

## REVIEW

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Evolving solar cell manufacturing: the promising  
outlook of open-air perovskite printing

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Perovskite-based solar cells stand out as promising candidates due to their remarkable optoelectronic properties and cost-effective processing methods. These advanced materials have garnered considerable research interest owing to their rapidly increasing power conversion efficiencies. Additionally, perovskite solar cells (PSCs) can be flexible, lightweight, and semi-transparent, expanding their applicability. While conventional spin-coating techniques have achieved record power conversion efficiencies for PSCs, scalability remains a challenge. Furthermore, these materials face two significant hurdles: instability when exposed to open air and concerns regarding chemical toxicity, primarily from lead (Pb) and solvent use. Recent advancements have focused on open-air printing techniques, which offer scalability and adaptability for large-scale production. However, the lack of standardized fabrication protocols and the need to mitigate chemical toxicity remain ongoing challenges. In this comprehensive review, we thoroughly examine the latest developments in perovskite solar cell technology, with a particular emphasis on open-air printing processes. We explore the strategies employed to enhance stability, efficiency, and scalability, highlighting the critical role of open-air printing in achieving these objectives. Furthermore, this review addresses the challenges and opportunities associated with open-air printing, including material synthesis, and device architecture. We analyze recent breakthroughs in materials and interface, and solvent engineering, as well as device fabrication techniques, driving advancements in the field towards simplified, large-area fabrication protocols for PSCs.

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# 1. Introduction

Renewable and clean energy findings have become increasingly important in recent years as a means to combat climate change. The use of photovoltaic devices (solar cells) is a promising technology, which convert the freely available solar energy to electricity. According to current statistics, solar cells account for just 3.6% of global electricity production.<sup>1</sup> However, current solar cells face several limitations, including high production costs, limited power conversion efficiency, heavy-weight modules, and a lack of tunable transparency, making them opaque and less versatile.<sup>2–4</sup> To tackle these issues, researchers have focused on exploring halide perovskites for solar cells. However, fabrication of PSCs in open-air has remained challenging.<sup>5–7</sup> Open-air fabrication is a process where materials are applied to a substrate within no sealed environment. This allows for more flexibility and lower costs to produce large-area solar cells.

Perovskite materials have a distinctive crystal structure characterized by the chemical formula  $ABX_3$ , where 'A' represents a monovalent cation, 'B' a divalent cation, and 'X' a monovalent anion. In perovskite-based solar cells (PSCs), the monovalent 'A' cations are typically alkyl amines or inorganic cations such as  $Cs^+$  and  $Rb^+$ . The divalent 'B' positions within the lattice are occupied by metal ions like Pb, Sn, Cu, or Mn. The anionic components ('X') in the perovskite lattice are halides, such as  $I^-$ ,  $Br^-$ , and  $Cl^-$ , or a combination of these halides in mixed compositions. The mixed halide composition in perovskites can significantly influence their optical properties. Numerous research groups have explored mixed halide compositions in PSCs to achieve an optimal optical bandgap, enhancing both efficiency and transparency in solar cells. At the same time, several studies have focused on improving the stability of these solar cells by tuning the cationic composition.<sup>8–10</sup>

Semiconductors in solar cells with a bandgap of 1.1 to 3.5 eV are capable of absorbing solar radiation within the 1100–350 nm range. Identifying a semiconductor with both a high absorption coefficient and excellent charge mobility remains a critical challenge for achieving efficient solar cells. Notably, laboratory-scale PSCs have surpassed the efficiency of commercial multi-crystalline silicon solar cells and are now nearly on par with the performance of CIGS and CdTe thin-film solar cells.<sup>11,12</sup> Similar to the PSCs, the colored organic dye and inorganic quantum dot solar cells have distinctive optical and structural properties and can be solution-processed. Nevertheless, their lower power conversion efficiencies (PCEs) have impeded their adoption in the photovoltaics field.<sup>13–26</sup> Even though, the reached efficiencies for PSCs are high (Record PCE >26%,<sup>27</sup>), and set a benchmark, their long-term stability, chemical toxicity and scalability needs to be improved for commercial viability. Moreover, PSCs must withstand towards environmental factors like high temperatures, humidity, and



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Lioz Etgar

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*hole conductor in solar cells, leading to a seminal publication in the field. Awarded the Krill Prize and Kaye Innovation Award, his research focuses on advanced solar cell and LED technologies. His contribution includes revising the MS.*

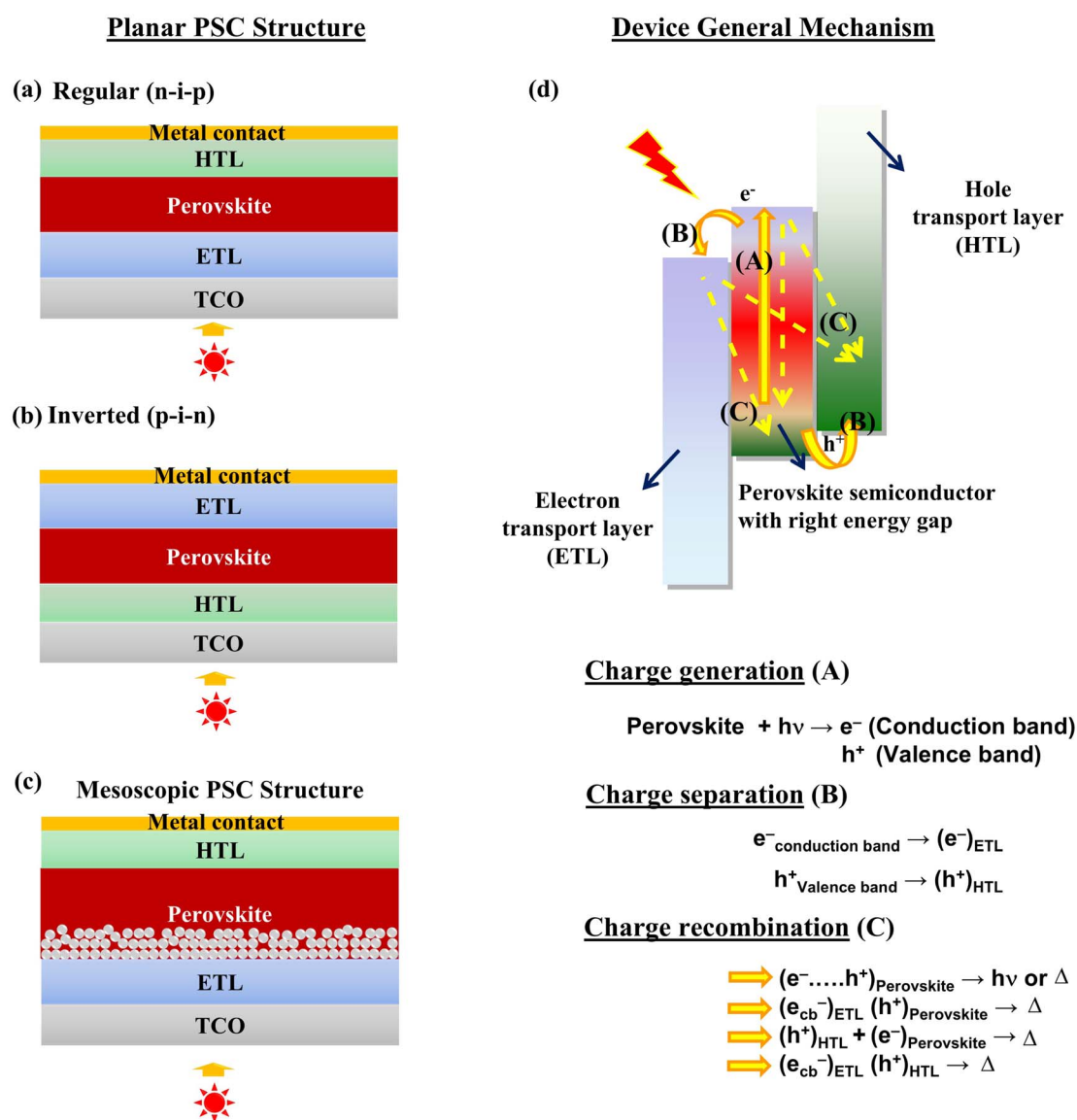


UV-light over long duration of time. The morphology of perovskite solar cells has a significant impact on the efficiency and stability of the device. The morphology of perovskite is highly dependent on the fabrication process and has a significant effect on the performance of the device. This can be achieved by controlling the perovskite growth parameters such as temperature, pressure, and deposition rate. For perovskite solar cells, other than perovskite layer's quality, the electron transport layer (ETL), and hole transport layer (HTL) also play an important role. These layers provide a pathway for the electrons and holes to move from the perovskite layer to the electrodes. In recent times, the concept of structural confinement of perovskites has been introduced. The regular perovskite films are considered as bulk perovskite or 3D perovskites whereas if the A cation in  $ABX_3$  is larger than the  $BX_6$  octahedra, it forms sheets of corner shared 2D perovskite layers. Thus, the A cations used are alkyl/

aryl amines with longer carbon chains that protect from moisture, improving the stability of the perovskite solar cell. Additionally, the confinement of the perovskite structure in lower dimensions allows for tuning of its optical properties.<sup>28–34</sup> Thus, in this review, we have discussed the literature involved in perovskite's structural and compositional tuning, additive engineering, solvent engineering, surface treatments and process engineering, *etc.*, in improving the open-air fabrication methodology.

## 2. Perovskite solar cell structure

The potential PSC device architectures are illustrated in Fig. 1(a–c), showcasing various construction approaches. These designs highlight different configurations and structural components crucial to optimizing the performance and



**Fig. 1** The schematic illustration details the sandwich structure of a perovskite solar cell in two configurations: n-i-p and p-i-n (a and b). It further illustrates the n-i-p configuration with a mesoporous structure (c), and demonstrates the process of charge generation under light, highlighting potential charge recombination pathways, including radiative ( $h\nu$ ) and thermal ( $\Delta$ ) recombinations (d).



efficiency of perovskite solar cells. Printed perovskite solar cells typically consist of multiple layers, including a transparent conductive electrode (such as indium tin oxide, ITO), a perovskite absorber layer, hole transport layer (HTL), electron transport layer (ETL), and metal contacts. Based on the solar cell construction, top layer's stability, fabrication temperatures, and device performance, one can choose to work with either n-i-p or p-i-n structures. The ETL, Perovskite, and HTL layers are deposited in a sequence over the conducting substrate to produce n-i-p structure and *vice versa*.

Upon absorption of a photon from the solar radiation, the electron will be excited from the valence band to its conduction band (CB), leaving holes in the valence band (VB), as it is represented in Fig. 1b. Since the perovskite layer is sandwiched in between the ETL and the HTL. The photoelectron is transported to the load by the ETL, and the hole will be scavenged by the HTL. This directional movement of charges is driven by the built-in potential and the electric field within the device. Thus, the perovskite layer can produce electricity continuously out from the device until we stop irradiating the PSC. Under

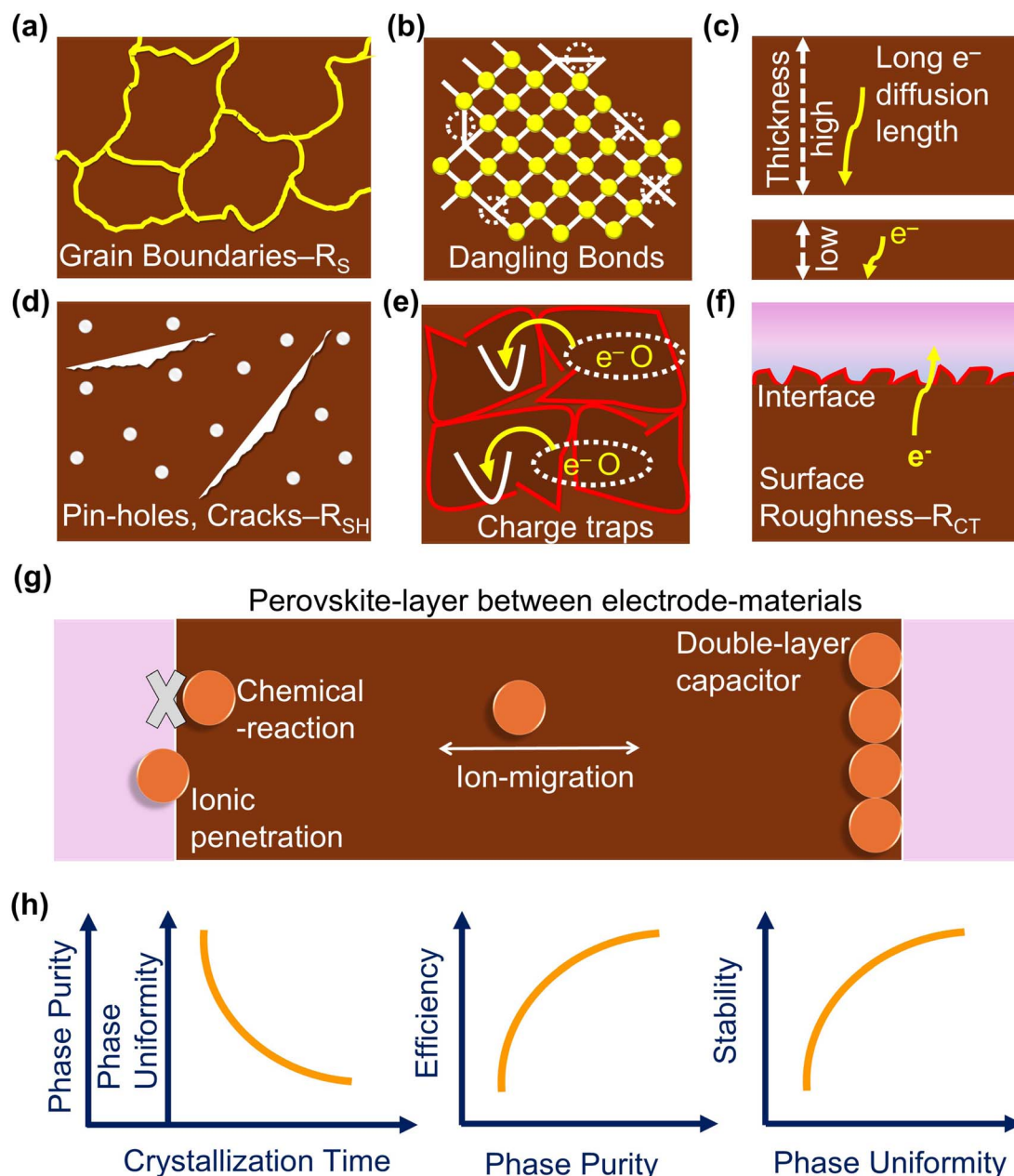


Fig. 2 Key performance-influencing factors are identified, such as grain boundaries (a), dangling bonds on the perovskite surface (b), excessive thickness causing charge trapping (c), cracks and pinholes (d), and charge traps from all these lattice defects (e), surface roughness (f). Illustration of possible chemical reactivity, ion diffusion, double-layer capacitor formation, and ionic penetration within the perovskite layer under applied bias conditions (g). Additionally, the schematic explores the relationship between perovskite phase purity and perovskite crystallization time, the correlation between PSC efficiency and phase purity, and the impact of phase uniformity on device stability (h).



irradiation, three key processes occur in PSCs. The first is charge generation, where the perovskite layer acts as the primary light-absorbing material. The second is charge separation, facilitated by the interfaces between the perovskite, HTL, and ETL, which are crucial for efficient charge extraction. Finally, charge recombination can occur, often due to the presence of pinholes, cracks, or poor interfacial properties, which lead to the loss of charge carriers and diminished device performance.

The potential charge trapping defects and other challenges faced by perovskite materials are illustrated schematically in Fig. 2a–f. This figure highlights the key issues affecting perovskite performance, providing a visual representation of the various defects and obstacles that impact charge transport and overall efficiency. Compared to the lab-scale spin-coating method, open-air printing techniques encounter significant challenges in growing perovskite films. In open-air conditions, there is no control over oxygen and moisture exposure. If the perovskite formulation is not optimized, this can result in uncontrolled and non-uniform perovskite crystallization, leading to grain boundaries and surface dangling bonds. These imperfections are particularly vulnerable to air and moisture, resulting in poor interfaces and reduced charge separation efficiency. Additionally, the thickness of the perovskite film in large-scale production tends to be irregular, in contrast to the more consistent layers produced in lab-scale settings. This irregularity can cause photoelectrons to become trapped at defect sites, hindering their transport to charge collectors. Moreover, the lack of control over surface roughness in large-scale production further exacerbates the problem, increasing the series resistance ( $R_s$ ) and hampering efficient charge separation. Controlling perovskite thickness remains a significant

challenge. The formation of cracks and pinholes during large-scale production further degrades performance, as these defects reduce shunt resistance ( $R_{SH}$ ), promote radiative charge recombination, and ultimately lead to poor PCE. Moreover, PSCs exhibit hysteresis in current-voltage measurements, primarily attributed to ion migration. Under applied voltage, halide ions and organic cations tend to migrate, causing chemical reactions at interfaces, penetration into electrode materials, and the formation of ionic double layers (Fig. 2g). These processes contribute to reduced device efficiency and stability. Additionally, the phase purity and uniformity of the perovskite material are strongly influenced by crystallization time (Fig. 2h). In open-air conditions, delayed crystallization often leads to suboptimal perovskite growth, significantly impairing both the overall efficiency and the long-term stability of PSCs.

To address this issue, researchers have employed various strategies such as encapsulation with moisture-resistant materials, interface engineering to minimize moisture ingress, and developing moisture-resistant perovskite compositions.

The degradation mechanisms of halide perovskites in open air typically involve the reaction of the halide ions (*e.g.*, iodide, bromide, or chloride) with moisture and oxygen. One of the key reactions is the oxidation of the halide ions by oxygen, leading to the formation of halogen gases (*e.g.*, iodine, bromine, or chlorine) and other byproducts. For example, in the case of methylammonium lead iodide perovskite, results in the formation of lead iodide ( $PbI_2$ ), methylamine ( $CH_3NH_2$ ), molecular iodine ( $I_2$ ), and water ( $H_2O$ ), leading to the degradation of the perovskite structure and a decrease in device performance. Halide perovskites are also prone to thermal degradation, especially at elevated temperatures encountered

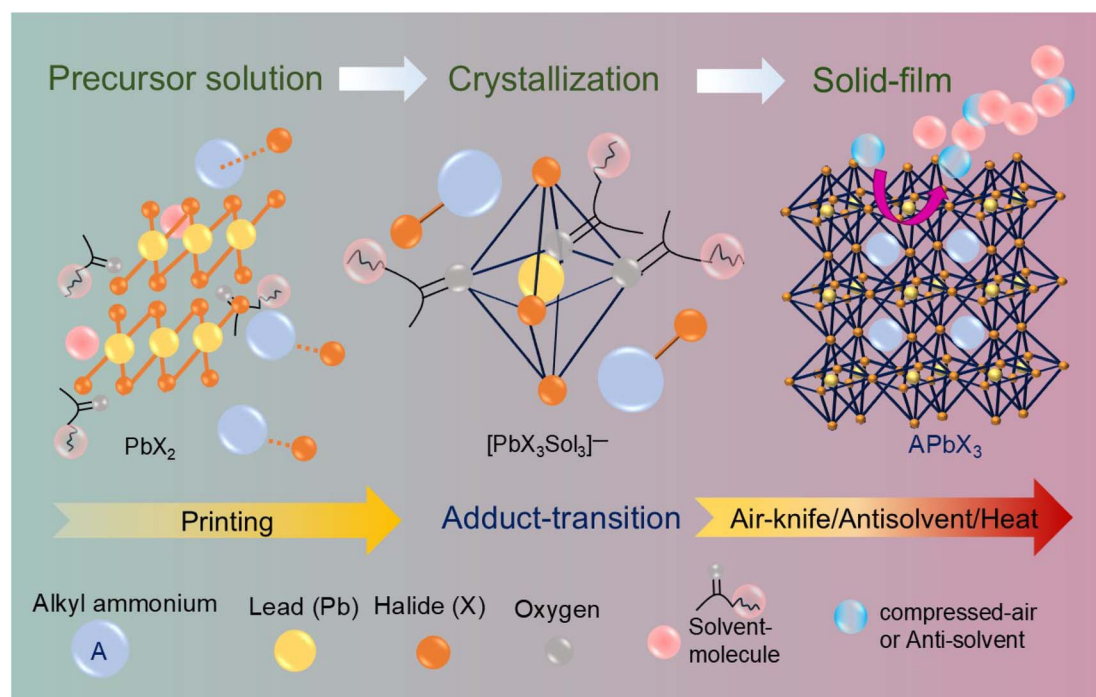


Fig. 3 The schematic depicts the perovskite thin film formation from its solution phase.



during device fabrication processes or under operational conditions.<sup>35,36</sup>

Regardless of the perovskite deposition method, a critical step in device fabrication involves precisely controlling the perovskite layer's thickness, morphology, and crystallinity during the crucial phase transition from solution to solid film, as illustrated in the schematic (Fig. 3). The most commonly used solvents in the spin-coating approach are *N,N*-dimethylformamide (DMF) and dimethyl sulfoxide (DMSO). However, these solvents are less frequently used in large-scale printing techniques. For instance, Mai and his team used *N*-methyl-2-pyrrolidinone (NMP) that forms a stronger coordination with  $\text{PbI}_2$  compared to DMF or DMSO. This characteristic plays a crucial role in achieving uniform crystalline perovskite thin films through the blade-coating approach.<sup>37</sup> However, aprotic solvents are not suitable for all perovskite formulations. For example, 1-methoxy-2-propanol (PM) has proven to be an effective co-solvent in the inkjet printing of uniform perovskite thin films.<sup>38</sup> Similarly, in the blade-coating approach, 2-methoxyethanol is identified as an efficient solvent.<sup>39</sup> This underscores the importance of carefully selecting appropriate solvents for perovskite processing. The illustration below demonstrates how lead halide coordinates with solvent molecules and alkylamines in the precursor solution state. This coordination also persists in the adduct state, where the thin film is initially deposited. However, the adduct form remains stable for only a few seconds, as the solvent molecules rapidly evaporate. To achieve better and more uniform crystallization, techniques such as antisolvent treatment or air-knife-assisted perovskite crystallization are employed. These methods facilitate the removal of solvent molecules, promoting the formation of crystalline films. In particular, the interaction between the antisolvent or the compressed air pressure, as well as the air-knife's duration over the film, plays a crucial role in ensuring the complete extraction of residual solvent molecules from the evolving perovskite lattice.<sup>40–42</sup>

### 3. Large-scale deposition methods

Printed perovskite solar cells represent a promising avenue in the field of photovoltaics, combining the high efficiency potential of perovskite materials with the scalability and cost-effectiveness of printing techniques. These solar cells are fabricated by depositing of perovskite materials and other functional layers onto a substrate using various printing methods such as inkjet printing, screen printing, blade coating, or roll-to-roll coating. Inkjet printing, for example, enables precise droplet deposition, while screen printing allows for large-area patterning can be used for producing semi-transparent layers without chemical modifications for building-integrated photovoltaics (BIPVs). Whereas, the blade coating and slot-die coating offer continuous deposition over large areas. The Perovskite inks are formulated by dissolving perovskite precursors, such as lead halides and organic cations, in suitable solvents. Additives may be included to optimize ink properties, such as viscosity, surface tension, and drying behavior. Formulating stable and reproducible inks is essential for successful printing. Once the successful ink is formulated, the

next step is printing the so + lar cell. Printing techniques allow for precise deposition of each layer, facilitating the fabrication of efficient solar cells. However, in recent times, the current research is highly focused on finding protocols of developing perovskite layer. This includes the development of stable perovskite compositions, interface engineering to improve moisture resistance, and the integration of advanced encapsulation techniques to protect against both moisture and heat-induced degradation, discussed below for every printing method.

The importance of low-temperature processability has led to the use of multiple approaches for producing the PSCs. Thus, the perovskite precursors are used as inks suitable for printing/coating approaches. However, the perovskite morphology and crystallization is highly dependent on each method with processing conditions. Two different approaches can be used to fabricate the perovskite layer, in the first approach (contact method), this technique involves contact between the perovskite precursor and a sharp metal part of the instrument, thus the distance that is maintained between the substrate and the metal contact controls the perovskite layer thickness. In this contact approach, the perovskite layer will be grown from blade coating, roll-to-roll slot-die, and screen printing or mesh-assisted methods. Whereas in the second approach (non-contact method), there is no direct contact between the drying perovskite layer and the instrument. In this non-contact approach, the perovskite layer will be grown from spray coating, inkjet printing. Based on the required perovskite layer thickness, morphology, dimensional control and the feasibility, the contact or non-contact perovskite printing approach can be chosen. Both contact and non-contact approaches are schematically shown in the Fig. 4.

In printing techniques, the key strategy is to apply materials during the critical adduct transition phase. Consequently, much of the research has focused on ink and solvent engineering. To optimize open-air printable methods for PSCs several innovations have emerged recently. These include solvent engineering, ink formulation, passivation strategies, modifications of the interfacial layers, improvements in deposition methods, and advancements in both pre-and post-deposition processes. The table below (Table 1) summarizes key findings from the literature concerning the development of various printing technologies. It specifically details the performance metrics of PSC configurations produced under open-air conditions, with efficiency parameters provided for each perovskite printing method.

For the fabrication of stable PSCs, the formulation of mixed cations and mixed halides has been widely reported as an effective strategy.<sup>86–88</sup> This review examines key advancements in ink engineering, including perovskite formulations with additives, solvent optimization, surface treatments, and process innovations, all implemented across various open-air printing techniques are discussed below.

#### 3.1. Blade-coating approach, advancement strategies

Blade coating, also known as the doctor-blading approach, involves depositing a thin layer of perovskite precursor solution



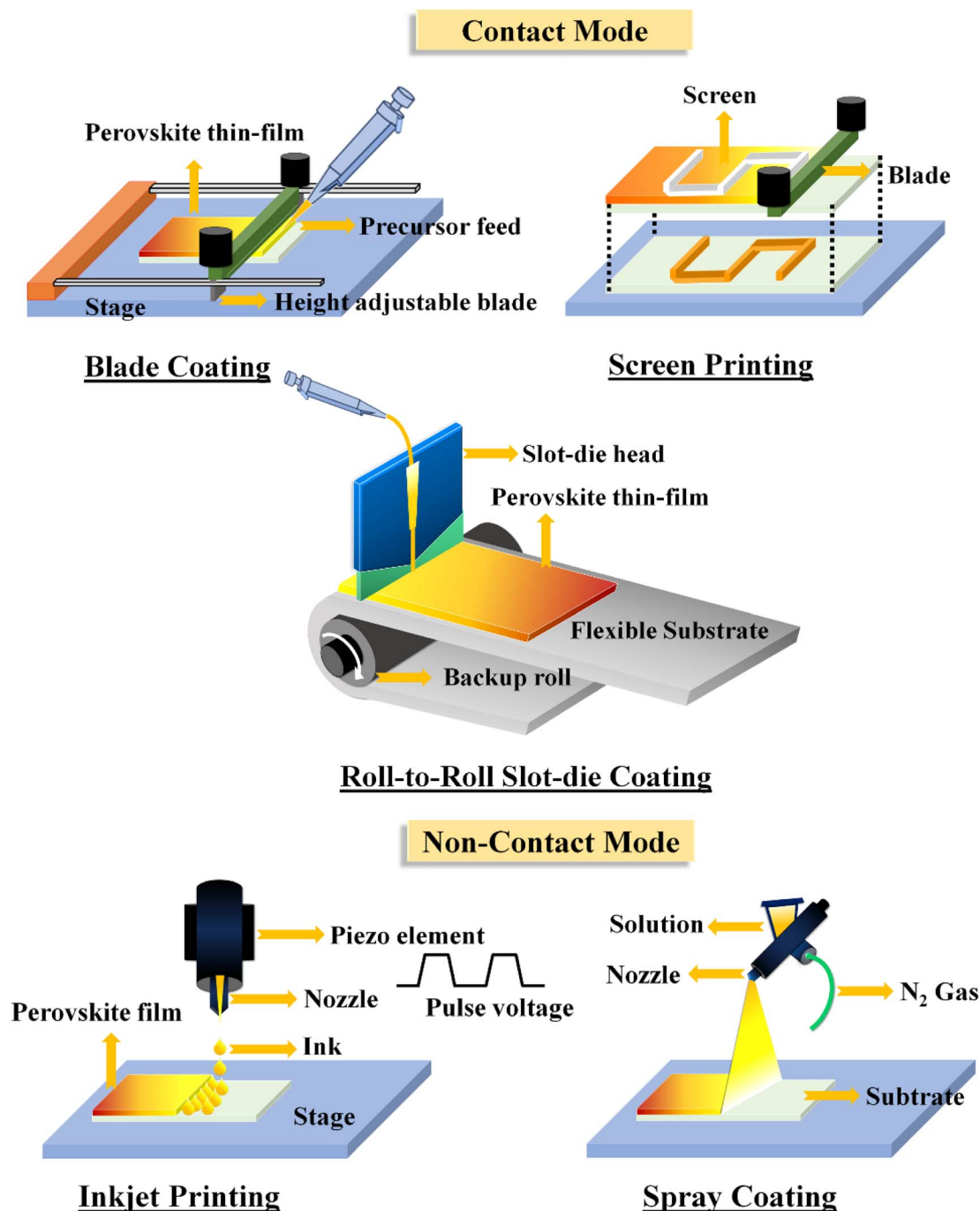


Fig. 4 The diagram illustrates both contact and non-contact methods for applying a perovskite solution onto a substrate.

onto a substrate using a moving blade apparatus. In blade coating, the thickness of the deposited film is determined by the gap between the blade and the substrate, as well as the properties of the solution, such as viscosity and surface tension. In the coating, the substrate will be placed over the stage then the perovskite precursor will be dropped, without further delay, a blade will be moved over the solution, to form a thin layer on top of the substrate. The concentration of the perovskite ink, blade moving speed, solvent evaporation rate *etc.*, influences the quality of the perovskite film morphology. During this

process, there is a precise control over the thickness of the solution deposited onto the substrate. Compared to Spin-coating, it has very low material waste and reduced manufacturing costs. This method can be also used to deposit various layers in the perovskite solar cell stack, including the perovskite absorber layer, HTL, and ETL. This versatility makes it a valuable technique for the fabrication of multi-layered devices. However, there are a few challenges, perovskite precursor solutions need to be carefully formulated to ensure stability during the coating process. Achieving optimal coating





Table 1 The table below represents the recent report on the fabrication of Perovskite solar cells using different open-air processable printing techniques, processed in an ambient conditions

| Device configuration                                                                                                                                                                                | Printing method                                            | $J_{sc}$<br>( $\text{mA cm}^{-2}$ ) | $V_{oc}$<br>(V) | FF<br>(%) | Efficiency<br>(%) | Progression                                                       | Substrate<br>condition                            | Anti solvent<br>treatment | References<br>(year) |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------|-------------------------------------|-----------------|-----------|-------------------|-------------------------------------------------------------------|---------------------------------------------------|---------------------------|----------------------|
| ITO/PTAA/PSK/PC <sub>70</sub> BM/BCP/Ag<br>perovskite:PSK (MA <sub>0.7</sub> FA <sub>0.3</sub> PbI <sub>3</sub> )                                                                                   | Blade coating: only PSK                                    | 24.61                               | 1.15            | 79.9      | 22.7              | Surface-treatment                                                 | RT, ambient air,<br>RH $\sim 15 \pm 5\%$          | No                        | 43 (2024)            |
| FTO/NiO <sub>x</sub> -Zn/PSK/PC <sub>61</sub> BM/BCP/Ag<br>(PSK: MAPbCl <sub>3</sub> )                                                                                                              | Blade coating: only PSK                                    | 18.23                               | 1.06            | 74.7      | 14.4              | Solvent-engineering                                               | 150 °C, ambient<br>air, RH% (NA)                  | No                        | 44 (2024)            |
| Glass/ITO/SnO <sub>2</sub> /PSK/Spiro-OMeTAD/Au<br>(PSK: Cd-FAPbI <sub>3</sub> )                                                                                                                    | Blade coating: SnO <sub>2</sub> , PSK<br>and Spiro-OMeTAD. | 25.9                                | 1.10            | 79.6      | 22.7              | Ink-engineering                                                   | RT, ambient air,<br>RH $\sim 35\%$                | No                        | 45 (2024)            |
| FTO-glass/SnO <sub>2</sub> /PSK/carbon<br>(PSK: FAPbBr <sub>3</sub> )                                                                                                                               | Blade coating: SnO <sub>2</sub> , PSK                      | 8.47                                | 1.57            | 82.0      | 10.85             | <i>In situ</i> defect-<br>passivation                             | RT, ambient air,<br>RH $\sim 20 \pm 5\%$          | No                        | 46 (2024)            |
| FTO/bTiO <sub>2</sub> /SnO <sub>2</sub> /PSK/Spiro-OMeTAD/Au<br>(PSK: ((FAPbI <sub>3</sub> ) <sub>0.95</sub> (MAPbBr <sub>3</sub> ) <sub>0.05</sub> ))                                              | Blade coating: SnO <sub>2</sub> , PSK                      | 23.8                                | 1.16            | 85.0      | 23.4              | Ink-engineering                                                   | RT, ambient air,<br>RH $\sim 25\%$                | No                        | 47 (2023)            |
| ITO/SnO <sub>2</sub> /PSK@KSCN/Spiro-OMeTAD/<br>Au (PSK: MAPbI <sub>3</sub> )                                                                                                                       | Blade coating: PSK and<br>Spiro-OMeTAD                     | 22.62                               | 1.116           | 80.8      | 20.40             | Ink-additive<br>engineering (KSCN<br>addition)                    | RT, ambient air,<br>RH% (NA)                      | No                        | 48 (2023)            |
| Glass/ITO/PTAA/PSK-SCW/PEACI/C <sub>60</sub> /<br>BCP/Cu (PSK: MAPbI <sub>3</sub> )                                                                                                                 | Blade coating: only PSK                                    | 22.75                               | 1.11            | 80.0      | 20.05             | Ink-additive<br>engineering (PEACI<br>addition)                   | RT, ambient air,<br>RH $\sim 30\%$                | No                        | 49 (2023)            |
| FTO/C-TiO <sub>2</sub> /TiO <sub>2</sub> /PSK/Spiro-OMETAD/<br>Au (PSK: CH <sub>3</sub> NH <sub>3</sub> PbI <sub>3</sub> )                                                                          | Blade coating: only PSK                                    | 18.9                                | 1.0             | 70.5      | 13.3              | Crystallization of<br>PbI <sub>2</sub> with air-flow              | Air flow 100 °C,<br>RH% (NA)                      | No                        | 50 and 51<br>(2023)  |
| Glass/ITO/PTAA/PSK@BTACI/C <sub>60</sub> /BCP/<br>Ag (PSK: MAPbI <sub>3</sub> )                                                                                                                     | Blade coating: only PSK                                    | 22.5                                | 1.13            | 81.3      | 20.5              | Additive assist-<br>passivation<br>technique, stability           | RT, ambient air,<br>RH of $<50\%$                 | No                        | 51 and 52<br>(2022)  |
| Glass/ITO/SAM/PSK/C <sub>60</sub> /BCP/Ag<br>(PSK: MAPbI <sub>3</sub> )                                                                                                                             | Blade coating: only PSK                                    | 21.5                                | 1.08            | 79.2      | 18.4              | HTL surface<br>engineering-<br>improved perovskite<br>wettability | RT, ambient air,<br>RH of $\leq 50\%$             | No                        | 52 (2022)            |
| Glass/FTO/C-TiO <sub>2</sub> /mp TiO <sub>2</sub> /PSK/CB:Two<br>bis(alkoxy)diphenylaminocarbazole/Ag<br>(PSK: CH <sub>3</sub> NH <sub>3</sub> PbI <sub>3</sub> )                                   | Blade coating: both PSK<br>and HTL                         | 23.6                                | 1.15            | 78.0      | 21.1              | Dopant-free HTL for<br>printing techniques                        | 130 °C, ambient<br>air, RH $\sim 30\text{--}40\%$ | No                        | 53 (2022)            |
| Glass/ITO/PEDOT:PSS/PSK/PCBM/BCP/<br>Ag (PSK: CH <sub>3</sub> NH <sub>3</sub> PbI <sub>3</sub> )                                                                                                    | Blade coating:<br>PEDOT:PSS,PSK, PCBM<br>and BCP           | 21.1                                | 1.02            | 69.1      | 14.1              | Buffer layer to block<br>hole transfer                            | RT, ambient air,<br>RH $\sim 35\text{--}50\%$     | No                        | 54 (2020)            |
| Glass/ITO/PSK + Me-4PACz/C <sub>60</sub> /(BCP)/Ag<br>(PSK: Cs <sub>0.05</sub> (FA <sub>0.98</sub> MA <sub>0.02</sub> ) <sub>0.95</sub><br>Pb(I <sub>0.98</sub> Br <sub>0.02</sub> ) <sub>3</sub> ) | Blade coating: PSK + SAM                                   | 23.88                               | 1.16            | 81.23     | 22.1              | Co-deposition of<br>perovskite and HTL                            | RT, ambient air,<br>RH $\sim 40\%$                | No                        | 55 (2023)            |
| Glass/ITO/NiO <sub>x</sub> /SAM/PSK/PCBM/BCP/Ag<br>(PSK: MAPbI <sub>3</sub> )                                                                                                                       | Spray coating: only PSK                                    | 23.13                               | 1.06            | 82.0      | 20.3              | Wetability/<br>interfacial<br>engineering                         | 40 °C, ambient<br>air RH% (NA)                    | No                        | 56 (2024)            |
| FTO/SnO <sub>2</sub> /PSK( <i>n</i> -propylammonium<br>chloride)/PC <sub>61</sub> BM/Au (PSK: FAI/FABr/<br>PACl)                                                                                    | Spray coating: only PSK                                    | 20.33                               | 1.17            | 81.6      | 19.42             | Additive<br>engineering                                           | RT, ambient air,<br>RH $\sim 40\%$                | No                        | 57 (2023)            |
| PEN/ITO/PTAA/PSK/C <sub>60</sub> /BCP/Au<br>(PSK: (CsPbI <sub>3</sub> ) <sub>0.02</sub> (FA <sub>0.8</sub><br>MA <sub>0.2</sub> Pb(I <sub>2.8</sub> Br <sub>0.2</sub> )) <sub>0.98</sub> )          | Spray coating: only PSK                                    | 22.4                                | 1.06            | 75.7      | 18.04             | Uniform film on<br>flexible substrate                             | 60 °C ambient<br>air, RH% (NA)                    | No                        | 58 (2022)            |



Table 1 (Contd.)

| Device configuration                                                                                                                                  | Printing method                                                                                            | $J_{sc}$<br>( $\text{mA cm}^{-2}$ ) | $V_{oc}$<br>(V) | FF<br>(%) | Efficiency<br>(%) | Progression                                                        | Substrate<br>condition           | Anti solvent<br>treatment | References<br>(year) |
|-------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------|-------------------------------------|-----------------|-----------|-------------------|--------------------------------------------------------------------|----------------------------------|---------------------------|----------------------|
| FTO/c-TiO <sub>2</sub> /PSK/MoO <sub>3</sub> -with-5.0 wt% PTAA/carbon black (CB) submodule (PSK: CsPbI <sub>2</sub> Br)                              | Spray coating: all layers                                                                                  | 107.17                              | 3.32            | 70.85     | 10.08             | Additive assist-<br>wettability                                    | 60 °C, ambient<br>air, RH% (NA)  | No                        | 59 (2022)            |
| Glass/ITO/c-TiO <sub>2</sub> /m-TiO <sub>2</sub> /perovskite/<br>Spiro-OMeTAD/Au                                                                      | Spray coating: Only PSK<br>2nd step                                                                        | 19.11                               | 0.91            | 56.0      | 9.86              | Defect formation<br>mechanism                                      | 50 °C, ambient<br>air, RH% (NA)  | No                        | 60 (2023)            |
| ITO/PTAA/PSK/OMXene-CsPbI <sub>3</sub><br>composite/CPTA/BCP/Ag (PSK: CsPbI <sub>3</sub> )                                                            | Spray coating: only PSK                                                                                    | 19.86                               | 1.21            | 81.9      | 19.69             | Surface engineering                                                | 170 °C, ambient<br>air, RH% (NA) | No                        | 61 (2022)            |
| ITO/NiO <sub>x</sub> /PSK/C <sub>60</sub> /BCP/Ag (PSK:<br>CH <sub>3</sub> NH <sub>3</sub> PbI <sub>3</sub> )                                         | Spray coating: only PSK                                                                                    | 22.04                               | 1.00            | 80.0      | 17.43             | Additive assisted<br>perovskite<br>crystallization                 | Ambient air, 40 °<br>C, RH% (NA) | No                        | 62 (2022)            |
| Glass/ITO/c-TiO <sub>2</sub> /m-TiO <sub>2</sub> /PSK/Spiro-<br>OMeTAD/Au (PSK: MAPbI <sub>3</sub> )                                                  | Spray coating: only PSK                                                                                    | 21.40                               | 1.02            | 74.7      | 16.34             | Argon assisted spray<br>coating                                    | RT, ambient air,<br>RH% (NA)     | No                        | 63 (2022)            |
| FTO/compact-TiO <sub>2</sub> /mp-TiO <sub>2</sub> /MAPbI <sub>3</sub> /mp-<br>ZrO <sub>2</sub> /mp-carbon (PSK: MAPbI <sub>3</sub> )                  | Screen printing: TiO <sub>2</sub> , ZrO <sub>2</sub> ,<br>and carbon layers<br>(PSK is dropped)            | 24.31                               | 0.93            | 68.12     | 15.39             | Additive -assisted<br>perovskite<br>crystallization                | RT, ambient air,<br>RH% (NA)     | No                        | 64 (2023)            |
| FTO/TiO <sub>2</sub> /ZrO <sub>2</sub> /PSK/carbon (PSK: FAPbI <sub>3</sub> )                                                                         | Screen printing: TiO <sub>2</sub> , ZrO <sub>2</sub> ,<br>and carbon layers (PSK is<br>dropped)            | 22.08                               | 1.02            | 76.0      | 17.11             | $\alpha/\delta$ phase perovskite<br>interface enhanced<br>$V_{oc}$ | RT, ambient air,<br>RH% (NA)     | No                        | 65 (2022)            |
| Glass/FTO/c-TiO <sub>2</sub> /PSK/ZrO <sub>2</sub> /C-layer<br>(PSK: MAPbI <sub>3</sub> )                                                             | Screen printing: TiO <sub>2</sub> , ZrO <sub>2</sub> ,<br>and carbon layers<br>(PSK is dropped)            | 23.3                                | 0.96            | 73.0      | 16.32             | Influenced<br>precursor<br>concentration                           | RT, ambient air,<br>RH% (NA)     | No                        | 66 (2020)            |
| Glass/FTO/c-TiO <sub>2</sub> /ZrO <sub>2</sub> /C-layer/PSK<br>(PSK: CH <sub>3</sub> NH <sub>3</sub> PbI <sub>3-x</sub> Cl <sub>x</sub> )             | Screen printing: TiO <sub>2</sub> , ZrO <sub>2</sub> ,<br>and carbon layers<br>(PSK is blade coated)       | 20.01                               | 0.96            | 60.0      | 11.53             | Compact layer<br>deposited from<br>chemical bath                   | 100 °C, ambient<br>air, RH% (NA) | No                        | 67 (2019)            |
| Glass/FTO/c-TiO <sub>2</sub> /TiO <sub>2</sub> /Al <sub>2</sub> O <sub>3</sub> /NiO/PSK/C<br>(PSK: CH <sub>3</sub> NH <sub>3</sub> PbI <sub>3</sub> ) | Screen printing: TiO <sub>2</sub> ,<br>Al <sub>2</sub> O <sub>3</sub> and NiO layer<br>(PSK is dip coated) | 21.62                               | 0.91            | 76.0      | 15.03             | Additional NiO<br>interlayer for charge<br>separation              | 70 °C, ambient<br>air, RH% (NA)  | No                        | 68 (2015)            |
| FTO/compact-TiO <sub>2</sub> /mp-TiO <sub>2</sub> /mp-ZrO <sub>2</sub> /<br>mp-carbon/PSK (PSK: MAI)                                                  | Screen printing: TiO <sub>2</sub> , ZrO <sub>2</sub> ,<br>and carbon layers<br>(PSK is drop casted)        | 24.3                                | 0.97            | 65        | 15.4              | Low-temperature<br>processed mp-<br>carbon                         | RT, ambient air,<br>RH ~40%      | No                        | 69 (2022)            |
| FTO/compact-TiO <sub>2</sub> /mp-TiO <sub>2</sub> /mp-ZrO <sub>2</sub> /<br>mp-carbon/FA-perovskite                                                   | Screen printing: TiO <sub>2</sub> ZrO <sub>2</sub><br>and carbon<br>(PSK is drop casted)                   | 23.74                               | 0.98            | 78        | 18.3              | Additive-assisted<br>perovskite<br>crystallization                 | RT, ambient air,<br>RH% (NA)     | No                        | 70 (2023)            |
| ITO/SnO <sub>2</sub> /PSK/Spiro-OMeTAD/Au (PSK:<br>PbI <sub>2</sub> + FAIEMABR:MACI)                                                                  | R2R: SnO <sub>2</sub> and PSK<br>(PSK is drop casted)                                                      | 21.31                               | 1.09            | 72.9      | 16.87             | IPL for annealing                                                  | RT, ambient air,<br>RH ~20–30%   | No                        | 71 (2024)            |
| ITO-PET/SnO <sub>2</sub> /PSK/P3HT/C (PSK: MAPI)                                                                                                      | R2R: SnO <sub>2</sub> , PSK and P3HT                                                                       | 16.93                               | 1.01            | 56.95     | 9.8               | Finding compatible<br>HTL for carbon<br>electrode                  | RT, ambient air,<br>RH% (NA)     | No                        | 72 (2024)            |
| FTO/In-TiO <sub>2</sub> /mp-TiO <sub>2</sub> /Na-TFSI/<br>Perovskite/Spiro-OMeTAD/Au (module)                                                         | R2R: TiO <sub>2</sub> , PSK, and<br>Spiro-OMeTAD                                                           | 2.55                                | 10.25           | 76.29     | 19.9              | Additives, echo<br>friendly solvents                               | RT, ambient air,<br>RH% (NA)     | No                        | 73 (2023)            |
| ITO/SnO <sub>2</sub> /MAPI/PEDOT/carbon (PSK:<br>MAPI)                                                                                                | R2R: All the layers                                                                                        | 20.91                               | 0.89            | 65.1      | 13.26             | All roll-to-roll<br>printed                                        | RT, ambient air,<br>RH% (NA)     | No                        | 74 (2023)            |
| ITO/PTAA/Ionogel-perovskite/choline<br>chloride/C <sub>60</sub> /BCP/Cu                                                                               | R2R: PTAA and PSK                                                                                          | 22.21                               | 1.19            | 82.33     | 21.76             | Additive-assisted<br>perovskite<br>crystallization                 | 65 °C, ambient<br>air, RH% (NA)  | No                        | 75 (2022)            |



Table 1 (Contd.)

| Device configuration                                                                                                                                                                                                                                                  | Printing method                                     | $J_{sc}$<br>(mA cm <sup>-2</sup> ) | $V_{oc}$<br>(V) | FF<br>(%) | Efficiency<br>(%) | Progression                                                                              | Substrate<br>condition                 | Anti solvent<br>treatment       | References<br>(year) |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------|------------------------------------|-----------------|-----------|-------------------|------------------------------------------------------------------------------------------|----------------------------------------|---------------------------------|----------------------|
| PET/TCE/SnO <sub>2</sub> /PSK/Spiro-OMeTAD/<br>carbon/Ag (PSK: Cs <sub>0.05</sub> FA <sub>0.81</sub><br>MA <sub>0.14</sub> PbI <sub>2.55</sub> Br <sub>0.45</sub> )                                                                                                   | R2R: SnO <sub>2</sub> , PSK and<br>Spiro-OMeTAD     | 20.9                               | 1.17            | 68.1      | 16.7              | Vacuum and<br>solvent-free                                                               | 17–21 °C,<br>ambient air RH<br>~30–60% | No                              | 76 (2022)            |
| ITO glass/SnO <sub>2</sub> /PSK/Spiro-OMeTAD/Ag<br>(PSK: CsPbI <sub>3</sub> )                                                                                                                                                                                         | R2R: SnO <sub>2</sub> , PSK and<br>Spiro-OMeTAD     | 21.45                              | 1.0             | 60.59     | 13.0              | All roll-to-roll<br>printed                                                              | 70 °C, ambient<br>air, RH% (NA)        | No                              | 77 (2022)            |
| ITO/SnO <sub>2</sub> /PSK/Spiro-OMeTAD/Ag<br>(PSK: FAPbI <sub>3</sub> )                                                                                                                                                                                               | Inkjet printing: Only PSK                           | 19.87                              | 1.207           | 73.16     | 17.5              | Ink engineering                                                                          | Ambient air, RT<br>and RH ~30–<br>35%  | No                              | 78 (2024)            |
| ITO/SnO <sub>2</sub> /PSK/spiro-OMeTAD/Ag<br>(PSK: CsFAMAPbBr <sub>x</sub> I <sub>3-x</sub> )                                                                                                                                                                         | Inkjet printing: Only PSK                           | 18.32                              | 1.187           | 77.73     | 16.90             | Focused on ETL                                                                           | 23 °C, ambient<br>air, RH ~40%         | No                              | 79 (2023)            |
| PEN/ITO/NiO <sub>x</sub> /polymer pillar/PSK/<br>PCBM/BCP/Ag (PSK:<br>Cs <sub>0.2</sub> FA <sub>0.8</sub> PbI <sub>2.55</sub> Br <sub>0.45</sub> )                                                                                                                    | Inkjet printing: polymer-<br>pillar, and perovskite | 11.7                               | 1.06            | 73.55     | 9.14              | Solvent engineering,<br>digital control,<br>flexible and<br>semitransparent for<br>BIPVs | Ambient air, RT,<br>RH% (NA)           | No                              | 38 (2023)            |
| FTO/c-TiO <sub>2</sub> /m-TiO <sub>2</sub> /PSK/carbon<br>(PSK: CsPbBr <sub>3</sub> )                                                                                                                                                                                 | Inkjet printing: only PSK                           | 7.36                               | 1.51            | 81.7      | 9.09              | Device structural<br>engineering                                                         | 60 °C, ambient<br>air, RH ~35%         | No                              | 80 (2022)            |
| FTO/TiO <sub>2</sub> /PSK/Spiro-OMeTAD/Au<br>(PSK: MAPbI <sub>3</sub> /MAPbBr <sub>3</sub> )                                                                                                                                                                          | Inkjet printing: only<br>MAPbBr <sub>3</sub> QDs    | 21.69                              | 1.21            | 75.0      | 17.06             | Intense pulse light<br>sintering                                                         | RT, ambient air,<br>RH% (NA)           | No                              | 81 (2021)            |
| PEN/AgNWs/PEDOT: PSS/PSK/PC <sub>71</sub> BM/<br>PEI/Ag NWs (PSK: CH <sub>3</sub> NH <sub>3</sub> PbI <sub>3</sub> )                                                                                                                                                  | Inkjet printing: all the<br>layers                  | 21.96                              | 1.02            | 75.0      | 16.78             | All inkjet printing                                                                      | 50 °C, ambient<br>air, RH% (NA)        | Yes (ethyl<br>acetate<br>fumes) | 82 (2021)            |
| PET/IZO/PEDOT: PSS/PSK/BCP/Ag<br>(PSK:<br>Cs <sub>0.1</sub> [(HC(NH <sub>2</sub> ) <sub>2</sub> ) <sub>0.83</sub> (CH <sub>3</sub> NH <sub>3</sub> ) <sub>0.17</sub> ] <sub>0.9</sub> Pb<br>(I <sub>0.83</sub> Br <sub>0.17</sub> ) <sub>3</sub> )                    | Inkjet printing: only PSK                           | 19.0                               | 1.0             | 69.2      | 11.4              | Additive<br>engineering, green<br>solvent                                                | RT, ambient air,<br>RH ~20–25%         | No                              | 83 (2021)            |
| FTO/TiO <sub>2</sub> /C <sub>60</sub> /Cs <sub>0.05</sub> MA <sub>0.14</sub><br>FA <sub>0.81</sub> PbI <sub>2.55</sub> Br <sub>0.45</sub> /SpiroOMeTAD/Au.<br>(PSK: Cs <sub>0.05</sub> MA <sub>0.14</sub> FA <sub>0.81</sub> PbI <sub>2.55</sub> Br <sub>0.45</sub> ) | Inkjet printing: only PSK                           | 23.48                              | 1.108           | 76.2      | 19.6              | Ink engineering                                                                          | RT, ambient air,<br>and RH ~25%        | No                              | 84 (2020)            |
| Glass/ITO/NiO <sub>x</sub> /TCP/PCBM/BCP/Au                                                                                                                                                                                                                           | Inkjet printing: all layers                         | 23.6                               | 1.02            | 71.5      | 17.2              | All inkjet printed                                                                       | RT, ambient air,<br>and RH ~45%        | No                              | 85 (2020)            |

conditions requires careful optimization of parameters such as solution concentration, coating speed, blade geometry, and substrate temperature. Variations in these parameters can affect film morphology, crystallinity, and device performance. Here we focus on the improvements achieved by incorporating additives, engineering solvents, and utilizing low-dimensional perovskites *via* blade-coating approach.

The key challenges in this method lie in optimizing the perovskite ink to achieve the appropriate wettability and in stabilizing the perovskite film under open-air conditions. This includes high-end crystallization process, protecting the surface of the blade-coated perovskite layer making it rigid towards moisture air, and thus the required interfacial engineering, and ink-engineering techniques, which are critically examined based on recent advancements in the literature.

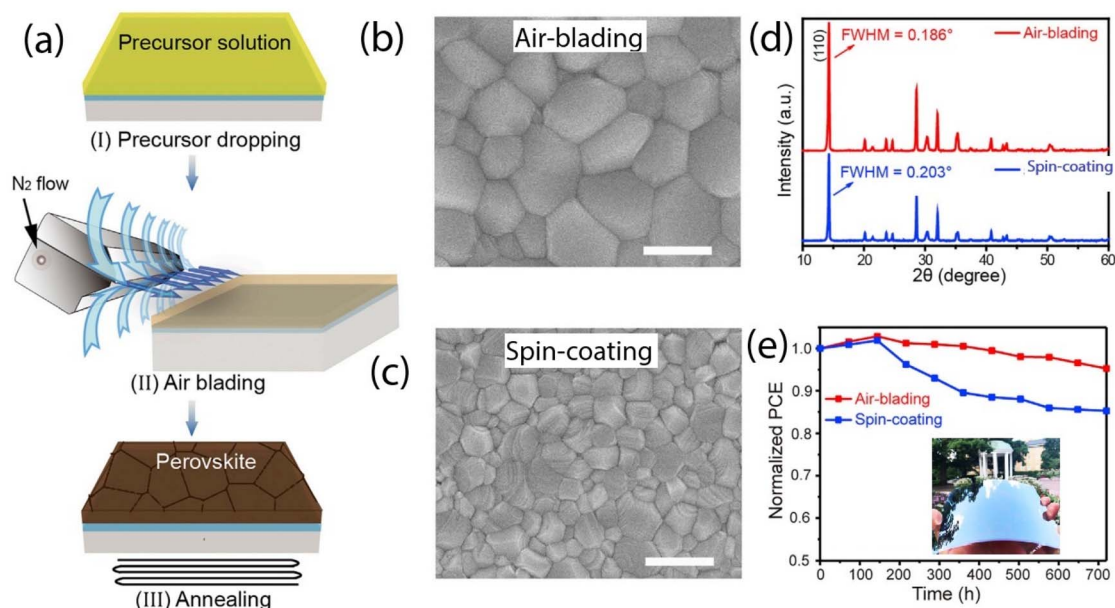
**3.1.1 Air-knife or air-blade assisted perovskite layer crystallization.** After depositing the perovskite layer, carefully controlling the drying process is essential for achieving well-crystallized perovskite films. Unlike the lab-scale spin-coating method, where a controlled environment is often maintained, larger-scale processes can suffer from uncontrolled solvent evaporation, leading to poorly crystallized films. Addressing this challenge, Jin-Song Hu's group developed an air-knife-assisted perovskite deposition technique in 2019, enabling stable, large-scale device fabrication.<sup>89</sup>

In the air-blade-assisted deposition method (Fig. 5a), nitrogen ( $N_2$ ) is applied with constant pressure in the direction of the substrate's movement immediately after the perovskite layer is deposited *via* blade coating. The airflow serves to dynamically remove solvent molecules, facilitating the formation of a perovskite layer with enhanced crystallinity. This approach resulted in perovskite films with larger grain sizes, the surface view seen

from scanning electron microscopy (SEM) images, compared to those produced by spin-coating (see Fig. 5b and c). XRD analysis also supports the air-blade technique, showing narrower FWHM values relative to spin-coating, indicating improved crystallinity. Furthermore, devices produced with air-knife-assisted deposition demonstrate enhanced stability (Fig. 5e).

**3.1.2 Interfacial engineering through additives.** The PSCs consist of several layers, with the protection of the top layer being crucial for the overall stability of the cell. Failure to adequately protect this layer can lead to delamination of the device. To prevent such issues, the top layer of the printed solar cell must be sufficiently rigid to resist air and moisture penetration. In 2022, Chen *et al.*<sup>90</sup> demonstrated the fabrication of a PSC using the blade-coating approach. The authors opted for a p-i-n configuration, sequentially coating the HTL, perovskite layer, and ETL using the blading technique. Notably, the hydrophobic poly(ethylene-vinyl acetate) (EVA) was incorporated into the ETL phenyl-C61-butyric acid methyl ester (PCBM), improving the top layer's morphology and acting as a barrier against water and oxygen.

The study found that the distribution of PCBM was influenced by the additive, which also caused a significant change in the zeta potential. The EVA additive further prevented the diffusion of halide ions through the ETL, as illustrated in Fig. 6. As a result, the blade-coated device achieved a PCE of 19.32%, with 80% retention of its initial efficiency after 1500 hours of storage under ambient conditions (52% humidity), notably without encapsulation. Additionally, when the active area of the solar cell was increased to 25 cm<sup>2</sup>, a PCE of over 10% was reported. Thus, the use of EVA significantly enhanced the blade-coating method for PSC fabrication.<sup>90</sup>



**Fig. 5** (a) Schematic illustration of perovskite film deposition using the air-knife-assisted approach. (b and c) Top-view SEM images of perovskite (MAPbI<sub>3</sub>) films deposited by air-knife (b) and spin-coating (c) methods, showcasing the differences in grain structure. (d) XRD patterns of MAPbI<sub>3</sub> films, highlighting crystallinity improvements with the air-knife technique. (e) Stability comparison for solar cells made with each method; the inset displays a 15 cm × 15 cm perovskite module. This figure has been adapted from ref. 89 with permission from Elsevier, copyright 2018.



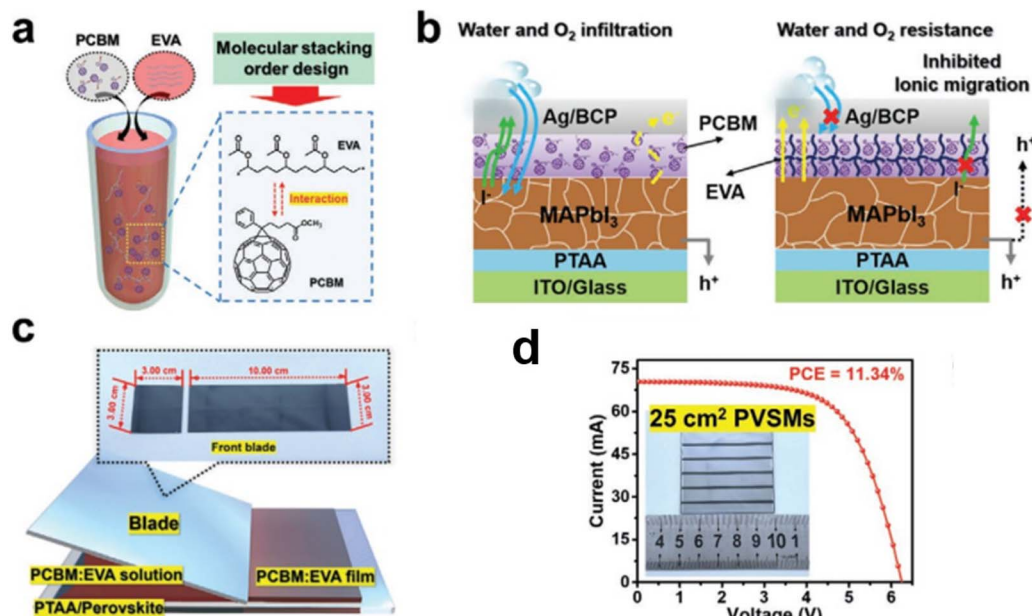
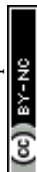


Fig. 6 (a) Schematic illustration depicting the molecular stacking order regulation of PCBM with the addition of an EVA (ethylene-vinyl acetate) additive. (b) Diagram of PSC utilizing a PCBM-EVA ETL, highlighting improved charge transfer capability, enhanced water and oxygen barrier properties, and reduced ion migration. (c) Schematic showing the blade-coated PCBM buffer layer incorporating EVA additive. (d) Current density–voltage ( $J$ – $V$ ) curves of the larger-area PSC module based on the PCBM ETL with best efficiency. This figure has been adapted from ref. 90 with permission from John Wiley and Sons, copyright 2021.

**3.1.3 Two-dimensional (2D)-perovskites as the protecting layer.** Strategies have also been developed to enhance the rigidity of the perovskite layer for better durability in open-air conditions. Ink engineering plays a crucial role in the advancement of 2D-perovskites. In the development of 2D perovskites, structural modifications to the organic cation moiety are pivotal. Increasing the length of the alkyl ammonium chains makes the perovskite layer more hydrophobic. Although this hydrophobic nature enhances the layer's stability towards open-air conditions, it also introduces electrical insulation challenges that limit the use of 2D perovskites in full device construction. However, using 2D perovskites as a protecting layer over bulk perovskite has been identified as a promising approach to improve the stability of PSCs and enhance their efficiency in converting harvested light into electricity. Studies have shown that integrating 2D perovskites with 3D perovskites can significantly boost solar cell performance, leveraging the strengths of both materials to create more stable and efficient devices.<sup>91–93</sup> In a report by F. Guo's team, a 2D/3D PSC was fabricated using a blade-coating approach, the structure of the spacer molecule, *S*-benzyl-L-cysteine (SBLC), along with the device fabrication process, is schematically illustrated in Fig. 7a and b. Detailed cross-sectional SEM images, showcasing the layer formation and structural integrity, are provided in Fig. 7c. This study demonstrates that in a single-step printing process, a 2D perovskite layer was grown over the 3D methylammonium lead triiodide (MAPbI<sub>3</sub>) layer, resulting in improved device performance compared to PSCs without the 2D passivation layer. Despite the inherent insulating behavior of the additional 2D perovskite,

which could potentially reduce device efficiency, the challenge was effectively addressed in this work. The enhanced performance was achieved through a three-step charge transport process: first, photogenerated charge carriers diffuse to the 2D/3D perovskite interface; next, lateral diffusion occurs as the carriers move towards regions where the PCBM is in direct contact with the 3D perovskite; and finally, since the 3D perovskite film is only partially covered by the 2D layer, sufficient area remains for effective charge extraction. This strategic integration of 2D and 3D perovskites ultimately enhanced the overall efficiency and stability of the device (Fig. 7d).<sup>94</sup>

**3.1.4 Solvent engineering.** Powalla *et al.* have demonstrated that using 100% DMSO in a blade-coating approach can achieve nearly the same efficiency as perovskite films produced with conventional solvent mixtures. Their research indicates that DMSO alone can effectively facilitate the crystallization of perovskite films, yielding results comparable to those obtained with traditional solvent combinations, even in non-inert conditions. This finding challenges conventional understanding and suggests that DMSO, when used as the sole solvent, may enhance perovskite crystallization more effectively than previously recognized in open-air conditions.<sup>95</sup> In addition, the combination of DMSO:GBL is compatible with standard ETLs, leads to highly dense films with very low leakage currents making the devices adequate for devices that operate under low lighting conditions.<sup>96</sup> Further, fine tuning of the process using hexafluorobenzene in small proportions lead to efficiencies of 20.7% for PSCs, blade coated in air.<sup>97</sup> Thus, solvent engineering is a highly promising strategy for fabricating open-air solar cells using the blade-coating method.



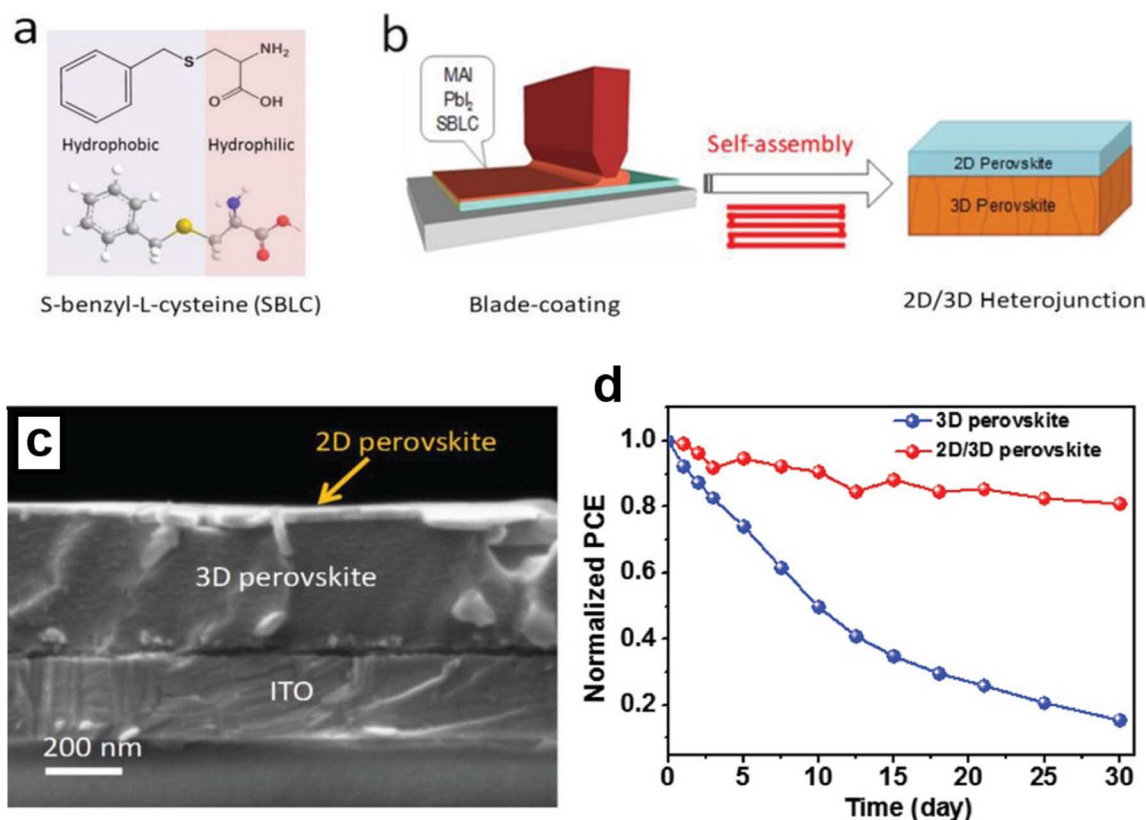


Fig. 7 SBLC molecular structure (a); the blade-coating of the 2D/3D perovskite film schematic (b); SEM surface images of the 2D/3D perovskite film (c); shelf stability of the 3D and 2D/3D heterostructure solar cells stored in ambient air with a relative humidity (RH) of 50%  $\pm$  10% (d). This figure has been adapted from ref. 94 with permission from John Wiley and Sons, copyright 2020.

**3.1.5 Formulation engineering towards less toxicity.** The concept of ink engineering also addresses the challenge of lead toxicity in perovskite formulations. Efforts are underway to replace lead (Pb) with tin (Sn) in these formulations to mitigate environmental and health risks. However, this substitution has been reported to compromise efficiency. Consequently, the long-term goal is to refine ink-engineering techniques to effectively replace Pb with Sn while maintaining or even enhancing solar cell efficiency.<sup>98,99</sup> Leveraging the concept of 2D/3D quasi-perovskite and employing the blade coating approach, Ivan and his team developed a flexible mini-module of Sn-PSC measuring 25 cm<sup>2</sup>, achieving a PCE of 5.7%.<sup>100</sup>

Thus, in the blade coating approach, all the above strategies are employed in recent times for the fabrication of large-scale modules in open-air conditions as we have discussed above, and the attention to be paid for further development of the high efficient PSCs of reduced chemical toxicity.

### 3.2. Roll-to-roll slot-die printing approach, advancement strategies

This approach is commonly referred to as roll-to-roll (R2R) printing or the R2R-based slot-die printing technique. Similar to R2R, flexographic printing and gravure printing are two additional techniques that operate in a comparable manner. However, due to its suitability for versatility, and higher

resolution printing, R2R is specifically utilized for PSCs.<sup>101</sup> R2R processing is a high-throughput manufacturing technique that involves the continuous fabrication of flexible electronic devices on a roll of flexible substrate material, such as plastic or metal foil. Ensuring compatibility with perovskite materials and deposition processes is crucial to achieving high-quality devices. Maintaining precise control over deposition parameters such as coating speed, temperature, and atmosphere in a continuous roll-to-roll environment can be challenging. Variations in these parameters can affect film quality, device performance, and yield. R2R processing holds great promise for the scalable production of flexible perovskite solar cells. In a conventional roll-to-roll slot-die approach, there will be a slot-die coater, where the perovskite will be coated and then the substrate will be passed through a compressed air flow, followed by passing through a thermal heater which leads the perovskite crystallization. However, the drying process is often ineffective in producing high-quality perovskite films. As a result, researchers are actively seeking alternative methods to improve the fabrication process.

#### 3.2.1 Process engineering

**3.2.1.1 Infrared pulsed light (IPL) annealing treatment.** In 2018, Michael Saliba and his team pioneered the Infrared Pulsed Light (IPL) Annealing treatment, a breakthrough technique specifically designed for halide perovskites with a high level of phase purity,

which has significantly advanced the efficiency and stability of these materials in solar cell applications.<sup>102</sup>

In 2024, Dong Seok Ham's research group made significant progress in understanding the phase purity of perovskite layers within the realm of ink engineering. Their study focused on incorporating cesium salts, such as cesium iodide (CsI) and cesium formate (CsF), into the  $\text{PbI}_2$  solution. This approach notably improved the preservation of phase purity in the perovskite layer, particularly when combined with formamidinium iodide (FAI) and followed by IPL annealing treatments. As illustrated in Fig. 8, this innovative ink engineering method resulted in a higher-quality perovskite layer, with IPL treatments yielding better outcomes compared to conventional thermal drying methods.<sup>71</sup>

**3.2.1.2 Dry press deposition (DPD).** The fabrication of fully printed perovskite solar cells (PSCs) necessitates the careful addition of a top contact layer, which plays a critical role in achieving proper ohmic contact. A major challenge in this process is protecting the sensitive perovskite layer from damage, particularly due to solvent exposure. Additionally, the use of vacuum-assisted metal deposition significantly drives up the cost of solar cell technology. To address these challenges, Hasitha W.'s team developed a novel approach that involves mechanically pressing the top contact onto the device without the need for solvents (Fig. 9). This technique significantly reduces the risk of solvent-induced damage, making it a promising innovation in PSC fabrication. However, the success of this method hinges on the precise optimization of pressing conditions to ensure that the fragile perovskite layer remains undisturbed. Furthermore, the exceptional bending durability of flexible PSCs with printed DPD electrodes underscores their potential for various flexible electronic applications. This approach represents a crucial advancement towards the commercial viability of PSCs, offering a cost-effective, vacuum-free, and solvent-free alternative to the traditionally expensive evaporative deposition of metal electrodes. Such innovations

are pivotal in driving the widespread adoption and practical implementation of perovskite solar technology.<sup>103</sup>

### 3.3. Screen-print or mesh-assisted perovskite deposition, advancements

The screen-printing technique excels in rapidly coating micrometer-thick films over large areas, leveraging a screen or mesh as a support structure. These screens, often crafted from durable polymer materials, are resistant to the chemicals used during the process. As a result, this method yields highly uniform films and enables efficient production on a large scale, with the ability to achieve rapid processing times.

**3.3.1 Introducing ionic liquids.** By the screen-printing technique, mostly the metal oxide films are grown. However, in 2022, Wei Huang's team reported the screen-assisted perovskite layer deposition from a viscous perovskite ink prepared using the methylammonium acetate ionic liquid. In this approach, the author has reported an efficiency of 20.52%. This work reports the fabrication of solar cells based on a screen-printing approach that can be completed in ambient air, regardless of humidity.<sup>104</sup>

**3.3.2 Process engineering.** While much of this review emphasizes scientific strategies to simplify the fabrication methodologies, and to improve PSC efficiency and operational stability, this section highlights advancements geared toward integrating PSCs into BIPVs using the screen-printing strategy. For integration into windows, PSCs must be designed to be semitransparent, which can be achieved by reducing the perovskite film thickness to below 300 nm or by modifying the perovskite composition. However, these approaches often entail a trade-off between transparency and PCE. In a recent advancement, from our lab a mesh-assisted technique has been employed to structure the perovskite layer into a grid, allowing for precise control over the film's transparency. In these perovskite grids, a thickness gradient within the perovskite layer effectively tunes the transparency. A transparent

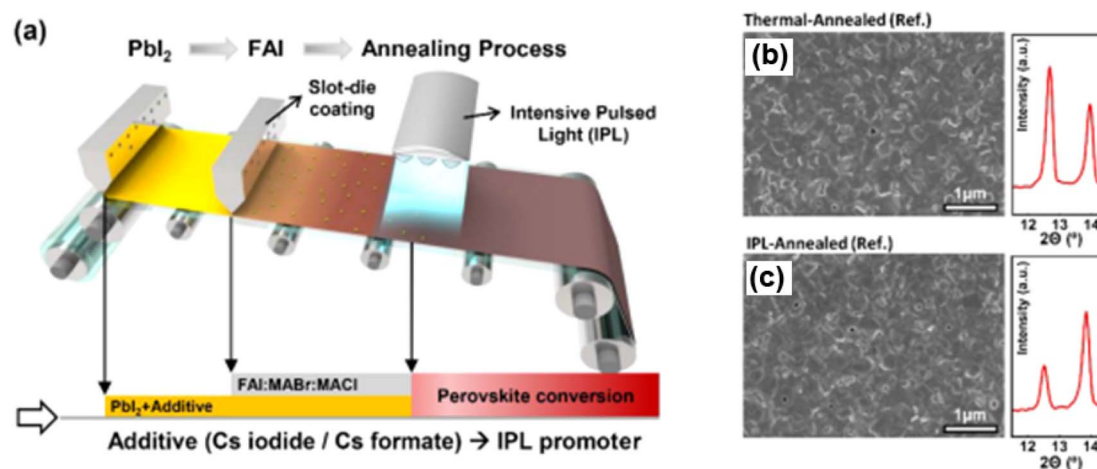
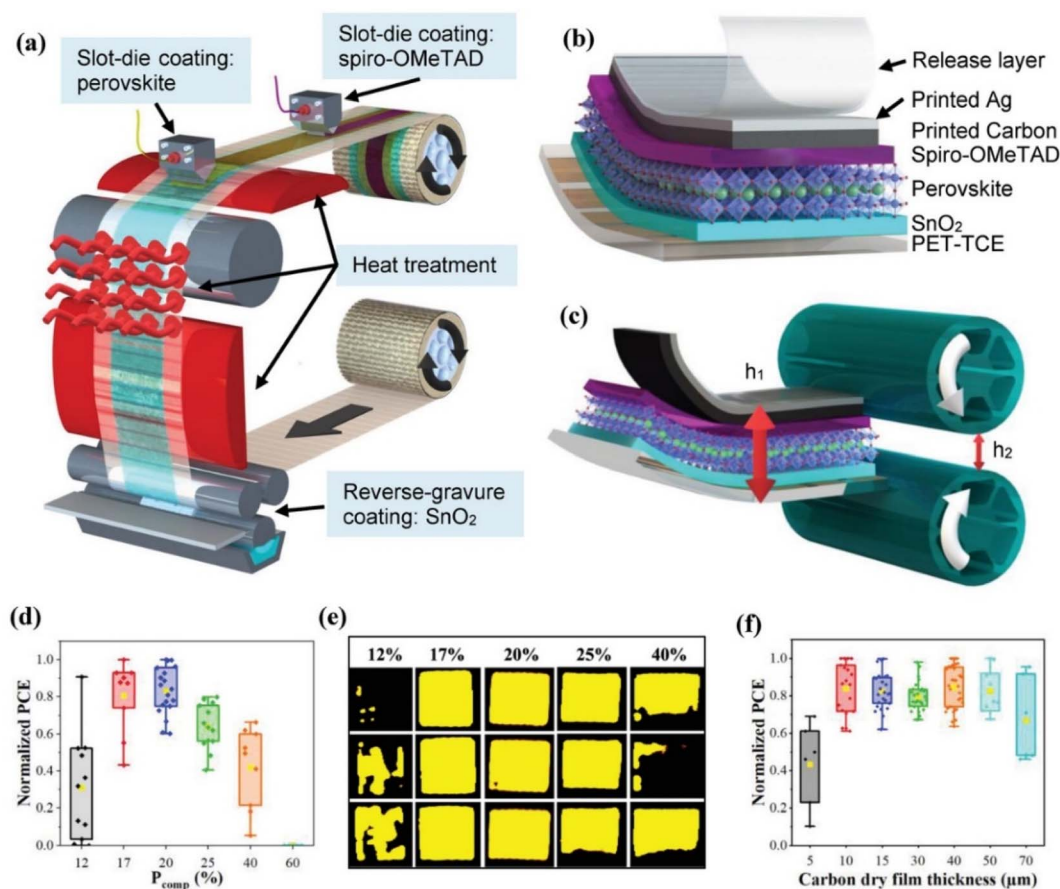


Fig. 8 Schematic representation of the R2R two-step processing method utilizing an IPL treatment (a); FE-SEM and XRD graphs of the perovskite surface (pristine  $\text{PbI}_2$ ) (b); FE-SEM and XRD (pristine  $\text{PbI}_2$ ) analysis of perovskite surfaces treated with IPL (c). This figure has been adapted from ref. 71 with permission from American Chemical Society, copyright 2024.



**Fig. 9** The diagram illustrates the R2R fabrication process for the PSC precursor stack (a); the PSC device architecture is depicted, highlighting the release layer mechanism that facilitates the removal of the device from the substrate (b); the Dry Press Deposition (DPD) process is shown alongside the equation used to calculate the compressive pressure applied during fabrication (c); a graph displays the normalized PCE results for devices fabricated under varying levels of compression pressure, illustrating the impact of pressure on device performance (d); light-beam induced current (LBIC) maps provide a visual representation of PSCs fabricated at different compressive pressures, indicating how pressure variations affect the uniformity and performance of the cells (e); another graph presents the normalized PCE results for devices fabricated with varying carbon film thicknesses, demonstrating the relationship between carbon layer thickness and overall device efficiency (f). This figure has been reproduced from ref. 103 with permission from John Wiley and Sons, copyright 2022.

dielectric-metal-dielectric structure is then applied as the top contact, enhancing light transmission while maintaining electrical performance. The process involves dropping perovskite precursor solution from a defined height and angle onto a mesh in direct contact with the substrate. The perovskite fills the mesh's contact points, creating a uniform grid over the mesoporous  $\text{TiO}_2$  (m- $\text{TiO}_2$ ), with the empty spaces forming thin perovskite layers. This design allows for free light passage with minimal absorbance in these regions, making the technique well-suited for producing various semi-transparent perovskite films.

The mesh size and precursor concentration are critical factors in tuning the film's transparency and thickness. The non-viscous nature of the perovskite solution enables it to spread uniformly over the mesh, forming a grid structure with voids that are later covered by a thin perovskite layer. The crystallization of the perovskite layer, and thus the device's efficiency, is further controlled by adding surfactants and adjusting the substrate temperature. Mixed cation and halide

perovskite formulations have shown excellent stability and efficiency with this approach. Initially, perovskite grid-based solar cells achieved PCEs of around 5% with an average visible transparency (AVT) of 30%. Through compositional modifications and a refined 1.5-step deposition process (seen in Fig. 10), PCEs were later increased to 10%, with a slightly reduced AVT of 28%. This technique demonstrates significant potential for developing high-performance, semi-transparent PSCs for building-integrated applications.<sup>106</sup>

#### 3.4. Ink-jet printing, advancements

Inkjet printing has garnered considerable attention in the fabrication of PSCs due to its advantages in low-cost, scalable production and precise material deposition. This technique minimizes material wastage by applying only the necessary amount of perovskite solution onto the substrate, which helps reduce costs associated with material consumption. Inkjet printing's non-contact nature enables precise patterning of films by controlling droplet deposition and allows for the



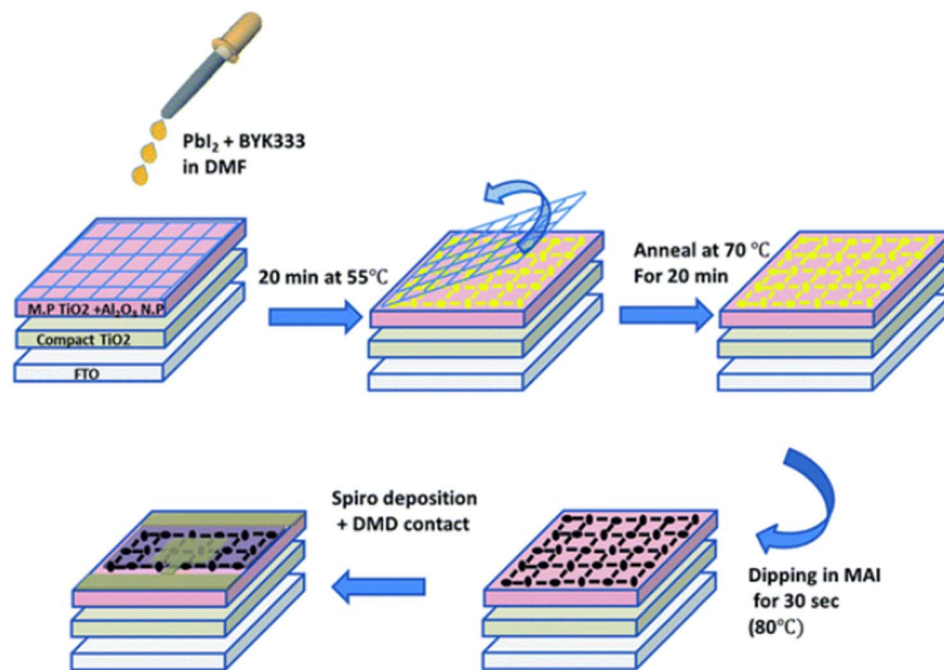


Fig. 10 Schematic illustration of the perovskite grid formation using the mesh-assistance method. This figure has been reproduced from ref. 105 with permission from Royal Society of Chemistry, copyright 2016.

incorporation of other functional materials into the perovskite layer at specific locations and quantities. Furthermore, inkjet printing is more environmentally friendly, as it releases fewer solvents into the environment compared to other printing technologies. Despite these benefits, there are notable challenges in using inkjet printing for perovskite solar cells. Developing stable, high-quality perovskite inks that are compatible with inkjet printing is crucial, requiring careful control of ink stability, viscosity, and overall compatibility with the printing process. Additionally, managing the crystallization of printed perovskite is essential to achieve the desired morphology and optoelectronic properties. After the perovskite precursor is printed, the film undergoes a crystallization process, typically involving vacuum treatment followed by heat treatment at carefully controlled temperatures as discussed below. Rapid ink drying can result in non-uniform film formation and defects, impacting the performance and reliability of the solar cells. These subsequent processing steps ensure the formation of a high-quality perovskite layer with optimal structural and optoelectronic properties. However, challenges also remain with the chemical compatibility of the printer's head. The efficiency of inkjet printing also depends on the viscosity and chemical behavior of the solvents used, and clogging of any nozzles can cause significant damage to the entire solar cell.

**3.4.1 Ink engineering.** In 2024, Jae-Wook's research group conducted an in-depth study on how the boiling points of solvents impact the properties of perovskite films, focusing on their effects on film roughness, thickness, and overall morphology. The study also examined how these factors influence the efficiency of PSCs. A key finding was that the

crystallinity of perovskite films is markedly affected by the solvents' evaporation kinetics, particularly during the transition phase. To elucidate these kinetics, the researchers incorporated 1,3-dimethyl-2-imidazolidinone (DMI) and  $\gamma$ -butyrolactone (GBL) into a solvent mixture of DMF and DMSO. This method enabled a comprehensive evaluation of how different solvent combinations influence the film formation process and the resulting quality of the perovskite layers. The study also involved analyzing the entire printing setup, including the viscosity *versus* shear rate and the chemical interactions within the ink, as depicted in Fig. 8. After comparing PSCs based on DMI with those using GBL over a storage period of 1680 hours, it was found that the DMI-based devices demonstrated significantly better efficiency retention (Fig. 11).<sup>107</sup>

Extensive research has been conducted on utilizing inkjet printing technology for fabricating fully printed PSCs. In a 2021 study, Ulrich and his team reported the development of a p-i-n structured PSC using a triple cation perovskite formulation. This innovative design achieved a reported efficiency of over 17%. The uniformity of the layers within this structure is illustrated in Fig. 12. The authors emphasized that controlling wettability plays a crucial role in enhancing both the stability and efficiency of the device.<sup>108</sup>

**3.4.2 Maximum solubility factor.** The "coffee-ring" effect, a common issue in ambient air, arises from the uneven distribution of deposits during the evaporation of solvent from printed droplets. This phenomenon occurs due to the slower evaporation rate of the ink solvent on the substrate, leading to capillary flows that cause material to accumulate more at the edges of the droplet while leaving less in the center. To address this challenge and enhance the performance and stability of



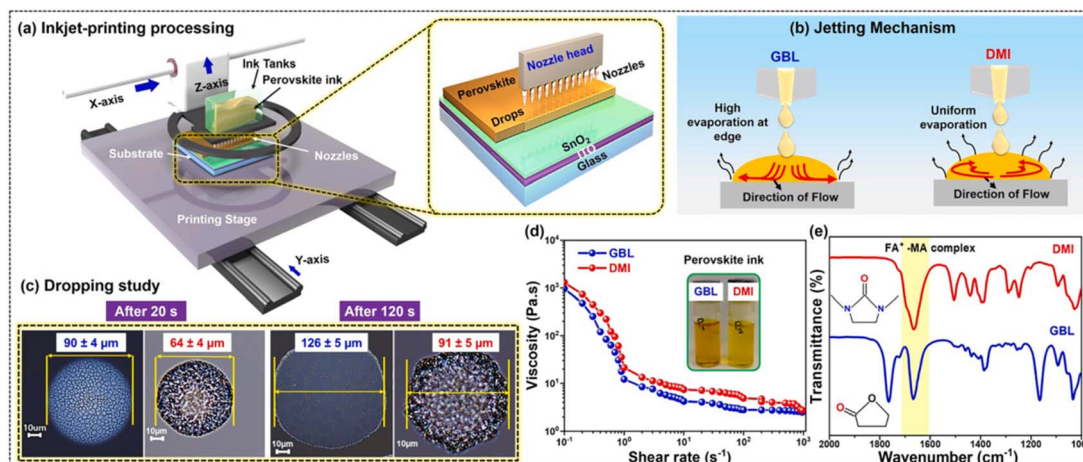


Fig. 11 Schematic representation of the inkjet-printed perovskite film fabrication process, illustrating the steps involved from inkjet deposition to film formation (a); diagram depicting the jetting mechanism of perovskite ink formulated with GBL and DMI, detailing how these solvents influence ink ejection and patterning (b); graph showing the perovskite ink drop spreading rate over time, measured at 20 seconds and 120 seconds post-printing, highlighting the ink's behavior as it settles and spreads on the substrate (c); plot of the viscosity of GBL and DMI-based perovskite inks as a function of shear rate, demonstrating how the ink's viscosity changes under different shear conditions (d); FTIR analysis of perovskite inks prepared with GBL and DMI solvents, providing insights into the chemical composition and interactions within the inks (e). This figure has been reproduced from ref. 107 with permission from Elsevier, copyright 2024.

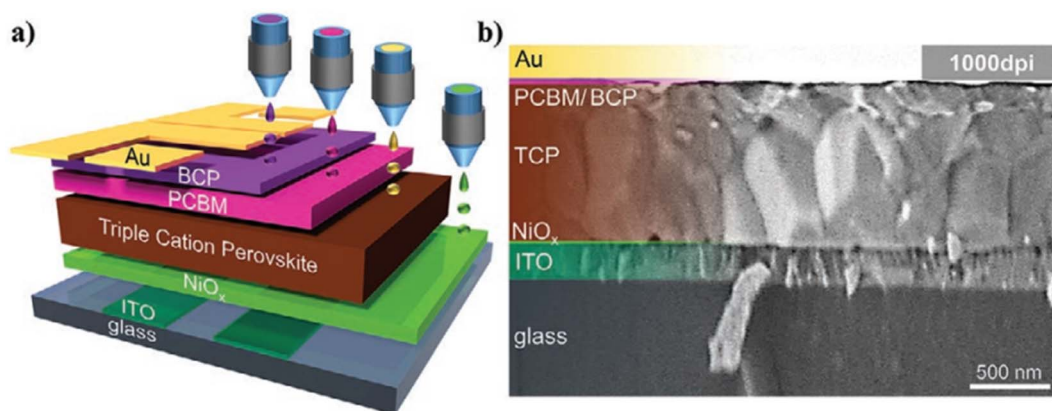


Fig. 12 Schematic illustration of the p-i-n perovskite solar cell architecture featuring all printed layers (a). The SEM image showing a cross-section of the device (b). This figure has been adapted from ref. 108 with permission from John Wiley and Sons, copyright 2020.

inkjet-printed perovskite layers in ambient conditions, Chalkias *et al.* implemented a concentration regulation strategy for the perovskite precursor ink. By increasing the molar concentration of perovskite precursors in the ink to the maximum solubility limits, the ink's ability to jet and achieve optimal wetting properties on the mesoscopic substrate was significantly improved. This adjustment facilitated a more uniform deposition of the perovskite layer, ultimately leading to enhanced performance and greater stability of all-printed perovskite photovoltaic systems.<sup>109</sup>

### 3.4.3 Polymer pillar integrity: transparent PSCs for BIPVs.

Inkjet printing allows for the precise incorporation of functional materials, enabling uniform spatial distribution with high control over material placement within the perovskite layer. Leveraging this capability, our lab developed a semi-transparent perovskite solar cell by printing polymeric pillars

on the substrates before applying the perovskite layer (Fig. 13a). By varying the dimensions of these transparent polymer pillars, the transparency of the perovskite film was tuned between 10% and 30%. The addition of surfactant significantly impacted the surface morphology of the perovskite layer. After introducing Triton X-114, pinholes and cracks were effectively eliminated, resulting in a notably smoother and more uniform morphology (Fig. 13b and c). Furthermore, the integration of polymer pillars enhanced the transparency of the perovskite layers. These findings highlight that inkjet printing can be used to achieve tunable optical properties in PSCs without modifying the chemical composition or concentration of the perovskite precursor solution (Fig. 13d and e). Overall, this work demonstrates the successful development of flexible and semi-transparent PSCs through an inkjet printing approach,



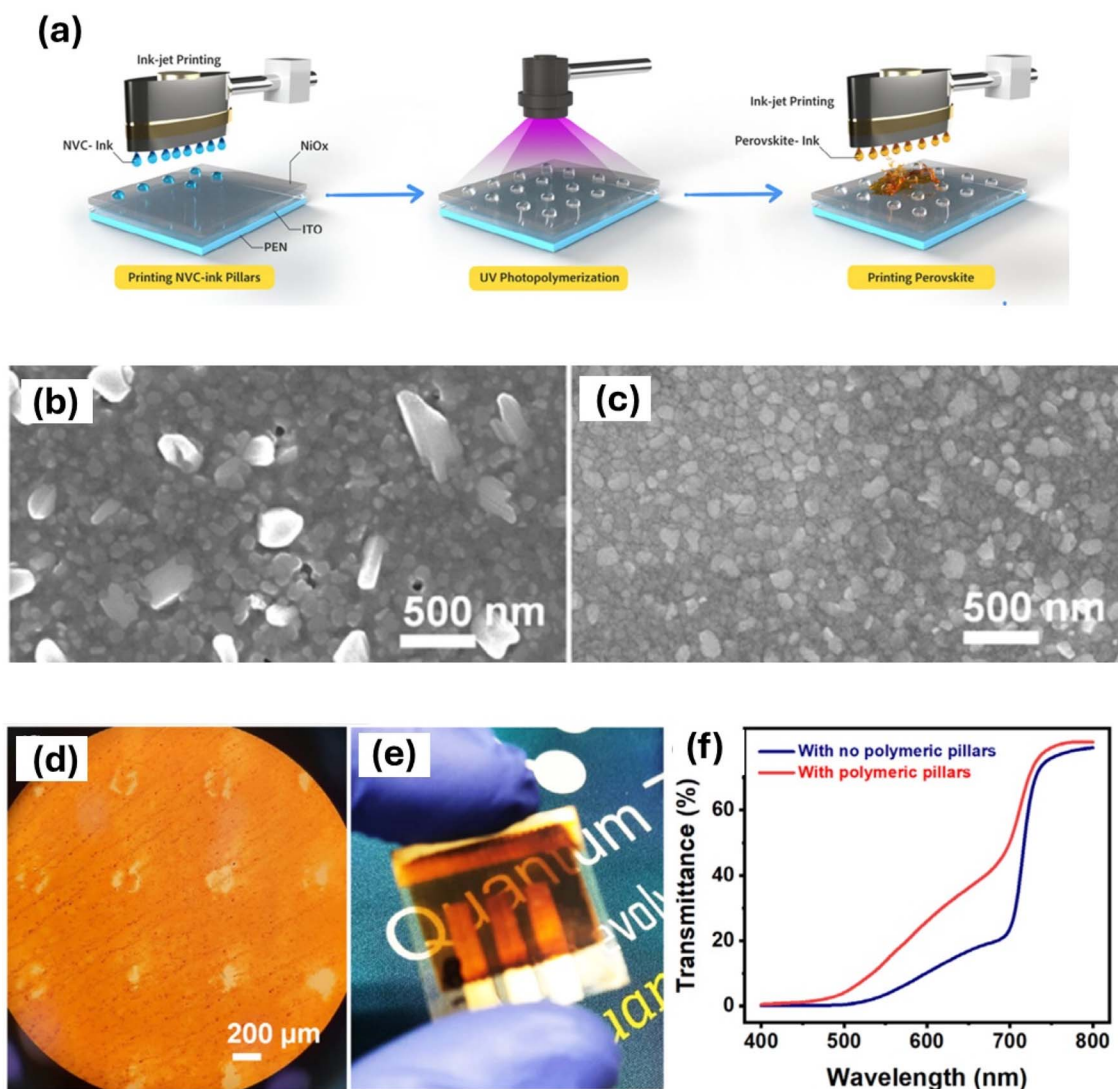


Fig. 13 The ink-jet printing of monomer and polymerization under UV light, followed by deposition of a perovskite layer over a flexible substrate (a). The surface SEM images of the inkjet-printed perovskite are shown without surfactant (b) and with surfactant (c). Additionally, the optical image of the polymer pillar-integrated perovskite film is presented in (d), alongside the transparent, flexible PSC (e), and the optical transparency comparison of the PSC with and without polymer pillar integration is displayed in (f). This figure has been adapted from ref. 38 with permission from John Wiley and Sons, copyright 2023.

incorporating polymer pillars in precise patterns within the perovskite layer.<sup>38</sup>

While inkjet-printed PSCs have demonstrated promising efficiencies, further optimization is necessary to enhance device performance, stability, and long-term environmental resilience.

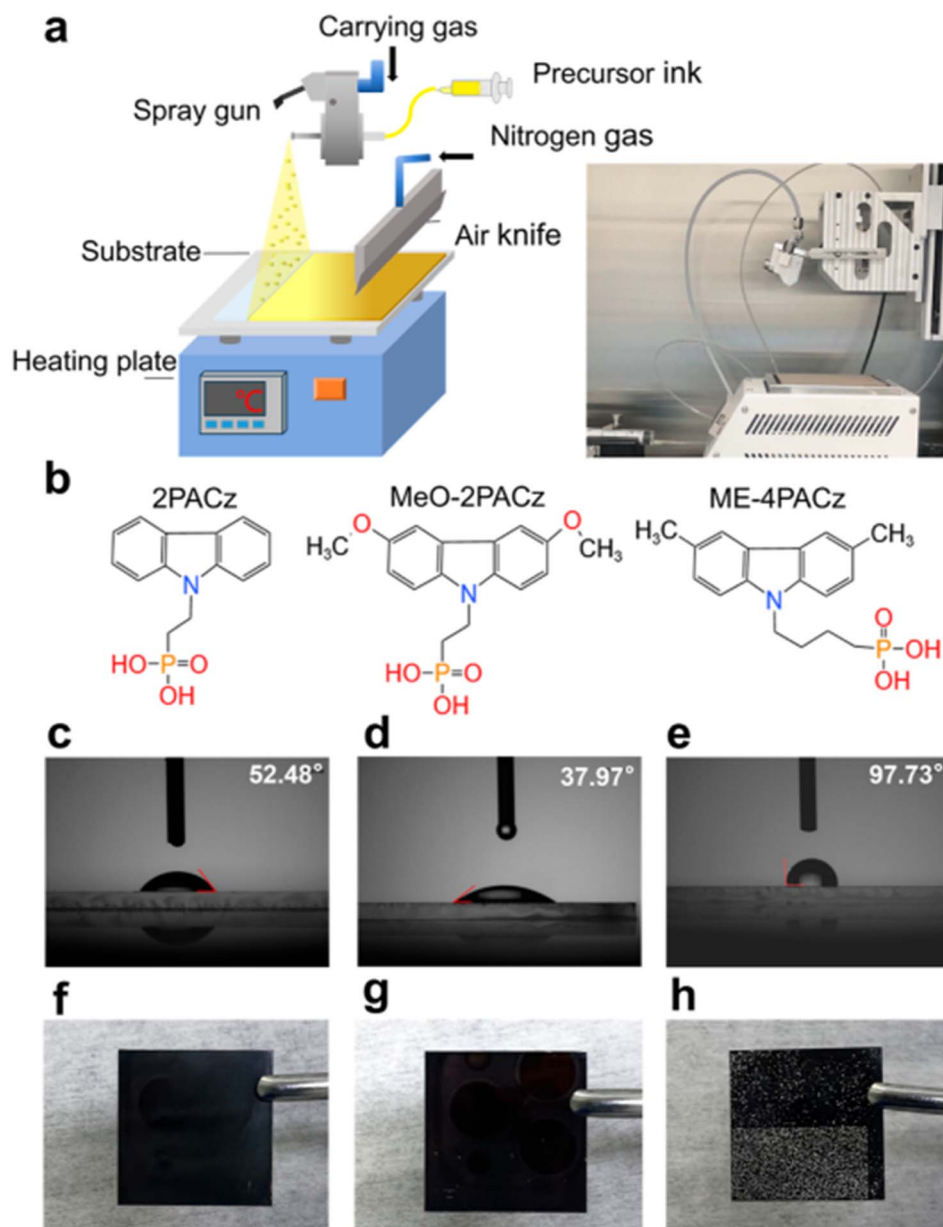
### 3.5. Spray-coating, advancements

Spray coating is another promising technique for fabricating perovskite solar cells, in this method, a solution containing perovskite precursors is atomized and sprayed onto a substrate, forming a thin film upon drying. Proper optimization of spray parameters, such as nozzle size, spray distance, solution concentration, and substrate temperature, is crucial for achieving uniform perovskite films with controlled thickness and morphology. As such, a diluted precursor solution is

sprayed over the substrate at room temperature or at desired temperatures. Currently, spraying is often done manually, but mechanical sprayers can achieve spatial uniformity.

**3.5.1 Wettability.** The poor wettability of the perovskite precursor solution leads to the formation of pinholes and suboptimal interfaces, significantly compromising device efficiency. To mitigate this, additives in the perovskite solution and targeted surface treatments are frequently used to improve wettability. Notably, UV-ozone surface treatment partially hydroxylates the metal oxide surface, thereby significantly increasing its hydrophilicity.<sup>110</sup> In 2024, Yi Ding's team made significant advancements in enhancing the interface between NiO and the perovskite layer by introducing self-assembled monolayer (SAM) molecules, specifically 2-(9H-carbazol-9-yl) ethyl]phosphonic acid (2PACz), [2-(3,6-dimethoxy-9H-carbazol-





**Fig. 14** Schematic illustration and photograph of perovskite film fabrication using the ultrasonic spray-coating method (a); molecular structures of 2PACz, Me-4PACz, and MeO-2PACz (b); contact angles of the precursor solution on 2PACz, (c); MeO-2PACz, (d); and Me-4PACz (e); images of the perovskite film sprayed on 2PACz, (f); MeO-2PACz, (g); and Me-4PACz (h). This figure has been reproduced from ref. 111 with permission from American Chemical Society, copyright 2024.

9-yl)ethyl]-phosphonic acid (MeO-2PACz), and [4-(3,6-dimethyl-9H-carbazol-9-yl)butyl]phosphonic acid (Me-4PACz). The researchers focused on ink engineering by incorporating a methylammonium acetate (MAAc) additive into the precursor solution. Their work demonstrated that 2PACz and MeO-2PACz facilitate the formation of uniform perovskite films with high crystallinity, which in turn improves hole extraction at the buried interface. The improved wettability for different SAM molecules has been shown in Fig. 14. This approach led to an impressive PCE of 20.3%, highlighting the potential of SAM molecules in optimizing perovskite solar cell performance.<sup>111</sup>

## 4. Conclusions and challenges

Perovskite solar cells are in high demand for commercialization. The focus should be on fabricating larger PSCs with improved lifetime at a lower cost using less-toxic approaches. Printable approaches, such as blade-coating, ink-jet printing, slot-die approach, spray-coating, and screen-printing, are useful for constructing solar cells in open-air conditions that could produce larger-area modules. Each approach presents its own benefits and challenges. The R2R process, for example, is limited by flexible substrates, while inkjet printing struggles with chemical and coagulation issues that affect jetting. Spray



coating encounters spatial uniformity problems, and screen printing often results in poor perovskite crystallization. However, many of these challenges are being addressed. Additives in perovskites have been shown to enhance crystallization and morphology, surface treatments improve wettability, and low-dimensional perovskites boost device stability. Furthermore, simplifying processes and modifying device structures have proven effective in improving optical properties. Thus, in this review, we have discussed the literature on printing PSCs, with improved properties, including PSCs with more advanced and simplified fabrications, and with digital control over the semitransparency for BIPVs, *etc.* It is important to note that the chemical compositions of the hybrid perovskite materials and solvents should be less toxic in particular when working in open air. While most open-air processing currently focuses on Pb-based perovskites, directing printable approaches toward the development of Pb-free PSCs offers promising potential. Additionally, it is important to highlight that employing open-air techniques for constructing all layers is crucial for the successful production of PSC modules. Equally significant is the need to recycle PSCs to mitigate the adverse environmental effects of the materials used.

## Data availability

No primary research results, software or code have been included and no new data were generated or analysed as part of this review.

## Conflicts of interest

There are no conflicts to declare.

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