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Design parameter optimization of a membrane reactor for methanol synthesis using a sophisticated CFD model†

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Carbon capture and utilization technologies are considered crucial in reducing carbon dioxide levels in the atmosphere and mitigating climate change. One of the most promising utilization options is the catalytic hydrogenation of the captured carbon dioxide to methanol. However, this reaction requires large energy-consuming recycles due to the limitation of the chemical equilibrium. To shift the chemical equilibrium and increase per-pass conversion, membrane reactors that remove the produced water from the reaction zone can be applied. A sophisticated CFD model of the membrane reactor with a NaA zeolite membrane is developed, to identify key constructive and operating parameters. The model implements the Maxwell–Stefan approach for permeation that considers the complex behavior of pervaporating water–alcohol mixtures through microporous zeolite membranes. In a full-factorial design of experiment, two general categories of parameters (ratio between reaction and permeation, permeation driving force) that influence conversion and yield in membrane reactors are identified that need to be optimized in construction and operation. In the most promising configuration, the application of the membrane reactor results in an increased CO_2 conversion of 20.6% and a 16.0% enhanced methanol yield compared to an equivalent conventional reactor. With the findings of this study, key parameters for the general optimization of the construction and operation of membrane reactors for industrial applications are identified.

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1 Introduction

According to the Intergovernmental Panel on Climate Change (IPCC), human emission of greenhouse gases (GHGs) has unequivocally led to global warming.[1] In the last 50 years, the global surface temperature has been increasing faster than in any other comparable period of time over the last 2000 years due the consumption of fossil fuels for energy production and transportation.[1] As a consequence, the frequency as well as the intensity of heat waves, heavy precipitation events, and droughts have increased, causing substantial damage and irreversible loss in global ecosystems.[1]

To reduce the atmospheric level of carbon dioxide (CO_2) as the main anthropogenic GHG and mitigate global warming, carbon capture and storage (CCS) is considered a crucial technology by permanently sequestering CO_2 in geological storages such as aquifers.[1–3] Alternatively, carbon capture and utilization (CCU) is gaining significant attention by recycling CO_2 and providing non-fossil carbonaceous feedstocks to industry.[3,4] Catalytic hydrogenation of captured CO_2 to methanol (CH_3OH) is one of the most promising CCU pathways because of its high revenue stream, partially recovering the costs of capturing CO_2, and its technological maturity.[3–5]

With an estimated market size of 43.91 billion U.S. dollars in 2024, CH_3OH is a versatile chemical feedstock as precursor to acetic acid (7% of total CH_3OH demand), formaldehyde (23%), methyl *tert*-butyl ether (MTBE) (11%), and olefins (31%).[6,7] Due to the liquid state of CH_3OH at ambient temperature and the related simple handling, it is also discussed as an alternative fuel (17%) as well as a potential chemical energy storage for fluctuating renewable energy sources.[7,8]

The formation of CH_3OH proceeds predominantly *via* CO_2 hydrogenation following eqn (1a), even when using carbon monoxide (CO) rich feedstock.[9] Thus, the hydrogenation of CO according to eqn (1b) occurs scarcely. The reverse water–gas shift (RWGS) reaction shown in eqn (1c) denotes the competing conversion of CO_2 to CO by consumption of hydrogen (H_2). The stoichiometric ratio indicates that a H_2 to CO_2 feed gas ratio of

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3 to 1 is optimal for the process.[9] A higher CO_2 concentration inhibits CH_3OH synthesis due to a rise in water (H_2O) formation following the RWGS reaction.[9] Due to the exothermicity and the volume decrease of the hydrogenation reaction, CH_3OH synthesis is favored by low temperatures and elevated pressures.[9] The endothermic RWGS reaction expedites the formation of the undesired by-products CO and H_2O, reducing CH_3OH selectivity.[4]

$$CO_2 + 3H_2 \rightleftharpoons CH_3OH + H_2O \quad \Delta H_R = -49.5 \text{ kJ mol}^{-1} \quad (1a)$$

$$CO + 2H_2 \rightleftharpoons CH_3OH \quad \Delta H_R = -90.7 \text{ kJ mol}^{-1} \quad (1b)$$

$$CO_2 + H_2 \rightleftharpoons CO + H_2O \quad \Delta H_R = 41.2 \text{ kJ mol}^{-1} \quad (1c)$$

Historically, industrial-scale CH_3OH synthesis was performed at high pressures (250 bar to 350 bar) and temperatures (320 °C to 450 °C).[9] Due to catalyst advances in the 1960s, today, lower operational pressures of 50 bar to 100 bar and temperatures of 200 °C to 300 °C are sufficient for CH_3OH production.[9]

Commercially, heterogenic copper/zinc-oxide (Cu/ZnO) catalysts on supports such as alumina (Al_2O_3) designed for the hydrogenation of synthesis gas to CH_3OH are used to convert CO_2 feedstock.[9,10] Specialized catalysts using main group metal oxides (*e.g.* In_2O_3), intermetallic composites (*e.g.* Ni–Ga), or nanostructured supports (*e.g.* metal oxide frameworks (MOFs)) are potential candidates for the promotion of activity, selectivity and stability in CO_2 hydrogenation to CH_3OH.[10]

Two main challenges have to be addressed during reactor design for CH_3OH synthesis. First, the formed heat of the reaction needs to be removed economically.[9,11–13] Industry has come up with a variety of possible solutions, including the generation of medium-pressure steam in a steam-raising fixed bed reactor (*e.g.* Lurgi tubular reactor) or preheating the feed with the generated reaction heat (*e.g.* ICI tube-cooled converter). Affiliating, several companies have combined both solutions to reduce the overall heat demand as well as the operating costs by effective energy integration in two coupled reactors (*e.g.* Johnson Matthey Combi Loop, Mitsubishi Superconverter, Lurgi MegaMethanol).[9,11–13] A summary of operating reactor concepts is provided in several reviews.[9,11–14]

Second, due to the chemical equilibrium of the hydrogenation reactions, single-pass CH_3OH yield is limited.[12] Compared to the conventional CH_3OH synthesis from synthesis gas, the use of CO_2 as feedstock decreases the single-pass conversion even more, resulting in an even higher recycle duty and consequently higher operating costs.[15] In literature, several concepts have been experimentally tested or simulated to shift the chemical equilibrium and decrease the required compression duty by removing reaction products. Bos *et al.* achieved a carbon yield above 99.5% using a small laboratory scale reactor with liquid-out-gas-in concept (LOGIC). By lowering the temperature above the catalyst bed, H_2O and CH_3OH are condensed and unreacted gases are recycled back into the catalyst bed *in situ*.[16,17] A different approach is taken by Kuczynski *et al.*, who were able to achieve full conversion in one pass by incorporating CH_3OH adsorbing silica-alumina particles into the catalytic fixed bed. These so-called sorption-enhanced reactors are frequently discussed in literature and show potential for enhanced carbon conversion. In a simulative study, Arora *et al.* present a H_2O adsorbing NaX zeolite sorption-enhanced reactor that increases CH_3OH yield compared to a traditional reactor (TR) by 8.17%.[18,19] Another approach to shift the chemical equilibrium is introducing a permselective membrane into the reaction zone that removes one or both reaction products. Thus, improving CO_2 conversion, CH_3OH selectivity, and CH_3OH yield with less recycling effort than TRs; potentially decreasing the reactor's size, energy demand, and ultimately costs.[20,21] Struis *et al.* first provided proof of the benefit of using membrane reactors (MRs) for CH_3OH synthesis in 1995.[22] A perfluorinated cation exchange Nafion membrane separates the reaction products, resulting in an increase of CH_3OH yield by 2.5% compared to a TR.[22] However, as Nafion is not stable at temperatures above 205 °C, different membrane materials have been investigated.[22,23] In 2003, Gallucci *et al.* published their work on MRs for CH_3OH synthesis implementing an A-type zeolite membrane that separates H_2O and CH_3OH. With an increase of CO_2 conversion of 6.3% compared to a TR, Gallucci *et al.* state that the same conversion rates can be achieved at lower operating conditions in a MR. However, due to the necessity of pore condensation for permeation, the operating parameters should not surpass the critical parameters of CH_3OH.[24] Tran *et al.* applied a MR with a NaA zeolite membrane manufactured by the Frauenhofer Institute for Ceramic Technologies and Systems (IKTS) at low pressures between 3 and 7 bar reporting an increased CH_3OH space time yield compared to a TR.[25] Li *et al.* also adopted a NaA zeolite membrane in a small-scale reactor and obtained a CO_2 conversion of up to 61.4% with an increase in CH_3OH yield of up to 38.9%. Demonstrating a 95% *in situ* removal of H_2O, Li *et al.* state to have achieved the highest space time yield published for CH_3OH synthesis from CO_2 hydrogenation in literature.[26]

Several researchers have investigated additional materials for membranes in CH_3OH synthesis, revealing the great potential to increase per-pass conversion.[21,27,28] However, there is a lack of research concentrating on the actual realization of MRs for CH_3OH synthesis and the in-depth optimal reactor design as well as operating principle.

For simplified reactor prototyping, computational fluid dynamics (CFD) is a fast and cost-effective approach that allows the analysis of the influence and interactions of constructive and operating parameters. In literature, several mathematical models regarding CH_3OH synthesis in MRs exist, investigating the behavior of the reaction with various membranes and operating conditions. Samimi *et al.* analyse the potential of MRs in the CAMERE process, that combines CH_3OH synthesis with a prior RWGS reactor. By implementing an hydroxy sodalite (H-SOD) membrane in the two-dimensional simulation, the CH_3OH production rate was increased by 20.8%.[29] Thermodynamic analysis of a MR for CH_3OH synthesis from Barbieri *et al.* shows significant increase in conversion, selectivity and yield.[30] Ountaksinkul *et al.* compare different MR constructions with two-dimensional CFD models revealing the

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potential of planar micro-structured MRs for CH_3OH synthesis.[31] Hamedi *et al.* present a one-dimensional model of a H-SOD MR for CH_3OH synthesis that incorporates back diffusion of permeated species. An increase in CO_2 conversion is shown when implementing a non-adiabatic over an adiabatic MR. However, both MRs result in an improved conversion compared to a TR.[32] A general approach for the design of MRs to enhance thermodynamically-limited reactions is provided by Huang *et al.* For reactor optimization, the dimensionless parameter DaPe (Damköhler Péclet) is introduced describing the compatibility of the reaction kinetics and the permeation flux. Applied to the dry reforming of methane and the RWGS reaction, reactor geometry and operating principles are improved, resulting in an increased conversion.[33]

All aforementioned models use simple descriptions of product permeation implementing empirical equations for H_2O permeance with permeability coefficients and partial pressure differences. Thereby, the interactions between competing permeating species are overlooked, resulting in an inaccurate description of permeation and, eventually, an improper analysis of MRs for CH_3OH synthesis. In this work, a sophisticated novel approach for the description of reactant and product permeation in a MR for CH_3OH synthesis is adopted based on the permeation model of Maxwell–Stefan (M–S) that considers the findings of Krishna and van Baten concerning the distinct characteristics of pervaporating water–alcohol mixtures in zeolite membranes.[34–36] The approach incorporates the interactions between different permeating species by considering all individual species in the mixture, the forces applied to them, and the resulting induced motions.[34,35] Accounting for the interactions between species is particularly crucial in water–alcohol mixtures, where coupling effects significantly impact permeation, resulting in the inapplicability of unary diffusion coefficients, the uncoupled M–S formulation, and Vignes interpolation.[37] With the more general M–S approach, the model can be easily adapted to different applications, as the model, as well as the coefficients, are independent of the reference frame.[34,36] Additionally, as permeation is a function of temperature, a vant Hoff-type temperature dependence is incorporated for the adsorption model, and an Arrhenius-type temperature dependence is adopted for the diffusion model. Hence, a more comprehensive depiction of multicomponent diffusion through the membrane is applied, resulting in a more accurate analysis of MRs for CH_3OH synthesis.[36]

Using the aforementioned novel approach, the objective of this work is to:

- Implement the novel more detailed permeation model based on the M–S approach in a comprehensive CFD model.
- Improve the understanding of the key parameters that affect CO_2 conversion and CH_3OH yield in the examined MR.
- Reveal an optimal construction and operating guide for improved CH_3OH synthesis in a MR with a NaA-gated water-conducting membrane.
- Create a systematic approach for virtual prototyping of MRs that can be applied for optimization of various applications.

2 Modelling

The simulated membrane reactor (MR) employs a commercial copper–zinc-oxide–alumina (CZA) catalyst and the microporous NaA zeolite membrane developed by Li *et al.*[26] The computational fluid dynamics application Ansys Fluent 2022 R1 is used to create a three-dimensional simulation of the MR. Reaction and permeation are integrated within two user-defined-functions (UDFs).

2.1 Geometry and mesh

The MR is designed as a tube-in-tube reactor running in counter-current with an inner membrane and an outer wall as shown in Fig. 1. As thermal boundary conditions, the inside and outside of the membrane are thermally coupled and the outer wall has a constant temperature corresponding to the operating temperature. The synthesis gas feed flows over the catalyst bed between the membrane and the outside wall, whereas the purge gas sweep flows inside the membrane in the opposite direction to maximize the partial pressure difference along the reactor, enhancing permeation. Thus, the inlets as well as the outlets of the synthesis gas and purge gas streams are situated on opposite ends of the reactor. The computer-aided-design (CAD) program SpaceClaim is used to create a

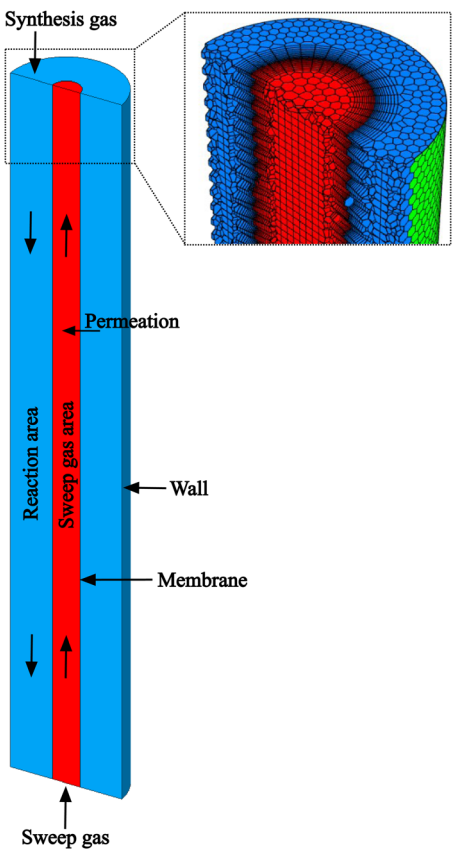

Fig. 1 Cross-section of the simulated MR with the reaction area on the outside of the membrane and the sweep gas area on the inside. Additionally the magnified mesh is indicated with the more detailed boundary layer around the membrane.

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Table 1 Geometric paramters of the simulated MR

Parameter	Symbol	Value	Unit
Membrane diameter	d_m	10	mm
Membrane thickness	t_m	1.5	mm
Wall diameter	d_w	40	mm
Wall thickness	t_w	6	mm
Length	l	250	mm

three-dimensional geometry model of the tubular MR, whose geometric parameters are summarized in Table 1.

The required mathematical discretization is generated based on the spatial geometry model in the meshing mode of Fluent. To ensure sufficient accuracy of the mesh around the membrane, boundary layers are grown into the fluids on either side of the membrane. The poly-hexcore mesh with a minimal and maximal cell size of 0.004 mm and 1.024 mm has an orthogonal quality of 41 across 284 936 cells. A mesh independence study attached in A1 is conducted affirming sufficient grid refinement.†

2.2 Reaction

Four different volumetric reaction rate UDFs are implemented in Fluent based on the kinetic models by Graaf *et al.*, Vanden Bussche and Froment, Mignard and Pritchard, and Nestler *et al.* to describe CH_3OH synthesis.[38–42] The kinetic models are validated using the empirical results published by Gallucci *et al.* CO_2 conversion (x_{CO_2}) and CH_3OH selectivity (S_{CH_3OH}) are calculated according to eqn (2) and (3). The dimensions of the simulated reactor derived from the experimental setup of Gallucci *et al.*, the corresponding mesh independence study as well as the validation results are attached in A2.1.[24] †

$$x_{CO_2} = \frac{\dot{N}_{CO_2,in} - \dot{N}_{CO_2,out}}{\dot{N}_{CO_2,in}} \times 100 \quad (2)$$

$$S_{CH_3OH} = \frac{\dot{N}_{CH_3OH,out}}{\dot{N}_{CO_2,in} - \dot{N}_{CO_2,out}} \times 100 \quad (3)$$

In this simulative study an inlet feed temperature of 250 °C is employed to account for the highest kinetically achievable CO_2 conversion.[30] Analyzing the kinetic regressions, the related models developed by Vanden Bussche and Froment and Mignard and Pritchard show the most accurate reproduction of the experimental data at the specific operation temperature. Based on the knowledge that CO_2 is the main source of CH_3OH, both kinetic models neglect the CH_3OH synthesis route *via* CO and only regard CO_2 hydrogenation and RWGS reaction.[41] Mignard and Pritchard adjust the activation energies of both reactions from the kinetic model of Vanden Bussche and Froment to improve the sensitivity of the model at lower temperatures.[41] Moreover, since the adjustment extends the range of applicability of the model by Vanden Bussche and Froment in terms of pressure from 51 bar to 75 bar, the model by Mignard and Pritchard is selected for the description of the CH_3OH synthesis reaction mechanism.[40,41] The corresponding reaction rates are specified in eqn (4) and (5).[41] The necessary constants are listed in Table 2 including the chemical equilibrium constants based on Graaf *et al.*[41,43] To assess the accurate integration of the kinetic model, the reaction UDF is additionally validated in A2.2 with simulative data obtained by Bussche and Froment.[40] †

Table 2 Parameters of the kinetic model by Vanden Bussche and Froment modified by Mignard and Pritchard based on the chemical equilibria by Graaf *et al.*

Parameter	Unit	Equation	Source
k_1	mol s^{-1} kg bar^2	$1.07 \exp\left(\frac{40\,000}{RT}\right)$	41
k_2	mol s^{-1} kg bar	$1.22 \times 10^{10} \exp\left(\frac{-98\,084}{RT}\right)$	41
K_{H_2O}	1 bar^{-1}	$6.62 \times 10^{-11} \exp\left(\frac{124\,119}{RT}\right)$	40
$K_{H_2}^{1/2}$	1 $bar^{-1/2}$	$0.499 \exp\left(\frac{17\,197}{RT}\right)$	40
K_{H_2O,H_2}	—	3453.38	40
$K_{eq,1}$	1 bar^{-2}	$10^{\frac{3066}{T}-10.592}$	43
$K_{eq,2}$	—	$10^{\frac{-2073}{T}+2.029}$	43

$$r_{CO_2} = \frac{k_1 p_{CO_2} p_{H_2} \left(1 - \frac{p_{H_2O} p_{CH_3OH}}{K_{eq,1} p_{H_2}^3 p_{CO_2}}\right)}{\left(1 + \frac{K_{H_2O,H_2} p_{H_2O}}{p_{H_2}} + \left(K_{H_2} p_{H_2}\right)^{1/2} + K_{H_2O} p_{H_2O}\right)^3} \quad (4)$$

$$r_{RWGS} = \frac{k_2 p_{CO_2} \left(1 - \frac{p_{H_2O} p_{CO}}{K_{eq,2} p_{H_2} p_{CO_2}}\right)}{\left(1 + \frac{K_{H_2O,H_2} p_{H_2O}}{p_{H_2}} + \left(K_{H_2} p_{H_2}\right)^{1/2} + K_{H_2O} p_{H_2O}\right)} \quad (5)$$

2.3 Permeation

The employed membrane consists of sodium ion (Na^+)-gated water-conducting nanochannels with a diameter of 4.2 Å which impede the permeation of gas molecules and strain H_2O from the reaction zone.[26] Due to the high H_2O permselectivities against CO and CO_2 of the hydrophilic membrane developed by Li *et al.*, only the permeation of H_2O, CH_3OH, and H_2 is considered.[26] The process of permeation across the microporous membrane is modeled with a novel method for CFD simulation, which properly considers the interactions between water and alcohol species. According to Krishna *et al.*, mixture permeation across zeolite membranes can be expressed most properly by the multicomponent Langmuir approach for adsorption and the Maxwell–Stefan (M–S) approach for diffusion.[36] Whereas the Langmuir approach is based on the Langmuir adsorption parameters (b_i), the M–S approach uses the species M–S diffusivities ($Đ_i$), which reflect the interactions between the species i and the zeolite membrane, as well as the exchange M–S diffusivities ($Đ_{ij}$), which reflect the interaction between species i and j.[37] A temperature dependence is incorporated with a van't Hoff type temperature dependence of adsorption for the Langmuir adsorption parameters shown in eqn (6) as well as an Arrhenius

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Table 3 Values used in the permeation UDF with literature sources

Symbol	Value	Unit	Source
ρ_m	1900	kg m^{-3}	44
b_{o,H_2O}	1.64×10^{-12}	1 Pa^{-1}	Fitted values
b_{o,CH_3OH}	5.64×10^{-15}	1 Pa^{-1}	Fitted values
b_{o,H_2}	3.22×10^{-9}	1 Pa^{-1}	Fitted values
$\Delta H_{ads,H_2O}$	−40	kJ mol^{-1}	45
$\Delta H_{ads,CH_3OH}$	−65	kJ mol^{-1}	46
$\Delta H_{ads,H_2}$	−5.9	kJ mol^{-1}	47
q_{sat,H_2O}	15	mol kg^{-1}	46
q_{sat,CH_3OH}	6.2	mol kg^{-1}	46
q_{sat,H_2}	1	mol kg^{-1}	48
$Đ_{o,H_2O}$	7.08×10^{-4}	m^2 s^{-1}	37,49
$Đ_{o,CH_3OH}$	1.03×10^{-7}	m^2 s^{-1}	37,49
$Đ_{o,H_2}$	1.7×10^{-8}	m^2 s^{-1}	47
$Đ_{H_2O,CH_3OH}$	3×10^{-9}	m^2 s^{-1}	37
E_{A,H_2O}	36	kJ mol^{-1}	49
E_{A,CH_3OH}	17	kJ mol^{-1}	49
E_{A,H_2}	1.9	kJ mol^{-1}	47

type temperature dependence of diffusion for the Maxwell–Stefan diffusivities shown in eqn (7). Table 3 comprises all parameters used in the permeation UDF with their respective sources.[36]

$$b_i = b_{o,i} e^{\frac{-\Delta H_{ads,i}}{RT}} \tag{6}$$

$$Đ_i = Đ_{o,i} e^{\frac{-\Delta E_{A,i}}{RT}} \tag{7}$$

As Langmuir adsorption equilibrium constants are missing in literature, the experimental data of Li *et al.* is used to fit the parameters.[26] By contrast, the species M–S diffusivities are readily available in literature. Moreover, based on Vignes interpolation, Krishna and Wesselingh propose eqn (8) to predict the exchange M–S diffusivities by interpolating the species' M–S diffusivities.[50]

$$Đ_{ij} = Đ_i^{\frac{\theta_i}{\theta_i+\theta_j}} Đ_j^{\frac{\theta_j}{\theta_i+\theta_j}} \tag{8}$$

Furthermore, Krishna and Wesselingh state for ideal gas mixtures, the M–S exchange coefficients in a ternary mixture are identical to those in the corresponding binary pairs.[51] Additionally, the Onsager reciprocal relation displayed in eqn (9) holds, with the net effect that the faster-moving species decelerates and the slower-moving species accelerates.[36]

$$Đ_{ij} = Đ_{ji} \tag{9}$$

High exchange M–S diffusivities indicate small correlations between the permeating species.[37] For zeolite frameworks like LTA, which allow only one molecule at a time to jump from one cage to the neighboring one, correlations can be negligible leading to a set of uncoupled M–S equations.[37] However, Krishna and van Baten identify several pitfalls for M–S modeling of water–alcohol mixture permeation across pervaporation membranes resulting from two types of diffusional coupling effects.[37,52] The first type are correlation effects, when the less mobile species slows down its more mobile partner by not vacating an adsorption site quickly enough for its more mobile partner to occupy that position.[52] The second type is molecular clustering due to hydrogen bonding, which can cause the mutual slowing down of the partner molecules.[52] The coupling effects have the following consequences for modeling permeation of water–alcohol mixtures:

- The species M–S diffusivities are lower than for their respective pure components. Thus, the species M–S diffusivities can not be obtained from unary permeation data.[37,52]
- Due to increased correlation, the Vignes interpolation formula is inappropriate for the prediction of the exchange M–S diffusivities. It is not hydrogen bonding, *per se*, that contributes to the deviation from the Vignes formula, rather, it is the difference in the degrees of hydrogen bonding between constituent molecular pairs.[37]
- Employing the uncoupled M–S equations is not justified.[37]

Specifically for the CFD model of the present work, this means that the species M–S diffusivities published by Krishna and van Baten, who report the values for water–alcohol mixtures in LTA zeolites for a temperature of 350 K, are incorporated into the permeation UDF.[37] Furthermore, since, the Wesselingh interpolation formula is based on the Vignes interpolation formula, it is not used to calculate the exchange M–S diffusivity between H_2O and CH_3OH. Moreover, the coupled M–S eqn (10)–(14) are applied in the permeation UDF. Therefore, in contrast to other CFD models, by employing the coupled M–S equations, the present work does not disregard the interaction between the different species in a permeating gas mixture. Rather, in the present study, the coupled M–S method is employed for a proper description of multicomponent permeation of water–alcohol mixtures across microporous zeolite membranes.[34,36,37]

$$-\rho_m \frac{\theta_i}{RT} \frac{\partial \mu_i}{\partial z} = \sum_{\substack{j=1 \\ j\neq i}}^{n} \frac{q_j J_i - q_i J_j}{q_{i,sat} q_{j,sat} Đ_{ij}} + \frac{J_i}{q_{i,sat} Đ_i} \tag{10}$$

$$\Gamma_{ij} = \frac{\theta_i}{p_i} \frac{\partial p_i}{\partial \theta_j} = \delta_{ij} + \frac{\theta_i}{\theta_v} \tag{11}$$

$$B_{ii} = \frac{1}{Đ_i} + \sum_{\substack{j=1 \\ j\neq i}}^{n} \frac{\theta_i}{Đ_{ij}} \tag{12}$$

$$B_{ij} = -\frac{\theta_i}{Đ_{ij}} \tag{13}$$

$$(J) = -\rho_m [q_{sat}][B]^{-1}[\Gamma] \frac{\partial \theta}{\partial z} \tag{14}$$

The surface coverage (θ) also known as the fractional loading describes the fraction of occupied adsorption sites, as shown in eqn (15), with the molar loading (q) and the saturation loading (q_{sat}). Correspondingly, the fraction of empty sites called fractional vacancy (θ_v) is calculated by eqn (16).

$$\theta_i = \frac{q_i}{q_{sat,i}} = \frac{b_i p_i}{1 + \sum_{j=1}^{n} b_j p_j} \tag{15}$$

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Table 4 Results of the gas mixture separation experiments by Li *et al.*[26]

p, *T*	H_2O permeance	H_2O selectivity *vs.*		H_2O flux
[bar], [°C]	[10^{-7} mol m^{-2} s Pa]	CH_3OH [–]	H_2 [–]	[kg m^{-2} h]
21, 200	1.62–2.03	>49	>138	0.46–0.56
21, 250	1.56–1.85	>41	>104	0.44–0.68
38, 250	1.40–1.85	>52	>186	0.45–1.11

Table 5 Simulation results of the permeation validation

p, *T*	H_2O permeance	H_2O selectivity *vs.*		H_2O flux
[bar], [°C]	[10^{-7} mol m^{-2} s Pa]	CH_3OH [–]	H_2 [–]	[kg m^{-2} h]
21, 200	2.07	53.7	265	0.50
21, 250	1.69	142	239	0.43
38, 250	1.42	117	201	0.60

$$\theta_v = 1 - \sum_{i=1}^{n} \theta_i = \frac{1}{1 + \sum_{j=1}^{n} b_i p_i} \tag{16}$$

From an implementation perspective, the permeation UDF introduces source terms for the conservation of mass and energy in the cells adjacent to the membrane. The gas mixture separation experiments conducted by Li *et al.* are recreated in simulation to validate the permeation UDF. The experimental results by Li *et al.* are shown in Table 4 and the results of the permeation validation simulated with the permeation UDF are shown in Table 5. Except for a slight overshoot in H_2O permeance of 1.97% at 21 bar and 200 °C and a slight undershoot of H_2O flux of 2.27% at 21 bar and 250 °C the simulative results agree with the empirical data by Li *et al.* The mesh independence study of the geometry based on Li *et al.* is attached in A3.[26] †

2.4 Base case scenario

Besides the description of the reaction as well as the permeation in the applied model, base case operating parameters need to be specified. Therefore the following three parameters are adopted in this study:

The gas hourly space velocity (GHSV) is calculated according to eqn (17), with the standard feed volume flow ($\dot{V}_{feed,N}$) and the volume of the reaction zone (V_r). The a sweep-to-feed (S/F) ratio is defined by the molar flows of the sweep ($\dot{N}_{in,sweep}$) and the feed ($\dot{N}_{in,feed}$) following eqn (18). Lastly, the ratio of membrane surface to reaction volume (O_M/V_r) is based on eqn (19) comprising the membrane diameter (d_m), the wall diameter (d_w) and the length of the reactor (l).

$$\mathrm{GHSV} = \frac{\dot{V}_{feed,N}}{V_r} \tag{17}$$

$$\mathrm{S/F} = \frac{\dot{N}_{in,sweep}}{\dot{N}_{in,feed}} \tag{18}$$

$$O_M/V_r = \frac{\pi \cdot d_m \cdot l}{\frac{\pi}{4} \cdot l(d_w^2 - d_m^2)} = \frac{4 \cdot d_m}{d_w^2 - d_m^2} \tag{19}$$

If not otherwise specified, the performance of the MR is analysed in a defined base case scenario with a GHSV of 5000 h^{-1} resembling a $\dot{V}_{feed,N}$ of 24.54 L min^{-1} with a stoichiometric $H_2:CO_2$ ratio of 3:1, a S/F-ratio of 1, no pressure difference between the reaction and sweep zones, and a O_M/V_r-ratio of 26.67 m^{-1}.

3 Results and discussion

3.1 Operating conditions

First, the correlation between the operating conditions and the output parameters CO_2 conversion (Fig. 2), CH_3OH selectivity (Fig. 3), and CH_3OH yield (Fig. 4) of the membrane reactor (MR) is investigated in a commonly employed pressure range of 20–100 bar and temperature range of 200–300 °C. The distinguished

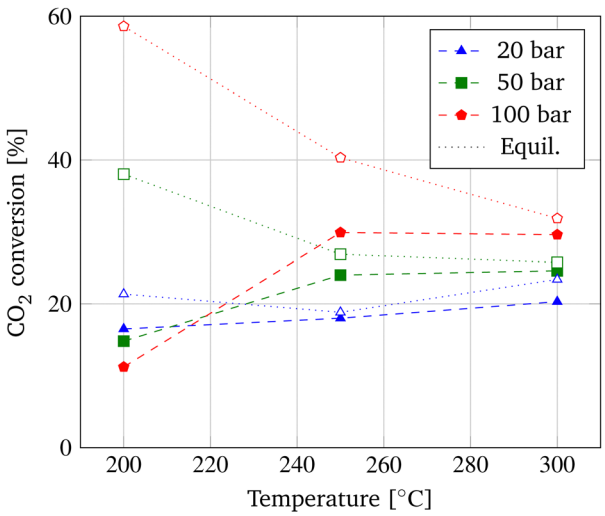

Fig. 2 Pressure and temperature dependency of CO_2 conversion of the MR.

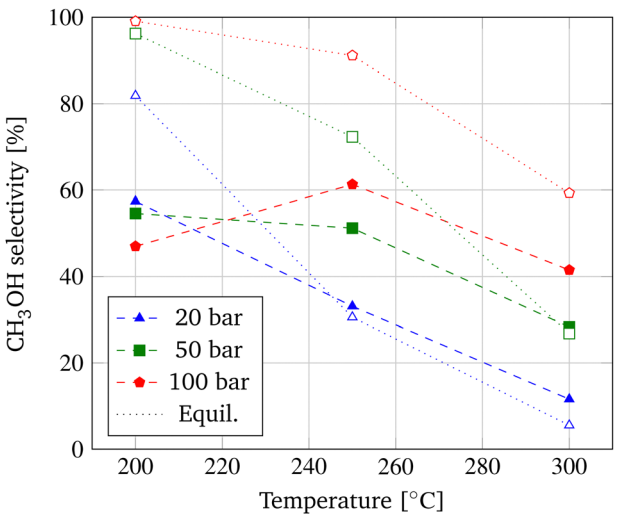

Fig. 3 Pressure and temperature dependency of CH_3OH selectivity of the MR.

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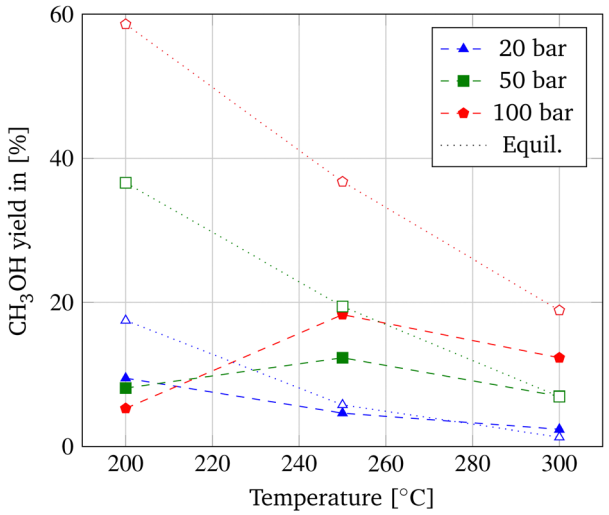

Fig. 4 Pressure and temperature dependency of CH_3OH yield of the MR (dashed lines) and equilibrium CH_3OH yields from ref. 9 (dotted lines).

performance trends of the MR due to equilibrium and kinetic considerations are applicable to methanol synthesis in general. A distinct differentiation between the behavior of a MR and TR is employed subsequently.

According to the principle of Le Châtelier, CO_2 conversion decreases with temperature due to the exothermic nature of the hydrogenation reaction and increases with pressure as a consequence of the volume-reducing reaction. In Fig. 2, the temperature dependence of the CO_2 conversion in the MR is displayed alongside the achievable equilibrium CO_2 conversion derived from Dieterich *et al.*[9] In contrast to the temperature dependency of the chemical equilibrium, CO_2 conversion in the MR increases with temperature due to the acceleration of the reaction kinetics. Only at a pressure of 100 bar a slight decrease in CO_2 conversion is apparent from 250 °C to 300 °C. According to Barbieri *et al.*, the resulting maximum in CO_2 conversion at 250 °C is due to the promotion of CO_2 activation.[30] At lower pressures, no such optimum at 250 °C is obtained, which could be explained by the less distinctive enhancement of the shift of the equilibrium of the hydrogenation reaction due to pressure and, hence, a different correlation between the competing RWGS and hydrogenation reaction.

This explanation is supported by the behavior of the CH_3OH selectivity shown in Fig. 3, depicting a maximum selectivity to CH_3OH at a temperature of 250 °C and a pressure of 100 bar and a decrease of the selectivity at higher temperatures. This implies that at a temperature of 250 °C, more CO_2 is converted to CH_3OH in contrast to the formation of undesired CO and H_2O due to the RWGS reaction. Due to the smaller significance of the pressure shift of the equilibrium at lower pressures as explained above, CH_3OH selectivity decreases with temperature at pressures of 20 bar and 50 bar following the equilibrium selectivities adopted from Dietreich *et al.*[9]

Eqn (20) depicts the interrelation of CH_3OH yield with CO_2 conversion and CH_3OH selectivity and explains the comparable behavior of CH_3OH yield with temperature as depicted in Fig. 4.

When referring to the principle of Le Châtelier, CO_2 conversion should increase with pressure as depicted in Fig. 2 for temperatures above 200 °C and is the same for CH_3OH selectivity and yield. However, at a temperature of 200 °C, the relation is reversed for all three parameters, as also previously reported in experimental data by Gallucci *et al.*[24]

$$y_{CH_3OH} = \frac{x_{CO_2} \cdot S_{CH_3OH}}{100\%} \tag{20}$$

This transition of the pressure dependency could be induced by a smaller temperature dependency of the RWGS reaction compared to the hydrogenation reactions. Hence, the water formation due to the RWGS reaction is less imposed at lower temperatures resulting in a higher share of water at low temperatures and high pressures. This explanation could also be the reason why when looking at the CH_3OH yield depicted in Fig. 4 and comparing the achievable equilibrium yield obtainable by CO_2 hydrogenation included from Dieterich *et al.*, the equilibrium is deviating most at a temperature of 200 °C and higher pressures.[9] The findings correspond to published literature and result in the adoption of a pressure of 100 bar and a temperature of 250 °C in this optimization study of the MR.[26,30]

3.2 Permeation characteristics

The performance of the membrane is investigated in a pressure range of 20–100 bar and a temperature range of 200–300 °C. For evaluation, the species removal R_i is calculated following eqn (21). In Fig. 5, the species removal for the permeating species H_2O, CH_3OH, and H_2 are depicted as a function of pressure and temperature.

$$R_i = \frac{\dot{N}_{i,\text{sweep,out}}}{\dot{N}_{i,\text{sweep,out}} + \dot{N}_{i,\text{syngas,out}}} \tag{21}$$

In accordance to the trends observed by Li *et al.*, the species removal increases with increasing pressure.[26] This is due to the

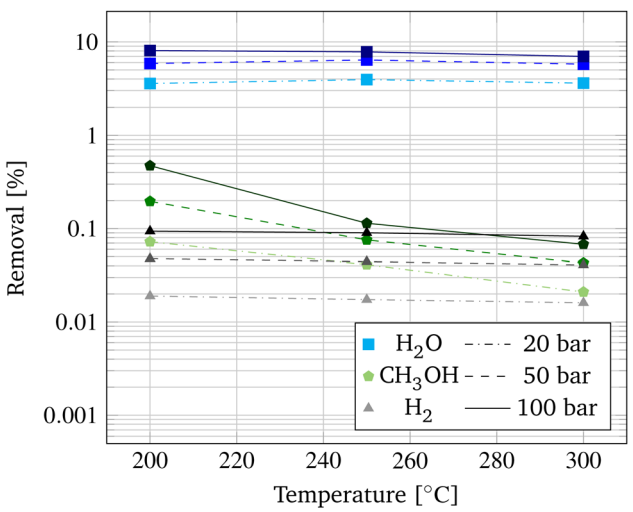

Fig. 5 Species removal by the membrane as a function of pressure and temperature.

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enhanced partial pressure difference causing a higher driving force for permeation. Due to the high polarity of the zeolite channels in the membrane, the desired H_2O removal is significantly higher compared to the CH_3OH and H_2 removal. The in-depth mechanism of the permeation through the Na^+-gated zeolite membrane is disclosed by Li *et al.*[26]

In contrast to the pressure dependency on the species removal, an increased temperature results in a decrease in permeation. This could be attributed to the decreased adsorption ability of the gas molecules at higher temperatures caused by the increased velocity.[53] Overall, permeation of H_2 and H_2O is not greatly influenced by variations of temperature in the analysed range, as the van't Hoff type temperature dependence of adsorption and the Arrhenius type temperature dependence of diffusion seem to outbalance each other. However, the CH_3OH removal shows a steep decrease in permeation between 200 °C and 250 °C. This could be induced by the critical temperature of CH_3OH at 239.9 °C, above which CH_3OH becomes a non-condensable fluid inhibiting permeation by capillary condensation.[24,54]

3.3 Membrane performance

The performance of the MR applying the base case operating parameters is illustrated in Fig. 6. The molar fractions are depicted along the length of the MR with the synthesis gas inlet shown at 0% and the counter-current sweep inlet at 100%. As expected, the molar fraction of H_2 and CO_2 decrease in the reaction zone along the length of the MR, while the molar fractions of CH_3OH, H_2O, and CO increase along the reactor due to the occurring reactions. On the sweep gas side, the molar fractions of the permeating species H_2O, CH_3OH, and H_2 increase in counter-current along the length of the MR indicating the water-conducting and gas-impeding characteristics of the applied membrane. As mentioned in the modeling section, CO_2 and CO are not considered to permeate through the membrane and are hence indicated on the abscissa.

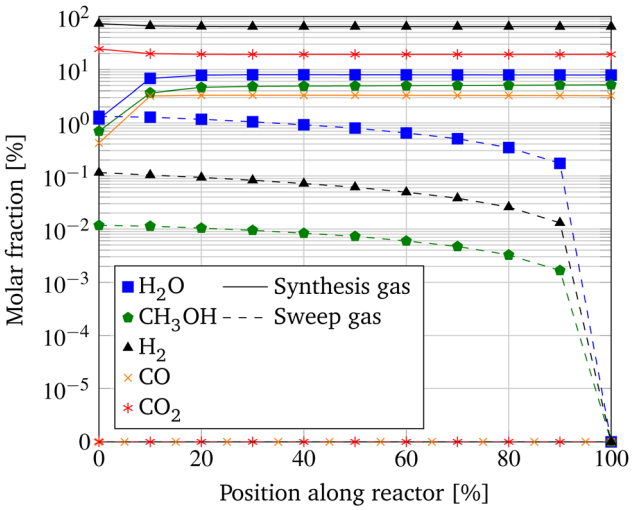

Fig. 6 Molar fractions along the length of the MR with base case parameters at a pressure of 100 bar and a temperature of 250 °C.

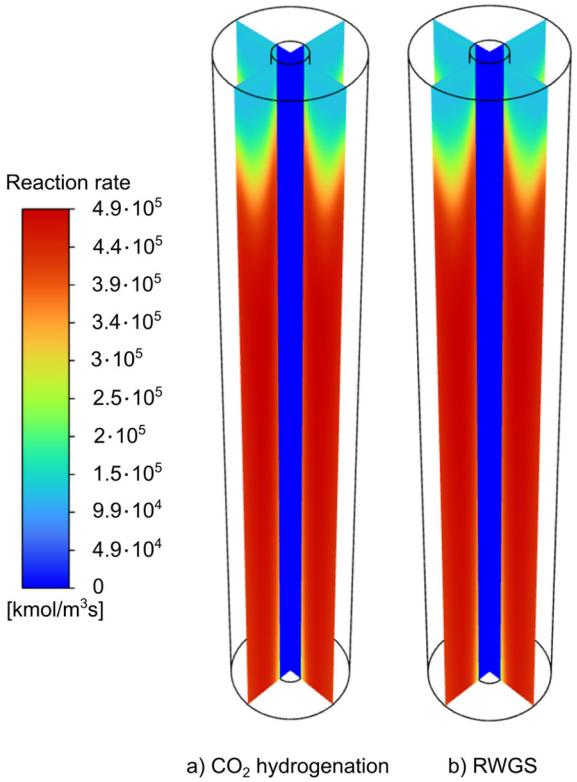

Fig. 7 Profiles of the (a) CO_2 hydrogenation and (b) RWGS reaction rates along the length of the MR with base case parameters at a pressure of 100 bar and a temperature of 250 °C.

The reaction rates of the CO_2 hydrogenation and the RWGS reaction as well as the temperature profile along the MR for the base case scenario are shown in Fig. 7 and 8. Conceivably, the temperature profile coincides with the distribution of the reaction rates. As shown by the colour scheme, the reaction rates first increase and remain rather constant over the length of the reactor. Due to the low heat transfer coefficient of the sweep gas, the temperature of the nitrogen stream stays fairly constant over the length of the MR.

To evaluate the performance of the MR, the H_2O removal is calculated for the base case scenario. As already indicated by the logarithmic scale of the *y*-axis in Fig. 6, only 7.82% of the generated H_2O is removed by the membrane. Hence, the shift of the equilibrium towards the products is small causing a negligible increase in the efficiency of the CH_3OH synthesis reaction. To validate this behavior, the simulation is repeated with impeding permeation through the membrane revealing an increase in CO_2 conversion of only 0.3%.

To optimize the performance of the MR, and increase CO_2 conversion and CH_3OH yield, the effects of the previously introduced parameters (GHSV, S/F, O_M/V_r) are investigated in a full factorial design of experiment. In Table 6, the factors as well as the evaluated values are summarized.

The main effects E_f of the factors are calculated following eqn (22), with m being the number of factors and y_i the target value (CO_2 conversion or CH_3OH yield) at the high-level setting

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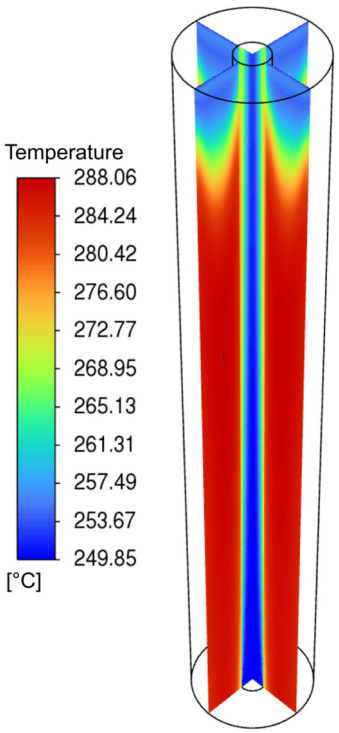

Fig. 8 Temperature profile along the length of the MR with base case parameters at a pressure of 100 bar and a temperature of 250 °C.

Table 6 Structure of the full factorial design of experiments

Number of experiment	GHSV / 1 h^{-1}	$\dot{V}_{feed,N}$ / L min^{-1}	S/F / —	O_M/V_r / 1 m^{-1}
1	500	0.49	1	133.33
2	5000	4.91	1	133.33
3	500	0.49	10	133.33
4	5000	4.91	10	133.33
5	500	2.45	1	26.67
6	5000	24.54	1	26.67
7	500	2.45	10	26.67
8	5000	24.54	10	26.67

of the factor ($y_{i,+}$) and the low level setting of the factor ($y_{i,-}$).[55]

$$E_f = \frac{2}{m} \cdot \sum_{i=1}^{m} (y_{i,+} - y_{i,-}) \quad (22)$$

In Fig. 9–11, the main effects of the parameters are depicted, showing comparable trends for CO_2 conversion and CH_3OH yield. To identify the impact of the MR, the resulting CO_2 conversion and CH_3OH yield of a comparable TR is added in a dashed line with round marks. For the simulation of the TR, the same CFD model is used with impeded permeation.

As shown in Fig. 9, the lower the GHSV, the higher CO_2 conversion and CH_3OH yield. This is primarily the result of the longer residence time of the reactants in the reactor, as indicated by the increase of conversion of the TR from 29.7% to 31.3%. However, the impact of the membrane is significantly larger at a lower GHSV. While the increase in CO_2 conversion of

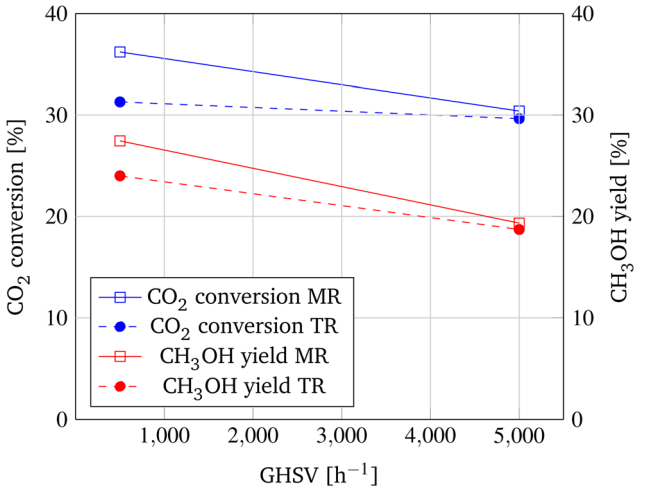

Fig. 9 Main effect of GHSV on CO_2 conversion and CH_3OH yield at 100 bar and 250 °C.

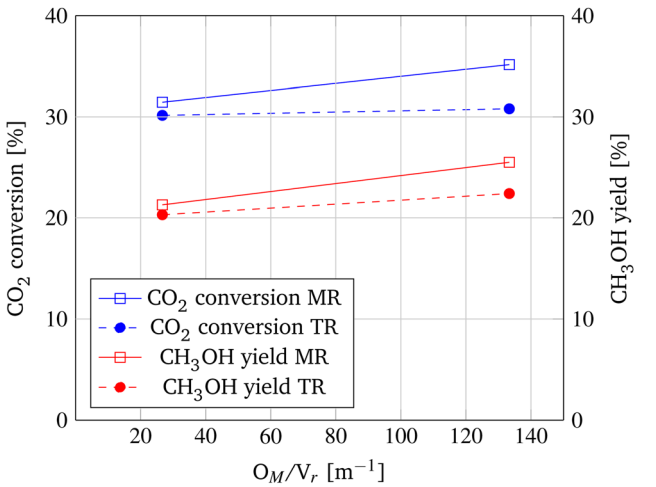

Fig. 10 Main effect of O_M/V_r ratio on CO_2 conversion and CH_3OH yield at 100 bar and 250 °C.

the MR only accounts for an increase of 0.8% at a GHSV of 5000 h^{-1}, at a decelerated GHSV of 500 h^{-1} the application of the MR leads to an increase of CO_2 conversion of 4.9%. This is due to the increased residence time of the reaction products at the membrane and the higher adsorption ability of the gas molecules resulting from the lower velocity.[24] Hence, a higher amount of reaction product permeates through the membrane and is removed from the reaction zone, resulting in an enhanced shift of the chemical equilibrium and consequently an increase in CO_2 conversion and CH_3OH yield.

Permeation seems to be the limiting factor in shifting the chemical equilibrium and enhancing conversion. As a second parameter, the ratio of membrane surface to reaction volume is investigated to accelerate permeation, enhance the shift of the chemical equilibrium, and ultimately improve CO_2 conversion. Therefore, while the membrane geometry is kept constant, the diameter of the reactor tube is decreased from 40 mm to

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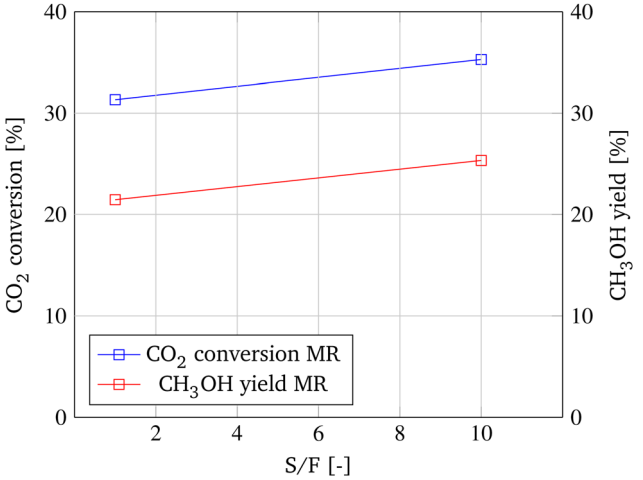

Fig. 11 Main effect of S/F ratio on CO_2 conversion and CH_3OH yield at 100 bar and 250 °C.

20 mm, leading to a O_M/V_r ratio of 26.7 m^{-1} and 133.3 m^{-1}, respectively. As depicted in Fig. 10, at the lower O_M/V_r ratio, the performance of the MR only marginally surpasses the CO_2 conversion and CH_3OH yield of the TR by 1.3% and 1.0%, respectively. However, when increasing the ratio of membrane surface to reaction volume, CO_2 conversion increases from 31.45% to 35.2% and CH_3OH yield is enhanced by 4.2% compared to the TR.

Besides improving the permeation on the reaction side of the membrane, CO_2 conversion and CH_3OH yield could be enhanced by increasing the partial pressure difference as the driving force of permeation. This can be realized by removing the permeated species inside the membrane faster from the reactor. The influence of an accelerated sweep transporting the permeated species out of the MR is shown in Fig. 11. With a ten times faster sweep, an increase of CO_2 conversion from 31.3% to 35.3% and an enhancement of the CH_3OH yield of 3.9% is achievable.

Comparable to Fig. 6, the molar fractions of the involved species over the length of the MR with the most promising parameter compilation of a GHSV of 500 h^{-1}, a S/F ratio of 10 and a O_M/V_r ratio of 133.3 m^{-1} are displayed in Fig. 12. As before, the educts H_2 and CO_2 decrease in the reaction zone, and the permeating species H_2O, H_2, and CH_3OH increase in counter-current in the sweep. However, in contrast to the base configuration of the MR, the molar fraction of H_2O shows an increase over the first 10% of the reactor length and starts declining subsequently, indicating the functionality of the membrane reactor. As a result, the chemical equilibrium of the hydrogenation reaction is shifted, and the molar fraction of CH_3OH increases over the entire length of the reactor rather than remaining nearly constant after an initial steep increase when comparing it to the base case configuration in Fig. 6. Due to the optimization of the constructive and operational configuration of the MR, the H_2O removal is increased to 88.1%. To identify the impact of the MR, the simulation is repeated with impeding permeation through the membrane, disclosing an increase in CO_2 conversion by the membrane of 14.0%.

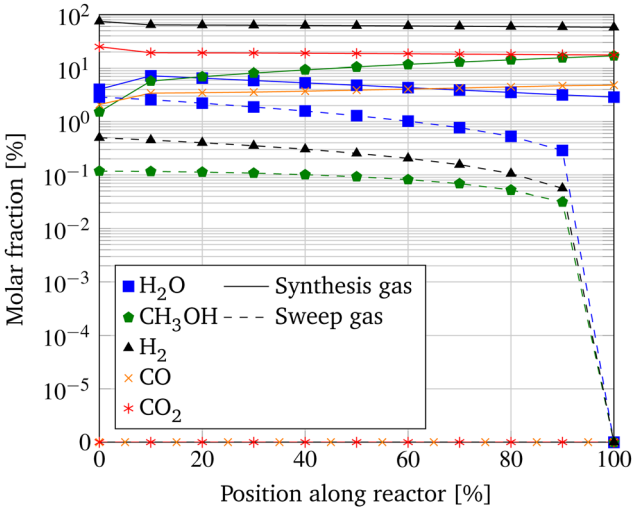

Fig. 12 Molar fractions along the length of the MR with best case parameters (GHSV = 500 h^{-1}, S/F ratio = 10, O_M/V_r ratio = 133.3 m^{-1}) at a pressure of 100 bar and a temperature of 250 °C.

Finally, a fourth influential factor, a potential pressure difference between reaction zone and membrane is investigated for the previously introduced most promising parameter compilation (GHSV = 500 h^{-1}, $\dot{V}_{feed,N}$ = 0.49 L min^{-1}, S/F-ratio = 10, O_M/V_r-ratio = 26.67 m^{-1}). Based on the manufacturer's statements, the membrane is capable of withstanding a pressure difference of up to 100 bar. Hence, a 99 bar pressure difference is adjusted for the simulation. The results are depicted in Fig. 13, showing an increase of CO_2 conversion of 6.1% and an enhancement of CH_3OH yield of 4.3% when the pressure difference is applied.

This increase is caused by the greater partial pressure difference, the driving force of permeation, that is depended on the prevalent absolute pressure. In the dashed lines, the comparable outcomes of the TR are depicted, illustrating the maximum increase of CO_2 conversion of 20.1% and the maximum increase of CH_3OH yield of 14.8% when using the MR.

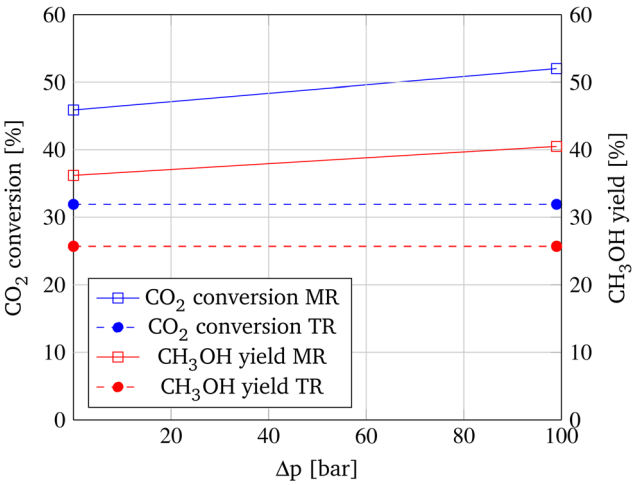

Fig. 13 Impact of Δp across the membrane on CO_2 conversion and CH_3OH yield at 100 bar and 250 °C.

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In the most optimal configuration (GHSV = 500 h^{-1}, $\dot{V}_{feed,N}$ = 0.49 L min^{-1}, S/F-ratio = 10, O_M/V_r-ratio = 26.67 m^{-1}, Δp = 99 bar), the application of the MR results in a maximum CO_2 conversion of 52.0% exceeding the equilibrium conversion at a pressure of 100 bar and a temperature of 250 °C by 11.7%.[9] The methanol yield is increased to a maximum of 40.5%, transcending the equilibrium yield by 5.2%.[9] These roughly 20% increases compared to the TR result in the reduction of the necessary recycling volume flow and the corresponding energy consumption for the recycling compression by about 1/5. When assessing the added value of a membrane reactor for methanol synthesis, a surpassing of 10% CO_2 conversion illustrates the great potential of membrane reactors for equilibrium-limited reactions.

3.4 Findings of the full-factorial design of experiments

The findings of this study show the importance of optimization for the construction as well as the operation when implementing MRs instead of TRs. It shows, that for a comparison of MR and TR in any application, it is not sufficient to just apply the optimal parameters of a TR to the substituting MR. As a guideline for the optimization of MRs, in general, following key parameters should be regarded:

- Ratio between reaction and permeation
  Permeation seems to be the rate determining step to shift the equilibrium towards the products. Hence, when the residence time of the permeating species is too low or the diffusion towards the membrane takes too long, too little permeating species are removed from the reaction zone and the membrane has negligible impact. Two parameters are determined influencing the ratio between reaction and permeation:
  (1) GHSV: when decreasing the GHSV, the feed volume flow is decreased. Thus, the residence time of the reactants is increased leading to an enhanced permeation and a shift in the chemical equilibrium of the synthesis.
  (2) O_M/V_r: when increasing the ratio between surface area of the membrane and volume of the reaction zone, a shorter distance needs to be surpassed by the permeating species towards the membrane. Thus, more reaction products are removed from the reaction zone shifting the equilibrium towards higher conversion.
- Partial pressure difference
  Since the partial pressure difference between the reaction zone and sweep side is the driving force for permeation, an increase in partial pressure difference results in a higher conversion. Two parameters are identified to influence the partial pressure difference:
  (1) Total pressure difference: when depressurizing the sweep stream, a difference in the total pressure increases the partial pressure difference leading to a significant shift in the equilibrium.
  (2) Sweep velocity: on the inside of the membrane, a sweep stream removes the permeated species from the reactor. The faster this transportation occurs, the larger the partial pressure difference and the greater the increase in conversion.

Conclusions

This work determines key constructive and operating parameters for a membrane reactor for methanol synthesis *via* CO_2 hydrogenation. As the reaction of CO_2 and H_2 to CH_3OH is thermodynamically limited by the chemical equilibrium, the achievable conversion is restricted. To overcome the chemical equilibrium, membrane reactors are adopted, removing reaction products from the reaction zone and, consequently, enhancing conversion. Eventually, the required expensive recirculation of unconverted reactants can be downsized, resulting in a more efficient methanol production approach. For the parameter study, a sophisticated CFD model of the MR with a NaA zeolite membrane is developed, incorporating the kinetics of the chemical reactions as well as the permeation of diffusing species. Unlike previous simulative studies on membrane reactors for methanol synthesis, in this work, permeation is described in more detail by the M–S approach that does not disregard interactions between competing permeating species. Moreover, the distinct characteristics of pervaporating water–alcohol mixtures in zeolite membranes are considered.

After first investigating the correlation between operation conditions and CO_2 conversion and CH_3OH yield, revealing the optimal operating conditions for methanol synthesis in a MR at a temperature of 250 °C and pressure of 100 bar, the permeation through the membrane is characterized. Therefore, the parameter of the species removal, depicting the effect of the membrane on the permeating species, is introduced, revealing the temperature independence of the permeation of CH_3OH and H_2. On the contrary, the characterization shows the significant decrease in methanol permeation past the critical temperature due to the inhibition of permeation by capillary condensation. After analyzing the membrane performance in a base case scenario, a full-factorial design of experiment is conducted to optimize operational and construction parameters. The findings show that the impact of the MR is higher for lower GHSVs, a higher ratio of membrane surface to catalyst volume, higher sweep volume flows, and higher total pressure differences across the membrane. These parameters can be summarized in two general categories that have to be optimized for membrane reactors for industrial applications: the ratio between reaction and permeation and the permeation driving force. In the most optimal configuration, the application of the MR results in an increase of CO_2 conversion of 20.6% and a 16.0% enhanced CH_3OH yield. With the surpassing of the chemical equilibrium, this study shows the potential to shift the chemical equilibrium of methanol synthesis in membrane reactors towards the products, reducing recycling flows and necessary compression energy.

Based on the findings of this study, several research questions can be proposed: considering the significant impact of the pressure difference across the membrane, experimental high pressure investigations of the MR should be conducted to analyze the durability of the membrane and help identify the actual influence the pressure difference can have on CO_2 conversion and CH_3OH yield. Moreover, long-term experimental

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investigations of the MR could provide insights into the lifetime of the membrane, which is crucial for the feasibility of industrial applications. Furthermore, these long-term tests could reveal degradation effects of the membrane in the process that are neither known nor considered in literature. The experimental results can finally help to evaluate the impact MRs for methanol synthesis can have on an industrial scale.

Recapitulating, the results of the study on construction parameters and operating guidelines show how crucial optimization of the reactor design and operating conditions are especially important for membrane reactors and can help to increase the understanding of the possible impact membrane reactors can have on methanol synthesis but also on various other applications where the use of membrane reactors is discussed.

Author contributions

Theresa Hauth: conceptualization, methodology, formal analysis, investigation, writing – original draft; Konstantin Pielmaier: software, investigation, visualization, writing – original draft; Vincent Dieterich: conceptualization, methodology, investigation, writing – review & editing; Nicolas Wein: software, investigation, writing – review & editing; Hartmut Spliethoff: conceptualization, writing – review & editing, supervision, funding acquisition; Sebastian Fendt: conceptualization, writing – review & editing, supervision, project administration, funding acquisition.

Data availability

The data supporting this article have been included as part of the ESI.†

Conflicts of interest

There are no conflicts to declare.

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