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Swelling-induced patterning in soft microchannels†

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We study the effect of inflation on the swelling-induced wrinkling of thin elastic membranes in a set-up that is commonly used to create microchannels in lab-on-chip applications. Using a combination of experiments and associated numerical simulations, we demonstrate that the out-of-plane deformation of the inflated membrane and the resulting anisotropic stress lead to two distinct instabilities as the swelling progresses. The membrane first develops small-amplitude wrinkles that retain the cross-channel symmetry. Their wavelength depends on the pressure and is set in a process similar to the axisymmetric buckling of pressurised, uni-axially compressed cylindrical shells. As swelling increases, the membrane undergoes a secondary instability during which the wrinkles coarsen into large-amplitude folds whose morphology can be controlled by the degree of pre-inflation. We elucidate the fundamental mechanisms responsible for this behaviour and explain how inflation can be used as a control mechanism in the manufacture of microchannels.

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1 Introduction

Soft structures, such as polymeric membranes and biological tissues, readily undergo deformations due to mechanical actuation and intermolecular interactions.^{1–6} The stresses induced by these deformations can initiate buckling instabilities which are particularly common if the structure is thin and becomes subject to in-plane compression. In many engineering applications buckling is undesired and its occurrence indicates mechanical failure. However, constructive use of such instabilities has recently brought an explosion of their applications in robotics,⁷ surface science (in wetting,⁸ adhesion,⁹ and friction¹⁰), electronics,¹¹ renewable energy,¹² bio-^{13,14} and nano-sciences.^{15–17}

The current study is motivated by the use of buckling instabilities for manufacturing patterned microchannels. In many lab-on-chip-type applications, the shape of the microchannels is important because it affects the flow and can therefore be used to enhance mixing,^{18,19} focus flow, and guide and sort particles.^{20–22} For example, compared to smooth-walled microchannels, the length scale of mixing can be reduced by an order of magnitude by introducing moderate

amplitude corrugations to the wall shape.¹⁸ One way of manufacturing patterned microchannels is to exploit buckle delamination due to swelling of a thin surface layer.²³ The swelling creates internal stresses which cause the layer to detach from an underlying substrate along regions of weakened adhesion created by a preparatory surface treatment. Takahashi *et al.*²³ performed a comprehensive experimental study to classify the different channel morphologies which can be produced by this procedure, using a thin hydrogel layer. They have found that, generally, the layer tends to detach from the low-adhesion regions by initially creating a microchannel with an axially uniform, symmetric cross-section. However, upon further swelling, the detached surface layer evolves *via* symmetry-breaking into worm-like patterns, characterised by the crest snaking between channel sides. This simultaneously breaks axial and cross-channel symmetries of the system, resulting in patterns with axial wavelengths comparable to the width of the low-adhesion regions. At even larger levels of swelling, such shapes become subject to further period doubling instabilities in which individual wrinkles merge with their neighbours, creating multiscale hierarchical structures of coarsened folds.²⁴ The resulting microchannels are delicate, but could be stabilised by adding a second tougher layer on top of the swollen channel, thus creating a “layer-stack device” capable of conveying fluids at large pressures.²⁵

Once delaminated, the behaviour of the detached surface layer studied in ref. 23 is similar to that of a horizontally pre-stressed, but otherwise unsupported membrane. Indeed, theoretical studies of a membrane’s response to increasing in-plane

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where the membrane has length $X(t)$, width $Y(t)$ and height $Z(t)$ at time t (see the inset in Fig. 1(d)). We measured it in experiments with a PDMS membrane floating freely in 20 cSt silicone oil. The swelling ratio C was found to be well described by an exponentially evolving function of t , *i.e.*

$$\frac{C(t)}{C_{\text{eq}}} = 1 - \exp\left(-\frac{t}{T}\right) \quad (1)$$

for a characteristic time $T = 14.3 \pm 0.2$ s, where $C(T) = C_{\text{eq}} = 0.152 \pm 0.008$ is its equilibrium value (Fig. 1(d)).

The membrane profiles before swelling and once the equilibrium swelling states were reached, were measured using a one-point profilometer (ConfocalDT 2421 measuring system with IFS2405-3 sensor, Micro-Epsilon) mounted on a 3D translation platform that translated at a speed of 2 mm s^{-1} . The relative accuracy of these measurements is comprised of a positional accuracy related to the translation stage and a depth accuracy related to the confocal device, each estimated to be $1 \mu\text{m}$. To measure the equilibrium swelling profiles, the excess oil covering the membrane had to be removed.

For more experimental details, see the ESI.†

2.2 Theoretical model

Following,²⁶ we model the membrane deformation using the Föppl-von Kármán (FvK) equations

$$P = \frac{Eh^3}{12(1-\nu^2)} \nabla^4 w - h \left[\frac{\partial}{\partial x} \left(\sigma_{xx} \frac{\partial w}{\partial x} + \sigma_{xy} \frac{\partial w}{\partial y} \right) + \frac{\partial}{\partial y} \left(\sigma_{yx} \frac{\partial w}{\partial x} + \sigma_{yy} \frac{\partial w}{\partial y} \right) \right], \quad (2)$$

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} = 0 \quad \text{and} \quad \frac{\partial \sigma_{yx}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} = 0. \quad (3)$$

Here w is the out-of-plane displacement of the membrane and $\sigma_{\alpha\beta}$ are the components of the in-plane stress tensor. Assuming a Hookean constitutive relationship, they are given by

$$\sigma_{xx} = \frac{E}{1-\nu^2} [e_{xx} + \nu e_{yy}] + \sigma_0, \quad (4a)$$

$$\sigma_{yy} = \frac{E}{1-\nu^2} [e_{yy} + \nu e_{xx}] + \sigma_0, \quad (4b)$$

$$\sigma_{xy} = \frac{E}{1+\nu} e_{xy}. \quad (4c)$$

In these equations, σ_0 is an isotropic pre-stress and $e_{\alpha\beta}$ is the in-plane strain tensor for the deformation relative to the stress-free isotropically swollen state, *i.e.*

$$e_{xx} = \frac{\partial u_x}{\partial x} + \frac{1}{2} \left(\frac{\partial w}{\partial x} \right)^2 - C, \quad (5a)$$

$$e_{yy} = \frac{\partial u_y}{\partial y} + \frac{1}{2} \left(\frac{\partial w}{\partial y} \right)^2 - C, \quad (5b)$$

$$e_{xy} = \frac{1}{2} \left(\frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x} + \frac{\partial w}{\partial x} \frac{\partial w}{\partial y} \right), \quad (5c)$$

where u_x and u_y are the in-plane displacements, and $h = h_0(1+C)$ due to the assumed isotropic swelling. We solved this system of equations numerically using our open source finite element library oomph-lib,^{36,37} assuming the membrane to be pinned at the boundaries of the microchannels; the use of clamped boundary conditions resulted in the same wrinkling patterns.

The model (2)–(5) is quasi-steady, and the membrane deformation for different values of P and C was obtained by numerical continuation. This was facilitated by the introduction of viscous forces of the form $-\mu w_t$ to the left hand side of eqn (2), where μ is a small positive damping factor. Starting from the steady solution of eqn (2)–(5) for given values of the parameters P and C , we incremented these parameters by a small amount and then time-stepped the equations until the kinetic energy of the membrane had become sufficiently small. The solution obtained by this procedure was then used as the initial guess for the solution of the steady equations, *i.e.* for $\mu = 0$.

3 Results & discussion

3.1 Deformation prior to buckling

Prior to the onset of wrinkling instabilities, the membrane deformation in the central part of the channel is relatively simple (see Fig. 2(a)) and approximately independent of the axial coordinate, x . If bending effects are neglected and the inflation/swelling of the membrane is assumed to induce a constant cross-channel tension, σ_{yy} , the membrane's cross section deforms into a circular arc, defined by a radius, R , and an opening angle θ . The axial and cross-channel strains in the membrane are then given by

$$e_{xx} = (1 - \nu^2)\sigma_0/E - C \quad \text{and} \quad e_{yy} = R\theta/a - 1 - C, \quad (6)$$

respectively. For small values of w_0/a , where w_0 is the vertical deflection in the centre of the channel, we have $\theta \ll 1$ and thus $R = w_0/2 + a^2/8w_0 \sim 1/w_0$, resulting in

$$\frac{P}{w_0} = \frac{8(1+C)h_0}{a^2} \left(\sigma_0 - \frac{EC}{1-\nu} + \frac{8E}{3a^2(1-\nu^2)} w_0^2 \right). \quad (7)$$

The relationship (7) is a variant of the classical ‘‘bulge model’’³⁸ that is frequently used to determine the constitutive properties of thin elastic sheets of large aspect ratio ($L/a > 5$). For small values of pre-stress and swelling ($\sigma_0/E, C \ll (w_0/a)^2$), eqn (7) predicts a cubic relation between pressure and deflection, $P \sim w_0^3$.

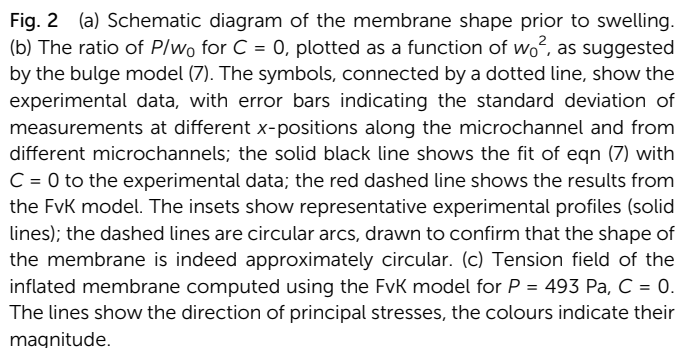
In the limit of small vertical deflections, we can also approximate the two principal stresses as

$$\sigma_{yy} \approx \frac{a^2 P}{8(1+C)h_0 w_0} \quad \text{and} \quad \sigma_{xx} \approx \nu \sigma_{yy} + (1-\nu^2)\sigma_0 - EC, \quad (8)$$

with the former being an approximation of Laplace's law.

For $C = 0$, eqn (7) simplifies to the standard form of the bulge model which suggests that a plot of P/w_0 as a function of

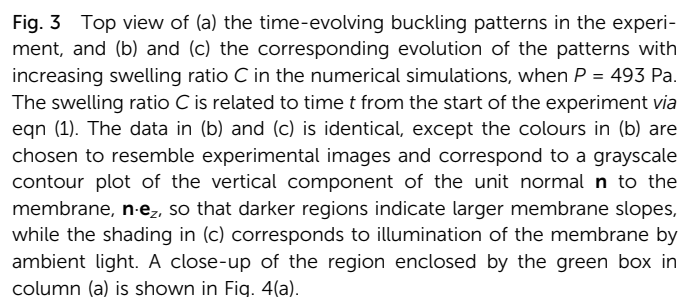




The insets of Fig. 2(b) show typical transverse membrane profiles measured using the confocal device (solid curves). Note that the measurements proved to be difficult in regions where the membrane had a large slope. As a result, in the top left inset only the data in the central part of the membrane was accessible. The dashed lines are circular arcs fitted to the experimentally measured profiles, from which the vertical displacements w_0 plotted in Fig. 2(b) were extracted. The plot confirms our assumption that the shape of the membrane's cross section resembles a circular arc.

3.2 Pattern evolution during swelling

Fig. 3 illustrates the deformation of the swelling membrane, pre-inflated by a pressure of $P = 493$ Pa, obtained experimentally (Fig. 3(a)) and in the corresponding numerical simulations (Fig. 3(b) and (c)). Here and in all remaining figures, top view images are cropped around the geometrical centre of the channel. Moving vertically down the columns, Fig. 3 shows that an increase in swelling leads to a transition between three distinct states: initially the membrane is inflated uniformly, with a symmetric vertical deflection across the channel and no variation along its length. The membrane then wrinkles in a varicose pattern, which breaks the axial uniformity but retains the cross-channel symmetry. As swelling increases, the amplitude of the initial wrinkles increases until a new coarser periodic pattern which breaks the cross-channel symmetry



emerges. The agreement between the experimental observations and the numerical results is pleasing, though it is noticeable that the axial wavelength predicted by the computations is slightly smaller than that observed in the experiments.

The green box in Fig. 3 identifies the smallest repeating unit in the final pattern obtained in the experiments. Fig. 4(a) provides a zoomed-in version of this region to show that the pattern has a hierarchical structure: the axial wavelength of the coarsened pattern, λ_{fold} , is equal to two wavelengths of the original wrinkling pattern, $\lambda_{\text{fold}} = 2\lambda_{\text{wrinkle}}$, but we also observe the formation of shorter wrinkles close to the boundary. To illustrate the spatial distribution of these patterns, we extracted the wavelength λ of the coarsened pattern at different y -coordinates (*i.e.* across the channel), as shown with the arrows in Fig. 4(a), and averaged this data along the channel length. The resulting wavelengths are shown in Fig. 4(b) where the error bars represent the standard deviation of the data. We observe intervals of approximately constant wavelength, connected by shorter intervals within which the wavelength adjusts from one generation of wrinkles to the next (see, *e.g.*, the data in the vicinity of $y/a = -0.3$). Three distinct plateaus in the value of λ emerge and are shown with gray shading to encompass data from repeated experimental runs. All plateau values are closely related to the wrinkling wavelength λ_{wrinkle} observed in the varicose pattern in Fig. 3(a). Fig. 4(b) also shows wavelengths extracted from the numerical simulation shown in Fig. 3(b) and (c). It is again noticeable that the axial wavelength predicted by the computations is slightly smaller than that observed in the experiments.

The transition between the three states in Fig. 3 can be understood by looking at the variation of three key quantities along the channel centreline: the vertical deflection, w , and the axial and cross-channel components of the membrane stress, σ_{xx} and σ_{yy} , respectively. Fig. 5(a)–(c) show a plot of these

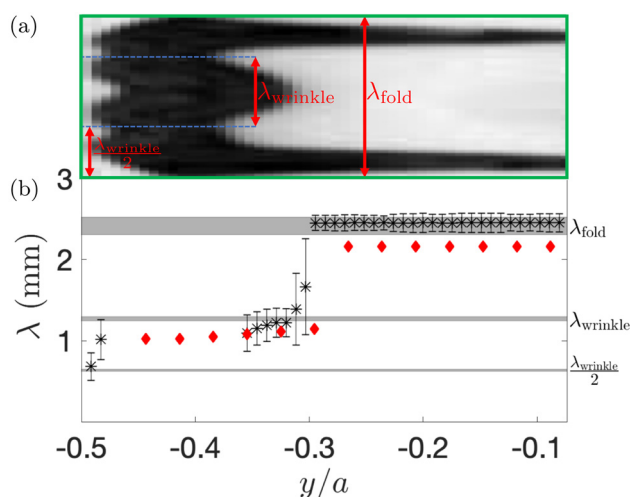


Fig. 4 (a) Hierarchical wrinkling within the smallest repeating unit of the “alternating folds” pattern, identified by the green box in Fig. 3, aligned with (b) the corresponding axial wavelength λ , plotted as a function of the cross-channel coordinate y ; data in (b) is obtained from experiments (stars) and the FvK model (diamonds).

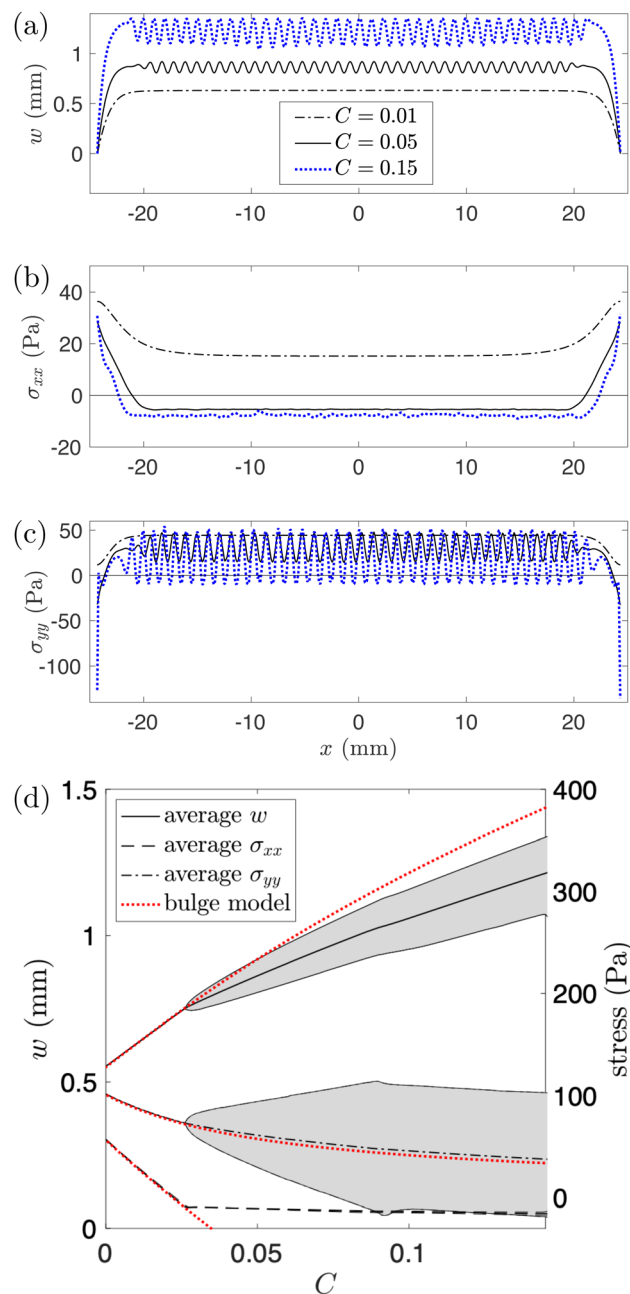


Fig. 5 (a) The deflection, w , (b) the axial stress, σ_{xx} , and (c) the cross-channel stress, σ_{yy} , along the channel centreline ($y = 0$) for $P = 493$ Pa and varying C . (d) The average (computed over the central part of the channel, $|x| < L/2 - \delta$) of the same three quantities, with lighter lines indicating the minimum/maximum of the relevant quantity with the range shaded. Corresponding predictions from the bulge model are shown with red dotted lines.

quantities, computed using the FvK model, for the same value of the pressure as in Fig. 3; different lines correspond to different values of C . In Fig. 5(d) we also show the maximum, minimum and average of these three centreline quantities over the central channel region for varying C , along with the corresponding predictions from the bulge model (eqn (7) and (8); dotted red lines).

Before the onset of wrinkling, the membrane deformation is well described by our bulge model (see Fig. 5(d)): as the swelling increases, the membrane's deflection becomes larger, leading to an increase in its transverse curvature. Since the pressure P is kept constant, Laplace's law (8) implies a reduction in the transverse stress, σ_{yy} , with an increase in C . Note that this mechanism for the reduction in σ_{yy} is different from the mechanism that operates in a flat membrane (*i.e.* for $P = 0$, the case analysed in ref. 26). In the latter case an increase in C leads to a linear reduction in σ_{yy} because swelling directly releases the pre-stress σ_0 ; for inflated membranes, the reduction in stress is indirect and leads to a different functional relation between σ_{yy} and C . In particular, prior to the onset of wrinkling, σ_{yy} always remains positive.

The change in axial stress σ_{xx} arises through a combination of the Poisson effect and the reduction in the axial strain e_{xx} due to the increase in swelling (see eqn (6)). This leads to an overall reduction in σ_{xx} with an increase in C .

As swelling increases, both principal stresses are therefore reduced and for a sufficiently large value of C the axial stress becomes negative. Once the axial compression is sufficiently strong the membrane wrinkles and thus reduces the compressive stress to a small, approximately uniform value; see the solid lines in Fig. 5(a)–(c) which show the three centreline quantities at $C = 0.05$, just past the onset of wrinkling. The initial wrinkling retains the cross-channel symmetry, resulting in the varicose pattern observed in Fig. 3. The axial variations in the vertical displacement, w , are directly translated into variations in the cross-channel membrane stress, σ_{yy} , because, compared to a uniformly inflated membrane, the membrane becomes more/less stretched along the peaks/valleys of the wrinkling pattern. Beyond the onset of wrinkling the average deflection and the axial stress deviate from the bulge model, with the latter remaining approximately constant with a further increase in C ; see Fig. 5(d). Conversely, the average of the cross-channel stress σ_{yy} , shown by the dash-dotted line in Fig. 5(d) remains close to the predictions from the bulge model, implying that, on average, the force balance in the membrane is still well described by Laplace's law.

Further swelling leads to an increase in the amplitude of the wrinkles. Thus the variation in the cross-channel stress increases until the minimum of σ_{yy} becomes negative, creating cross-channel compressive stresses in the valleys of the wrinkling pattern. Once these compressive stresses are sufficiently strong, they induce a secondary symmetry-breaking instability in which the compressed material in the valleys of the primary wrinkling pattern buckles in the transverse direction, thus breaking the cross-channel symmetry. Consecutive valleys buckle in opposite directions and remain separated by the peaks of the wrinkling pattern which retain their cross-channel symmetry, resulting in the coarsened patterns shown in Fig. 3, which we refer to as “alternating folds”.

3.3 Controlling patterns by varying pressure

We will now show that changes to the level of pre-inflation can be used to alter the wavelength and morphology of the buckling patterns.

For this purpose, we show in Fig. 6 a plot of the axial wavelength, λ_{wrinkle} , at the onset of wrinkling as a function of the pressure, P . The experimental data (indicated by circular symbols) was obtained by averaging the distance measured between consecutive valleys in the wrinkling pattern, with the vertical error bars representing the standard deviations of the data within each experiment, and repeated experiments shown as clusters of points. The corresponding numerical data is represented by the square symbols. Although the numerical predictions systematically underestimate the wavelength of the wrinkling pattern, the log-log plot of the same data in the inset shows that experiments and simulations both suggest a power-law behaviour for the dependence of the wrinkling wavelength on the pressure, with larger pressures resulting in shorter wavelengths.

To explain this, we exploit that, as demonstrated in Fig. 2, at the onset of wrinkling, the central part of the membrane resembles a sector of an axisymmetric circular cylindrical shell, subject to a compressive axial stress (equivalent to σ_{xx}) and a tensile hoop stress (equivalent to σ_{yy}). In the classical literature on axisymmetric buckling of cylindrical shells under this load,²⁸ the wavelength of buckling $\lambda_{\text{buckle}}^{[\text{shell}]}$ is shown to depend on their radius R

$$\lambda_{\text{buckle}}^{[\text{shell}]} \propto \sqrt{R}. \quad (9)$$

We have demonstrated above that, for moderate values of the vertical deflections at the centre of the channel, w_0 , the radius of the inflated membrane is $R \sim 1/w_0$ and the pressure follows a relationship $P \sim w_0^3$. Combining this with eqn (9) and assuming that $\lambda_{\text{wrinkle}} \approx \lambda_{\text{buckle}}^{[\text{shell}]}$ yields

$$\lambda_{\text{wrinkle}} \sim P^{-1/6}, \quad (10)$$

consistent with the experimental and numerical results (see inset to Fig. 6). Thus, pressurisation of the membrane prior to swelling provides an easy and reliable way to control the axial wavelength of the initial wrinkling pattern.

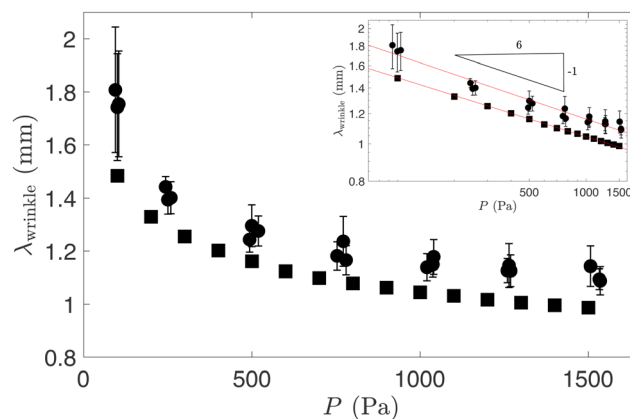


Fig. 6 The initial wrinkling wavelength, λ_{wrinkle} , as a function of the pressure P in experiments (circle) and numerical simulations (square). The inset shows the same data on a log-log scale with lines corresponding to power law fits to the data.



Next we analyse the effect of varying the pressure on the transition between the different buckling patterns. For this purpose we introduce the quantities M_x and M_y , where

$$M_x = \frac{1}{a^2} \int_{-L/2+\delta}^{L/2-\delta} \int_{-a/2}^{a/2} \left[\frac{\partial w}{\partial x} \right]^2 dy dx \quad (11)$$

is a measure of the axial non-uniformity of the deformation, while

$$M_y = \frac{2}{a^4} \int_{-L/2+\delta}^{L/2-\delta} \int_{-a/2}^{a/2} [(w(x, y) - w(x, -y))]^2 dy dx \quad (12)$$

provides a measure of the extent to which the deformation breaks the cross-channel symmetry.

In Fig. 7 we plot $M = M_x + M_y$, computed from the numerical solution of the FvK equations, as a function of C for various pressures. Initially both M_x and M_y are zero but as swelling increases, M_x increases sharply when we reach the primary wrinkling instability (at the points marked by the square symbols) which induces axial variations throughout the length of the membrane. Following the onset of the primary instability, M_x continues to increase as the amplitude of the wrinkling pattern grows. M_y is initially zero but then increases sharply when the secondary cross-channel symmetry-breaking instability occurs (at the points marked by the circular symbols). Given the inevitable imperfections it is difficult to establish unambiguously at which point the transition between the three patterns occurs in the experiments. However, the insets in Fig. 7 show that the experimentally observed patterns fall into the ranges of C predicted by the FvK equations.

To explain how variations in pressure affect the value of C at which the instabilities that cause the transition between the different patterns arise, we recall that if the membrane is subjected to a larger pressure, the associated pre-swelling

tensile membrane stresses increase like $\sigma_{xx} \sim \sigma_{yy} \sim P/w_0 \sim P/P^{1/3} \sim P^{2/3}$ (see eqn (8)). Wrinkling only occurs when swelling has reduced the axial membrane stress σ_{xx} in the central part of the membrane to just below zero; see Fig. 5(a). Hence, an increase in P will delay the onset of the wrinkling instability to larger values of C . This is consistent with the observations in Fig. 7. The same applies to the onset of the secondary instability, and hence an increase in P results in an increasing separation between the two critical points in Fig. 7. Conversely, a reduction in pressure implies that both instabilities not only occur at smaller values of C but that their onsets approach each other. As $P \rightarrow 0$ we therefore recover the behaviour described in ref. 26: without pre-inflation the initial wrinkling pattern breaks the axial uniformity and the cross-channel symmetry simultaneously.

An increase in pressure not only delays the onset of the secondary instability but it also affects the coarsened patterns that emerge. This is illustrated in Fig. 8 where we show experimental observations of the final, fully-swollen membranes at three different values of the pressure. For $P = 493$ Pa we obtain the alternating folds, which we already discussed in detail. However, for a larger pressure of $P = 1020$ Pa, we observe the appearance of isolated “connected folds” which develop when one of the valleys in the initial wrinkling pattern grows inwards while relaxing the amplitude of the adjacent wrinkles. For this value of the pressure, the connected folds occur randomly within the remaining alternating folds, so we refer to such patterns as “mixed folds”. For yet larger pressures, e.g. $P = 1259$ Pa in Fig. 8, the connected folds completely replace the alternating pattern. Their axial spacing is not random: since they emerge from the initial wrinkling pattern, the distance between any two subsequent connected folds is close to an integer multiple of λ_{wrinkle} .

The transition between the alternating and connected fold regimes is quantified in Fig. 9 where we plot the ratio $\lambda_{\text{fold}}/\lambda_{\text{wrinkle}}$ as a function of the pressure. The wavelengths were measured as in Fig. 4, except for the mixed folds regime, for which they were measured separately in the regions of connected and alternating folds. For smaller pressures, we obtain

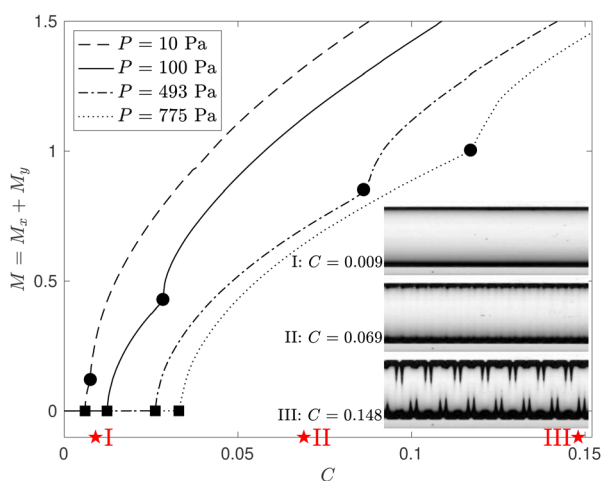


Fig. 7 The combined norm, $M = M_x + M_y$, where M_x and M_y are defined in eqn (11) and (12), respectively, as a function of the level of swelling, C , for four different pressures, P . The onset of wrinkling and the secondary symmetry-breaking instability are identified by square and circular markers, respectively. The insets show experimental images at $P = 775$ Pa for three values of C , as marked with stars on the C -axis.

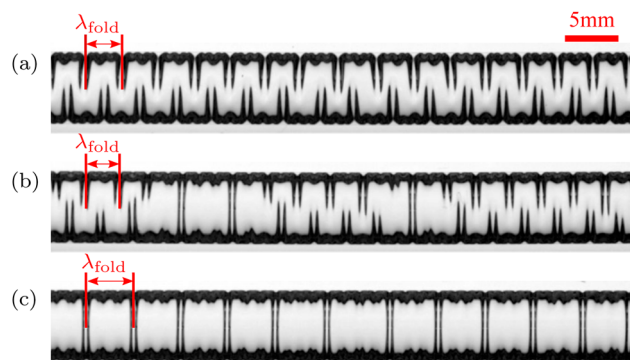


Fig. 8 The swelling patterns in experiments with soft microchannels that were pre-inflated by imposing a constant pressure (a) $P = 493$ Pa, (b) $P = 1020$ Pa and (c) $P = 1259$ Pa, resulting in (a) alternating, (b) mixed and (c) connected folds after coarsening, respectively.



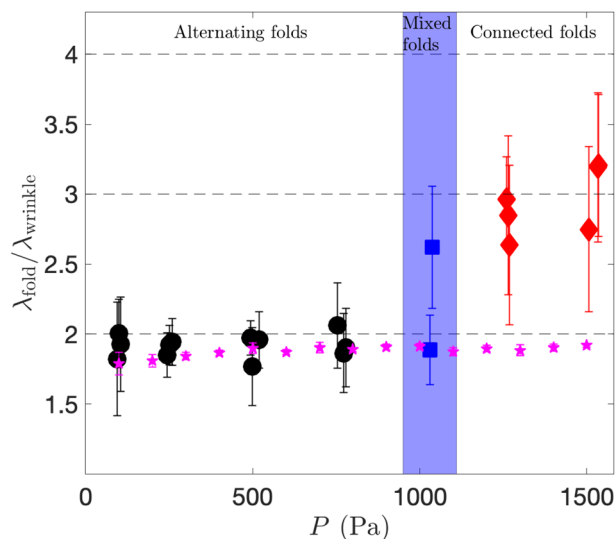


Fig. 9 The wavelength ratio $\lambda_{\text{fold}}/\lambda_{\text{wrinkle}}$ as a function of the pressure P for different types of coarsened patterns obtained experimentally, and the alternating folds obtained numerically (stars).

$\lambda_{\text{fold}} \approx 2\lambda_{\text{wrinkle}}$, characteristic of the period doubling underlying the formation of the alternating folds. For larger pressures we find that the dominant wavelength of the coarsened pattern, which corresponds to the average distance between two connected folds, is about three wavelengths of the original wrinkling pattern.

Interestingly, we were not able to reproduce the connected folds in our numerical simulations. For the pressures for which connected folds are observed in the experiments, the FvK-based computations show that the induced cross-channel stress σ_{yy} is so large that the development of alternating folds is delayed to values of C that exceed the equilibrium value C_{eq} . The computations therefore result in a finite-amplitude wrinkling pattern whose wavelength remains close to λ_{wrinkle} , without any coarsening. This suggests that the instability that leads the development of the connected folds involves constitutive and/or geometrical non-linearities that are not represented in our theoretical model. It would be possible to account for those rationally using a more complicated plate model, such as the Koiter-Steigmann model,^{39,40} but this is beyond the scope of our paper. For the alternating folds formed in the numerical simulations, we find $\lambda_{\text{fold}} \approx 2\lambda_{\text{wrinkle}}$ at all values of P , see Fig. 9. (The error bars, which correspond to the standard deviation of the data, quantify mesh-induced perturbations to the wavelengths).

All the results presented so far were obtained by allowing the membrane to swell to its saturation while keeping the pressure constant; the value of the pressure determined the morphology of the final pattern that arises from this process.

Fig. 10(a) demonstrates that it is possible to initiate the transition between the different coarsened regimes by adjusting the pressure a posteriori, *i.e.* after the membrane has reached its fully-swollen state. The figure shows a sequence of membrane shapes, starting with the alternating folds state

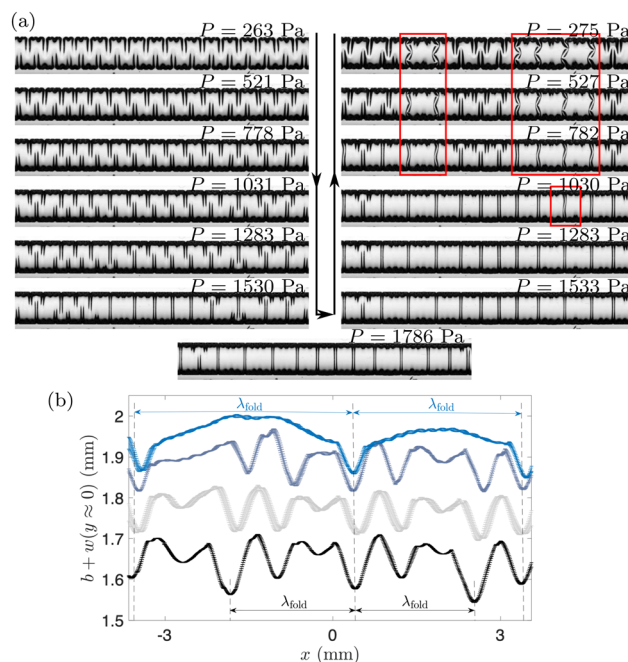


Fig. 10 Transition from alternating folds to connected folds and back in experiments with a membrane that is fully swollen at $P = 263$ Pa and subjected to increasing (arrow down) and then decreasing (arrow up) pressure. Red rectangular boxes identify regions of frustrated patterns not seen in Fig. 8. (b) The axial cross-sectional profiles of the membrane during the transition from alternating to connected folds, characterised by the wavelength λ_{fold} as indicated, for $P = 240$ Pa, 750 Pa, 1241 Pa and 1488 Pa (bottom to top) in experiments equivalent to (a).

which was reached after swelling the membrane at a constant pressure of 263 Pa (top left). A slow increase in pressure (down the left column) leads to a quasi-steady transition to mixed folds, and ultimately to the connected folds pattern (at $P = 1786$ Pa). A subsequent reduction in pressure (upwards along the right column) then returns the deformation back to an alternating folds pattern. Comparison of the inflation/deflation phases indicates the presence of hysteresis: the pressure at which the mixed fold pattern appears during pressurisation is larger than the pressure at which it disappears during deflation; furthermore, during deflation, localised frustrated patterns (highlighted by red boxes) are formed. Both are likely to be consequences of the patterns representing local minima in strain energy in a highly nonlinear system that, for a given pressure, has many alternative nearby equilibria. However, overall the results in Fig. 10 suggest that swelling and inflation can be considered as approximately independent processes – consistent with the assumptions of our theoretical model, where we have ignored any feedback to the swelling from the sheet deformation.

We note that the patterns formed in these experiments are visibly imperfect. For example, the profiles in Fig. 10(b) near the channel centreline, measured in experiments analogous to the ones in Fig. 10(a), show the membrane deflection along the channel length for various P , for which the patterns change from alternating ($P = 240$ Pa) to connected folds ($P = 1488$ Pa).



While λ_{fold} is still identifiable in all the data, undulations of higher wavenumber are also seen in the alternating folds patterns; these are caused by the rearrangement of hierarchical structures with increasing pressure. By contrast, the centreline profiles associated with connected folds appear to be more regular. For this pattern, valleys are connected by bulging regions of the membrane, which relax some of the wrinkles observed at smaller values of the pressure. The position of the valleys stays approximately the same in all experiments irrespective of the value of P , once again illustrating the importance of localisation during this pattern development.

4 Conclusion

We have studied the pattern formation in pre-inflated swelling membranes mounted on the upper boundary of a micro-channel. We showed that the inflation creates a disparity in the magnitudes of the principal stresses which leads to the occurrence of two distinct instabilities as the swelling increases while keeping the pressure constant: the uniformly inflated membrane first becomes unstable to regular small-amplitude varicose wrinkling, which is analogous to the axisymmetric buckling of pressurised, uni-axially compressed cylindrical shells.²⁸ As the swelling increases further, the initial wrinkling pattern is coarsened via a secondary instability. We showed that variations in pressure not only allow us to control the axial wavelength of the emerging patterns (an increase in pressure reduces the wavelength by nearly a factor of two in the range of studied pressures), but that the pressure also determines the coarsened patterns that emerge in the secondary instability: for modest pressures, the initial wrinkling pattern undergoes a transition to an “alternating folds” pattern which breaks the cross-channel symmetry; at larger pressures the wrinkling pattern coarsens into “connected folds” which retain the cross-channel symmetry. This behaviour is different from that observed in initially flat incompressible membranes for which the instability that breaks the axial non-uniformity also breaks the cross-channel symmetry, see, e.g. ref. 26. Therefore, inflation of the membrane prior to swelling allows control over the wavelength and morphology of the emerging patterns, providing a useful additional tool in designing and manufacturing soft microchannels and augmenting methods explored by ref. 23 and 25 for flat unpressurised membranes. Using the techniques from ref. 25, our microchannels could be stabilized to create layer-stack devices, which are capable of conveying fluids at large pressures, and are therefore useful in mixing, flow focusing and particle sorting applications.^{18–22} Earlier works have already demonstrated benefits of using swelling for designing and manufacturing of patterned microchannels over more traditional methods in which the channel shape is ‘frozen’ early in the production. Our study suggests new opportunities for robustly producing corrugated microchannels by providing a pathway to a range of patterns that are otherwise inaccessible.

Author contributions

H. L., A. J. and D. P.-P. designed research; H. L., A. R., M. H. and D. P.-P. performed research; and H. L., A. R., A. J., M. H. and D. P.-P. wrote the paper.

Conflicts of interest

There are no conflicts to declare.

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