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# Integrated CO<sub>2</sub> capture and electrochemical conversion: coupled effects of transport, kinetics and thermodynamics in the direct reduction of captured-CO<sub>2</sub> adducts†

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Upgrading anthropogenic CO<sub>2</sub> from concentrated point sources or directly from the atmosphere is a valuable approach in closing the carbon cycle. Existing processes capture the CO<sub>2</sub>, concentrate it into pure gas streams, transport it, and then convert it into fuels and chemicals in a separate process plant. This sequential approach results in higher energy and operating costs which can be reduced by integrating the capture and conversion steps to directly reduce the captured CO<sub>2</sub>-bound adduct to value-added products. The direct reduction of the captured CO<sub>2</sub>-bound adduct is called the captured-CO<sub>2</sub> reduction reaction (c-CO<sub>2</sub>RR). Understanding of c-CO<sub>2</sub>RR has been obscured by the higher intrinsic complexity of the system. The CO<sub>2</sub> capture media is a complex space of several buffer reactions that allow the co-existence of different carbon species in solution depending on CO<sub>2</sub> loading, temperature, pressure, and pH. In order to design improved capture agents and catalysts for integrated CO<sub>2</sub> capture and conversion, it is essential to identify the carbon source and the primary factors influencing product formation on a c-CO<sub>2</sub>RR catalyst. This review delineates the strategies to determine the active carbon species for integrated CO<sub>2</sub> capture and conversion systems. Furthermore, it summarizes the fundamental applications of mass transport, thermodynamics, and kinetics across various c-CO<sub>2</sub>RR scenarios.

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## Broader context

Existing processes for CO<sub>2</sub> capture and conversion start by separating the CO<sub>2</sub> from the effluent of a point source or the atmosphere, and then this concentrated CO<sub>2</sub> stream is used as the feedstock for a catalytic conversion step in a separate unit. The CO<sub>2</sub> capture step involves multiple thermal and pressure cycles that result in energy losses and increased operating costs. Recently, a one-step process called reactive capture of CO<sub>2</sub> has been proposed in which CO<sub>2</sub> in its captured form (c-CO<sub>2</sub>) is directly transformed into value-added products while circumventing the CO<sub>2</sub> release step. The research on the electrochemical c-CO<sub>2</sub> reduction reaction (c-CO<sub>2</sub>RR) is just starting, but it is already evident that the complexity of the system pushes the limits of what is known in science and engineering. Understanding individual phenomena of CO<sub>2</sub> capture and CO<sub>2</sub> conversion is not enough. When capture and conversion are integrated, new phenomena emerge that are unique to the performance of the capture step in the presence of a catalyst, and to the performance of catalysis in the presence of the capture agent. Thus, it is of critical urgency that all researchers entering this field learn the fundamentals of transport, thermodynamics, and kinetics that link CO<sub>2</sub> capture and conversion. This review covers the latest developments in c-CO<sub>2</sub>RR research and our viewpoint on the challenges and future opportunities that exist in this space as the field matures.

## 1 Introduction

CO<sub>2</sub> contributes to almost 79% of total greenhouse gas emissions and is considered the major cause of global warming.<sup>1</sup> The development of technologies that contribute to the

reduction of CO<sub>2</sub> emissions and its direct capture from the atmosphere is more urgent than ever before. Global emissions of CO<sub>2</sub> are estimated to be approximately 35 billion tons per year, with approximately 2 billion tons per year attributed to the chemical industry.<sup>2,3</sup> Despite the increasing adoption of electrification for heating in various chemical manufacturing processes, burning of fossil fuels for heating is just a fraction of the CO<sub>2</sub> emissions and there remains a pressing need to source carbon atoms for chemicals from sources different from fossil fuels. As the demand for chemicals continues to grow,

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technologies that can upgrade the anthropogenic CO<sub>2</sub> from concentrated point sources and the atmosphere are needed to close the carbon cycle. Although the use of renewable electricity to capture and convert CO<sub>2</sub> into value-added chemicals offers a pathway to decarbonization, significant challenges persist in terms of energy intensity and cost compared to conventional methods. Overcoming these hurdles is crucial to making these processes industrially viable.<sup>4</sup>

Existing processes capture CO<sub>2</sub>, concentrate it in pure gas streams, compress CO<sub>2</sub>, and then convert it into fuels and chemicals, all in separate reaction units (top panel in Fig. 1). This sequential multistep approach results in higher energy and operating cost, arising from the inefficiency of the CO<sub>2</sub> release and capture media regeneration step before CO<sub>2</sub> compression. CO<sub>2</sub> release from direct air capture (DAC) processes have an estimated energy cost between 3400 and 8810 kJ per kg CO<sub>2</sub> for solid and liquid sorbent, while the CO<sub>2</sub> compression step along with the transport of gas requires an energy of 324–432 kJ per kg of CO<sub>2</sub>.<sup>5–10</sup> Recently, a one-step route has been proposed where CO<sub>2</sub> capture and conversion are integrated into one process that circumvents the inefficient CO<sub>2</sub> release step, by directly reducing the captured CO<sub>2</sub>-bound adduct to value-added chemicals (bottom panel in Fig. 1). The elimination of the inefficient temperature and pressure swing cycles during CO<sub>2</sub> capture and conversion can potentially reduce 50% of the total energy cost. The gains, however, must occur on both processes: (1) the CO<sub>2</sub> capture, and (2) the electrochemical captured-CO<sub>2</sub> reduction reaction (c-CO<sub>2</sub>RR) steps. This requires that the yield and energy efficiency of the c-CO<sub>2</sub>RR electrolyzer is comparable to current state of the art CO<sub>2</sub> electrolyzers.<sup>11</sup> In principle, integrated CO<sub>2</sub> capture and conversion has the potential to be more efficient and less expensive than the conventional approach relying on CO<sub>2</sub> electrolyzer technologies for the CO<sub>2</sub> reduction reaction (CO<sub>2</sub>RR). However, a long road

remains ahead to bring c-CO<sub>2</sub>RR electrolyzer technologies in par with today's CO<sub>2</sub>RR electrolyzers.

CO<sub>2</sub> capture technologies are much more mature than the reduction step in c-CO<sub>2</sub>RR. Many studies have been conducted on solvent-based capture technologies with amines or carbates. However, preliminary work suggest that amines might not be appropriate for c-CO<sub>2</sub>RR due to their strong interactions with the catalyst surfaces and the enhanced hydrogen evolution reaction.<sup>12</sup> Alternative capture agents like phenoxides,<sup>13</sup> alkoxides,<sup>12</sup> and amino acids<sup>14</sup> could indeed result in renewed interest in the development of capture agents specifically designed for integration with c-CO<sub>2</sub>RR, beyond those being commercialized today. Further optimization of the capture step is guaranteed once we find promising catalysts for c-CO<sub>2</sub>RR and as we start to extract capture agent design rules for integrated carbon capture and conversion.

Integrated CO<sub>2</sub> capture and conversion systems are complex, with several carbon species co-existing in the reactors. Identifying the source of carbon while quantifying products, and elucidating the key factors that affect the activity and selectivity of a catalyst, is important. Although c-CO<sub>2</sub>RR has been studied in the context of electrochemical,<sup>15–19</sup> thermal<sup>20–23</sup> and biological systems,<sup>24–27</sup> this review focuses solely on the electrochemical route. In recent years, researchers have reported evidence of electrochemically reducing the captured CO<sub>2</sub>-bound adduct to products.<sup>28</sup> However, significant challenges still remain in understanding the transformation of the captured CO<sub>2</sub>-bound adduct. In the electrolyte solution the vapor-liquid equilibrium, ion-speciation, and reaction equilibria dynamically varies as a function of the temperature, pressure, and pH. These factors are further governed by the fundamental principles of mass transport, thermodynamics, and kinetics, which when not carefully investigated can convolute the way we interpret the data collected from c-CO<sub>2</sub>RR.



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*conversion, with an emphasis on understanding the roles of transport, thermodynamics and kinetic phenomena in these processes.*

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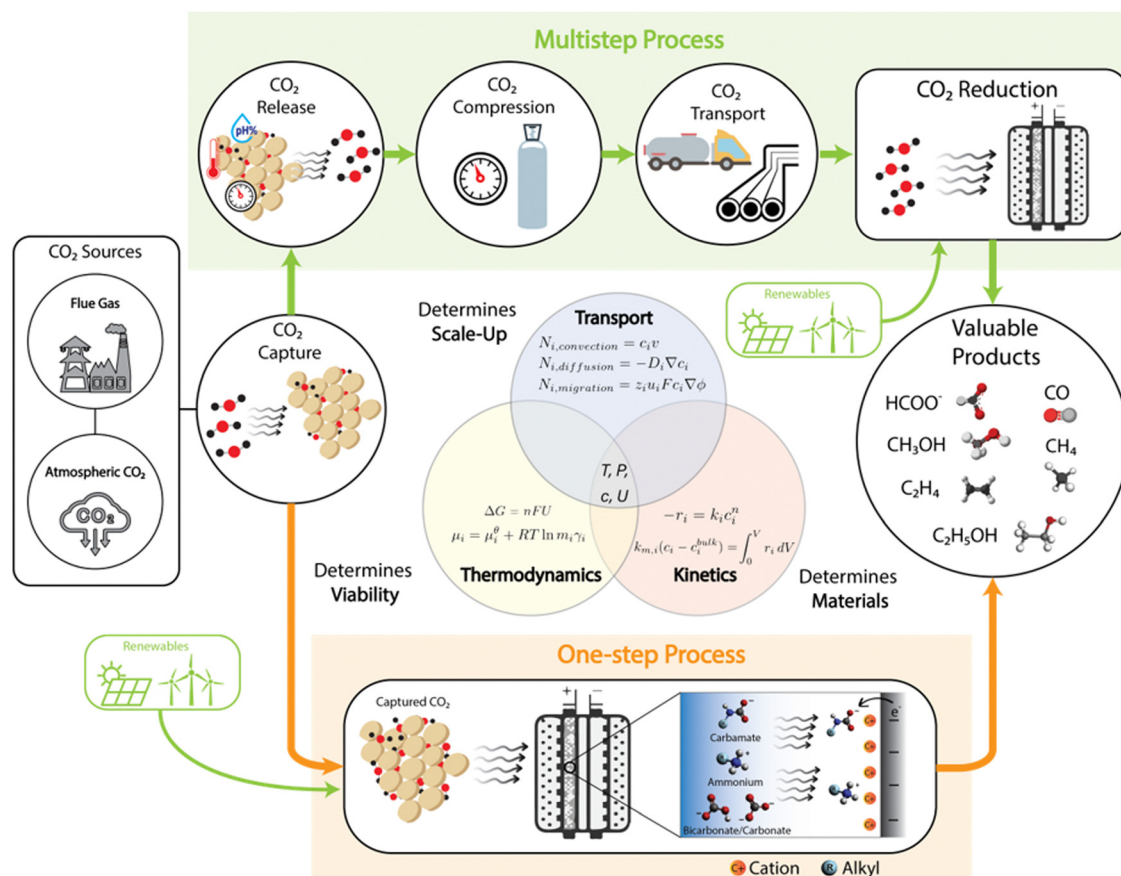


**Carlos G. Morales-Guio**

*focuses on understanding the fundamentals of mass, charge and heat transport at the electrode/electrolyte interface, reactor design, process intensification and process automation to guide the development of sustainable energy applications.*

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**Fig. 1** Illustration showing the conventional CO<sub>2</sub>RR pathway (shown by the green path) and the c-CO<sub>2</sub>RR pathway (shown by the orange path). The CO<sub>2</sub>RR pathway is a multistep process comprising additional energy costs from the CO<sub>2</sub> release, compression, and transport steps before the CO<sub>2</sub> reduction reaction can take place, whereas the integrated c-CO<sub>2</sub>RR is a one-step process that could potentially reduce energy and operating costs. Furthermore, both the pathways are interrelated to the fundamental principles of thermodynamics, transport, and kinetics which influences the product formation.

In the field of electrocatalysis, there is a consensus within the scientific community regarding the importance of transport, thermodynamics, and kinetics; however their full integration into scientific studies remain somewhat limited. Thermodynamics determines the feasibility of a process by delineating the minimum energy requirements and equilibrium conditions. It also links variations in local concentration, temperature, pressure, and electric field of an electrochemical system to changes in the electrochemical potential. Thermodynamics further determine the direction of mass and energy fluxes in and out of a control volume, which is linked to spacial and temporal differences in local concentration, temperature, and pressure. Transport properties determine the scalability of a process by giving insights into technically feasible energy and mass fluxes, which in turn will be linked to reactions in multidimensional space and time coordinates. Transport phenomena are used to describe processes of diffusion, convection, and migration of species in electrochemical cells. Different reactors have different hydrodynamics, resulting in different transport properties. By and large, the electrocatalysis community has failed to recognize that we measure experimentally reactor kinetics and not

reaction kinetics, slowing the progress of the field. Thus, understanding of mass, heat, and charge transport is necessary to decouple reaction kinetics from reactor kinetics, and this is also true for c-CO<sub>2</sub>RR systems. Thermodynamics, transport, and kinetics cannot be disentangled because of their interdependence. In order to overcome the challenges of successfully scaling-up electrochemical systems, it is necessary to measure, model and control the coupling of thermodynamics, transport, and kinetics even when studying the most basic electrochemical system at a bench scale (Fig. 1).

Most reviews and perspectives focuses on the different amine capture agents and discusses scalability challenges that could arise from c-CO<sub>2</sub>RR, while comparing the value proposition of c-CO<sub>2</sub>RR with traditional CO<sub>2</sub>RR.<sup>11,29–34</sup> In contrast, our review is meant to serve as an introduction to the field of c-CO<sub>2</sub>RR for chemists, material scientists, and engineers who although might have learned the various concepts of transport, thermodynamics, and kinetics separately, have not seen how these three concepts come together at different length and time scales in c-CO<sub>2</sub>RR. This review will further aim to lay out some guidelines on the processes and factors that influence product selectivity and that should be considered while studying and



reporting data for c-CO<sub>2</sub>RR systems. It also includes the latest breakthrough results and the wider implications for the scientific community, and provides the tools necessary for understanding the fundamentals of electrochemical c-CO<sub>2</sub>RR.

## 2 Understanding vapor–liquid equilibrium and ion speciation under c-CO<sub>2</sub>RR conditions

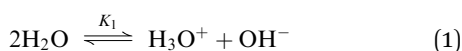
The different species present in a solution filled with a CO<sub>2</sub>-bound capture agent can be probed by understanding the vapor–liquid equilibrium of the system. When a capture agent is dissolved in a solution, and then it is put in contact with a gas phase containing CO<sub>2</sub>, free and dissolved CO<sub>2</sub> will always be present in solution due to the equilibrium reactions between the gas and liquid phases. The amount of dissolved CO<sub>2</sub> is furthermore a function of CO<sub>2</sub> loading, pH, temperature and pressure of the system. Industrially, amines are currently the leading CO<sub>2</sub> sorbents, and an entire field of science and engineering has been developed around the optimization of CO<sub>2</sub> absorption capacities of different amines.<sup>35–39</sup> This section dives deeper into CO<sub>2</sub> capture with amines used primarily in post-combustion processes along with insights into other groups of capture agents, including hydroxyls used for direct air capture (DAC),<sup>40–44</sup> and the untapped group of alkoxides and phenoxides that is recently gaining interest.<sup>13,45</sup>

### 2.1 Chemical reaction processes

The CO<sub>2</sub> absorption process into different capture solutions is governed by different equilibrium reactions, allowing different species to coexist in the system.

For amine capture solutions, it is known that the species present are RNH<sub>2</sub>, RNH<sub>3</sub><sup>+</sup>, RNHCOO<sup>−</sup>, H<sub>3</sub>O<sup>+</sup>, OH<sup>−</sup>, HCO<sub>3</sub><sup>−</sup>, CO<sub>3</sub><sup>2−</sup>, CO<sub>2</sub>, and H<sub>2</sub>O. R represents an alkyl/alkanol group and can belong to a primary, secondary or tertiary family of amines. Primary and secondary amines have a higher basicity than water, and thus CO<sub>2</sub> being the Lewis acid attacks the amine to undergo a zwitterion mechanism to form carbamates. Initially, two amines are consumed for each CO<sub>2</sub> molecule absorbed, generating an ammonium carbamate. However, if the CO<sub>2</sub> loading is increased and the amine is almost depleted, then the ammonium carbamate decomposition reaction starts occurring to form ammonium bicarbonate and carbonate species.<sup>46</sup> Similarly in the presence of more sterically hindered amines, like tertiary amines, water comparatively becomes a stronger Lewis base and can directly assist in the formation of ammonium bicarbonate with the amines.<sup>47</sup> The following chemical reactions describe the formation of different species.<sup>37,38</sup>

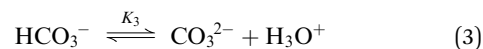
Water ionization:



CO<sub>2</sub> reaction with water:



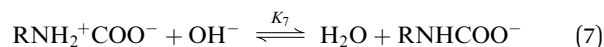
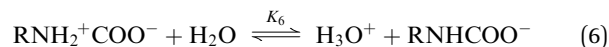
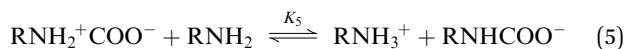
dissociation of bicarbonate ion:



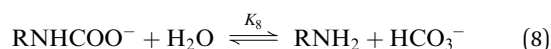
zwitterion formation from RNH<sub>2</sub> and CO<sub>2</sub> reaction:



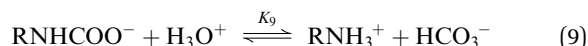
carbamate formation by deprotonation of zwitterion:



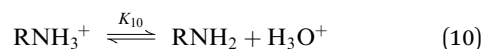
carbamate hydrolysis:



carbamate consumption:



de-protonation of amine:



bicarbonate formation:



The equilibrium constants of these reaction,  $K_1$ – $K_{11}$ , can subsequently be used to understand the speciation as a function of pH, temperature and CO<sub>2</sub> loading. In the case of primary and secondary amines, carbamate is the main species formed when the CO<sub>2</sub> is bound to the amine, while tertiary amines follow a base-catalyzed hydration mechanism producing only bicarbonate ions and no carbamate, which would essentially mean that reactions (4)–(9) would not occur in the presence of tertiary amines.

Similarly, hydroxyls commonly used for DAC, form bicarbonate and carbonate species in the solution. The different species that are known to co-exist are H<sub>3</sub>O<sup>+</sup>, OH<sup>−</sup>, HCO<sub>3</sub><sup>−</sup>, CO<sub>3</sub><sup>2−</sup>, CO<sub>2</sub>, and H<sub>2</sub>O, *i.e.*, reactions (1)–(3), and (11) would only occur in such systems, and it reduces the number of buffer reactions compared to amine capture agents. In CO<sub>2</sub>RR, we are largely concerned only with the equilibrium reactions between CO<sub>2</sub> and bicarbonates. It should thus be evident for researchers working with CO<sub>2</sub>RR that c-CO<sub>2</sub>RR represents a step-up in complexity when amines and other capture agents are involved.

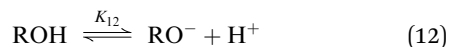
Other capture agents belonging to the alkoxide family have also been recently investigated for c-CO<sub>2</sub>RR. Kowalski *et al.*, recently investigated potassium methoxide as a CO<sub>2</sub> capture agent, and observed that the methoxide ions require alcohols (other non-aqueous medium) as the solvent medium to capture CO<sub>2</sub> and form methyl carbonate. In an aqueous medium, the OH<sup>−</sup> present in the reaction primarily behave as the capture





agent forming  $\text{HCO}_3^-$  and  $\text{CO}_3^{2-}$ , limiting the methylcarbonate production pathway. In the presence of alkoxide ions, similar reactions were described to understand the capture mechanism.<sup>13</sup>

Alcohol ionization:



$\text{CO}_2$  reaction with alkoxides:



In the alkali metal alkoxide systems, the speciation looks fairly simple with only species being the ROH,  $\text{RO}^-$ ,  $\text{ROCOO}^-$ ,  $\text{CO}_2$ , and  $\text{H}^+$  in addition to the alkali metal cation. The R could represent a primary, secondary, tertiary or an aromatic alcohol group.

The equilibrium equations shown here only describe the vapor–liquid equilibrium, while a full description of the system needs to add the solid components and all the reactions that lead to precipitation of species as well as dissolution of the solids in equilibrium. For simplicity, solid phases will be not discussed here but these need to be considered for any practical system.

## 2.2 $\text{CO}_2$ loading effect on speciation

The concentration distribution in the bulk of the solution is a function of the  $\text{CO}_2$  loading when the temperature and pressure is constant. From the different equilibrium constants of the reactions shown in Section 2.1, vapor–liquid equilibrium models have been developed to predict the  $\text{CO}_2$  absorption in different amines. Fig. 2 shows a typical chemical speciation distribution at different  $\text{CO}_2$  loadings in amines. The  $\text{CO}_2$  loading ( $\text{mol mol}^{-1}$ ) is defined as the ratio of mol of  $\text{CO}_2$  present (dissolved + captured) to the mol of capture agent present in the solution. The concentration of  $\text{CO}_3^{2-}$  does not vary significantly, especially for primary and secondary amines, when the  $\text{CO}_2$  loading is varied between 0–1  $\text{mol mol}^{-1}$ . At low  $\text{CO}_2$  loadings, it is typically observed that all the  $\text{CO}_2$  dissolved in

the solution gets converted to carbamate as denoted by reactions (5)–(7).  $\text{CO}_2$  loadings of 0.5  $\text{mol mol}^{-1}$  usually give the highest carbamate concentration, which could be also rationalized from the stoichiometry of the reaction where 2 amine molecules are required to capture 1  $\text{CO}_2$  molecule. Through the predicted equilibrium concentration of different species as a function of  $\text{CO}_2$  loading, it has been shown that the carbamate consumption, as denoted by reaction (8), and  $\text{CO}_2$  hydrolysis starts to simultaneously occur at around 0.3  $\text{mol mol}^{-1}$ . When a  $\text{CO}_2$  loading of 1  $\text{mol mol}^{-1}$  is reached the speciation is mostly dominated by bicarbonate and free  $\text{CO}_2$  present in the system, with little to no carbamate. Thus for electrochemical  $\text{c-CO}_2\text{RR}$ , it is necessary to probe the loading of the systems to understand the speciation and also it is beneficial to be at a loading  $< 0.5 \text{ mol mol}^{-1}$  if the intention is to reduce the carbamate species within the system. However in case of higher loadings, if small amounts of carbamate present near the active site of the catalyst is reduced, it is possible that the bicarbonate can equilibrate back to carbamate. The speed of this equilibration will vary and would depend on the  $\text{p}K_a$  and the equilibrium constants of the different amines. For comparison,  $\text{CO}_2$  loadings cycle typically between 0.3 and 0.7 during the thermal regeneration of amine capture solutions, where the low loadings belong to the  $\text{CO}_2$ -lean capture solution that is fed to the absorber unit and the high loading belong to the  $\text{CO}_2$ -rich amine streams that leave the bottom of the absorber.<sup>38,48</sup>

Although most studies just look at speciation considering all amines behave similarly, but there lies differences in how these vary between primary, secondary and tertiary amines. As can be seen from Fig. 2, the VLE models of a primary, secondary and tertiary amine shows that the equilibrium concentration of the different species are different as a function of loading when the sterics of the amines change. Also, even between the same group of amines, the speciation curves could be different, which mainly arises from the different equilibrium constants of carbamate consumption and amine deprotonation in aqueous systems,  $K_9$  and  $K_{10}$ . For instance, between monoethanolamine (MEA) and diethanolamine (DEA), at 0.5  $\text{mol mol}^{-1}$  of loading the carbamate concentration is slightly higher in MEA

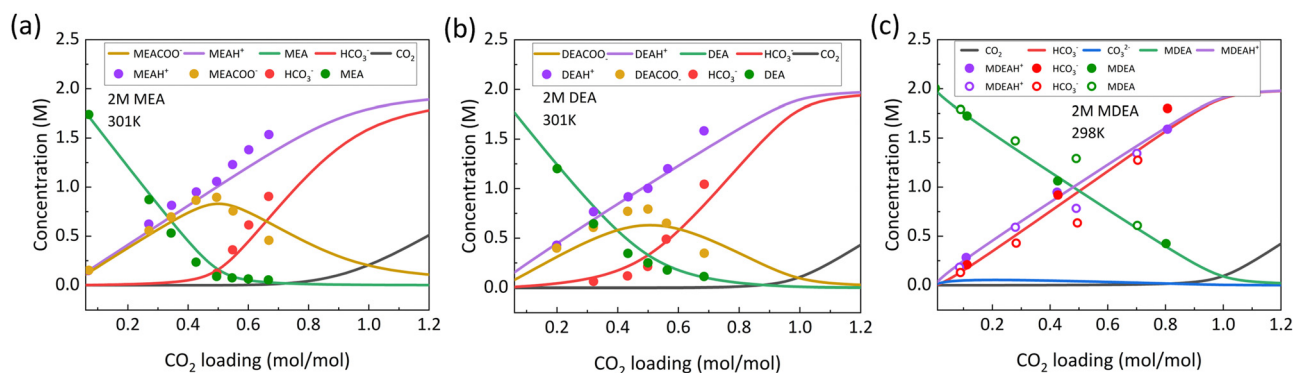
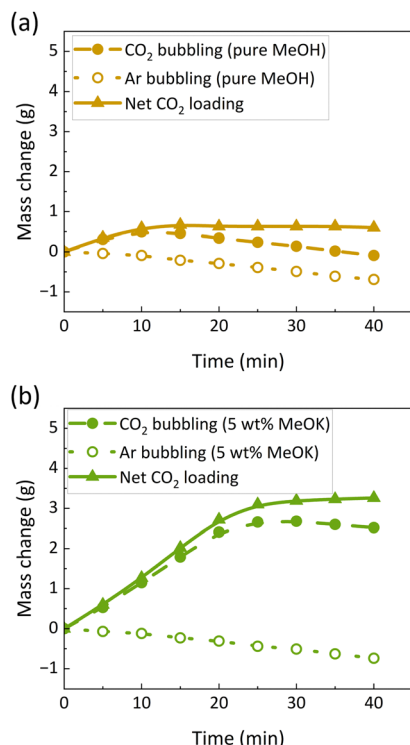


Fig. 2 VLE models showing equilibrium concentration of different species in liquid-phase as a function of loading in (a) 2 M MEA at 301 K which is a primary amine (lines represent model and dots represent experimental data points from Liu *et al.*)<sup>49</sup> (b) 2 M DEA at 301 K which is a secondary amine (lines represent model and dots represent experimental data points from Liu *et al.*)<sup>49</sup> (c) 2 M MDEA at 298 K which is a tertiary amine (lines represent model and dots and hollow dots represent experimental data points from Derks *et al.* and Jakobsen *et al.* respectively)<sup>50,51</sup> Reproduced with permission from ref. 48, copyright 2024 American Institute of Chemical Engineers.





**Fig. 3** Comparison of mass change from CO<sub>2</sub> loading in (a) mass change during CO<sub>2</sub> absorption in 100 mL of pure methanol. The net mass change is approx. 0.7 g of CO<sub>2</sub> after subtracting the CH<sub>3</sub>OH evaporation amount measured under the flow of Ar and the mass change observed during CO<sub>2</sub> flowing into the methanol solvent. (b) Mass change during capture of CO<sub>2</sub> in 100 mL of 5 wt% CH<sub>3</sub>OK in CH<sub>3</sub>OH. CO<sub>2</sub> forms CH<sub>3</sub>OCOO<sup>-</sup> when reacted with the methoxide ions and the mass change for this process is about 3.5 g. This measurement is also an experimental verification of the fact that the solubility of CO<sub>2</sub> is different in water and in methanol. The CO<sub>2</sub> loading, defined as the ratio of mol CO<sub>2</sub> captured and dissolved to the mol CH<sub>3</sub>OK present, was calculated to be 1.09 mol mol<sup>-1</sup> from (b).<sup>12</sup> Reproduced with permission from ref. 12, copyright 2024 American Chemical Society.

than in DEA (Fig. 2a and b). From the equilibrium constant values, it was determined that the carbamate consumption (reaction (9)) is slightly faster for DEA compared to MEA which is responsible for the difference. Also, at loading of 1 mol mol<sup>-1</sup> slightly lower concentrations of RNH<sub>3</sub><sup>+</sup> and HCO<sub>3</sub><sup>-</sup> was observed compared to MEA. The pK<sub>a</sub> of DEA is lower than MEA and so it acts as a weaker Lewis base leading to weak binding of CO<sub>2</sub> to the amine. This leads to faster deprotonation of DEA allowing the carbamate consumption reaction to accelerate (reaction (9)). For tertiary amines like methyldiethanolamine (MDEA), the dominant species that forms is bicarbonate and thus the CO<sub>2</sub> loading is equivalent to bicarbonate formation with small amounts of CO<sub>3</sub><sup>2-</sup>. This small amount of CO<sub>3</sub><sup>2-</sup> arises from the high pK<sub>a</sub> of MDEA that accelerates the deprotonation of the bicarbonate (Fig. 2c).

When hydroxyls are used as capture agents, the main species present in the system is HCO<sub>3</sub><sup>-</sup>, CO<sub>3</sub><sup>2-</sup> and dissolved CO<sub>2</sub>. It is understood that at the beginning of CO<sub>2</sub> loading the main reaction is the formation of HCO<sub>3</sub><sup>-</sup> with CO<sub>3</sub><sup>2-</sup> forming at low CO<sub>2</sub> loadings, when the pH of the solution is highly alkaline.<sup>45</sup>

Similarly alkoxide capture agents can be modeled to understand the speciation at different CO<sub>2</sub> loadings. Considering the stoichiometry of alkoxides, it requires 1 molecule of alkoxide to capture 1 molecule of CO<sub>2</sub>, which means the highest concentration of alkylcarbonate will form at CO<sub>2</sub> loading of 1 mol mol<sup>-1</sup>. Also, the bonding characteristics of CO<sub>2</sub> on alkoxides is similar to a deprotonated amino group. Recently, Kowalski *et al.* studied the loading of CO<sub>2</sub> in a methoxide capture agent in methanol solvent. Experimentally the mass change was measured while flowing pure CO<sub>2</sub> in 5 wt% methoxide and they observed that the change in mass was higher in the presence of methoxide in the methanol solvent compared to when no methoxide was present in the methanol. They further experimentally calculated the CO<sub>2</sub> loading to be 1.09 mol mol<sup>-1</sup> which is similar to the expected stoichiometric loading (Fig. 3).<sup>12</sup>

### 2.3 pH effects on chemical speciation

The pH of the solution affects the equilibrium species distribution in the capture solution. As CO<sub>2</sub> is an acidic gas, its capture is favored in more alkaline conditions. The concentration of the different species when plotted as a function of pH shows that at very low pH the species concentration is dominated by free CO<sub>2</sub> and HCO<sub>3</sub><sup>-</sup>, at intermediate pH the species concentration is dominated by the carbamate, and at very high pH the dominant species is the amine capture agent in its initial form. In MEA the highest carbamate concentration is achieved at a pH of 9.3 whereas for DEA it is at a pH of 8.85, which also corresponds closely to the pK<sub>a</sub> of these amines which are 9.45 and 8.88 at 298 K respectively.<sup>52</sup> The faster rates of carbamate consumption and CO<sub>2</sub> hydrolysis in DEA can also be realized from Fig. 4a and b, where it can be seen that the HCO<sub>3</sub><sup>-</sup> and free CO<sub>2</sub> shoots up slightly quicker at lower pH compared to MEA. The pH is also a function of the CO<sub>2</sub> loading, and typically it decreases as more CO<sub>2</sub> is captured within the system, giving rise to the different speciation at lower pH. Also, the partial pressure of CO<sub>2</sub> in equilibrium with the solution is higher at higher temperatures. This translates into a higher release rate at higher temperatures resulting in a more alkaline solution, indicating temperature as an important parameter in regulating the pH. Also, the partial pressure of CO<sub>2</sub> increases by several orders of magnitude at a low pH, which is attributed to the presence of a high concentration of free CO<sub>2</sub> in the bulk of the solution. Thus in general it can be concluded that for aqueous systems a more alkaline pH is favorable for CO<sub>2</sub> capture, while a more acidic pH favors the release of CO<sub>2</sub> from the CO<sub>2</sub> captured adduct. Consequently, pH-swing for release of CO<sub>2</sub> from the captured adduct is currently being explored as an alternative to temperature-swing or pressure-swing cycles.<sup>53–56</sup> Similar conclusions can be drawn for alkaline CO<sub>2</sub> capture systems where hydroxyls are used as the capture agent. In such systems, a low pH is accompanied by the formation of carbonic acid H<sub>2</sub>CO<sub>3</sub>, a neutral pH consists of HCO<sub>3</sub><sup>-</sup>, while a high pH forms CO<sub>3</sub><sup>2-</sup> in the system.<sup>57</sup>

Although the vapor–liquid equilibrium models can be leveraged to predict the speciation as a function of pH in the aqueous systems, for alkoxide/phenoxide capture agents, the solvent medium is primarily non-aqueous. Thus, it becomes



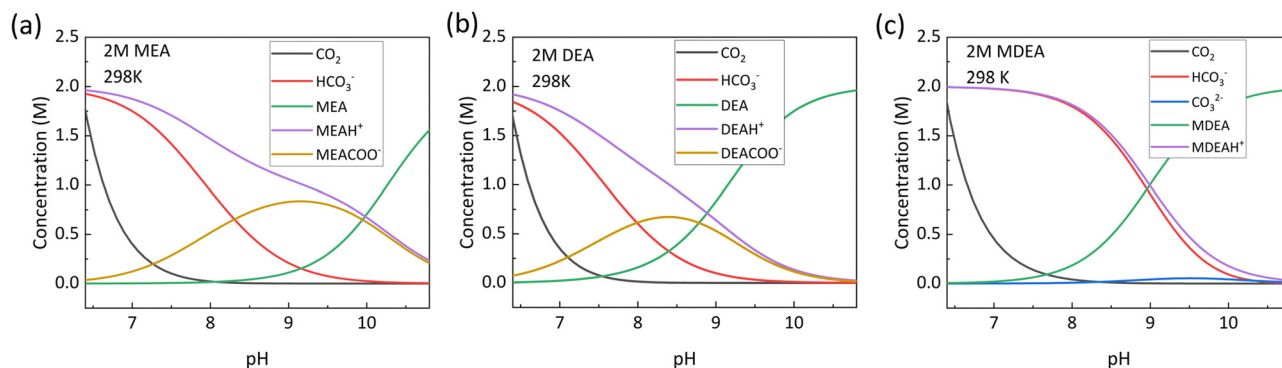


Fig. 4 Equilibrium speciation as a function of pH at 298 K for (a) 2 M MEA (primary amine), (b) 2 M DEA (secondary amine) and (c) 2 M MDEA (tertiary amine) obtained from VLE models. It can be seen that at a low pH, dissolved  $\text{CO}_2$  has a very high concentration along with high concentration of  $\text{HCO}_3^-$ . Reproduced with permission from ref. 48, copyright 2024 American Institute of Chemical Engineers.

difficult to define pH under such conditions and find equivalent speciation plots. However, Zhang *et al.* reported that the  $\text{CO}_2$  binding strength to different alkoxides followed a linear scaling relation (LSR), and more interestingly it lied on the same LSR as the amines, which suggests that the binding of  $\text{CO}_2$  is solely a function of the  $\text{pK}_a$  of the capture agents (Fig. 5). Furthermore, the findings of their investigation can be extended to conclude that the equilibrium constants which vary between different amines for developing the VLE models are mainly a characteristic of the changing  $\text{pK}_a$  of the amines.<sup>13</sup>

#### 2.4 Temperature effects on equilibrium concentrations

The equilibrium species concentration of capture solutions as a function of temperature can be probed to investigate its influence on c- $\text{CO}_2$ RR. The equilibrium constants of all the reactions stated in Section 2.1 are a function of the enthalpy ( $\Delta H$ ) and temperature ( $T$ ) by eqn (14).

$$\frac{\partial \ln K}{\partial T} = \frac{\Delta H}{RT^2} \quad (14)$$

For amine capture solutions, at low  $\text{CO}_2$  loading the  $\text{RNHCOO}^-$  concentration increases with temperature, and

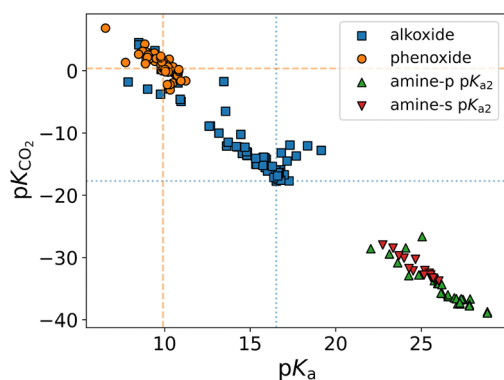


Fig. 5 DFT calculated values of  $\text{CO}_2$  binding constant ( $\text{pK}_{\text{CO}_2}$ ) as a function of  $\text{pK}_a$  for different amines and alkoxides. The orange dashed line and the blue dotted line represent the data points of phenoxide and methoxide, respectively.<sup>13</sup> Reproduced with permission from ref. 13, copyright 2022 National Academy of Sciences.

reaches a maximum value at  $0.5 \text{ mol mol}^{-1}$  loading. As the loading is increased more, it has been observed that the  $\text{RNHCOO}^-$  concentration declines. This decline accelerates at higher temperatures which could be explained by Le Chatelier's principle, where higher temperatures shift the equilibrium to the left, which in amine capture solutions shift the equilibrium for reactions (5)–(7) towards the formation of the zwitterionic intermediate to ultimately form dissolved  $\text{CO}_2$  and  $\text{RNH}_2$ , as shown in reaction (4). Furthermore, carbamate consumption reaction becomes more dominant at loadings  $> 0.5 \text{ mol mol}^{-1}$ , as  $K_9$  is negatively related to temperature denoting the process is exothermic. In addition, the temperature was shown to have an effect on the concentration of dissolved  $\text{CO}_2$ . As the loading increased, the concentration of dissolved  $\text{CO}_2$  was increased, and it increased further at higher temperatures. At higher loadings, it is rationalized that the amine capture agent is completely consumed and then the  $\text{CO}_2$  undergoes hydrolysis to form bicarbonates in the system. Also, as  $\text{CO}_2$  hydrolysis is an exothermic reaction, it facilitates the release of more  $\text{CO}_2$  at higher temperatures. Consequently, when the partial pressures of  $\text{CO}_2$  is compared to the  $\text{CO}_2$  loading with the use of the temperature dependent Henry's constant, it is observed that higher temperature results in a higher partial pressure of  $\text{CO}_2$ , implying lower solubility in the solution (Fig. 6). When comparing primary and secondary amines, DEA shows a lower partial pressure of  $\text{CO}_2$  compared to MEA, which again arises because of the faster carbamate consumption and  $\text{CO}_2$  hydrolysis in secondary amines. Also for MDEA which is a tertiary amine, the effect of temperature on partial pressure of  $\text{CO}_2$  had little effect compared to MEA and DEA (Fig. 6c).

For hydroxyl capture agents, the partial pressure of  $\text{CO}_2$  as a function of loading is only governed by  $\text{CO}_2$  hydrolysis and  $\text{HCO}_3^-$  formation, reactions (1)–(3). The partial pressures at similar conditions of pressure and temperature are usually higher for such systems implying more free dissolved  $\text{CO}_2$  present in the solution.

For alkoxide capture agents, the partial pressure of  $\text{CO}_2$  is one order of magnitude lower than amine/hydroxyl capture agents. This difference arises mainly because of the higher Henry's constant when using methanol as solvent and also a higher solubility of  $\text{CO}_2$  in methanol.



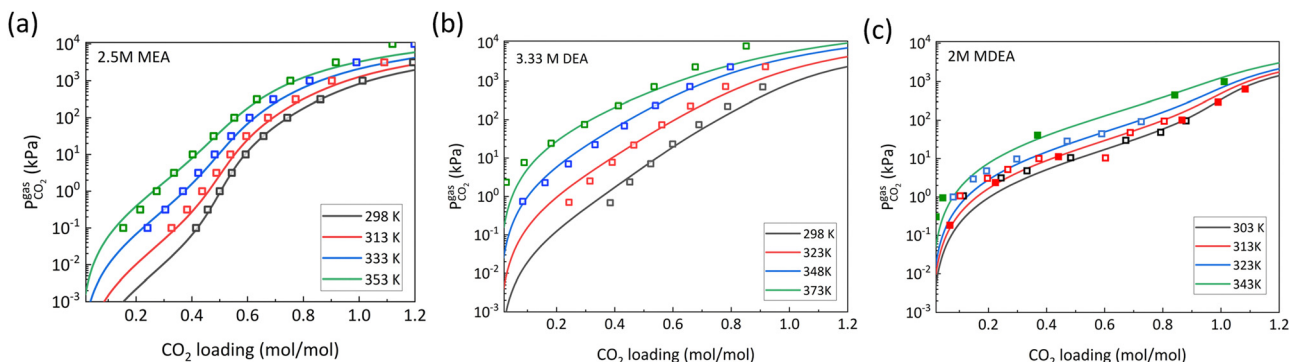


Fig. 6 Partial pressure of  $\text{CO}_2$  as a function of  $\text{CO}_2$  loading and temperature for (a) 2.5 M MEA (primary amine) where solid lines are predicted from VLE models and hollow dots are experimental data points from Lee *et al.*,<sup>58</sup> (b) 3.33 M DEA (secondary amine) where solid lines are predicted from VLE models and hollow dots are experimental data points from Bottinger *et al.*,<sup>59</sup> and (c) 2 M MDEA (tertiary amine) where solid lines are predicted from VLE models and hollow dots and solid dots are experimental data points from Sulaiman *et al.* and Jou *et al.*<sup>39,60</sup> Reproduced from with permission ref. 48, copyright 2024 American Institute of Chemical Engineers.

Temperature has a significant effect on the chemical speciation of the system and can be captured in the vapor-liquid equilibrium model used while studying c- $\text{CO}_2$ RR systems. At high temperature conditions, the  $\text{CO}_2$ -bound adduct can release free  $\text{CO}_2$  and regenerate the capture agent. This is known as temperature-swing capture agent regeneration. In conventional carbon capture and utilization processes, the capture step is followed by a high-temperature capture agent regeneration process while simultaneously releasing a concentrated stream of  $\text{CO}_2$  for further storage or upgrading. Similarly, in c- $\text{CO}_2$ RR, the captured  $\text{CO}_2$ -adduct will decompose at higher temperatures leading to low c- $\text{CO}_2$ RR performance, however, consequently higher temperatures will release more free  $\text{CO}_2$  in the system that can compete for the active sites of the catalyst for further reduction. Banerjee *et al.*, in their study showed that by increasing the temperature of the capture solution during electrolysis, they can achieve a higher partial current density of CO using silver catalyst. They concluded that this behavior is mainly due to the release of free  $\text{CO}_2$  in the system as they increase the temperature from 20 °C to 40 °C.<sup>48</sup> In such cases, at higher temperatures the performance of c- $\text{CO}_2$ RR can appear to be improved, but this is not to be confused with the direct reduction of the  $\text{CO}_2$ -bound adduct. Therefore, understanding the vapor-liquid equilibrium effects discussed throughout Section 2 will be important in identifying the active carbon species getting reduced as the field of c- $\text{CO}_2$ RR evolves.

### 3 Identifying the source of carbon in c- $\text{CO}_2$ RR

The VLE models can provide a clear understanding of the speciation and its variation with the pH, temperature and  $\text{CO}_2$  loading. Leverick *et al.* quantified the speciation of amines with different  $\text{pK}_a$  through NMR analysis to verify the speciation with the VLE-models and identify the source of carbon. There have been three main approaches that have been undertaken to identify the active carbon species which are by leveraging characterization techniques to correlate with the VLE-models

of different amines, continuum modeling, and correlating the two-film theory with reaction transport model. The last method provides a robust way for quick screening of different capture agents, especially if VLE models are not easily accessible. This section goes through each method in detail.

#### 3.1 Characterization techniques coupled with VLE-models

Recently, the most detailed study to identify the source of carbon in c- $\text{CO}_2$ RR systems with the VLE-models have been performed by Leverick *et al.* using amine capture agents. Using a H-cell reactor with an Ag catalyst, they investigated the faradaic efficiency (F.E.) of CO in the presence of amines with varying  $\text{pK}_a$  and different propensity to form carbamates. They reported that at  $\text{pH} > 10$  the F.E. CO is  $< 0.1\%$  and the F.E. CO increases to  $> 20\%$  when the pH is decreased, and it is ubiquitous to all the amines tested (Fig. 7c). To rationalize this behaviour they correlated the experimental data to the VLE-models, and explained that the carbamate concentration decreases at lower pH but the concentration of  $\text{HCO}_3^-$  and dissolved  $\text{CO}_2$  increases, which also increases the  $\text{CO}_2$  partial pressure (Fig. 7a and b). The changes in carbamate concentration were further tracked with  $^{13}\text{C}$  NMR along with the different species present in the solution. Furthermore, they showed that the partial current density of CO ( $j_{\text{CO}}$ ) had a first-order dependence with the partial pressure of  $\text{CO}_2$  verifying that the source of carbon is the dissolved  $\text{CO}_2$  in the solution and not the carbamate itself. In cases, where they did not see a linear increase of  $j_{\text{CO}}$  with decreasing pH, they discussed the possibility of the different amines having different activity towards HER, which could suppress the production of CO.<sup>61</sup>

Similar studies were performed by Kim *et al.* using a membrane electrode assembly with a single atom Ni catalyst and a Ag foil as catalyst. With both catalysts, they probed the source of carbon for the produced CO by changing the concentration of the carbamate in the system and also by changing the temperature of the reactor. They also quantified the carbamate concentration in the system using  $^{13}\text{C}$  NMR and observed a zero-order dependence on the F.E. CO with the carbamate





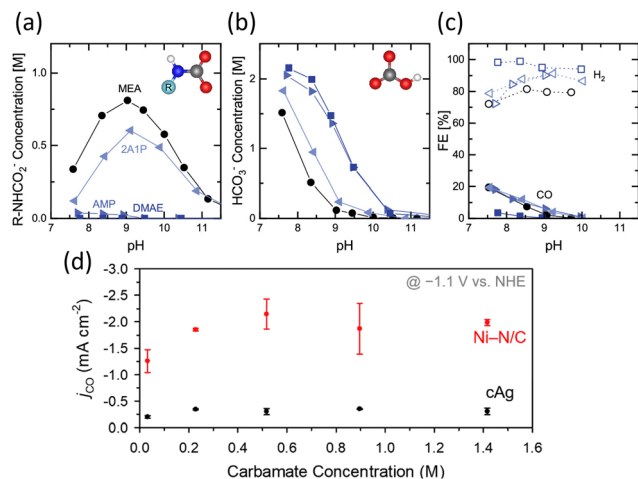


Fig. 7 (a) Concentration of carbamate from NMR vs. pH for 2 M KCl + 2 M amine with DMAE (square), AMP (right-pointing triangle), 2A1P (left-pointing triangle), and MEA (circle). (b) Concentration of bicarbonate from NMR vs. pH. (c) FE of CO (filled symbols) and H<sub>2</sub> (open symbols) production vs. pH from potentiostatic measurements at  $-1.30$  vs. SHE-iR.<sup>61</sup> Reproduced with permission from ref. 61, copyright 2023 American Chemical Society. (d)  $j_{\text{CO}}$  at  $-1.1$  V vs. normal hydrogen electrode (NHE) of Ni-N/C and cAg for the c-CO<sub>2</sub>RR in CO<sub>2</sub>-absorbed MEA (1–5 M) solutions with purging Ar.<sup>15</sup> Reproduced with permission from ref. 15, copyright 2022 Royal Society of Chemistry.

concentration, meaning the carbamate did not act as the active species for reduction (Fig. 7d). They further observed an increase in the F.E. CO as the temperature increased, which they attributed to more dissolved CO<sub>2</sub> released in the system at higher temperature.<sup>15</sup>

Thus, VLE models can be an important source to identify the active species. Changing the CO<sub>2</sub> loading, temperature, pH, and pressure of the system affects the species distribution and thus the VLE models in conjunction with the multi-variable dataset can rationalize the results to provide a basis for identification. In c-CO<sub>2</sub>RR studies, keeping track of these parameters can help in understanding how the amount of dissolved CO<sub>2</sub> changes in the system, and these changes can be correlated with the changing faradaic efficiency/partial current density of the products. If there were to be any direct reduction of the CO<sub>2</sub>-bound capture agent, the total partial current density of the reduced product should have a dependence on the carbamate concentration of the solution.

### 3.2 Continuum models

Safipour *et al.* investigated CO<sub>2</sub>RR with MEA solution in a flow-cell configuration to investigate the species getting reduced. By increasing the concentration of MEA they observed an increase in HER activity and reduction in CO production activity. To understand this effect, they developed a 1D continuum model to determine the concentration distribution of different species within the electrical double layer. Assuming concentration dependent Tafel kinetics, the electrode reactions were modelled. It was found that the CO<sub>2</sub> concentration at the surface of the electrode is lower in the presence of amines compared to

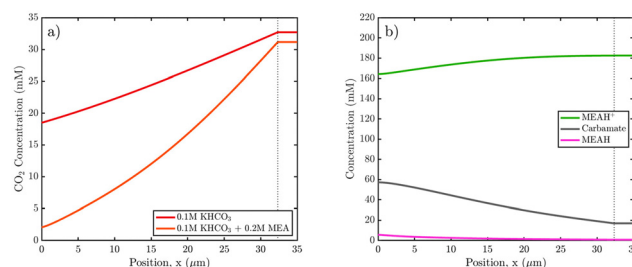


Fig. 8 Simulated boundary-layer concentration profiles at an applied potential of  $-1.5$  V vs. SHE, where the zero coordinate corresponds to the Ag cathode surface. (a) Comparison of the dissolved CO<sub>2</sub> concentration profile in 0.1 M KHCO<sub>3</sub> electrolyte with and without 0.2 M MEA additive. (b) MEA, MEAH<sup>+</sup>, and carbamate concentration profiles in 0.1 M KHCO<sub>3</sub> + 0.2 M MEA electrolyte, showing the depletion of MEAH<sup>+</sup> and accumulation of MEA and carbamate relative to their respective bulk values. Carbamate concentration is elevated due to the reaction of locally generated MEA with aqueous CO<sub>2</sub>, causing the result in (a).<sup>17</sup> Reproduced with permission from ref. 17, copyright 2023 American Chemical Society.

conventional CO<sub>2</sub>RR, which was responsible for the lower CO<sub>2</sub> conversion rates. The high activity for HER was related to the presence of high concentration of MEAH<sup>+</sup> at the surface which can act as a proton source. While a higher concentration of carbamate was observed to be present at the surface, the lower partial current density of CO compared to amine free electrolytes ruled out the possibility of any carbamate reduction (Fig. 8).<sup>17</sup>

Thus in different c-CO<sub>2</sub>RR settings, a similar approach can be taken to estimate the captured CO<sub>2</sub>-bound adduct concentration at the surface of the electrode and compare it with the partial current density of the reduced product to estimate if there is any CO<sub>2</sub>-bound capture agent reduction. Physics-based continuum models is therefore a key tool in establishing connections between device level performance metrics (like current density and product selectivity), electrode characteristics, and operational parameters. In c-CO<sub>2</sub>RR systems, continuum models can provide information regarding polarization behaviour, transport of products and reactants, and limitations in operational lifespan, which when complemented with experimental investigations can expedite the development of c-CO<sub>2</sub>RR technologies.<sup>62</sup>

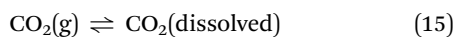
### 3.3 Two-film theory combined with reaction transport model

Recent investigations by Shen *et al.* and Kowalski *et al.* used the rotating cylinder electrode (RCE) setup to study the activity for c-CO<sub>2</sub>RR.<sup>16</sup> Shen *et al.* looked into different mass transport regimes by changing the rotation speed and observed that the partial current density of CO is linearly dependent with the partial pressure of CO<sub>2</sub>. They further developed a model for the partial current density of CO under limited mass transport regime of dissolved CO<sub>2</sub> to correlate  $j_{\text{CO}}$  to the amount of dissolved CO<sub>2</sub> in the system. Kowalski *et al.* used the same model to study the activity of c-CO<sub>2</sub>RR and compared methoxide capture agents to hydroxyls and amines. They also reported dissolved CO<sub>2</sub> as the primary species being reduced in c-CO<sub>2</sub>RR. This model is robust and unique where it measures



the partial pressure of CO<sub>2</sub> from the headspace in operando to identify the active species getting reduced and allows for quick screening of different activity descriptors. The two main parameters that are relevant to understand the model are (i) the mass film transfer coefficient at the gas–liquid interface and (ii) the mass film transfer coefficient at the liquid–electrode interface.<sup>16</sup>

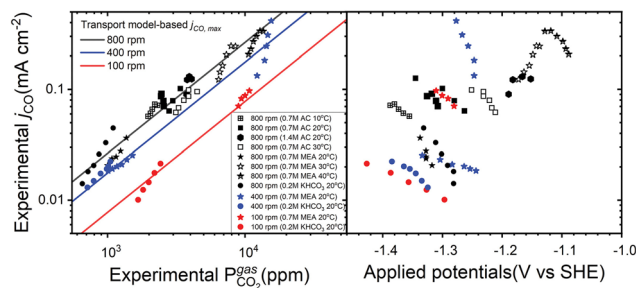
**3.3.1 Gas–liquid interface.** CO<sub>2</sub> absorption is a reversible process characterized by an equilibrium constant. The equilibrium between hydroxyl ions and dissolved CO<sub>2</sub> is given by reaction (11) for alkaline solutions. The absorption of CO<sub>2</sub> in alkaline amine solutions leads to the additional formation of the corresponding carbamate and ammonium ions (reactions (4)–(7)). The experimental challenge in c-CO<sub>2</sub>RR systems is measuring the concentration of dissolved CO<sub>2</sub> which could be a source of carbon for the reduced products and to decouple the dissolved CO<sub>2</sub> from the CO<sub>2</sub>-bound capture agent reduction. The CO<sub>2</sub> present in the solution will also be in equilibrium with the partial pressure of CO<sub>2</sub> (g) in the electrochemical cell. When a fast equilibrium is reached at the gas/liquid interface (eqn (15)), the partial pressure of CO<sub>2</sub> can be used to estimate the concentration of CO<sub>2</sub> dissolved in the solution using Henry's Law, given by eqn (16)



$$C_{\text{CO}_2}^{\text{liq}} = H_{\text{CO}_2} P_{\text{CO}_2}^{\text{gas}} \quad (16)$$

The Henry's constant,  $H_{\text{CO}_2}$  is a function of the temperature, pressure and also the solvent that is used in the system. Kowalski *et al.* in their study also pointed out that when looking at c-CO<sub>2</sub>RR systems under different capture agents such as amines and alkoxides, the solubility of CO<sub>2</sub> is different in the different solvents and this changes the Henry's constant value to be used in eqn (16). The difference in solubilities in different media must be taken into account while investigating c-CO<sub>2</sub>RR. This can be achieved through the use of VLE models and multi-scale models.

**3.3.2 Liquid–electrode interface.** The liquid–electrode interface is important in determining the flux of dissolved CO<sub>2</sub> to the electrode and realizing the local reaction conditions. Jang *et al.* developed a gas-tight rotating cylinder electrode (RCE) reactor which has well-defined mass transport properties and can quantify both gas and liquid products. In their work they characterized the mass transport properties of the RCE reactor and developed a Sherwood number relationship (eqn (17)) that universally holds true regardless of the experimental conditions including the effects of reactants, their concentration, electrode rotation, and temperature.<sup>63</sup> Using this relationship, both Shen *et al.* and Kowalski *et al.* determined the flux of CO<sub>2</sub> to their electrodes from the amount of dissolved CO<sub>2</sub> in their system. The equation was used as a reference to determine the convective transport-limited rates of reactions that cannot be readily obtained from experiments due to the complexity of c-CO<sub>2</sub>RR systems including multiple electrocatalytic and buffering reactions. For instance, the limiting current density ( $j_{\text{lim}}$ ) of CO in electrochemical reactors cannot be measured explicitly with the dominating hydrogen



**Fig. 9** Left panel: Experimental and transport model-based maximum partial current density for the reduction of dissolved CO<sub>2</sub> in a solution at equilibrium with a partial pressure of CO<sub>2</sub> determined using a gas chromatogram. Experiments containing amines were conducted using 0.099 M KClO<sub>4</sub> + 0.001 M KOH. All the experiments were conducted using an electrodeposited Ag catalyst as the working electrode, a Pt counter electrode, and a Ag/AgCl reference electrode. Right panel: Applied potential versus partial CO current density for experimental data in the left panel.<sup>16</sup> Reproduced with permission from ref. 16, copyright 2023 Elsevier.

evolution and is complicated to estimate with equilibrium reactions between CO<sub>2</sub> and absorber adducts. However, the maximum flux of CO<sub>2</sub> ( $J_{\text{CO}_2,\text{max}}$ ) that can reach the electrode surface can be determined from eqn (18), assuming that the local concentration of CO<sub>2</sub> at the electrode is zero. This calculated maximum flux of CO<sub>2</sub> or its corresponding maximum partial current density to CO ( $j_{\text{CO},\text{max}}$ ) was sufficient to explain the relationship between the observed partial pressure of CO<sub>2</sub> and  $j_{\text{CO}}$  to a large extent (Fig. 9) considering the low concentration of dissolved CO<sub>2</sub> in this system (eqn (19)). The potential impact of dissolved CO<sub>2</sub> reacting directly with hydroxyls generated at the cathode electrode during electrochemical reduction reactions in aqueous electrolytes was disregarded. These chemical reactions can lead to lower maximum current densities compared to what was observed in the absence of such reactions. However it was rationalized that within the boundary layer as dissolved CO<sub>2</sub> becomes depleted, it is probable that bicarbonate and carbamate will decompose (reversing reactions (5) and (6), and (7)) to generate additional CO<sub>2</sub>, offsetting the CO<sub>2</sub> consumed at the electrode surface. Local heating induced by ohmic resistance and the heating of the vicinity of the electrode due to the overpotential required to drive the reaction can facilitate further desorption of CO<sub>2</sub> from the amine absorber near the cathode electrode. Nonetheless, under steady-state conditions, the maximum flux of dissolved CO<sub>2</sub> from the electrolyte bulk would not exceed that given by eqn (18) and (19).

$$\text{Sh} = 0.204\text{Re}^{0.59}\text{Sc}^{0.33} \quad (17)$$

$$J_{\text{CO}_2,\text{max}} = k_{\text{m},\text{CO}_2} C_{\text{CO}_2,\text{bulk}} \quad (18)$$

$$j_{\text{CO},\text{max}} = 2FJ_{\text{CO}_2,\text{max}} \quad (19)$$

## 4 Reactor and catalyst design for c-CO<sub>2</sub>RR

Reactor and catalyst design have been extensively studied in the past for CO<sub>2</sub>RR, but there is not much consensus on how these



parameters play a role in c-CO<sub>2</sub>RR. Indeed, many strategies have been suggested to improve CO<sub>2</sub>RR performance. However, the community has now started to recognize that electronic modifications (d-band center tuning), alloying, and interface engineering alone are not sufficient to deliver a scalable CO<sub>2</sub>RR technology. Jang *et al.* has recently shown that transport alone has a larger impact in product selectivity during CO<sub>2</sub>RR on Cu than interface engineering (cation effects Cs<sup>+</sup>, K<sup>+</sup>, Na<sup>+</sup> *etc.*) or the predominant surface termination (*i.e.* comparison of pc-Cu, Cu(111), Cu(100), and Cu(751)).<sup>64</sup> Much of what has been claimed as catalytic enhancements are not maintained when the electrode areas are increased, indicating that the catalyst has a limited effect on the performance of the CO<sub>2</sub>RR electrolyzer.<sup>65,66</sup> The explanations based on morphology control, d-band center tuning, and interface engineering often emerge as an explanation to an experimental observation in a restricted set of experimental conditions. Reproducibility across labs working on CO<sub>2</sub>RR is an issue.<sup>67</sup> We note that this is not limited to CO<sub>2</sub>RR, but that this is indeed a widespread issue in electrocatalysis.<sup>68</sup> Our purposeful reduced discussion of catalyst optimization strategies in this review originates from our interest in discussing at depth what we consider has been phenomena ignored in the field, that is, the role of transport in electrocatalysis for c-CO<sub>2</sub>RR applications. Nevertheless, in order to provide a balanced discussion, other optimization strategies that do not focus on the role of transport are also discussed in Section 4.2. Additionally, in this section, we reflect on the effect that reactor geometry has on product selectivity where often different reactors result into different product distribution when using the same catalyst, suggesting reaction kinetics and reactor kinetics are convoluted in most electrocatalytic studies.

In this section, we will dive deeper into these discussions to understand how much knowledge from CO<sub>2</sub>RR can be translated to c-CO<sub>2</sub>RR, if at all.

#### 4.1 Role of catalyst morphology and geometry

In the past, a bulk of research for CO<sub>2</sub>RR has mostly focused on selecting catalyst based on their electronic properties and DFT calculations of binding energies of different intermediates. Two main descriptors for CO<sub>2</sub>RR has been the binding energies of \*CO and \*H,<sup>69,70</sup> but complexities arising from the presence of capture agents raises questions on whether CO<sub>2</sub>RR descriptors could be translated to c-CO<sub>2</sub>RR. Recently, Choi *et al.*, in their work showed that catalyst in the presence of amine capture agents can undergo corrosion, so binding energies of the amine to the surface is an important parameter when looking into c-CO<sub>2</sub>RR.<sup>71</sup>

Early works by Hori *et al.* was conducted in an H-cell configuration where the CO<sub>2</sub> dissolved in the solution is reduced to products.<sup>72</sup> This happens in the two-phase solid-liquid interface. Hori broadly divided metals into two categories; (i) CO producing metals like Au, Ag, Cu, and (ii) HCOO<sup>−</sup> producing metals like Sn, Pb, In, Cd, Hg. To operate at higher current densities reactor configurations were later modified to gas-diffusion electrolyzers which operate at the three-phase

boundary of solid-gas-liquid. However, with new reactor geometries researchers did not observe changes in selectivity of the catalysts, meaning the intrinsic activity of these catalysts at the two-phase boundary and the three-phase boundary remained the same. Although early reports suggest that CO<sub>2</sub>RR catalysts do not work well in c-CO<sub>2</sub>RR systems, there is still value in working with these catalysts to see if there is a suitable catalyst that can activate the CO<sub>2</sub>-bound captured complex to make reduction products. The idea is that if a suitable catalyst is identified then there is value in developing a new reactor design like the gas-diffusion electrodes to operate at higher current densities, however it is still likely that in the case of c-CO<sub>2</sub>RR the reaction will still occur at the two-phase boundary where the catalyst will be in contact with the liquid as in the H-cells.

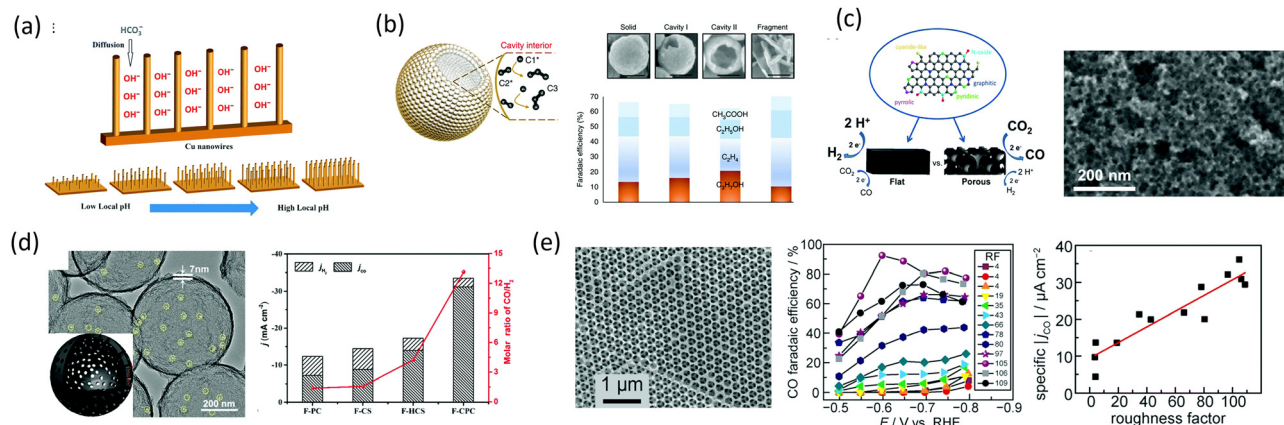
Although most studies have focused on catalyst activity, recent studies have shown that catalyst morphology and geometry also plays an important role in determining product distribution and tuning them could increase the efficiency of electrochemical systems. For CO<sub>2</sub>RR, several studies have already demonstrated that morphology of the catalyst plays a role to increase faradaic efficiency however for direct reduction of the captured CO<sub>2</sub>-bound adduct, there are additional buffer reactions occurring at the interface which makes it harder to delineate the mechanisms. In this section, we will look into the direct reduction of the CO<sub>2</sub>-bound capture agents from a catalyst perspective, where the two most important things is determining the active species at the surface of the electrode and investigating the effect of the geometry of catalyst on the electroreduction of these CO<sub>2</sub>-bound capture agents.

The transport of species from the bulk of the electrode to the catalyst surface (external mass transport) and from the catalyst surface to inside the pores (internal mass transport) both influences the product distribution in CO<sub>2</sub>RR and simultaneously can influence c-CO<sub>2</sub>RR. Studies that have used porous catalysts to increase the CO<sub>2</sub> conversion argued that a porous structure by means of internal mass transport can increase the OH<sup>−</sup> concentration within the pores and can suitably create a local CO<sub>2</sub> environment which increases the CO<sub>2</sub> utilization. The pH also plays an important role as a high pH reduces HER by reducing the concentration of protons.<sup>73,74</sup> In 1989 Hori *et al.* showed that a locally high pH at the electrode-electrolyte interface can facilitate C-C coupling to form multicarbon products.<sup>75</sup> A highly porous electrode have been argued to enhance this effect creating a very high pH within the pores by means of internal mass transport. Thus studies have looked into different mesoporous, microporous and nanoporous structure for CO<sub>2</sub>RR. Macropores can shorted the ion diffusion distance by increasing the buffer-volume of the reactions, while mesopores facilitate mass transport properties and micropores help in increasing the active surface area.<sup>76</sup>

Tuning the morphology of the catalyst can thus affect the local electronic structure by altering the grain boundaries, edges, facets, and corners. This can modify the pH, mass transport, adsorption/desorption kinetics, and local CO<sub>2</sub> concentration, at different scales. Different morphologies including nanocavities, mesopores, nanocages, crystalline







**Fig. 10** (a) Schematic of the diffusion of electrolytes into Cu nanowire arrays.<sup>77</sup> Reproduced with permission from ref. 77, copyright 2016 Wiley (b) energy profile for the formation of the  $\text{C}_3$  intermediate. Red, grey, and orange balls represent oxygen, carbon, and copper, respectively and schematic showing that the cavity confinement effect boosts  $\text{C}_2$  species binding and further conversion to  $\text{C}_3$  and the corresponding faradaic efficiency.<sup>78</sup> Reproduced with permission from ref. 78, copyright 2018 Nature (c) schematic showing the activity difference on flat and porous NC and TEM image of NC-27.<sup>84</sup> Reproduced with permission from ref. 84, copyright 2019 Elsevier (d) TEM image of F-CPC. The insert shows the schematic structure and  $\text{CO}_2\text{RR}$  performance of various catalysts at  $-1.0\text{ V}$ .<sup>87</sup> Reproduced with permission from ref. 87, copyright 2020 American Chemical Society (e) SEM image of an Ag-IO film with CO FEs and ECSA-normalized CO current of Ag-IO films with varied RF.<sup>88</sup> Reproduced with permission from ref. 88, copyright 2016 American Chemical Society.

porous frameworks and porous thin films have been studied in the past for  $\text{CO}_2\text{RR}$ .<sup>76</sup>

Ma *et al.* using Cu nanowires showed that the structure of the catalyst can regulate the pH causing the changes in the internal transport of the  $\text{HCO}_3^-$  and  $\text{OH}^-$  species in and out of the pores, which altered the selectivity leading to more preferred CO dimerization pathway (Fig. 10a).<sup>77</sup> Zhuang *et al.* showed that a Cu catalyst structure with nanocavity can promote the C-C coupling between the  $\text{C}_2$  and  $\text{C}_1$  intermediates to form  $\text{C}_3$  products.<sup>78</sup> They observed that a nanocavity could concentrate  $\text{C}_2$  species inside the cavities through steric confinement, increasing the  $\text{C}_3$  production inside the cavities (Fig. 10b). Mesoporous structures, mainly carbon-based, were also investigated for  $\text{CO}_2\text{RR}$ , as larger surface areas could potentially increase the active sites.<sup>79–81</sup> Although pristine carbon is known to be electrochemically neutral, chemical doping using N, B, F, and S atoms have been used to break the neutrality to generate active sites for  $\text{CO}_2\text{RR}$ .<sup>82,83</sup> Hursan *et al.* showed that morphological attributes like porosity and pore size can have an effect on the performance of N-doped catalysts on  $\text{CO}_2\text{RR}$ .<sup>84</sup> They observed that the nonporous N-doped catalyst was the least hydrophobic and produced the highest HER, compared to the porous films which enhanced  $\text{CO}_2\text{RR}$  performance. To describe this behavior, they correlated wettability with surface energy. Changes in wetting properties influence the dynamics of gas bubble formation on the electrodes. The non-porous samples can result in large bubbles that can block the active sites of the catalyst for  $\text{CO}_2$  reduction. They highlight that the release of gas bubbles which are dependent on the wetting properties of the catalyst can bring about changes in mass transport leading to changes in the catalytic current densities. Hydrophobic surfaces enhance gas bubble diffusion and release. Other reports also suggest that the surface hydrophobicity can diminish the catalyst-water

contact inducing a high concentration of  $\text{OH}^-$  near the electrode, increasing the local pH and decreasing HER<sup>85</sup> (Fig. 10c). The wetting properties of a material are usually determined by the interfacial interaction forces between a solid and the fluid. These van der Waals forces, which are dependent on polarity, dipole moment, structures, and charging states, develop at the solid-liquid interface. The net surface energy then determines the wetting properties of the material.<sup>85,86</sup> It has thus been observed that higher surface energy generally leads to more hydrophilic surfaces. However, during electrochemistry, these forces will act under an electric field which can further modify the interaction of these forces. Different studies have reported that the electrowetting properties of electrodes can be adjusted by tuning (i) the dielectric properties of the electrode and electrolyte and (ii) choosing a catalyst PZC such that there is no excess-charge at the solid-liquid interface.<sup>85</sup> Therefore, wetting properties have potential to further enhance the performance of c- $\text{CO}_2\text{RR}$  and must be explored during the development of c- $\text{CO}_2\text{RR}$  technologies. Hierarchical porosity has also been investigated by Ni *et al.* where they used an F-doped hierarchical nanocage structure and compared it to F-doped solid carbon and F-doped carbon with mesopores. They observed that the hierarchical structure possessed the largest surface area among all and also the highest F.E and current density for CO, which was rationalized by increased mass transport and low diffusion resistance from the hierarchical structure (Fig. 10d).<sup>87</sup> Dutta *et al.* showed that porous thin films, like Cu foam, have a difference in product selectivity where they make more  $\text{C}_2\text{H}_4$  and  $\text{C}_2\text{H}_6$  compared to CO in flat Cu. The catalytic difference was attributed to the presence of (100) facet in porous electrodes which have an intrinsic activity for C-C coupling (Fig. 10e).<sup>88</sup> Existing knowledge on  $\text{CO}_2\text{RR}$  can thus provide a basis on the activity of catalysts with different geometries for c- $\text{CO}_2\text{RR}$  and should be further investigated to





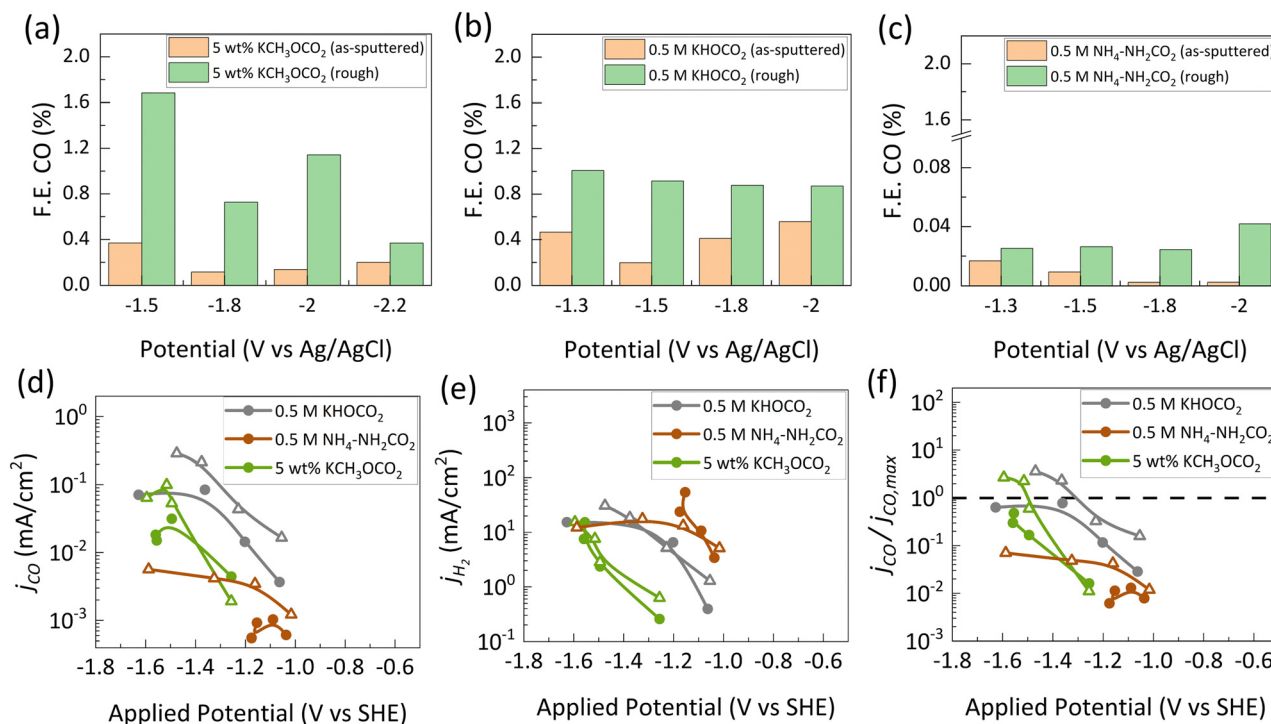
understand how the presence of amines or other capture agents might alter the product distribution.

A few studies have been conducted while flowing  $\text{CO}_2$  in the presence of amines. Although they are not analogous to c- $\text{CO}_2\text{RR}$  conditions, they can help understand the role of amines in electrochemical reduction reactions. Chen *et al.* reported an increase in formate production in porous In catalyst and an increase in CO production in porous Ag and Zn catalyst in a 30 wt% MEA solution.<sup>89</sup> Hossain *et al.* prepared nano-dendrites of Cu, Au, and Ag on a glassy carbon electrode and investigated  $\text{CO}_2\text{RR}$  in a 0.05 M MEA solution, where they observed an enhancement in current densities with the nanostructured catalyst.<sup>90</sup>

The only study that reports the effect of porosity under c- $\text{CO}_2\text{RR}$  environment is by Kowalski *et al.* where they investigated the current densities and faradaic efficiencies between sputtered Ag electrodes and electrochemically roughened Ag electrodes (Fig. 11). They found that although c- $\text{CO}_2\text{RR}$  predominantly produces HER, increasing the porosity had an effect in slightly enhancing the CO production. They looked into amines, hydroxyls and methoxides as capture agents and in all of them the faradaic efficiency and  $j_{\text{CO}}$  of CO increased with porosity. Maximum F.E. CO of  $\approx 1.5\%$  and  $\approx 1\%$  were reported for the electro reduction of methyl carbonate  $\text{CH}_3\text{OCOO}^-$  and bicarbonate  $\text{HOCO}_2^-$ , respectively (Fig. 11a and b). The F.E. CO for ammonium carbamate although increased, the maximum remained very low at  $\approx 0.03\%$  (Fig. 11c). They further normalized

their  $j_{\text{CO}}$  values to the mass transport limited  $j_{\text{CO}}$  from the flux of dissolved  $\text{CO}_2$  and observed that the normalized  $j_{\text{CO}}$  values crossed the limiting transport line for reduction of dissolved  $\text{CO}_2$  (Fig. 11d and e). They hypothesize that with porous electrodes the local pH within the pores becomes higher than at the entrance of the pores. This high pH suppresses HER resulting in more available sites for  $\text{CO}_2$  reduction to produce CO. Although the increase in  $j_{\text{CO}}$  was higher than the calculated limiting value they still reported it as dissolved  $\text{CO}_2$  reduction. Furthermore, from the partial current density obtained from the different capture agents it was concluded that  $\text{H}_2$  was mostly produced from outside the pores as no changes in  $j_{\text{H}_2}$  was observed with the as-sputtered electrodes and the electrochemically roughened electrodes. Whereas the increase in CO was the result of more  $\text{CO}_2$  being reduced within the pores. Thus internal mass transport and local reaction environment within and around the pores also play a role along with external mass transport in c- $\text{CO}_2\text{RR}$  systems.

In electrocatalysis, recent investigations have deployed the use of the Thiele modulus to understand the relative balance between kinetic and mass transport resistances inside catalyst pores. The Thiele modulus in catalysis is used to describe the relation between reaction rates and diffusion rates. For large values of Thiele modulus, the overall reaction rate is constrained by diffusion resistance, and the reaction predominantly occurs within the outer catalyst layers. Conversely, when Thiele modulus values are small, the overall reaction rate



**Fig. 11** The faradaic efficiency of CO obtained from as-sputtered Ag electrode compared to roughened Ag electrode at different applied potentials (vs. Ag/AgCl) for (a)  $\text{KCH}_2\text{OCO}_2$  (methyl carbonate), (b)  $\text{KHOCO}_2$  (bicarbonate) (c)  $\text{NH}_4\text{-NH}_2\text{CO}_2$  (ammonium carbamate). Comparison of (d)  $j_{\text{CO}}$  and (e)  $j_{\text{H}_2}$  between the sputtered Ag electrodes (solid dots) and the roughened Ag electrodes (hollow triangles). (f) The  $j_{\text{CO}}$  is further normalized against the maximum flux of  $\text{CO}_2$  and it is observed that the rough electrodes are able to cross the transport-based limiting  $j_{\text{CO}}$  which was rationalized from the local release of  $\text{CO}_2$  within the pores.<sup>12</sup> Reproduced with permission from ref. 12, copyright 2024 American Chemical Society.

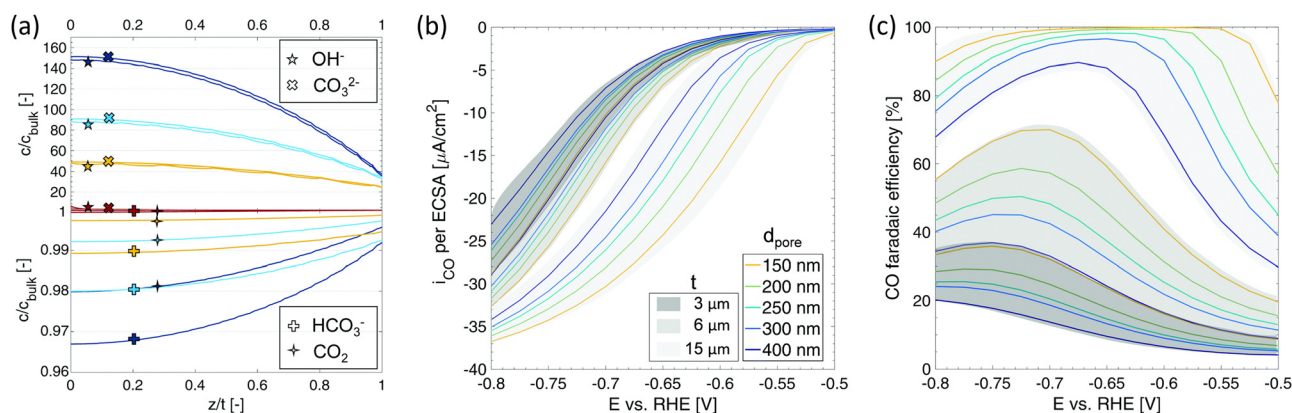
is restricted by the catalyst volume, specifically the total accessible pore surface area. Traditionally, this concept has been mostly used for fuel cell reactor development across multiple length scales, however its use in other electrochemical systems is somewhat limited. Recently, Thiele modulus analysis have been explored by a few researchers to understand the effectiveness factor of their catalyst. Kim *et al.* and Wang *et al.* used Thiele modulus modeling in gas diffusion electrodes for CO<sub>2</sub> reduction and also developed analytical models to describe catalyst effectiveness.<sup>91,92</sup> Similarly Wan *et al.*, investigated the potential dependent Thiele modulus models to probe the utilization of pores as a function of catalyst particles and reactant properties. Using a 1D reaction diffusion model through the pores they developed the Thiele modulus model and delineated external and internal mass transport to effectively outline design principles for the electrocatalysts.<sup>93</sup> The Thiele modulus can also be defined for c-CO<sub>2</sub>RR to understand and quantify the effectiveness of morphology and catalyst geometry. It will further be effective in understanding the relative timescales of reaction and diffusion within the pore of the catalyst to rationalize the increased CO<sub>2</sub> reduction products observed within the pores under c-CO<sub>2</sub>RR conditions.

Since all studies point towards the free CO<sub>2</sub> as the active species for reduction, the knowledge existing for CO<sub>2</sub>RR on the effect of porosity can further be used to understand c-CO<sub>2</sub>RR mechanisms. However, one study by Ma *et al.* reports the direct reduction of carbonate to formate which is discussed in detail in Section 5. The local OH<sup>−</sup> concentration dynamically influences the buffer reactions, and when imagined in the context of c-CO<sub>2</sub>RR there are additional buffer reactions that make these systems more complex. Suter *et al.* using a finite element model investigated different porosity and species concentration within the pores to predict CO and H<sub>2</sub> current densities. The model predicts that OH<sup>−</sup> and CO<sub>3</sub><sup>2−</sup> concentration within the pores are higher than at the surface resulting in a high alkaline pH, which is more obvious in a thicker film, as can be seen from Fig. 12. Predicted CO FEs and current density increased

with increasing RF factor which also aligned with experimental findings.<sup>94</sup> Thus, a high alkaline pH is understood to suppress HER within the pores allowing more available sites for CO<sub>2</sub> reduction. The same study also coupled the effect of pore diameter and film thickness to investigate the changes in CO FE and observed a linear dependency of roughness factor (RF) with film thickness and non-linear dependency of RF with pore diameter. They concluded that multiple combinations of pore diameter and film thickness can give similar faradaic efficiency. For instance, a FE CO of 90% can be achieved from a pore diameter of 200 nm and film thickness of 10 μm or a pore diameter of 100 nm and film thickness of 7 μm. Thus it was concluded that roughness factor alone is not enough to characterize a porous film.<sup>95</sup> Experimentally, it is difficult to determine the local OH<sup>−</sup> or CO<sub>2</sub> concentration inside the pores. A recent study by Bohme *et al.* developed a pOH sensor where a confocal laser scanning microscopy technique was used to map the pOH around the electrode during CO<sub>2</sub>RR. They were able to experimentally verify that the OH<sup>−</sup> concentration is high within the pores compared to outside the pores as suggested by many other studies mentioned before.<sup>96</sup> When extending it to c-CO<sub>2</sub>RR, the high alkalinity of the pores can also suppress HER and promote CO<sub>2</sub> reduction, as has been observed by Kowalski *et al.* through their experimental findings. Furthermore, the additional buffer reactions of amine deprotonation and carbamate consumption is also affected with changes in local pH that contribute to altering the selectivity of the products formed. Thus, it is important to be critical about all these factors while investigating different activity and stability descriptors for c-CO<sub>2</sub>RR.

## 4.2 Tuning catalyst properties for c-CO<sub>2</sub>RR

Designing catalyst for c-CO<sub>2</sub>RR that can tune (i) electronic properties, (ii) binding properties, and (iii) intermediate concentration at the electrode–liquid interface will be necessary as the field evolves. Electronic properties in particular has been shown to play an important role in modifying the binding properties of key intermediates in CO<sub>2</sub>RR and can have the



**Fig. 12** (a) Concentration profiles along the  $z$ -axis, where  $z = 0$  is the innermost point inside the pore and  $z = 1$  is the entrance of the pore, of OH<sup>−</sup>, CO<sub>3</sub><sup>2−</sup>, HCO<sub>3</sub><sup>−</sup> and CO<sub>2</sub> versus their bulk concentration at a potential of  $-0.8$  V vs. RHE. (b) Partial CO current density and (c) CO faradaic efficiency for Ag-IO with pore diameters of 150–400 nm and film thickness of 3, 6 and 15 μm.<sup>95</sup> Reproduced with permission from ref. 95, copyright 2019 Royal Society of Chemistry.



same effect on c-CO<sub>2</sub>RR. The upper shift of d-band energy level results in increased binding strength of the adsorption intermediates. This understanding has been used at different scales to tune the selectivity of reduction products, from single atom catalysts (SAC), to nanoparticles, and surfaces with different terminations.<sup>97</sup>

Different SACs have been designed with different metal centers like Ni, Fe, Co, In, Bi, and Sn for producing CO and HCOO<sup>−</sup>.<sup>97–99</sup> These dispersed metal sites along with their coordination environment create M–N<sub>4</sub> moieties of superior performance over their metal counterparts. In this unique assembly the electronic structure of the metal center is modified by the adjacent coordination environment and this has been shown to modify the catalytic activity, selectivity and stability. Further optimization of electronic structure has been studied by looking into vacancy defects to generate the Ni–N<sub>3</sub>–V moiety or through heteroatom doping to generate Ni–N<sub>3</sub>P. Both of these approaches have been suggested to have superior performance for c-CO<sub>2</sub>RR compared to the Ni–N<sub>4</sub>.<sup>100,101</sup>

For nanoparticles it is generally observed that the electrocatalytic performance is determined by the amount of under-coordinated sites where the CO<sub>2</sub>RR intermediates preferentially bind and is dependent on the ratio of surface to bulk atoms. Gu *et al.* observed that the Ni-based nanoparticles had lower faradaic efficiencies compared to Ni SAC.<sup>102</sup> However, this behavior varies depending on the metal that is being used as the catalyst. Huang *et al.* investigated the production of HCOO<sup>−</sup> on In based catalysts and found that In<sub>2</sub>O<sub>3</sub> nanocrystals which are 15 nm in diameter were more active than the nanocrystals which are 200 nm or In foil, which they attributed to the increased uncoordinated sites with lower particle size. On reducing the nanoparticle size to 5 nm they observed that the partial current densities for HCOO<sup>−</sup> decreased. This shows that smaller may not be always better in catalyst design and that a deep understanding of structure–property relationship is important when designing catalysts.<sup>103</sup>

Strategies like alloying have also been explored in numerous CO<sub>2</sub>RR studies in the past to tune the spatial distribution of reduction intermediates and enhance the selectivity towards certain products.<sup>104–106</sup> For instance, Gao *et al.* designed a CuAg catalyst to improve the selectivity of CO<sub>2</sub> reduction to ethylene. Using operando Raman spectroscopy they showed that the bimetallic catalyst produces more \*CO binding sites that can then hydrogenate at neighboring sites and couple to make C<sub>2</sub> products. This is often coupled with interface engineering strategies, as discussed in Section 5, to modify the local concentration of the active species and its intermediates.<sup>107</sup>

Although, these strategies are useful to design catalyst for improved activity and selectivity, however it is often argued for scalable technologies transport plays a more significant role than the catalyst itself. Hursan *et al.* in their study highlighted on this effect. Using N-doped carbon they designed electrodes of different porosity and depending on the pore size they observed different selectivity towards CO and H<sub>2</sub> formation in CO<sub>2</sub>RR. They concluded that porosity modifies mass transport and consequently the CO<sub>2</sub> adsorption properties that primarily

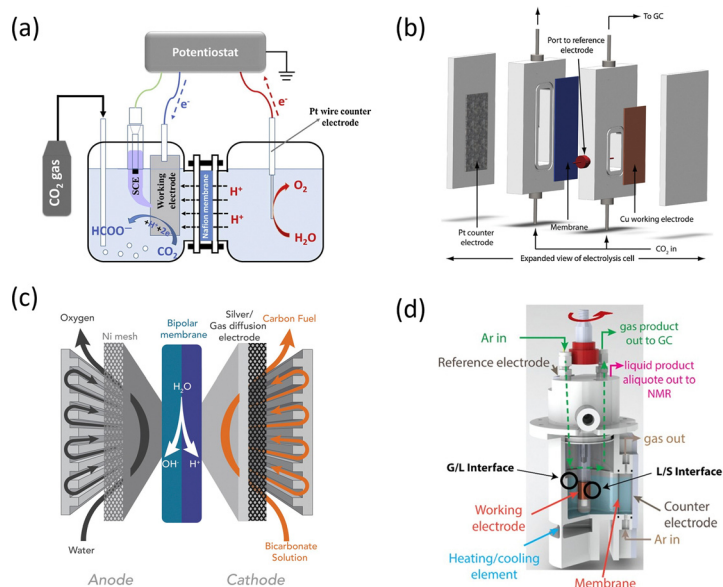
governs CO<sub>2</sub>RR. Therefore, morphological attributes that determines transport affect the catalytic performance and needs to be given more importance while designing large scale electrolyzers.<sup>84</sup>

### 4.3 Engineering reactor design to tune mass transport and kinetics

The electrolyzer design and cell configuration are important considerations in c-CO<sub>2</sub>RR. The electrolyzer architecture and the operating conditions (*e.g.* temperature, pressure, potential, current) influence the transport of the active species and products between the bulk of the solvent and the electrode surface, as well as the temporal speciation of the capture agent and CO<sub>2</sub> adducts. The reactor design will also determine the rate of equilibration between the species in the gas phase and those dissolved in the liquid. Recent studies on c-CO<sub>2</sub>RR have been carried out in different reactor designs which have different mass transport characteristics. The commonly used electrochemical reactors, the H-cell and the flow cell configuration, have also been used extensively for CO<sub>2</sub>RR in the past and recent work has shown that hydrodynamics in the cell indeed determine the product distribution obtained.<sup>63,108</sup> To date, very few works have been reported for c-CO<sub>2</sub>RR but it can be anticipated that the type of reactors used will also impact the product distribution in this reaction. In some of the c-CO<sub>2</sub>RR systems discussed in this section, the membrane separating the cathode and anode compartments is used to control the generation and transport of protons that shift the equilibrium and release CO<sub>2</sub> in the proximity of the catalyst (reverse direction of eqn (5)–(7)). Electrolyzer design is thus tightly tied to the performance of c-CO<sub>2</sub>RR systems and needs to be carefully studied.

This section discusses four types of electrochemical cells (H-cell, compression, zero gap, and rotating electrode) that have been used for activity benchmarking in c-CO<sub>2</sub>RR, as shown in Fig. 13. Leverick *et al.*, used an H-cell to investigate amines of varying pK<sub>a</sub> and sterics and reported the differences in faradaic efficiencies for producing CO as a function of pH and temperature.<sup>61</sup> They observed that the partial current density of CO had a weak amine dependence but had a first order dependence with the partial pressure of CO<sub>2</sub> in the system, which suggested that the active species undergoing reduction is the dissolved CO<sub>2</sub> and not the amine. Safipour *et al.*, investigated CO<sub>2</sub>RR in the presence of mono-ethanol amine (MEA) in a sandwich-type compression cell configuration (Fig. 13b) and observed a maximum partial current density for CO of 5 mA cm<sup>−2</sup>, which decreased with the increasing concentration of MEA. With the help of a 1D continuum model they report that the addition of MEA increases the concentration of MEAH<sup>+</sup> which acts as a proton source for H<sub>2</sub> and reduces the local concentration of CO<sub>2</sub>, which in turn reduces the partial current density of CO, with no evidence of any carbamate getting reduced.<sup>17</sup> To increase the amount of reduced products from CO<sub>2</sub> capture solutions, the Berlinguette group designed the bicarbonate electrolyzer as shown in Fig. 13c, where they used a bi-polar membrane or a proton exchange membrane in a





**Fig. 13** (a) Conventional H-type cell configuration used by Leverick *et al.* to study the  $j_{\text{CO}}$ ,  $j_{\text{H}_2}$  and F.E. CO and FE  $\text{H}_2$  of c- $\text{CO}_2\text{RR}$  at different pH and applied potentials for amines of different  $\text{pK}_a$  and sterics.<sup>61</sup> Reproduced with permission from ref. 61, copyright 2023 American Chemical Society (b) a schematic of the compression cell type configuration used by Safipour *et al.* to investigate the species distribution near the surface of the electrode while studying  $\text{CO}_2\text{RR}$  in the presence of MEA.<sup>17,111</sup> Reproduced with permission from ref. 17 and 111, copyright 2023 American Chemical Society and 2012 Royal Society of Chemistry (c) the zero-gap membrane electrode assembly used as the bicarbonate electrolyzer by Li *et al.* and Lees *et al.* to release  $\text{CO}_2$  in the bulk of the solution by supplying protons to increase the FE  $\text{CO}$ .<sup>18,19</sup> Reproduced with permission from ref. 18 and 19, copyright 2020 American Chemical Society and 2019 Elsevier (d) a schematic of the gas-tight rotating cylinder electrode cell used by Shen *et al.* to investigate mass transport limited conditions for c- $\text{CO}_2\text{RR}$ .<sup>16,63</sup> Reproduced with permission from ref. 16 and 63, copyright 2023 Elsevier and 2022 Wiley.

membrane electrode assembly for supplying protons and locally release  $\text{CO}_2$  from bicarbonate in the solution and promote  $\text{CO}_2\text{RR}$ .<sup>18,19</sup> This increased the flux of  $\text{CO}_2$  to the surface of the electrode and high faradaic efficiencies for CO was achieved, but at a penalty of high input energy. The thermodynamic minimum energy for converting  $\text{CO}_2$  to CO is  $-1.33$  V whereas the input voltage required to reach a current density of  $-100$   $\text{mA cm}^{-2}$  was  $-4.4$  V in their electrolyzer, while lab-scale  $\text{CO}_2\text{RR}$  electrolyzers have already demonstrated to achieve  $-200$   $\text{mA cm}^{-2}$  at cell voltages below  $-3$  V.<sup>109,110</sup> A similar setup was also used by Kim *et al.* to study the reduction of carbamates using single atom Ni catalyst and a high CO selectivity was achieved with FE of  $\approx 69\%$ .<sup>15</sup> Shen *et al.*, using the RCE cell investigated different mass transport regimes by changing the rotation speed and observed different faradaic efficiencies and partial current densities of CO, and further concluded that the produced CO is from the dissolved  $\text{CO}_2$  within the system. The RCE cell system is unique in that it measures the partial pressure of  $\text{CO}_2$  in the headspace of the cell, which is in a pseudo-equilibrium with the solution. The partial pressure of  $\text{CO}_2$  can be used to estimate the amount of free and dissolved  $\text{CO}_2$  in the bulk of the electrolyte and facilitates the discrimination between different carbon sources during c- $\text{CO}_2\text{RR}$ .<sup>16</sup>

Transport of mass, heat, and charge affect the kinetics in c- $\text{CO}_2\text{RR}$  and therefore must be considered while designing electrolyzers for this reaction. A cell design with a thick hydrodynamic layer, like the H-cell, could slow down the local mass

transfer of the species resulting in lower faradaic efficiency.<sup>112</sup> Also, as the dominant product of c- $\text{CO}_2\text{RR}$  is  $\text{H}_2$ , the design must include considerations for ways to suppress HER. For instance, a cell design with very good mass transport, like the RCE cell, promotes HER as along with  $\text{CO}_2$  and carbamate they also increase the flux of the bicarbonate and the ammonium cations to the electrode which act as a proton source.<sup>12</sup> Furthermore, cell resistance and uniform current distribution are some other factors that can potentially affect product distributions in electrochemical systems, especially for organic solvents with lower conductivity.

The availability of the active species at the surface of the electrode determines the production efficiencies. Thus designing the catalyst geometry to efficiently increase the contact of the active species can enhance c- $\text{CO}_2\text{RR}$ . For instance, fundamental mass transport studies have mostly been carried out using the RDE/RRDE (rotating disk electrode/rotating ring disk electrode),<sup>113</sup> however RDE setups present challenges of having low surface area, with poor hydrodynamics resulting in bubble formation at the tip of the electrode and concentration gradient along the radial direction of the disk.<sup>114</sup> In comparison, the rotating cylinder electrode proposed by Jang *et al.* had a higher surface area, which leads to the availability of a higher concentration of  $\text{CO}_2$  near the surface of the electrode, which was eventually used for mass transport studies.<sup>63</sup>

$\text{CO}_2\text{RR}$  suffers from slow kinetics and is rapidly limited by mass transport of  $\text{CO}_2$  in most conventional cells used for fundamental studies. Similar difficulties can also be





anticipated for c-CO<sub>2</sub>RR if species relevant to the catalytic process are present in small amounts, and thus it is important to maintain a high flux of the active species to the electrode. Changing the residence time of reactants and reaction intermediates can alter the product selectivity without altering the intrinsic kinetics of the electrode itself, and distinguishing the relative timescales for transport and reaction at the catalyst scale is increasingly necessary.<sup>63</sup>

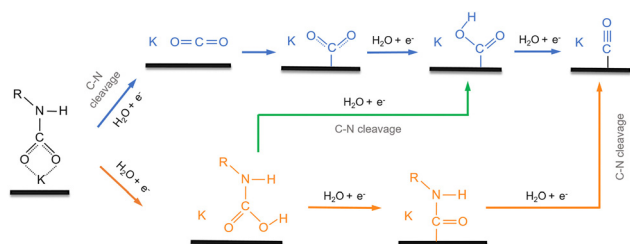
## 5 Heterogeneous reaction mechanism

Although reaction mechanisms and reaction intermediates are known for CO<sub>2</sub>RR, little is known about c-CO<sub>2</sub>RR. It is unclear why hydrogen is the major product and what happens within the double layer. It is a common consensus that protonated amines act as the extra source of proton to facilitate hydrogen production, but how the carbamate is transported to the electrode-electrolyte interface is not known.<sup>61</sup> Also, how the local pH or the buffer reactions play a role in such systems is not well-understood. To date c-CO<sub>2</sub>RR studies have mostly looked into the formation of CO and HCOO<sup>−</sup> as products and thus, delineating the different possible pathways at the surface of the electrode is important to gain deeper insights into the mechanisms relevant to c-CO<sub>2</sub>RR.

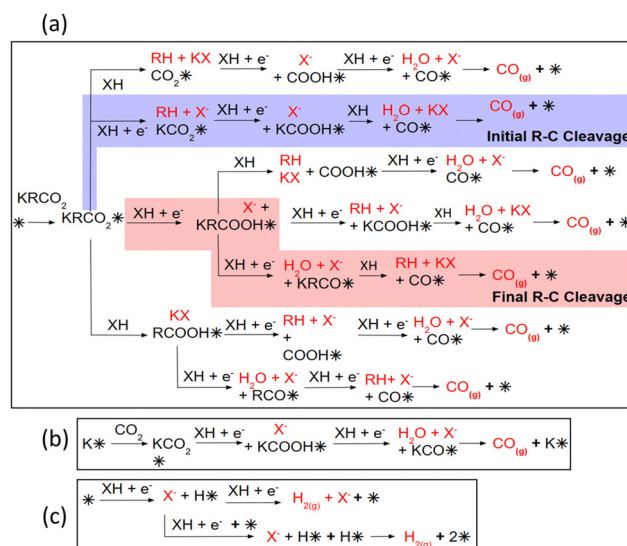
Shen *et al.* proposed the competitive mechanism of electrochemical carbamate reduction on Ag as shown in Fig. 14. They proposed that cations present in the system help in bringing the carbamate to the electrode and can facilitate the electron transfer from the electrode to the carbamate for its further reduction. The carbamate can either decompose through a C–N bond cleavage to form CO<sub>2</sub> and the amine RNH<sub>2</sub> (blue pathway) or a direct proton–electron transfer on the carbamate to form the \*RNHCOOH intermediate (orange pathway, \* indicates a chemisorbed species on the Ag electrode). Once CO<sub>2</sub> is formed, it can chemisorb on the catalyst surface as shown on the blue pathway and reduced subsequently to \*CO *via* two proton–electron transfer steps, which is the typical CO<sub>2</sub>RR pathway on Ag.<sup>115</sup> In contrast, the orange pathway directly reduces the carbamate, initially keeping the C–N bond formed. After forming \*RNHCOOH, the C–N bond can break to generate \*COOH on the surface (green path) or it can further reduce by proton–

electron transfer to \*RNHCO and water (orange path). Consequently, \*RNHCO undergoes an additional proton–electron transfer on N and C–N bond cleaves to form \*CO and restore the amine simultaneously. In short, along the pathway, C–N bond cleavage and further reduction of CO<sub>2</sub> compete with the direct proton–electron transfer to O in the –CO<sub>2</sub> group of the carbamate and C–N cleavage at a later step, thus creating three possible bifurcating pathways.<sup>16</sup>

Kowalski *et al.* in their work describes a generic reaction network with different possible elementary pathways that could occur in c-CO<sub>2</sub>RR systems. They use KRCO<sub>2</sub> as the captured CO<sub>2</sub> adduct and study the different pathways that can occur when the R is CH<sub>3</sub>O (methyl carbonate), NH<sub>2</sub> (carbamate) or OH (bicarbonate) as shown in Fig. 15.<sup>12</sup> They show that after the adsorption of the KRCO<sub>2</sub> on the Ag electrode four different pathways can occur. The first route is the cleavage of R–C bond by protonation from the proton source XH (XH is either the solvent or the capture agent) producing adsorbed CO<sub>2</sub>, RH and KX. This pathway then leads to the usual CO<sub>2</sub>RR pathway with the first proton-coupled electron transfer (PCET) producing \*COOH and the second producing \*CO and water. The second route modifies the order of PCET and protonation, starting from a PCET assisted cleavage of R–C bond followed by a second PCET to form \*COOH. The final C–O bond cleavage in



**Fig. 14** Proposed mechanism for the competition between electrochemical carbamate decomposition combined with CO<sub>2</sub> electroreduction (blue pathway) and carbamate direct reduction (orange pathway). The C–N bond cleavage can occur at three possible steps in the mechanism. K is the alkali metal potassium.<sup>16</sup> Reproduced with permission from ref. 16, copyright 2023 Elsevier.



**Fig. 15** (a) Reaction scheme for the reduction of the captured CO<sub>2</sub> with a general capture agent (R–H, examples being NH<sub>2</sub>–H, CH<sub>3</sub>O–H, and HO–H). R represents the deprotonated capture agent (NH<sub>2</sub> for NH<sub>3</sub>, OCH<sub>3</sub> for methanol, or OH for H<sub>2</sub>O), XH represents a general proton source. In methanol solvent, the proton sources in our study include methanol and NH<sub>4</sub><sup>+</sup>, written formally as NH<sub>4</sub>CIO<sub>4</sub> to be in the XH form. In the water–amine solvent, this includes H<sub>2</sub>O, KHCO<sub>3</sub>, and NH<sub>4</sub><sup>+</sup>. \* represents the catalytic Ag site. All species containing \* are adsorbed on the site. Chemicals in red text represent the products evolving in the solvent at each step. The two most favored pathways from our calculations both initiate with a proton-coupled electron transfer and are highlighted in blue (initial R–C cleavage in the CO<sub>2</sub> complex) or in red (final R–C cleavage). Reaction schemes for (b) CO<sub>2</sub>RR, and (c) HER are also recalled with similar notations.<sup>12</sup> Reproduced with permission from ref. 12, copyright 2024 American Chemical Society.

this pathway is chemically assisted by the proton transfer from XH. The third route starts with a PCET at an O atom forming  $\text{KRCOOH}$  from where it can either go through a PCET step to cleave C–OH bond to form RCO and then the R–C bond is cleaved in a final proton transfer step to make CO, water, and KX, or it can cleave the R–C bond first by PCET or proton transfer followed by C–O bond cleavage. The fourth route treats the first step as chemical protonation using the XH proton source, and the second and third steps can be electrochemical PCET. Thus, these different pathways provide an overview of the mechanisms that could exist for different capture agents in different  $\text{c-CO}_2\text{RR}$  setups.

Recently Ma *et al.* reported the direct electroreduction of carbonate to formate using a Cu catalyst. Through DFT calculations they discussed four possible reaction pathways that can occur at the electrode. In Fig. 16, path 1 shows the adsorption of the  $\text{CO}_2$  through the O sites in the  $^*\text{OCO}^-$  bidentate form, in path 2 a molecular  $\text{CO}_2$  is attacked by a hydride to make formate, path 3 is a typical  $\text{CO}_2\text{RR}$  pathway where the adsorbed  $\text{CO}_2$  undergoes a hydration to produce formate, and path 4 shows the direct carbonate reduction mechanism. They further discuss that the dominant pathway is a function of potential. At lower potentials between 0.0 and  $-0.4$  V vs. RHE, the dominant species is  $^*\text{CO}_3^{2-}$  with only  $^*\text{H}$  competing for adsorption,

while  $^*\text{CO}_2^-$  and  $^*\text{OCO}^-$  adsorb at potentials more negative than  $-0.4$  and  $-0.8$  V vs. RHE, respectively. At potentials more negative than  $-0.8$  V vs. RHE, it is difficult to adsorb  $^*\text{OCO}^-$ , and also for path 2 the  $^*\text{H}^-$  intermediate is unstable and mostly dominated by HER. Thus the only relevant path for formate production is path 3 in medium potential ranges. At larger potentials it will converge to CO, which can further undergo chemical hydration to make formate. But, at potentials more negative than  $-0.8$  V vs. RHE the authors discuss that the  $^*\text{CO}$  is more likely to reduce to  $\text{C}_1$  and  $\text{C}_{2+}$  products limiting the further reduction to formate. However, in their study formate production pathway corresponds to path 4, which is through the direct  $\text{CO}_3^{2-}$  reduction. The first step in this pathway is to hydrogenate the adsorbed  $^*\text{CO}_3^{2-}$  into  $^*\text{HCO}_3^-$ , which further reacts with H to give formate, while  $\text{OH}^-$  is eliminated. In path 4, their proposed mechanism does not form CO which eliminates the possibility of forming any  $\text{C}_2$  products, as these products are primarily formed *via* CO–CO coupling. It provides a comprehensive insight into the heterogeneous mechanisms that can occur in  $\text{c-CO}_2\text{RR}$  systems, especially for the formate producing pathway.<sup>116</sup>

The DFT studies can be further supported by operando analysis, including Raman, FTIR, UV-vis. For example, to experimentally verify the reduction of carbonate, Ma *et al.* mounted a carbonate complex,  $\text{Cu}_2(\text{CO}_3)(\text{OH})_2$ , on a glassy carbon working electrode and studied the reduction with *in situ* Raman spectra. They observed that copper hydroxide bands of  $\text{Cu}_2(\text{CO}_3)(\text{OH})_2$  gradually disappear while the carbonate peaks become sharper. They concluded that the  $\text{Cu}_2(\text{CO}_3)(\text{OH})_2$  was first converted to carbonate. After 900 s of electrolysis, they observed that the carbonate band disappeared, and they attributed this to the direct reduction of carbonate on Cu electrode. They also observed that after electrolysis the color of the electrode changed from green to brown which is the color of metallic Cu. They also used the same  $\text{Cu}_2(\text{CO}_3)(\text{OH})_2$  mounted working electrode in a H-cell with a solution of 0.1 M KOH and they observed 1.01% of formate faradaic efficiency. Using this data, they solidify their claim of direct carbonate reduction. They describe the low faradaic efficiencies of formate as a result of the carbonate species detaching from the electrode driven by high HER activity. They also acknowledge that by introducing KOH and flowing  $\text{N}_2$  in their system they create conditions where the solution is free of dissolved  $\text{CO}_2$  which allows the study of carbonate reduction. In an analogous experiment with  $\text{PbCO}_3$  they observed a faradaic efficiency of 0.89% for formate. Their study concluded that  $\text{PbCO}_3$  can also be reduced in a similar mechanism to formate.<sup>116</sup>

Choi *et al.* investigated different transition metals, Ag, Au, Cu, and Sn, for direct reduction of ammonium carbamate. The binding energies of the protonated ammonium cation ( $\Delta E_{\text{NH}_4^+}$ , solid lines) and  $\text{CO}_2$ -captured carbamate anion ( $\Delta E_{\text{H}_2\text{NCO}_2^-}$ , dotted lines) were plotted as a function of potential for Ag, Au, Cu, and Sn as shown in Fig. 17. They investigated the potential of zero charge (PZC) of all the metals, which influences the electroadsorption properties in electrocatalysis, and

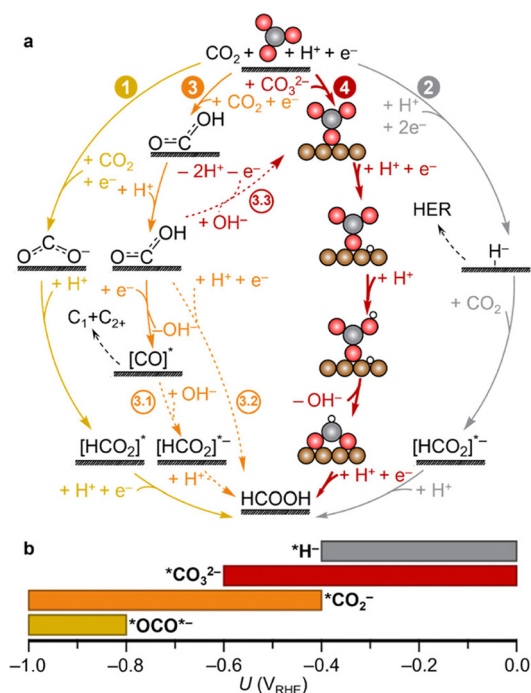


Fig. 16 (a) Reaction network of  $\text{eCO}_2\text{RR}$  and carbonate reduction mechanisms leading to  $\text{HCOOH}$ . The consensual  $\text{eCO}_2\text{RR}$  mechanisms to formate start by  $\eta_{\text{O}_2}$   $^*\text{OCO}^-$  (path 1) or by  $^*\text{H}^-$  (path 2) adsorptions. Additionally, path 3 leads to  $^*\text{CO}$  which can further evolve to  $\text{HCOOH}$  by hydration (path 3.1).  $^*\text{COOH}$  can also evolve to  $\text{HCOOH}$  (path 3.2). Path 4 is the newly proposed carbonate mechanism that can have contributions from path 3 through the conversion of the  $^*\text{COOH}$  intermediate (path 3.3). (b) Range of potential stability of different intermediates.<sup>116</sup> Reproduced with permission from ref. 116, copyright 2023 American Chemical Society.

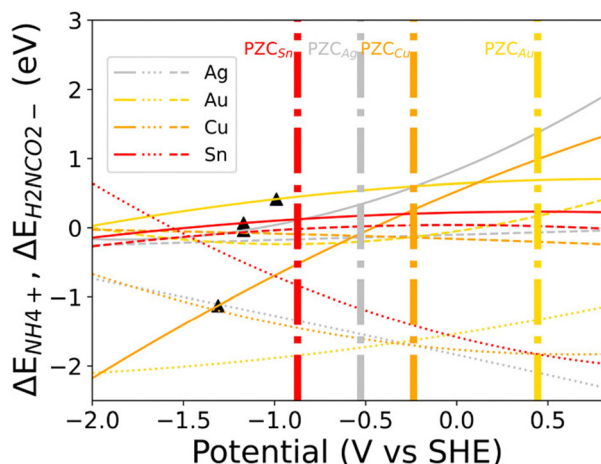


Fig. 17 The binding energies of ammonium cation  $\text{NH}_4^+$  ( $\Delta E_{\text{NH}_4^+}$ , solid lines) and carbamate anion  $\text{H}_2\text{NCO}_2^-$  ( $\Delta E_{\text{H}_2\text{NCO}_2^-}$ , dotted lines) as a function of potential for Ag, Au, Cu, and Sn. The potential of zero charge (PZC) for each metal is plotted with a vertical dash-dotted line. The applied potential to reach  $-12 \text{ mA cm}^{-2}$  in the c- $\text{CO}_2\text{RR}$  experiments conducted by Choi *et al.* is marked with a triangle on the respective  $\Delta E_{\text{NH}_4^+}$  curve.<sup>71</sup> Reproduced with permission from ref. 71, copyright 2024 American Chemical Society.

found that all the PZCs are more positive than the experimental applied potentials (black triangles). Therefore, they hypothesize that the solvated  $\text{NH}_4^+$  are preferentially accumulated on the surface of the electrode while the  $\text{H}_2\text{NCO}_2^-$  are repelled due to its negative charge. They further discussed that the binding energies  $\Delta E_{\text{NH}_4^+}$  is stronger than  $\Delta E_{\text{H}_2\text{NCO}_2^-}$  at the experimentally applied potentials, which limits the production of carbon based products.<sup>71</sup> Thus,  $\text{NH}_4^+$  will not only block the active sites but also serve as a proton source to promote HER, leading to the predominant production of hydrogen on all metals. Bringing the captured  $\text{CO}_2$  to the electrode surface while limiting HER activity from the capture agent is a major roadblock in c- $\text{CO}_2\text{RR}$  that needs to be overcome.

Thus, tuning the local reaction environment becomes particularly important for c- $\text{CO}_2\text{RR}$ , which can provide a sufficient supply of the active species while suppressing the unwanted HER. Along with the bulk speciation, the local speciation can also vary with  $\text{CO}_2$  loading, temperature, pH, electrochemical operating conditions and the cations, as shown in Fig. 18. The

Conditions under direct  $\text{CO}_2$  capture and conversion with high  $\text{CO}_2$  flux across G/L interface

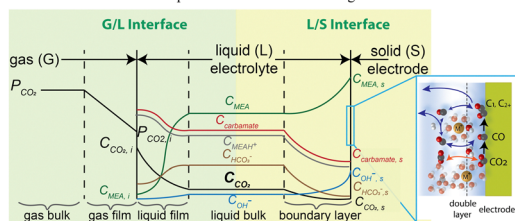


Fig. 18 Conceptual local reaction environment for  $\text{CO}_2$  loaded amine solutions. Speciation at the gas-liquid interface, electrolyte bulk and liquid-electrode interface.<sup>16</sup> Reproduced with permission from ref. 16, copyright 2023 Elsevier.

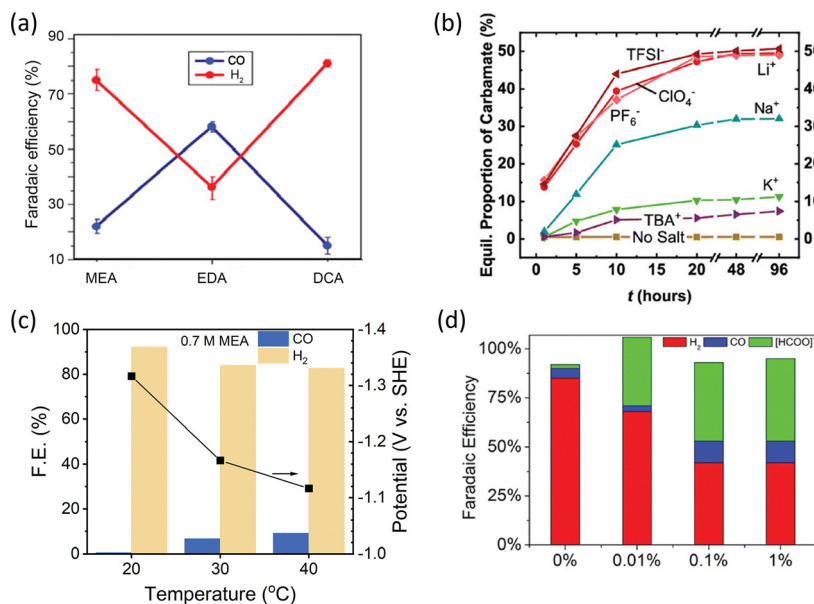
common ways deployed until now to alter the reaction environment in the presence of amine capture agents is by (i) changing the types and concentration of the amines, (ii) addition of alkali cations, (iii) increasing the temperature, or (iv) incorporating surfactants to suppress HER.

Abdinejad *et al.* used MEA, ethylenediamine (EDA) and decylamine (DCA) with a Cu electrocatalyst in 0.1 M  $\text{NaClO}_4$  solution for  $\text{CO}_2\text{RR}$  and observed that EDA gives the highest faradaic efficiency of CO which they attributed to the presence of two amine molecules that increases the capture efficiency of the system (Fig. 19a).<sup>117</sup> Similarly Shen *et al.* studied the activity for c- $\text{CO}_2\text{RR}$  with ammonium carbamate (AC) and MEA using a electrodeposited Ag catalyst and observed similar faradaic efficiency of CO for both capture agents.<sup>16</sup>

Few studies have investigated the addition of alkali cations as a way to increase selectivity towards  $\text{CO}_2$  conversion. Monteiro *et al.* investigated  $\text{CO}_2\text{RR}$  on Cu, Ag, and Au and showed that the presence of large alkali cations ( $\text{K}^+$  or  $\text{Cs}^+$ ) in particular can undergo weak hydration spheres that can be concentrated at the electrode surface and stabilise the  $\text{CO}_2^-$  intermediate *via* local electric field effect.<sup>119</sup> In an amine containing solution it can further enhance charge transfer and destabilise the formation of carbamate to enhance the C-O bond cleavage. Khurram *et al.* reported a high CO current density with alkali cations in a solution of 2-ethoxyethylamine (EEA) in dimethylsulphoxide (DMSO) for  $\text{CO}_2\text{RR}$  which depended on the size of the cations with  $\text{K}^+ < \text{Na}^+ < \text{Li}^+$ , and attributed the behaviour to the unstable carbamate formation in the presence of large cations with easier desolvation and rapid pairing kinetics (Fig. 19b).<sup>118</sup> As observed by Khurram *et al.* the size of the cations has an effect on the carbamate formation. With  $^1\text{H}$  NMR studies they showed that the proportion of carbamate formed in their solution was a function of the alkali cation present in their electrolyte. The Lewis acidity of the cations was found to dictate the amount of ammonium cation that will be formed. For alkali cations, the Lewis acidity decreases in the order  $\text{Li}^+ > \text{Na}^+ > \text{K}^+$ , and thus it was found that the stronger Lewis acid,  $\text{Li}^+$ , associates more strongly with the initial carbamic acid driving the reaction faster to the formation of carbamate. The interaction of the alkali cation with carbamate thus played a role in the binding of the cations to the carbamate anion. DFT studies also showed that the reaction of the carbamate anion with the alkali cations is spontaneous in decreasing order of  $\text{Li}^+ > \text{Na}^+ > \text{K}^+$ . The type of anion present in the electrolyte did not play any significant role in the formation of carbamate. Larger cations like  $\text{K}^+$  and  $\text{Cs}^+$  have been reported to be able to increase the availability of  $\text{CO}_2$  near the surface of the electrode in  $\text{CO}_2\text{RR}$  studies. The measurement of interfacial  $\text{CO}_2$  concentration for different alkali metal cations through *in situ* ATR-SEIRAS have also shown that  $\text{Li}^+$  has the highest  $\text{CO}_2$  concentration and  $\text{K}^+$  has the lowest  $\text{CO}_2$  concentration.<sup>120</sup> This is primarily because the hydration sphere of cations inversely scales with the size of the cations where  $\text{Li}^+ > \text{Na}^+ > \text{K}^+ > \text{Cs}^+$  which changes the local buffering capacity by changing the interfacial  $\text{pK}_a$ .<sup>121</sup> In contrast, for c- $\text{CO}_2\text{RR}$  larger cations can potentially help in reducing the







**Fig. 19** (a) Faradaic efficiency of CO and H<sub>2</sub> over Cu catalyst in 0.1 M NaClO<sub>4</sub> solution with MEA, ethylenediamine (EDA), and decylamine (DCA) at -0.78 V vs. RHE.<sup>117</sup> Reproduced with permission from ref. 117, copyright 2020 American Chemical Society (b) comparison of equilibrium population and concentration of alkali and tetrabutylammonium (TBA<sup>+</sup>) cations in CO<sub>2</sub>-loaded 0.1 M EEA in DMSO.<sup>118</sup> Reproduced with permission from ref. 118, copyright 2022 Royal Society of Chemistry (c) faradaic efficiency and applied potential during the electrochemical reduction of a 0.7 M MEA electrolyte with an Ag electrocatalyst at a fixed current density of 4 mA cm<sup>-2</sup> at an electrode rotation speed of 800 rpm.<sup>16</sup> Reproduced with permission from ref. 16, copyright 2023 Elsevier (d) product distributions of CO<sub>2</sub> reduction over indium catalyst at -0.8 V vs. RHE in CO<sub>2</sub>-saturated 30 wt% MEA aqueous solution with different concentrations of CTAB surfactant.<sup>89</sup> Reproduced with permission from ref. 89, copyright 2017 Wiley.

local pH of the system near the electrode, enabling the local release of CO<sub>2</sub> near the electrode from the captured-CO<sub>2</sub> adduct. This can help in reducing HER and promote c-CO<sub>2</sub>RR activity. In current c-CO<sub>2</sub>RR studies the local pH is alkaline and thus tuning the cations to maintain pH close to the pK<sub>a</sub> of the capture agents can help prevent the deprotonation of the amines and the shifting of equilibrium reactions locally.

Temperature studies were also investigated for c-CO<sub>2</sub>RR and it was seen that higher temperatures increases the faradaic efficiency of CO formation. Shen *et al.* and Kim *et al.*, investigated the temperature dependency and reached faradaic efficiency of ≈20–40% at higher temperatures which they attributed to the shift in equilibrium to have more free CO<sub>2</sub> in the system (Fig. 19c). The effect of surfactants on CO<sub>2</sub>RR has also been studied in 30 wt% MEA by Chen *et al.*, as they are known to reduce HER activity by blocking the active sites. Using CTAB they show that they can boost CO<sub>2</sub> conversion to formate and CO, primarily through HER suppression. They further show that a high concentration of CTAB (>0.1 wt%) helps in producing CO while a low concentration (0.01 wt%) was sufficient to promote CO in indium electrodes. The highest formate faradaic efficiency of 45.4% and CO faradaic efficiency of 17.0% was achieved when combined with porous In electrodes (Fig. 19d).<sup>89</sup>

Although these techniques have been mostly investigated under CO<sub>2</sub>RR conditions, the same ideas can be translated to c-CO<sub>2</sub>RR conditions. The interactions at the liquid-electrode interface can be tuned to increase the selectivity towards CO. The trimethylammonium alkyl tail in surfactants like CTAB can align itself at the surface of the electrode creating hydrophobic

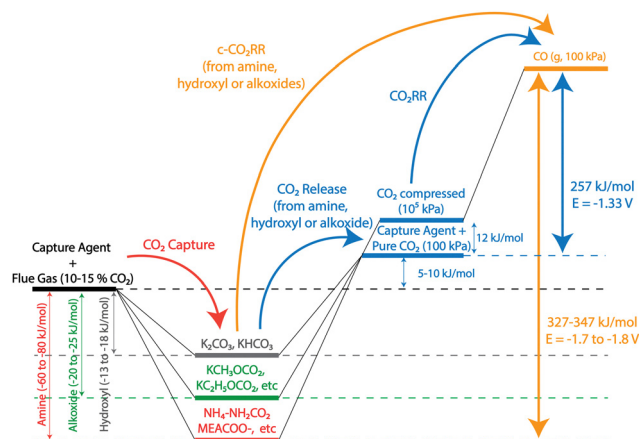
interactions that suppresses HER in c-CO<sub>2</sub>RR studies.<sup>122,123</sup> Similarly different sizes of alkali cations can also be combined with surfactants to alter the selectivity.<sup>124</sup> Larger cations like Cs<sup>+</sup> have been reported to be able to maintain a near neutral pH at the surface of the electrode increasing the availability of CO<sub>2</sub> in CO<sub>2</sub>RR studies.<sup>125–127</sup> In current c-CO<sub>2</sub>RR studies the local pH is alkaline and thus tuning the cations to maintain pH close to the pK<sub>a</sub> of the capture agents can help prevent the deprotonation of the amines and the shifting of equilibrium reactions locally. The use of ionomer coatings have also been studied to tailor micro-environments by controlling water and ion transport through the polymers. Ionomers like Nafion and Sustanion has shown that they can maintain a high local pH and CO<sub>2</sub> concentration to increase C<sub>2+</sub> products with Cu catalyst and CO with Ag catalyst.<sup>128–130</sup> In addition, pulsed electrolysis can also be investigated to increase CO selectivity.<sup>131</sup> The challenge in c-CO<sub>2</sub>RR systems is to bring the negatively charged carbamate species close to the cathode, which could be overcome by the pulsing technique. It can also reduce the local pH during the anodic cycle to shift the equilibrium and generate more carbamate species near the electrode that can potentially undergo reduction reactions.

## 6 Effect of different capture agents on c-CO<sub>2</sub>RR

Different capture agents behave differently under c-CO<sub>2</sub>RR conditions. So far only the changing binding energies and the CO<sub>2</sub> loading capacity have been investigated,<sup>16,61</sup> however it







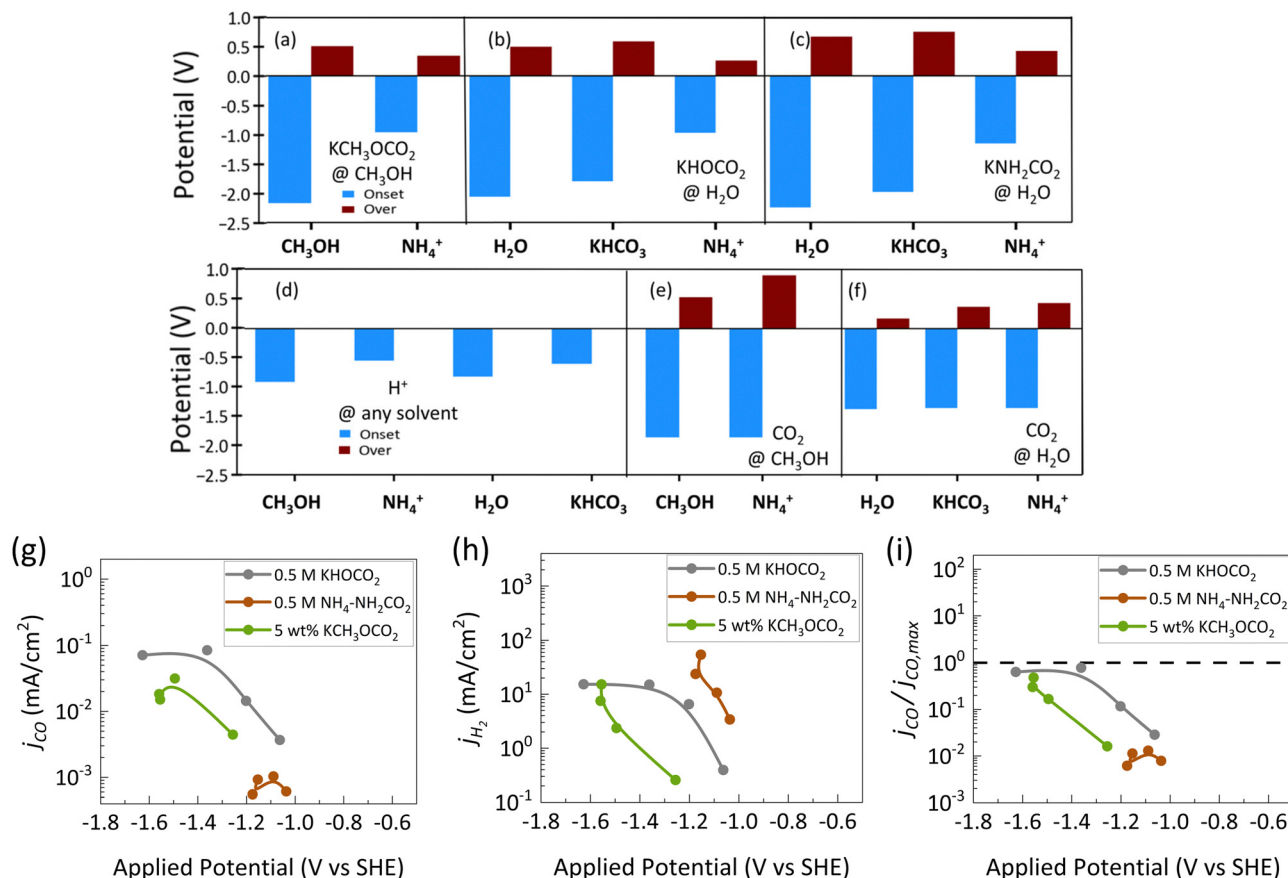
**Fig. 20** Conceptual thermodynamic free energy change comparing c-CO<sub>2</sub>RR and CO<sub>2</sub>RR of amine, hydroxyl and alkoxide capture agents. The free energy of capture of a dilute stream of flue gas in amine is  $-60$  to  $-80$  kJ mol<sup>-1</sup> (shown in red), in alkoxide is  $-20$  to  $-25$  kJ mol<sup>-1</sup> (shown in green), and in alkali hydroxyls is  $-13$  to  $-18$  kJ mol<sup>-1</sup> (shown in grey).<sup>31,45</sup> The extra steps of release and compression in CO<sub>2</sub>RR (shown in blue lines) are responsible for the inefficiencies in the conventional CO<sub>2</sub>RR system. Although the barriers to go from captured-CO<sub>2</sub> to reduced products are the same through the CO<sub>2</sub>RR and the c-CO<sub>2</sub>RR paths, the c-CO<sub>2</sub>RR process (shown in orange line) can facilitate the conversion in a one step process reducing the inefficiencies in the capture and conversion process.

needs to be understood that the mass transport conditions, thermodynamics of the captured-CO<sub>2</sub> adduct species and vapor-liquid equilibrium in different capture agents change at different conditions which needs due consideration. In theory, the best capture agent will be the one that has the minimum thermodynamic barrier to get reduced to products, but species with different equilibrium constants will have different rates of making CO<sub>2</sub> in the bulk of the solution that will further influence the products that we see. For instance, as shown in Fig. 20, from a thermodynamic standpoint it can be observed that CO<sub>2</sub> binding to the amines are the strongest which is around  $-60$ – $80$  kJ mol<sup>-1</sup> followed by alcohol based capture agents  $-20$  to  $-25$  kJ mol<sup>-1</sup>, followed by bicarbonates  $-13$  to  $-18$  kJ mol<sup>-1</sup>.<sup>31,45</sup> Thus when we talk about c-CO<sub>2</sub>RR, a larger thermodynamic barrier needs to be overcome while going from the carbamates to reduced products compared to the alkoxide based capture agents or the hydroxyl based capture agents. Furthermore, Appel *et al.* in their work showed that the partial pressure of CO<sub>2</sub> also determines the free energy of the CO<sub>2</sub>-bound adduct and dictates the thermodynamic potential required to make reduced products.<sup>132</sup> They further discuss that if the capture agent has the ability to bind CO<sub>2</sub> stronger than what is required from a specific dilute stream then the process could lead to inefficiencies from the excess binding energy. Thus the influence of these different binding energies on c-CO<sub>2</sub>RR is important to understand for future research in c-CO<sub>2</sub>RR.

To investigate these changes, Kowalski *et al.* used methoxide as a capture agent to determine its activity for c-CO<sub>2</sub>RR and compared it to hydroxyls and amine capture agents using a silver electrocatalyst. Through DFT calculations they show that

the nature of proton source and its pK<sub>a</sub> has a significant impact on the onset potentials for c-CO<sub>2</sub>RR. They hypothesized that a proton source with a low pK<sub>a</sub> and use of a solvent like methanol which has a low dielectric constant can improve c-CO<sub>2</sub>RR while penalizing the CO<sub>2</sub>RR. However, on Ag(111) surfaces they found that HER has a lower onset potential than CO<sub>2</sub>RR or c-CO<sub>2</sub>RR Fig. 21a–f, which is the dominant product also seen experimentally. As can be seen from (Fig. 21g and h), they measured the partial current density of CO and H<sub>2</sub> as a function of potential for all the three capture agents. In all cases, the partial current density of CO observed was very low with H<sub>2</sub> being the dominant product. For the ammonium carbamate, negligible amounts of CO were observed as it was more selective for H<sub>2</sub> evolution. The authors further normalized the partial current densities of CO observed to the limiting partial current density of CO to quantify the activity for c-CO<sub>2</sub>RR and determine the active species undergoing reduction. Using the method described in Section 3.3, they found that in all cases it was the free dissolved CO<sub>2</sub> that is getting reduced (Fig. 21i). They also discussed that alcohol based capture agents are promising as the only proton source in such systems is the alcohol itself compared to more Bronsted acidic HCO<sub>3</sub><sup>-</sup> or NH<sub>4</sub><sup>+</sup>. Thus it can suppress HER which is the bottleneck for c-CO<sub>2</sub>RR systems (Fig. 21b).<sup>12</sup> The work then needs to be combined with new catalyst design, moving away from Ag or other transition metals that are typically known for its good activity in CO<sub>2</sub>RR. Catalysts that are known to suppress HER to improve the activity for c-CO<sub>2</sub>RR are thus needed along with the ability to bring the negatively charged carbamate species to the surface of the electrode.

Alkanolamine solutions for CO<sub>2</sub> capture faces limitations with regard to high degradation rates, toxicity and high regeneration energy requirements. More recently amino acids have been proposed as an alternative to circumvent these challenges. Amino acids have advantages of low toxicity, low corrosivity, fast capture kinetics with CO<sub>2</sub>, and good resistance to oxidative and thermal degradation. Ramezani *et al.* compared different amino acid salts at different conditions to position their effectiveness with respect to alkanolamines, MEA in particular.<sup>133</sup> In their comparison, they reported that amino acid salts like K-Lys (lysine), K-Pro (proline), and K-Sar (sarcosinate) have higher pK<sub>a</sub> and higher CO<sub>2</sub> loading capacity than MEA. The high pK<sub>a</sub> of these salts makes the carbamate unstable and facilitates the formation of carbonates and bicarbonates which in turn reduces the heat of absorption in these systems. They further report that the CO<sub>2</sub> absorption rate increased as the temperature and concentration of the amino acid salt increased. Thus, the advantages of amino acids makes them favorable for c-CO<sub>2</sub>RR. The challenge in c-CO<sub>2</sub>RR systems with amines is the strong binding of the CO<sub>2</sub> in the form of stable carbamates that makes it hard to directly reduce the CO<sub>2</sub>-bound adduct. From the investigation of Ramezani *et al.*, it was observed that the absorption rate and the desorption rate can be tuned by using smaller chains of amino acids that reduces the distance between the amino and the carboxyl groups. This along with sterically hindered amino acids can slow down the absorption



**Fig. 21** Calculated onset potential (blue, vs. SHE) and over-potential (brown) for the electroreduction of (a) methyl carbonate  $\text{KCH}_3\text{OCO}_2$ , (b) bicarbonate  $\text{KHOCO}_2$ , (c) carbamate  $\text{KNH}_2\text{CO}_2$  on Ag(111) using the various solvent-proton source combinations of  $\text{CH}_3\text{OH}$  and  $\text{H}_2\text{O}$ . The compound being electrochemically reduced is labeled in the top right of each panel, together with the solvent (notation: compound@solvent). The x axis denotes the proton source. Values for (d) HER, (e)  $\text{CO}_2\text{RR}$  in  $\text{CH}_3\text{OH}$  solvent, and (f)  $\text{CO}_2\text{RR}$  in  $\text{H}_2\text{O}$  solvent are also given for comparison. Onset potential is defined as the least negative potential lower than the equilibrium potential at which the ES becomes equal to 0.75 eV, while the overpotential is equal to the difference between the equilibrium potential and the onset potential. The pathway that has the smallest onset potential is displayed. Partial current densities of (g) CO and (h)  $\text{H}_2$  and (i) CO with respect to the maximum  $\text{CO}_2$  flux as a function of applied potential. Three  $\text{CO}_2$ -captured complexes are considered:  $\text{KHOCO}_2$  (bicarbonate),  $\text{NH}_4\text{-NH}_2\text{CO}_2$  (ammonium carbamate) and  $\text{KCH}_3\text{OCO}_2$  (methyl carbonate).<sup>12</sup> Reproduced with permission from ref. 12, copyright 2024 American Chemical Society.

rate and enhance the desorption rate due to the bulkier substituent group (Fig. 22a).<sup>133</sup> For instance, K-Asp (asparagine), K-Tau (taurate), K-Ser (serine), K-Arg (arginine), K-Cys (cysteine), and K-Glu (glutamine) showed faster desorption rate than MEA and can be promising candidates for c- $\text{CO}_2\text{RR}$  (Fig. 22b). Thus for c- $\text{CO}_2\text{RR}$  it is important to achieve a balance between absorption and desorption kinetics to optimize the conversion.

Although amine capture agents are the state of the art for postcombustion capture processes due to its high capture efficiency, most c- $\text{CO}_2\text{RR}$  studies only show dissolved  $\text{CO}_2$  as the active species getting reduced. Selecting capture agents for c- $\text{CO}_2\text{RR}$  thus becomes more complicated. Amine capture agents binds to  $\text{CO}_2$  via chemical absorption, however if dissolved  $\text{CO}_2$  is the main species getting reduced then other solvents, for instance the ones used in precombustion  $\text{CO}_2$  capture via physical absorption, can also be explored. Physical solvents exhibit characteristics such as low vapor pressure, high reactivity or absorptivity, facile regeneration, high thermal and mechanical resilience, minimal corrosiveness,

and minimal environmental impact which proves ideal for  $\text{CO}_2$  capture.<sup>134,135</sup> Such solvents also possess exceptional thermal stability, mitigating the risk of solvent loss and contamination while regenerating at elevated temperatures. Commercially available physical processes for CCS encompass selsol (dimethyl ether of polyethylene glycol (DMPEG)), rectisol (methanol), purisol (*N*-methyl-2-pyrrolidone (NMP)), morphysorb, sulfolane (tetrahydrothiophenedioxide), and fluor (propylene carbonate) solvent.<sup>136,137</sup> Selsol (a liquid glycol solvent) stands out among these processes, having been widely utilized in  $\text{CO}_2$  capture for decades. Its advantages over other physical solvents include lower vapor pressure, non-corrosive properties, reduced heat requirements, and inertness towards select gases.<sup>138</sup>

c- $\text{CO}_2\text{RR}$  can pose challenges on stability depending on the capture agent that is being used.  $\text{CO}_2$  capture solutions consist of several species that coexist in the solution which can trigger the interaction between the catalyst and the capture solution resulting into side reactions. There have been reports of



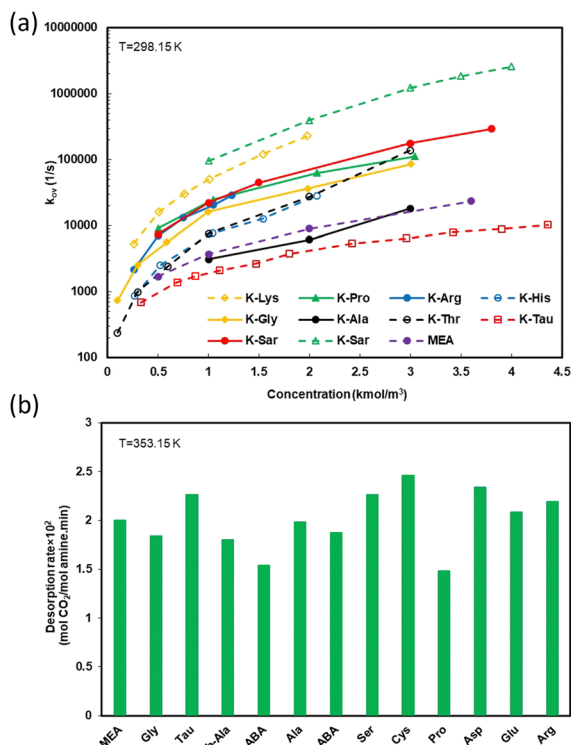


Fig. 22 (a) The overall rate constant for CO<sub>2</sub> absorption as a function of concentration for different amino acid salts at 298.15 K. (b) The desorption rate of 1 M potassium salts of different amino acid at 353.15 K. K-Lys: potassium lysine, K-Pro: potassium proline, K-Arg: potassium arginine, K-His: potassium histidine, K-Gly: potassium glycine, K-Ala: potassium alanine, K-Thr: potassium threonine, K-Tau: potassium taurate, K-Ser: potassium serine, K-Sar: potassium sarcosinate, and MEA: monoethanolamine.<sup>133</sup> Reproduced with permission from ref. 133, copyright 2022 De Gruyter.

morphological changes and corrosion of metal electrodes under c-CO<sub>2</sub>RR conditions.<sup>71</sup> Thus, understanding the vapor-liquid equilibrium models and linking them with electrochemical c-CO<sub>2</sub>RR is important to determine the concentration of different species present in the capture solution and identify the species getting reduced or causing the instability of the catalyst. Recent studies have reported that direct reduction of CO<sub>2</sub>-capture solutions undergoes high HER.<sup>12,61,71</sup> For instance, in amine capture solution the protonated amines contribute to the high HER. This reduces the generation of carbon products favoring the side reaction of HER. Therefore, according to the reported studies, the reduction of CO<sub>2</sub>-bound complex is not favored at the electrode surface. In addition, catalysts like Cu which is known to produce multi carbon products in CO<sub>2</sub>RR have been reported to undergo corrosion in the presence of amine capture agents, whereas catalysts like Au and Ag have been reported to be relatively stable and inert to corrosion.<sup>71</sup> In the presence of ammonia, Cu was reported to be able to form ligands with the free amines in the solution to form copper-ammonia complex. This is possible even at reductive potential, making Cu not suitable for c-CO<sub>2</sub>RR with amine capture agents.<sup>139</sup> Many other mechanisms have been proposed for cathodic corrosion, including cathodic etching in both aqueous and non-aqueous solutions, formation of

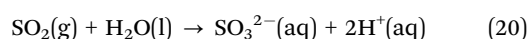
(meta)stable metal hydrides at the cathode as possible intermediates that eventually are released from the cathode, and leaching due to the interaction of alkali metals with the cathode. These would also need to be investigated as new capture agents are developed to determine the stability of the catalysts (*Chem. Rev.*, 2021, **121**(17), 10241–10270). This requires a deep understanding of the degradation and restructuring mechanisms of the catalyst along with an understanding of the transport of different species during electrocatalysis to be able to develop strategies to mitigate these processes.

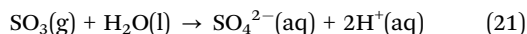
## 7 Effect of impurities on electrochemical c-CO<sub>2</sub>RR

Industrial flue gas contains contaminants like NO<sub>x</sub>, SO<sub>x</sub> and O<sub>2</sub> that should be considered while developing c-CO<sub>2</sub>RR technologies. Several challenges have been identified by researchers on the impact of impurities for CO<sub>2</sub>RR that includes identifying catalysts that can maintain high selectivity and activity and designing suitable reactor configurations for viable operation. The presence of O<sub>2</sub> which is 25 times less soluble in water than CO<sub>2</sub> at STP conditions can result in significant loss of current density to oxygen reduction reaction (ORR). The lower standard reduction potential due to lower thermodynamic requirements and higher kinetic favorability promotes ORR compared to CO<sub>2</sub>RR. Furthermore, the higher diffusion rate of O<sub>2</sub> compared to CO<sub>2</sub> also plays a role in changes observed in selectivity. O<sub>2</sub> can also oxidize the catalyst leading to changes in the oxidation state of the catalyst during catalytic turnover or lead to corrosion. To prevent catalyst oxidation and maintain CO<sub>2</sub>RR selectivity, strategies like deploying ionomer coatings which are hydrophilic in nature have been suggested.<sup>140</sup> Hydrophilic nanopores have been argued to reduce the mass flux of O<sub>2</sub> in to the electrode as the O<sub>2</sub> needs to diffuse in the electrolyte-wet form, while the CO<sub>2</sub> mass flux have been observed to not have any significant difference from different ionomer coatings. Hydrophilic support of TiO<sub>2</sub> has also been proposed by Xu *et al.* that has shown to impede the effects of O<sub>2</sub> an undergo stable CO<sub>2</sub>RR.<sup>141</sup>

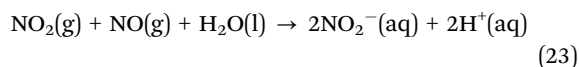
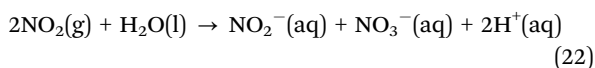
NO<sub>x</sub> and SO<sub>x</sub> impurities in flue gas have high solubility in water which dissolve to form acids in the solution as described in eqn (20)–(23). The formation of acids lowers the pH of the solution which then leads to increased HER, lowering the current densities for CO<sub>2</sub>RR. Both NO<sub>2</sub> and SO<sub>2</sub> also can adversely react with the catalyst to poison its surface and reduce the activity of the catalyst.<sup>142,143</sup> NO<sub>2</sub> concentrations above 1600 ppm have been shown to reduce the CO<sub>2</sub>RR faradaic efficiency on Cu catalyst. Similar results have been observed for SO<sub>2</sub> on Cu catalysts. However, exception to this poisoning effect have been observed when using Ag or Sn catalysts. This has been attributed to the fact that they form Ag<sub>2</sub>S and SnS<sub>2</sub> during CO<sub>2</sub>RR which are both thermodynamically unstable.<sup>144</sup>

SO<sub>x</sub> dissolution:





NO<sub>x</sub> dissolution:



Therefore, similar effects could be observed in c-CO<sub>2</sub>RR. In the presence of O<sub>2</sub>, c-CO<sub>2</sub>RR which has a higher thermodynamic barrier than CO<sub>2</sub>RR, will result in even higher thermodynamic unfavorability while competing with ORR compared to CO<sub>2</sub>RR, unless the oxidized catalyst surface is a better catalyst for the absorption and activation of the CO<sub>2</sub>-bound adduct. Similarly, as alkaline environments are preferred for CO<sub>2</sub> capture, unreacted NO<sub>x</sub> and SO<sub>x</sub> could accumulate in the capture agent and reduce the capture efficiency by lowering the pH of the capture solution resulting in lower CO<sub>2</sub> loadings. Therefore, the system will have lower concentrations of CO<sub>2</sub>-bound adducts in the presence of SO<sub>x</sub> and NO<sub>x</sub> that can eventually be electrochemically reduced. However, there are instances where Ag and Sn have been reported to be stable in SO<sub>2</sub> impurities. Therefore, for c-CO<sub>2</sub>RR catalysts which have stable activity and selectivity in the presence of impurities will be important to identify.

## 8 Energy comparison of CO<sub>2</sub>RR vs. c-CO<sub>2</sub>RR

The energy benefits of c-CO<sub>2</sub>RR can be extrapolated by comparing them with state-of-the-art CO<sub>2</sub> electrolyzers. Most high-performance CO<sub>2</sub> electrolyzer designs are inspired from the fuel cell community and are developed as zero-gap gas-fed electrolyzers to maximize the CO<sub>2</sub> transport to the electrode and thus enable their operation at high current densities. These electrolyzers can typically operate at current densities higher than 100 mA cm<sup>-2</sup> with a cell voltage of 3–3.5 V to make CO with a faradaic efficiency as high as 90%. Thus, these typically require 600–700 kJ mol<sup>-1</sup> of energy to operate at standard temperature and pressure conditions. However, energy penalties lie at the anode where the bicarbonates or carbonate salts can be converted to CO<sub>2</sub> which requires at least 254 kJ mol<sup>-1</sup> and therefore the CO<sub>2</sub> utilization rate is typically low in CO<sub>2</sub> electrolyzers (Fig. 23).<sup>145</sup>

Compared to the CO<sub>2</sub> electrolyzers, although the current c-CO<sub>2</sub>RR system requires significantly higher energy (800–10 000 kJ mol<sup>-1</sup>), primarily because of the low CO production and high HER. Therefore, as discussed earlier, improving the CO production rates remains a challenge and addressing which can improve the energy requirements of c-CO<sub>2</sub>RR systems. This requires fundamental insights on reaction environments, catalysts activity and stability, and influence of different capture agents to optimize the c-CO<sub>2</sub>RR system. However, as reported by Li *et al.*, considering that the c-CO<sub>2</sub>RR system can achieve similar faradaic efficiencies and current densities at similar cell

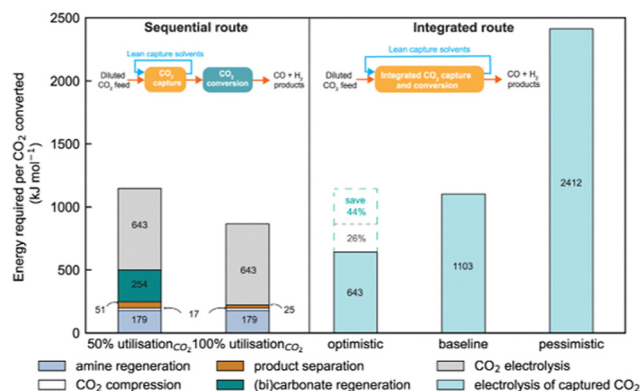


Fig. 23 Energy comparison between the sequential route (conventional CO<sub>2</sub>RR route) vs. the integrated route (the c-CO<sub>2</sub>RR route).<sup>33</sup> The optimistic scenario assumes that c-CO<sub>2</sub>RR performs at the same efficiency as the current state-of-the-art CO<sub>2</sub> electrolyzers with a 90% F.E. CO at cell potential of 3 V, the baseline scenario uses Lee *et al.*'s report of 72% F.E. CO at −0.8 V vs. RHE,<sup>28</sup> and the pessimistic scenario assumes a 40% F.E. CO at a large cell potential of 5 V. Reproduced with permission from ref. 33, copyright 2022 Nature.

voltage as the CO<sub>2</sub> gas-fed electrolyzers, there is a potential of saving 44% of the total energy required (Fig. 23). This saving is due to the fact that c-CO<sub>2</sub>RR can save energy costs arising from capture agent regeneration, CO<sub>2</sub> compression, and product purification needed in conventional CO<sub>2</sub> reduction process.<sup>33</sup>

## 9 Conclusion and future outlook

The long term development of c-CO<sub>2</sub>RR technologies possesses many challenges that needs to be overcome to make this technology industrially viable. Along with the coupled effects of transport, kinetics, and thermodynamics that plays a role in c-CO<sub>2</sub>RR development, recent studies have reported corrosion and restructuring of the catalyst in the presence of amines as a crucial obstruction to further technology development.<sup>71</sup> The activity and stability of the transition metal catalyst that were known for CO<sub>2</sub>RR thus do not apply to c-CO<sub>2</sub>RR anymore. Furthermore, alkoxide capture agents showed promise in suppressing HER, but the reaction when looked from the anodic half would probably oxidize the methyl carbonate to give back CO<sub>2</sub>, thus eliminating the purpose of c-CO<sub>2</sub>RR. Thus finding a combination of suitable capture agent, catalyst and operating condition is needed to advance the development of c-CO<sub>2</sub>RR. Although, the use of VLE models, effect of thermodynamic barriers, high HER, catalyst stability are discussed for selected capture agents, similar concepts and understanding are relevant for all capture agents that are used for c-CO<sub>2</sub>RR.

To advance research in c-CO<sub>2</sub>RR the integration of capture agent, operando characterization, catalyst discovery, and reactor and catalyst design needs to be simultaneously investigated for achieving c-CO<sub>2</sub>RR and for potential scale-ups (Fig. 24). The selection of capture agents will determine the binding energy of CO<sub>2</sub> to the capture agent and the thermodynamic energetic barriers relevant for direct reduction of the captured CO<sub>2</sub>-





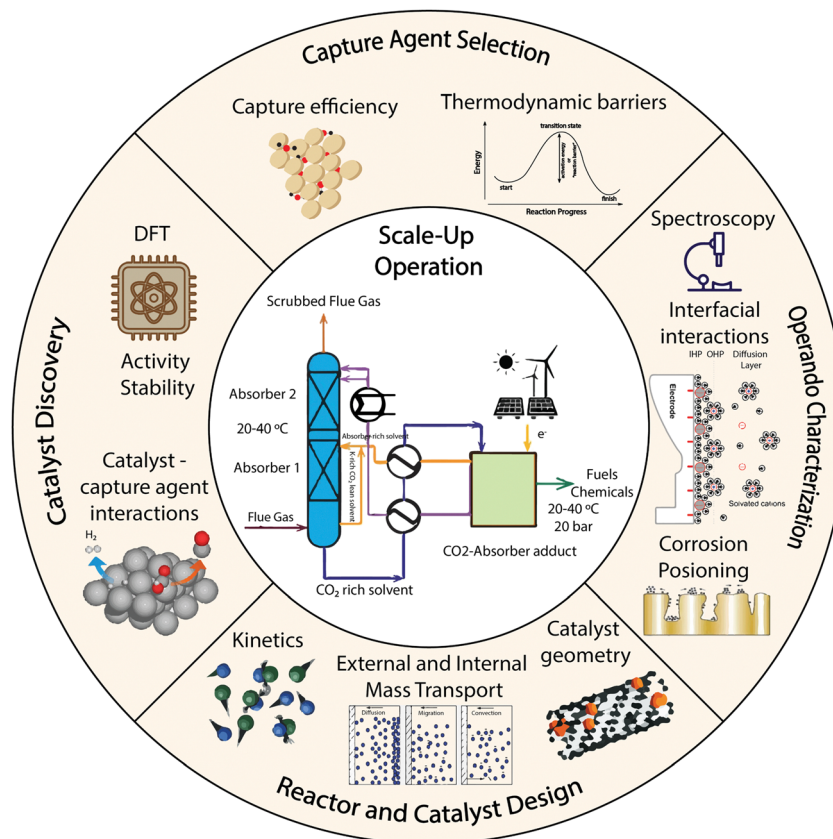


Fig. 24 Illustration showing the screening loop between capture agent discovery, catalyst discovery, reactor and catalyst design principles, and operando characterization that needs to be investigated for the eventual scale-up of c-CO<sub>2</sub>RR systems.

bound adduct. Catalyst discovery will involve investigating different catalysts for activity and stability under c-CO<sub>2</sub>RR by leveraging the use of both DFT calculations and experiments. These findings will further need to be linked with operando characterization to gain insights into the morphology, composition, crystallographic structural information to correlate experimental and theoretical results. Reactor and catalyst design also needs to be investigated in parallel to tune external and internal mass transport properties of the system and facilitate selectivity towards c-CO<sub>2</sub>RR. This screening loop of finding activity, stability and design descriptors for c-CO<sub>2</sub>RR is also beneficial to determine and address system-level challenges and accelerate the development of c-CO<sub>2</sub>RR processes (Fig. 24).

Most literature on c-CO<sub>2</sub>RR reported C<sub>1</sub> products, more specifically, CO. Table 1 summarizes the recent works on c-CO<sub>2</sub>RR. As the field evolves strategies for producing C<sub>2+</sub> products should be explored. Currently, several challenges lie in c-CO<sub>2</sub>RR which should be investigated to gain more fundamental insight into the process. These include the higher thermodynamic barrier to reduce captured CO<sub>2</sub>-adduct, high HER, and identifying the carbon source getting reduced during electrolysis. Furthermore, catalysts like Cu which are known for producing multi carbon products undergo corrosion and restructuring when amines are used as capture agents.<sup>65</sup> However, as reported by Choi *et al.*, transition metals like Au and Ag

do not undergo corrosion in the presence of amines.<sup>71</sup> These metals are known for producing CO with faradaic efficiencies as high as 90% which perhaps explain why only C<sub>1</sub> products have been observed. The understanding of corrosion mechanisms, which is one of the key bottlenecks in using catalysts like Cu in c-CO<sub>2</sub>RR needs to be addressed. Inhibiting cathodic corrosion can be achieved with the use of additives to tailor the electrical double layer or by alloying to alter the physico-chemical properties of the cathode. The addition of (poly)cationic ammonium salts can prevent the formation of parasitic hydrogen and corroding compounds in the double layer. Alloying can change the electronic band structure which can result in lower interaction between the cathode and the corrosive species or increase the energy barrier for reaction with the corrosion intermediates. The ternary alloy of CuSn<sub>7</sub>Pb<sub>15</sub> has been shown to be physically and chemically stable towards the formation of formate in electroreduction of CO<sub>2</sub> and can be employed in amine-based solvents in c-CO<sub>2</sub>RR.<sup>146</sup> Therefore, a combination of design strategies is necessary for eventually extending the space of c-CO<sub>2</sub>RR towards C<sub>2+</sub> products.

In addition to the following, developing anodes for the captured CO<sub>2</sub> media will guide the development of c-CO<sub>2</sub>RR technologies. Water oxidation reaction at the anode is kinetically sluggish and can lead to lower efficiency of the electrochemical reactor. Thus, choosing a catalyst that is thermodynamically favorable to water oxidation can improve the overall system efficiency.



**Table 1** Summary of electrolyzer design, capture agent, catalyst, and c-CO<sub>2</sub>RR performance in heterogeneous electrocatalysis. (All the chemical names are provided under the acronym section)

| Reactor                              | CO <sub>2</sub> capture agent                | Catalyst           | Supporting electrolyte      | Gas flow        | c-CO <sub>2</sub> RR performance                                        | Ref.                                 |
|--------------------------------------|----------------------------------------------|--------------------|-----------------------------|-----------------|-------------------------------------------------------------------------|--------------------------------------|
| Zero-gap membrane electrode assembly | 5 M MEA                                      | Ni–N/C             | —                           | Ar              | F.E. CO: 78.3%<br>$j_{\text{CO}}$ : 2.6 mA cm <sup>−2</sup>             | Kim <i>et al.</i> <sup>15</sup>      |
|                                      | 5 M MEA                                      | Ag                 | —                           | Ar              | F.E. CO: 38.3<br>$j_{\text{CO}}$ : 0.79 mA cm <sup>−2</sup>             | Kim <i>et al.</i> <sup>15</sup>      |
| Compression cell                     | 0.1 M MEA                                    | Ag                 | 0.1 M KHCO <sub>3</sub>     | CO <sub>2</sub> | $j_{\text{CO}}$ : 6 mA cm <sup>−2</sup>                                 | Safipour <i>et al.</i> <sup>17</sup> |
|                                      | 0.2 M MEA                                    | Ag                 | 0.1 M KHCO <sub>3</sub>     | CO <sub>2</sub> | $j_{\text{CO}}$ : 3 mA cm <sup>−2</sup>                                 |                                      |
| H-cell                               | 2 M MEA, 2 M BAPN, 2 M <i>n</i> -BA,         | Ag                 | 2 M KCl                     | N <sub>2</sub>  | F.E. CO: 1–20%<br>$j_{\text{CO}}$ : 0.01–1 mA cm <sup>−2</sup>          | Leverick <i>et al.</i> <sup>61</sup> |
|                                      | 2 M 2A1P, 2 M AMP, 2 M DMAE                  | Ag                 |                             |                 |                                                                         |                                      |
| RCE reactor                          | 0.2 M and 0.7 M AC, 0.2 and                  | Ag                 | 0.099 M KClO <sub>4</sub> + | Ar              | F.E. CO: 1–9%<br>$j_{\text{CO}}$ : 0.01–0.4 mA cm <sup>−2</sup>         | Shen <i>et al.</i> <sup>16</sup>     |
| RCE reactor                          | 0.7 M MEA, 0.2 M and 0.7 M KHCO <sub>3</sub> | Ag                 | 0.001 M KOH                 | Ar              | F.E. CO: 0.01–1.68%<br>$j_{\text{CO}}$ : 0.001–0.28 mA cm <sup>−2</sup> | Kowalski <i>et al.</i> <sup>12</sup> |
|                                      | 0.5 M AC, 0.5 M KHCO <sub>3</sub> ,          | Ag                 | 0.099 M KClO <sub>4</sub> + | Ar              | F.E. CO: ≈0.01%<br>$j_{\text{CO}}$ : 12 mA cm <sup>−2</sup>             |                                      |
| RCE reactor                          | 5 wt% methoxide                              |                    | 0.001 M KOH                 |                 |                                                                         |                                      |
|                                      | 0.2 M AC                                     | Cu, Ag, Au, Sn, Ti | 0.099 M KClO <sub>4</sub> + | Ar              | F.E. CO: 10%<br>$j_{\text{CO}}$ : 0.6 mA cm <sup>−2</sup>               | Choi <i>et al.</i> <sup>71</sup>     |
| Three electrode configuration        | 2 M MEA                                      | Ag                 | 2 M KCl                     | N <sub>2</sub>  | F.E. CO: 10%<br>$j_{\text{CO}}$ : 0.6 mA cm <sup>−2</sup>               | Lee <i>et al.</i> <sup>28</sup>      |
| Three electrode configuration        | 2 M MEA                                      | Ag                 | 2 M KCl                     | N <sub>2</sub>  | F.E. CO: 10%<br>$j_{\text{CO}}$ : 0.6 mA cm <sup>−2</sup>               | Lee <i>et al.</i> <sup>28</sup>      |
| H-cell                               | 0.05 M K <sub>2</sub> CO <sub>3</sub>        | Cu                 | —                           | N <sub>2</sub>  | F.E. HCOO <sup>−</sup> : 0.61%                                          | Ma <i>et al.</i> <sup>116</sup>      |

Furthermore, the loss of CO<sub>2</sub> from the anode during c-CO<sub>2</sub>RR should be at similar rates as CO<sub>2</sub>RR considering a similar acidic microenvironment is generated at the anode during water oxidation. However, there could be added complexities to the development of catalyst materials for the anode for c-CO<sub>2</sub>RR. Cathodic corrosion that has been observed in c-CO<sub>2</sub>RR conditions, especially with Cu electrode in amine solutions, can occur at the anode too. Therefore, catalysts that are compatible with the CO<sub>2</sub>-captured complex are needed to be identified to prevent any anodic corrosion. Pt so far has been used for different c-CO<sub>2</sub>RR studies as the anode, but their stability in these capture solutions has not been investigated. Additionally, cheaper alternatives are required and needs to be tested for industrial scale electrolyzers that can operate at overpotentials similar to Pt.

Integrated CO<sub>2</sub> capture and conversion possesses benefits in terms of energy and capital cost, however there may be trade-offs when trying to implement the capture and conversion in one unit. In current carbon capture and utilization processes, the CO<sub>2</sub> is fed in a compressed form which increases the conversion efficiency of CO<sub>2</sub> compared to if the whole process takes place at room temperature and atmospheric pressure. Thus the current technologies still outcompetes the conversion efficiency of c-CO<sub>2</sub>RR. Until now c-CO<sub>2</sub>RR technologies have mostly focused on batch mode of operation, and thus continuous mode of operation will simultaneously have to be investigated and compared with the current state-of-the-art conversion efficiency.<sup>147</sup> Also, point sources of CO<sub>2</sub> has a wide range of gas temperature, CO<sub>2</sub> concentration, and contaminants which must also be explored during the development phase. A typical c-CO<sub>2</sub>RR system should be stable for thousand of hours at high current densities and operating in a continuous mode of operation.<sup>11</sup>

In addition to performance, the development of c-CO<sub>2</sub>RR can further be coupled with life-cycle and techno-economic analysis (TEA) analysis in parallel keeping in mind future

viability. Li *et al.* in their work compared the TEA of a conventional CCU process to the integrated route of c-CO<sub>2</sub>RR. They found that at the current level of technology development there is no foreseen advantage of using the integrated route as the energy cost of converting captured CO<sub>2</sub> to products is higher. This offsets the cost reduced from process intensification. Also due to higher cost of electricity than heat, the integrated route further uses up more costs. However in an optimistic scenario, where c-CO<sub>2</sub>RR reaches the same performance in terms of current density and faradaic efficiency, the overall energy can be reduced by 44% with a 22% savings in energy cost.<sup>33</sup> Thus the development of c-CO<sub>2</sub>RR technologies is an attractive option for closing the carbon cycle using renewable electricity.

## Acronym

|                                |                       |
|--------------------------------|-----------------------|
| MEA                            | Monoethanolamine      |
| AC                             | Ammonium carbamate    |
| BAPN                           | β-Aminopropionitrile  |
| <i>n</i> -BA                   | <i>n</i> -Butylamine  |
| 2A1P                           | 2-Amino-1-propanol    |
| AMP                            | Aminomethyl propanol  |
| DMAE                           | Dimethylethanolamine  |
| DEA                            | Diethanolamine        |
| MDEA                           | Methyldiethanolamine  |
| KHCO <sub>3</sub>              | Potassium bicarbonate |
| K <sub>2</sub> CO <sub>3</sub> | Potassium carbonate   |
| KClO <sub>4</sub>              | Potassium perchlorate |

## Data availability

The review article consists of information and research findings which are already published in peer-reviewed journals. All



the necessary citations are included in the main article and permission for reproducing the figures are also obtained.

## Conflicts of interest

There are no conflicts to declare.

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