

PAPER

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Exploring materials that simultaneously possess high conductivity and electrochemical stability is critical for various energy-conversion applications. In this study, our combined computations and experiments suggest the Mg–Ti–O chemical space for novel ternary oxide compounds offering high electrical conductivity and corrosion stability in acidic conditions to be potentially used as catalyst supporter of polymer electrolyte membrane fuel cells. High electrical conductivity ($6.09 \times 10^{-1} \text{ S cm}^{-1}$) is achieved at room temperature by tuning the chemical composition of $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$ while still maintaining good corrosion stability ($1.2 \times 10^{-4} \text{ mA cm}^{-2}$ after six days) in acidic conditions. Furthermore, we discover that a reducing gas environment during the synthesis increases the Ti solubility in $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$ with a reduced valence state of Ti, thus resulting in high conductivity.

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Introduction

There is often a trade-off between functionality and compatibility in materials, where a single material cannot simultaneously fulfill all the material properties required in applications. Electrical conductivity and electrochemical stability are needed in materials for nearly all clean-energy electrochemical technologies, including batteries, solar cells, fuel cells, water splitting, and CO_2 reduction.^{1–3} Good examples are protective coatings of battery current collectors, bipolar plate coatings in fuel cells, electrolyzers, and catalyst supporters.^{4–7} These properties are essential for increasing the energy efficiency and reliability and reducing maintenance costs. In particular, the electrical conductivity and electrochemical stability in an acidic environment are important for energy conversion in polymer electrolyte membrane fuel cells (PEMFCs).

Generally, transition-metal oxides offer better electrochemical stability in acidic environments at the expense of conductivity. Various metal oxides such as TiO_2 , WO_3 , RuO_2 , MoO_3 , SnO_2 , CeO_2 , and MnO_2 have been investigated as acid-stable compounds.^{8–10} Among the set of materials explored in the literature, TiO_2 has been found to be quite stable in acidic medium.^{11–13} However, its less conducting nature results in a low electronic conductivity, thereby contributing significantly to the ohmic overpotential in PEMFCs.^{14–16} According to a recent study from Kumar *et al.*,⁹ WO_3 nanorods exhibit good electrochemical stability for catalyst-support applications. Their stability in an acidic environment appears to be quite good, with a negligible relative decrease in the electrochemically active surface area after 10 000 cycles. However, its low electronic conductivity ($7.8 \times 10^{-5} \text{ S cm}^{-1}$) requires further improvement.

To develop a highly conductive and highly corrosion-resistant material, one typical strategy is the aliovalent substitution into acid-stable but less conductive materials to improve their electrical conductivity.¹⁰ Various binary metal oxides, including Nb-doped TiO_2 , Sn-doped In_2O_3 , and Sb-doped SnO_2 have been reported thus far.^{10,13,14,17} Recently, a high-throughput computational approach was used to search for appropriate alternatives among ~48 000 oxides in the Materials Project database.¹⁸ As a result of this effort, Wang *et al.* proposed 68 ternary and quaternary metal oxides after evaluating the aqueous stability of all candidates in strong acid and further ruling out the materials with a large energy bandgap (E_g), *i.e.*, low electrical conductivity. Ternary or quaternary oxide compounds are good systems to explore because the valence state of the transition-metal ions and electronic structure can be

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tuned, thereby improving the electrical conductivity while maintaining electrochemical stability in an acidic environment.

In this work, we conducted a combined computational and experimental study to investigate ternary oxide compounds that exhibit both high electrical conductivity and stability in an acidic environment. Our computational density functional theory (DFT) study proposed Mg–Ti–O chemical space as a promising candidate, and the chemical space is thoroughly investigated experimentally. Despite Mg–Ti–O compounds commonly being considered insulating materials,^{19,20} we achieved high electrical conductivity ($6.09 \times 10^{-1} \text{ S cm}^{-1}$) and good electrochemical stability in acidic environments by controlling the composition of $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$ (hereafter, MTO) and synthesis conditions.

Experimental details

DFT calculations

First-principles DFT calculations were performed using the Perdew–Burke–Ernzerhof (PBE) formulation of the generalized gradient approximation (GGA) with the projected augmented wave method, as implemented in the Vienna *Ab Initio* Simulation Package (VASP).^{21–25} To screen the various oxide materials, we used the GGA to consistently perform the binding energy comparison, rather than applying the U value (*i.e.*, material-dependent empirical parameters).²⁶ A plane-wave basis set cutoff energy of 520 eV and a minimum of 1000 k -points per reciprocal atom were used for the calculations. We used a vacuum thickness of at least $>12 \text{ \AA}$ to avoid the interactions between the top and bottom surfaces. For additional details regarding the computational details, please see the ESI.†

Material synthesis

The MTO materials used in the study were prepared using a solid-state method. First, we weighed and mixed precursor powders (MgCO_3 (Acros Organics, reagent grade), MgO (Sigma-Aldrich, 99.99%), TiO (Sigma-Aldrich, 99.9%), Ti_2O_3 (Sigma-Aldrich, 99.9%), and TiO_2 -anatase nanoparticle (Sigma-Aldrich, 99.7%)) to the appropriate stoichiometry. To prevent the hydration of MgCO_3 powder or any potential contamination of the mixtures, most of the preparation procedures were conducted in an Ar-filled glove box. The mixture was then pelletized and sintered at 1100–1500 °C for 5 h under various gas environments of H_2 (2%)/Ar (98%) mixed gas, Ar gas (99.999%), and ambient air.

Microstructural and chemical analyses

The crystal structure of each sample was analyzed using X-ray diffraction (XRD; Rigaku Miniflex 600) with Cu $K\alpha$ radiation, and the structural parameters were determined using the Rietveld method and Profex software.²⁷ For the XRD analysis, the as-synthesized MTO pellets were ground well using a mortar and pestle. High-angle annular dark-field scanning transmission electron microscopy (HAADF-STEM) and electron energy-loss spectroscopy (EELS) spectra were collected on a FEI Tecnai F20 UT microscope equipped with a Gatan imaging filter at an acceleration voltage of 200 kV. TEM samples were prepared using

a dual-beam focused ion beam-scanning electron microscopy (SEM) system (FIB-SEM, FEI Helios UX). X-ray photoelectron spectroscopy (XPS) measurements were performed on a Thermo Scientific K-Alpha XPS System with a monochromatic Al $K\alpha$ X-ray source. The spectra were acquired with a passing energy of 50 eV and a dwell time of 50 ms. Each sputtering was performed with a 1 keV Ar^+ beam for 20 s. All the instruments for FIB, TEM, and XPS analyses were located at the Molecular Foundry at Lawrence Berkeley National Laboratory (LBNL).

Hard X-ray absorption spectroscopy (hXAS) at the Ti K -edge were measured in transition mode at beamline 20-BM-B of the Advanced Photon Source, Argonne National Laboratory. An Si (111) monochromator was used for selecting the incident beam energy. An Rh-coated mirror was applied to obtain harmonic rejection. The energy calibration was accomplished by simultaneously measuring the spectra of Ti-metal foil. Normalization, calibration, and linear combination fitting of raw data were performed by Athena software.²⁸ Ti $L_{3\text{-edge}}$ resonant inelastic X-ray scattering (RIXS) spectra were obtained in the iRIXS end-station at beamline 8.0.1 of the Advanced Light Source at LBNL. The MTO samples were mounted on a copper sample holder and transferred to the ultrahigh vacuum chamber for the measurement. The resolving power of the incident X-rays is around 1500, and the samples were continuously moved within a 5 mm range to minimize photon-beam damage. The emission spectra at each excitation energy were collected for 200 s. The excitation energy of 458 eV was used for the measurement of RIXS, which corresponds to the t_{2g} resonance for the Ti $L_{3\text{-edge}}$.

Evaluation of conductivity and corrosion stability

The electrical conductivities of the MTOs were measured using the direct-current (DC) polarization method. DC voltages of 0.1–1 V were applied, and the saturated currents at each applied voltage were measured using a multipotentiostat (Biologic VMP-300). For the electrical/electrochemical analyses of the synthesized MTO, as-sintered pellets were used to ensure a higher pellet density ($\sim 85\%$). Static corrosion current measurements were performed in a three-electrode liquid-cell setup. The counter electrode used in our experiments was a $\sim 16 \text{ cm}^2$ Pt mesh, and the reference electrode was a Ag/AgCl electrode in KCl solution. MTO pellets with a high relative density ($\sim 85\%$) were used for the corrosion current measurements. The MTO sample with an effective area of 1 cm^2 was used as the working electrode. Before the corrosion measurement, all the sample surfaces (including SS316 and graphite sheets) were polished using 320 to 800 grit sandpaper. This was performed to achieve a similar surface roughness for the different samples for static corrosion current measurements; sulfuric acid (pH = 2) was used as the electrolyte. The static corrosion current was recorded at 1.0 V bias vs. a Ag/AgCl reference electrode for 144 h at 60 °C in a temperature chamber.

Results

Materials prediction

To search for chemically protective oxides, first-principles DFT calculations were conducted between various adsorbing

corrosive chemical molecules and the oxide substrate DFT slab models. Fig. 1a presents the DFT single-adsorption calculation results of $\Delta E_{\text{F,ads}}$ as a function of $\Delta E_{\text{H,ads}}$ for 23 binary oxide and nitride materials tested in this work and the approximate range of experimental conductivities, σ , in S m^{-1} (see Table S1 in ESI†). For further details and rationales on our theoretical calculation procedure and analysis, please refer to ESI Note 1 and Fig. S1–S4.† In Fig. 1a, MgO is observed to be the most protective chemical species against H and F adsorption (*i.e.*, more positive binding energies); however, MgO is also known to have an experimental bandgap greater than 5 eV (*i.e.*, insulating). Most conducting materials such as NbO, MoO₂, RuO₂, and nitrides are located near the lower-left quadrant of Fig. 1a – *i.e.*, not very protective against corrosive species. We note in Fig. 1a that TiO, which is typically observed as a matrix within reduced titanium oxide (TiO_x), is moderately protective and electronically conducting. According to our theoretical analysis in Fig. 1a, we propose a hypothesis that a ternary Mg–Ti–O compound may be able to have both anti-corrosive and conductive characters if the oxidation state of Ti can be controlled (*i.e.*, less than +4). Here, we made an admittedly simple assumption that the surface characteristics of a ternary Mg–Ti–O compound may be similar to that of Mg–O and Ti–O octahedrons in binary oxide systems. There are several different stable MTO compounds, including MgTiO₃, Mg₂TiO₄, and MgTi₂O₅, that are experimentally accessible (*i.e.*, synthesizable). Among these, we selected the Ti-excess MgTi₂O₅ (orthorhombic, *Cmcm*) as a model system, as shown in Fig. 1b, to verify our proposed hypothesis of Mg–O and Ti–O contributing to the anti-

corrosive character and increased conductivity, respectively, for a ternary Mg–Ti–O chemical system.

Furthermore, we performed hydrogen-dissociation DFT calculations on MgTi₂O₅, TiO, and TiO₂, as shown in Fig. S5.† The (110), (100), and (101) surface facets were selected for MgTi₂O₅, TiO, and TiO₂, respectively, because they are the most energetically stable (*i.e.*, lowest surface energy) surface facet for each material. We report in Fig. 1c that the calculated hydrogen dissociation energies ($\Delta E_{\text{H,diss}}$) for MgTi₂O₅, TiO, and TiO₂ are similar: approximately 1 eV per adsorption site. However, a significantly reduced hydrogen coverage ($\theta_{\text{H,cov}}$, the ratio between H atoms to surface oxygen atoms) was observed in the (110) MgTi₂O₅ system (~30.8%), whereas the (100) TiO and (101) TiO₂ surfaces were fully covered by hydrogen. This finding directly hints at the possibility of the improved anticorrosive characteristic of MgTi₂O₅-based compounds.

Next, we examined the electronic structures of various MgTi₂O₅-based compounds by varying the composition ratio of Mg/Ti to find the conductive phase of MTO compounds. Fig. 1d–e present the chemical structures of Mg_{1.23}Ti_{1.77}O₅ and Mg_{0.73}Ti_{2.27}O₅, which were selected as representative phases where an extra Mg or Ti atom is occupying the Ti or Mg site in MgTi₂O₅, respectively. According to our DFT calculations, while Ti substitution on the Mg site is energetically favored (−0.158 eV per site with respect to elemental Mg and Ti), Mg substitution at the Ti site is not very feasible (+6.602 eV per site). We find in Fig. 1f that the Ti-excess MTO system (here, Mg_{0.73}Ti_{2.27}O₅) drastically modifies the electronic structure of pristine MgTi₂O₅. The calculated density of states (DOS) of MgTi₂O₅ clearly shows a DFT bandgap of ~2.5 eV, underestimated from

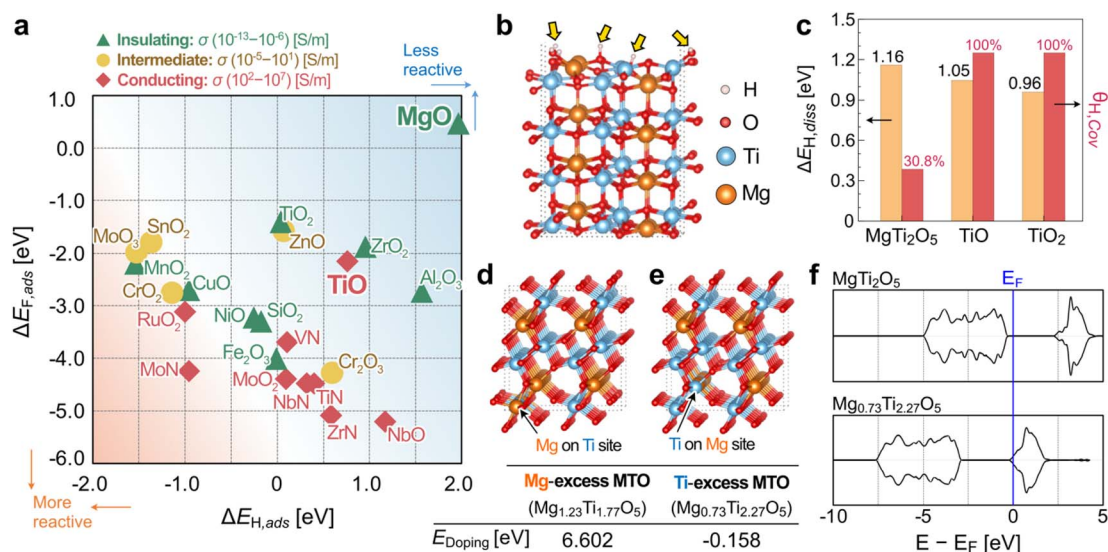


Fig. 1 (a) Correlation observed between $\Delta E_{\text{H,ads}}$ and $\Delta E_{\text{F,ads}}$ after DFT single-adsorption calculations. (b) Hydrogen dissociation on a (110) MgTi₂O₅ slab model and (c) comparison of the hydrogen dissociation energy ($\Delta E_{\text{H,diss}}$) and hydrogen coverage ratio ($\theta_{\text{H,cov}}$) of each Ti oxide. Note that only a few oxygen sites (~30.8%) showed hydrogen adsorption (denoted by the yellow arrows), suggesting MgTi₂O₅ is more protective in an acidic environment. Illustration of (d) Mg_{1.23}Ti_{1.77}O₅ and (e) Mg_{0.73}Ti_{2.27}O₅ structures, where an excessive Mg or Ti atom is occupying the Ti or Mg site in MgTi₂O₅, respectively. The inset table presents a comparison of the doping energy of each model. (f) Total density of states (DOS) for MgTi₂O₅ and Mg_{0.73}Ti_{2.27}O₅. Note that the Fermi level (E_{F}) of the Ti-excess MgTi₂O₅ system is occupied, in contrast to that of the stoichiometric MgTi₂O₅.

the experimentally reported bandgap of 3.4 eV.^{29,30} Although it is well known that DFT underestimates band gaps for semi-conductors,³¹ our DFT calculation proves the insulating nature of the pristine MgTi_2O_5 compound. We observe that the Fermi level (E_F) of $\text{Mg}_{0.73}\text{Ti}_{2.27}\text{O}_5$ is now being occupied from the DOS analysis in Fig. 1f for the Ti-excess MTO system. This indicates that the electronic structures can be tuned to become metallic for Ti-excess MTO phases (for details, see Fig. S6 in ESI†). Our DFT calculations also suggest that oxygen vacancy formation is challenging in the MTO system. For both bulk and (110) surface cells, the calculated oxygen vacancy formation energies are higher than +5 eV: for bulk MTO cell ($\text{Mg}_{12}\text{Ti}_{24}\text{O}_{59}$, equivalent to $\text{MgTi}_2\text{O}_{4.92}$), $E_{\text{Ovac,bulk}} = +5.694$ eV per site. For (110) surface of MTO cell ($\text{Mg}_{16}\text{Ti}_{32}\text{O}_{79}$, equivalent to $\text{MgTi}_2\text{O}_{4.94}$), $E_{\text{Ovac,surf}} = +5.271$ eV per site. It is slightly easier to take O from the surface, but in either case, the oxygen vacancy formation energy is huge. In other words, +5 eV of the energy means that it is extremely difficult to remove the oxygen from bulk MTO or (110) facet of MTO surface. Therefore, in our XRD studies below, we assume that MTOs have a full oxygen occupancy. In the following section, we will discuss our experimental efforts to find the optimal chemical composition of MTO compounds that preserve both conductivity and anti-corrosive character.

Understanding synthesis parameters to make conductive MTO

To select the appropriate precursors for practical access to the Mg–Ti–O ternary compounds, we first tested various precursors of Mg and Ti, including MgO, MgCO_3 , TiO, Ti_2O_3 , and TiO_2 (see

Fig. S7 in ESI†). According to the XRD results of the products from each precursor set, MgCO_3 and TiO_2 precursors were selected to form the pure MgTi_2O_5 phase. Subsequently, we applied a systematic approach by tuning the precursor ratio and the gas environments (H_2 (2%)/Ar (98%) mixed gas, Ar gas, and ambient air) to achieve the lowest oxidation state of Ti within the solubility limit in MTO (Fig. 2). When MgCO_3 is excessive (Ti/Mg < 2.3) in the precursor mixture, a MgTiO_3 phase (denoted * in Fig. 2a) appears in the synthesized MTO as an impurity under H_2/Ar mixed gas flow. Similarly, we observed the MgTiO_3 phase as an impurity (denoted * in Fig. 2b and c) under Ar gas flow or ambient air environment when the Ti/Mg ratio is smaller than 1.8. In contrast, a rutile TiO_2 phase (denoted ▼ in Fig. 2b and c) remains as an impurity after the synthesis reactions in Ar gas and ambient air environments when relatively more TiO_2 precursor (Ti/Mg > 1.8) is used. In contrast, MTOs synthesized under the mixed gas (H_2/Ar) do not contain the rutile TiO_2 impurity until the Ti/Mg ratio reaches 2.3, where a pure MTO phase forms. MTOs synthesized under H_2/Ar mixed gas flow are expected to have the most Ti^{3+} components compared with the MTOs synthesized under the other gas environments due to their expected composition (Ti-rich composition) and darkest powder color. In general, a darker color of titanium-based oxide powder indicates that their electrical conductivity is high.^{32–34} For the Ti/Mg precursor ratio = 2.3, the highest Ti content in the test (Fig. 2a and d), we observed that $\text{Mg}_{0.77}\text{Ti}_{2.23}\text{O}_5$ is formed, according to Rietveld refinement results. This corresponds to $\text{Ti}^{3.80+}$ as an average oxidation state of Ti (see Fig. S8a†). Under the Ar gas environment, the purest MTO phase is produced at a lower TiO_2 precursor ratio, compared with the H_2/Ar mixed

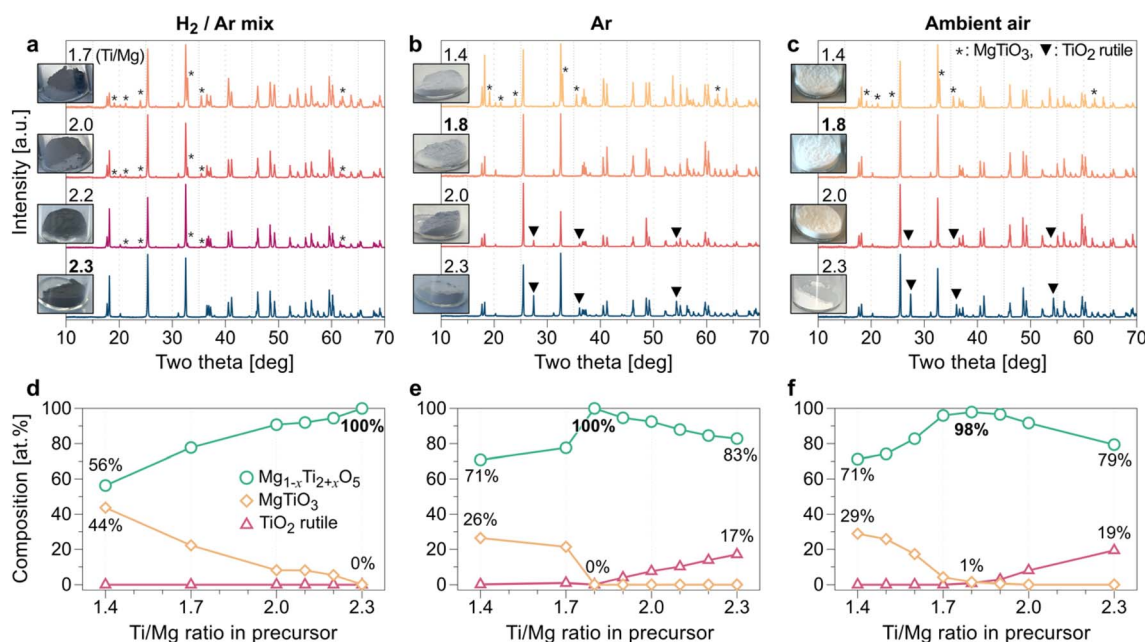


Fig. 2 (a–c) XRD results and optical images of MTOs from various ratios of the precursor mixture and various gas environments. (d–f) Composition curves of the products as a function of the Ti/Mg molar ratio in the precursor mixture. Each column of the figure refers to the MTO series synthesized under (left) 2% H_2/Ar mixed gas, (center) Ar gas, and (right) ambient air environment. Note that the amount of the rutile phase (denoted as ▼) increases with increasing Ti content in the precursor, whereas the MgTiO_3 (denoted as *) content in the product increases with decreasing Ti content in the precursor.

gas flow (Fig. 2b and e). For Ti/Mg = 1.8, according to the Rietveld refinement results, $\text{Mg}_{0.89}\text{Ti}_{2.11}\text{O}_5$ ($\text{Ti}^{3.90+}$) is formed (see Fig. S8b†). Under ambient air, the purest MTO phase is produced for Ti/Mg = 1.8 (Fig. 2c and f), and we confirmed the formation of $\text{Mg}_{0.97}\text{Ti}_{2.03}\text{O}_5$ ($\text{Ti}^{3.97+}$) using Rietveld refinement (see Fig. S8c†). Notably, regardless of the Ti content in the precursors, the color of the synthesized MTO is likely to be determined by the gas environment (see Fig. 2a–c and S9†). To better understand the roles of temperature and the gas environment in the synthesis of MTO, we conducted temperature- and gas-controlled experiments (see Fig. S10†). We found that a lower temperature always results in less purity of MTO regardless of the gas environment. This can be explained by previous reports on the formation of the MgTi_2O_5 phase, which requires high temperature for phase transformation.^{35,36} H_2/Ar mixed gas flow could form a black MTO powder even at a relatively low temperature (1100 °C). This clearly demonstrates that the synthesis of black MTO powder is determined by H_2/Ar gas

(i.e., reducing environment), which will likely help in reducing the oxidation state of Ti in MTO.

Improving electrical conductivity of MTOs

The electrical conductivities of the MTOs were evaluated using the DC polarization test on the as-sintered MTO pellets (Table 1). As expected from its dark color, MTO synthesized under H_2/Ar mixed gas ($\text{Mg}_{0.77}\text{Ti}_{2.23}\text{O}_5$) exhibits the highest conductivity among the other gas environments. The measured value from the MTO synthesized under H_2/Ar gas is ~5 orders of magnitude higher than that of the MTO under Ar. The MTO synthesized under ambient air exhibited insulating properties. Its conductivity was beyond the range of our instrument.

To improve the conductivity of MTO, we increased the Ti component to further reduce the oxidation state of Ti. Fig. 3 presents the series of XRD results of MTO synthesized from varied TiO_2 precursor, $\text{Ti}/\text{Mg} \geq 2.3$. No noticeable impurity peak was observed for the MTOs ranging from $2.3 \leq \text{Ti}/\text{Mg} \leq 4.0$. This implies that the Ti solubility limit in the reductive environment (H_2/Ar mixed gas) is much higher than that of the other gas environments ($\text{Ti}/\text{Mg} = 1.8$ for both cases of Ar gas and ambient air). For a greater Ti content in the precursor mixture than $\text{Ti}/\text{Mg} = 4.0$, the TiO_2 rutile phase (indicated by the red box in Fig. 3) appears as an impurity. For the higher TiO_2 precursor mixing composition with $\text{Ti}/\text{Mg} \geq 6.5$, unknown additional peaks appeared at 25° – 30° , 34° – 35° , etc. (indicated by the yellow box in Fig. 3) while the peak intensity of MTO decreases, indicating phase transformation or decomposition.

Table 1 Comparison of the synthesized MTO under H_2/Ar mixed, Ar gas, and ambient air

Gas environment	H_2/Ar mixed	Ar gas	Ambient air
Precursor ratio (Ti/Mg)	2.3	1.8	1.8
Formula	$\text{Mg}_{0.77}\text{Ti}_{2.23}\text{O}_5$	$\text{Mg}_{0.89}\text{Ti}_{2.11}\text{O}_5$	$\text{Mg}_{0.97}\text{Ti}_{2.03}\text{O}_5$
Color of powder	Black	Gray	White
Conductivity [S cm^{-1}]	3.1×10^{-3}	5.0×10^{-8}	—

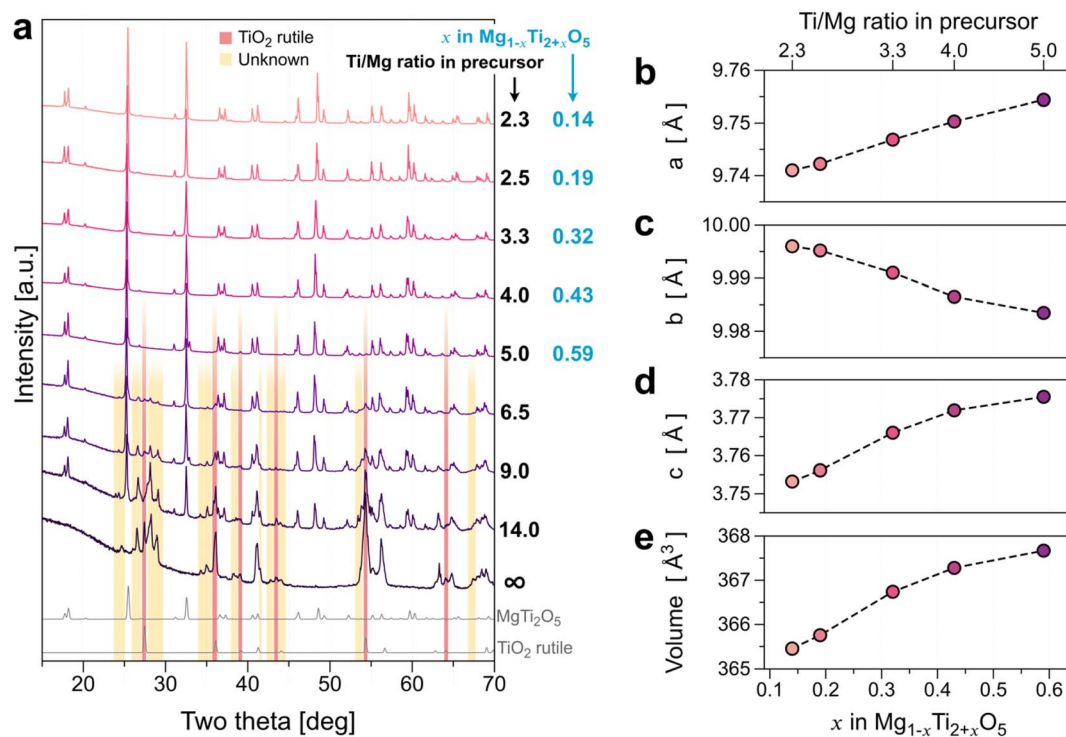


Fig. 3 (a) Series of XRD results of MTO synthesized from precursor with a TiO_2 content greater than $\text{Ti}/\text{Mg} = 2.3$. Note that the remaining TiO_2 rutile phase (indicated by the red box) appears in MTOs ($\text{Ti}/\text{Mg} > 4.0$) from the excessive Ti in the precursor. (b–e) Relations between the unit-cell parameters and volume as a function of x in $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$.

Table 2 Comparison on the XRD and SEM-EDS results

Ti/Mg ratio in precursor	Ti/Mg = 2.3		Ti/Mg = 3.3		Ti/Mg = 4.0		Ti/Mg = 5.0	
	Mg	Ti	Mg	Ti	Mg	Ti	Mg	Ti
XRD	0.86	2.14	0.68	2.32	0.57	2.43	0.41	2.59
SEM-EDS	0.72	2.28	0.43	2.57	0.42	2.58	0.37	2.63

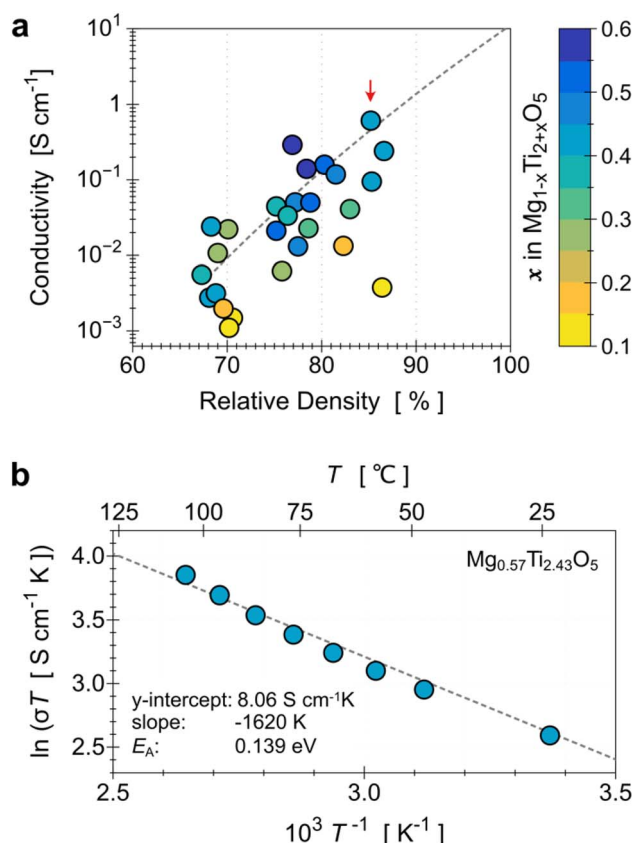


Fig. 4 (a) Relation between the electrical conductivity, relative density of the MTO pellet, and relative Ti content (x in $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$). Note that the dotted line is the fit of the MTOs with a similar valence state of Ti ($+3.65 \pm 5\%$), which is the condition that resulted in the best conductivity in the present study ($6.09 \times 10^{-1} \text{ S cm}^{-1}$ at $\text{Mg}_{0.57}\text{Ti}_{2.43}\text{O}_5$, indicated by the red arrow). (b) Temperature dependence of the conductivity of $\text{Mg}_{0.57}\text{Ti}_{2.43}\text{O}_5$, plotted as $\ln(\sigma T)$ vs. T^{-1} . The dotted line is the best-fit line with eqn (1).

Therefore, we will only discuss the effect of the Ti content of the MTOs for Ti/Mg ratios ranging from 2.3 to 5.0 in the precursor. Fig. 3b–d illustrate the lattice parameters and unit cell volume of the MTOs synthesized in this study with no impurity peaks (*i.e.*, ≤ 5.0 of Ti/Mg ratios in precursor). Lattice parameters a and c increase as Ti content increases in the precursor, whereas b decreases. The overall volume of the unit-cell (Fig. 3e) increases monotonically as Ti content increases, indicating solid-solution of $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$. The unit-cell volume increase could be explained by the reduction of the Ti's oxidation state as the Ti content increases. We also performed SEM-EDS

quantitative analysis (Table 2) to better understand the composition of the samples. Note that the characteristic X-ray signal from the EDS measurement is generated at $\sim 500 \text{ nm}$ depth from the sample surface. Given the particle size of the MTO samples are $\sim 6.2 \mu\text{m}$ as shown in Fig. S11,[†] the EDS results will show the composition information of the surface rather than the bulk.

To evaluate the electrical conductivity dependence on the increased Ti content (x in $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$), we also need to consider the relative density of the samples. Fig. 4a shows the relation among the three parameters (Ti content, relative density, and electrical conductivity) in a single plot. The x values were determined from the Rietveld refinement of the XRD results, and they have a positive relationship with the Ti/Mg ratio in the precursor mixture. The graph shows that as the density of the sample increases, the conductivity increases on a logarithmic scale. It also clearly shows that if the MTO samples have the same (or at least similar) density, the conductivity increases as the Ti content increases (*i.e.*, x in $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$). The highest conductivity we obtained as $6.09 \times 10^{-1} \text{ S cm}^{-1}$, measured for the $\text{Mg}_{0.57}\text{Ti}_{2.43}\text{O}_5$ ($x = 0.43$, Fig. S8d[†]) pellet with a density of 85.5% (indicated by the arrow in Fig. 4a). The activation energy of its electrical conduction, calculated from the Arrhenius eqn (1), is 0.139 eV (Fig. 4b).

$$\ln(\sigma T) = \ln A - \frac{E_A}{k_B} \left(\frac{1}{T} \right) \quad (1)$$

This is much higher than the known experimental conductivities of binary metal oxides, existing ESI (see Table S1).[†] By using a higher Ti/Mg ratio precursor mixture (Ti/Mg = 5.0), we could increase the x value up to 0.59; however, the TiO_2 rutile phase of at least 5% or more formed as an impurity.

Origin of high electrical conductivity of MTO with high Ti content

We used various chemical analysis techniques to evaluate how the Ti content determines the electronic structure of MTOs. First, X-ray absorption near-edge structure (XANES) analysis was performed to obtain Ti K-edge spectra. The XANES spectra of four MTO compounds, as well as Ti_2O_3 and TiO_2 standards, are presented in Fig. 5a. The Ti edges of all the MTO compounds are located between Ti_2O_3 and TiO_2 , indicating that the valence states of Ti in those MTOs are between +3 and +4. The intensity of the Ti pre-edge in the inset of Fig. 5a decreases, indicating the reduction of the valence state of Ti as the Ti content increases in MTOs. Note that the pre-edge and edge position not only depend on the valence but also on the coordination environment. Therefore, the quantitative analysis for the valence states of Ti in MTOs using XANES may not be reliable.

RIXS was also employed to evaluate the oxidation-state changes of Ti in MTOs because the technique is very sensitive to the 3d electron configurations.³⁷ In particular, Ti^{4+} is a d^0 system so RIXS features from excitations of d electrons from occupied to unoccupied state, so-called d–d excitations, is completely missing in contrast with other $\text{Ti}^{3+/2+}$ states,³⁸ as

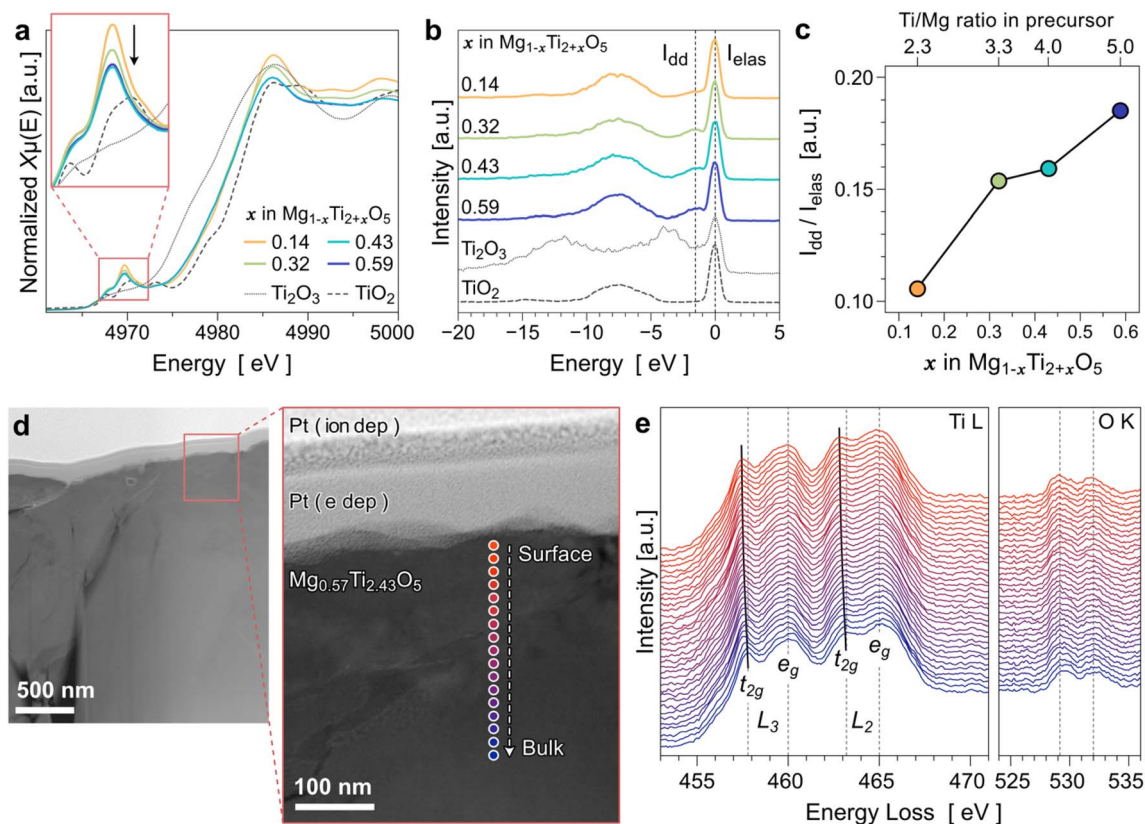


Fig. 5 Chemical analysis of synthesized MTOs ($x = 0.14, 0.32, 0.43$, and 0.59 in $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$). (a) Ti K-edge XANES results. The inset presents an enlarged view of the pre-edge region. (b) RIXS spectra collected with the excitation energy of 458 eV. Standard spectra of Ti^{3+} (Ti_2O_3) and Ti^{4+} (TiO_2) are included as references. (c) Relative peak areas of $I_{\text{dd}}/I_{\text{elas}}$ plotted as a function of x . (d) HAADF-STEM images of the surface region of $\text{Mg}_{0.57}\text{Ti}_{2.43}\text{O}_5$. (e) Series of Ti L and O K-edge EELS spectra measured along the line from the surface to the interior of the $\text{Mg}_{0.57}\text{Ti}_{2.43}\text{O}_5$ particle.

shown by the reference spectra in Fig. 5b. The occurrence of the weak peak close to the elastic line in the MTO samples corresponds to such dd-excitation (indicated by the dotted line under I_{dd}), indicating reduced Ti states.³⁹ The relative peak areas of $I_{\text{dd}}/I_{\text{elas}}$ plotted in Fig. 5c increased with increasing Ti content in the MTO. This demonstrates that the oxidation state of Ti in the MTO decreases as the Ti/Mg ratio increases.

Although the Ti reduction trend according to the Ti content is consistent with our initial expectation, the RIXS analysis integrates all signals of the near surface region with a probe depth of about 100 nm. To better understand whether the valence state of Ti is identical throughout the particle from the surface to the inner part, we conducted a comparative study along the depth of the material (*i.e.*, depth profile analysis). This can be evaluated through the Ti 2p_{3/2} peak shifts depending on the Ar sputtering cycle *via* XPS. However, for transition-metal oxides such as MTO, there is a limitation that an accurate chemical evaluation is impossible. This is because the Ar sputter removes oxygen from the surface faster than the other elements of the transition-metal oxide; thus, oxygen vacancies can be artificially formed.^{40,41} We also confirmed this issue in the preliminary XPS study (see Fig. S12†). Hence, we conducted an electron energy-loss spectroscopy (EELS) line profile analysis using transmission electron microscopy (TEM) at the surface region of the $\text{Mg}_{0.57}\text{Ti}_{2.43}\text{O}_5$ sample ($x = 0.43$ in $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$).

Fig. 5d presents a STEM-HAADF image recorded at the surface of the sample. Because the sample was prepared *via* FIB, the Pt layers from the ion-beam and e-beam deposition are clearly observed at the surface. Fig. 5e presents a series of Ti L_{2,3} near-edge structures of the EELS line profile analysis results. The splitting of the Ti L_{2,3} edge spectra observed in Fig. 5e indicates that the octahedral crystal field lifts the degeneracy of the Ti 3d states into t_{2g} and e_g components.⁴² The t_{2g} components of the Ti L_{2,3} edge shift slightly toward the lower energy loss as it is close to the surface, suggesting that the MTO surface has a lower Ti valence than the interior. Therefore, we speculate that the electron conduction is promoted more near the surface of MTOs. We expect that the gradual shift of the Ti valence state near the surface is attributable to the composition change (Ti/Mg ratio). This is also agreed with the fact that the EDS quantitative analysis shows slightly higher Ti concentrations in the MTO samples than the XRD-refined composition results as shown in Table 2. This is because the characteristic X-ray signal from the EDS measurement is generated at ~500 nm depth from the sample surface.

Corrosion resistance

To evaluate the corrosion resistance of the optimized MTO (*i.e.*, $\text{Mg}_{0.57}\text{Ti}_{2.43}\text{O}_5$), we first measured the structural changes of MTOs before and after exposing the MTO pellets to 0.01 M HCl

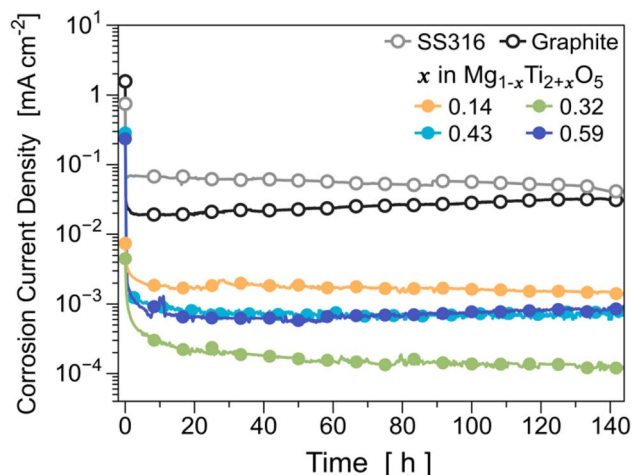


Fig. 6 Development of the corrosion rate for MTOs with various compositions during 6 days of exposure in H_2SO_4 solution, $\text{pH} = 1$.

($\text{pH} = 2.0$) solution (see Fig. S13†). There was no noticeable structural change in the MTO sample after exposure to the acid solution. In addition, we did not observe any color change in the solution when the MTO sample was stored in the acid solution (inset figure of Fig. S13†), demonstrating that MTO does not react with the acid solution. We also conducted static corrosion current measurements on the MTOs in acidic environments (Fig. 6). We used graphite and 316 stainless steel (SS316) as references because they are typical acid-resistant materials. For $\text{Mg}_{0.68}\text{Ti}_{2.32}\text{O}_5$ (i.e., $x = 0.32$), its static corrosion current density is $1.2 \times 10^{-4} \text{ mA cm}^{-2}$, which indicates that the corrosion stability of the optimized MTO is ~ 350 times higher than that of SS316 and ~ 250 times higher than that of graphite carbon. In addition, we found that the corrosion resistance of $\text{Mg}_{0.68}\text{Ti}_{2.32}\text{O}_5$ ($x = 0.32$) is better than that of other compositions such as $\text{Mg}_{0.57}\text{Ti}_{2.43}\text{O}_5$ ($x = 0.43$) and $\text{Mg}_{0.41}\text{Ti}_{2.59}\text{O}_5$ ($x = 0.59$). It is speculated that this optimal stability composition emerges from the trade-off between the enthalpic penalty of Ti substitution and the entropic gain of added disorder, as described in detail in ESI Note 3† and the subsequent discussion section.

Discussion

We have demonstrated that the electrical conductivity of MTO can be improved by controlling the relative contents of Mg and Ti in the MTO structure. As the Ti content increases, we can achieve higher electrical conductivity of MTO within the solubility limit ($x = 0.43$ in $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$), as shown in Fig. 3a. However, the optimal corrosion resistance is achieved at a specific Mg/Ti composition ($x = 0.32$), as shown in Fig. 6. To better understand the tunable stability of MTO upon Ti substitution, we analyzed the substitution energy by performing a convex-hull analysis in the MTO phase space.^{43,44} Although typically, Mg occupies the M1 site and Ti occupies the M2 site, high-temperature processing can stabilize the disordered structures, where some Mg (Ti) moves to M2 (M1);³⁶ this

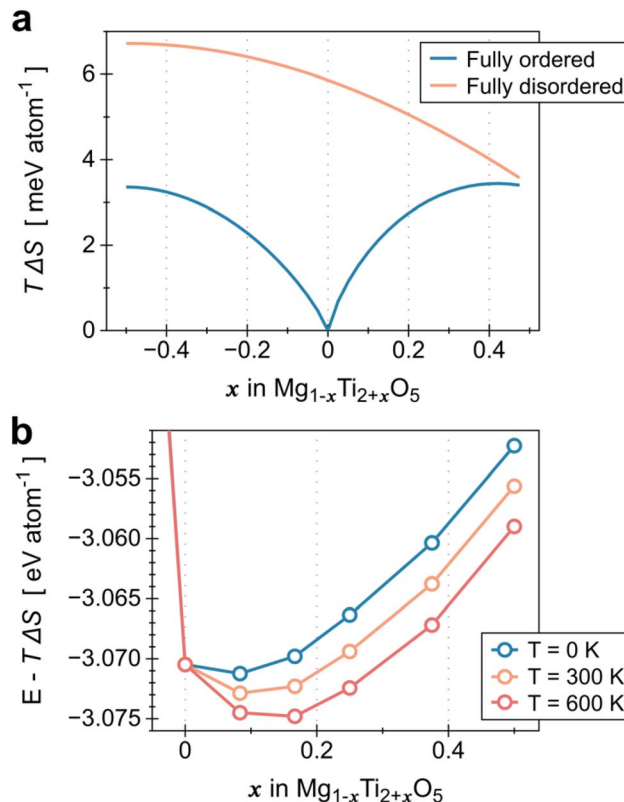


Fig. 7 (a) Contribution of mixing entropy at 300 K for $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$, ranging from the fully ordered experimental structure (all Mg/Ti fill the M1/M2 sites, respectively) to fully disordered (random occupation of M1/M2 states). Note that the mixing entropy for the fully ordered MgTi_2O_5 ($x = 0$) is 0. (b) Formation free energy of $\text{Mg}_{1-x}\text{Ti}_{2+x}\text{O}_5$ at zero temperature, room temperature, and elevated temperature; the entropic stability is observed to be significant.

disorder corresponds to the mixing entropy, $S = -R \sum c_i \ln c_i$, plotted in Fig. 7a. The Rietveld refinement parameters derived from our experimental results (Table S2 in ESI†) indicate that our materials are highly ordered, with almost all the M2 sites occupied by Ti, leading to the free energies of formation plotted in Fig. 7b. We therefore discovered that excess Ti can stabilize MTO despite the enthalpic penalty, indicating that there is some optimal Ti substitution that could stabilize the MTO. We include further details on the entropy and interfacial reactivity in Fig. S13 and S14.†

One might expect that the black color of the MTO powder and corresponding high electrical conductivity originate from the residual carbon in the sample because MgCO_3 was used as a precursor. However, it is less likely that carbon survives under the high-temperature synthesis condition ($\sim 1500^\circ\text{C}$). In addition, we confirmed that the black color of the synthesized MTO originates from the reduction of Ti (see Fig. S16†) instead of residual carbon. If the black color originates from carbon, it could not be recovered after a sequential re-sintering under (1) ambient air and (2) H_2 (2%)/Ar (98%) gas flow. This is because the residual carbon will be irreversibly removed after the reaction with O_2 in the ambient air to form CO_2 from the former re-sintering process. However, as observed in Fig. S16,† the black

color is recovered after the sequential (1) and (2) re-sintering process. Upon further considering the Rietveld refinement results, we observed that the Ti content of MTO decreased after the first re-sintering under ambient air, indicating decomposition of Ti-rich MTO into Mg-rich MTO and TiO_2 . After the second re-sintering under H_2 (2%)/Ar (98%) gas flow, Ti-rich MTO is recovered.

In addition to the key idea used in the present study (*i.e.*, controlling the Ti/Mg ratio in MTO), we further suggest possible alternative routes to increase the electrical conductivity of MTO. According to our DFT calculations on various MTO models, the same phenomenon with the Ti-excess MTO system (here, $\text{Mg}_{0.73}\text{Ti}_{2.27}\text{O}_5$) may also occur by further tuning the chemical composition by either creating an oxygen vacancy ($\text{MgTi}_2\text{O}_{4.92}$) or doping Al^{3+} in MgTi_2O_5 ($\text{Al}_{0.08}\text{Mg}_{0.92}\text{Ti}_2\text{O}_5$). The DOS calculation results indicate that the Fermi level (E_F) is occupied in all those systems (see Fig. S6d–ff), therefore, we expect that oxygen vacancy and Al^{3+} doping reduce the Ti oxidation state; thus, they will exhibit increased conductivity.

Although we demonstrate that Ti-rich MTO synthesized under a controlled synthesis condition at high temperature exhibits high electrical conductivity and corrosion resistance, it is challenging to use this MTO material in a practical PEMFC in its current state. This is because the catalyst supporter requires a high surface area to hold large amounts of Pt catalyst. Because Ti-rich MTO can only be synthesized at high temperature in our solid-state synthesis method, we need to reduce the particle size by post-ball milling. Unfortunately, we found that the particle color becomes brighter with increasing ball-milling time, indicating a decrease in the conductivity. Therefore, a low T synthesis method such as the sol-gel method or hydro/solvothermal methods may be required to synthesize Ti-rich MTOs to be used and tested as a catalyst support for PEMFCs.

Conclusion

We presented a strategy to overcome the trade-off between good electrical conductivity and electrochemical stability of ternary oxide materials. A conductive and corrosion-resistive MTO phase ($\text{Mg}_{0.68}\text{Ti}_{2.32}\text{O}_5$) was successfully synthesized under controlled synthesis environments with a reducing reaction environment (H_2/Ar mixed gas flow) and high temperature ($\sim 1500^\circ\text{C}$). The origin of the high conductivity of MTO was investigated and is attributed to the oxidation state of Ti reaching +3.65 (reduction toward +3 from +4) for the MTO. In addition, we found that a reducing gas environment ensured higher Ti solubility and lower Ti oxidation states, thus promoting the electrical conductivity.

Author contributions

Y.-W. B.: formal analysis; investigation; methodology; visualization; writing – original draft; writing – review & editing. J. M., M. K., G.-H. L., Z. C.: formal analysis; investigation; writing – original draft. Y. S.: formal analysis; investigation. W. Y.: formal analysis; supervision; writing – review & editing. C. J., J. C.: supervision; project administration. S. K.: conceptualization;

software; supervision; project administration; visualization; writing – original draft. L. C.: conceptualization; methodology; supervision; validation; writing – original draft; writing – review & editing. H. K.: conceptualization; formal analysis; funding acquisition; methodology; supervision; writing – original draft; writing – review & editing.

Conflicts of interest

L. C., S. K., M. K., J. C., and J. M. are inventors on several U.S. patent applications assigned to Robert Bosch GmbH related to this work. The other authors declare that they have no competing interests.

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