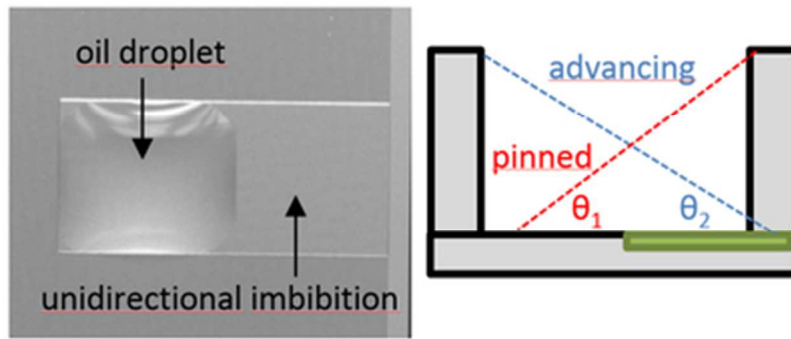




**Directional Imbibition on a Chemically Patterned Silicon  
Micropillar Array**

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Silicon micropillar arrays overlaid with specific surface chemistry patterns allow unidirectional, two types of bidirectional and tridirectional imbibition of oils.



34x14mm (300 x 300 DPI)

## ARTICLE

# Directional Imbibition on a Chemically Patterned Silicon Micropillar Array

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Directional imbibition of oils (hexadecane, tetradecane, dodecane) and water is demonstrated on a chemically patterned silicon micropillar array. Four different directional imbibition types are shown: unidirectional, two types of bidirectional and tridirectional. The surfaces consist of a silicon micropillar array with an overlaid surface chemistry pattern. This configuration leads to anisotropic wetting behaviour into various directions of the advancing meniscus. Due to the free energy landscape obtained, the advancing meniscus gets pinned in some directions (determined by the surface chemistry pattern) while it is free to move to the remaining directions. The conditions for directional imbibition and design criteria for the surfaces are derived and discussed.

## 1 Introduction

There have been significant advances in the last decade in understanding and controlling wetting interactions between liquids and structured solids. The research field of superhydrophobic surfaces has been at the forefront of these developments and has seen a lot of activity especially in the last decade<sup>1,2</sup>. Other areas that have seen advances include omniphobic surfaces<sup>3</sup>, hydrophilic/hydrophobic patterning<sup>4</sup> and anisotropic wetting<sup>5,6</sup>.

Anisotropic wetting encompasses surfaces where the droplet either spreads or rolls off anisotropically. These types of behaviors are also found in the nature in e.g. bird feathers<sup>7</sup> and fish fins<sup>8</sup>. The studies of anisotropic wetting can be divided into anisotropic non-wetting and anisotropic wetting. Anisotropic non-wetting surfaces are characterized by low adhesion and the Cassie Baxter state<sup>9</sup> with limited but anisotropic interaction between the droplet and the solid. Examples include anisotropic roll-off of water droplets from surfaces<sup>10</sup>, directional water droplet movement on topography gradients<sup>11</sup> and underwater anisotropic roll-off of oil droplets<sup>8</sup>.

Surfaces that exhibit anisotropic wetting utilize higher surface energy coatings and most commonly the Wenzel state<sup>12</sup>. Due to the stronger anisotropic interaction with the surface, the droplets adopt clearly nonspherical shapes, such as faceted droplet shapes on top of partially wetting rectangular micropillar lattices<sup>13</sup>. Anisotropic wetting surfaces can be classified based on the number of cardinal directions that the droplets spreads to. Our own previous work demonstrated uni- and bidirectional wetting based purely on topography utilizing

triangular microstructures<sup>14</sup>. Other topography based approaches have been unidirectional wetting based on stooped micro- or nanopillars<sup>15,16</sup>, bidirectional wetting on micro-grooved surfaces<sup>17,18</sup> and anisotropic imbibition on polygonal posts<sup>19</sup>. Surface energy patterns combined to pillar topographies can also be utilized for creating anisotropic wetting, as demonstrated by uni- bi-, and –tridirectional wetting based on oblique glancing angle deposition<sup>20,21</sup>. Anisotropic wetting can also be achieved based strictly on surface energy patterns without a topography contribution, as demonstrated by bidirectional wetting on top of hydrophilic grooves<sup>22</sup>. Temperature tunable unidirectional wetting has been achieved through a poly(N-isopropylacrylamide) coating on top of prism structure<sup>23</sup> or a half shell nanocone structure<sup>24</sup>.

Most of the studies of anisotropic/directional wetting approach the topic from the point of view of the droplet and the differing contact angles into different directions<sup>15-24</sup>. However, less attention has been given to the anisotropic nature of the imbibition front<sup>25</sup> that often precedes the movement of the droplet contact line.

Here we present uni-, bi- and tridirectional imbibition of liquids. The anisotropy of imbibition is achieved by a micropillar surface combined with a lithographically overlaid surface chemistry pattern. Directional imbibition is studied primarily with various oils (hexadecane, tetradecane, dodecane) but is also demonstrated for water. The fabrication process and the design parameters are explained for achieving directional wetting.

## 2 Experimental Section

### Fabrication of silicon micropillar arrays

Plasma enhanced chemical vapor deposition (Plasmalab 80+, Oxford Instruments, 300°C, 1000 mTorr, 20 W, 8.5 sccm SiH<sub>4</sub>) was used to deposit a 840 nm (70 nm/min) thick silicon dioxide layer to act as the mask during deep silicon etching. The silicon dioxide was patterned by optical lithography (MA6, Karl Süss MicroTec) and reactive ion etching (Plasmalab 80+, Oxford Instruments, 200 mTorr, 30 W, 25 sccm CHF<sub>3</sub>, 25 sccm Ar). After photoresist removal, the structures were etched to the desired thickness with cryogenic deep reactive ion etching (PlasmalabSystem100, Oxford Instruments, 8 mTorr, -110°C, 1000 W ICP power, 3 W forward power, 40 sccm SF<sub>6</sub>, 6 sccm O<sub>2</sub>). Finally, the silicon dioxide mask was removed by HF wet etching. After the HF, the micropillar arrays were ready for surface chemistry modification and patterning.

The micropillar array consisted of 10 μm x 10 μm square shape pillars in a 30 μm pitch square lattice. Etch depth was measured by a profilometer (Dektak XT, Bruker).

### Chemical modification and patterning

A patterned fluoropolymer/oxidized silicon coating was utilized for directional wetting of oils. A 40 nm thick fluoropolymer coating was deposited on top of the pillar array by plasma enhanced chemical vapour deposition (Plasmalab 80+, Oxford Instruments, 250 mTorr, 50 W, 100 sccm CHF<sub>3</sub>, deposition time 5 min). After the fluoropolymer deposition, a 6.2 μm thick AZ-4562 photoresist layer was spin coated (4000rpm, 30s) on the sample and soft baked (50 min at 90 °C in an oven), exposed and developed. Next, the exposed fluoropolymer areas were etched away by oxygen plasma (Plasmalab 80+, Oxford Instruments, 250mTorr, 50W, 45 sccm O<sub>2</sub>, 5 sccm Ar). The same plasma process simultaneously oxidizes the underlying silicon, creating a completely wetting surface for both water and oils. The photoresist was then stripped in acetone by ultrasonication for 10 minutes.

The patterned coating utilized for directional wetting of water was a hydroxyl terminated silane. First, the wafers were pretreated in oxygen plasma (PVA Tepla Plasmasystem 400, 500ml/min O<sub>2</sub>, power 1000W). Glycidoxypropyltrimethoxysilane (Sigma Aldrich, >98%) was deposited on the surface from dry toluene (20% solution, deposition time 1 hour), followed by rinsing in toluene for 10 minutes, sonicating in acetone for 20 minutes and sonicating in water for 20 minutes. The resulting surface was then further modified by 70mM mercaptoethanol in phosphate buffered saline (normal solution) for 16 hours. The lithography and the oxygen plasma removal and silicon oxidation processes are the same as above.

### Contact angle measurements

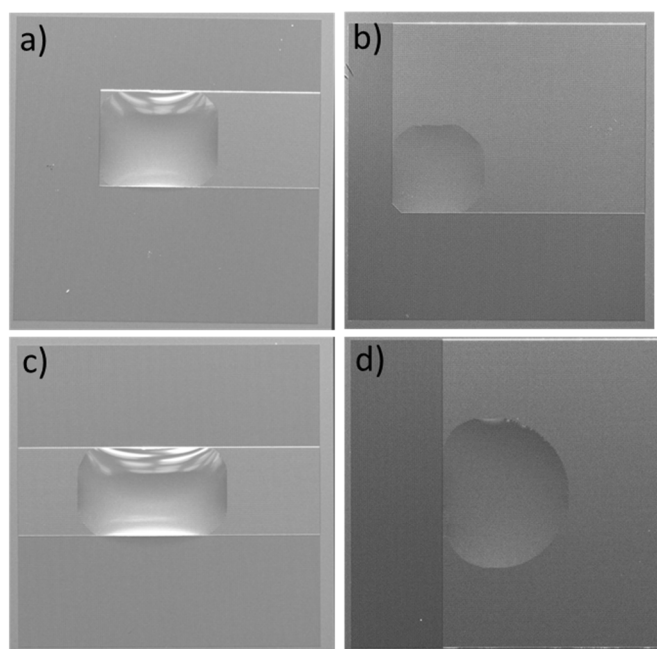
Advancing contact angles of hexadecane, tetradecane and dodecane (Sigma Aldrich, >99%) and deionized water were measured by the sessile droplet method (Theta, Biolin Scientific).

### Directional imbibition tests

A directional imbibition test was done by manually pipetting a 2 μl droplet of the chosen test liquid into the center of a 1 cm x 1 cm square shaped test area. After deposition, the droplet was given enough time to reach mechanical equilibrium, after which the end state was photographed. The majority of the experiments were done in a cleanroom environment at 21°C ± 0.5°C temperature and 45% ± 5% humidity. The exception is the experiment depicted in Fig. 1 and the supplementary videos, but these experiments were only used for illustration purposes.

## 3 Results and Discussion

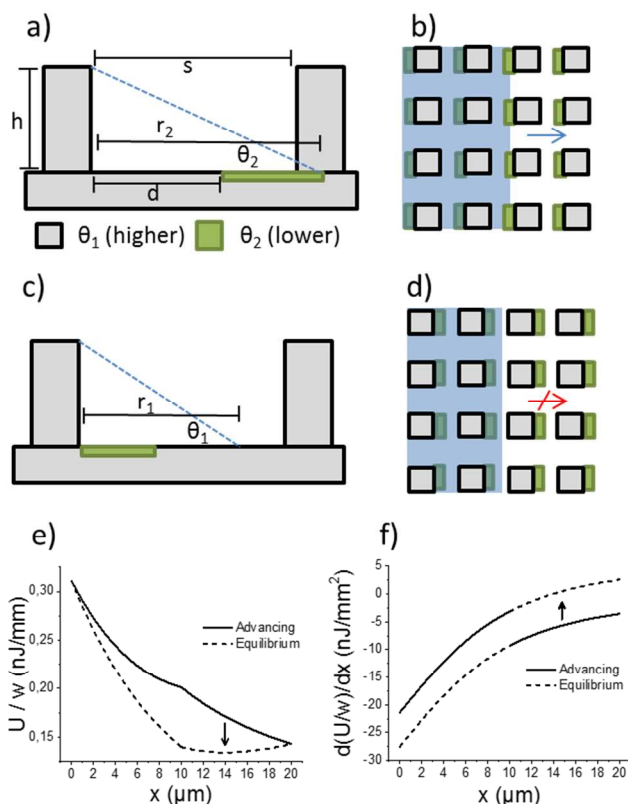
The four types of directional imbibition observed and discussed in this work are shown in Fig. 1. The four possible directions that the liquid can spread from the initial deposited droplet on the surfaces are: left, right, top and bottom. Various combinations of these lead to the four different types of directional imbibition. In Fig. 1a, the liquid only spreads right so we call this unidirectional imbibition (1D). In Fig. 1b, the liquid spreads toward right and top, so we call it bidirectional square imbibition (2Da). In Fig. 1c, the liquid spreads left and right, and we call it bidirectional line imbibition (2Db). Finally, in Fig. 1d, the liquid spreads top, bottom and right, and we call this type tridirectional imbibition (3D).



**Fig. 1** Four types of directional imbibition. a) unidirectional imbibition (1D) b) bidirectional square imbibition (2Da) c) bidirectional line imbibition (2Db) d) tridirectional imbibition (3D). All pictures depict a 1 cm x 1 cm square shaped test structure. The liquid is hexadecane in b, c and d and a 2:1 mixture of hexadecane and dodecane in a. The volume is 2μl.

### Mechanism

The mechanism of directional imbibition (movement of the liquid in-between the pillars) is explained in Fig. 2. The parameters of the system are chosen so that imbibition is energetically favourable to some directions while a local energy minimum stops the imbibition to other directions. This is achieved by utilizing a lithographically patterned surface energy pattern overlaid on top of square array micropillar topography. The micropillar array is characterized by two important parameters: the row to row spacing ( $s$ ) and the height of the array ( $h$ ). Two different surface chemistries are used. The first chemistry (marked grey in Fig. 2) has lower surface energy (higher contact angle,  $\theta_1$ ) and the second (marked green) has higher surface energy (lower contact angle,  $\theta_2$ ). The lower contact angle coating is patterned so that it is in contact with one pillar and extends partially toward the previous/next pillar row. The parameter to characterize the lower contact angle coating is  $d$ , the distance to the lower contact angle area from the previous pillar row (see Fig. 2a). The distance  $d$  is compared to the maximum spontaneous reach ( $r$ ) of the liquid meniscus from a row of pillars. We mark the maximum spontaneous reach on  $\theta_1$  as  $r_1$  and the maximum reach on  $\theta_2$  as  $r_2$  (see Fig. 2a and 2c).



**Fig. 2** Mechanism and parameters of directional imbibition. *a)* Advancing direction, side view. *b)* Advancing direction, top view. *c)* Equilibrium direction, side view. *d)* Equilibrium direction, top view. *e)* Surface energy landscape for the meniscus in the advancing direction (solid line) and the equilibrium direction (dashed line). *f)* Surface energy derivative

for the meniscus in the advancing direction (solid line) and the equilibrium direction (dashed line). The arrows in *e)* and *f)* indicate the pinning location.

This setup leads to asymmetric imbibition with a certain set of parameters. The direction depicted in Fig. 2a-b is called the advancing direction. The meniscus comes into contact with the more hydrophilic coating, which helps it reach the next row of pillars. The direction depicted in Fig. 2 c-d is called the equilibrium direction. The liquid meniscus finds an equilibrium position with the appropriate contact angle in the middle of two pillar rows.

Directional imbibition based on this mechanism is achieved when several conditions are fulfilled. First, the liquid should not get stuck in an equilibrium position in the advancing direction and second, the liquid should not spontaneously advance in the equilibrium direction. The first part is achieved when the following two conditions are fulfilled:

$$d < r_1, \quad (1)$$

and

$$s < r_2. \quad (2)$$

Eq. 1 guarantees that the liquid meniscus reaches the more hydrophilic surface chemistry ( $\theta_2$ ) while Eq. 2 guarantees that the meniscus moves from that point to the next pillar row. The final condition is that the liquid does not advance spontaneously to the equilibrium direction, which is achieved when:

$$s > r_1 \quad (3).$$

No expressions for the parameters  $r_1$  and  $r_2$  exist currently in the literature but they can be approximated by  $r_1 \approx h / \tan(\theta_1)$  and  $r_2 \approx h / \tan(\theta_2)$ . These approximations are based on assuming that a row of pillars has a similar meniscus as a uniform wall with the same height, which gives simply  $h / \tan(\theta)$ . However, it should be stressed that these approximations somewhat overestimate the values of  $r_1$  and  $r_2$  since it is known that a discontinuous line of micropillars does not support the meniscus quite to the same extent as a uniform wall<sup>14</sup>. With these approximations, the conditions for directional imbibition can be written as:

$$d < h / \tan(\theta_1), \quad (4)$$

$$s < h / \tan(\theta_2), \quad (5)$$

and

$$s > h / (\tan \theta_1). \quad (6)$$

Fig. 2e shows the total surface energy per unit length when the meniscus is advancing into both directions (see Supplementary for derivation). For calculating the figure, the following parameters were used:  $h = 11.3 \mu\text{m}$ ,  $d = 10 \mu\text{m}$ ,  $s = 20 \mu\text{m}$ ,  $\theta_1 = 39^\circ$ ,  $\theta_2 = 0^\circ$  and  $\gamma = 27.5 \text{ mJ/m}^2$ . Fig. 2f shows the derivatives  $dU/dx$  of the curves in Fig. 2e. In the advancing direction, the surface free energy steadily decreases until the meniscus reaches the next pillar row. However, in the equilibrium direction, the surface energy would start to increase once the

meniscus passes the equilibrium position at  $x \approx 14 \mu\text{m}$ . The reason for the equilibrium is that at  $x = 14 \mu\text{m}$ , the meniscus makes a  $39^\circ$  angle on the chosen  $11.3 \mu\text{m}$  height. The total surface energy change over the whole distance is the same into both directions (since the same surface area is covered in either direction), but the distribution over the length of the inter-pillar gap is different.

### Oil contact angle ranges, stability and pinning types

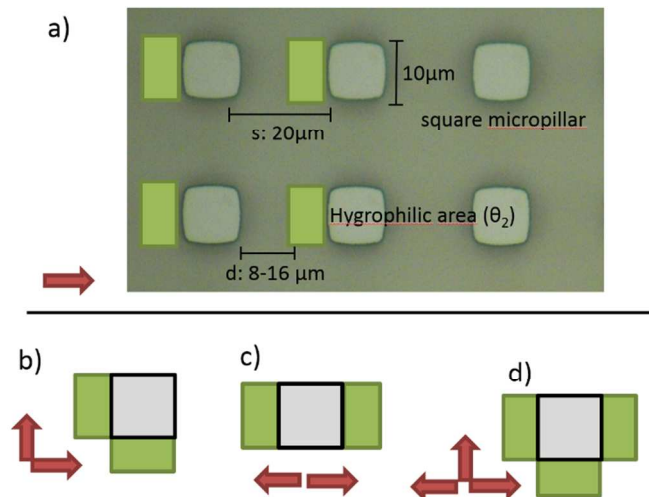
The contact line on a regular microstructure can get pinned in two ways as described by Blow and Yeomans<sup>19</sup>: either between pillar rows (connected contact lines) or in geometrical valves on areas where the front edge of the meniscus needs to advance (disconnected contact lines). Due to the low surface tension of oils, all oil contact angles in this work were  $<40^\circ$ . Because of this, the pinning observed in this work was always of the connected contact line type, as shown in Fig. 2c.

Another difference in contact angles between oils and water is the long term stability. For oils it is relatively easy to realize  $\theta_2$  that is stable over long times due to the low surface tensions of oils. We observed that a silicon surface oxidized by oxygen plasma remained nearly complete wetting for oils (advancing contact angle less than  $10^\circ$ , irregular droplet shapes) for at least two months when stored in a cleanroom environment. Similarly, the oil contact angles on the fluoropolymer  $\theta_1$  were stable due to the inertness of a fluorinated surface.

For water, it is not so easy to achieve long term superhydrophilicity at least on planar surfaces. Many naturally occurring completely wetting surfaces, such as noble metals and potentially rare earth oxides lose their hydrophilicity due to atmospheric hydrocarbon adsorption<sup>26</sup> and the hydrophobic recovery of plasma hydrophilized polymers is well known<sup>27</sup>.

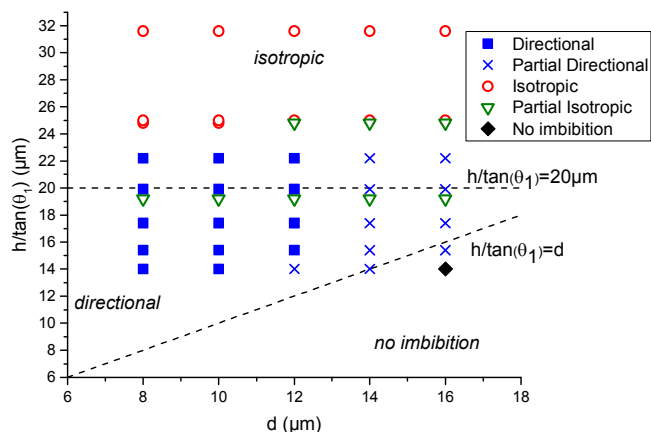
### Directional oil imbibition experiments

The geometries that we utilized in this study are shown in Fig. 3. The micropillar arrays consisted of  $10 \mu\text{m}$  times  $10 \mu\text{m}$  square pillars in a square lattice with the inter row spacing of  $20 \mu\text{m}$ . Three different heights were utilized:  $11.3 \mu\text{m}$ ,  $12.5 \mu\text{m}$ ,  $16.1 \mu\text{m}$ . Three different oils were tested: hexadecane ( $27.5 \text{ mJ/m}^2$ ), tetradecane ( $26.6 \text{ mJ/m}^2$ ) and dodecane ( $25.3 \text{ mJ/m}^2$ ). The more hydrophilic coating was completely wetting for all of the test oils so  $\theta_2 = 0^\circ$ . The advancing contact angles of the less hydrophilic area was depended on the oil used. The advancing contact angles ( $\theta_1$ ) were  $39^\circ \pm 2^\circ$ ,  $33^\circ \pm 2^\circ$  and  $27^\circ \pm 2^\circ$  for hexadecane, tetradecane and dodecane respectively. Finally, for all combinations above, we tested five different  $d$  values,  $8 \mu\text{m}$ ,  $10 \mu\text{m}$ ,  $12 \mu\text{m}$ ,  $14 \mu\text{m}$  and  $16 \mu\text{m}$ .



**Fig. 3** Geometries used in this study. The red arrows indicate the advancing directions of liquid. a) Micropillar array optical micrograph with overlaid geometrical parameters and the surface chemistry pattern for unidirectional wetting. b) Surface chemistry pattern for bidirectional square wetting. c) Surface chemistry pattern for bidirectional line wetting. d) Surface chemistry pattern for tridirectional wetting.

The results of the 45 different combinations of parameters (3 heights, 3 liquids, 5  $d$ -values) are summarized in Fig 4. The end states of the experiments were classified into 5 categories: Fully directional imbibition, partial directional imbibition, fully isotropic imbibition, partial isotropic imbibition and no imbibition. The criteria were as follows: an experiment was classified as fully directional if all four different imbibition types were directional in the manner shown in Fig 1. If only partial directional character (some structures worked but others did not or the imbibition stopped midway), the experiment was classified as partial directional. If all the samples filled to all directions regardless of the patterns, the experiment was classified fully isotropic. If the liquid mostly spread everywhere, except for a few directions, the experiment was marked partially isotropic. Finally, an experiment was classified as no imbibition if the liquid did not advance into any direction from the initial droplet. This process is further illuminated in supplementary Figure S1, which shows the end states of two experiments with the corresponding classifications.



**Fig. 4** Directional imbibition parameter map. The y-axis error bars of the experimental data points, resulting from the error margin of contact angle measurement, are omitted for clarity and lie between  $1.0 \mu\text{m}$ -  $2.9 \mu\text{m}$ . The hatched lines show theoretically derived dividing lines.

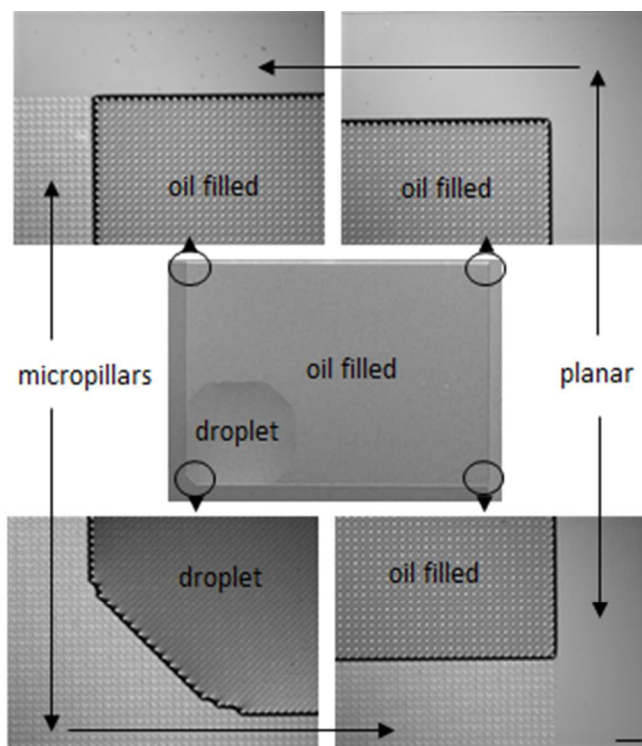
The directional imbibition parameter space is shown in Fig. 4. The parameter space is divided into three regions: isotropic imbibition, directional imbibition and no imbibition. The division is based on the conditions (1) - (3) which can be approximated by the conditions (4) - (6). On the coordinate system chosen for Fig. 4, condition (4) translates to  $h/\tan(\theta_1) > d$ , condition (5) is always satisfied since  $\theta_2 = 0$ , and condition (6) translates to  $h/\tan(\theta_1) < 20 \mu\text{m}$  (since the same spacing of  $20 \mu\text{m}$  was used for all tests). The main artifact of the approximation is that all of the datapoints in Fig. 4 are shifted upward with regards to the approximated conditions. This is because we approximated that  $r_1 = h / \tan(\theta_1)$  while in reality it is known that for a row of micropillars  $r_1 < h / \tan(\theta_1)$ <sup>14</sup>.

The experimental data matches the theoretical considerations above reasonably well. We observed strictly isotropic imbibition above roughly  $h/\tan(\theta_1) > 23 \mu\text{m}$ , as opposed to  $h/\tan(\theta_1) > 20 \mu\text{m}$  predicted theoretically. On the isotropic part of the parameter space, the pillar array is too high (or too hydrophilic) compared to the pillar row spacing. Because of this, the meniscus of the equilibrium direction is also able to reach the next row, resulting in isotropic imbibition. On the other hand, either no or only limited imbibition was observed when  $h/\tan(\theta_1) < 20 \mu\text{m}$ . Here, the height of the pillars is too low (or the contact angle too high) compared to the distance to the fully wetting area. Because of this, the meniscus of the advancing direction never reaches the  $\theta_2$  area and gets pinned. In-between these areas we observed directional imbibition with most parameters when  $d = 8 \mu\text{m}$ ,  $10 \mu\text{m}$  or  $12 \mu\text{m}$ . We never observed full directional imbibition when  $d = 14 \mu\text{m}$  or  $16 \mu\text{m}$ . The reason for this is unknown. We speculate that it could be due limitations in the development of the photoresist. The photoresist thickness is roughly the depth of the pillar array +  $6.2 \mu\text{m}$ , and as  $d$  increases, the size of the opening in the resist

decreases leading to high aspect ratios that could develop inefficiently.

Microscopy images of an end state of an experiment are shown in Fig. 5. The figure shows that the oil has advanced towards top and right until the micropillar array ends, while toward left and bottom the droplet did not move from the initial position. The droplet itself is located then in the bottom left corner (Fig 5c). The droplet edges sometimes made faceted shapes and sometimes straight  $90^\circ$  angles, as discussed by Courbin et al.<sup>13</sup> and our own previous work<sup>28</sup>.

The oil droplet itself does also spread from the initial contact position. If we consider that the imbibition has already happened, then the oil droplet is spreading on tops of the pillar on a composite surface comprised partly of the oil itself ( $f_1 = 8/9$ ) and partly of  $\theta_1$  ( $f_2 = 1/9$ ). Utilizing the Cassie formula<sup>9</sup> and a  $\theta_1$  of  $33^\circ$ , we get Cassie contact angle of  $\approx 11^\circ$ . This means that the oil droplet spreads to the imbibition directions until this angle is reached.



**Fig. 5** Microscopy images showing the end state of a directional oil imbibition experiment. The type of the structure is the 2Da (square) and the advancing directions were toward top and right. The parameters are  $h = 11.3 \mu\text{m}$ ,  $d = 8 \mu\text{m}$ ,  $\theta_1 = 39^\circ$  (hexadecane). The circles in the central image show the areas where the microscopy images are taken from. The scalebar (bottom right) is  $100 \mu\text{m}$ .

### The imbibition process

The liquid fills the micropillar topography by a two stage imbibition process. The meniscus first makes contact with the next pillar row (like shown in Fig. 2a) on a random spot. After contact is made at one point, the whole row is filled laterally.



This type of imbibition process is well known<sup>13</sup>, and its kinetics are mostly determined by the slow row to row movement step. The imbibition is driven by the negative capillary pressure and opposed by the viscous drag in the liquid. The capillary pressure is highly position (and direction) dependent for the directional imbibition surfaces. For the 1D imbibition, the capillary pressure as a function of  $x$  can be obtained from Fig 2f and the supplementary equations S6 - S9 by dividing with the layer thickness. For the 1D with  $h = 11.3\mu\text{m}$ ,  $d = 10\mu\text{m}$ ,  $s = 20\mu\text{m}$ ,  $\theta_1 = 39^\circ$ ,  $\theta_2 = 0^\circ$  and  $\gamma = 27.5\text{ mJ/m}^2$ , the pressure has its lowest value of  $\approx -280\text{ Pa}$  at  $x = 10\mu\text{m}$  in the advancing direction. The expression for 2Da is the same as for 1D. In the case of 2Db, the surface chemistry between pillar rows is divided into three parts: the first and the last ( $s-d$ )  $\mu\text{m}$  is covered by  $\theta_2$  and the area inbetween by  $\theta_1$  (when  $d < 10\mu\text{m}$  these areas overlap). The 3D case is a mix between the 1D and the 2Db.

Supplementary videos S1-S4 show the start of the filling processes (from the droplet application) for all four directional imbibition types. The videos are shot in 100 fps and are displayed in real time. The videos are from the same experiments whose end states are shown in Figure 1. It typically took less than 1s for the droplet to stop moving and after that 5s – 60s for the whole 1 cm x 1 cm test structure to be filled by capillary imbibition, depending on the wetting type, the parameters and also the location of the initial droplet.

We noticed that the filling rate was a much more variable parameter between samples than the final filling type. A tentative explanation is that small errors in the surface chemistry pattern alignment accuracy are expected to have a big effect in the minimum capillary pressure as explained above. However, small inaccuracies in the alignment are not expected to have an effect in the final filling result for most parameters, excluding those cases where  $r_1$  is very nearly the same as  $d$ .

#### Directional water imbibition experiments

All four types of directional imbibition were also achieved with water (see Supplementary Figure S2). The water experiments were performed on  $18.5\mu\text{m}$  high micropillars with otherwise identical geometries to the oil imbibition experiments. The advancing contact angle ( $\theta_1$ ) between water and the hydroxyl terminated silane was  $52^\circ$ . The oxidized silicon surface ( $\theta_2$ ) had a water contact angle of  $0^\circ$ .

#### Design implications

The directional imbibition mechanism explained in Fig. 2 and the results shown in Fig. 4 present a clear path for optimizing the robustness of the directional imbibition filling type. First, the more hydrophilic surface area ( $\theta_2$ ) should have as low advancing contact angle as possible in order for Eq. 5 to be fulfilled. There are no tradeoff considerations for this parameter.

The higher contact angle ( $\theta_1$ ) needs to be optimized alongside the height ( $h$ ), pillar spacing ( $s$ ) and distance to the more hydrophilic area ( $d$ ) in order to satisfy Eq. 4 and Eq. 6. In

addition to this,  $\theta_1$  needs to be low enough to sustain capillary imbibition in the pillar array. Conditions for the latter have been derived from an energy minimization point of view<sup>25</sup>. In previous experiments, we noticed that advancing contact angles of roughly  $55^\circ$  and below were able to sustain capillary imbibition on micro and nanopillar surfaces<sup>28</sup>. Above this limit the imbibition fronts easily get pinned between pillar rows even if global energy minimization considerations would favour filling. The pinning cutoff is likely related to the  $45^\circ$  degree limit of capillary flow into the bottom corners of the pillars that act as V-shaped wedges<sup>29</sup>. The flow in corners is a possible mechanism by which the meniscus can bypass geometrical pinning sites on pillar arrays.

In this study we kept  $s$  fixed at  $20\mu\text{m}$  and varied  $d$  from  $8\mu\text{m}$  to  $16\mu\text{m}$ . The results showed that the directional imbibition behavior was achieved reliably  $d$  values from  $8\mu\text{m}$  to  $12\mu\text{m}$ , so it is recommended to use these or even lower values. While  $d$  values lower than  $8\mu\text{m}$  were not tested, they can be expected to perform even more reliably and with faster kinetics. Lower  $d$  values also makes the fabrication procedure less demanding since the openings in the thick photoresist will be larger. The only tradeoffs of very low  $d$  values are that the tolerance for errors in aligning gets reduced and that the meniscus in the equilibrium direction comes to rest quite close to the next pillar row. With these considerations, the following set of parameters could be used as a guideline for achieving robust directional imbibition:

$$0 < d < h, \quad (7)$$

$$\theta_2 = 0^\circ, \quad (8)$$

$$\theta_1 < 45^\circ, \quad (9)$$

$$s > h / (\tan \theta_1). \quad (10)$$

These conditions are a sufficient, but not necessary, rewriting of Eqs. (4)- (6) taking into account the discussion about  $\theta_1$ ,  $\theta_2$  and  $d$  above.

In this study we kept the size of the micropillar fixed and altered the height, the contact angles and the  $d$  parameter. Due to the contact line pinning happening mostly between the pillar rows, we do not expect the pillar size to have a big effect on the phenomenon as long as the height and the spacing are kept the same. It is possible that there would be some deviations due to the fine structure of the advancing meniscus based on either the Laplace pressure of the meniscus<sup>19</sup> or the solid line fraction of the meniscus<sup>14</sup>.

#### 4. Conclusion

In conclusion, four different types of directional imbibition were demonstrated. The four types were all the possible cardinal direction combinations available on a square lattice. It might be possible to utilize e.g. a hexagonal array and expand on the ideas presented in this work to achieve an even wider array of directional imbibition types. The possibility to control the spreading directions could find use in combination with printing technologies as the typical ink has a surface tension much lower than water, down to the values of the test oils used in this work.

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## Notes and references

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