

Cite this: *Nanoscale Adv.*, 2022, 4, 4648

# Superhigh energy storage density on-chip capacitors with ferroelectric $\text{Hf}_{0.5}\text{Zr}_{0.5}\text{O}_2$ /antiferroelectric $\text{Hf}_{0.25}\text{Zr}_{0.75}\text{O}_2$ bilayer nanofilms fabricated by plasma-enhanced atomic layer deposition

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Thanks to their excellent compatibility with the complementary metal–oxide–semiconductor (CMOS) process, antiferroelectric (AFE)  $\text{HfO}_2/\text{ZrO}_2$ -based thin films have emerged as potential candidates for high-performance on-chip energy storage capacitors of miniaturized energy-autonomous systems. However, increasing the energy storage density (ESD) of capacitors has been a great challenge. In this work, we propose the fabrication of ferroelectric (FE)  $\text{Hf}_{0.5}\text{Zr}_{0.5}\text{O}_2$ /AFE  $\text{Hf}_{0.25}\text{Zr}_{0.75}\text{O}_2$  bilayer nanofilms by plasma-enhanced atomic layer deposition for high ESD capacitors with TiN electrodes. The effects of the FE/AFE thickness composition and annealing conditions are investigated, revealing that the  $\text{Hf}_{0.5}\text{Zr}_{0.5}\text{O}_2$  (1 nm)/ $\text{Hf}_{0.25}\text{Zr}_{0.75}\text{O}_2$  (9 nm) bilayer can generate the optimal ESD after optimized annealing at 450 °C for 30 min. This is mainly ascribed to the factor that the introduction of a 1 nm  $\text{Hf}_{0.5}\text{Zr}_{0.5}\text{O}_2$  layer enhances the formation of the tetragonal (T) phase with antiferroelectricity in the AFE  $\text{Hf}_{0.25}\text{Zr}_{0.75}\text{O}_2$  layer as well as the breakdown electric field of the bilayer while fixing the FE/AFE bilayer thickness at 10 nm. As a result, a ESD as high as 71.95 J cm<sup>-3</sup> can be obtained together with an energy storage efficiency (ESE) of 57.8%. Meanwhile, with increasing the measurement temperature from 300 and 425 K, the capacitor also demonstrates excellent stabilities of ESD and ESE. In addition, superior electrical cycling endurance is also demonstrated. Further, by integrating the capacitor into deep silicon trenches, a superhigh ESD of 364.1 J cm<sup>-3</sup> is achieved together with an ESE of 56.5%. This work provides an effective way for developing CMOS process-compatible, eco-friendly and superhigh ESD three-dimensional capacitors for on-chip energy storage applications.

Received 30th June 2022  
Accepted 23rd September 2022

DOI: 10.1039/d2na00427e

rsc.li/nanoscale-advances

## Introduction

With the rapid development of wireless sensor networks and the Internet of Things, the demand for high performance, smaller and lighter energy storage devices is increasing, especially for those that can be integrated into silicon-based chips. Thus, advanced energy storage materials and associated technologies have attracted intense research interest from both academic and industrial communities.<sup>1–3</sup> As one kind of competitive energy storage device, micro-capacitors can offer many advantages, such as fast charge/discharge rates and a theoretically infinite number of charge/discharge cycles, which thus make micro-capacitors more appropriate for truly autonomous systems.<sup>4</sup> So far, numerous efforts have been made towards integrating micro-capacitors (*e.g.*, electrostatic

capacitors or electrochemical supercapacitors) into chips.<sup>5,6</sup> Unlike electrochemical supercapacitors that store energy based on the electrochemical double layer effect and/or pseudo capacitance effect, electrostatic capacitors store electrical energy in the form of an electrostatic field *via* dielectric polarization. Thus, electrostatic capacitors possess some advantages such as larger charging voltage, higher operating frequencies and higher power densities, which make them more competitive for practical applications.<sup>7,8</sup>

For the sake of obtaining a high ESD, various types of dielectrics have been explored for electrostatic capacitors, including antiferroelectrics (AFEs), ferroelectrics (FEs) and linear dielectrics (LDs).<sup>9–11</sup> In contrast to FEs and LDs, the use of AFEs can achieve a much higher ESD because of significant changes in polarization during the AFE–FE phase transition, and thus the AFE materials have greater potential for use in energy storage devices.<sup>9,12,13</sup> To date, some potential AFE materials including organic dielectrics (*e.g.*, poly vinylidene fluoride) and inorganic perovskite dielectrics (*e.g.*,  $\text{Bi}_{0.5}\text{Na}_{0.5}\text{TiO}_3$ –

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BaTiO<sub>3</sub>, PbZrO<sub>3</sub>, AgNbO<sub>3</sub>) have been investigated for high ESD capacitors.<sup>9,14–16</sup> Organic dielectrics can often withstand quite high electric field strengths and thus produce large ESDs, but they usually suffer from the drawbacks of lower melting points and thermal destruction after quick charge–discharging cycling.<sup>17</sup> This makes them unsuitable for use in high temperature environments. By contrast, inorganic perovskite dielectrics possess high dielectric constants and relatively high ESDs, but suffer from low breakdown electric fields, large leakage currents and reliability issues.<sup>12,18</sup> Besides, these materials are very challenging for on-chip integration because of their complex deposition processes such as sol–gel spin coating and high-temperature calcination.

Recently, CMOS process-compatible AFE fluorite-structured dielectrics, including Si, La, Al or Zr-doped HfO<sub>2</sub>,<sup>8,19–22</sup> and ZrO<sub>2</sub> films<sup>23</sup> have been studied intensively for electrical energy storage applications, exhibiting high reliability, excellent thermal stability and high ESDs. Compared to inorganic perovskite AFE materials, fluorite-structured AFE dielectrics possess smaller polarization strengths and dielectric constants, but they have much larger bandgaps (>5.5 eV) and thus can sustain higher electric fields.<sup>24</sup> This can compromise the negative effects of other drawbacks and so far, the highest ESD of 63.7 J cm<sup>−3</sup> has been achieved for AFE HfAlO<sub>x</sub> films.<sup>21</sup> Moreover, fluorite-structured AFE dielectric films can be easily deposited by atomic layer deposition (ALD), which can ensure excellent step coverage, precise film thickness control, and perfect large-area uniformity, particularly suitable for deposition on a 3-D structure. By adjusting the ALD cycles of individual metal oxide (*i.e.*, binary oxide), ternary or quaternary AFE materials can also be readily realized. Therefore, inorganic fluorite-structured AFE dielectrics are potential candidate materials for high performance on-chip energy storage capacitors. On the other hand, increasing the energy density of on-chip capacitors has always been an ambitious goal for researchers, who are trying to make them competitive with electrochemical supercapacitors. Recently, Zhang *et al.*<sup>25</sup> have reported that by introducing a lower dielectric constant and thinner PbZrO<sub>3</sub> layer with improved quality into the PbZr<sub>0.52</sub>Ti<sub>0.48</sub>O<sub>3</sub> capacitor, the fabricated bilayer dielectric capacitor exhibits a significant increase in ESD due to the enhanced breakdown electric field. Therefore, the design of AFE/FE bilayer thin films could be an effective way for developing high ESD capacitors.

In this study, we adopt the concept of FE/AFE bilayer dielectrics for energy storage capacitors, and investigate the effects of the FE Hf<sub>0.5</sub>Zr<sub>0.5</sub>O<sub>2</sub>/AFE Hf<sub>0.25</sub>Zr<sub>0.75</sub>O<sub>2</sub> thickness composition and annealing conditions on the characteristics of the capacitors. It is demonstrated that the introduction of an ultrathin underlying FE layer onto the TiN bottom electrode is an effective way to improve the ESD of the AFE capacitors. By combining plasma-enhanced ALD technology, three-dimensional (3-D) TiN/FE/AFE/TiN capacitors are successfully fabricated with a deep silicon trench template, exhibiting a ESD as high as 364.1 J cm<sup>−3</sup>.

## Experimental

A 300 nm SiO<sub>2</sub> film was formed on p-type Si wafers by thermal oxidation. Various stacks of TiN (20 nm)/FE/AFE/TiN (50 nm)

were deposited on the above-mentioned SiO<sub>2</sub> film in one ALD chamber without breaking the vacuum. The Hf<sub>1−x</sub>Zr<sub>x</sub>O<sub>2</sub> films were deposited *via* PEALD at 220 °C using Hf[N(C<sub>2</sub>H<sub>5</sub>)CH<sub>3</sub>]<sub>4</sub>, Zr [N(CH<sub>3</sub>)<sub>2</sub>]<sub>4</sub> and O<sub>2</sub> plasma as the Hf, Zr precursors and the oxygen source, respectively. The bottom and top TiN films were deposited by PEALD at 200 °C using [(CH<sub>3</sub>)<sub>2</sub>N]<sub>4</sub>Ti and NH<sub>3</sub> plasma. The growth rates of HfO<sub>2</sub> and ZrO<sub>2</sub> were about 0.81 Å per cycle. The ALD cycle ratios of HfO<sub>2</sub>/ZrO<sub>2</sub> were fixed at 1 : 1 for the deposition of the Hf<sub>0.5</sub>Zr<sub>0.5</sub>O<sub>2</sub> FE layer and 1 : 3 for the growth of the Hf<sub>0.25</sub>Zr<sub>0.75</sub>O<sub>2</sub> AFE layer, which exhibited the best FE and AFE behavior, respectively.<sup>26</sup> The total thickness of FE/AFE stacks was fixed approximately at 10 nm. To investigate the influence of the FE and AFE layer thicknesses on the capacitor performance, various thickness compositions of the FE/AFE layers were engineered, *i.e.*, 1 nm/9 nm, 3 nm/7 nm, and 5 nm/5 nm, respectively. Moreover, single FE and AFE layers with the same thickness of 10 nm were also deposited respectively as control samples. Subsequently, top TiN electrodes with a thickness of 50 nm were defined by photolithography, and then both the TiN and Hf<sub>1−x</sub>Zr<sub>x</sub>O<sub>2</sub> films outside the electrodes were etched by reactive ion etching until the TiN bottom electrode was exposed. Finally, post-annealing was conducted in a gaseous mixture of 96% N<sub>2</sub> and 4% H<sub>2</sub> at temperatures ranging from 350 °C to 500 °C, and the annealing time was changed from 10 min to 90 min. Further, to evaluate the performance of 3-D capacitors, silicon trenches with a depth of 70 μm and a width of 10 μm were fabricated by dry etching. Then, a 300 nm SiO<sub>2</sub> film was grown on the walls of silicon trenches by thermal oxidation at 1050 °C, and the subsequent fabrication processes were described as above.

The crystal structures of the Hf<sub>1−x</sub>Zr<sub>x</sub>O<sub>2</sub> films were analysed using a grazing-angle incidence X-ray diffractometer (GIXRD, Bruker D8 Advance) with an incidence angle of 0.5°. The cross-section of the capacitor and the corresponding energy dispersive spectroscopy (EDS) map were characterized using a high-resolution transmission electron microscope (HRTEM, Talos F200XG2) equipped with an EDS system. The Fast Fourier Transform (FFT) of the HRTEM images was performed using a Digital Micrograph (Gatan). The cross-section of the trench template was observed using a scanning electron microscope (SEM, Zeiss SIGAMA HD). The polarization–voltage (*P*–*V*) and endurance characteristics of the devices were measured using a ferroelectric test system (Precision Premier II, Radiant Technologies). The breakdown electric field of the samples was measured using a semiconductor device analyser (Agilent B1500A).

## Results and discussion

Fig. 1(a) shows the representative polarization–electric field (*P*–*E*) hysteresis loops of the capacitors with different dielectrics at 1 kHz after annealing at 450 °C for 30 min while keeping the total dielectric thickness at 10 nm. The capacitor with a single FE layer exhibits a square loop characteristic of the FE material. However, for the capacitor with a single AFE layer, pinched double hysteresis loops are clearly demonstrated, which should be ascribed to the electric field-induced AFE–FE phase



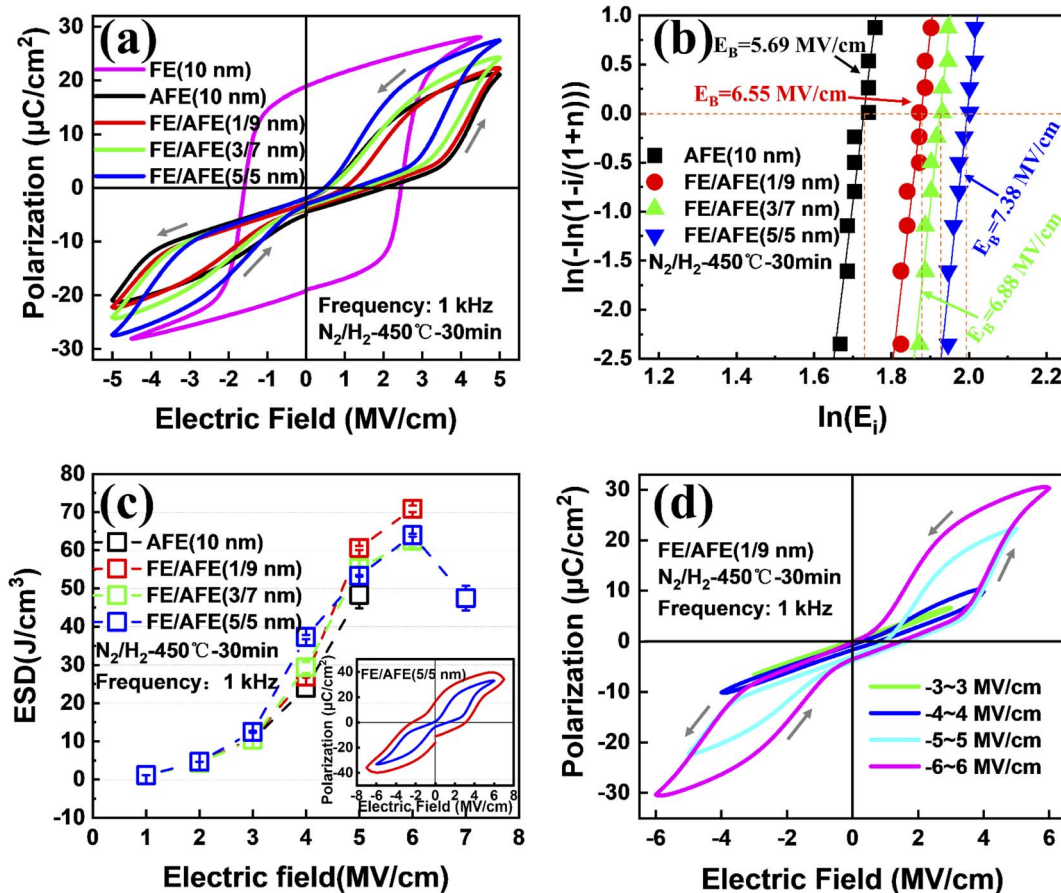


Fig. 1 (a) Typical  $P$ - $E$  hysteresis loops of the capacitors with different FE/AFE stacks as well as a single FE or AFE layer while keeping the total dielectric thickness at 10 nm; (b) Weibull distributions of breakdown electric fields for the capacitors with the FE/AFE stacks and the single AFE layer; (c) the ESD of the above capacitors as a function of an external electric field (10 devices were measured for each sample), the inset shows the  $P$ - $E$  hysteresis loop of the capacitor with the FE/AFE(5/5 nm) stack at 6  $\text{MV}/\text{cm}^{-1}$  and 7  $\text{MV}/\text{cm}^{-1}$ , respectively; (d) dependence of the  $P$ - $E$  hysteresis loops on the external electric field for the capacitor with the FE(1 nm)/AFE(9 nm) stack.

transition.<sup>27</sup> As the thickness of the incorporated FE layer increases from 1 to 5 nm, the fabricated capacitors still exhibit double hysteresis loops and the maximum polarization ( $P_{\text{max}}$ ) increases gradually from 22.2 to 27.4  $\mu\text{C}/\text{cm}^2$  in contrast to 21.3  $\mu\text{C}/\text{cm}^2$  for the single AFE layer. Fig. 1(b) shows the Weibull distribution of breakdown electric fields ( $E_B$ ) for the capacitors with different dielectrics. The mean value of  $E_B$  can be extracted from the intersection of the fitting line and the  $X$  axis when  $Y = 0$ . Compared with the single AFE layer, the diverse FE/AFE stacks generate higher mean  $E_B$ , *i.e.*, 6.55–7.38  $\text{MV}/\text{cm}^{-1}$ . Meanwhile, the resulting  $E_B$  gradually increases with the increase of the FE thickness. This is because the dielectric constant of the AFE layer is greater than that of the FE layer.<sup>26</sup> Based on the Gauss law and Kirchhoff voltage law, the introduction of the FE layer reduces the electric field across the AFE layer in the FE/AFE stack, and at the same time, the generated electric field across the AFE layer decreases gradually with the increase of the FE layer thickness at a fixed external bias.

The recoverable ESD ( $W_{\text{rec}}$ ) of a capacitor can be calculated by the integration of the electric field by polarization, described as eqn (1):<sup>28</sup>

$$W_{\text{rec}} = - \int_{P_{\text{max}}}^{P_r} E dP \quad (1)$$

where  $E$  is the external electric field, and  $P_r$  and  $P_{\text{max}}$  represent the remanent polarization and maximum polarization, respectively. Therefore, the calculated ESD is demonstrated in Fig. 1(c) for the different dielectric capacitors. In terms of the single AFE capacitor, the resulting ESD gradually rises to its near-maximum of 47.3  $\text{J}/\text{cm}^3$  with increasing the external electric field up to 5  $\text{MV}/\text{cm}^{-1}$ . This is because a slightly higher electric field ( $\geq 5.54 \text{ MV}/\text{cm}^{-1}$ ) could give rise to electrical breakdown of the single AFE capacitor, as shown in Fig. 1(b). In addition, all the FE/AFE capacitors exhibit higher ESDs than the single AFE capacitor at 5  $\text{MV}/\text{cm}^{-1}$ , and the FE (1 nm)/AFE (9 nm) stack gives rise to the largest ESD, even at 6  $\text{MV}/\text{cm}^{-1}$ . It is worth mentioning that the  $E_B$  of capacitors with the FE (5 nm)/AFE (5 nm) stack is bit higher than 7  $\text{MV}/\text{cm}^{-1}$ , so the corresponding  $P$ - $E$  loops can be measured under the maximum external electric field of 7  $\text{MV}/\text{cm}^{-1}$ . Nevertheless, it is found that the calculated ESD dramatically decreases to 46.9  $\text{J}/\text{cm}^3$  in comparison with that at 6  $\text{MV}/\text{cm}^{-1}$  because the  $P_r$  value greatly increases at 7  $\text{MV}/\text{cm}^{-1}$ , as shown in the inset in Fig. 1(c). There are two





Fig. 2 Comparison of the maximum ESD and the corresponding ESE for the capacitors with different FE/AFE compositions (ten devices are measured for each sample).

possible reasons for the significant increase in  $P_r$ . On one hand, the electric field of  $7 \text{ MV cm}^{-1}$  is particularly close to the breakdown electric field of the FE (5 nm)/AFE (5 nm) stack, leading to a large leakage current, and the polarization charges contributed by the leakage current during the  $P$ - $E$  measurement are also derived from the  $P$ - $E$  loops, so the high leakage current can lead to a large increase in  $P_r$ .<sup>22</sup> On the other hand, the antiferroelectricity of the  $\text{Hf}_{1-x}\text{Zr}_x\text{O}_2$  films results from the field-induced phase transition between the FE orthorhombic (O) and AFE tetragonal (T) phases.<sup>10</sup> When the applied electric field increases, the T-phase changes into the O-phase, and changes back into the T-phase after reducing the applied electric field, and thus the AFE films show double hysteresis loops.<sup>10</sup> However, when the applied electric field is too large, the field-induced phase-transition processes are partially disrupted, making the O-phase unable to return to the T-phase completely. Therefore, the relative content of the O-phase in the film increases, thus resulting in an increase in  $P_r$ . Based on the above experimental results, it is concluded that the employment of FE

(1 nm)/AFE (9 nm) can offer the highest ESD. Further, the corresponding  $P$ - $E$  hysteresis loops are displayed in Fig. 1(d). As the maximum electric field increases from 3 to  $6 \text{ MV cm}^{-1}$ , the resulting  $P$ - $E$  loops gradually widen, and the  $P_{\text{max}}$  increases from 6.6 to  $30.3 \mu\text{C cm}^{-2}$ . For the electric fields of  $\leq 4 \text{ MV cm}^{-1}$ , the  $P_{\text{max}}$  is quite small because the applied electric field is lower than the transition electric field from the AFE phase to the FE phase ( $E_{\text{AFE-FE}}$ ), resulting in a very low ESD.

On the other hand, the ratio of the recoverable ESD to the total stored energy density is defined as the ESE ( $\eta$ ) of a capacitor, which can be calculated by using eqn (2)<sup>28</sup>

$$\eta = \frac{-\int_{0}^{P_r} E dP}{\int_{0}^{P_{\text{max}}} E dP} \quad (2)$$

Fig. 2 shows the calculated ESE and the maximum ESD for the capacitors with different FE/AFE compositions after annealing at  $450 \text{ }^\circ\text{C}$  for 30 min. As the FE thickness increases from 0 to 5 nm at a fixed total dielectric thickness of 10 nm, the ESE decreases from 61% to 53%, demonstrating relatively small variations. Moreover, the composition of FE (1 nm)/AFE (9 nm) shows the largest ESD of  $71.93 \text{ J cm}^{-3}$ , accompanied by an ESE as large as 57.6%.

To observe the effects of annealing temperature and annealing time on the ESD and ESE, the capacitors with the FE (1 nm)/AFE (9 nm) stack are further annealed under various annealing conditions. Fig. 3 shows the influences of annealing temperature and time on the maximum ESD and ESE for the FE (1 nm)/AFE (9 nm) capacitors. As the annealing temperature rises from 350 to  $450 \text{ }^\circ\text{C}$  at a constant annealing time of 30 min, the obtained maximum ESD initially increases rapidly from 59.01 to  $71.93 \text{ J cm}^{-3}$ , and then decreases to  $67.47 \text{ J cm}^{-3}$  at the annealing temperature of  $500 \text{ }^\circ\text{C}$ . In addition, the corresponding ESE also demonstrates a similar variation trend, reaching a maximum value of 57.6% after annealing at  $450 \text{ }^\circ\text{C}$  for 30 min. Further, the annealing time is also optimized at a fixed annealing temperature of  $450 \text{ }^\circ\text{C}$ , as shown in Fig. 3(b). It is found that when the annealing time is maintained between 30 and 70 min, the resulting maximum ESD and ESE remain

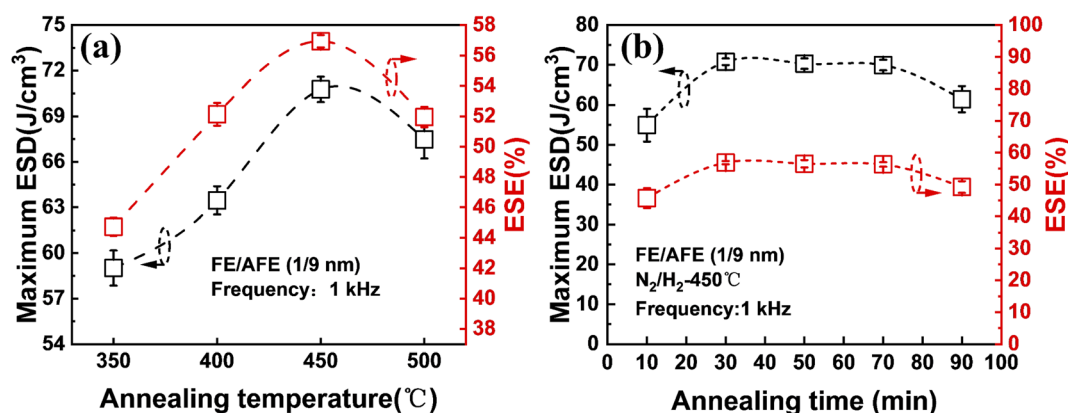


Fig. 3 The maximum ESD and corresponding ESE of the capacitor with the FE (1 nm)/AFE (9 nm) stack: (a) at different annealing temperatures for 30 min; (b) at  $450 \text{ }^\circ\text{C}$  for different annealing times. Ten devices are measured for each sample.

relatively stable, corresponding to  $71.93 \text{ J cm}^{-3}$  and  $\sim 57.6\%$ , respectively. However, both of them decrease for a shorter or longer annealing time (*i.e.*, 10 or 90 min). When the annealing time is 10 min, it is possible that the FE/AFE stack is not fully crystallized and fails to form enough T-phase, resulting in lower ESD and ESE. When the annealing time increases to 90 min, the grain sizes of the FE/AFE layer become larger, resulting in a reduction in the relative content of the T-phase in the film because a larger grain size would be more favourable for the formation of the O-phase.<sup>29</sup> Thus, the energy storage performance of the device deteriorates as the annealing time increases to 90 min. Therefore, 30 min annealing at  $450^\circ\text{C}$  can be considered as the optimized annealing conditions for the capacitor with the FE (1 nm)/AFE (9 nm) stack.

To find out the influence of thermal annealing on the textures of the investigated dielectrics, the top TiN films of the TiN/dielectrics/TiN samples were removed by dry etching after post-annealing, and then the resulting samples were characterized by GIXRD, as shown in Fig. 4. As for the single AFE film and different FE/AFE stacks, an intense diffraction peak at  $\sim 30^\circ$  is observed after annealing at  $450^\circ\text{C}$  for 30 min, which should be related to O- and T-phases, *i.e.*, O (111)/T (101)/T (011)

phases.<sup>22,30</sup> Moreover, two weak diffraction peaks at  $\sim 35.0^\circ$  and  $\sim 51.1^\circ$  result from O (200)/T (110) and O (220)/T (200) phases, respectively, and the other two peaks originate from the TiN films.<sup>31,32</sup> Since the  $2\theta$  values corresponding to the O (111) and T (101), (011) phases are very close for the  $\text{Hf}_{1-x}\text{Zr}_x\text{O}_2$  films due to their structural similarities,<sup>31,33</sup> the intense diffraction peak at  $\sim 30^\circ$  is further de-convoluted into several Gaussian peaks in order to clarify the phase composition, as shown in Fig. 4(b). Here, we only estimate the relative content of the T/O-phase based on the most intense peak, and it does not represent the absolute content of the T/O-phase in the film since another two weak diffraction peaks are also present at  $\sim 35.0^\circ$  and  $\sim 51.1^\circ$ , respectively. Regarding the single AFE layer, the resulting two peaks are located at  $29.8^\circ$  and  $30.4^\circ$ , corresponding to the T (011) and O (111) phases, respectively.<sup>31,33</sup> For the FE/AFE stacks, the fitted two peaks appear at  $29.8^\circ$  and  $30.17^\circ$ , resulting from the T (011) and T (101) phases, respectively.<sup>33,34</sup> The aforesaid results indicate that the introduction of a FE underlying film prevents the formation of the ferroelectric O (111)-phase and generates a new antiferroelectric T (101) phase. Such an increased proportion of the T-phase is beneficial to the AFE behavior.<sup>21</sup> Further, as the FE layer increases from 1 to 5 nm, the

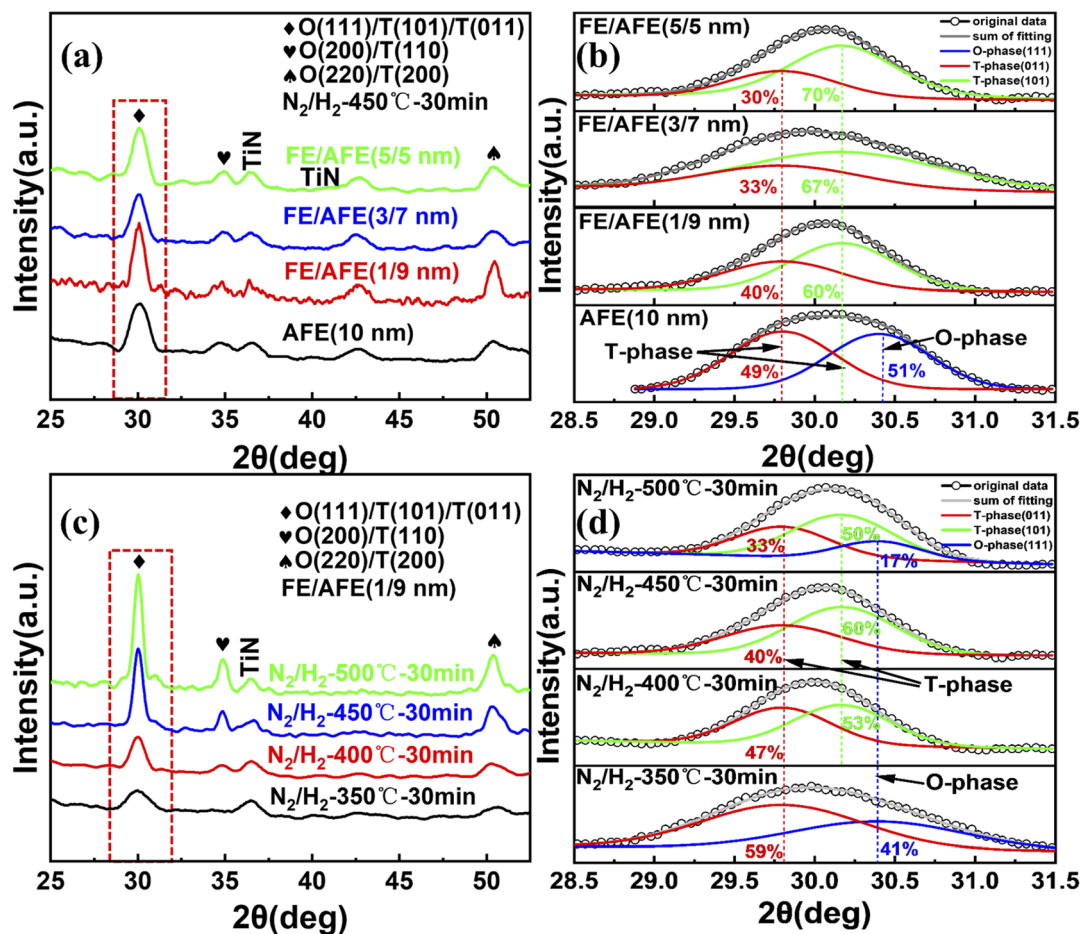


Fig. 4 (a) GIXRD patterns and (b) de-convolution of the diffraction peak of O (111)/T (101)/T (011) for the single AFE film and different FE/AFE stacks on the TiN film after annealing at  $450^\circ\text{C}$  for 30 min; (c) GIXRD patterns and (d) de-convolution of the peak of O (111)/T (101)/T (011) for the FE (1 nm)/AFE (9 nm) stack on the TiN film after annealing at different temperatures for 30 min.



relative percentage of the T (101) phase rises from 60% to 70%; however, the relative content of the T (011) phase decreases from 40% to 30%. Based on the intensity of the peak at  $\sim 30^\circ$ , it is found that the most T-phases are formed in the FE (1 nm)/AFE (9 nm) stack in comparison with the other stacks. This should correlate with a thicker AFE layer which is helpful to enhance the T-phase texture. In short, the incorporation of the underlying FE film even as thin as 1 nm affects the enhancement of the AFE phases. Fig. 4(c) shows the GIXRD patterns of the FE (1 nm)/AFE (9 nm) stack as a function of annealing temperature at a constant annealing time of 30 min. It can be observed that the diffraction peaks gradually enhance with the annealing temperature, especially when the annealing temperature reaches  $450^\circ\text{C}$  or higher. This indicates that the grains formed in the FE/AFE stacks grow up gradually with the increase of annealing temperature. For example, according to the Scherrer formula, the calculated average grain sizes are equal to  $\sim 6.1$  nm and  $\sim 7.8$  nm, respectively, in terms of  $450^\circ\text{C}$  and  $500^\circ\text{C}$  annealing temperatures. A smaller grain size means the presence of more grain boundaries in the thin films, which is favorable for the formation of T-phases associated with the AFE behaviors.<sup>29,32</sup> Further, the most intense diffraction peak associated with the O (111)/T (101)/T (011) phases is fitted with Gaussian functions, as shown in Fig. 4(d). In terms of  $350^\circ\text{C}$  annealing, two components corresponding to the T (011) and O (111) phases are deduced. Owing to the existence of the ferroelectric O (111) phase, the resulting maximum ESD is rather low. When the annealing temperature increases to  $400^\circ\text{C}$ , the O (111) phase disappears and the antiferroelectric T (101) phase comes into being. Therefore, the total content of the antiferroelectric T (011) and (101) phases increases in the sample, leading to a further increase in the ESD. After annealing at

$450^\circ\text{C}$  for 30 min, the peaks associated with the T (011) and (101) phases become more intense, indicating a significant increase in the T phases. This should give rise to a rapid rise in the ESD. However, when the annealing temperature is elevated to  $500^\circ\text{C}$ , one additional O (111) phase is formed, accounting for 17% of the total peak area. This means that the T phase content is reduced, hence resulting in a decrease in the ESD. The above analyses are in good agreement with the change of ESD with annealing temperature, as shown in Fig. 3(a). In a word, our experimental results confirm that the composition of FE (1 nm)/AFE (9 nm) can achieve the optimal energy storage performance at the annealing temperature of  $450^\circ\text{C}$ .

Fig. 5(a) and (b) show the cross-sectional TEM image and corresponding EDS maps of various elements for the TiN/FE (1 nm)/AFE (9 nm)/TiN capacitor, demonstrating a uniform dielectric thickness and clear interfaces of  $\text{Hf}_x\text{Zr}_{1-x}\text{O}_2/\text{TiN}$ . In addition, the interface of FE (1 nm)/AFE (9 nm) cannot be distinguished intuitively, which is due to the similar elemental composition in the FE and AFE layers and the ultrathin thickness of FE. Further, the elemental profiles along the cross-section of the capacitor are drawn in Fig. 5(c). It is found that the atomic fractions of Hf and Zr display distinct variations near 60 nm, that is, the atomic ratio of Hf/Zr increases from 1 : 3 (*i.e.*, 12.2%/35.6%) to 1 : 1 (*i.e.*, 23.2%/24.3%). Meanwhile, the plateau width corresponding to Hf/Zr = 1 : 3 is much larger than that associated with Hf/Zr = 1 : 1. Thus, this discloses the transition from the  $\text{Hf}_{0.25}\text{Zr}_{0.75}\text{O}_2$  (AFE) layer to the  $\text{Hf}_{0.5}\text{Zr}_{0.5}\text{O}_2$  (FE) layer, which is in accord with our experimental design. For comparison, the elemental profiles of the single AFE (10 nm) capacitor are also demonstrated in Fig. 5(d). Both Zr and Hf profiles exhibit stable plateaus, in which the atomic ratio of Hf/

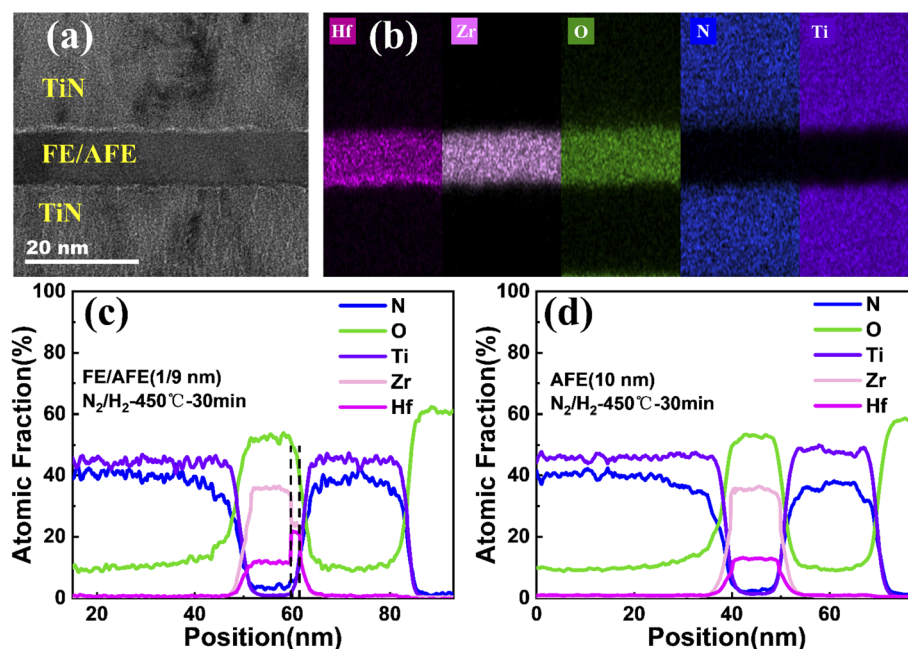


Fig. 5 (a) Cross-sectional TEM image and (b) the corresponding EDS maps of Hf, Zr, O, N, and Ti elements for the FE (1 nm)/AFE (9 nm) capacitor; cross-sectional profiles of the elements from (c) the FE (1 nm)/AFE (9 nm) capacitor and (d) the single AFE (10 nm) capacitor, respectively.



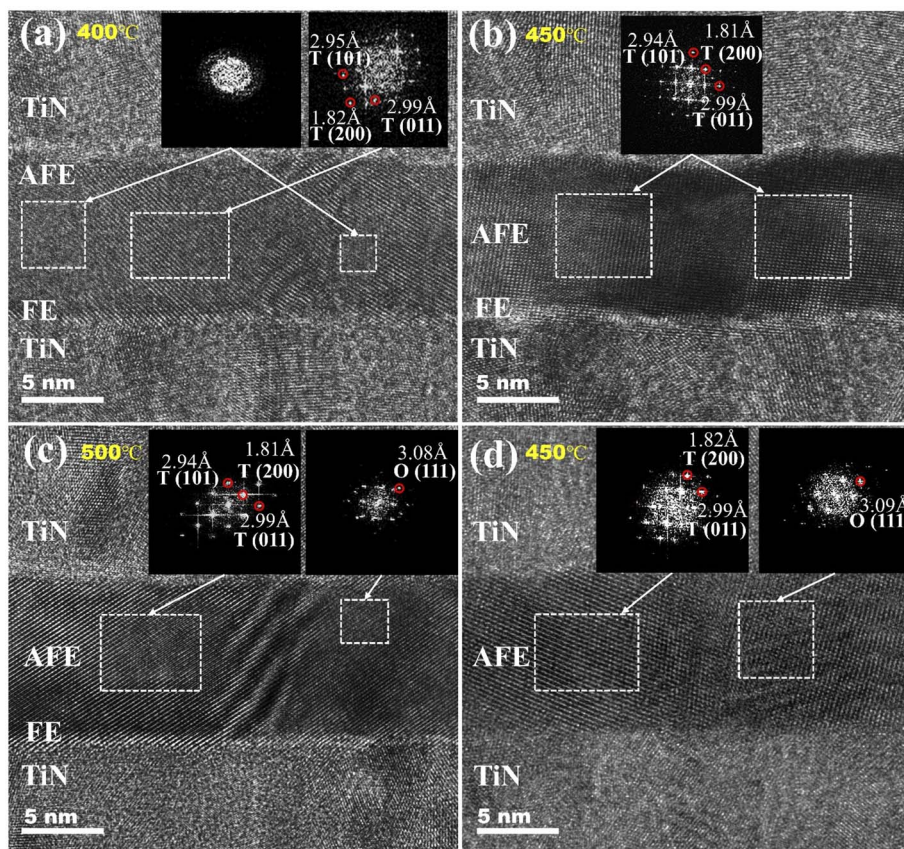


Fig. 6 Cross-sectional HRTEM images and FFT (insets) of the FE (1 nm)/AFE (9 nm) stack annealed for 30 min at (a) 400 °C, (b) 450 °C and (c) 500 °C, respectively. (d) Cross-sectional HRTEM image and FFT (insets) of the single AFE layer annealed at 450 °C for 30 min.

Zr is kept at 1 : 3 (*i.e.*, 12.6%/35.9%). This is also consistent with the composition of the AFE layer.

For insight into the effect of annealing temperature on the microstructures of the AFE and FE layers, HRTEM analyses are carried out on the FE (1 nm)/AFE (9 nm) sample annealed at different temperatures, as shown in Fig. 6. In terms of 400 °C

annealing, crystalline T (101), (011), (200) phases and amorphous texture are coexistent in the AFE layer according to the FFT diffractograms of selected areas, as shown in Fig. 6(a). After annealing at 450 °C, the AFE layer becomes fully crystalline, revealing the coexistence of T (101), (011), and (200) phases, as indicated in Fig. 6(b). When the annealing temperature

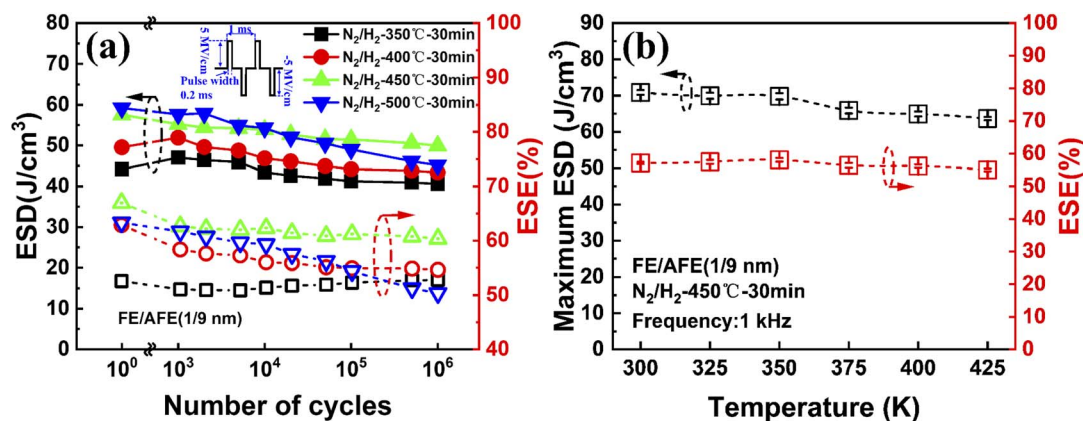


Fig. 7 (a) Evolution of the ESD and ESE with the number of electrical pulse cycles (switching frequency: 1 kHz; pulse amplitude:  $\pm 5$  MV cm; pulse width: 0.2 ms; waveform: square) for the FE (1 nm)/AFE (9 nm) capacitor annealed at different temperatures for 30 min, respectively; (b) dependence of the maximum ESD and corresponding ESE on measurement temperature for the FE (1 nm)/AFE (9 nm) capacitor annealed at 450 °C for 30 min (ten devices are measured at each temperature).



increases to 500 °C, the T (101), (011), and (200) phases still exist in the AFE layer, but the O (111) phase is also observed in some selected regions, see Fig. 6(c). This indicates that an excessively high annealing temperature can induce partial transformation of the T phase into the O phase, hence inhibiting the contributions from the AFE component. On the other hand, as for the single AFE capacitor annealed at 450 °C for 30 min, the O (111) phase is coexistent with the T (011) and (200) phases, as shown in Fig. 6(d). This causes a decrease in the proportion of the T-phase in the AFE film, so the AFE behavior and the ESD are

weakened. To sum up, the above HRTEM analyses further confirm the XRD results in Fig. 4; meanwhile, the introduction of an ultrathin underlying FE layer changes the crystallization behaviors of the AFE film, and is beneficial to the formation of the AFE T-phases especially at the annealing temperature of 450 °C. Thus, the resulting energy storage performance is greatly improved compared with the single AFE capacitor.

To further explore the effect of annealing temperature on the electrical cycling endurance of the FE (1 nm)/AFE (9 nm) capacitors, the  $P$ - $E$  loops of the capacitors annealed at different

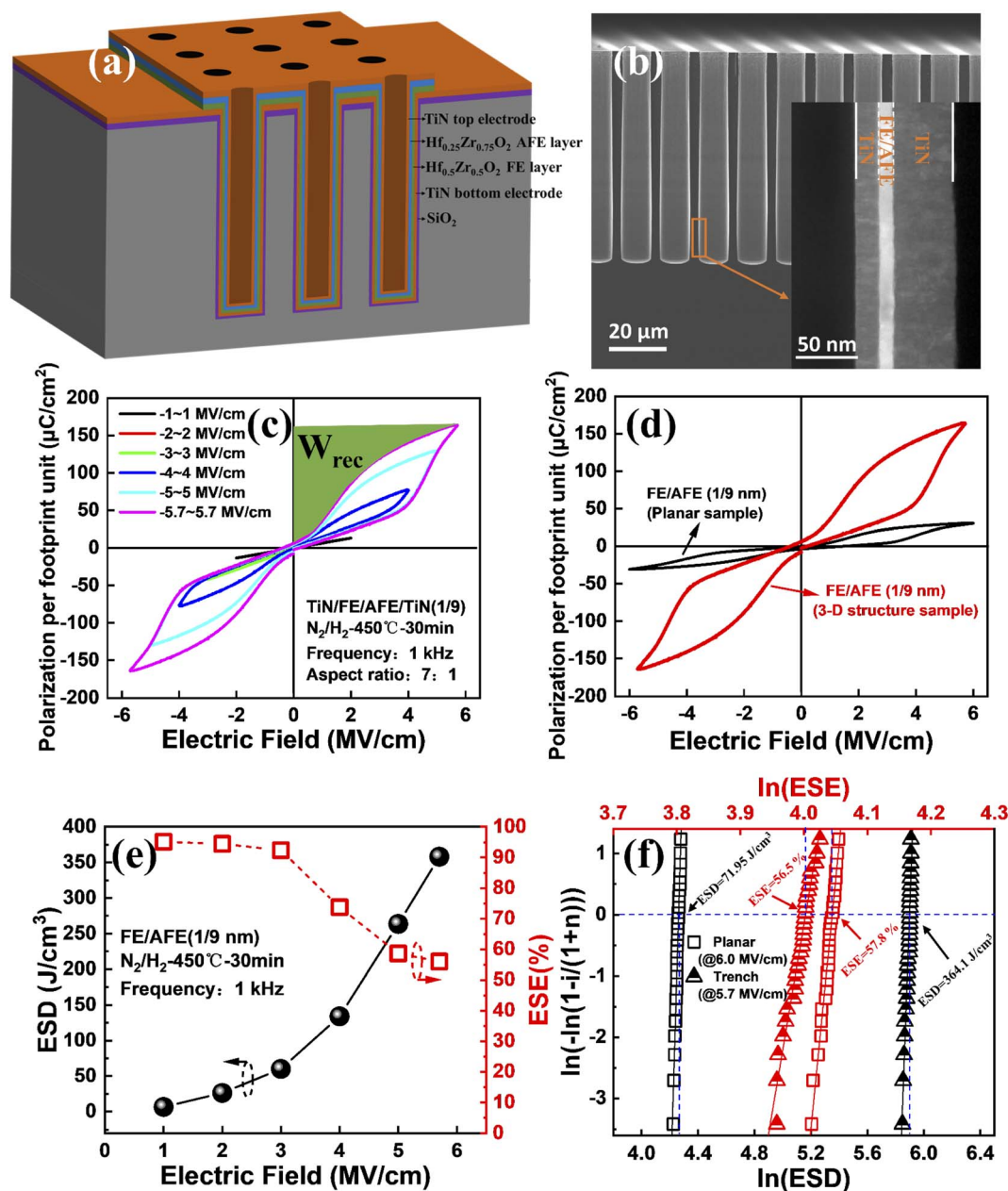


Fig. 8 (a) Schematic of a 3-D trench capacitor; (b) cross-sectional SEM image of the 3-D capacitors with the FE (1 nm)/AFE (9 nm) stack, which are fabricated on the silicon trench substrate with an aspect ratio of 7 : 1; (c) dependence of the  $P$ - $E$  hysteresis loops on the external electric field for the 3-D trench capacitor with the FE (1 nm)/AFE (9 nm) stack; (d)  $P$ - $E$  hysteresis loops for a planar and a 3D FE (1 nm)/AFE (9 nm) stack-based capacitor; (e) the extracted ESD and ESE as a function of the electric field for the 3-D capacitor; (f) Weibull distributions of the extracted maximum ESD and ESE for the 3-D and planar capacitors (30 devices are measured for each kind of capacitor).





temperatures are measured as a function of electrical pulse cycles, and the extracted energy storage performance is shown in Fig. 7(a). It is found that the capacitor annealed at 450 °C still exhibits the largest ESD and ESE after  $10^6$  operating cycles at 5  $\text{MV cm}^{-1}$ , and the corresponding degradation rates are close to 13.2% and 2.7%, respectively. However, both the capacitors annealed at 400 °C and 500 °C show larger degradation rates of ESD and ESE, which are equal to 16.4% and 4.6%, 23.7% and 15.6%, respectively. Furthermore, both the maximum ESD and the corresponding ESE are also extracted at different measurement temperatures for the capacitor annealed at 450 °C for 30 min, as illustrated in Fig. 7(b). It is observed that the maximum ESD and ESE demonstrate reductions of only 10% and 4%, respectively, with the increase of measurement temperature from 300 to 425 K. This also indicates that the FE (1 nm)/AFE (9 nm) capacitors have excellent temperature stability for energy storage applications.

It is well known that a much higher ESD per footprint unit can be realized through integration of the capacitor into a 3-D template because of a significant increase in the surface area of electrodes. Therefore, it is of significance to integrate the FE (1 nm)/AFE (9 nm) capacitor into deep silicon trenches. Fig. 8(a) shows the schematic of the fabricated 3-D capacitor, and the corresponding cross-sectional SEM image is shown in Fig. 8(b). Regular trenches with vertical and smooth side walls are obtained successfully, showing an aspect ratio of 7 : 1. Moreover, diverse material layers including TiN electrodes and  $\text{Hf}_x\text{Zr}_{1-x}\text{O}_2$  dielectrics are well filled into the trenches by PEALD (see the inset). The dependence of the  $P$ - $E$  hysteresis loops on the external electric field for the 3-D trench capacitor with the FE (1 nm)/AFE (9 nm) stack is shown in Fig. 8(c), and as the maximum electric field increases from 1 to 5.7  $\text{MV cm}^{-1}$ , the resulting  $P$ - $E$  loops gradually widen, and the max polarization per footprint unit increases from 13.3 to 163.2  $\mu\text{C cm}^{-2}$ . The green area indicates the recoverable ESD ( $W_{\text{rec}}$ ), which can be calculated by the integration of the electric field by polarization per footprint unit. As shown in Fig. 8(d), compared with the planar capacitor, the polarization per footprint unit for the 3-D trench capacitor greatly increases, which is attributed to a significant increase in the actual electrode area of the 3-D capacitor since the total stored charges are proportional to the capacitor area. Fig. 8(e) shows the ESD and ESE of the fabricated 3-D capacitor under different electric fields. As the electric field increases from 1 to 5.7  $\text{MV cm}^{-1}$ , the ESD increases gradually from 6.45 to 358.14  $\text{J cm}^{-3}$ , however, the ESE decreases from 95% to 56%. In particular, when the electric field is larger than 3  $\text{MV cm}^{-1}$ , the ESE exhibits a remarkable decrease. This is because the enlarged  $P$ - $E$  hysteresis loop leads to a larger hysteresis loss. To evaluate the uniformity of the fabricated 3-D capacitors, 30 devices are measured in comparison with the planar capacitors. The Weibull distributions of the extracted maximum ESD and ESE are shown in Fig. 8(f). It is found that the 3-D capacitors demonstrate a mean ESD of 364.1  $\text{J cm}^{-3}$ , which is around five times that (71.95  $\text{J cm}^{-3}$ ) for the planar capacitors. In addition, although the planar capacitors display excellent electrical uniformity, the 3-D capacitors also have a quite narrow distribution of maximum ESD. On the other hand, both the planar



Fig. 9 Comparison of the achievable ESD and the ESE between our FE/AFE stack capacitors and other  $\text{HfO}_2/\text{ZrO}_2$ -based single AFE capacitors.

and 3-D capacitors exhibit very close ESEs, corresponding to 57.8% and 56.5%, respectively.

Fig. 9 compares the ESDs and ESEs of our FE (1 nm)/AFE (9 nm) capacitors and the reported  $\text{HfO}_2/\text{ZrO}_2$ -based single AFE capacitors.<sup>35–37</sup> It can be observed that our planar capacitor demonstrates the highest ESD compared with other  $\text{HfO}_2/\text{ZrO}_2$ -based single AFE capacitors, which should be attributed to the introduction of an ultrathin FE layer between the AFE layer and the TiN electrode, hence enhancing the formation of the AFE T-phases. Further, our 3-D capacitor shows much greater superiority in ESD than others while holding an above average ESE. By increasing the density and aspect ratio of trenches, the resulting ESD can be vastly elevated. Thus, the 3-D FE/AFE capacitors provide a promising opportunity for practical on-chip energy storage applications.

## Conclusion

The FE- $\text{Hf}_{0.5}\text{Zr}_{0.5}\text{O}_2/\text{AFE}-\text{Hf}_{0.25}\text{Zr}_{0.75}\text{O}_2$  capacitors with TiN electrodes are fabricated using the PE-ALD technique. By optimizing the FE/AFE thickness composition and post-annealing conditions, the highest ESD planar capacitors are obtained for the 1 nm FE/9 nm AFE bilayer after annealing at 450 °C for 30 min, *i.e.*, the resulting ESD and ESE are equal to 71.95  $\text{J cm}^{-3}$  and 57.8% at 6  $\text{MV cm}^{-1}$ , respectively. This should be attributed to the introduction of the ultrathin FE layer between the AFE layer and the TiN electrode, hence enhancing the formation of the T phase with antiferroelectricity in the AFE  $\text{Hf}_{0.25}\text{Zr}_{0.75}\text{O}_2$  layer. Meanwhile, compared with the single AFE capacitor, the introduction of the 1 nm FE layer increases the breakdown electric field of the FE/AFE capacitor. Moreover, the FE (1 nm)/AFE (9 nm) bilayer capacitors also demonstrate superior electrical cycling endurance, and an excellent temperature stability from 300 to 425 K, which makes them more competitive for applications in high-temperature environments. Further, by integrating the capacitor into deep silicon trenches, a superhigh



ESD of  $364.1 \text{ J cm}^{-3}$  is achieved together with an ESE of 56.5%. The current study provides a new strategy to achieve CMOS process-compatible, eco-friendly and superhigh ESD capacitors for practical on-chip energy storage applications.

## Author contributions

The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.

## Conflicts of interest

There are no conflicts to declare.

## Acknowledgements

This work was supported in part by the National Natural Science Foundation of China under Grant 61874029.

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