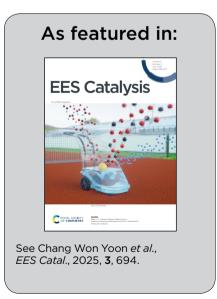


Showcasing research from Prof. Chang Won Yoon's lab., Pohang University of Science and Technology, Republic of Korea.

Direct electrolysis of liquid anhydrous ammonia for continuous production of high-purity, pressurized hydrogen at ambient temperature

NH $_3$ is valued as a large-scale H $_2$ carrier due to its high H $_2$ storage capacities (\geq 108 kg-H $_2$ m- 3 , 17.7 wt%) and simple liquefaction conditions (25 °C at 10 bar). However, producing high-purity and pressurized H $_2$ via catalytic NH $_3$ (g) thermolysis requires high temperatures (>600 °C) with multiple purification and compression steps. Here, we present a proof-of-concept study using a zero-gap liquid anhydrous NH $_3$ electrolyzer comprising electrocatalysts and a cation exchange membrane that directly converts gap liquid anhydrous NH $_3$ into high-purity (>99.99%) and pressurized (>5.5 bar) H $_2$ at 10 °C with a Faradaic efficiency of >98.8%.

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Direct electrolysis of liquid anhydrous ammonia for continuous production of high-purity, pressurized hydrogen at ambient temperature†

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The direct electrolysis of liquid anhydrous ammonia (NH₃(l), >99.99% of NH₃, free of water and solvent) is demonstrated using a 25 cm² zero-gap electrolyzer, consisting of a Ru/C anode and a Pt/C cathode, with the two electrodes spatially separated by a cation exchange membrane. This system, supplied by NH₃(l) and NH₄Br as the supporting electrolyte, continuously produces high-purity and pressurized hydrogen (H₂, >99.99%, >5.5 bar) at a temperature of 10 °C and a pressure of 6.2 bar, without requiring H₂/N₂ separation and compression processes. The direct NH₃(l) electrolyzer exhibits a cell potential of 1.1 V at 0.1 A cm⁻², presenting a faradaic efficiency of > 99.3% for H_2 production. The developed system achieves a H_2 production rate of >18.8 mol-H₂ g_{cat}^{-1} h⁻¹ at 0.5 A cm⁻², which is 4.7-fold higher than the highest H₂ production rate reported to date for NH₃(g) thermolysis at temperatures of over 500 °C.

Introduction

Hydrogen (H₂) is a promising renewable energy carrier owing to its high gravimetric energy density (33.3 kWh kg-H₂⁻¹) and environmentally benign properties. However, its low volumetric energy density (3 kWh m⁻³ at 20 °C, 1 bar) poses a substantial scientific challenge, particularly for its large-scale storage and long-distance transportation. 1-3 To address these limitations, green and/or blue ammonia (NH₃) has been proposed as a promising H₂ carrier due to its high volumetric H_2 storage capacity (≥ 108 kg- H_2 m⁻³),⁴⁻⁷ and ease of liquefaction (e.g., 25 °C, 10 bar). The transported liquid anhydrous NH₃ (NH₃(l), >99.99% of NH₃, free of water and

Broader context

Hydrogen (H2) is a key energy carrier that resolves the imbalance between renewable energy production and demand, contributing to global carbon neutrality. However, the low volumetric energy density of gaseous H2 (3 kWh m⁻³ at 20 °C, 1 bar) poses challenges for large-scale storage and transportation. To address this limitation, ammonia (NH3) has gained significant attention as a sustainable H2 carrier due to its superior H2 storage capacity and simple liquefaction conditions (10 bar at 25 °C). NH3(g) thermolysis for hydrogen production is currently being developed for commercial implementation, but it requires high reaction temperatures (>600 °C) with multi-step purification, separation and compression processes. This study presents a proof-of-concept demonstration of the direct electrolysis of liquid anhydrous NH3 (>99.99%, water/solvent-free) to produce H2 at near-ambient temperature (10 °C). The zerogap NH3(l) electrolyzer, designed with electrocatalysts and a cation exchange membrane, enables the production of high-purity (>99.99%) and pressurized (>5.5 bar) H2 in a single process. Our developed system achieves a faradaic efficiency of >98.8% and a 4.7-fold higher H₂ production rate compared to the state-of-the-art NH3(g) thermolysis. The proposed continuous NH3(l) electrolyzer offers an alternative H2 production model from NH3, potentially improving the cost efficiency and flexibility of H2 generation facilities.

solvent) can then release H₂ on demand through thermal cracking, releasing only nitrogen (N_2) as a byproduct, as shown in eqn (1). However, due to its endothermic nature, most of the processes currently being developed to thermally crack NH3(g) typically require high temperatures exceeding 600 °C and even higher temperatures are needed to obtain high-pressure H₂.8 Accordingly, a thermally enhanced NH₃(g) dehydrogenation process integrated with multistep separation procedures may be suitable for a centralized H₂ production facility (Fig. 1A). 9,10

$$NH_3 \rightarrow 0.5N_2 + 1.5H_2, \quad \Delta H = +46 \text{ kJ mol}^{-1}$$
 (1)

$$NH_3(l) \rightarrow 0.5N_2 + 1.5H_2, E = 0.068 V$$
 (2)

As an alternative strategy, electrochemically converting NH₃ to H₂ has been proposed. Two concepts for the electrolysis of NH₃ exist: (i) aqueous NH₃ electro-oxidation reaction (AOR, NH₃(aq), Fig. 1B)¹¹⁻¹³ and (ii) direct electrolysis of liquid

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[†] Electronic supplementary information (ESI) available: Document S1: equations of ammonia electro-oxidation reaction S1-S3, Notes S1-S4, Fig. S1-S12, Tables S1-S3 and references. See DOI: https://doi.org/10.1039/d5ey00140d

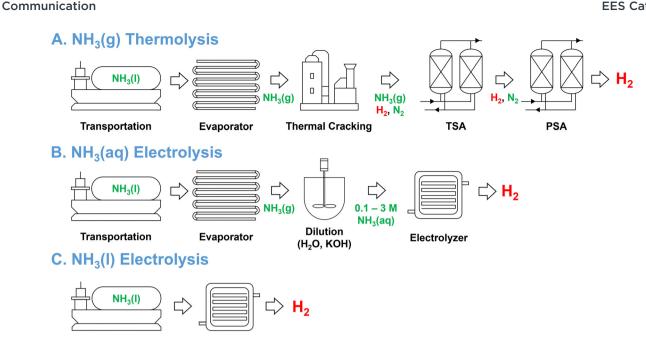


Fig. 1 Schematic illustration of three H₂ production methods utilizing NH₃. (A) Thermolysis of NH₃(g). (B) Ammonia electro-oxidation reaction (AOR) of diluted NH₃(ag). (C) Direct electrolysis of NH₃(l).

anhydrous NH₃ (NH₃(l), Fig. 1C). 14-17 Compared with the potential of water electrolysis (+1.23 V), 18,19 these methods lower the cell voltage (E_{cell}) to 0.060 V for the AOR (eqn (S1)-(S3), ESI†) and 0.068 V for direct NH3(l) electrolysis (eqn (2) and Note S1, ESI†), thereby potentially achieving high energy efficiency for H₂ production. For the AOR, however, diluted aqueous NH₃(aq) solutions (ca. 0.1-3 M, 0.2-5 wt%) with potassium hydroxide (KOH, ca. 0.1-7 M, 0.6-30 wt%) in distilled H₂O are commonly used, 20-22 which require additional chemicals and waste treatment facilities, thus potentially increasing the cost of H2 production. In addition, anodic N₂ production in the AOR competes with the oxygen evolution reaction in water electrolysis, possibly leading to the formation of byproducts such as NO_x. ^{23,24} Thus, cell operation at a high current density is limited, making it challenging to achieve a high H₂ production rate.

Electrolyzer

Transportation

In contrast, direct NH₃(l) electrolysis requires no water addition and can be conducted under ambient temperature. In addition, NH₃(l) has favorable liquefaction conditions (25 °C at 10 bar) and appropriate viscosity (1.57 mPa s at 20 °C) for electrolysis.²⁵ Moreover, the volumetric and gravimetric H₂ storage capacities of NH₃(l) are higher than those of H₂O (112 kg-H₂ m⁻³ and 11.2 wt%). Previously, pioneering studies on NH₃(l) electrolysis using metal plates or disks in a batch reactor by adding either anionic (KNH2, NaNH2) or cationic (NH₄PF₆) supporting electrolyte have been shown to achieve H₂ generation. 14-16 However, the basic electrochemical properties (e.g., anode/cathode potentials, overpotential and Tafel slopes) of the active metals used for NH₃(l) electrolysis have not been elucidated. Moreover, separation processes for the produced H₂/N₂ mixed gases are still necessary to obtain high-purity H₂ due to the limitations of batch reactions on small scales. Therefore, designing an efficient and scalable electrolysis system that enables the continuous production of high-purity H₂ in a flow reactor and acquiring fundamental parameters associated with NH₃(l) electrochemical reactions is necessary.

Here, we describe a continuous system for the direct electrolysis of NH₃(l) to produce high-purity and pressurized H₂. Potential anode and cathode active metals are initially screened in a batch reactor. Subsequently, a zero-gap type electrolysis cell, configured with a Ru/C anode and Pt/C cathode, each with an active area of 25 cm² on carbon foam and NH₄Br as a supporting electrolyte, is designed and operated under near-ambient temperature and pressurized conditions (10 °C, 6.2 bar). The developed electrochemical splitting system utilizing NH₃(l) demonstrates the continuous production of high-purity and pressurized H₂ (>99.99%, > 5.5 bar) without a H₂/N₂ separation process, achieving a faradaic efficiency of > 98.8% for H₂ production.

Results and discussion

Anode (NER):
$$4NH_3(l) \rightarrow 0.5N_2 + 3NH_4^+ + 3e^-$$
,
 $E = 0.041 \text{ V } \text{vs. SHE}$ (3)

Cathode (HER):
$$3NH_4^+ + 3e^- \rightarrow 1.5H_2 + 3NH_3(l)$$
,

$$E = -0.018 \text{ V } \nu \text{s. SHE}$$
 (4)

$$K_{eq} \text{ of } 2NH_3(l) \leftrightarrow [NH_4^+][NH_2^-] = 10^{-33} (223 \text{ K})$$
 (5)

Because most of the electrochemical reactions studied to date are defined in aqueous media, calculating the theoretical potentials of the N2 (nitrogen evolution reaction: NER) and H2 (hydrogen evolution reaction: HER) evolution reactions for the direct electrolysis of NH3(l) is necessary. When the partial **EES Catalysis**

pressures of H2 and N2 are considered, the theoretical potentials for the NER and HER in the batch system are calculated as 0.041 and -0.018 V (eqn (3), (4) and Note S1-S3, ESI†), respectively, yielding an overall cell potential of 0.059 V. To screen potential catalysts for the electrolysis of NH₃(l), we initially design a semi-batch reactor using NH₄Br (1 M) as a supporting electrolyte (Fig. S1, ESI†) in NH₃(l) media. In this system, ammonium ions (NH₄⁺) serves as a charge carrier and acts as a conjugated acid due to the autoionization property of NH₃(l) into NH₄⁺ and amide ions (NH₂⁻) (eqn (5)), similar to water $(2H_2O \rightarrow H_3O^+ + OH^-)$. Standard electrodes are fabricated using various commercial metal species (Pt, Ru, Pd, Ni, Fe and Co) on carbon. High-angle annular dark-field scanning transmission electron microscopy (HAADF-STEM) analyses indicate that the uniformly distributed Pt, Ru and Pd nanoparticles have average sizes of 2.1, 2.8 and 3.7 nm, respectively, while Ni, Fe and Co metals exist as aggregated forms with sizes of > 6 nm (Fig. S2, ESI \dagger).

$$NH_3 \rightarrow NH_2^* + H^* \tag{6}$$

$$N^* + N^* \rightarrow N_2 + 2^*$$
 (7)

The catalytic activities of the prepared electrodes are then determined based on overpotentials (η) and Tafel slopes obtained from linear sweep voltammograms (LSVs). The electrolysis conditions of 6.2 bar and 10 °C are selected to maintain the liquid state of NH3 during the reaction. For the NER, among the screened metals, the Ru electrode exhibits the highest activity with the lowest overpotential ($\eta = 489 \text{ mV}$ at 10 mA cm⁻², 829 mV at 50 mA cm⁻², 1113 mV at 100 mA cm⁻², with *iR*-compensation) (Fig. 2A and Fig. S3A, ESI†). The overpotential at 10 mA cm⁻² in NH₃(l) electrolysis is higher compared to that observed in water electrolysis using Ru/C (<400 mV at 10 mA cm⁻²).^{26,27} In addition, the high Tafel slope of Ru/C (381 mV dec⁻¹, Fig. S3B, ESI†) further indicates the sluggish kinetics of the NER. Note that the Ru catalyst in the NER electrode undergoes gradual deactivation over time due to nitriding and metal dissolution (Fig. S4 and Table S1, ESI†), consistent with a previous report.²⁸ Nonetheless, the relatively high activity of Ru/C could likely be associated with the capability of Ru metal to promote both N-H bond scission (eqn (6)) and associative N₂ desorption (eqn (7)), as proposed by previous reports. 29,30 Consistently, Hansgen et al. reported that Ru metals facilitate the reaction steps of N-H scission and associative N2 desorption, which are the ratedetermining steps of NH₃ decomposition.³¹

Then, we further screen potential HER electrocatalysts, demonstrating that the activities toward $\rm H_2$ evolution increase in the following order: $\rm Pt/C > Ru/C > Pd/C > Fe/C > Ni/C > \rm Co/C$. However the overpotential of $\rm Pt/C$ for the HER is significantly larger (479 mV at 50 mA cm⁻²) than its theoretical potential ($\rm < 0.018~V$, Fig. 2B and Fig. S5A, ESI†). Given the low overpotential ($\rm < 100~mV$) typically observed in $\rm H_2O(l)$ electrolysis with a $\rm Pt/C$ cathode, $\rm ^{19}$ the high overpotential in $\rm NH_3(l)$ electrolysis is attributed to the limited $\rm H^+$ dissociation from $\rm NH_4^+ (NH_4^+ \rightarrow NH_3 + H^+)$ on the Pt surface. The released proton adatoms quickly generate $\rm H_2$, as evidenced by the low Tafel

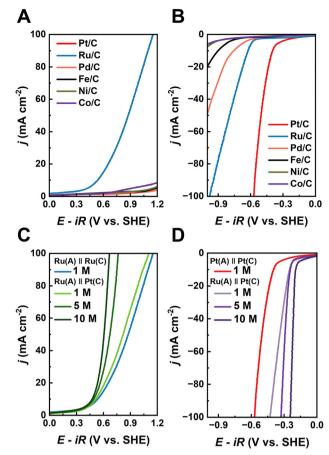


Fig. 2 Electrochemical characteristics of the as-prepared catalysts determined by linear sweep voltammetry (LSV) with a scan rate of 5 mV s⁻¹ under liquid anhydrous NH₃ (NH₃(I)) conditions at 10 °C and 6.2 bar. (A) and (B) LSVs of the nitrogen evolution reaction (NER) and hydrogen evolution reaction (HER), respectively, using an electrode configuration with identical metals (M||M, 2.5 μ mol cm⁻²) at both the anode and cathode in 1 M NH₄Br/NH₃(I) (see also Fig. S3 and S5, ESI†). (C) LSVs of the NER over Ru||Ru in 1 M NH₄Br and Ru||Pt configurations in 1 M, 5 M and 10 M NH₄Br (see also Fig. S6, ESI†).

slope (121 mV dec^{-1} , Fig. S5B, ESI†). Thus, incorporating metals (Ni, Co or Mo, etc.), known to promote H⁺ dissociation from NH₄⁺, into Pt metals could potentially reduce the HER overpotential.³¹ Based on the screened results, we perform additional electrochemical characterizations using a Ru (anode)||Pt (cathode) configuration with a 1 M NH₄Br electrolyte. Compared with the Ru||Ru configuration, the NER overpotential shifts to 775 mV at 50 mA cm⁻² (Fig. 2C and Fig. S6, ESI†). Likewise, the HER overpotential decreases to its theoretical value compared with that of the Pt||Pt configuration (Fig. 2D and Fig. S7, ESI†). The results are likely attributed to improved electrochemical properties of each component arising from a decrease in solution resistance (R_s) (Fig. S8, ESI†). To promote catalytic activity in the Ru||Pt configuration, additional NH₃(l) electrolysis is performed by increasing the concentration of the supporting electrolyte from 1 to 5 and 10 M. The electrochemical properties of the anode are slightly improved, reducing the

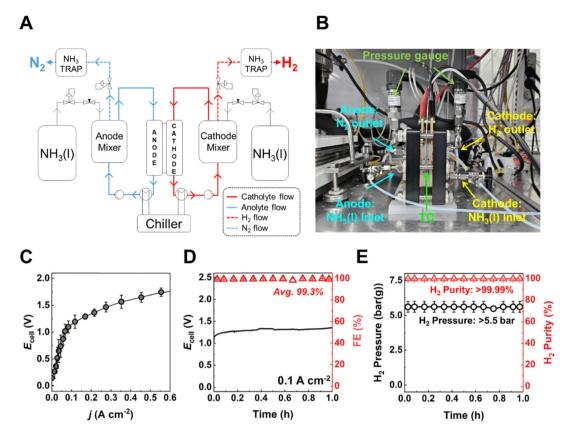


Fig. 3 Continuous production of high-purity, pressurized H_2 using the as-designed $NH_3(l)$ electrolyzer. (A) Process flow diagram (PFD) of the as-designed $NH_3(l)$ electrolysis system. (B) Digital photograph of the $NH_3(l)$ electrolyzer (see also Fig. S10, ESI†). (C) I-V polarization characteristics of the $NH_3(l)$ electrolyzer (anode: $2.5 \,\mu$ mol cm⁻² of Ru/C, cathode: $2.5 \,\mu$ mol cm⁻² of Pt/C) are determined with a scan rate of 5 mA s⁻¹ at a flow rate of 30 mL min⁻¹ and 10 °C, 6.2 bar conditions with 5 M NH_4 Br. (D) Potential response of chronopotentiometry measured at 0.1 A cm⁻² and Faradaic efficiency for H_2 production during electrolysis. (E) Purity and pressure of H_2 produced (see also Fig. S11, ESI†).

overpotential (η) at 50 mA cm⁻² from 775 mV at 1 M to 625 mV at 5 M and 561 mV at 10 M (Fig. S6A, ESI†). In addition, the rate of the NER is further improved, as evidenced by a lower Tafel slope (237 mV dec^{-1} at 10 M) (Fig. 2C and Fig. S6B, ESI†). The enhanced activity is also associated with the lowering of the charge transfer resistance (R_{ct}) as shown by the Nyquist plot obtained from electrochemical impedance spectroscopy (EIS) (Fig. S8A, ESI†): 5.1 Ω at 1 M, 2.5 Ω at 5 M and 2.1 Ω at 10 M. To determine whether the bromide anion (Br⁻) from the supporting electrolyte participated in the NH₃(l) electrolysis, we conducted an additional experiment using NH₄PF₆ as the supporting electrolyte, in which PF₆⁻ functions as an electrochemically inert anion. The resulting LSV profiles using NH₄PF₆ showed negligible differences compared to those obtained with NH₄Br (Fig. S9, ESI†). These results strongly suggest that the Br was inactive in the anodic process and did not contribute to the formation of byproducts such as Br_2 ($2Br^- \rightarrow Br_2 + 2e^-$). Conversely, Pt/C at the cathode exhibits a gentler Tafel slope (40 mV dec^{-1} at 10 M ν s. 90 mV dec⁻¹ at 1 M) with an overpotential of 202 mV at 50 mA cm⁻² in 10 M of electrolyte (Fig. 2D and Fig. S7, ESI†). These results indicate that the enhanced charge and mass transfers under the high concentration of NH₄Br only slightly influence H⁺ dissociation from NH₄⁺, which could likely be the ratedetermining step in the HER. Unlike the HER catalyst used in

H₂O(l) electrolysis, developing alternative cathode materials for the HER in NH₃(l) electrolysis is necessary.

To evaluate the practical feasibility of the NH₃(l) electrolysis concept for extracting high-purity H2, a continuous H2 production system with a 25 cm² zero-gap type electrolysis cell is constructed (Fig. 3A, B and Fig. S10, ESI†). The NH₃(l) electrolyzer comprises Ru/C as the anode and Pt/C as the cathode, with a cationic exchange membrane. In the continuous electrochemical cell, NH₃(l) is mixed with the NH₄Br electrolyte, and the resulting 5 M NH₄Br/NH₃(l) solution is supplied to both the anode and cathode at 10 °C and 6.2 bar. During the reaction, unreacted NH₃(l) is recirculated into the mixer, and the produced H_2 and N_2 gases, along with less than 1% residual $NH_3(g)$, are purified through an NH₃(g) trap (Fig. 3A). The I-V characteristic of the $NH_3(l)$ electrolysis system shows a cell potential (E_{cell}) of ca. 1.1 V at 0.1 A cm⁻² and ca. 1.6 V at 0.5 A cm⁻² (Fig. 3C). This suggests that H2 production is achievable at a lower potential than the cell potential of ca. 1.4 V at 0.1 A cm⁻² for H₂O(l) electrolysis. 32,33 Despite this advantage, the NH₃(l) electrolysis system still exhibits a much higher cell potential than its theoretical value (0.068 V). Based on the results from both batch and flow electrolysis (Fig. 2 and 3, respectively), the high cell voltage is primarily attributed to activation polarization, while ohmic polarization and concentration overpotential are

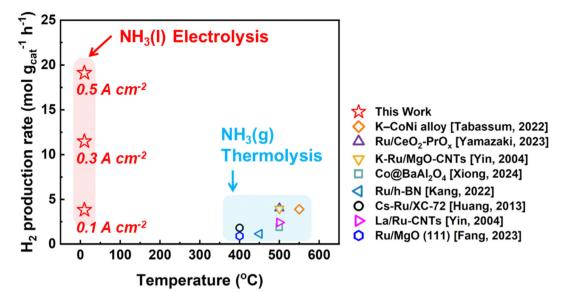


Fig. 4 Comparison of H_2 production rate (mol $g_{cat}^{-1} h^{-1}$) obtained by $NH_3(I)$ electrolysis and $NH_3(g)$ thermolysis. The unit mass of a catalyst for $NH_3(I)$ electrolysis is defined as the mass of the catalyst of the cathode (12.2 mg of Pt/C).

considered negligible. To further determine the efficiency of H_2 production, $NH_3(l)$ electrolysis is conducted at a constant current density of 0.1 A cm⁻² for 1 h. The cell voltage remains below 1.3 V while maintaining a high Faradaic efficiency (FE) of 99.3% (Fig. 3D and Note S4, ESI†). Since only N_2 is detected at the anode and only H_2 at the cathode, it confirms the complete separation of hydrogen from N_2 and NH_3 , with the H_2 purity exceeding 99.99% (Fig. 3E and Fig. S11, ESI†). The high-purity, pressurized H_2 (>5.5 bar) can be directly connected to a fuel cell without the need for additional pressure-boosting facilities.³⁴ Compared to previously reported batch type systems, the present $NH_3(l)$ electrolysis system, designed in a zero-gap configuration, enables continuous production of high purity H_2 and demonstrates significantly enhanced activity for H_2 generation (Table S2, ESI†).

Finally, the rates of $\rm H_2$ production via $\rm NH_3(l)$ electrolysis as a function of current density (j) are compared with those of reported thermal $\rm NH_3(g)$ decomposition systems (Fig. 4). $^{6,35-41}$ The as-designed $\rm NH_3(l)$ electrolysis system produces highpurity and pressurized $\rm H_2$ continuously at 10 °C at a rate of 3.8 mol- $\rm H_2$ $\rm g_{cat}^{-1}$ h⁻¹ with a current density (j) of 0.1 A cm⁻², which is comparable to that of state-of-the-art $\rm NH_3(g)$ thermolysis (4.0 mol- $\rm H_2$ $\rm g_{cat}^{-1}$ h⁻¹) at 500 °C and 1 bar. 35 When the operating current density is increased to 0.5 A cm⁻², an FE of 98.8% is achieved and the rate of $\rm H_2$ release further increases to 18.8 mol- $\rm H_2$ $\rm g_{cat}^{-1}$ h⁻¹, which is 4.7-fold higher than that of the aforementioned $\rm NH_3(g)$ thermolysis (4.0 mol- $\rm H_2$ $\rm g_{cat}^{-1}$ h⁻¹). 35 Additionally, > 98% of the initial $\rm NH_4Br$ electrolyte is recovered after two cycles (195.9 g \rightarrow 192.0 g) and reused with negligible activity loss (Fig. S12, ESI†).

Conclusion

In this proof-of-concept study, to the best of our knowledge, we first demonstrate continuous H_2 production via direct electrolysis

of anhydrous NH₃(l) at 10 °C under 6.2 bar without a high-cost separation process. Potential catalysts for NH₃(l) electrolysis are initially screened, with Ru/C (anode) and Pt/C (cathode) showing better activities than other metal catalysts. Based on the results, a continuous NH₃(l) electrolysis system equipped with a 25 cm² zero-gap cell and a cationic exchange membrane is designed. This system demonstrates high-purity and pressurized, continuous H2 production at a rate of 18.8 mol-H₂ g_{cat}⁻¹ h⁻¹, achieving an FE of >98.8% at 0.5 A cm⁻². This electrochemical cell has the potential to replace the thermochemical NH3(g) decomposition systems currently under development, which require multiple separation processes (e.g., temperature swing adsorption, pressure swing adsorption) and pressurizing components; moreover, the developed system holds significant promises for various commercial applications, particularly as an initial solution for small-scale and decentralized H₂ production facilities utilizing NH₃ (Table S3, ESI†). Despite these advantages, the obtained cell potential is higher than the theoretical value of 0.068 V. To lower the cell voltage, reducing the cathodic overpotential, enhancing the anodic N₂ evolution rate, stability of the electrocatalysts, developing cationic and/or anionic membranes for NH3(l) electrolysis and improving system durability are essential.

Experimental section

Materials

Commercial active metal species (20% Pt, Ru, Pd, Fe, Co and Ni on Vulcan XC-72 conductive carbon black) were purchased from Premetek (Cherry Hill, NJ, US). Nafion solution (5 wt%, DS520) was obtained from Dupont (Wilmington, Delaware, US). Carbon paper (GDS210) for the batch experiment and carbon foam with a gas diffusion layer (EQ-bcgdl-1400S-LD) for the cell test were purchased from CeTech (Taichung, Taiwan) and MTI Korea (Seoul, South Korea), respectively. The cation exchange

membrane was purchased from Solvay (Aquivion E98-09S Brussels, Belgium), and its properties are listed as follows: thickness, 90 μm; tensile stress (MD: Break), 40 MPa; tensile stress (TD: Break), 30 MPa. Isopropanol (anhydrous, 99.5%) and NH₄Br (ACS reagent, \geq 99.0%) were purchased from Sigma-Aldrich (St. Louis, MO, US) and used without further purification. Deionized water (DI·H₂O) was purified to a resistance of over 18 MΩ cm⁻¹ using a water purification system (Pure ROUP 30, Purewater, Gyeong-gi, South Korea). NH₃(I) was supplied

from a siphon tank at a purity of >99.99% (free of water and

Electrode fabrication

solvent).

Communication

To screen the activities of different metals for the NER and HER, the commercial metals (M = Pt, Ru, Pd, Fe, Co and Ni) on carbon (C, Vulcan XC-72) are loaded on the carbon paper by the slurry coating method. In a typical batch experiment, an active metal amount is set to 2.5 μmol cm⁻². First, a metal precursor is initially dissolved in 530 µL of the mixture of isopropanol (IPA) and DI H₂O (1:1, vol%), and 100 μL of Nafion solution is added to the IPA/H₂O solution as a binder, making a total 630 µL. This precursor solution is then sonicated for 1 h to produce a well-dispersed solution, referred to as an 'ink'. Next, 31.5 µL of the ink is dropped onto 1 cm² of carbon paper to fabricate the electrode for screening the activities. Then, the prepared electrodes are dried in a vacuum for 30 min at 25 °C. For full-cell operation, the metal loadings for the NER and HER electrodes are also maintained at 2.5 µmol cm⁻² (the total weight of Ru/C, 6.3 mg) for the anode and 2.5 μmol cm⁻² (the total weight of Pt/C, 12.2 mg) for the cathode, respectively. The ink solution containing the mixture of IPA and DI H₂O (1:1, vol%, 2.12 mL) and 5 wt% Nafion solution (400 μL) is prepared. Next, 78.8 µL of the ink is dropped onto 25 cm² of carbon foam and then dried in a vacuum for 30 min at 25 $^{\circ}$ C.

Electrochemical measurements in the batch reactor

Electrochemical analyses for active metal screening are conducted using a high-pressure three-electrode batch reactor at 10 °C and 6.2 bar (specific cell configuration in Fig. S1, ESI†) with the addition of the supporting electrolyte (NH₄Br, 0-10 M). The Ag/AgCl (3.4 M KCl, Innovative Instruments, Inc., Tampa, FL, US) reference electrode, covered with polyetheretherketone (PEEK), along with the working and counter electrodes, is connected to a potentiostat (VSP with 4A booster; Bio-Logic Science Instruments, Seyssinet-Pariset, France) for electrochemical measurements. Prior to an experiment, the reactor is purged with Ar for 1 h to remove residual air. NH₃(l) is then supplied from a siphon-type container to the reactor, and a liquid regulator is used to maintain the reaction pressure at 6.2 bar. The applied potential is recalculated based on experimental conditions, with further details provided in Notes S1-S3 (ESI†). Analyses with linear sweep voltammetry (LSV) are performed at a scan rate of 5 mV s⁻¹, with the scan direction selected properly for each half-reaction: an oxidative sweep for the anodic reaction (NER) and a reductive sweep for the cathodic reaction (HER). Before conducting an experiment,

85% iR compensation was applied using the value of solution resistance ($R_{\rm s}$) estimated from electrochemical impedance spectroscopy (EIS). To ensure an improved evaluation of intrinsic kinetics, the remaining 15% of uncompensated resistance was additionally corrected. The Nyquist plot from the EIS is obtained from 100 kHz to 100 MHz at +1.0 V_{SHE} for the anode and -1.2 V_{SHE} for the cathode. Tafel plots are calculated along the linear portion of the LSV.

Electrochemical measurements in the full-cell

Before an experiment, the NH₃(l) electrolyzer is purged with Ar for 1 h to remove residual air. In a typical electrolysis experiment, NH₃(l) and the supporting electrolyte (5 M NH₄Br) are initially homogenized using a magnetic stirrer in the anode and cathode mixers (200 mL) (refer to Fig. 3A). The resulting solutions are then supplied into the anode and cathode at a flow rate of 30 mL min⁻¹, followed by continuous circulation for 3 h to stabilize the cell. This procedure allows both the anode, cathode and membrane to be fully wet by NH₃(l). Note that the Aquivion membrane, which features perfluorosulfonic acid (PFSA) functionality, is reported to exhibit NH₄⁺ conductivity of ca. 30 mS cm⁻¹, ⁴² making it suitable for the purpose of this study. 43-47 The 25 cm² zero-gap type electrolyzer is operated at 10 °C and 6.2 bar using a DC power supply XG 20-76 (20 V, 76 A, Ametek, Berwyn, PA, US) with the current sweep (scan rate: 5 mA s⁻¹) and constant current methods. After the NH₃(l) splitting reaction, unreacted NH₃(l) is pumped back to each mixer for reuse. Finally, the obtained H2 and N2 gases are analyzed using a mass flow meter (F-201C; Bronkhorst, Ruurlo, Netherlands) and gas chromatography (YL6500; Young-In Chromass, Gyeong-gi, South Korea). Specific cell configuration and process flow diagrams are shown in Fig. 3A and Fig. S10 (ESI†).

Author contributions

Conceptualization, S. H., C. H. L. and C. W. Y.; methodology, S. H., J. S. H., H. L., C. H. L. and C. W. Y.; investigation, S. H. and H. L.; writing – original draft, S. H. and C. W. Y.; validation, J. S. H., J. S. L., C. H. L. and K. C. and C. W. Y.; writing – review and editing, S. H., J. S. H., J. S. L., H. L., C. H. L., K. C. and C. W. Y.; project administration, C. H. L., K. C. and C. W. Y.; funding acquisition, C. W. Y.; supervision, C. W. Y.

Data availability

The data supporting this article have been included as part of the ESI.†

Conflicts of interest

The authors declare no competing financial interest.

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