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Towards non-contact pollution monitoring in sewers with hyperspectral imaging†

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Monitoring water quality in sewers is challenging, particularly because state-of-the-art technologies require contact with the raw wastewater. The presence of fat, oil, grease, and solids makes automated grab sampling difficult and causes sensor fouling. To overcome these limitations, non-contact methods based on light reflectance, such as hyperspectral imaging (HSI), are gaining attention. However, HSI has never been tested for raw wastewater. To assess its accuracy for measuring pollution, we developed a laboratory setup and performed targeted experiments with a combination of raw and diluted wastewater, as well as synthetic turbidity stock solutions. We measured seven pollution variables: chemical oxygen demand, turbidity, dissolved organic compounds, ammonium, total nitrogen, phosphate, and sulphates. We used automated pixel selection and partial least squares regression to retrieve pollution information from the hyperspectral images. Our results, based on 144 samples, suggest that HSI can estimate pollution levels with a precision in the range of state-of-the-art absorbance spectrophotometric methods. Additionally, we found that the combination of pixel and wavelength selection, enabled by the hyperspectral data structure, significantly influences the performance of partial least square modelling. Overall, our findings indicate that HSI is a promising technology for non-contact monitoring of water quality in raw wastewater.

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Water impact

Non-contact wastewater quality monitoring can revolutionize urban water management. It avoids sensor fouling and corrupted measurements by eliminating physical contact with aggressive wastewater. Hyperspectral monitoring provides near-real-time water quality data with minimal maintenance, enabling cost-effective analyses in sewers and remote areas. Though correlation-based, it empowers researchers, policymakers, and communities to protect water resources, make informed decisions, and foster environmental sustainability.

1 Introduction

Emissions from urban drainage systems (UDS) cause significant environmental pollution, including the release of particles, microplastics, and nutrients.¹ However, there is a lack of knowledge about the occurrence and dynamics of pollutants in UDS, partly because continuous monitoring of raw wastewater is extremely challenging.² Sensors and sampling equipment that are in contact with wastewater are difficult to manage and maintain due to exposure to grease, fat, solids, *etc.*³ Non-contact water quality monitoring

techniques have the potential to address these challenges, but research on this topic is still limited to seven peer-reviewed publications.^{4–10}

In a pioneering study, Russell *et al.*, 2003 measured the light reflection intensity of an 880 nm laser on 200 wastewater samples in the laboratory.⁵ They obtained promising results for the estimation of oxygen demand (COD) ($R^2 = 0.79$) and suspended solids ($R^2 = 0.83$), but the subsequent field trials were unsatisfactory. We believe that either the use of a laser as a light source was too restricting for pollution measurement, or that external disturbances, such as direct reflection from surface waves or ripples of the moving water, were not adequately filtered out.

More than 10 years later, Agustsson *et al.*, 2014 improved upon the limitations of Russell's single-wavelength setup by using a Xenon light source and a spectrophotometer (200–1100 nm).⁷ They estimated COD ($R^2 = 0.85$) and turbidity ($R^2 = 0.96$) with slightly better accuracy using a partial least squares (PLS) approach. However, they only used synthetic

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wastewater, which limits the generalizability of their results. Additionally, the use of a spectrophotometer in real world applications might be challenging due to its limited field of view.¹¹

Fortunately, these limitations can now be overcome with the use of hyperspectral imaging (HSI) technologies. Unlike a spectrophotometer, which measures a single absorbance spectrum representing the total light intensity in the ultraviolet (UV) to near infrared (NIR) range from a surface of interest, a hyperspectral imaging (HSI) system can capture a picture with a spectrum on each pixel. This enables the use of advanced object classification, machine learning, and image analysis techniques on the resulting 3D data-cube structure.¹² Recently, HSI has been used to monitor highly polluted industrial wastewater, with promising results.¹⁰

To the best of our knowledge, the application of HSI for monitoring the pollution of untreated municipal wastewater has not been explored. In this proof-of-concept study, we aim to assess its potential for high-frequency, precise, and non-contact monitoring of raw urban sewerage. Therefore, we developed a laboratory setup to acquire hyperspectral images of mixtures of real wastewater samples and a synthetic turbidity standard. Our results demonstrate that the use of HSI for pollution monitoring is promising, even if the method is correlation-based. This paper finally discusses the potential for improvements and outstanding questions regarding real-world applications.

2 Material and methods

In this study, hyperspectral images of 144 different mixtures of untreated municipal wastewater with known pollution concentrations were acquired. Data-driven models were trained and validated to retrieve pollution estimations from the hyperspectral data.

2.1 Experimental setup for hyperspectral data acquisition

Hyperspectral imaging system. The MV.X hyperspectral imaging system from Headwall Photonics was used to perform the measurements (MV.X, Headwall Photonics, Bolton, U.S.). This is a push-broom camera using a line scan to measure hyperspectral data-cubes. Unlike snapshot cameras, which capture a data-cube in a single snap, push-broom cameras are designed to monitor moving material with a high spectral resolution.¹³

The MV.X hyperspectral imaging system is water-resistant (rated IP66 and IP67), therefore suitable to remotely measure the reflectance of wastewater. It measures 300 spectral bands with a 2 nm spectral resolution in the visible and near infrared (VNIR) range between 400 nm and 1000 nm across a line of 1020 spatial pixels. The temporal resolution ranges from milliseconds to seconds, depending on the lighting conditions and the reflection properties of the object being measured. Additionally, the MV.X is equipped with an embedded processor for fast data processing, allowing for continuous spectral analysis in near-real time.

Image acquisition setup. The laboratory setup for the hyperspectral acquisitions was inspired by previous works.^{7,10,14} A volume of 200 mL of each sample was placed in a 7.8 cm diameter high-density polyethylene cup. A black cup was used to minimize the reflection from the bottom and walls of the cup. The measurements were performed in a dark room to eliminate external light interferences. A 50 W Philips halogen light was used to illuminate the sample since it covers the VNIR spectral range. The exposure time of the MV.X was set to 200 ms to collect enough light. The camera was placed above the sample at a height of 35 cm, while the light was positioned at a height of 30 cm with an angle of 16°, to maximize the lighting of the area of interest and minimize direct reflection from surface ripples. In this configuration, the scanned line of the imager was centered on the middle of the cup and covered approximately 10 cm. The wastewater was mixed with a magnetic stirrer so that, firstly, the capture area in front of the scanning line of the camera rotates, and secondly, to avoid the settling of suspended solids. Details of the setup are presented in the ESI† (SI A).

Collection of black and white references for the optical calibration of the camera. Before performing the sample HSI measurement, it was necessary to collect a black and a white optical reference. While the black reference accounts for the camera noise, the white reference compensates for the setup-specific lighting conditions. We used a Zenith Lite™/Greyscale Coating Ultralight Target with 95% reflectance because we found that it ensured better calibration than a normally used white target due to its closer colour similarity with the samples studied. For these experiments, the lighting conditions were constant, so the white reference was only measured once at the beginning.

2.2 Description of the hyperspectral data-cube structure

Each hyperspectral data-cube is composed of a series of 10 cm wide lines. Each line is measured as a series of 1020 pixels, and each pixel contains a reflectance spectrum corresponding to 300 wavelength bands. The camera takes a measurement of each line every 200 ms for a duration of 10 s, resulting in 51 lines for a single water sample.

A pseudo red-blue-green (RGB) visualization of a data-cube is shown in Fig. 1, with different pixels represented by their spectra. The area of interest, corresponding to the wastewater surface, is represented by the dark pixels. The areas at the border of the cup and in the middle of the cup (due to the magnetic stirrer) have very different spectral signatures and can be easily removed during pre-processing.

2.3 Wastewater sample collection, mixture preparation, and image acquisition

For this first laboratory proof-of-concept experiment, we acquired hyperspectral data-cubes of 144 samples obtained from mixtures of real wastewater from a trunk sewer at Eawag (Dübendorf, Switzerland), synthetic wastewater, and tap water.

For the purpose of conducting a first study on the use of HSI for pollution measurement, we consider this dataset





Fig. 1 Top: typical data-cubes (normalized) with pseudo-RGB colouring corresponding to 380 nm, 500 nm, and 900 nm. One line consists of 1020 pixels, which have a spatial resolution of about 0.1 mm. The image consists of 51 lines collected in 10 seconds. Each image's pixel contains a spectrum ranging from 400 to 1000 nm. Bottom: the spectral dimension is visualized to show the differences between various image areas.

sufficient. The mixture generation protocol, despite imposing limitations on the interpretability of the results (discussed in 3.5), made it possible to generate a wide variety of different samples while limiting the amount of laboratory reference measurement.

Wastewater mixture preparation and image collection. We collected 8 raw wastewater samples at different times over two days (26/07/22 – 10:00, 11:30, 13:00, 14:30, 16:00, 17:30; 27/07/22 – 6:00, 7:30 CEST) to capture the daily changes in wastewater composition. The sample volume was 1 L to have sufficient water for mixture generation and reference measurements. To generate more mixtures from those 8 samples, we combined them together and with formazine, a turbidity calibration standard of 4000 NTU (Sigma Aldrich), as done by Agustsson *et al.*, 2014.⁷ Formazine is an organic nitrogenous compound ($C_{17}H_{13}N_5O_3$), and therefore not only increases turbidity, but also COD, dissolved organic carbon (DOC) and total dissolved nitrogen (TDN), making it possible to create more variability in the sample composition, while remaining within in sewer-pollution ranges.

The mixing procedure followed four steps, with hyperspectral data being collected after each one (Fig. 2). The

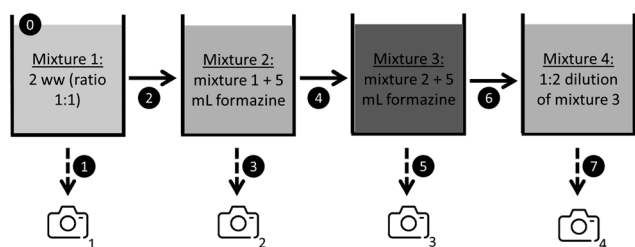


Fig. 2 Schematic overview of the 7 steps necessary for the generation of 4 different mixtures and the capture of 4 data-cubes, starting with a 1:1 mixture of 2 wastewater samples (step 0).

first step consisted of mixing two 100 mL samples from the eight raw wastewaters samples. The second and third step consisted of adding 5 mL of formazine, increasing the turbidity with steps of 96.6NTU and 95.2NTU. Finally, the third mixtures were diluted twice with tap water. Starting with 8 raw wastewater samples, a maximum of 36 combinations were obtained after the first mixing step. Therefore, 144 (36×4) different data-cubes could be captured following this procedure.

Reference water quality variables measurements. We measured seven water quality variables for each of the eight raw wastewater samples: COD, turbidity, DOC, TDN, phosphate (PO_4-P), sulphates (SO_4-S) and ammonium (NH_4-N). As 800 mL of raw wastewater from the collected volume (1 L in total) was necessary for mixture generation, the remaining 200 mL were used for laboratory analysis. Except for turbidity measurements, Chromafil GF/PET 0.45 μm filtration was used to condition the samples. Table 1 summarizes the measurement method, instrumentation, and accuracy for each water quality variable from the manufacturer's data for the specific measurement range.

Collecting the 144 data-cubes lasted about 9 hours. In our experience, the organic pollution of the wastewater used in this study degrades at a rate of about 10% each day due to biological activity. To account for this, reference pollution measurements were performed before (08:00) and after (17:00) full data acquisition, and the average of both measurements was used as ground truth. Because of the known mixing proportions for the 144 mixtures, we were able to calculate their pollution. An overview of the pollution characteristics of the mixtures is presented in SI B.†

2.4 Chemometric modelling of wastewater pollution

To retrieve wastewater pollution from the hyperspectral data-cubes, a two-step procedure was developed and applied (Fig. 3).



Table 1 Information on the laboratory measurement methods used to determine the reference concentrations of wastewater pollution in the 144 mixtures

Water quality variable	Measurement method	Instrument	Accuracy
COD	Cuvette test	Hach LCK-314	3 mg L ⁻¹
PO ₄ -P, SO ₄ -S	Ion-chromatography: DIN EN ISO 10304-1, 2009	Metrohm 930 Compact IC Flex	<0.1 mg L ⁻¹
NH ₄ -N	Flow injection analysis: standard method 4500-NH ₃ , EPA 600/4-79-020, 1983	Lachat QC8500	0.2 mg L ⁻¹
Turbidity	Turbidimeter: DIN EN ISO 7027-1, 2016	Hach TL2300	2%
DOC	TOC analyzer: DIN EN ISO 20236, 2023	Shimadzu TOC-L CSH	0.5 mg L ⁻¹
TDN	TOC analyzer: DIN EN ISO 20236, 2023	Shimadzu TOC-L CSH	0.4 mg L ⁻¹

2.4.1 Step 1: data-cubes pre-processing and spectra extraction. In the first step, we extracted a single spectrum from each data-cube to represent the wastewater surface. This dimensionality reduction was necessary to apply PLS modelling. The spectra extraction was done in five sub-steps, inspired by previous work.^{15,16} All the mathematical equations used for this section, as well as a visualization of the data-cube transformation, are provided in SI C.†

Substep 1.1 – conversion to reflectance. The raw images were converted by subtracting the camera noise (dark reference) and dividing by the reflection of the calibration target (white reference).

Substep 1.2 – data-cube re-framing. The data-cubes were cropped (i) to remove border wavelengths showing high noise (400–418 nm and 982–1000 nm), (ii) to remove some sample lines (lines 46 and above) in order to ensure that all the data-cubes have the same dimension, and (iii) to remove pixels that do not represent the water surface (pixels 1 to 110 and 861 to 1020).

Substep 1.3. – pixel selection. A threshold method was used to filter out the outlier pixels not corresponding to the wastewater surface (as highlighted in Fig. 1). Specifically, we created and applied a 2D mask that excludes the lowest and highest 20% of the light reflection intensity values.

Substep 1.4. – extraction of the mean reflectance spectra. The remaining 60% of the pixels were used to calculate the mean and standard deviation of the wastewater reflectance for every wavelength. For all samples and all wavelengths, the obtained standard deviation was below 10% of the mean value, which was a satisfactory criteria to consider this method as reliable. The mean values obtained at every wavelength for a single sample were considered as a spectrum representative of the wastewater surface.

Substep 1.5. – spectra pre-processing. Each spectrum was further processed by applying (i) a Savitzky–Golay filter with a window size of 17 and a polynomial order of 2,¹⁷ and (ii) a logarithmic transformation. This pre-processing was found to be leading to optimal PLS model performance in step 2.

2.4.2 Step 2: partial least squares parameter optimization and model evaluation. In a preliminary series of tests, we tried regression approaches such as linear regression, support vector regression, PLS, and random forest regression. We concluded that PLS is the most promising, being a simple and well-established approach for dealing with high dimensional data in the field of wastewater spectrophotometry.¹⁸ In this work, we optimized two types of PLS model parameters for each of the seven pollution variables. First, the number of latent variables – the number of components to which the input features are decomposed – was investigated between 1 and 20. Second, the number of wavelengths used as model input was optimized to assure linearity of the response variable to the variable of interest,¹⁹ and to avoid overfitting, which is frequent with spectra containing hundreds of highly correlated frequencies.²⁰ We used the iterative stepwise elimination (ISE-PLS) method described by Wang *et al.*, 2017,²¹ which is based on the one-by-one removal of the wavelength with the lowest regression coefficient weight. We applied cross validation to estimate the predictive performance. The mathematical formulas are presented in SI D.†

Substep 2.1 – classification of the wavelengths. To perform the ISE-PLS, it was first necessary to classify the wavelengths, *i.e.*, the model features, by absolute regression coefficient. For each number of latent variables and each pollution variable, a PLS model was fitted with all the wavelengths to retrieve the wavelength classification. This approach was applicable without input normalization, as the features were already normalized in step 1.1.

**Fig. 3** Overview of the processing steps to retrieve wastewater pollution from the data-cubes.

Substep 2.2 – optimization of the PLS. The optimization was performed by calculating the performance of each PLS model based on a combination of latent variable number and of discarded wavelength number from the wavelength classification obtained in the previous step. The PLS model performance was measured with the root mean squared error (RMSE) between the reference pollution values and the predictions obtained with leave-one-out cross-validation (LOOCV).

Substep 2.3 – detailed optimal model evaluation. Once the optimal combination was found, we calculated not only the RMSE of the model but additionally the determination coefficient R^2 and the relative RMSE to better compare different model performance indicators. The relative RMSE is useful to compare the performance of each model. Table 2 shows previously defined scale rate model performances in the field of wastewater UV-vis spectrophotometry.²²

2.5 Numerical experiment to quantify the impact of pixel and wavelength selection on the partial least squares model quality

Due to the multi-dimensionality of the hyperspectral data-cubes, the modelling methods described above rely on (i) a pixel selection for the extraction of a wastewater representative spectrum from the hyperspectral acquisition (Substep 1.3) and (ii) a wavelength selection to select wavelengths that carry relevant information for a given pollution variable (Substeps 2.1 and 2.2). To quantify their respective impacts, we conducted three additional numerical experiments:

1. A PLS model was optimized without pixel selection and without wavelength selection.
2. A PLS model was optimized without pixel selection but with wavelength selection.
3. A PLS model was optimized with pixel selection but without wavelength selection.

A comparison between these three models' performances and the result of the previous section was conducted in terms of RMSE for each pollution variable.

3 Results and discussion

3.1 Exploratory analysis of raw reflectance spectra and the effect of turbidity

Fig. 4 (left) shows the 144 raw reflectance spectra extracted from the data-cubes. All spectra have a similar shape, with moderate peaks or bumps at specific wavelengths, such as

Table 2 Performance rating depending on the relative RMSE, as defined by Brito et al., 2014 (ref. 22)

RMSE _{relative}	Performance rating
<5%	Very good
5–10%	Good
10–20%	Satisfactory
>20%	Unsatisfactory

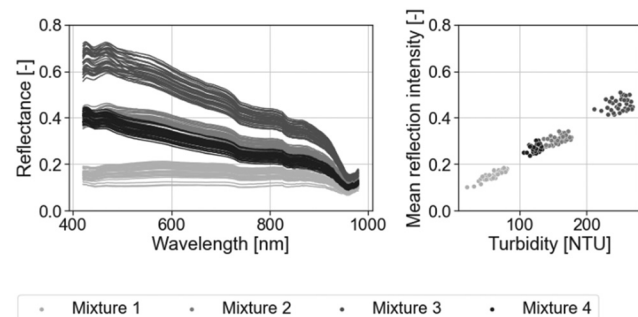


Fig. 4 Left: overview of the 144 raw wastewater reflectance spectra extracted from the hyperspectral data-cubes (after step 1.4, see Fig. 3). Right: linear relationship between turbidity and mean reflectance intensity.

around 470 nm, 770 nm, and 820 nm. Each of the four mixture types, as defined in Fig. 2, has a distinct spectral signature, which indicates that the use of formazine influences the spectral shape by increasing the light reflection more for shorter wavelengths.

Turbidity is linearly ($R^2 = 0.96$, see SI E†) related to the mean reflection intensity of each spectrum, as highlighted in Fig. 4 (right). This linear relationship is only true for turbidity, which is expected because the number of suspended particles determines how much light is reflected. Interestingly, the variance of the reflection intensity also increases with turbidity concentration, indicating that specific methods such as weighted regression models might even provide better estimation than the linear model.²³ We will discuss the practical implications of this relationship between turbidity and light reflection in section 3.3.1.

3.2 Overview of the model's performance and parameters for water quality prediction

The water quality predictions of the PLS model are presented in Fig. 5. For all water quality variables except $\text{SO}_4\text{-S}$, the prediction and laboratory values match each other well ($R^2 > 0.9$).

The model's performances and parameters are summarized in Table 3. The optimal number of latent variables is between 12 and 20 (the maximum tested values). This is consistent with the experimental design, as at least 10 latent variables were needed to explain the variability of the mixtures (see 2.3). Sample degradation may also have contributed to increased sample variability. In addition, by using wavelength selection (Steps 2.1 and 2.2), the 280 initial wavelengths could be reduced to 21–44%. Nevertheless, 82% of wavelengths are still used in at least one of the models. An overview of the selected wavelengths for each variable is shown in Fig. 6. The wavelength in the visible range (400–750 nm) plays a predominant role for every variable except COD, where wavelengths above 650 nm are more important.

The overall good performance of the modelling approach is reflected in the low RMSE. All the pollution variables are



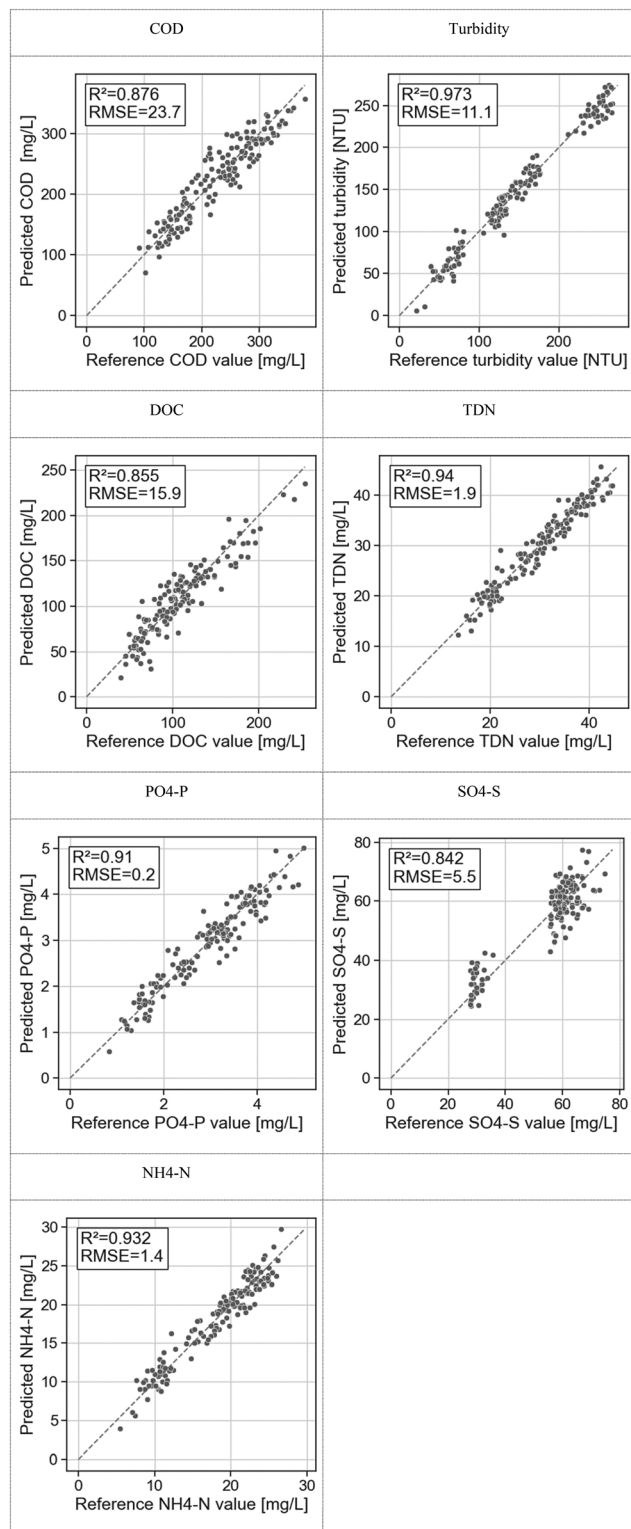


Fig. 5 Overview of the PLS regression LOOCV results for each pollution variable. A high R^2 value (close to 1) and a low RMSE, arguably, describe a good predictive performance of the PLS model.

estimated with a relative RMSE of about 10%, which is considered good to satisfactory in wastewater spectrophotometry (Table 2). A similar study with a UV-vis

probe in sewers obtained similar results for COD, ammonium, sulphate and phosphate.²⁴ Even if turbidity, DOC, and TDN were not included in this other study, our results suggest that HSI performance in this specific monitoring setup is comparable to that of immersed spectrophotometric probes to measure pollutant concentrations.

3.3 Discussion of the results for each pollution variable

3.3.1 Turbidity is the most promising variable due to its direct link with light reflection intensity. Turbidity is linearly associated with light reflection intensity, as seen in Fig. 4b. Based on this linear relationship, turbidity may be estimated with an RMSE of 12.6 NTU (see SI E†), which is comparable to the best PLS model (11.0 NTU). This explains why the PLS model is not significantly improved by wavelength selection (13.9%) or pixel selection (5.4%).

Analysis of the selected wavelengths shows that wavelengths between 400 and 600 nm are the most important. This supports the results of other studies that found that the visible range is significant for turbidity measurement.^{25,26} Interestingly, accurate turbidity measurements were obtained from laboratory experiments using a standard RGB camera.^{27,28} Similarly, when we only use the three RGB wavelengths as input into a PLS model, we obtain good predictions for turbidity prediction (RMSE: 12.2 NTU; see SI E†). We plan to investigate this in future work since our results indicate that turbidity might be quantified well using a low-cost camera.

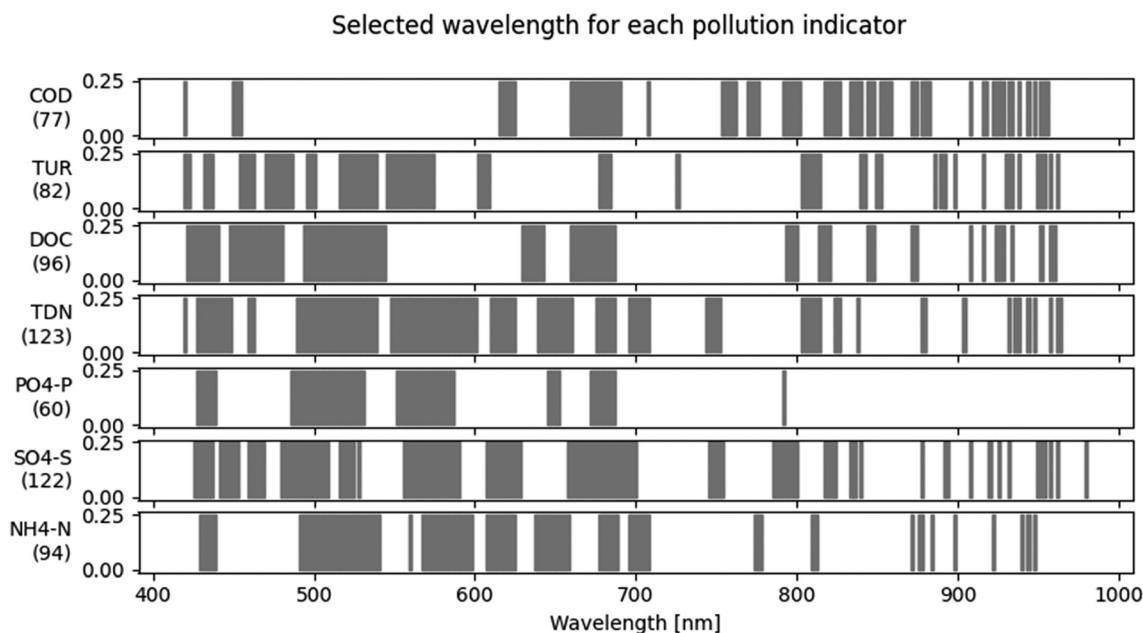
3.3.2 Total nitrogen and ammonium appear to have a specific influence on the reflectance. The high sensitivity of TDN and $\text{NH}_4\text{-N}$ to the selected wavelengths and pixels (45.6–48%, respectively) suggests that their estimation relies heavily on the specific extraction of information from the reflectance spectra. TDN is mainly composed of ammonium, but also includes other forms of nitrogen, such as nitrite, nitrate, and organically-bound nitrogen. Ammonium cannot be directly measured with UV-vis spectrophotometry,²⁵ and nitrite and nitrate were not detected in the wastewater samples (concentration below the detection limit of 0.4 mg L^{-1}). This may indicate that organically bound nitrogen has a strong influence on the reflectance spectra, and that the good estimation of $\text{NH}_4\text{-N}$ is at least partly due to its correlation with TDN ($\rho = 0.84$). This is also reinforced by the fact that similar wavelengths are selected for both ammonium and TDN.

The addition of formazine ($\text{C}_{17}\text{H}_{13}\text{N}_5\text{O}_3$) has an impact on the concentration of organically bound nitrogen, and therefore the mixtures with formazine have a different ammonium–TDN ration than typical wastewaters. This did not prevent the PLS model from estimating them accurately, which reinforces the possibility that specific and different features of the reflectance spectra are informative for the estimation of ammonium and TDN. When training a model with the 36 mixtures containing only raw wastewater (analysis presented in SI F†), both ammonium and total dissolved nitrogen are estimated with a precision below 3% ($R^2 = 0.97$), which implies that the use of formazine might even worsen



Table 3 Performance of the PLS model trained with the full dataset. The high R^2 , low RMSE, and comparably low MAPE suggest a good performance of non-contact wastewater quality monitoring

Water quality variable	Unit	Min	Max	Optimal number of latent variables	Optimal number of wave-lengths	R^2	RMSE	RMSE (relative)
COD	mg L ⁻¹	91.2	379.0	19	77	0.88	23.7	10.5%
Turbidity	NTU	21.6	267.3	18	82	0.97	11.1	7.6%
DOC	mg L ⁻¹	45.1	302.9	13	96	0.85	16.0	14.9%
TDN	mg L ⁻¹	13.5	44.6	17	123	0.94	1.9	6.6%
PO ₄ -P	mg L ⁻¹	0.8	5.0	12	60	0.91	0.2	9.8%
SO ₄ -S	mg L ⁻¹	27.8	74.7	18	122	0.84	5.5	10.4%
NH ₄ -N	mg L ⁻¹	5.4	26.6	20	94	0.93	1.4	7.9%

**Fig. 6** Number of selected wavelengths (left, in brackets), PLS weights (dots), and selected wavelengths (grey vertical lines) for each pollution variable. Some patterns are recognizable, but their interpretability is limited (see 3.6).

the accuracy of nitrogen compound estimation. Nevertheless, further analysis with more samples is necessary to investigate this.

3.3.3 Organic pollution, phosphate, sulphate, and discussion about the role of UV light. Organic compounds are known to absorb UV light but not VNIR light.²⁶ However, similar to other studies using VNIR reflectance spectra, the model could still estimate COD and DOC with satisfactory precision, likely resulting partly from their strong correlation with suspended solids ($\rho = 0.58$ and 0.7).^{8,10} Carreres-Prieto *et al.* (2020) brought supplementary evidence to this, showing that independently of the region of the visible spectra used for COD estimation, genetic algorithm models are performing well.²⁹ Similarly, we observe in Fig. 6 that COD and DOC model optimization selected very different wavelengths, which might indicate that the estimation of organic carbon is not based on specific areas of the spectra.

Despite a low RMSE, Fig. 5 shows that, contrary to the other variables, SO₄-S estimations are not reliable. Finally,

PO₄-P is estimated with a similar precision as NH₄-N and TDN. Phosphate and ammonium were initially very well correlated ($\rho = 0.95$). The selected wavelengths are also similar. However, a big difference is that the optimal PO₄-P model uses fewer latent variables¹² and wavelengths (60). We could not find any satisfactory explanation for those observations yet.

3.4 Result of the numerical experiment to quantify the benefit of hyperspectral imaging and discussion of further advantages

HSI makes non-contact measurement of a wide range of pollutants possible. The unique HSI data-structure allows for the selection of informative pixels within the field of view, combined with wavelength selection. The results of the numerical experiment to quantify their impact are presented in Table 4.



Table 4 Quantification of the improvement in the RMSE of the PLS model by applying pixel and wavelength selection. Using both methods substantially improves the accuracy, with up to a 46.4% decrease in the RMSE

Pixel selection	Wavelength selection		COD [mg L ⁻¹]	Turbidity [NTU]	DOC [mg L ⁻¹]	TDN [mg L ⁻¹]	PO ₄ -P [mg L ⁻¹]	SO ₄ -S [mg L ⁻¹]	NH ₄ -N [mg L ⁻¹]
No	No	RMSE	29.8	12.8	22.5	3.6	0.4	8.3	2.7
No	Yes	RMSE	27.1	11.0	19.9	3.1	0.4	7.2	2.3
		% of improvement ^a	8.9	13.9	11.4	14.8	10.8	12.7	17.4
Yes	No	RMSE	26.1	12.1	17.0	2.3	0.3	6.3	1.7
		% of improvement ^a	12.3	5.4	24.5	37.4	26.0	23.6	38.9
Yes	Yes	RMSE	23.8	11.1	16.0	2.0	0.3	5.6	1.4
		% of improvement ^a	20.2	13.1	29.0	45.6	34.9	32.9	48.0

^a Compared to the RMSE without optimization.

The improvements after wavelength selection (8.9–17.4%) are lower than those achieved by pixel selection (5.4–38.9%). As expected, combining both results in the largest improvement (13.1–48.0%, 32% on average). So, this numerical experiment highlights the advantage of HSI for pollution measurement over other measurement techniques with lower spectral and spatial resolution. We believe this to be crucial for UDS application as surface perturbations, including foam, ripples, or floating objects, are ubiquitous in sewer infrastructures and will cause a large number of anomalies.

In addition to the benefits of enabling contactless pollution measurement, HSI has a sampling dimension of several decimeters, which is on the same spatial scale as the grab samples collected as ground truth. Compared to state-of-the-art submerged spectrophotometers, which operate with an optical window of a few millimeters, we expect that the estimation of pollution is less sensitive to disturbances from wastewater variability and sampling artefacts, such as the position of the sensor in the sewer cross section.

Finally, another advantage of HSI is the potential to extract hydrodynamic information from the hyperspectral data-cubes. Current imaging technology can detect the water level in sewer videos,^{30,31} measure the water flow³² and detect fat layer accumulation.³³ To what extent hyperspectral information could improve this, *e.g.*, by better distinguishing pipe material from water surfaces or by facilitating superior particle-image-velocimetry, should be investigated in future studies.

3.5 Limitations of the experimental design to generalize the results

We identified two major limitations. First, despite collecting HSI data from 144 different mixtures, the pollution variability is low compared to real-world sewage because the mixtures are prepared with a smaller number of initial samples (*i.e.*, 8). This was motivated by the desire to create a simple experimental design to serve as a proof-of-concept for the use of HSI for pollution measurement. Another drawback of this

protocol is that the data collection lasted nine hours. During this time, organic compounds in the samples were slightly degraded, which probably changed the wastewater matrix. For future work, continuous cooling of the samples could help stabilize the wastewaters since the organic degradation rate increases with temperature.

Second, as highlighted in 3.1 and 3.3.2, the use of formazine has a significant impact on both the spectral reflectance and on the correlation between water quality variables. This limits the generalization of the PLS results and of the wavelength analysis for the real wastewater matrix. To draw conclusions on data without synthetic stock solutions, we tested the modelling approach with 36 of the 144 mixtures without formazine (see SI D†), and obtained similar results as with the 144 mixtures. This is encouraging, but the number of samples is too small to draw reliable conclusions.³⁶

Ultimately, investigating more samples of real wastewater, without synthetic mixtures, will produce more reliable results. We are now planning to collect data over an open channel for several months to critically evaluate the HSI performance in real-world conditions.

3.6 Potential improvement of the chemometric pollution modelling

We deliberately used standard approaches to retrieve pollution from observed spectra because we believe that the regression results are more influenced by the raw data quality than by the methodological approach to data-driven modelling. Nevertheless, for future studies, we identified two potential areas for improvement.

First, alternative approaches for wavelength selection can improve the interpretability of the results. Because PLS is based on a reduction of the spectral dimension in the direction of minimal covariance with the targeted pollution variables, PLS weights are not easy to interpret physically.³⁴ In the future, LASSO regression³⁵ seems particularly promising to analyse the more representative wavelengths since this model is designed to discard features of low



importance. Other potential methods, such as principal component analysis and the random frog algorithm for variable selection, might also be explored.²⁶

Second, a nested cross-validation procedure suited to the specific data-structure may improve the interpretability of the results. We used LOOCV to minimize the bias from the splitting of the data into a training and a testing set in the model performance estimation.³⁶ However, because each model is trained with all the spectra but one, this procedure can overestimate performance due to data leakage, *i.e.*, the transfer of information about the testing set into the training set. This is particularly relevant when considering that the 144 mixtures are not independent but obtained after mixing a smaller number of raw samples (see 2.3). A nested cross-validation based on the exclusion of all the mixtures containing a specific raw wastewater from the testing set can solve this concern.³⁷

3.7 Knowledge gaps to consider for future sewer application

It was not within the scope of this proof-of-concept study to quantify the influence of light position and light intensity. Stronger lighting could enable positioning the light at a lower angle, which could maximize the amount of diffuse light reflection containing spectral information about the sample composition. This could also reduce the acquisition time for the camera, allowing for a more precise pixel selection by increasing the line acquisition frequency.

In UDS, HSI calibration will require more consideration because measurement conditions are not as stable as in controlled laboratory environments. Nonetheless, HSI systems are already widely used for more challenging monitoring tasks, such as the mapping of vegetation in daylight. Therefore, such UDS-specific conditions can be compensated for by selecting specifically stable monitoring sites or by including other sensors, such as a light detector, to control the environment.

On a more general level, it is important to understand the influence of light and camera position relative to the wastewater surface in the HSI measurement because water level and flow vary in sewers. In the future, it may be valuable to develop process-based models that can quantify light reflection in very turbid and variable media, such as wastewater, to account for those UDS variations. Possible approaches could include adapting well-established models such as a sea reflection model,³⁸ the Kubelka–Munk theory,³⁹ or using Monte Carlo simulation.⁴⁰

Finally, other experimental challenges must be addressed before installing hyperspectral cameras and halogen light sources for routine measurements in UDS. For instance, humidity, aerosols, and a changing sewer atmosphere could cause systematic errors through altered light propagation properties. One possible solution to this problem is on-line calibration with multiple light sources or varying light intensities. Additionally, condensation or splashing water could cause fouling of the camera, so a cleaning system may be necessary.

4 Conclusions

In this study, we investigated a non-contact hyperspectral imager as a novel system to measure wastewater pollution. Based on the satisfactory experimental results and on theoretical as well as practical considerations, we draw the following conclusions:

- By combining pixel and wavelength selection with PLS regression, one can accurately estimate pollutant concentrations (relative RMSE below 10%) for four of seven water quality indicators of interest: turbidity, TDN, $\text{NH}_4\text{-N}$, and $\text{PO}_4\text{-P}$. Aggregate organic constituents (COD, DOC) were also predicted with a relative RMSE below 15%, which is considered satisfactory.
- The reported accuracies are best for turbidity (7.6%) and TDN (6.6%). We showed that turbidity is directly linked to light reflection intensity, independently of the wavelength. For TDN, we hypothesize that the measurement is made possible by the detection of organically bound nitrogen, but additional research is needed to confirm this.
- Using a hyperspectral imager has several advantages over other imaging techniques with lower spatial or spectral resolution. The water quality predictions were, on average, 32% more precise when using a pixel and a wavelength selection. Furthermore, the benefits of pixel selection might be even greater in real-world applications where many disturbances must be filtered out.
- Our results support historical findings that proposed non-contact imaging technologies based on reflectance spectrophotometry for raw wastewater monitoring in sewers. The hyperspectral imaging system (HSI) deployed in this work brings this promise closer to reality due to being able to circumvent the negative effects of disturbances in the water surface, such as foam, ripples, *etc.*

List of abbreviations

COD	Chemical oxygen demand
DOC	Dissolved organic carbon
HSI	Hyperspectral imaging
ISE-PLS	Iterative stepwise elimination – partial least squares
LOOCV	Leave-one-out cross validation
MAPE	Mean absolute percentage error
$\text{NH}_4\text{-N}$	Ammonium
NIR	Near infrared
NTU	Nephelometric turbidity unit
PLS	Partial least squares
$\text{PO}_4\text{-P}$	Phosphate
RMSE	Root mean square error
RGB	Red blue green
SI	Supplementary information
$\text{SO}_4\text{-S}$	Sulfate
TDN	Total dissolved nitrogen
UDS	Urban drainage system
UV	Ultraviolet
VNIR	Visible near infrared



Code and data availability

Custom Python scripts were developed for this research paper using the Spectral 0.23.1 and the Scikit-learn 1.2.0 Python modules. To make our research reproducible, the codes and the data are openly available here: <https://doi.org/10.25678/0007WY>.⁴¹

Author contributions

Conceptualization: PL, JR; experimental setup: PL, CF; data gathering: PL; data analysis and visualization: PL, KV; writing, review and editing: PL, JR, KV, CF; supervision: JR.

Conflicts of interest

There are no conflicts to declare.

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