</sub> conversion of up to 51.9% at 320 °C and a STY of C<sub>2-4</sub> of 315.1 g kg<sub>cat</sub><sup>-1</sup> h<sup>-1</sup>. This

work provides a reference for understanding the effects of cobalt on product regulation in CO<sub>2</sub> hydrogenation over Co-Fe catalysts.

## Data availability

The data supporting this article have been included as part of the ESI.†

## Author contributions

Z. Liu and W. Song: writing-original draft, data curation, methodology. P. Zhang: supervision, validation. J. Liang: writing-review & editing, validation. C. Wang, C. Liu, H. Song, and B. Chen: supervision, validation. K. Wang: writing-review & editing, validation. G. Liu, X. Guo, Y. He, X. Gao, J. Zhang, and G. Yang: conceptualization, validation, supervision. N. Tsubaki: funding acquisition, writing-review & editing, validation, supervision.

## Conflicts of interest

There are no conflicts to declare.



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