

# Green Chemistry

Cutting-edge research for a greener sustainable future

[rsc.li/greenchem](https://rsc.li/greenchem)



ISSN 1463-9262

## TUTORIAL REVIEW

Houqian Li, George W. Huber *et al.*  
Expanding plastics recycling technologies: chemical aspects,  
technology status and challenges



Cite this: *Green Chem.*, 2022, **24**, 8899

# Expanding plastics recycling technologies: chemical aspects, technology status and challenges†

Houqian Li,<sup>a</sup> Horacio A. Aguirre-Villegas,<sup>b</sup> Robert D. Allen,<sup>c,d</sup> Xianglan Bai,<sup>e</sup> Craig H. Benson,<sup>f</sup> Gregg T. Beckham,<sup>g</sup> Sabrina L. Bradshaw,<sup>f</sup> Jessica L. Brown,<sup>e,g</sup> Robert C. Brown,<sup>h</sup> Victor S. Cecon,<sup>h</sup> Julia B. Curley,<sup>c,d</sup> Greg W. Curtzweiler,<sup>h</sup> Son Dong,<sup>i</sup> Soumika Gaddameedi,<sup>j</sup> John E. García,<sup>a</sup> Ive Hermans,<sup>a,i</sup> Min Soo Kim,<sup>a</sup> Jiaze Ma,<sup>a</sup> Lesli O. Mark,<sup>i</sup> Manos Mavrikakis,<sup>a</sup> Olumide O. Olafasakin,<sup>e</sup> Tim A. Osswald,<sup>k</sup> Konstantinos G. Papanikolaou,<sup>a</sup> Harish Radhakrishnan,<sup>e</sup> Marco Antonio Sanchez Castillo,<sup>l</sup> Kevin L. Sánchez-Rivera,<sup>a</sup> Khairun N. Tumu,<sup>h</sup> Reid C. Van Lehn,<sup>a</sup> Keith L. Vorst,<sup>h</sup> Mark M. Wright,<sup>e</sup> Jiayang Wu,<sup>a</sup> Victor M. Zavala,<sup>a</sup> Panzheng Zhou<sup>a</sup> and George W. Huber<sup>a\*</sup>

Less than 10% of the plastics generated globally are recycled, while the rest are incinerated, accumulated in landfills, or leak into the environment. New technologies are emerging to chemically recycle waste plastics that are receiving tremendous interest from academia and industry. Chemists and chemical engineers need to understand the fundamentals of these technologies to design improved systems for chemical recycling and upcycling of waste plastics. In this paper, we review the entire life cycle of plastics and options for the management of plastic waste to address barriers to industrial chemical recycling and further provide perceptions on possible opportunities with such materials. Knowledge and insights to enhance plastic recycling beyond its current scale are provided. Outstanding research problems and where researchers in the field should focus their efforts in the future are also discussed.

Received 12th July 2022,  
Accepted 5th September 2022

DOI: 10.1039/d2gc02588d

rsc.li/greenchem

## 1. Introduction

Plastics have revolutionized our society, allowing us to inexpensively make a variety of materials that have a myriad of uses throughout industry. The first three synthetic plastics were polystyrene (PS) in 1839, polyvinyl chloride (PVC) in 1835 and Bakelite in 1907.<sup>1</sup> Industrial plastic production really began to expand in about 1950 when global plastic production reached 2 million tons per year.<sup>2</sup> Current global plastic production is around 380 million tons per year and it is estimated that humankind will have produced more than 30 000 million tons of plastics by the end of 2050.<sup>2</sup> The growth in plastic production is occurring for three likely reasons:<sup>2–4</sup> (1) new plastic materials (made by both changing the structure and processing conditions of the plastics) allow for the use of plastics in new applications, (2) the developing world is using more plastics as their economy improves, and (3) the decreasing cost of plastic production due to cheap fossil feedstocks.

Fig. 1 shows a Sankey diagram for the production, utilization and recycling of packaging plastics adapted from the Ellen McArthur Foundation.<sup>5</sup> This shows that 32 percent of all plastics is mismanaged (littered or inadequately disposed).<sup>6</sup>

<sup>a</sup>Department of Chemical and Biological Engineering, University of Wisconsin-Madison, Madison, WI, 53706, USA. E-mail: gwhuber@wisc.edu

<sup>b</sup>Biological Systems Engineering, University of Wisconsin-Madison, Madison, WI, 53706, USA

<sup>c</sup>Renewable Resources and Enabling Sciences Center, National Renewable Energy Laboratory, Golden, CO, 80401, USA

<sup>d</sup>BOTTLE Consortium, National Renewable Energy Laboratory, Golden, CO, 80401, USA

<sup>e</sup>Department of Mechanical Engineering, Iowa State University, Ames, IA, 50011, USA

<sup>f</sup>Department of Civil and Environmental Engineering, University of Wisconsin-Madison, Madison, WI, 53706, USA

<sup>g</sup>Bioeconomy Institute, Iowa State University, Ames, IA, 50011, USA

<sup>h</sup>Polymer and Food Protection Consortium, Department of Food Science and Human Nutrition, Iowa State University, Ames, IA, 50011, USA

<sup>i</sup>Department of Chemistry, University of Wisconsin-Madison, Madison, WI, 53706, USA

<sup>j</sup>Zoology and Environmental Studies, University of Wisconsin-Madison, Madison, WI, 53706, USA

<sup>k</sup>Department of Mechanical Engineering, University of Wisconsin-Madison, Madison, WI, 53706, USA

<sup>l</sup>Facultad de Ciencias Químicas, Universidad Autónoma de San Luis Potosí, San Luis Potosí 78210, Mexico

† Electronic supplementary information (ESI) available. See DOI: <https://doi.org/10.1039/d2gc02588d>



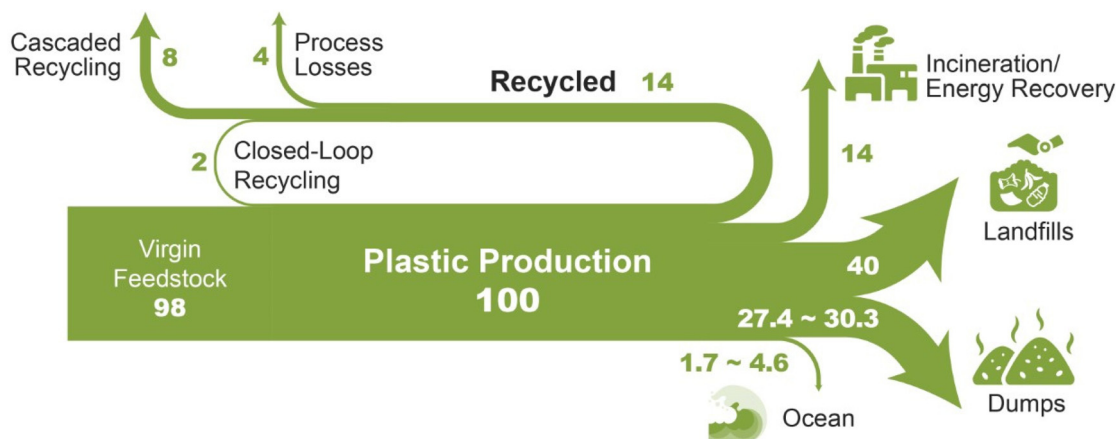


Fig. 1 Sankey Diagram showing the life cycle of plastic packaging.<sup>5</sup>

Between two to five percent of plastics are transported into the ocean through riverways.<sup>6</sup> Any plastic waste on land has the potential to eventually reach the ocean as the ocean is the ultimate sink of the earth.<sup>7</sup> In the environment, plastics will slowly degrade into microplastics, which are plastic fragments less than 5 mm in diameter. Recently, microplastics were even found in the troposphere.<sup>8</sup> Microplastics can also enter the environment from the degradation of plastic clothing into wastewater.<sup>9</sup> Degradation mechanisms include weathering, leaching, fragmentation and potentially assimilation and mineralization. Plastic leaks into the environment through improper disposal, transport of plastics from collection sites to a central facility, and leakage from the solid waste facilities. Ocean plastics have two well-studied impacts on marine and freshwater animals: waste ingestion–egestion of plastics and entanglement in plastic waste.<sup>7</sup>

Forty percent of plastics is landfilled. Developed countries often have landfills with thick plastic covering which prevents leakage into the environment.<sup>10</sup> However, less developed

countries often have open landfills where plastic can easily leak into the environment. In the US, which has a modern solid waste disposal infrastructure, it has been estimated that 0.98–1.26 million metric tons of plastic (or 2.33–2.99% of plastic waste generated) leak into the environment.<sup>11</sup> Large amounts of plastics wastes are also released into the environment during natural disasters. For example, in 2011 the Tohoku earthquake and tsunami in Japan deposited an estimated 5 million tons of debris into the ocean. By 2030, 58.4 million tons of plastics will be added to the oceans each year around the world.<sup>7</sup>

Fourteen percent of plastics is burned for energy recovery. While this does not create a solid waste problem, it does generate greenhouse gases. Fourteen percent of plastics are “recycled” with 8% being “cascaded recycled” to lower quality materials and only 2% of plastics used in closed-loop recycling where virgin plastics can be used. The amount of plastics recycled varies by countries, with the US recycling 10% and the EU 31% of plastics consumed.<sup>4</sup> As will be discussed in this



Houqian Li

Houqian Li is currently a post-doctoral research associate at University of Wisconsin Madison in Chemical and Biological Engineering and Chemical Upcycling of Waste Plastics (CUWP) center working with Professor George Huber. His research focuses on chemical methods to recycle/upcycle biomass and waste plastics and also the mechanistic study of sustainable catalysis. He received his PhD in Chemical

and Biological Engineering from Washington State University under the supervision of Prof. Yong Wang.



Jessica L. Brown

Jessica Brown received her Bachelor's Degree in chemical engineering in 2019 from Iowa State University. She is currently pursuing her Ph.D. at Iowa State University in mechanical engineering under Dr Robert Brown. Her research interests are upcycling plastic wastes using thermochemical deconstruction and hybrid processing.



review, the low amount of recycled plastics is due to several reasons including: (1) plastics have a wide variety of compositions, (2) the high cost of collecting and sorting different types of plastics, especially the removal of contamination, and (3) the high capital costs and technological uncertainties of more “advanced recycling options”. Recent changes in legislation along with the desire from consumers for more sustainable products has created a dramatic push by industry for more advanced plastic recycling technologies. IHS Markit has projected that \$300 billion of capital spending that is earmarked for new plastic production capacity should be redirected to plastic recycling technologies to meet circular economy goals.<sup>12</sup>

Fig. 2 shows the current and future infrastructure for plastic recycling technologies. The first step in plastic recycling is the sorting of plastic wastes into different streams through the material recovery facility (MRF). The MRF sorts out the glass, metals, carboard, and plastics, bails them, and then sells them to a downstream recycler. Plastic wastes can be divided up into four areas: post-industrial waste (PIW), post-consumer waste (PCW), plastics that are present in municipal solid wastes (MSW), and ocean plastics. PIW is typically of more uniform composition and lower in contaminants than the other types of plastic wastes. Oftentimes industry will recycle PIW in closed-loop recycling processes. However, PIW often contain multi-layer films which cannot be recycled by mechanical recycling due to material incompatibility. The current plastic recycling infrastructure is primarily focused on mechanical recycling of rigid #1 and #2 plastics. MRFs do not collect flexible films or textiles as this will clog the equipment. Ocean plastic waste is not currently collected at any large scale. MSW is primarily sent to landfills although some “dirty MRFs” can process these streams as well.

As shown in Fig. 2, several technologies currently exist to chemically recycle plastics. Plastics can undergo thermal

degradation to produce a liquid known as pyrolysis oil. Pyrolysis oil can be converted into aromatics and olefins by either steam cracking or using a form of catalytic upgrading as discussed in sections 5 and 6. This produces aromatics and olefins which can then be re-used to make new recycled plastics that have the same properties as the virgin plastics. Multilayer-plastics can be processed *via* dissolution-based recycling approaches generating pure plastic flakes which can then be re-extruded into recycled plastic resins. Polyesters and polycarbonates can be chemically or enzymatically (section 9) converted into their monomers by methanolysis and other technologies. These monomers can then be re-used to remake the polymers. Plastics can also be gasified to synthesis gas which can be used to make methanol or transportation fuels as discussed in section 7. Methanol can then be converted into aromatics and olefins.<sup>13</sup> Other approaches to recycle plastics, primarily being studied in academia at present, include hydrogenolysis to produce lubricants and oils, functionalization of plastics, and the creation of plastic alloys as discussed in section 10.

Sorting, recycling, disposal, and product redesign in the management of waste plastics have been reviewed.<sup>14–22</sup> The objective of this review is to first describe current plastic recycling infrastructure followed by a discussion of the chemistry, engineering, and technology of advanced plastic recycling. We first review the manufacture of plastics (section 2), landfilling of waste plastics and MSW sortation (section 3), and mechanical recycling of waste plastics (section 4). We then summarize the technologies that are being used or developed including pyrolysis (section 5), liquefaction (section 6), gasification (section 7), dissolution-based approaches (section 8), PET conversion to monomers (section 9), followed by other catalytic processes for plastics conversion (section 10). Conclusions and outlook are provided in section 11.



**Victor S. Cecon**

*Victor is a doctoral student and graduate research assistant in Food Science and Technology at Iowa State University (Ames, IA, USA) and is affiliated with the Polymer and Food Protection Consortium. His major professor is Dr Keith Vorst. He received his B.S. in Chemical Engineering from the Federal University of Sao Carlos (UFSCar, Brazil) in 2019, being a visiting scholar at the University of British Columbia (UBC, Canada) for*

*one year. His current research is focused on the sorting, processing, and characterization of post-industrial and post-consumer plastic waste, including landfill-diverted waste streams from Materials Recovery Facilities (MRFs).*



**Julia B. Curley**

*Julia Curley received her PhD in inorganic chemistry from Yale University under the supervision of Prof. Nilay Hazari in September 2021. Her graduate research included synthetic, catalytic, and mechanistic studies of iron and ruthenium pincer complexes used in reactions relevant to renewable energy storage. She began her postdoc at the National Renewable Energy Laboratory in October 2021 under the guidance of Dr Gregg*

*Beckham and Dr Robert Allen. Her current work focuses on the development of efficient and scalable systems for polyester chemical recycling.*



## 2 Manufacture of plastics and the environmental footprint of plastics disposal

### 2.1 Plastic industry supply chain

**2.1.1 Supply chain of plastics.** Fig. 3 depicts the current supply chain for production of virgin plastics. Natural gas and naphtha (a certain boiling fraction of crude oil) are the two main feedstocks. PET (#1) is formed from ethylene glycol (EG) and terephthalic acid (TPA), while both HDPE (#2) and low-density polyethylene (#4 LDPE) are produced from ethylene. Ethylene can also be used to produce vinyl chloride monomer, which in turn is the key precursor to PVC (#3). Polypropylene (#5 PP) and PS (#6) are made from propylene and benzene with ethylene, respectively. #1–#6 plastics meet the majority of demands, and the rest is fulfilled by other plastics (#7 plastic). Typically, these resins are inexpensive and easy to process.

The chemical process of polymerization is not the same for all plastics, since the reaction is dependent on monomer chemistry and controlled by several conditions such as temperature, pressure, monomer concentration, and desired end use as well as by structure-controlling additives including catalysts, activators, accelerators, initiators and inhibitors.<sup>23</sup> There are two basic classifications that encompass most polymerization schemes: step growth (condensation) and chain growth (addition) polymerization. Linear and non-linear step growth polymerizations are processes in which the polymerization occurs through the reaction of more than one molecular species. On the other hand, chain polymerization processes occur with monomers that have an unsaturated group. For example, polyethylene (PE) is produced from the polymerization of ethylene (or ethene, olefin) monomers through poly-

addition either from the radical polymerization of ethylene monomers or by using Ziegler–Natta or metallocene catalysts. Table 1 lists the various polymerization mechanisms and some examples of their polymer products.

PP, the most widely used thermoplastic globally, is exceptional due to its production cost-effectiveness and wide applications, such as flexible barrier film pouches, caps, closures, and containers. LDPE, the second most widely used resin, is typically used to make plastic films, and injection- or blow-molded products, such as wash bottles and computer hardware covers and packaging. HDPE is typically used as fibers for industrial plastics, pipes and tubing, and consumer products, such as containers. These polyolefins account for almost 48% of global plastic demand.<sup>24</sup>

Copolymerization is used to manipulate the properties of manufactured plastics to meet specific requirements and industrial needs, allowing for the improvement of mechanical and chemical properties.<sup>25</sup> Through manipulation of monomer chemistry, more customized materials like copolymers have been formed and successfully introduced commercially, such as acrylonitrile–butadiene–styrene (ABS), styrene–butadiene copolymer (SBR), nitrile rubber (NR), styrene–acrylonitrile (SAN), styrene–isoprene–styrene (SIS), and ethylene–vinyl acetate (EVA), all of which are formed through chain growth polymerization. Linear low-density polyethylene (LLDPE) is produced by polymerizing ethylene with 1-butene and smaller amounts of 1-hexene and 1-octene, leading to a product that is structurally similar to LDPE but with short, uniform branches, leading to improvements to the polymer's mechanical and chemical properties. Step growth polymerization has been used to produce most polyamides, *e.g.*, nylon-12 and 66 polymers, as well as the PET family. These polymers consist of at least two types of constituents (monomers, *e.g.*,



**Harish Radhakrishnan**

*Harish Radhakrishnan, born in 1996, obtained his master's degree in Mechanical Engineering from Iowa State University and has been working on his Ph.D. dissertation for the past three years. His dissertation concerns the thermochemical and plasma-based upcycling of post-consumer plastic wastes into fuels and chemicals for downstream processes. His research activities include pyrolyzing and liquefaction of poly-*

*mers, modeling polymer pyrolysis and plasma-based deconstruction chemistries, and plasma reactor design. He also performs catalytic and non-catalytic experiments with gas–solid, liquid–solid, and gas–gas plasma interactions for various applications, including natural and synthetic polymer deconstruction, as well as CO<sub>2</sub> conversion and NO<sub>x</sub> production.*



**Kevin L. Sánchez-Rivera**

*Kevin L. Sánchez-Rivera graduated from the University of Puerto Rico–Mayagüez in 2019 and joined Prof. George Huber's group at the University of Wisconsin–Madison in the Chemical and Biological Engineering Department. His current work focuses on developing the Solvent-Targeted Recovery and Precipitation (STRAP) technology to recycle different types of multilayer plastics, as part of the efforts of the Chemical Upcycling of Waste Plastics (CUWP) center.*



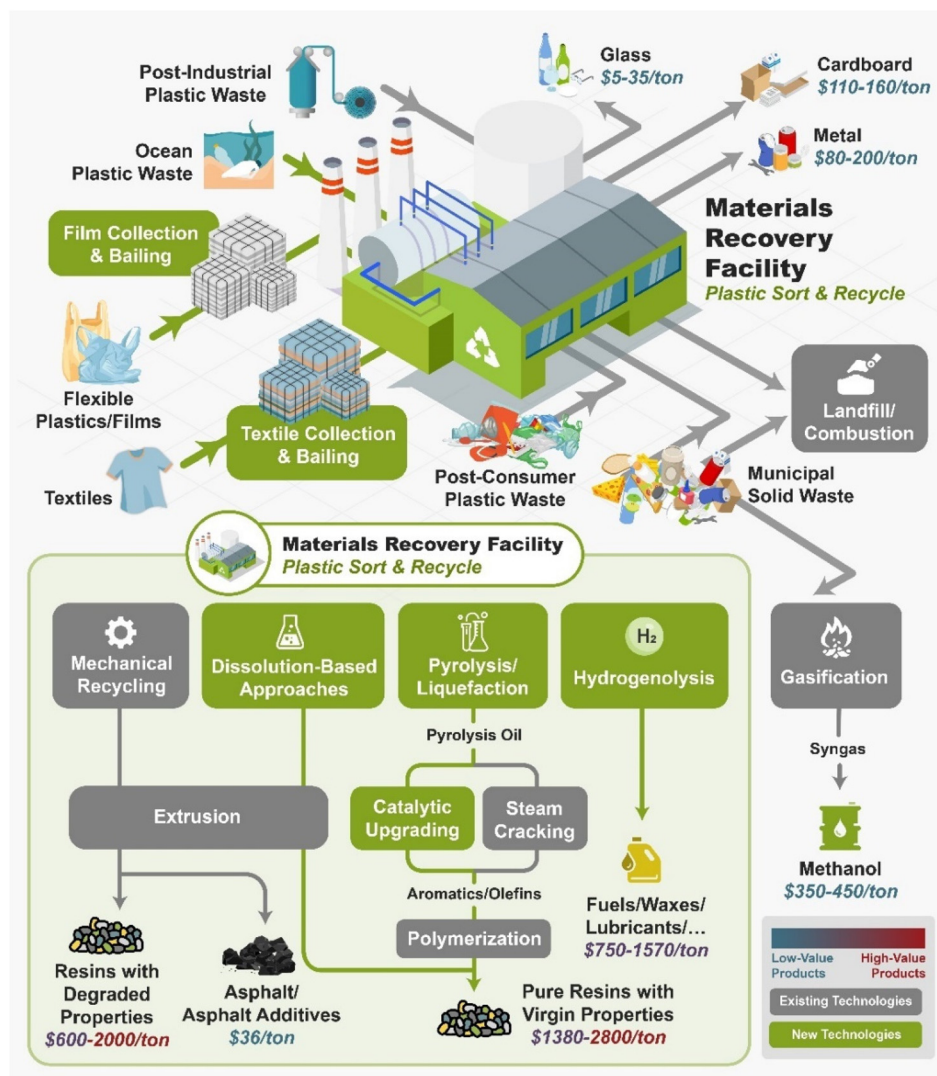


Fig. 2 Summary of current management system of waste plastics.

dicarboxylic acids and dialcohols) and can be classified depending on the repeat unit structure.

**2.1.2 Steam cracking to produce plastic feedstocks.** As shown in Fig. 3 the first step in the production of olefins is steam cracking of either ethane (for ethylene production) or naphtha.<sup>26</sup> Fig. 4 is a simplified flowsheet diagram of a steam cracking unit when naphtha is the feed, which we will describe since it can be used in chemical recycling of plastic pyrolysis oils. The feed is mixed with steam and heated by flue gas from the process in the convection zone. Before leaving the convection zone, the hydrocarbon stream is heated to 500–680 °C, which is the incipient cracking temperature range. After entering the tubular reactor of the radiant zone, the stream is heated to 750–875 °C in 0.1–0.5 s. During this short residence time, the feedstock is cracked into smaller molecules, including ethylene and propylene, and other byproducts. In a steam cracker, the reaction follows a free radical chain mechanism. For this reaction scheme, there are hundreds of radical and

molecular species and thousands of reactions between them. The chain reactions of ethane as the feedstock can be found in SI 1.0 in Electronic Supplementary Information (ESI†).

When the feedstock is naphtha, a similar free radical reaction mechanism occurs. Adding steam to the steam cracker facilitates the control over residence time, prevents coke formation, and reduces hydrocarbon partial pressure. Steam does not participate in the free radical reaction mechanism. Its main role is to react with coke to form CO and CO<sub>2</sub>. Since the cracking process is highly endothermic, energy is input from burners in the radiant zone.

The effluent stream from the cracking furnaces is cooled by a transfer line exchanger (TLE) where feed water is vaporized, and high-pressure steam is generated. Then the cracked gas is further cooled by contact with cooled oil in a quench tower. The resulting stream is sent to a primary fractionation column where fuel oil is obtained at the bottom. The stream on the top is further cooled down using a quench water tower. On the



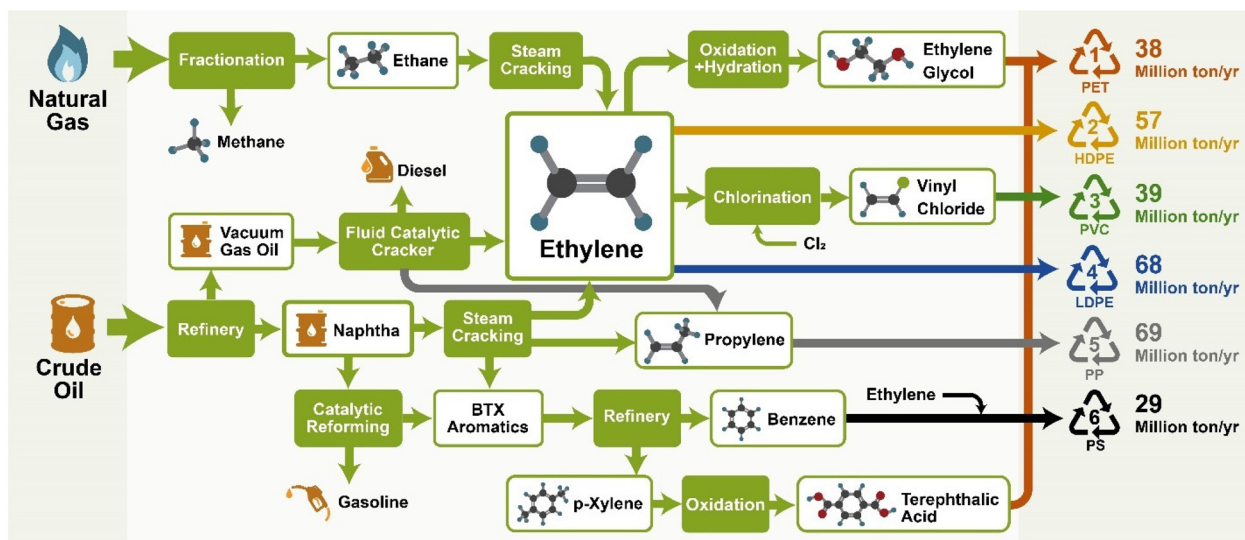


Fig. 3 Supply chain of the manufacture of #1-#6 plastics and their volume of production in 2019.<sup>19</sup>

Table 1 Polymerization classification and inhibitors<sup>23</sup>

Classification	Polymerization	Examples
Step linear	Polycondensation	Polyamides (PA) Polycarbonate (PC) Polyesteramide (PEA) Polyetherimide (PEI)
Step non-linear Chain	Polyaddition	Polyethylene (PE) Epoxy resins (EP)
	Network polymers	Melamine formaldehyde (MF)
	Free radical	Polymethylmethacrylate (PMMA) Polyvinyl acetate (PVAC) Polystyrene (PS) Polyvinyl chloride (PVC) Polyisobutene (PIB) Butadiene rubber (BR)
	Cationic	Polymethylmethacrylate (PMMA)
	Anionic	Polyamide from ε-caprolactam (PA6)
	Ring opening	Polycaprolactone (PCL) Polyethylene oxide (PEO) Polypropylene Oxide (PPO)
	Ziegler-Natta	Polyethylene (PE)
	Metallocene	Polypropylene (PP)

bottom of this quench tower, a three-phase separator splits water, liquid, and gas hydrocarbons. The liquid hydrocarbons are collected as gasoline-ranged products that is heavy in aromatics. These aromatics are also used to produce other types of plastics. On the top of the quench water tower, gas effluent is obtained and mixed with gas effluent of the three-phase separator. This stream contains light hydrocarbons, including ethylene and propylene.

After compressing the cracked gas with a multi-stage compressor, the gas is sent to an acid-gas removal unit where CO<sub>2</sub> and H<sub>2</sub>S are removed. After drying the purified gas with a molecular sieve dryer, the cracked gas is sent to the cold box where it is cooled down to -156 °C. Under these conditions, hydrogen is recovered for use in hydrogenation of C<sub>3</sub>H<sub>4</sub>. The

separation of hydrocarbons starts from a demethanizer where methane is removed. This methane stream is supplied to the cracker as fuel gas for providing the reaction heat. The bottom stream of the demethanizer is sent to a deethanizer where ethane or lighter components are obtained. To convert acetylene into ethylene, this C<sub>2</sub> stream is hydrogenated and fractionated cryogenically. The ethylene fractionator column splits ethylene and ethane. The ethane is mixed with propane and recycled back to the cracker. On the bottom of deethanizer, C<sub>3</sub> and heavier components are obtained and sent to a depropanizer where C<sub>3</sub> and C<sub>4</sub>/heavy fractions are separated.

After hydrogenating methylacetylene and propadiene, the C<sub>3</sub> stream is split into propylene and propane. The propane is recycled back to the cracker. Meanwhile, the C<sub>4</sub> and heavier components stream is sent to a debutanizer where butylene/butane and gasoline-ranged products are obtained. When ethane/propane are fed, no primary fractionator is needed. The gas cleaning and separation processes are very similar to the above one when feeding the cracker with ethane only. Information related to steam cracking facilities in the US can be found in SI 1.0 in ESI†.

## 2.2 Plastics processing

The conversion of raw or virgin plastics into finished products involves a series of plastic manufacturing processes. These manufacturing processes will vary depending on the type of plastic (thermoplastic, thermosetting, or elastomeric) and the final product desired. Plastic manufacturing can be commonly divided into three stages. The first stage is the compounding of the raw plastic with additives to achieve the desired material properties. For example, PE and PP films often stick together, which makes them difficult to separate, as when opening a PE bag. Anti-blocking agents (such as limestone and talc) can be added to lower the blocking force between the film layers. Table 2 lists the most common additives and their classifi-





mization of finishing processes as compared to the manufacture of more traditional materials.<sup>30</sup> Table 3 lists common methods attributed to the three stages of plastics manufacturing.

For polymeric materials, it is typical for a particular product to require multiple forming processes for ease of transfer and shipping (such as extruding a tube, then pelletizing for shipping and further use) or to carry out a specific chemical process (such as crosslinking or vulcanization). These forming processes typically involve the softened stage of the polymer, which is achieved by heating the polymer material. Each forming process will impact a thermal history and, in the case of reactive polymeric systems, will impact a degree of cure. These repeated forming processes will influence the properties of the material, either through the degradation of the material or unwanted side reactions. Setting the shape of the product is typically achieved either by cooling (which can cause crystallization, further impacting material properties) or a chemical process (crosslinking) to achieve dimensional stability. Table 4 demonstrates the most common plastics processing techniques used to form and set material shapes.

Most plastics produced are specifically designed to serve very particular applications. Fig. 5 demonstrates material pro-

**Table 2** Plastic additive classifications and common examples<sup>30</sup>

Additive classification	Common agents
Anti-blocking agents	Limestone Synthetic silica gel Natural silica Talc
Slip additives	Erucamide Oleamide Stearamide
Plasticizers	Diethylphthalate (DEHP)
Antioxidants	Hydrogen donors – phenols Hydroperoxide decomposers – phosphites and phosphonites Alkyl radical scavengers – hindered amine stabilizers and hydroxyl amines Metal deactivators
Flame retardants	Aluminum hydroxide/oxalate Zinc borate/chloride/sulfide Alumina trihydrate
UV stabilizers	Sterically hindered amines (HALS) Carbon black
Antistatic agents	Fatty acid esters Ethoxylated alkylamines
Antimicrobial agents	10,10'-Oxybisphenoxarsine (OBPA)
Antifogging agents	Glycerol esters Polyglycerol esters Alcohol ethoxylates Azodicarbonamide Carbonates Semi-carbazides
Chemical blowing agents	White – titanium dioxide, zinc oxide Black – spinel black, iron oxide black Yellow-orange – iron oxide yellow, zinc ferrite Brown – chrome iron brown, rutile brown Red – iron oxide red, cadmium orange Green – chrome oxide green, cobalt spinel green Blue – cobalt blue, ultramarine blue Metallic – aluminum, copper Bis-benzoxazoles
Fluorescent whitening agents	Phenylcoumarins
Fillers	Glass Talc Ceramic Porcelain clay

**Table 3** Typical stages in the plastics manufacturing processes

Stage	Methods
Compounding	Powder, melt, dispersion, solution
Forming	2-D: extrusion, calendaring, coating, spinning 3-D: thermoforming, molding (compression, transfer, injection, blow)
Finishing	Machining, decoration, assembly

properties and pricing of thermoplastics, aluminum, and ceramics compared to steel. During the forming of the product, it is standard for manufacturers to use additives to manipulate the properties of the raw material to achieve specific characteristics or homogenize the characteristics of their material batches as shown in Table 2. These additives influence the

mechanical and thermal properties of the plastics, either by manipulating the glass transition temperature, imparting higher chemical resistance or increasing impact strength and elasticity, among other things.<sup>31</sup> Fig. 5 demonstrates average mechanical properties and pricing of common commercial plastics. Many commercial plastics will have different characteristics from those of the base plastic, even though they may have the same chemistry. In general, it is important to understand that many plastics are technically combinations of several materials. As a result, mechanical and thermal properties are influenced by each component. Often, manufacturers change additives or blend ratios due to environmental concerns, to enhance specific properties, or simply for more economical processing. These subtle changes and introduction of new materials and compounding may drastically change one or more engineering properties; because of this, it is of utmost importance to continually test and evaluate commercial plastics and their specifications. Table 5 contains thermal and mechanical properties for common commercial plastics. It is of note that these properties are averages and specific material formulations can manipulate these properties for specific applications.

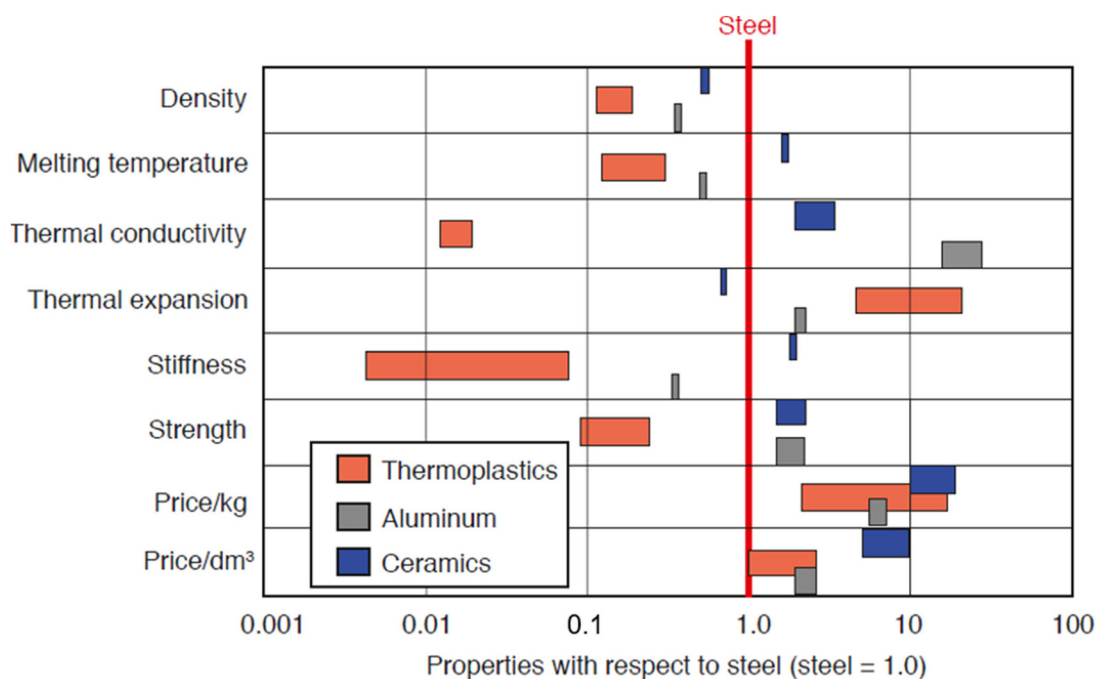
Temperature can have varying effects on polymer products, from melting to degradation to morphological transitions.<sup>33</sup> Temperature can also affect mechanical properties due to enhanced polymer chain movement and free volume. Two key temperatures describe these effects: the glass transition temperature and melting temperature. The glass transition temperature is a property of the amorphous region of the plastic, whereas the melting point is a property of the crystalline regions. At temperatures below the glass transition temperature, the molecules in the amorphous region exist in a frozen state where movement is minimized and the polymer chains can vibrate slightly. This is typically referred to as the plastic's glassy state. The rubbery state occurs when the plastic is heated above the glass transition temperature, allowing the polymer chains to move and shift around each other, which in turn allows the plastic to become soft and flexible. Glassy (amorphous) plastics exposed to heat eventually soften and flow into a viscous liquid.

Melting transitions in some plastics refer to the transition between a crystalline solid and a liquid. When a semi-crystalline plastic is heated above the melting temperature, it forms a viscous liquid and flows. Amorphous plastics do not experience melting since there are no crystal regions to melt. For semi-crystalline plastics, crystallinity is dependent on the type and structure of the plastic. Crystallinity is typically induced by cooling a melt, although strain-induced crystallization may occur due to the molecular chains disentangling, unfolding, and straightening above its yield point. Molecular weight plays a large role in crystallinity and most polymeric properties. A plastic's tacticity will also influence its crystallinity, with isotactic plastics demonstrating higher crystallinity than syndiotactic plastics, and atactic plastics being considered uncrystallizable due to the lack of chain regularity. Strong intermolecular



**Table 4** Important plastics processing techniques

Processing Method	Description
Extrusion	Thermoplastic granules are forced through a heated barrel and the plastic melt is squeezed through a die with the desired profile for the extruded component. The extruded material is cooled as it leaves the die, then cut to the desired length
Spinning	A specialized form of extrusion that utilizes a spinneret to form multiple continuous filaments. Extruded liquid plastic filament is continuously drawn and simultaneously solidified to form a continuous synthetic fiber
Blow molding	Compressed air is introduced underneath a warmed sheet of thermoplastic material, forcing the material into a cavity or allowing it to expand freely
Vacuum forming	A sheet of plastic is set over a mold, where it is warmed and softened. Air is drawn from under the softened plastic sheet, which forces it over or into a mold by atmospheric pressure
Extrusion blow molding	Plastic material is first extruded as a tube shape into an open die. The die is then closed to seal the ends of the tube and air is blown in, forcing the plastic tube to take the shape of the die cavity
Injection molding	Granulated plastic is heated until a melt is formed. The melt is then injected into a closed mold using high pressures and cooled inside the mold
Rotational molding	Plastic is placed in a closed mold that is heated and rotated slowly around a vertical and horizontal axis. The plastic material melts and sticks to the hot mold surface, building up the required thickness. The mold is gradually cooled while rotating
Foaming	The base plastic is mixed with foaming/blowing agents. When heated, these agents release gas which form bubbles in the plastic. A separate method is to inject compressed nitrogen gas into molten plastics during the molding process
Calendering	A thermoplastic melt is extruded onto heated rotating rollers which squeeze the material into a continuous sheet or film
Compression molding	A thermosetting plastic charge is placed into a preheated lower mold cavity. The mold is then closed and subjected to further heat and pressure. The combined pressure and heat caused polymerization and the flow of the plasticized material within the mold

**Fig. 5** Properties of thermoplastics, aluminum, and ceramics with respect to steel. Reproduced with permission from ref. 32 from Carl Hanser Verlag, Munich, copyright 2012.

forces and a stiff chain backbone favor the formation of crystals, while bulky side groups and branching have the opposite effect, due to the difficulty in folding and aligning the chains along the crystal growth direction. Crystallinity highly influences the thermal, mechanical, and physical properties since it impacts strength, toughness, and opaqueness depending on the degree of crystallinity. These properties are further varied

by the plastic's chemistry, composition, and compounding, which in turn influence the molecular weight of the plastic. Fig. 6 demonstrates the key characteristics of various amorphous and semi-crystalline plastics based on their performance and applications.

The mechanical properties of plastics are highly varied, although there are specific relations between plastic structure



**Table 5** Morphological, thermal, and mechanical properties of common plastics<sup>7,8</sup>

Material	Morphology	Density [g cm <sup>-3</sup> ]	Glass transition temperature [°C]	Melting temperature [°C]	Initial degradation temperature [°C]	Tensile strength (MPa)	Tensile modulus (Mpa)	Strain at break (%)
ABS	Amorphous	1.03–1.07	–85/95–105/ 125	—	420–428	32–45	1300–2700	15–30
EVA	Semi-crystalline	0.92–0.95	–40–20	30–110	345–360/ 470–480	18–35	7–120	600–900
LDPE	Semi-crystalline (40%–55%)	0.91–0.93	–130 to –100/ –30 to –10	100–115	487–498	8–23	200–500	300–1000
LLDPE	Semi-crystalline	0.91–0.94	–130 to –100/ –70 to –25	122–127	475–485	—	—	—
HDPE	Semi-crystalline (60%–80%)	0.94–0.96	–130 to –100	125–135	480–498	18–35	700–1400	100–1000
UHMWPE	Semi-crystalline	0.93–0.94	–130 to –100	130–145	480–490	—	—	—
PLA	Semi-crystalline	1.21–1.43	45–65	150–160	350–375	—	—	—
PP	Semi-crystalline	0.90–0.91	–20–20	160–165	450–470	21–37	1100–1300	20–800
PS	Amorphous or Semi-crystalline	1.05	80–105	—	415–425	45–65	3200–3250	3–4
PVAL	Semi-crystalline	1.21	70–100	220–260	260–320/ 420–450	—	—	—
PVC-Plasticized	Amorphous	1.16–1.35	–50–80	—	290–315/ 460–475	10–25	—	170–400
PVC-unplasticized	Amorphous	1.38–1.55	80–90	—	285–315/ 460–475	50–75	1000–3500	10–50
PA6	Semi-crystalline (30%–40%)	1.12–1.15	45–80	225–235	445–460	70–85	1400	200–300
PA66	Semi-crystalline (35%–45%)	1.13–1.16	65–90	225–265	430–473	77–84	2000	150–300
PC	Amorphous	1.20–1.24	140–150	—	480–535	56–67	2100–2400	100–130
PET	Semi-crystalline	1.33–1.45	70–85	245–260	425–445	47	3100	50–300
PUR	Thermoset	1.10–1.70	10–180	—	240–350	70–80	4000	3–6
SBR	Rubber with hard and soft segments	0.94	–55 to –35	–20	435–470	26–38	1800–2500	25–60

and their properties. A plastic's strength (tensile, compressional, flexural, torsional, and so on) depends on the molecular weight, presence of crosslinking, crystallinity, and structure. In general, a linear plastic has less strength than a branched plastic, followed by cross-linked plastics having greater strength, and network plastics exhibiting the highest strength. Low molecular weight plastics exhibit low strength, regardless of crystallinity, due to weak van der Waals forces and the ease of movement between chains, while high molecular weight plastics exhibit a greater degree of entanglement, which greatly increases the plastic's strength. Crosslinking increases the strength of the plastic by restricting chain motion, while crystallinity increases strength due to the significant intermolecular bonding. These properties are highly influenced by environmental and application factors such as loading, temperature, humidity, weather conditions, exposure, and time.

#### 2.4 Environmental assessment on plastic production systems

Fig. 7 presents the supply chain greenhouse gas emission (GHG) arising in the production of major types of plastic. PET has the largest carbon footprint of these plastics. The equivalent GHG emissions for producing one kg of PET film is up to 4.5 kg, where 60% of the emissions result from the usage of processing fuel and 28% of emissions are from electricity usage. General-purpose (GP) HDPE has the lowest GHG emissions among the plastics listed. The production of injected

molded (IM) LDPE tends to have a high emission associated with electricity usage (1.8 kg equivalent CO<sub>2</sub> per kg of plastic). In comparison with the GHG emissions of electricity and processing fuel, the emission associated with transportation is relatively low, and only corresponds to 9 to 18% of the emission of the plastic supply chain.

#### 2.5 LCA on plastic recycling technologies

In the past 17 years, 13 major life cycle assessment (LCA)/environmental assessment studies on recycling technologies and plastic waste disposal options have been conducted.<sup>35–47</sup> These recycling/disposal options could be classified into four types: mechanical recycling, chemical recycling, incineration, and landfilling. These studies explored the environmental impact of each technology from GHG emissions, water/air pollution, human health, and resource depletion perspectives. From these publications, some general conclusions can be made:

(a) Climate change: without considering the electricity credit, incineration of plastics has the highest GHG. The GHG emission of incineration ranges from 1.8–3 kg CO<sub>2,eq</sub> per kg plastic wastes.<sup>43,48</sup> However, accounting for the electricity credit lowers the GHGs of incineration to around 1.4 kg CO<sub>2,eq</sub> per kg plastic wastes. Meanwhile, the chemical recycling technologies (*e.g.*, pyrolysis, gasification) also have higher GHGs than the GHGs of mechanical recycling methods, due to the direct emission and electricity consumption.<sup>44</sup>





## IAPD THERMOPLASTICS RECTANGLE

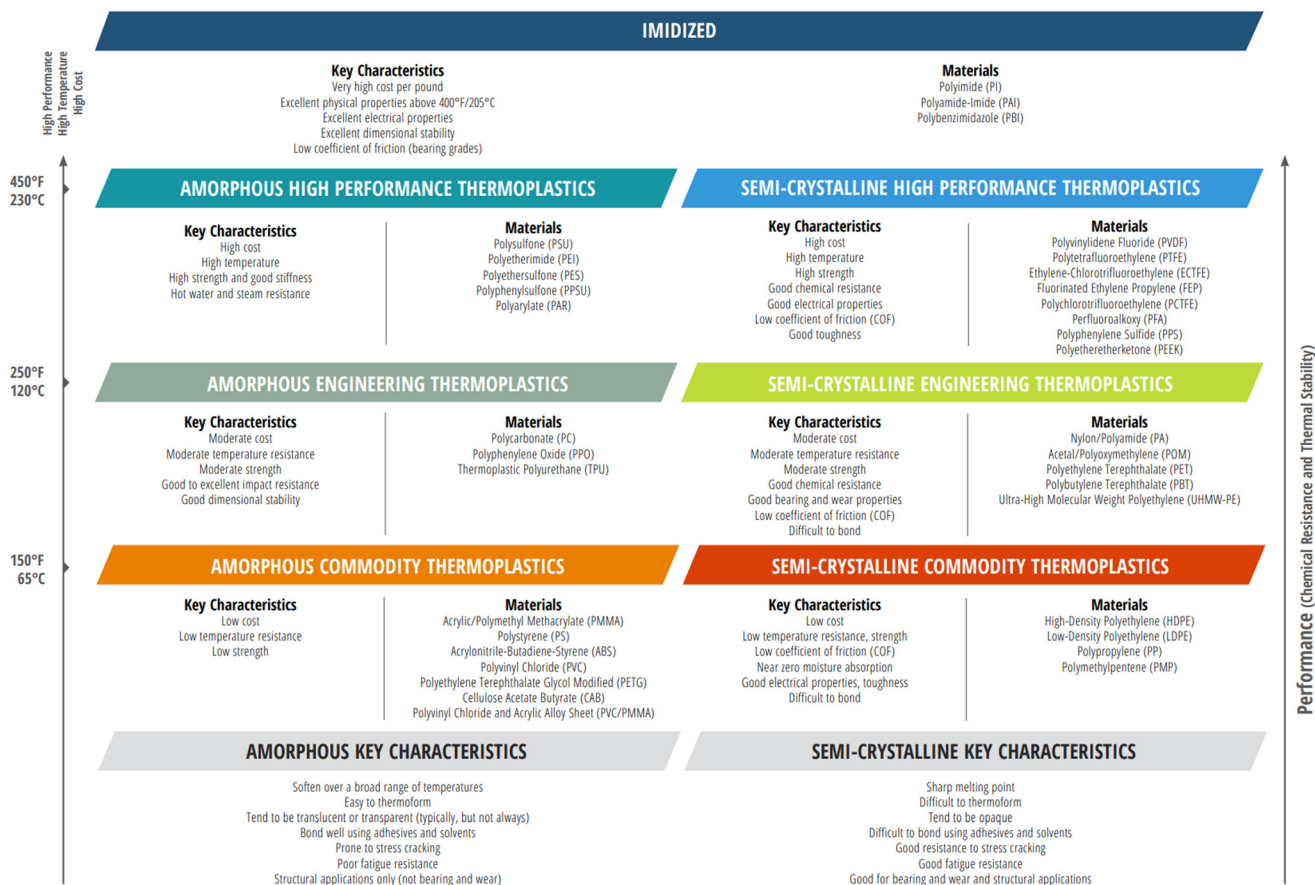


Fig. 6 International Association of Plastics Distribution Thermoplastics Rectangle. Reproduced from ref. 34 with permission from International Association of Plastics Distribution, copyright 2021.

(b) Acidification: chemical recycling technologies tend to have high acidification potential. For example, gasifying one ton of plastic waste results in 0.49 kg emission of  $\text{NO}_x$  and 0.09 kg emission of  $\text{SO}_x$ .<sup>48</sup> However, after accounting for credit to avoid incineration of plastic waste, the acidification potential of chemical recycling options is lower than the acidification potential of producing virgin plastic from fossil fuel.<sup>49</sup>

(c) Air pollution: incineration contributes to air pollution. The air emission of organic compounds is ten times higher than that of the air emission of pyrolysis (1.42 g emission of organic compounds per kg of plastic processed). Mechanical recycling has the lowest air emission among plastic disposal options.

(d) Resource depletion: it is estimated that producing 1 kg of plastic requires 2 kg of crude oil, which is lost in cases where plastics are landfilled.<sup>48</sup> Meanwhile, incineration also has high resource consumption, since the plastic is combusted for generating electricity.<sup>39</sup> Among all the disposal options, mechanical recycling has the advantage in terms of natural resource depletion. After accounting for the credit of avoided landfill or incineration, the amount of resource consumption of mechanical recycling (crude oil/gas) is even negative.<sup>39</sup>

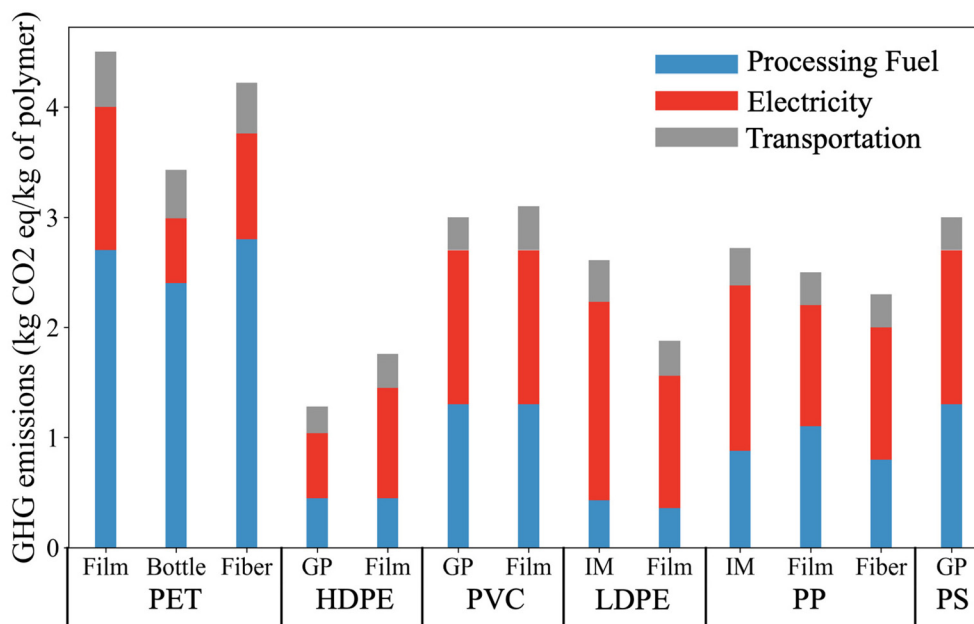
Incineration causes air pollution,  $\text{CO}_2$  emission, and acidification of the disposal of plastic wastes. Although landfills tend to have low air pollution, they can cause soil and groundwater pollution. The available space for landfills is limited, even if parts of these areas can be reused in some cases.<sup>49</sup> Therefore, landfills are not a sustainable option. In comparison with chemical recycling, mechanical recycling has a lower energy consumption and a lower carbon emission. However, as will be discussed in section 4, only a portion of plastic wastes can be mechanically recycled (e.g., PET and HDPE bottles). For plastics that cannot be mechanically recycled (e.g., plastic films), chemical methods are the most environmentally friendly approach.

### 3. Landfills, disposal, and sorting of post-consumer waste plastics

#### 3.1 Landfill and incineration

**3.1.1 Municipal solid waste overview.** MSW is the aggregate of materials discarded from households, businesses, and insti-





**Fig. 7** Supply chain GHG emissions arising in the production of different plastics. Reproduced from ref. 14 with permission from Cell Press, copyright 2021. LCA concepts were employed to estimate the cradle-to-gate energy requirement and GHG emissions. The GHG emissions associated with processing fuel and electricity correspond to the total energy consumption of the plastic supply chain. This includes emission associated with raw materials extraction, intermediate materials productions (e.g., monomer), and plastic production.

tutions and consists primarily of readily degradable organic materials (food wastes, green wastes such as landscaping debris) and less readily degradable solid materials with potential for recycling (e.g., paper/cardboard, plastic, glass, wood and metal). Landfills also accept a variety of other materials specific to the locale, which are referred to as “special wastes”. Wastewater treatment plant sludges, combustion wastes, and non-hazardous industrial wastes are examples of special wastes. Hazardous wastes and construction and demolition debris are not MSW and are generally managed differently. The composition of MSW varies geographically and by income level (Fig. 8), with the fraction of food and green waste decreasing as income level rises, replaced by a higher fraction of solid materials, particularly cardboard and plastics.

Plastics currently comprise 12% of all MSW generated globally.<sup>50</sup> In the US, only 9% of plastics are recovered through recycling, 16% incinerated, and 76% landfilled.<sup>51</sup> The EU recycles 33% of plastics, with 43% incinerated, and 25% landfilled.<sup>52</sup> Estimates for the cumulative global fate of plastics indicate 79% of plastics produced have been landfilled or left in the open environment, whereas 12% have been incinerated, and 9% recovered for recycling.<sup>6</sup>

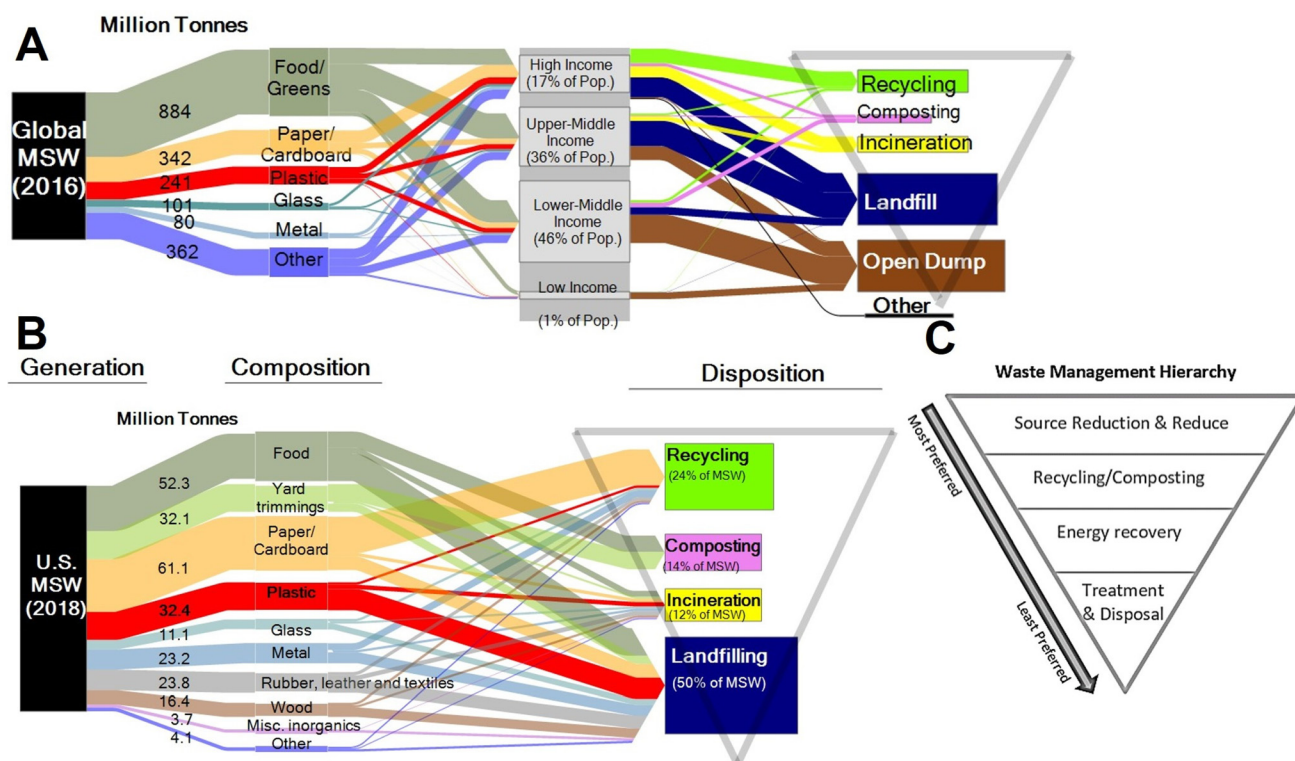
The UN Environment Programme and US EPA<sup>53,54</sup> have established waste hierarchies focused on shifting from a philosophy of waste management to a philosophy of resource management in the context of a circular economy. The recommended hierarchy (highest to lowest priority) consists of waste prevention, waste minimization, reuse, recycling, energy recovery, and disposal (Fig. 8). Most waste today, in the US and

globally, is managed by disposal in landfills – the lowest priority in the hierarchy.

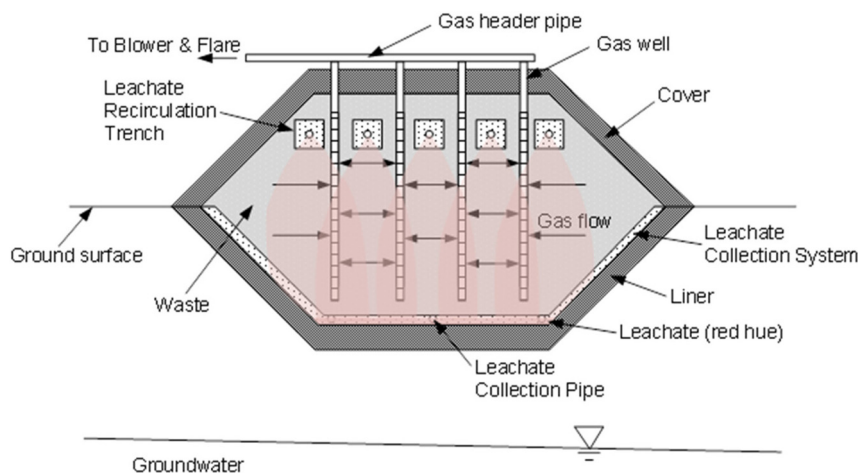
**3.1.2 Landfills.** Landfills and dumps are the largest disposition pathway for MSW (Fig. 8), primarily because this pathway is the least expensive and least cumbersome. Landfills and dumps have the common attribute of being a storage facility near the ground surface where waste is placed. However, a dump is an un-engineered facility with limited or no control on contaminated liquids or gases generated by the waste. In effect, waste is “dumped” and no longer managed. In contrast, landfills are engineered systems where liquids and gases are carefully managed so that impact on the environment remains within accepted norms. Dumps are more common in lower-income nations that lack the infrastructure and regulations for MSW management, although transitioning open dumps to engineered landfills has become a priority for some developing nations.<sup>55–58</sup> The remainder of this section focuses on landfills.

A modern engineered landfill consists of an engineered containment system situated in an earthen depression (Fig. 9). The base is comprised of a multicomponent liner overlain by a leachate collection system.<sup>10</sup> Waste is placed in layers approximately 3–4 m thick (called “lifts”) that are compacted with heavy machinery. A gas collection system is installed in the waste to collect landfill gas (LFG) for treatment or production of renewable energy. Interim cover (soil or synthetic material) is placed over the waste during filling to reduce ingress of precipitation, control emissions and odors, and limit vectors. Once final elevations are met, a final cover is placed to limit





**Fig. 8** Municipal solid waste (MSW) generation and final disposition: (A) global generation in 2016 with fractions associated with national income, (B) US generation in 2018, and (C) waste management hierarchy. Inserted triangle illustrating how disposition pathways fit with preferred waste management hierarchy.



**Fig. 9** MSW landfill with liner, cover, leachate collection, leachate recirculation, and gas collection.

the ingress of precipitation to *de minimis* amounts, facilitate gas collection, and provide separation from the surrounding environment for as long as the waste poses a threat. As with the liner, the final cover includes a multilayer hydraulic barrier overlain by a drainage layer. The surface is covered with vegetated cover soils for protection and aesthetics.<sup>10</sup>

Leachate is generated when water percolating through the landfill contacts the waste.<sup>59</sup> Leachate contains a variety of in-

organic and organic contaminants, and therefore is treated before being discharged. Leachates are pumped from the leachate collection system, and generally are transported to a public wastewater treatment plant (a publicly owned treatment works, or POTW) where they are treated along with other wastewater (*e.g.*, sewage from a community, *etc.*). In some cases, leachates are treated on site or are recirculated in the waste to stimulate waste decomposition to promote more



rapid waste stabilization and greater gas production for renewable energy.<sup>55,56</sup>

Landfills operate under anaerobic conditions where the microbial community decomposes the degradable organic fraction and generates gas comprised of approximately equal parts methane (CH<sub>4</sub>) and carbon dioxide (CO<sub>2</sub>).<sup>56</sup> MSW landfills are the third largest source of anthropogenic CH<sub>4</sub> in the US<sup>57</sup> and contribute approximately 3% of global GHG emissions.<sup>60</sup> LFG also contains a variety of other contaminants in small quantities. Consequently, LFG must be treated before being released. Thermal treatment is most common, either through a flare or through combustion to create renewable energy (e.g., LFG to electricity). In recent years, landfills have also become a significant source of renewable natural gas (RNG), which is produced by treating and compressing LFG extracted from the landfill.<sup>56</sup>

**3.1.3 Incineration with energy recovery.** Waste-to-energy (WtE) is the process of converting MSW into energy in the form of electricity, heat, or alternative fuels.<sup>61</sup> Within a circular economy framework, WtE technologies have a crucial role in providing an alternative disposal option for MSW that cannot be reused or recycled.<sup>61</sup> The technical, economic, and environmental aspects of common WtE have been evaluated extensively.<sup>62–66</sup> Astrup *et al.*<sup>67</sup> present a comprehensive review and comparison of WtE technologies. LCA methods were used to evaluate the environmental impacts of different technologies employed in WtE (e.g., plant type, energy recovery, type of energy output, flue gas cleaning, and residue types and management). Incineration is by far the most common technology for WtE, representing more than 88% of the global WtE market<sup>68</sup> with a valuation of \$50 billion predicted by 2027.<sup>69</sup> The remainder of this section focuses on incineration.

Incineration is the combustion of MSW at temperatures at around 750–1100 °C, with the heat being used to produce steam for generating electricity and/or heating.<sup>70,71</sup> Plants producing steam for heating and electricity can have efficiencies on the order of 80%; whereas the efficiency is on the order of 20% for plants producing only electricity.<sup>61</sup> Most MSW incineration is conducted as mass burn (bulk MSW incinerated in a single chamber) or as refuse derived fuel (RDF) where screened and shredded MSW is combusted.<sup>72</sup> RDF is common in the Portland cement industry and can represent up to 80% of the thermal requirements in cement plants.<sup>61</sup> Nearly 15% of all MSW is incinerated globally. Incineration rates vary significantly, with incineration more common in developed land-constrained countries and islands,<sup>70</sup> less common in developed countries without land constraints, and uncommon (<1%) in lower-middle and low-income countries. For example, Japan has significant land constraints and incinerates 74% of its MSW,<sup>73</sup> whereas the US has virtually no land constraints and incinerates only 12% of MSW. The effect of income is evident in the location of incinerators; 80% of MSW incinerators globally are located in North America, Europe, and Asia Pacific.<sup>70</sup> US incinerators manage 22% of discarded food and 16% of discarded plastics.<sup>74</sup> Most WtE incinerators in the US (77%) only generate electricity, 19% produce electricity and heat, and 4% export steam to local users.<sup>75</sup>

Incineration reduces the mass and volume of MSW that is landfilled (70–85% by mass and 75–90% by volume)<sup>71</sup> while generating energy for use or sale. Despite these advantages, incinerators are difficult to implement, especially in the US. Emissions from MSW incinerators can contain dioxins and furans, which are toxic persistent organic pollutants and human carcinogens.<sup>76,77</sup> These pollutants are often of great concern to surrounding communities even when plants are in compliance with emissions criteria in the Clean Air Act. MSW incineration also generates ashes that need to be managed,<sup>75</sup> generally through landfill disposal. Incinerator ashes tend to have higher levels of contaminants per unit mass than MSW, resulting in leachate with higher concentrations that requires more treatment. In some cases, ashes can be reactive, leading to heat generation that is problematic in landfills.<sup>78</sup>

### 3.2 Material recovery facilities (MRFs)

MRFs (pronounced “murfs”) receive waste material and separate (or bail) these materials. Their origin can be explained when terms such as MSW and waste management began to be established in the 1950–60s, with the increased waste generation linked to economic growth and popularization of petrochemical derivatives. In the US, the first MRF was established in Groton, Connecticut in the early 1980s,<sup>79</sup> with the number of facilities multiplying in the following years. There were 40 MRFs in operation or under planning in 1991, 166 in 1993, and 307 in 1995.<sup>80</sup>

MRFs are classified based on the input waste material they receive: single-stream, dual-stream, mixed-waste, or pre-sorted, with the first being a typical design in the US.<sup>42</sup> Single and mixed-waste MRFs (containing more organic contaminants from MSW) have similar inbound composition, receiving a single stream with paper, plastic, glass, and metals, usually from automatic or semi-automatic vehicles. Dual-stream MRFs have a two-category stream line: fibers, composed of paper and cardboard, and containers, composed of plastic, metal, and glass, whereas pre-sorted MRFs receive source-separated material streams.<sup>42,81</sup> Fig. 10 is a block flow diagram for single-, mixed-, and dual-stream MRF frameworks (differences between operation modes are shown; otherwise, the process is the same for all) based on the work of Pressley *et al.*<sup>42</sup> who drew on common MRF designs around the US. The design of a MRF is unique to each location, with different specifications required and associated with inbound composition, investment capacity, and ownership and operation type.

Single and dual-stream frameworks have their advantages and disadvantages. Single-stream benefits from waste collection with larger volumes and lower costs but with increased difficulty and costs for processing at the MRF, in addition to an increased contamination rate.<sup>82</sup> For example, during conversion from dual to single-stream, a MRF from Brookhaven (New York, US) observed a 25% increase in volume of input recycling streams, which led to a diversion of recyclable material from landfills from 50 000 to 35 000 tons, along with an increase in non-recyclables in the single-stream.<sup>83</sup> Another study that investigated GHG emissions observed benefits from



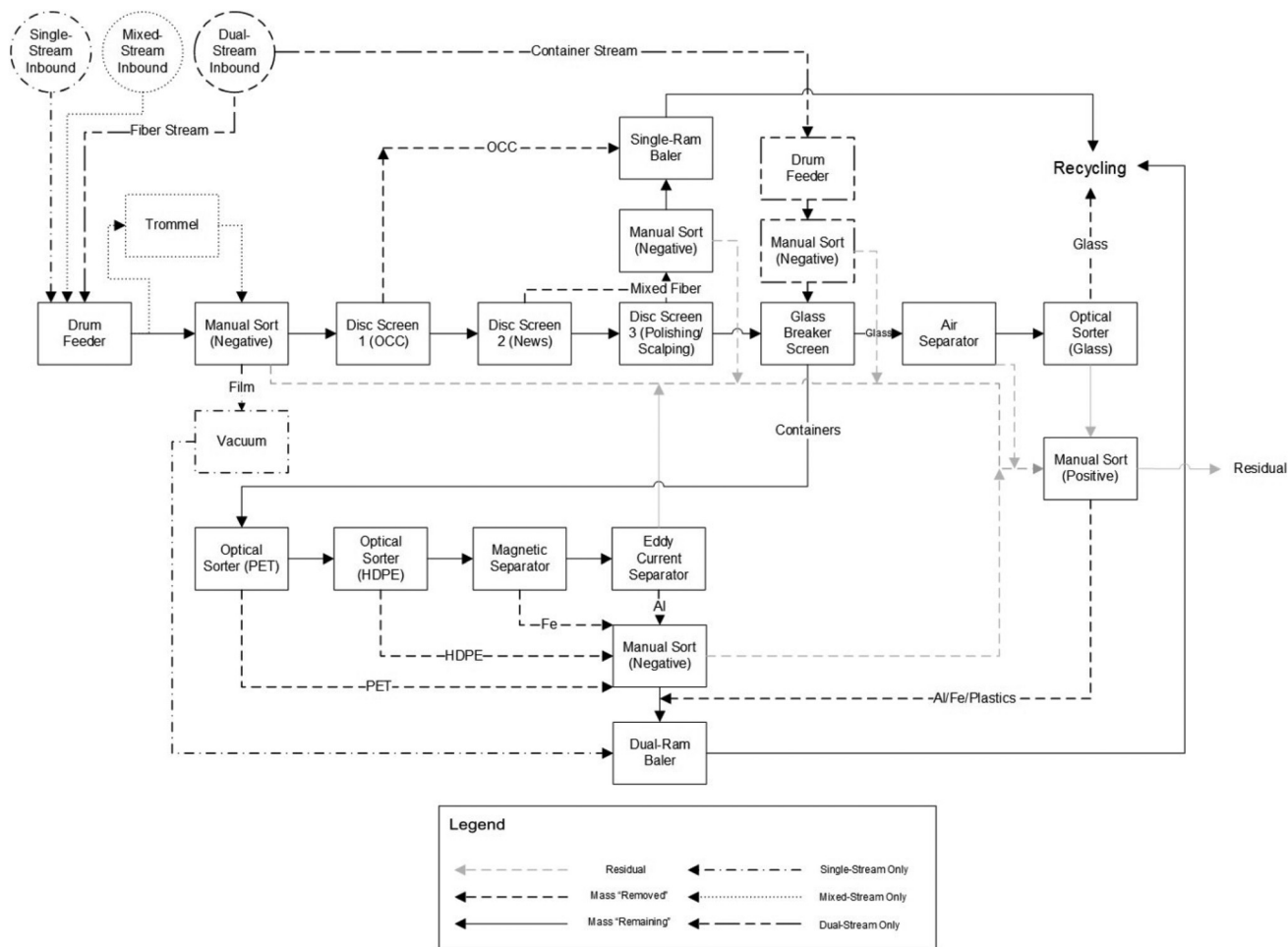


Fig. 10 Block Flow Diagram of a single-, mixed-, and dual-stream MRF. Reproduced from ref. 42 with permission from Elsevier, copyright 2015.

the conversion of three medium-size MRFs from dual-stream to single-stream systems, avoiding the emission of 711 kg-CO<sub>2</sub>-equivalent per metric ton.<sup>84</sup> The advantages of switching from a dual to single stream were not observed on the economic side, as observed in a study conducted using data from 223 municipalities in the province of Ontario, Canada. For example, it was found that single-stream recycling incurs 48.7% higher processing costs and 9.6% lower values of a recyclable saleable stream compared to multi-stream recycling systems, with only a 3% reduction in the collection costs.<sup>85</sup>

Specifications were determined in the US in an effort to standardize the inbound recycling streams at MRFs, such as those stipulated by the Institute of Scrap Recycling Industries (ISRI).<sup>86</sup> Table 6 describes the materials accepted, prohibited, and the possible contaminants in the majority of US MRFs. It should be noted that plastic bags and films are considered contamination due to the possibility of issues during sorting and are removed early in the process. A pilot study conducted by Resource Recycling Systems (RRF) for the Materials Recovery for the Future (MRFF) on an existing MRF in Birdsboro (Pennsylvania, US) looked at how to modify an MRF design to accept flexible packaging from residential single-

stream inbound waste. It demanded additional equipment for separation, with a processing cost of \$2.41 per ton and a break-even point compared with the sorted polypropylene market value.<sup>87</sup>

**3.2.1 Equipment overview.** Over the years, several new technologies have been applied to the equipment used in a MRF to increase sortation efficiency, maximize the recovery of marketable materials, and deal with the increased complexity and diversity of inbound waste streams. As a connector for the whole processing facility, conveyor belts transfer material between different equipment, sort stations, and storage areas, including infeed conveyors that receive the material from the tipping floor up to the conveyors carrying the final bales of material for shipping.

Two types of conveyors are usually used: rubber and chain belt conveyors. Rubber belts are divided into two categories: slider beds, where the belt moves through a flat or shaped trough and is ideal for sorting with the material more spread-out, and idler conveyors, which have a belt over idler rollers perpendicular to the material movement, better suited for fine or gritty material. Chain belt conveyors are often employed when there is a need to move material through increased



**Table 6** MRF inbound waste stream specification (ISRI)<sup>86</sup>

Allowed materials			
Paper (single stream)	Plastic (single stream)	Metal (single stream)	Glass (single stream)
Paper (dual stream-separated) Uncoated white office, printing, and writing paper Colored paper  Newspaper and magazines Phonebooks and junk mail Tissue boxes/rolls, paper towel and toilet paper rolls Paperboard and Cardboard Brown or kraft paper Paper boxes/cartons, Pizza boxes (without food/liner)	Containers (dual stream – not mixed with paper) Empty PET (#1), HDPE (#2), PP (#5) plastic bottles, jugs, jars, and containers Bulky rigid plastics such as crates, buckets, totes, and baskets Tubes and lids Cartons	Aluminum, tin, steel beverage and product containers	Bottles and jars of any color
<b>Contamination (materials which will be sent to landfill)</b>			
Shredded paper	Flexible plastics (plastic bags and plastic film)	All metal except for those allowed	All glass except for those allowed
Containers coated with wax, plastic or other materials	Expanded polystyrene foam (#6)	Aerosol cans that are under pressure or partly filled	Drinking glasses, crystal, or tableware
Wallpaper	Multi-layered juice pouches		Mirrors
Material with excess food residue or other organic material	Plastic form electronics Plastic marked as biodegradable or compostable		Non-container glass Light Bulbs Windows
<b>Prohibited materials</b>			
Sharps and needles, batteries, radioactive materials, hazardous materials, corrosives, medical waste, pesticides, poisons, biohazards, compressed gas cylinders, refrigerants, polychlorinated biphenyl (PCB)-containing capacitors, transformers, and ballast, asbestos, wax, electronics, wood, ceramics, food waste, rock, dirt, asphalt, concrete, regulated materials, materials that can damage the equipment			

angles, such as feeding other equipment or weighty loads due to chain-link drive systems being more robust than rubber conveyors. The top speed for these conveyors is considerably slower.<sup>88</sup>

After entering the MRF environment, the waste stream passes through multiple separation equipment and operations. The simplest method is known as manual sorting, a labor-intensive step in the MRF operation and a source of potential health and occupational hazards,<sup>89</sup> including physical, chemical, and biological concerns. The sorting can be divided into a negative sort when undesired materials are removed from the waste stream and a positive sort that looks for recyclables and placement into the correct bin.<sup>90</sup> For the separation involving multiple material sizes into a specific range, different types of screens are commonly employed, such as vibratory, disc, trommel, ballistic, and, more recently, auger screens, as described in Table 7.

Air separation exploiting different densities of materials in mixed waste streams is another option at MRFs. A heavy fraction composed of metal, glass, and stones falls to the bottom of the equipment while a lighter fraction of paper, plastic, and dry organics is carried away by the air stream, requiring the use of a cyclone, for example, for the recycling of the air stream.<sup>90</sup> Equipment in this category includes zig-zag classifiers, air-drum or rotary air, aspirator air or suction hood, cross-current air, and airbed classifiers.<sup>88,90</sup>




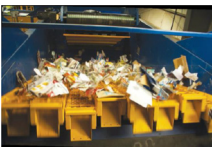

Another crucial piece of equipment typically used for material sorting is the optical sorter. The use of this type of equipment can substitute for manual labor and lead to high

sortation efficiencies; however, a significant capital cost is required for its installation, which hinders small and locally owned MRFs from selling bales in a market with low tolerance to contamination. An estimate using data from the United Kingdom by Eule showed that a MRF with a single operation shift could take up to 3.14 more years to break even after installing an optical sorter compared to manual labor.<sup>92</sup>

Optical sorters use color-sensitive cameras and near-infrared (NIR) and ultraviolet (UV) spectroscopy sensors, or a combination of them, to identify different materials that pass through a conveyor belt. Once the material desired to be positively sorted is identified, air jets are activated to eject the piece to a different chute.<sup>90,92</sup> Spectrometric techniques exploit the unique wavelength signature of different kinds of materials.<sup>88</sup> NIR optical sorters are most commonly used for plastic separation as a non-destructive technique with high-speed measurement, penetration depth and signal-to-noise ratio.<sup>91</sup> NIR optical sorter use has been growing for sorting fibers and cartons.<sup>93</sup> Another advance in sorting technology is the use of hyperspectral imaging (HSI), which combines imaging from a digital camera with spectrometric analysis, to obtain a discrete spectrum for every pixel collected. This is then computationally analyzed using algorithms such as principal component analysis<sup>94,95</sup> for the sorting of more complex plastic streams containing low and high density polyethylene, for example.<sup>96</sup> Machine learning algorithms are being studied to overcome some of the challenges associated with NIR sorters,<sup>97</sup> such as the difficulty of correctly sorting black plastics<sup>98</sup> or avoiding the still high costs of HSI technology.<sup>99</sup>



**Table 7** Common types of separation screens in MRFs. Reprinted from ref. 88 and 91, with permission from American Chemistry Council, CP Group Recycling Solutions, copyright 2016

Types	Description	Illustration
Vibratory (shaking)	The screen can be horizontal or inclined, with the waste stream cascading through a series of finger elements, perforated plates, or meshes, promoting material separation. Presents better performance when operating with dry and cleaner waste, as it can be easily clogged	
Disc	Rotating discs are positioned in shafts, moving the waste stream throughout the screen in horizontal or angled positions. The distance between discs (interface opening) is associated with the screened material size. Disc rolling might help by partially breaking the material on the screen. A specialized version of a disc screen that separates 2D (paper or film) from 3D materials (containers) can be called a polishing or planar screen	
Trommel (revolving)	Cylinder-mounted rollers in an inclined position contain holes in the sides and might have baffles. They are used for primary or final size screening. Factors that affect the input and separation efficiency include screen openings, trommel diameter, rotational speed, type and number of baffles, and cylinder inclination. Tumbling motion can be cascading, cataracting, or centrifuging	
Ballistic	Combines parallel paddles that vibrate (similar to a vibratory screen) with a 2D/3D screen framework. Three flows are collected: a fines stream with material that passed through the paddles, a 2D stream with paper, cardboard, and films, and a 3D stream mainly consisting of containers	
Auger	One of the newest types of equipment launched to the market consists of multiple cantilevered augers in corkscrewing motion, which prevents the wrap of plastic films and hoses. Mainly employed as a pre-sort step for removing large flat fractions such as (old corrugated containers) OCC from smaller objects	

For the sortation of ferrous materials, magnetic separators are used to sort materials such as steel from the remaining waste stream. Multiple factors are considered to determine the system's efficiency, including the distance between the conveyor carrying the waste stream and the magnet, the magnetic force employed, the conveyor speed, and the burden depth on the conveyor belt. Common types of setup include a drum holding magnet, a belt holding magnet, and a suspended type magnetic separator.<sup>100</sup> For non-ferrous materials, such as aluminum and copper, eddy current separators are used, often after the magnetic separator. The sorting is based on the eddy currents formed when conductive objects are close to a magnetic field (created using rotating magnets), with another magnetic field of opposite direction. According to Lenz's law, this creates a force that expels these objects from the initial magnetic field, giving them a different trajectory. Considering that less dense and conductive objects demand a lesser force, aluminum has the greatest potential for separation through this equipment since it has one of the highest conductivity/density ratios compared to other metals, such as lead, copper, zinc, and tin.<sup>90</sup>

At the end of the sorting process, each material stream is compacted or densified to reduce its volume to minimize storage space requirements and increase payload for recyclable material and residue transportation, significantly reducing costs.<sup>90</sup> Balers are commonly used to reduce the bulk density of the material and can be divided into two different types: vertical balers, an option with reduced output but low costs, or horizontal balers, which are the most utilized in MRFs.<sup>101</sup> Horizontal balers are usually single-ram or dual-ram (two-ram), with the first mainly used for fiber, paper, and OCC output lines, while the latter is considered a multipurpose equipment utilized for plastic and aluminum outputs due to its capacity to produce more heavy and uniformly packed bales.<sup>88,102</sup> Single-ram balers operate with the sorted material being pushed from a collection chamber into a narrow hopper, with the densified material moving continuously as more material is fed and tied with wires. On the other side, a dual-ram baler (Fig. 11) has the main ram that loads the material into a chamber until the desired amount is achieved, while a secondary ram is responsible for moving the bale to a tying process.<sup>88</sup>

The Association of Plastic Recyclers (APR) has developed some specifications to standardize plastic bales and facilitate the sales between MRFs and recycled plastic reprocessors, brokers, or companies that can use them in their process. For rigid plastic containers bales, including natural and colored HDPE, PP, and #1–7 plastics, it is expected to have a bale density between 15 and 20 lb ft<sup>-3</sup> (240 and 320 kg m<sup>-3</sup>), whereas, for a PET bottle bale, the targeted bale density is between 15 and 18 lb ft<sup>-3</sup> (240 and 288 kg m<sup>-3</sup>), all using non-corrosive galvanized bale wires of 10–12 gauge (2.6–3.2 mm).<sup>103</sup> The main products of a MRF are the bales of sorted material with the ultimate goal of producing saleable recycled material and the least amount of non-recyclable residues. In the optimal scenario, these residues can be used as





Fig. 11 Two-ram Baler from Machinex Recycling. Reproduced from ref. 104 with permission from Machinex Technologies, copyright 2022.

Table 8 Outbound mixed plastic bale specifications (ISRI)<sup>86</sup>

Bale type	Material description	Main product	Allowed contamination
#1–7 bottles and small rigid plastic	Rigid plastics, consisting of at least 65% bottles, bulky rigid containers greater than 5 gallons should be avoided	Bottle and non-bottle containers	5 wt% total, with less than 2 wt% paper/cardboard and 1 wt% of metal/plastic bags/liquid/other residues
#3–7 bottles and small rigid plastic	Rigid plastics without PET (#1) and (#2), bulky rigid containers greater than 5 gallons should be avoided	Bottle and non-bottle containers	5 wt% total, with less than 2 wt% paper/cardboard/metal and 1 wt% of liquid/other residues
Mixed bulky rigid (#2 and #5)	Large rigid plastics HDPE (#2) and PP (#5)	Bulky rigid plastic	15 wt% total, with less than 4 wt% for plastic/packaging items (#1, #3, #6, #7), 2 wt% of metals, glass, wood, liquid/other residues, paper/cardboard, plastic bags/sheets/films
Tubes and lids (#2, #4, and #5)	Any whole container of HDPE (#2), LDPE (#4), and PP (#5)	Tubes and lids	10 wt% total, with less than 2 wt% of metals, liquid/other residues, paper/cardboard, injection-molded HDPE (#2), PET (#1) bottles and thermoforms, plastic/packaging items (#1, #3, #6, and #7)

fuel for waste-to-energy conversion, in anaerobic digestion or, in the worst case, be an expense for discard in a landfill. For plastic bales, the ISRI Scrap Specifications Circular defines standards for some of the most common types of bales from a MRF in terms of composition, contaminants, and prohibited items, as shown in Tables 8 and 9. The historical prices for some plastic bales are listed in Table 10.

**3.2.2 MRFs in Europe vs. the US (typical size, numbers of MRFs in US).** According to the Environmental Protection Agency (EPA) there were 532 MRFs in the US in 2018 with an

estimated daily throughput of 91 129 tons.<sup>106</sup> The Recycling Partnership conducted another survey with data from Resource Recycling, initially finding 360 MRFs in the United States in 2019, a number that was updated in February 2020 to 367 after a verification conducted by The Last Beach Cleanup (a nonprofit 501(c)3 organization), with a spreadsheet available on their website<sup>107</sup> and results published by Greenpeace.<sup>108</sup> The distribution of MRFs across the U.S. is shown in Table 11. A list of the largest 75 MRFs in North America was published in 2019 by Recycling Today, with 65 located in the United States and 10 in Canada. The largest MRF was Sims Municipal Recycling's Sunset Park, located in New York, which shipped 241 884 tons in 2018.<sup>109</sup> In England, data from the last quarter of 2019 totaled 85 regulated material facilities (>1000 tonnes per year recyclables processed and required to submit their data to England's Environmental Agency), resulting in daily input of 9237 tonnes. In Wales, there were 12 facilities in the same year, with daily input of 710.6 tonnes.<sup>110</sup> Ali and Courtenay<sup>111</sup> observed from data that approximately 60% of United Kingdom MRFs have an annual capacity higher than 50 000 tonnes. Italy had 33 facilities for plastic sorting ("centri

Table 9 Outbound PET and HDPE plastic bale specifications by grade (ISRI)<sup>86</sup>

	Bale grade	Grade A	Grade B	Grade C	Grade F
PET (#1)	Total fraction (wt%)	>94	93–83	82–73	<72
	Max. contamination (wt%)	6	7–17	18–27	>28
HDPE (#2)	Total fraction (wt%)	>95	94–85	84–80	<79
	Max. contamination (wt%)	5	6–15	16–20	21



**Table 10** Historical prices for some plastic bales<sup>105</sup>

Materials Year	National average price (cents lb <sup>-1</sup> )					
	2017	2018	2019	2020	2021	2022
Plastics PET (baled)	11–16	14–17	9–15	6–11	7–26	18–25
Plastics film (grade A, sorted, 800 + lb bales)	8–11	8–12	9–12	8–11	11–21	21
Plastics Natural HDPE (baled)	24–33	30–39	20–59	33–64	56–108	55
Plastics colored HDPE (baled)	13–17	14–17	10–16	4–14	17–58	20
Plastics commingled (#1–7, baled)	2–3	2–3	2	1–2	1	1
Plastics PP post consumer (baled)	7–9	8–11	7–13	3–12	12–39	19–23
Plastics polystyrene EPS (baled)	2	2	2	2	2	2

**Table 11** Number of MRFs in the United States<sup>106,107</sup>

Region	Number of MRFs	
	EPA (2018)	The last beach cleanup/Greenpeace (2020)
Northeast	128	66
South	142	107
Midwest	139	76
West	123	118
<b>Total (U. S.)</b>	<b>532</b>	<b>367</b>

di selezione” – CSS) in 2020 associated with COREPLA (National Consortium for Collection and Recycling of Plastic Packaging) that receive a pre-sorted waste stream mainly composed of mixed plastics from 996 smaller and local sorting centers (“centri comprensoriali”).<sup>112,113</sup> Germany’s federal statistics reported 987 waste sorting facilities in 2019, with a total input of 25 120 700 tonnes.<sup>114</sup> In France, it was reported that 399 waste sorting facilities (“centres de tri de déchets”) were operating in 2016, receiving 11.1 million tons.<sup>115</sup>

**3.2.3 Waste pickers in Latin America.** In less economically developed countries, recycled material is typically manually removed from MSW by human “waste pickers”. A key issue in MSW management and/or waste recycling in developing countries is the role of waste pickers, who collect, haul, sort, and sell recyclable commodities from MSW. There are around 20 million people worldwide informally dedicated to waste recycling, which represents approximately 50% of the workers involved in waste management. In developing countries, this informal recycling sector recovers the largest fractions of recycled waste and in some cases, it is the only organized form of recycling.<sup>116–118</sup> In Latin American, waste pickers are recruited among vulnerable groups living under conditions of extreme poverty in communities that lack the educational, social, and psychological resources to prepare its citizens for more formal and remunerative employment. Another factor is the deficiency in MSW management systems in urban and rural areas. Under these conditions, waste collection and recycling offer waste pickers one of the few opportunities to support their families.<sup>116,118,119</sup>

In this section we discuss waste pickers in PET recycling in Mexico to illustrate the challenges in Latin America. Mexico is the second largest PET bottle consumer in the world, mainly

due to the high consumption of soft drinks and bottled water.<sup>120,121</sup> The high consumption of PET bottles, many of them discarded in public places, roads and transport systems and rural areas, combined with a lack of recycling programs caused environmental and health problems, and the clogging of drainage systems in urban areas. Since the mid-1990s, the Mexican government has set voluntary PET recovery and recycling programs that were successful to some extent.<sup>121</sup> PET recycling activities involve sorting, washing, re-granulating and pellet production by local enterprises. The pellets are then shipped to domestic Mexican plastic transformation industry (35%) or exported to other markets (65%). In Mexico, recycled PET facilities produce textile fibers, bottles for non-food uses and industrial strapping.

In Mexico, recycling of the MSW is mostly in the hands of waste pickers, middlemen or brokers.<sup>122,123</sup> Waste pickers are self-employed, sometimes resorting to collecting plastics from neighborhood garbage containers before they are collected by contracted waste management services. Waste pickers often organize themselves into associations, cooperatives, unions or microenterprises, through which they feel empowered to carry out their activities.<sup>116,121</sup> Often local authorities promote and recognize the formation of associations or cooperatives, which are able to negotiate agreements for waste collection and recycling services. However, even with these associations the waste pickers income is not fixed but based on the quantity and quality of recycled materials and the selling price in local markets.

Currently, recycled PET price depends on factors such as impurities (*i.e.*, amount of other plastics or residues), quality (*i.e.*, clear *vs.* color PET), cleanliness, type of organization the waste pickers belong to, middleman or broker who buys the product, and even the geographical area (*i.e.*, urban *vs.* rural) where PET is collected and sold. An average price for recycled PET ranges between \$0.24–0.48 per kg,<sup>105</sup> although it is likely that most waste pickers receive the lowest price. Waste pickers who recycle PET must work long hours to obtain sufficient income to support their families. The official minimum daily wage set by the Mexican federal government was \$8.25 per day in January 2022. If an average recycled PET price of \$0.36 per kg is considered, a waste picker must collect around 23 kg of PET every day to receive the equivalent of the minimum daily wage. A number of studies highlight the low monthly income



(\$120–360 per month) by waste pickers in Latin America.<sup>124</sup> There is an urgent need to propose business schemes that improve the income of waste pickers, in addition to providing them health, safety, labor and social benefits through formal employment. The development of business models in Latin America that formalize the inclusion of waste pickers in the recycling value chain, and that limit the actions and profits of middlemen, will have social benefits for waste pickers and will bring favorable economic benefits for the Mexican recycled PET industry.

Some successful initiatives show that when waste pickers are organized by non-profit and for-profit organizations and they are formally included in the PET recycling value chain, a number of favorable social and economic benefits occurs.<sup>118</sup> Social-oriented programs for waste pickers lead to their recognition and empowerment through the establishment of formal jobs, with fixed salaries and labor and health benefits with local government or private companies. Social-oriented programs may have a profound impact on the education and culture of waste picker's communities. These social-based initiatives are emerging in the MSW management value chain of Mexico, Brazil, Argentina, Colombia and Chile, but the benefits are still limited to a few communities. In the current socio-economic situation in Latin America, the development of technologies and industries that facilitate the processing of plastic waste into products with higher added value in the market, is a critical factor to facilitate the inclusion of waste pickers in the value chain of plastic recycling.

MSW from urban and rural areas is typically processed by public services run by local governments to avoid negative impacts on health and the environment. In countries such as Mexico and Brazil, the management of MSW is regulated by federal and local laws, which establish guidelines for the collection, separation, recycling and final disposal of waste, using strategies that, in principle, contribute to the preservation of the environment and take care of the health and safety of the employees.<sup>118,119</sup> Various technological, economic, administrative, social and cultural factors prevent risk and safety management from being carried out properly, especially in rural areas. As a result, it is estimated that around 40 million people (6% of population) in Latin American communities lack trash service. Up to a third of MSW is disposed in open dumps.<sup>125–128</sup> Consequently, the prevailing situation is that the MSW management in Latin America is a focus of concern in terms of public health, environmental risks, informal economy, security and social inequality, particularly for the communities where the MSW transfer units and final disposal sites are located.

A license is granted to private companies when MSW cannot be adequately collected by local governments. A growing number of companies in Latin America offer the following benefits in MSW management: a reduction in public spending, selective processing of domestic, commercial, and industrial waste, use of specialized technology and skilled workforce, generation of well-paying jobs, and management projects contributing to sustainable development.<sup>129,130</sup> This

recycling strategy is very distinctive from the circular economy and it has been identified as a vector contributing to the fulfillment of Sustainable Development Objectives set by the United Nations. For this reason, federal and local governments in Latin American communities have established legal frameworks to trigger waste recycling, as in the case of Brazil, which in 2010 established the National Solid Waste Policy, and Mexico, which in 2003 approved the Law for the Prevention and Integrated Management of Waste, and very recently the General Law of Circular Economy with the aim of promoting efficiency in the use of waste through reuse and recycling.<sup>119,131–133</sup>

Poverty and the growing market value of recyclable products has induced many people in conditions of social and economic vulnerability to work as waste pickers. It is very common nowadays to find fixed human settlements around waste transfer and final disposal units. Entire families live in these settlements. It is common for waste pickers' children to continue with the family tradition. The situation of waste pickers is similar in other countries that do not have a modern waste management system.<sup>134</sup> The development of advanced waste management systems combined with new plastic recycling technologies will drastically improve the quality of life for waste pickers.

## 4. Mechanical recycling

Mechanical recycling is defined by the U.S. Food and Drug Administration (FDA) as secondary recycling and is the most common approach for recycling plastic solid waste (PSW). This process has an established infrastructure in most countries. In secondary recycling, the post-consumer plastic waste is reprocessed and converted into new materials.<sup>135</sup> With the advancement and availability of mechanically recycled PSW, virgin plastics are substituted with post-consumer recycled materials or blends thereof in many industrial and consumer applications.<sup>136,137</sup> Mechanical recycling involves collection/segregation, cleaning and drying, chipping/sizing, coloring/agglomeration, pelletization/extrusion, and manufacturing the end product. Both primary and secondary recycling involve similar process steps.<sup>138</sup> Primary recycling as defined by the FDA recovers pre-consumer or post-industrial recycled (PIR) waste material and produces new products. Secondary recycling physically reprocesses post-consumer waste materials to produce new materials.<sup>139</sup> Primary recycling maintains the same quality as virgin material, whereas downcycling is common in secondary recycling due to some degradation of the plastic's properties.<sup>136</sup> Post-consumer materials, in particular polyolefins, can have unpredictable physical properties due to the large range of polymer structures, molecular weights, and additive packages. Such variation and lack of grading can make using these materials more difficult. The variation in color further complicates usage in new products due to the inability to control the final colors. For example, plastic



materials having different colors produce undesirable grey color after reprocessing into pellets.<sup>140</sup>

#### 4.1 Processing technologies in mechanical recycling

Mechanical recycling consists of a few general steps: shredding/granulation, contaminant removal, followed by flake segregation. The primary step involves the melting and re-extruding of the plastic into uniform pellets<sup>136</sup> which can then be utilized in cast/film extrusion, injection molding, blow molding, *etc.*<sup>136,141</sup> The molecular weight of a plastic is highly influential to all the plastic's innate properties.<sup>142–144</sup> In general, an increase in molecular weight increases the glass transition temperature, the melting temperature, plastic strength, elasticity, stiffness, toughness, and viscoelastic properties. The processing residence time and reprocessing of the material also influence the molecular weight of the polymeric materials.<sup>32,145–147</sup> Fig. 12 demonstrates the change in melt-flow index (MFI) of various plastics subjected to extrusion and injection molding. The repeated exposure to high heat, time, and shear rates can cause degradation of the polymeric material, and in some cases, unwanted side reactions that can either increase or decrease the molecular weight of the final product. These structural modifications lead to changes in both flow and mechanical properties of the material. Manufacturers may be inclined to utilize additives to recover material properties or homogenize the recycled material, although this typically adds cost to the recycled plastic and may further complicate future recycling attempts of the material waste. Different variations of mechanical and thermal processing technologies (Fig. 13) used in recycling are described below.

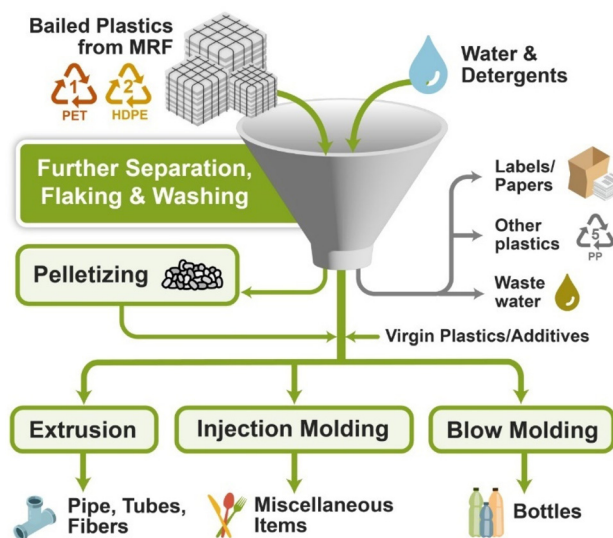


Fig. 13 Various approaches for mechanical recycling of PSW (plastic solid waste).<sup>136</sup>

#### 4.2 Extrusion molding

In extrusion molding, plastic pellets enter the hopper into the barrel of the extruder in a continuous process. The plastic is fed into the barrel in the screw feed zone, and the screw forces raw material through the hot barrel and causes melting. The constant moving of the plastic through the barrel restricts overheating and limits residence time, which may degrade the plastic.<sup>148</sup> Because of the heating during extrusion, some alteration to the polymer chain occurs. The plastic melt in the barrel passes through screen packs to remove gross contami-

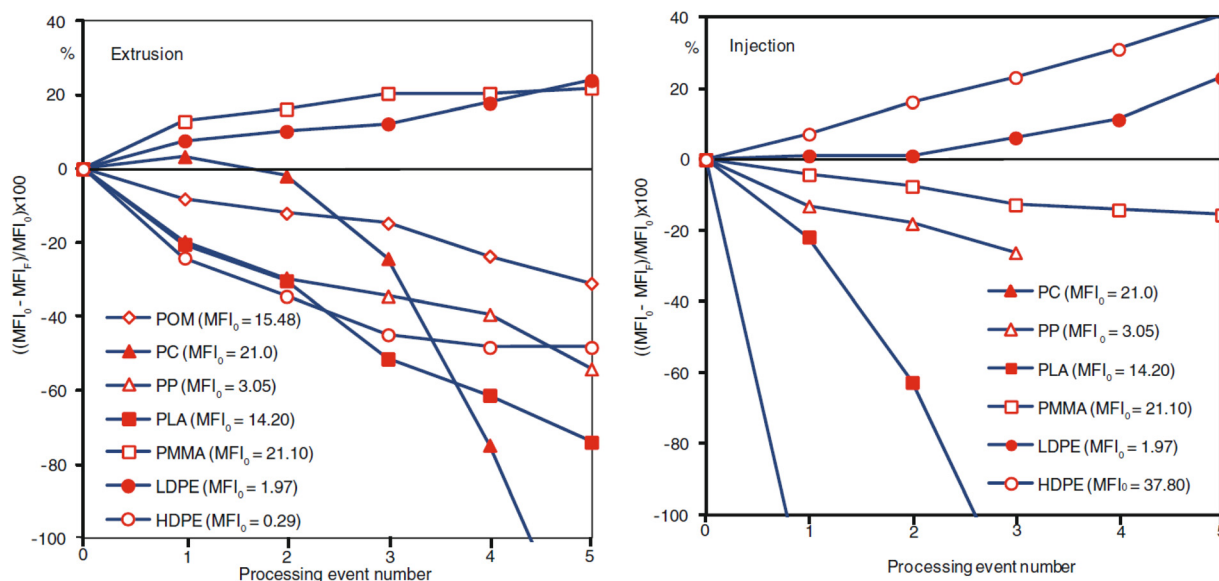


Fig. 12 Change in MFI as a function of number of processing events for extrusion (left) and injection molding (right). MFI<sub>0</sub> and MFI<sub>F</sub> are the MFI prior to any processing event and the MFI after the total processing events, respectively. Published from ref. 32 with permission from Carl Hanser Verlag, Munich, copyright 2012.

nants during the extrusion process. The screen pack and breaker plate are found in commercial plastic extrusion between the extruder and the die. Melted plastic is re-shaped using a die.<sup>136</sup> The breaker plate ensures the proper mixing in the screw of the plastic by creating backpressure and reorients the plastic creating a stable linear flow before entering the die. Uneven flow of the molten plastic into the die can create undesirable residual stress that can cause warping during the cooling stage.<sup>148</sup> The extrudate is cooled with a water bath or cooled air stream. This process is complicated as plastics are good thermal insulators.<sup>148</sup> The extrusion process for recycling is similar to a new product manufacturing technique. Details of extrusion molding, injection molding, blow molding, film molding, and fiber processing can be found in SI 2.0 in ESI†.

### 4.3 Mechanical reprocessing of PET

Bailed PET often contains a large number of contaminants including adhesives, sugars, and other plastics. It is important to clean the PET and separate it from other materials before it is melt-processed through extrusion to produce recycled PET pellets (rPET).<sup>149</sup> Fig. 14 illustrates a typical PET bottle recycling process which is adapted from one of the PET bottle recycling companies in Europe.<sup>150</sup> The delivered bottles are sorted depending on the type of material, color, processing method *etc.* The bottles are then shredded into small flakes followed by washing processes. The flakes go to the extruder after cleaning and drying.

Melt extrusion of clean washed PET flake or granules is used to manufacture pellets of uniform shape for subsequent manufacturing processes (injection molding, extrusion, injection stretch blow molding, *etc.*).<sup>151</sup> When PET reprocessing

uses an established facility, processing becomes more cost-effective, more straightforward, and possesses less environmental impact. Switching from virgin to recycled PET depends on material pricing, secure recycled material supply chains, and the ability to use existing facilities.<sup>152</sup> Processing PET at high temperatures may cause chain degradation which influences crystallinity of the plastic.<sup>146</sup> Plastic degradation from chain scission causes molar mass plastic decrease, which makes bottle-to-bottle recycling challenging.<sup>153</sup>

rPET can be used for most applications instead of virgin materials provided that the properties meet the quality criteria. Clarity and yellowing are major property challenges for rPET.<sup>137</sup> Like other plastics, PET's quality is also affected by chain degradation because of thermo-oxidation.<sup>154,155</sup> Some contaminants (such as PVC and polyvinyl alcohol) accelerate chain scission in PET plastic during melt processing due to acidolysis.<sup>156,157</sup> Impurities in PET enhance chain scission reactions, and traces of PVC and polylactic acid (PLA) can accelerate acidolysis or hydrolysis. These reactions alter the plastic's microstructure and the mobile amorphous region is altered causing thickening of the crystalline domains.<sup>155</sup> Crosslinking can also occur, resulting in increased viscosity in PET, hindering processability for applications such as injection molding. The multipole extrusion cycles of mechanical recycling increase the rate of chain scission because of thermo-oxidation.

Compounding additives into rPET during reprocessing can protect the plastic from chain scission and improve mechanical properties. To minimize thermo-oxidation of the plastic, metal-based stabilizers are often used.<sup>154</sup> The use of radical scavengers, such as organic phosphates, is another option to

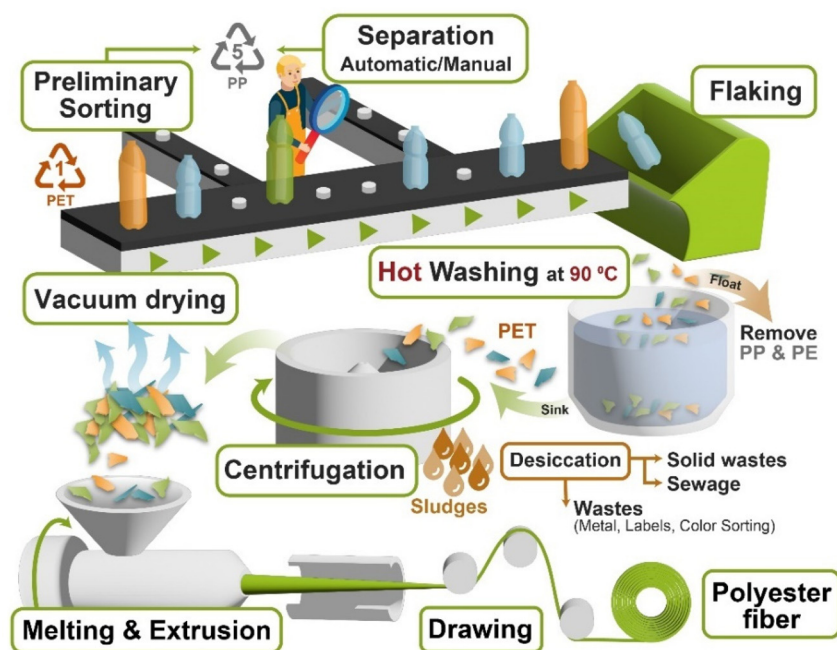


Fig. 14 A generalized process flow diagram for a recycling of PET bottles.<sup>150</sup>



hinder radical induced oxidation of the terephthalate ring, which is a source of yellowing.<sup>155,158</sup> The most common problem in PET reprocessing is viscosity reduction (molecular weight reduction) due to hydrolytic degradation and thermal oxidation. Color change in the post-consumer PET is another vital problem and normally the industry solves the problem by “open-loop recycling” or “semi-closed-loop recycling”.<sup>154</sup> The concepts of “open-loop recycling” or “semi-closed-loop recycling” are described in section 4.3.1.1.

If the molecular weight reduction is less severe, the plastic can be subjected to a process called solid state polymerization (SSP) to help rebuild the molecular weight.<sup>159</sup> The plastic is heated to a temperature between the melting and glass transition temperatures to induce esterification and transesterification reactions.<sup>153</sup> Industries are currently looking for a new stream of PET waste to reprocess, including colored PET.<sup>160</sup> For example, in 2018 ‘Indorama Ventures’ partnered with ‘Unilever’ to recycle fifty billion bottles per year by 2025, including colored PET. According to them, traditionally non-recyclable colored PET is subjected to a chemical recycling process. These colored PET are reduced to monomeric species, and then the contaminants removed before being used as raw material for polymerization. This technology produces transparent food-grade PET plastic material from post-consumer PET.<sup>161,162</sup> Recycling for food contact packaging requires a very demanding and clean plastic. No Objection Letters (NOLs) by the Food and Drug Administration are often sought by recyclers and manufacturers to demonstrate that their recycling process and materials are suitable for direct food contact applications.<sup>163</sup>

Continuous improvements in plastic reprocessing is an ongoing effort with new technologies in degassers and filters to facilitate increased plastic melting quality.<sup>164</sup> Degassing employs a vacuum vent on the extruder to enable volatile compound stripping from a plastic melt. This stage reduces hydrolysis by removing moisture and adds value by producing a high-quality plastic with maintained molecular weight and decreased contamination. The addition of a filter helps remove unwanted non-volatile contaminants from the plastic and increases the mechanical properties of the recycled plastic.<sup>165</sup> When selecting recycling technologies in manufacturing processes, it is important to select the appropriate mechanism to minimize the degradation of the plastic for high-quality new parts.<sup>155</sup>

#### 4.3.1 Utilization of recycled PET waste

**4.3.1.1 Closed-loop and open-loop recycling.** The recycled raw material supply increases as plastic waste collection increases. These raw materials can be used to produce new material as ‘open loop’ or ‘semi-closed loop’ or ‘closed loop’ recycling.<sup>166</sup> Closed-loop recycling means the recycled raw material is used for the same product and fully replaces the virgin material, e.g., PET bottle to bottle recycling. Open-loop recycling means the recycled material is used for a different product and fails to replace the virgin raw material in the original application, also referred to as downcycling. The inherent properties of raw materials for open-loop recycling are often

too degraded by the service life and recycling process and the plastic cannot be used in the original application. Semi-closed recycling means the recycled raw materials are used to produce another type of product but cause no change in the inherent properties of the recycled materials.<sup>167</sup>

**4.3.1.2 Recycled PET products.** rPET is incorporated to form a wide range of new products, for example, shoes, bags, fibers, boards, mechanical parts, etc., as open-loop recycling. Most rPET is used for fibers.<sup>168</sup> Consumers can currently purchase rPET food packaging containers. According to a 2020 NAPCOR (National Association for PET Container Resources) Report post-consumer rPET used in the US and Canada has continuously increased since 2004. It has been predicted that by 2026 the market will reach up to \$12.5 billion, representing an ~8% Compound Annual Growth Rate (CAGR) from 2019 to 2026.<sup>168,169</sup> The NAPCOR Chairman mentioned that post-consumer rPET utilization is proceeding towards a circular economy. According to NAPCOR, fiber sectors made up more than 40% of the worldwide rPET market in 2019.<sup>170</sup> The fiber market includes manufacturing mattresses, insulators, car equipment, etc. Asia Pacific plastic industries are increasing their dependency on rPET. Colored rPET is used for food and non-food applications for its stability and strength. These have high popularity as they are lightweight and provide strength for a long period.<sup>168</sup>

#### 4.4 Mechanical reprocessing of polyolefins

Mechanical processing of polyolefins also induces degradation at the molecular level and the formation of aldehydes, ketones, and short-chain hydrocarbons.<sup>171–173</sup> The degradation mechanism is different in each type of polyolefin. The general degradation mechanisms begin with the generation of macro-radicals within the molecular chain. This radical creates many shorter, branched, or cross-linked polymer chains. When these radicals react with oxygen centered radicals, further degradation occurs.<sup>174</sup> Previous studies have demonstrated that HDPE is more prone to crosslinking whereas PP shows a large number of chain scission events. These degradation reactions mainly occur in the amorphous phase below the plastic’s melting temperature because oxygen cannot diffuse into the crystalline phase.<sup>155</sup>

As post-consumer plastic films are contaminated with various waste materials, an intensive pre-treatment is crucial before extrusion. The source of raw material in secondary recycling is MSW mixed with other plastics. This needs an initial separation step to separate the contaminants. The mechanical recycling process described here (Fig. 15) is an example of a European processing facility.<sup>175</sup> The process starts with comminution of large plastic parts and shredding/sieving to remove as much of the contaminants (metals, glass, paper, etc.) as possible. The contaminant-free plastics are sent for pre-washing then vigorous washing to avoid micro-physical contamination. Afterward, the material enters the hydrocyclone to separate undesirable particles.<sup>175</sup> A friction washer is used for washing to consistently remove contaminants from the plastic such as labels, glue, or organic dirt on the



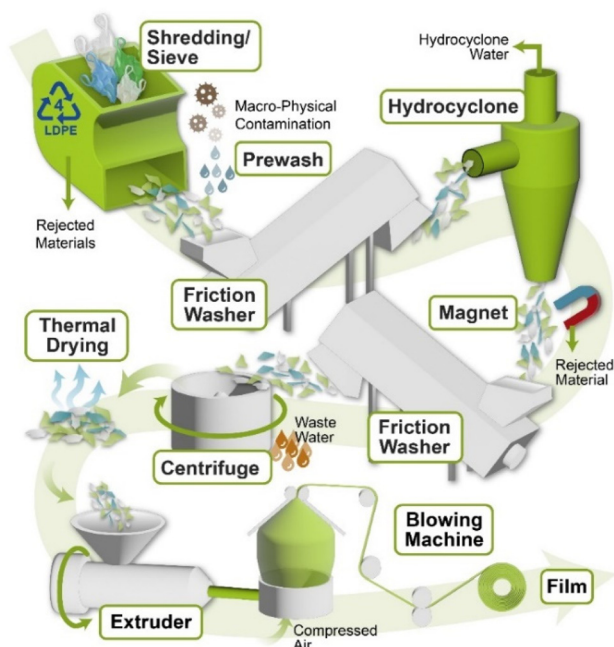


Fig. 15 Mechanical recycling process of polyethylene plastic film at an industrial plant.<sup>175</sup>

surface.<sup>176</sup> After washing, the plastics are dried thermally to lower the moisture content before entering the extrusion and pelletizing stage.<sup>175</sup> The function of extruder and blowing machines are discussed above. The quality of the recycled plastic film is degraded leading it to be used in applications such as products for constructions, public spaces, and traffic applications after injection molding or extrusion.<sup>177</sup>

**4.4.1 Mechanical processing of HDPE.** HDPE is a linear chain plastic with high molecular weight produced from carbon and hydrogen atoms. As this plastic has a straight chain, it has more strength than LDPE. It is an important component of MSW as this waste plastic has high recyclability potential.<sup>136</sup> Commercially, two kinds of HDPE are often found in MSW depending on either the extrusion process or injection molding; each type differs in its viscosity.<sup>155</sup> Like other plastics, chain scission and chain branching are also common in HDPE during the extrusion process. Generation of carbonyl groups in HDPE increases when the oxygen in the surrounding atmosphere is high. When oxygen is low, double bond formation is observed in the molecular backbone.<sup>178</sup> Because of these reactions, the HDPE molecular weight is reduced. When the plastic chain length is lower, the plastic becomes vulnerable to degradation by radical attack. This scenario worsens with each extrusion cycle. Studies have also shown that the viscosity in the plastic reaches a very high level (five fold higher than the starting level) after sixty extrusion cycles due to crosslinking in chains.<sup>155</sup> These degradation effects can partially be mitigated *via* controlling extruder parameters such as temperature, screw speed and screw design.<sup>179</sup>

Recycled HDPE and other recycled polyolefins have multiple applications in the food packaging sector and multilayer

packaging applications. However, there is a concern with recycled raw material in direct food contact because potentially toxic small molecules (plasticizers, stabilizers, *etc.*) could diffuse and migrate into food products.<sup>180</sup> As a result, recycled polyolefins are often utilized as the middle layer in multi-layered packaging, and the surface layers are made of virgin plastics. Recycled HDPE has a large market as the processing cost can be relatively low. Post-consumer HDPE is a feasible option to produce plastic lumber which is a replacement for wooden lumber.

#### 4.5 How legislation changes the scenario

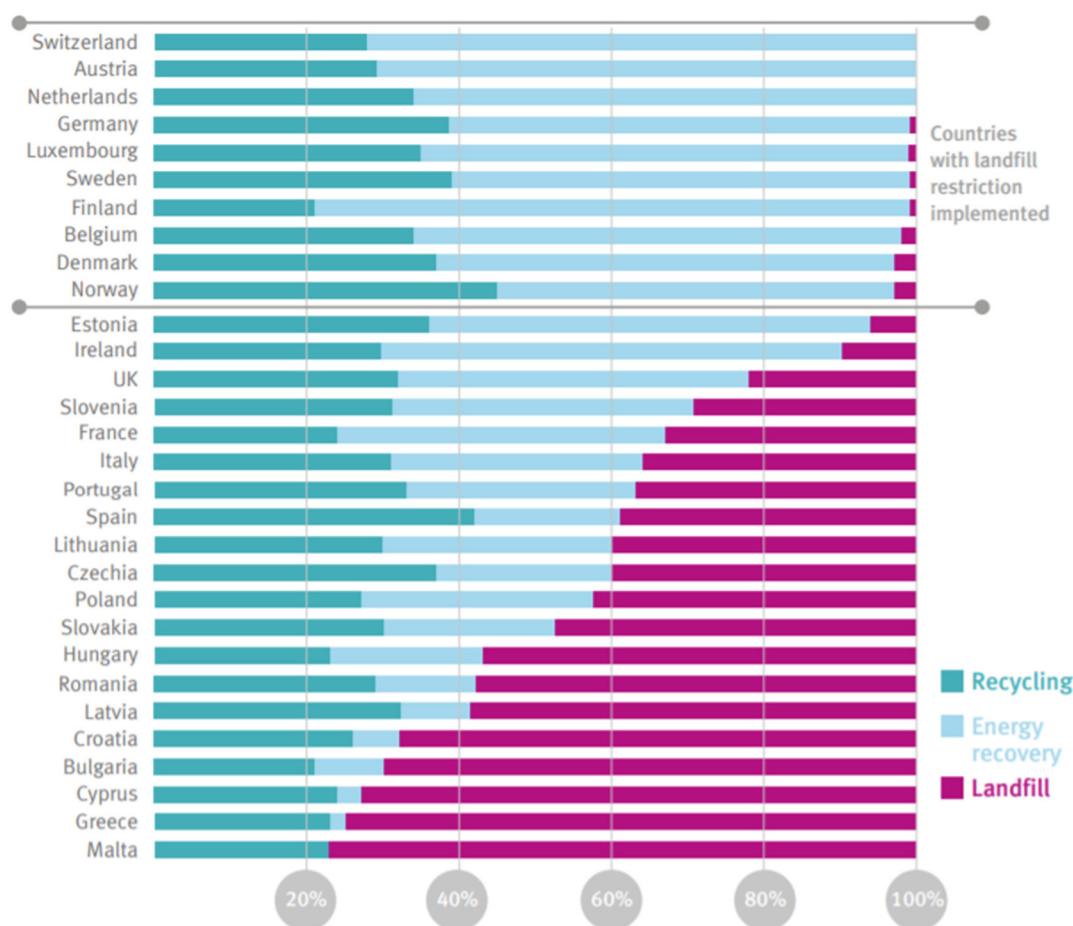
The municipal waste management system and plastic recycling in most European countries has made remarkable advancement. EU countries with landfilling restrictions or bans have higher recycling and waste recovering percentages as shown in Fig. 16. Recycling of HDPE, LDPE, PET, PP, and PS plastics are performed together.<sup>181</sup> Post-consumer plastic waste collection was more than 32% in several EU countries which was mostly comprised of mechanical recycling techniques. The highest recycling rate was found in Norway at 45% in comparison to ~9% in the United States.<sup>137,182</sup>

The number of recycling companies is increasing. There are almost 115 PET recycling and 40 PE recycling facilities in the US. For example, '77 recycling' is a plastics (post-industrial plastic scrap) recycling company that accepts most materials (PET, PP, PS, PVC, HDPE, LDPE, *etc.*).<sup>183</sup> China's ban on imports of plastic waste increased the recycling facilities across the US.<sup>184</sup> Good communication between product manufacturers and the recycling industries is needed to confirm the recycling of packaging materials. This communication can strengthen the use of recycled raw materials and create a new market for these recycled plastics.<sup>185</sup>

**4.5.1 Utilization of mechanically recycled post-consumer materials as food contact materials (FCM).** The most valuable type of recycled plastic is plastic that can be used for food packaging applications. In the US the FDA employs regulations regarding the safety of the use of recycled plastic materials as food contact materials (FCM).<sup>187</sup> The FDA expresses their concerns and regulations maintained for using recycled plastic:

- When recycled plastic/material is used as FCM, the chance of contaminants in the final product may increase.
- Post-consumer recycled plastic/materials are permissible to use as FCM material.
- The adjuvants (for example petroleum waxes, synthetic petroleum wax, colorants, plastic modifiers<sup>188</sup>) coming from the post-consumer recycled plastic/material may not be suggested for use in FCMs as the contaminant present in the recycled material can pass on to the new product and migrate into the food matrix.<sup>189</sup>
- The FDA regulates the plastic recycling processes to ensure that the recycled materials are not contaminated and that the recycling process is suitable for direct food contact.<sup>163</sup> For example, in secondary recycling, the physical reprocessing steps, grinding, melting, and reforming, are documented and submitted for evaluation to obtain a favorable opinion letter





**Fig. 16** Post-consumer plastic waste recycling rate, energy recovery rate and landfilling rate per European country in 2018. Reproduced from ref. 186 with permission Plastic Europe, copyright 2022.

through the No Objection Letter (NOL) program. For plastic depolymerization, it is necessary to confirm that the monomers are contamination-free and the produced plastic is the same as that from virgin monomers.<sup>190</sup>

- In the case of multi-layered packaging, sometimes, when proper contamination removal is complex, the recycled layer is used as the most outer layer. For example, for recycled PET, FCM is used as the outer layer in multi-layered containers, and the inner layer in contact with food is made of virgin material.<sup>155</sup>

Manufacturers of FCMs using post-consumer recycled materials often need special evaluation.<sup>163</sup> The NOL determines the assessment of the plastic used for a FCM and whether the recycling process is physical or chemical. The earliest NOL<sup>191</sup> was issued in 1990 for a physical recycling process of whole egg cartons.<sup>192</sup> Many of the early NOLs that granted favorable opinions were for PET and PS plastics.<sup>193</sup> However, in recent years, much of the focus has been on polyolefin materials; utilization of post-consumer polyolefin streams for direct food contact applications is challenging due to a large number of different molecular structures, additive packages, and uses for which consumer abuse can lead to incidental con-

tamination.<sup>194</sup> Such challenges are overcome through careful source control of the post-consumer material and challenge surrogate chemical testing to determine if the recycling process can reduce the concentration of different types of compounds, which is often a requirement for the NOL process.

For the surrogate chemical challenge testing, the plastic is soaked in a chemical cocktail containing a volatile polar compound (e.g., chloroform, chlorobenzene, 1,1,1 trichloroethane, diethyl ketone), a non-volatile polar compound (toluene), a heavy metal compound (copper(II) 2-ethylhexanoate), non-volatile polar (benzophenone or methyl salicylate), and a non-volatile non-polar compound (tetracosane, lindane, methyl stearate, phenylcyclohexane, 1-phenyldecane, 2,4,6-trichloroanisole) using an isopropyl/hexane solvent delivery mixture to artificially contaminate the plastic.<sup>163</sup> After the artificial contamination soaking of two weeks at 40 °C, the spiked plastic is subjected to recycling. The concentration of the artificial contaminants is quantified in the recovered, recycled plastic and the starting spiked plastic to demonstrate the ability of the recycling process to reduce contamination. These results, along with a description of the recycling procedure and post-consumer material feedstocks, are submitted to the FDA to evaluate



suitability for manufacturing direct FCMs. Upon favorable review of the packet, a NOL is issued. As of the end of 2021, 254 NOLs have been issued by the FDA.<sup>192</sup>

## 5. Thermal decomposition of plastics

### 5.1 Non-catalytic thermal decomposition of plastics

Pyrolysis is the thermal decomposition of organic compounds typically in an oxygen-deficient atmosphere. The decomposed products are then condensed and collected as oils, waxes, gases, and char, with distributions dependent on feedstock, reaction conditions, and reactor type. Temperatures in the range of 350–700 °C are typical for plastics pyrolysis,<sup>195</sup> with the general trend of higher yields of gas at higher temperatures.<sup>196</sup> Pyrolysis is generally classified according to heating rate (slow, fast, or ultra) and environment (catalytic pyrolysis, steam pyrolysis, vacuum pyrolysis, microwave pyrolysis, plasma pyrolysis, oxidative pyrolysis, *etc.*).

Pyrolysis is the most researched chemical recycling method for plastics.<sup>195</sup> The main advantage of plastic pyrolysis is the ability to convert plastic into lower molecular weight products to be used as fuels or feedstock for new chemicals or plastics.<sup>197</sup> Pyrolysis also produces less emission than plastics incineration.<sup>198</sup> Unlike mechanical recycling, pyrolysis can handle highly heterogeneous feedstocks with a higher degree of contamination.<sup>197</sup>

#### 5.1.1 Fundamental chemical processes during thermal pyrolysis of plastics

**5.1.1.1 Polyolefins.** PE follows a free radical thermal decomposition that takes place through sequential random bond-scissions.<sup>199–209</sup> The degradation begins in weak links (mainly peroxide groups formed during preparation and storage of PE) and proceeds in the pristine segments of the plastic.<sup>210</sup> Peterson *et al.*<sup>211</sup> employed thermogravimetric analysis to demonstrate that the activation energy depends on the extent of the decomposition reaction and assumes values between 150 kJ mol<sup>−1</sup> and 240 kJ mol<sup>−1</sup>. The latter number corresponds to the random scission process for pristine PE.<sup>212</sup> Huber and coworkers reported a similar activation energy (234.8 kJ mol<sup>−1</sup>), and argued that only models that include two random scission steps are capable of capturing the details of weight loss curves as obtained from thermogravimetric analysis.<sup>200</sup> The complexity of the free radical thermal decomposition of PE is substantial, and this is reflected in the large variety of pyrolysis products. The main products are alkenes, alkanes and alkadienes, while Diels–Alder reactions may also lead to the formation of small amounts of cycloalkenes.<sup>200</sup>

The initiation of PE pyrolysis involves a homolytic C–C cleavage reaction that happens at a random position along the PE chain, and gives two macroradicals (1) – (Scheme 1).<sup>213</sup> Each of these radicals may undergo a  $\beta$ -scission to produce ethylene monomer and another primary radical.<sup>214</sup> However, this unzipping process is not kinetically favorable at the early stage of PE decomposition (*ca.* 400 °C), and as a result no or little ethylene is produced in experiments (<1%).<sup>215,216</sup> In contrast, radical (1)

prefers to undergo a backbiting (often 1,5-backbiting through a six membered transition state) reaction, thereby generating a secondary internal radical (2) (Scheme 1).<sup>211,216</sup> Subsequently, a  $\beta$ -scission at (I) gives rise to an  $\alpha$ -olefin (3), whilst if the same process occurs at (II), a terminally unsaturated polymer residue (5) is produced, as well as a radical that transforms into an alkane (6) after abstracting a hydrogen atom. The formation of alkadienes (8) takes place either *via* a hydrogen abstraction reaction from (5) (Scheme 1) or *via* chain scission followed by a backbiting reaction. These processes give rise to (7) that, after a  $\beta$ -scission, is converted into an  $\alpha,\omega$ -alkadiene (8) (Scheme 1) and a new primary radical (1), which likely undergoes the processes of Scheme 1 anew.

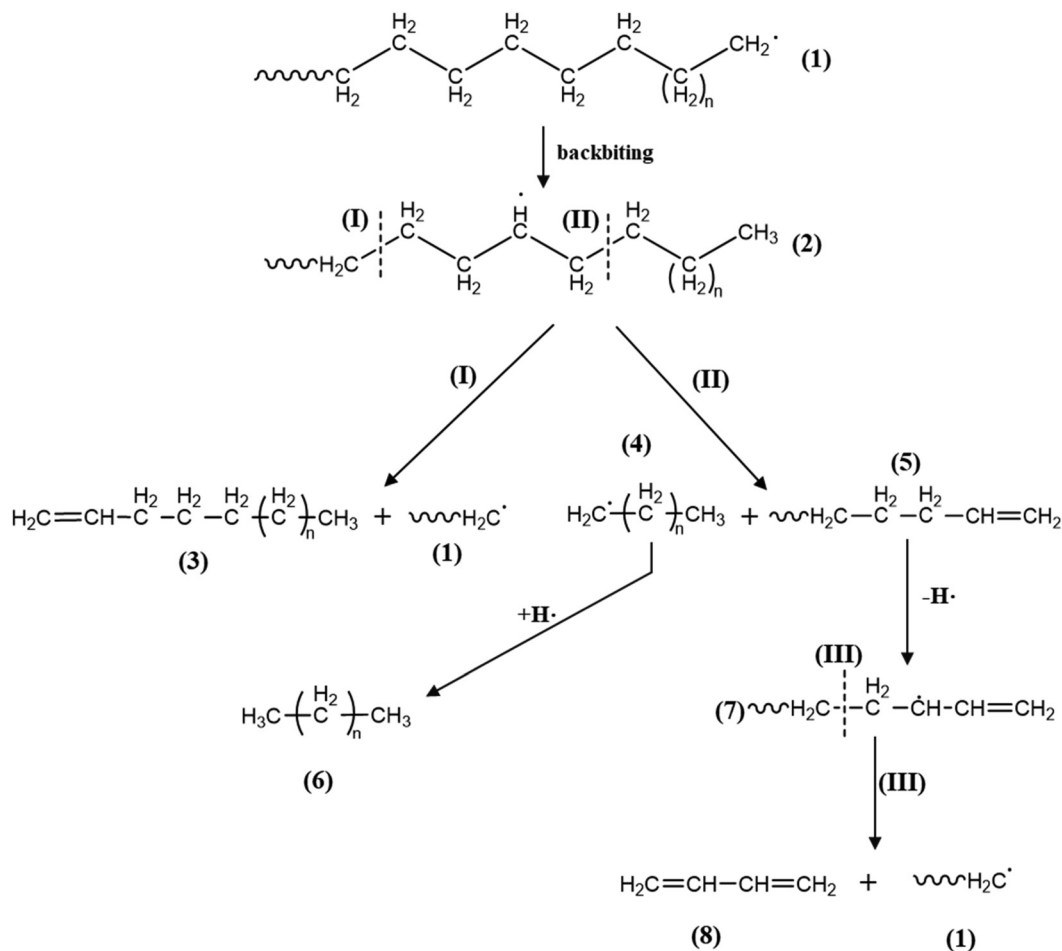
Similar to PE, the thermal decomposition of PP (9), Scheme 2, proceeds *via* random scissions along the backbone of the polymer with an activation energy of about 250.0 kJ mol<sup>−1</sup>.<sup>212</sup> Each random scission produces a primary (10) and a secondary (11) radical (Scheme 2), which, in turn, are converted to alkanes,<sup>214</sup> alkenes,<sup>217</sup> and alkadienes.<sup>218</sup> The major decomposition products are alkenes and alkadienes, and their formation takes place in a manner similar to what we described in Scheme 1.

The highest products from PP pyrolysis (*i.e.*, 2-methyl-1-pentene, 2,4-dimethyl-1-heptene) are produced *via* the decomposition of the secondary radical (11), while only minor quantities of products are derived from the primary radical (10).<sup>211</sup> On this basis, Scheme 2 focuses on the formation of alkenes and alkadienes *via* (11), which after a backbiting reaction and a  $\beta$ -scission at (IV) forms an alkene product (13) and another secondary radical (11). The new secondary radical is decomposed following the same sequence of steps. Alternatively, the  $\beta$ -scission may occur at (V), which results in a terminally unsaturated polymer (14). The latter species may undergo an atomic hydrogen abstraction reaction followed by a  $\beta$ -scission at (VI), thereby forming another secondary radical (11) and a series of alkadiene products (17).

**5.1.1.2 Polyvinyl chloride.** The thermal decomposition of PVC (18), Scheme 3, follows a completely different mechanism compared to polyolefins. According to thermogravimetric analysis studies, PVC (18) starts decomposing at much lower temperatures (<250 °C) than other common polymers, and its decomposition involves two distinct stages.<sup>219</sup>

The dominant reaction in the first stage (250 °C–350 °C) is the dehydrochlorination of the backbone that leads to a 60% weight loss.<sup>220</sup> The activation energy for this process has been determined in several studies, and values in the range of 112.0 kJ mol<sup>−1</sup>–150.0 kJ mol<sup>−1</sup> have been reported.<sup>221,222</sup> It has been conjectured that the initiation occurs in thermally labile defects like butyl branches associated with tertiary chloride.<sup>223,224</sup> Once the reaction is initiated, its propagation proceeds *via* a quasi-ionic mechanism whereby HCl is removed in a concerted manner *via* a four-center transition state (19).<sup>225</sup> Subsequently, the propagation reaction is relatively fast owing to the continuous formation of internal allylic chloride structures [see (20) in Scheme 3], which are more thermally unstable and susceptible to C–Cl heterolysis *via* HCl





**Scheme 1** Fundamental reactions for the thermal decomposition of PE leading to alkanes (6), alkenes (5) and alkydienes (8). Arabic numerals indicate chemical species that form during the pyrolysis of PE, while Roman numerals indicate the occurrence and position of the scission of chemical bond.

catalysis [*i.e.*, autocatalysis – transition state (21) in Scheme 3] than the pristine PVC polymer segments.<sup>226,227</sup> Remarkably, first-principles calculations by Yanborisov and Borisevich showed that the HCl-catalyzed dehydrochlorination of small chlorinated molecules (*e.g.*, 2-chlorobutane) can be 60.0 kJ mol<sup>-1</sup> more facile than the uncatalyzed process.<sup>228</sup>

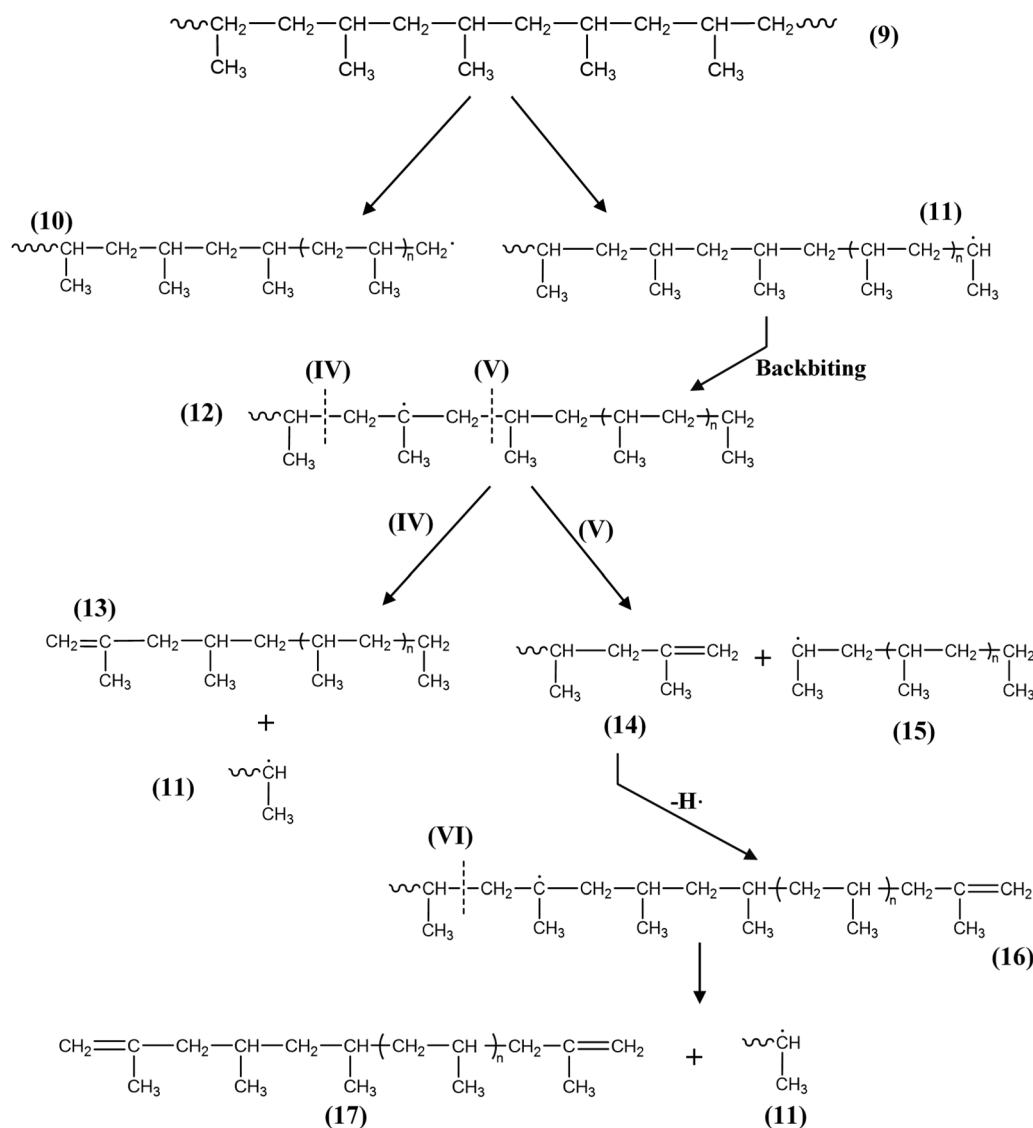
The main dehydrochlorination products are HCl gas and  $\pi$ -conjugated polyene sequences (22). The latter products are highly unstable under pyrolytic conditions and therefore undergo intramolecular and intermolecular reactions as soon as they form.<sup>229</sup> The intermolecular reactions require the interaction between two polyene chains (22),<sup>230</sup> and give rise to crosslinked polyene chains (23),<sup>229</sup> which are the precursor of char (24).<sup>231</sup> Char is extensively formed in the second stage of the thermal pyrolysis.<sup>231</sup> Alternatively, a polyene chain may undergo an intramolecular electrocyclic reaction, thereby giving rise to  $\pi$ -conjugated 1,3-cyclohexadiene rings (25). The latter are converted to benzene (26), and subsequently polyaromatics (27), after two consecutive homolytic C–C cleavages that occur at temperatures beyond 350 °C having activation energies larger than 220.0 kJ mol<sup>-1</sup>.<sup>232</sup> C–C bond breaking also

gives rise to small amounts of non-condensable gases (*e.g.*, CH<sub>4</sub> and H<sub>2</sub>).<sup>230</sup> Importantly, we note that the formation of aromatics can be promoted by applying a high-temperature pyrolysis step in the presence of a solid catalyst (*e.g.*, ZSM-5 zeolite).<sup>233</sup>

**5.1.1.3 Polystyrene.** The thermal degradation of PS (28) follows a radical chain mechanism (Scheme 4), with styrene (35) being the dominant product.<sup>234</sup> By means of thermolysis experiments, Wall *et al.*<sup>235</sup> demonstrated that the thermal stability of PS (28) depends on the polymerization method (*i.e.*, anionic or radical polymerization) used in its synthesis. Preparation through a radical polymerization gives rise to polymer chains with randomly distributed “weak links”, which perhaps are peroxidic in nature and are the sites where the thermal decomposition of PS starts.<sup>236</sup> Yet, anionic polymerization yields PS of high thermal stability;<sup>234</sup> the general thermal decomposition mechanism for this case is described in Scheme 4 and the following text.

The experimentally measured activation energy for the thermal degradation of PS is 200.0 kJ mol<sup>-1</sup> and remains constant regardless of the extent of the reaction.<sup>211</sup> This is indica-





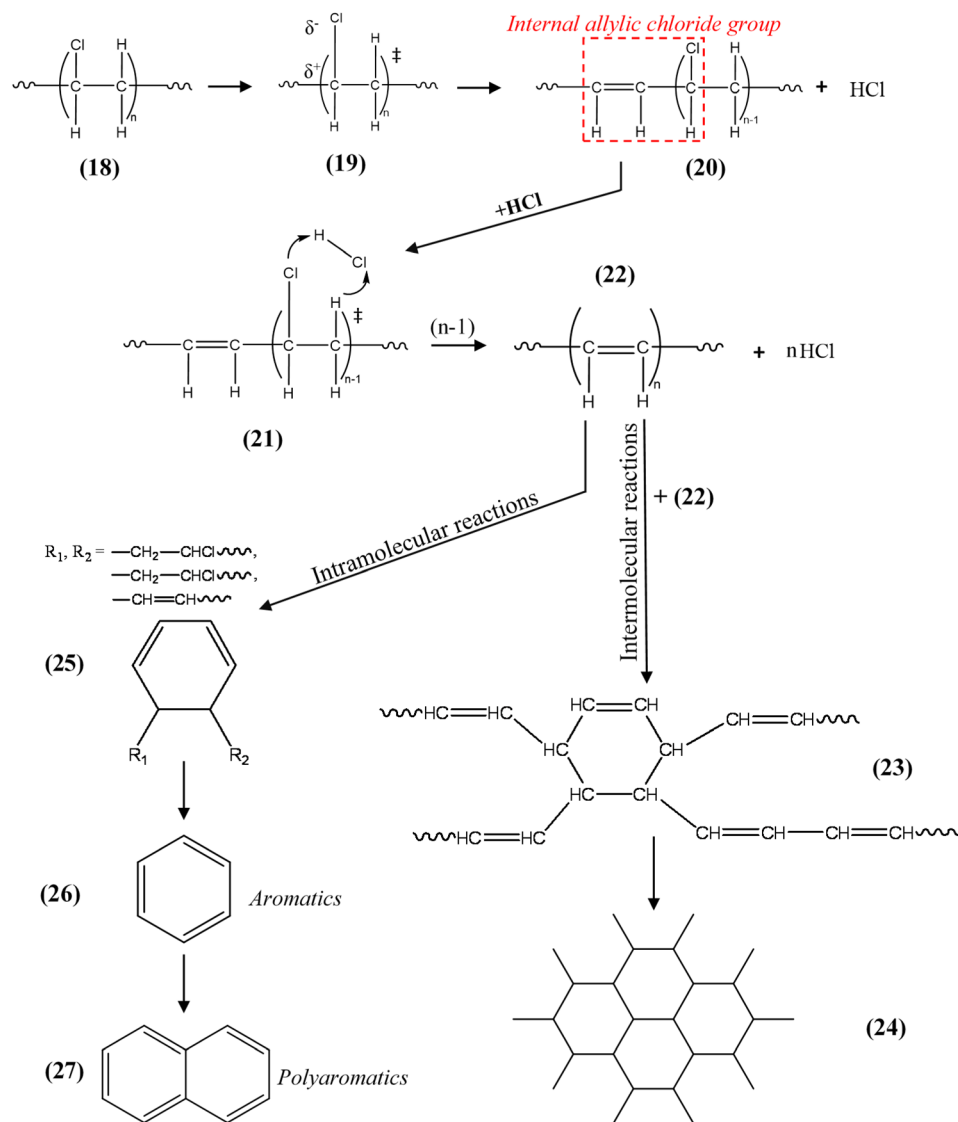
**Scheme 2** Fundamental reactions for the thermal decomposition of PP leading to alkenes and alkadienes. Arabic numerals indicate chemical species that form during the pyrolysis of PE, while Roman numerals indicate the occurrence and position of the scission of a chemical bond.

tive of a single rate-determine step during the reaction: the  $\beta$ -scission that forms styrene (35) (see Scheme 4).<sup>211</sup> According to Guyot and coworkers,<sup>234,237</sup> a likely initiation pathway for “anionically” prepared PS is *via* an end chain scission reaction that forms a benzyl radical (30) and a primary radical (29). The two radicals go through a disproportionation reaction and give toluene (32) and a chain with a thermally unstable unsaturated end (31). In turn, (31) decomposes into  $\alpha$ -methylstyrene (33) and a secondary radical (34) that leads the degradation process thereafter. DFT work by Huang *et al.* revealed that the latter reaction is exothermic by 80.8 kJ mol<sup>-1</sup> and its activation energy is 288.2 kJ mol<sup>-1</sup>.<sup>238</sup>

The propagation occurs by a  $\beta$ -scission process at (IX), thereby generating styrene (35) and another secondary radical (34). According to DFT calculations on a PS trimer, this reaction has an activation energy of *ca.* 117.0 kJ mol<sup>-1</sup>, but it is

strongly endothermic (+105.4 kJ mol<sup>-1</sup>) and therefore not favorable at temperatures below 250 °C.<sup>238</sup> Interestingly, the computed activation energy for the unbuttoning reaction (*i.e.*, 117.0 kJ mol<sup>-1</sup>) is in stark contrast to the experimental value (200.0 kJ mol<sup>-1</sup>) and this can, to some degree, be justified by the considerably smaller size of the simulated PS trimer as compared to actual PS chains. (34) can either undergo further unbuttoning to give extra monomer (35) or a backbiting reaction followed by another  $\beta$ -scission reaction at (X) and give a dimer (37) along with another secondary radical (34). Based on DFT, such backbiting and  $\beta$ -scission reactions require kinetic barriers of 174.0 kJ mol<sup>-1</sup> and 134.5 kJ mol<sup>-1</sup>, respectively, and the whole process that forms (34) and (37) is endothermic by 94 kJ mol<sup>-1</sup>.<sup>238</sup> We note that the formation of trimer or tetramer species takes place in an analogous manner to that for dimer production (37) (Scheme 4) with the only difference that





**Scheme 3** Fundamental reactions for the thermal decomposition of PVC leading to different products. The symbol  $\ddagger$  indicates a transition state. Arabic numerals indicate chemical species and intermediates that form during the thermal degradation of PVC.

different tertiary hydrogen atoms are involved in the backbiting reaction.

**5.1.1.4 Poly(ethylene terephthalate).** PET (38) is a thermally stable polymer thanks to the combination of short aliphatic chains and aromatic rings. Its thermal decomposition follows a molecular mechanism and the initiation reaction involves a scission at the ester linkage (Scheme 5).<sup>239–241</sup> This reaction takes place through a six-membered transition state (39), and recent DFT studies predict activation and reaction energies of 184.0 and +48.0 kJ mol<sup>−1</sup>, respectively.<sup>242</sup>

The initiation reaction leads to the formation of an oligomer with an olefin end group (40) and another oligomer with a carboxylic end group (41). These two species decompose further to produce a wide spectrum of products with acetaldehyde (44) and CO<sub>2</sub> (43) being the most abundant at temperatures around 300 °C.<sup>240</sup> The former can be produced directly from (40) and (41) or *via* the degradation of EG end

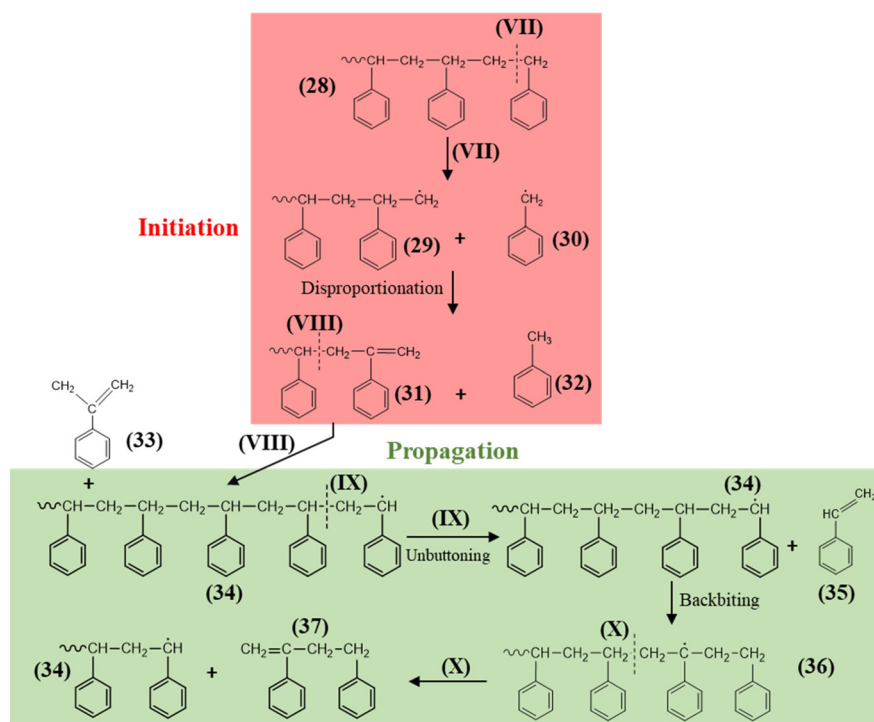
groups as proposed by Holland and Hay,<sup>243</sup> while CO<sub>2</sub> is released by decarboxylation of (41). More than 45 wt% of the PET is degraded into CO<sub>2</sub> with trace CO.<sup>244</sup>

**5.1.2 Variables affecting product distribution.** Pyrolysis begins with free-radical initiation in the plastic melt, or condensed phase. Volatile products are released from the melt as depolymerization progresses, leaving behind ash, fillers and (sometimes) char. Secondary reactions occur in the vapor phase that cause further cracking. Gas, liquid, and wax are produced, with distributions dependent on reaction conditions. These products are usually categorized according to their carbon length and/or phase:<sup>245</sup>

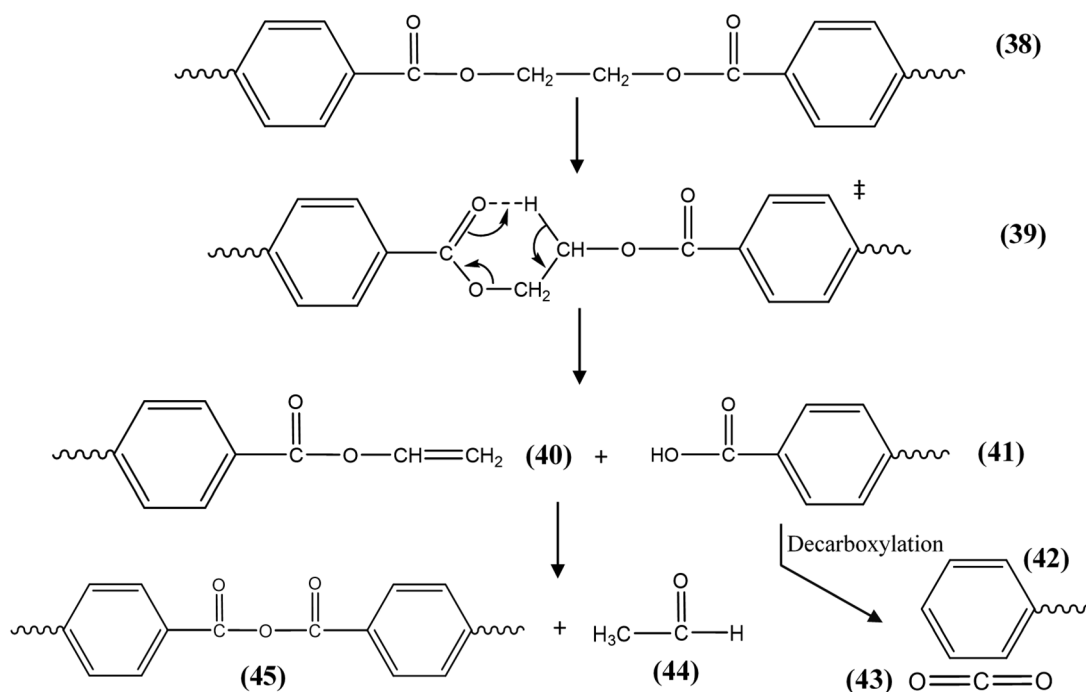
- C1–5 = gas
- C6–20 = naphtha or oil, liquid at ambient conditions
- C21+ = wax, solid or highly viscous liquid at ambient conditions

Al-Salem *et al.*<sup>246</sup> published an in-depth review addressing plastic pyrolysis variables and their influences on reaction and



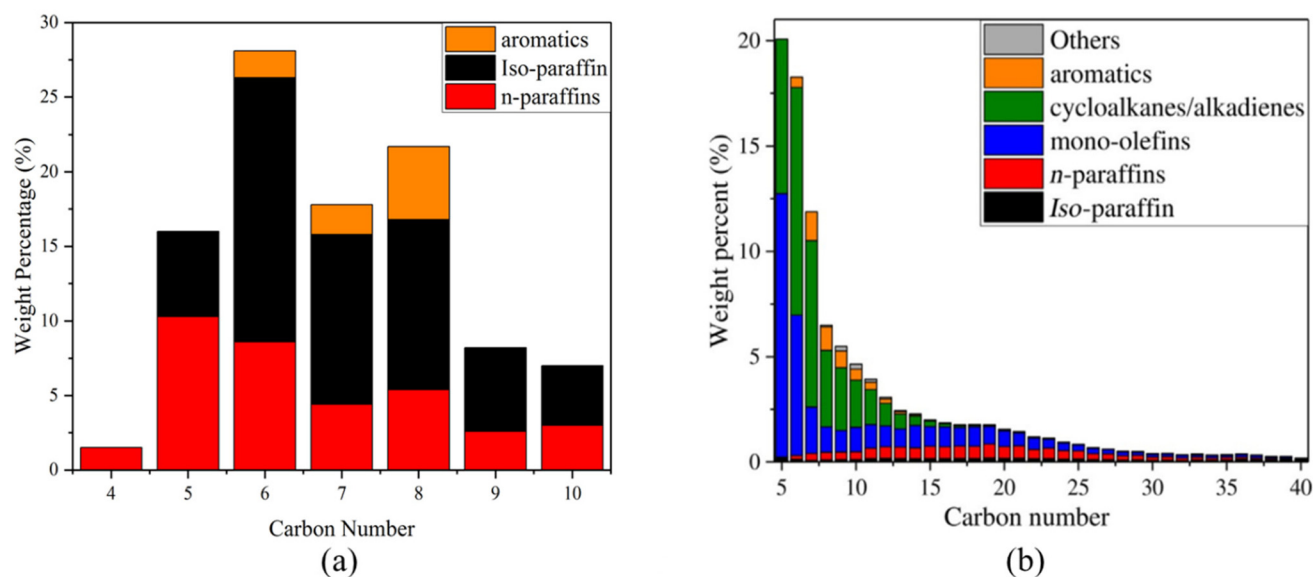


**Scheme 4** Fundamental reactions for the thermal decomposition of PS leading to different products. Arabic numerals indicate chemical species, while Roman numerals indicate the occurrence and position of the scission of a chemical bond.



**Scheme 5** Fundamental reactions for the thermal decomposition of PET. The symbol ‡ indicates a transition state. Arabic numerals indicate chemical species and intermediates formed during the pyrolysis of PET.





**Fig. 17** (a) A typical naphtha composition (graph made based on the data obtained from ref. 251, (b) a typical plastic pyrolysis oil composition obtained from PE pyrolysis. Reproduced from ref. 252 with permission from Wiley-VCH, copyright 2020.

product distribution and asserted that the main decomposition behavior of the plastic is controlled by temperature. In PE pyrolysis, early studies showed that only liquid and gas – no wax – are produced above 600 °C.<sup>247</sup> Increasing temperature leads to increased aromatic production, as gas is converted to aromatics through a Diels–Alder reaction and unimolecular cyclization reactions,<sup>248,249</sup> although a study by Kulas *et al.*<sup>250</sup> showed that the reaction pathway from gas to aromatics has low temperature dependence.

The composition of naphtha is vastly different than the composition of plastic oil (Fig. 17). The main products of naphtha are paraffin with around 10% aromatics, while the main products of plastic pyrolysis oil are olefins and cycloalkanes/alkadienes with a much wider range of carbon numbers.

Increasing vapor residence time increases the yields of oil and non-condensable gases.<sup>248,253</sup> As primary products are exposed to heat for longer periods of time, secondary reactions and further cracking to smaller molecules are encouraged.<sup>254</sup> Thus, the product distribution shifts from high molecular weight products to lower molecular weight hydrocarbons (MWHCs).<sup>255–257</sup> For polyolefin feedstocks, longer reaction times decreased product olefin concentrations and increased polyaromatic hydrocarbon concentrations.<sup>258</sup>

Polyolefins have received the most attention in the field of plastics pyrolysis. PE and PP decompose into a distribution of hydrocarbons, with decreasing product molecular weights as reaction temperature and time increase. Waxes and heavy oil olefins dominate product distributions at low temperatures, while gases and light oils are the main products at high temperatures.<sup>250</sup> Polyolefins such as HDPE, LDPE, and PP decompose into a distribution of hydrocarbon products that have high concentrations of olefins and dienes (>70%).<sup>259,260</sup> Mixed plastic feedstock with high PE content will lead to higher

paraffin concentrations.<sup>261</sup> Pure PP yields higher amounts of olefins, with lesser amounts of paraffins, naphthenes, and aromatics.<sup>262,263</sup> Due to the tertiary carbon present on the backbone of PP, multiple types of secondary radicals are formed, shifting liquid product composition towards branched olefins.<sup>261,264</sup>

PS decomposes primarily into the monomer styrene and its oligomers<sup>265,266</sup> with the polymer undergoing chain scission followed by random scission.<sup>266</sup> PS pyrolysis produces liquid products at yields greater than 90 wt% in both batch<sup>262,267,268</sup> and continuous<sup>247,269,270</sup> reactors. Liu *et al.*<sup>269</sup> pyrolyzed PS in a fluidized bed reactor at 600 °C and achieved 98.7 wt% oil, of which 78.7 wt% was styrene. Secondary reactions and increased reaction temperature decrease the concentration of styrene in the liquid product and increases the formation of coke and gas.<sup>269</sup> PS accelerates the pyrolysis of polyolefins due to higher concentrations of free radicals.<sup>271</sup> Green Mantra Technologies is commercializing PS pyrolysis to recover styrene.<sup>272</sup> A thorough review on the pyrolysis of PS can be found elsewhere.<sup>266</sup>

The pyrolysis of PET yields oxygenated compounds from the presence of oxygen in the backbone of the polymer chain. Fast pyrolysis of PET produces mostly mixtures of aromatics and the organic acids benzoic and phthalic acid, char, and gas.<sup>273</sup> Formation of TPA is particularly problematic due to its high boiling/sublimation temperatures, which clogs reactor and condenser internals.<sup>273,274</sup> The presence of phthalic acids in product oils increases viscosity and acidity and lowers calorific value, resulting in low-quality oils.<sup>273,275,276</sup> Pyrolysis temperature has little effect on calorific values of PET products.<sup>260</sup> PET in mixed plastics increases the CO and CO<sub>2</sub> concentrations in product gases from pyrolysis reactions.<sup>196,277</sup> While some investigators have concluded that PET is not suit-



able for plastic pyrolysis,<sup>255,278</sup> others advocate for it based on the valorization of product char to activated carbon and product oil to fuel.<sup>273</sup> US-based pyrolysis company Agilyx has undertaken pyrolysis of PET with some success,<sup>279</sup> but PET is rarely used as a feedstock in commercial pyrolysis processes. Other possible chemical recycling processes of PET are detailed elsewhere and in section 9.1.<sup>280–283</sup>

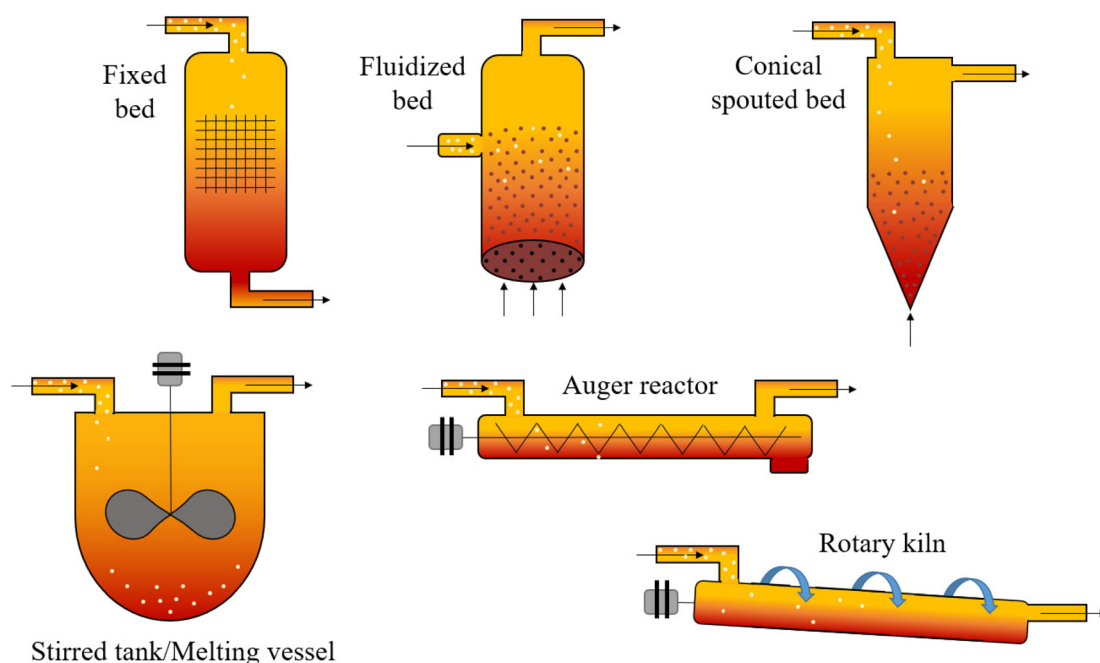
Many commercial pyrolysis processes have low tolerance to PVC, which produces significant concentrations of organic chlorine, HCl and a solid residue.<sup>275,277</sup> The HCl causes corrosion issues with downstream processing of the products. Thermal decomposition of PVC is initiated by a dechlorination reaction, resulting in the formation of hydrogen chloride and benzene.<sup>284,285</sup> The polymer chain then undergoes cyclization, yielding aromatic and alkylaromatic compounds that are often chlorinated.<sup>220</sup> Pyrolysis oil containing chlorinated compounds has limited use.<sup>286</sup> Most previously reported pyrolysis processes had a specification that the PVC content of the plastic feeds be less than 2 wt%.<sup>287</sup>

Plastics can also be co-processed with waste tires,<sup>288,289</sup> wastepaper,<sup>290</sup> and agricultural residues,<sup>291,292</sup> which has been shown to enhance products for fuels and value-added chemicals.<sup>293</sup> The majority of waste plastics will contain high levels of contaminants. Additives, heavy metals, and pigments are often added to plastic to enhance its physical appearance or performance. Specific problematic elements include nitrogen, oxygen, sulfur, chlorine, iron, sodium, and calcium.<sup>294</sup> In low-temperature pyrolysis, sulfur presents in the pyrolytic oil, which reduces its ability to be used as ultra-low sulfur diesel.<sup>294</sup> Produced liquid may also contain amines or alcohols

if the feedstock contains N, O, or S.<sup>295</sup> Siloxanes can be present in the pyrolysis oil as well.<sup>296</sup> Dechlorination is possible through the use of sorbents,<sup>286,297–301</sup> absorption and neutralization,<sup>302</sup> subcritical water treatment,<sup>303</sup> catalysts,<sup>304</sup> or stepwise pyrolysis,<sup>286</sup> but the latter was shown to modify the composition of liquid products.<sup>286</sup> Untreated plastic waste pyrolysis oils with high levels of contaminants are not feasible feedstocks for steam cracking unless sufficiently diluted.<sup>305</sup> Contamination may lead to catalyst deactivation if catalytic upgrading of products is desired. For example, a municipal plastic waste pyrolysis plant in Idaho, U.S.A. produced an oil only suitable for low-value applications due to severe contamination.<sup>306</sup>

Thermal oxo-degradation (TOD) involves adding small amounts of oxygen to the pyrolysis process to increase chain cleavage.<sup>307</sup> Plastics subjected to TOD are decomposed to oxygenated products and hydrocarbons, with exothermic partial oxidation reactions releasing energy to provide heat back to the process. This process mirrors that of autothermal pyrolysis developed for the process intensification of biomass,<sup>308,309</sup> with the possibility to achieve autothermal operation for plastics.<sup>310</sup>

**5.1.3 Reactor configurations.** Various reactor configurations have been used for plastic pyrolysis, including fixed beds, fluidized beds, rotary kilns, auger reactors, conical spouted bed reactors, and melting vessels (Fig. 18). Detailed information on reactor types for plastic pyrolysis can be found in recent review papers.<sup>264,275,311–313,314</sup> Fluidized bed reactors have excellent heat and mass transfer characteristics for pyrolysis of plastics and are the reactors that are most typically used



**Fig. 18** Schematics of various plastic pyrolysis reactors including fixed bed, fluidized bed, conical spouted bed, stirred tank, auger, and rotary kiln reactors.



for continuous large-scale processing of solids. In a gas–solid system, fluidized bed reactors have vigorous solid contact with different gas flow rates. An increasing of flow rate in a bubbling fluidized bed (BFB) leads to larger instabilities and bubbling channels of gas with a more vigorous solid movement.<sup>315</sup> In turbulent fluidized bed, with a sufficiently high gas flow rate, the terminal velocity of the solids is exceeded and solids undergo a turbulent motion so that the upper surfaces of the solid disappear.<sup>315</sup> Fluidized bed reactors were used extensively in the groundbreaking work in plastics pyrolysis by Walter Kaminsky at the University of Hamburg.<sup>288,289,316–318</sup> Both BFBs and circulating fluidized beds (CFB) have been commonly employed in both laboratory studies<sup>254,256,257,317,319–322</sup> and industrial deployment.<sup>323</sup> Fluidized beds usually employ smaller feedstock particles than other reactors, which, along with their inherently high convection coefficients, enhances heat transfer rates. Feedstock injected into a fluidized bed is rapidly dispersed and efficiently contacted with gas, resulting in high mass transfer rates.<sup>311,313</sup> The combination of high heat and mass transfer rates are responsible for significant yields of light hydrocarbons and non-condensable gas from the pyrolysis of plastics in fluidized beds.<sup>305,324</sup> Disadvantages include comminution of plastics to achieve small feedstock particles, and complicated reactor setups.<sup>275</sup> Additionally, the high gas velocities required for fluidization can cause entrainment of char particles, requiring particulate separation downstream of the reactor.<sup>196</sup> Fluidized beds may also see agglomeration of melted plastic that can lead to bed defluidization.<sup>325</sup>

Conical spouted bed reactors are a type of fluidized bed with a cylindrical geometry and a conical base. Cyclic and vigorous movements by sand particles in the bed prevent agglomeration upon melting and subsequent bed defluidization.<sup>259,326</sup> Conical spouted beds have been employed in laboratory-scale pyrolysis studies of PS<sup>327</sup> and polyolefins,<sup>326,328,329</sup> which report high yields of wax. Orozco *et al.*<sup>259</sup> identified stable operating conditions for conical spouted bed reactors for individual plastic feedstocks.

Fixed bed reactors are inexpensive, simple to operate, and have low maintenance requirements. However, these types of reactors would be difficult to operate for solid feedstocks on the industrial scale due to large amounts of solid coke/char formation. Vertical fixed beds use gravity to force products through the reactor. Tubular reactors are very similar to fixed beds, but are usually horizontal with co-current flow of feedstock and carrier gas.<sup>330,331</sup> Due to the relatively long times required to devolatilize plastic, the entrance to the tubular reactor can become quickly blocked with melted plastic, limiting feed rates. While commonly used in laboratory settings,<sup>332–335</sup> fixed beds are not suitable for industrial applications.<sup>275,313</sup> BASF reported the use of a tubular pyrolysis reactor to crack plastic wastes at scale to produce oil and gas, but the feed rates achieved were not documented.<sup>312</sup>

Auger reactors consist of a rotating screw inside a tubular reactor. The helical screw is used to convey feedstock while also discharging residual solid products. The auger reactor is a

simple system that can be easily scaled and is feedstock flexible. Providing enthalpy for pyrolysis through the reactor wall is increasingly difficult as the reactor is made larger. This limitation can be substantially overcome by conveying heated metal shot or granular material into the reactor.<sup>336</sup> As outlined by Campuzano *et al.*,<sup>336</sup> potential disadvantages of auger reactors include the risk of blockage, mechanical wear, and higher vapor residence times, which can lead to sometimes undesirable secondary reactions. Auger reactors have been used to pyrolyze plastics to high yields of liquids for use as fuel<sup>337</sup> or wax,<sup>338</sup> or as the first stage in a multi-staged pyrolysis system to activate molecules for further cracking.<sup>321</sup> Brightmark, a US company, is using an auger reactor to process plastic pyrolysis, and the reactor has five heating zones in series to improve the heat transfer. The number of zones of a reactor can be varied depending on different feedstocks.<sup>339</sup>

The rotary kiln is one of the most common reactors used in industrial pyrolysis processes. The kiln is a slightly inclined cylindrical vessel rotated slowly on its axis to allow feedstock and residual solids to move through the kiln. Because they can handle various feedstock sizes and shapes, rotary kilns have been used to process scrap tires<sup>340,341</sup> and municipal wastes.<sup>342,343</sup> Heat is supplied to the kiln by internally or externally heated walls,<sup>311</sup> although heating rates are so slow as to qualify as slow pyrolysis.<sup>314</sup> Residence times of solids and vapors in rotary kilns are highly controllable, depending upon rotational speed and carrier gas flow rates.<sup>344</sup> Rotary kilns are considered robust and affordable however they are limited to certain scales due to heat transfer.<sup>311</sup>

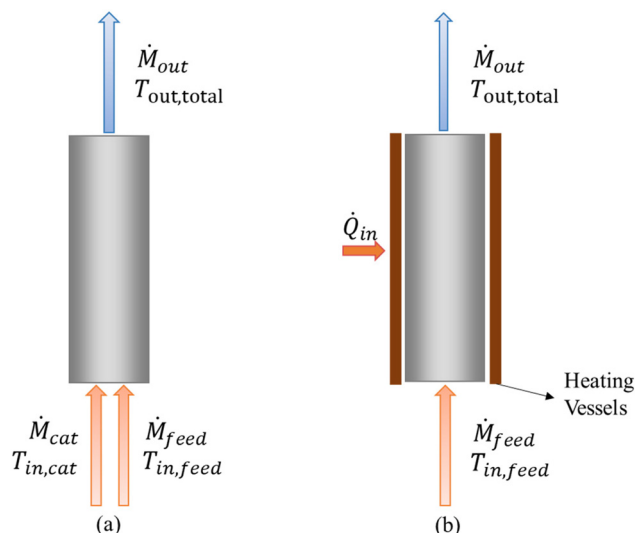
Stirred tank reactors, also known as melting vessels, have been used for pyrolysis of plastics in batch,<sup>267,345,346</sup> semi-batch,<sup>258</sup> and continuous operation. Commercial examples include the Smuda process,<sup>347</sup> the Hitachi Zosen process,<sup>275</sup> and the Plastic Energy process.<sup>348</sup> Stirred tank reactors are characterized by a simply-designed vessel heated through the reactor wall and a stirrer to promote uniform heat distribution and homogenous reactants. Heat gradients, large infrastructure requirements, and frequent maintenance limit the use of stirred tank reactors.<sup>312</sup> Stirred tank reactors are primarily used for batch reactions, which is not economical on a large continuous scale process.

Pyrolysis reactors can be heated by a heat carrier (Fig. 19a) or with an external heat exchanger (Fig. 19b). The heat balance when a heat carrier is used is shown in eqn (1), where  $\dot{M}_{\text{cat}}$  is the mass flow rate of catalyst (or heat carrier),  $C_p$  is the heat capacity of the gas,  $T$  is the temperature,  $\dot{M}_{\text{feed}}$  is the mass flow rate of reactant, and  $\Delta H_{\text{rxn}}$  is the net energy of the heat of the pyrolysis reaction. When using a heat carrier, the reactor can be scaled to larger industrial sizes without limitations to the heat transfer area by use of an external fluid. In contrast if an external fluid is used for heating the energy balance is dependent on the heat transfer area as shown in eqn (2) and (3).

$$\dot{M}_{\text{cat}} C_p (T_{\text{out}} - T_{\text{in}}) = \dot{M}_{\text{feed}} (\Delta H_{\text{rxn}} + C_p (T_{\text{out}} - T_{\text{in}})) \quad (1)$$

$$\dot{Q}_{\text{in}} = UA\Delta T = \dot{M}_{\text{feed}} (\Delta H_{\text{rxn}} + C_p (T_{\text{out}} - T_{\text{in}})) \quad (2)$$





**Fig. 19** (a). Scheme of reactor with heat carrier (b) Scheme of reactor with external heating vessels.

$$A = 2\pi rL \quad (3)$$

PE pyrolysis requires around  $260 \text{ kJ kg}^{-1}$  of heat.<sup>349</sup> In a larger reactor, the heat transfer efficiency decreases due to the larger reactor diameter. Brown *et al.*<sup>350</sup> reported that the maximum diameter of a biomass fast pyrolyzer is 9.4 mm, and an analogous calculation for a PE pyrolyzer obtained a maximum diameter of 6.4 cm. The reaction rate of PE used for the calculation is obtained from Zhao *et al.*<sup>252</sup> In addition, the overall heat transfer will be affected by the bulky nature of the fed plastic, and the real diameter of the plastic pyrolyzer may be smaller than 6.4 cm. Autothermal pyrolysis can help to reduce the amount of heat required for pyrolysis by adding a certain amount of oxygen to partially oxidize the hydrocarbon feed, which makes the rate of energy release from the oxidation reaction equal the rate of energy consumed by the plastic pyrolysis.<sup>350</sup> However, one main problem of the auto-

thermal process is that it causes hot or cold spots due to the heat absorbed or released from the autothermal pyrolysis. The key to eliminating the hot and cold spots is again improving heat transfer within the reactor.

**5.1.4 Economic analysis.** Hundreds of species of hydrocarbons may be present in the pyrolysis oil, including olefins, paraffins, aromatics, diolefins, iso-paraffins, and naphthenes. PE-derived oils have high concentrations of linear hydrocarbons, while PP-derived oils contain more branched components such as trimers, tetramers, and pentamers of propene.<sup>351</sup> Many petroleum companies like Shell, BP, TotalEnergies, SABIC, and ExxonMobil, are planning to upgrade pyrolysis oil through steam cracking.<sup>352–355</sup> Kusenberget *et al.*<sup>305</sup> has reported that the uncertainty and contaminants in the pyrolysis oil hampered industrialization.

Various studies have shown that the profitability of plastic pyrolysis refineries depends on several factors including feedstock cost, yield rate, product type, and facility scale. Feedstock composition, pyrolysis yield, and product selectivity are critical drivers for process efficiency. Feedstock cost, capital investment, and market prices play a significant role in the profitability of a plastic pyrolysis facility. Table 12 summarizes the key assumptions and findings from several studies on plastic pyrolysis.<sup>278,356–358</sup> Fivga & Dimitriou investigated the pyrolysis of plastic waste to produce wax/oil products that can be used as a heavy fuel oil substitute or as raw materials by the petrochemical industry. The study evaluated a base case scenario of a 0.7 kton per year pyrolysis pilot plant built by a recycling company in the United Kingdom. The base case analysis resulted in a capital cost of \$1.34 million. The product cost from the base case scenario was \$0.98 per kg of fuel produced, which was more than the market price of the heavy fuel oil product of ca.\$0.8 per kg. Increasing the pyrolysis scale from 70.1 kton per year to 701 kton per year decreased the product price from 29.4 cents to 3.39 cents per kg.<sup>356</sup> The pyrolysis plants can be designed as either closed-loop or open-loop.<sup>357</sup> Larrain *et al.* also emphasized that to make an open-loop and

**Table 12** Summary of waste plastic techno-economic analysis pyrolysis articles by feedstock, products, region, capacity, capital cost, and return on investment (ROI)

Technology	Feedstock	Major products	Region	Capacity (kton per year)	Capital Cost (\$ million)	NPV (\$)	Ref.
Pyrolysis	PS, PP, PE	Heavy oils petrochemical feedstock	United Kingdom	0.7–701	1.36–77.2	–0.44 per kg–0.71 per kg	356
Pyrolysis + upgrading	PS, PP, PE, PET	Hydrocarbon fuel	Korea	260	118	0.062 per gal	278
Pyrolysis	PE, PP, PET	Diesel power char	Australia	14.6	3.76	2.03 million	360
Pyrolysis & heat integration	HDPE	Ethylene propylene	United States	193	118.5–120.5	367.8 million–383million	359
Fast pyrolysis (open-loop & closed-loop)	Mixed polyolefins mainly LDPE and residual PP	Naphtha	Belgium	120	Not disclosed	open loop: 32.5 per ton closed loop: 2.72 per ton	357
Pyrolysis	Plastic waste (PP, PE, PS)	Light oil heavy oil	Malaysia	120	58.6	20.9 million	358



closed-loop pyrolysis of mixed olefins attractive to investors, closed-loop and open-loop plastic pyrolysis plants should be scaled up to at least 70 kton per year and 115 kton per year, respectively.<sup>357</sup>

Larrain *et al.* investigated the economic feasibility of open-loop and closed-loop pyrolysis of mixed polyolefins (mainly LDPE and residual PP) in a 120 kton per year facility in Belgium. In the open-loop system, the process only produces naphtha, while the closed-loop system produces naphtha and wax. The study recorded a base case net present value (NPV) per tonne of plastic waste processed of \$32.5 per ton and \$2.72 per ton for the open-loop and closed-loop systems, respectively. The market value of the products resulted in a significant difference of \$24.75 per ton, thereby emphasizing that the type of products plays a vital role in the facility's profitability. The study went further to consider the uncertainties in oil prices that significantly affect the prices of wax and naphtha in the market and concluded that the open-loop system has about 98% probability of achieving positive returns compared to 58% recorded for the closed-loop system.<sup>357</sup>

Gracida-Alvarez *et al.* conducted the economic analysis of a multi-product 193 kton per year pyrolysis-based refinery for the conversion of HDPE to value-added chemicals (ethylene, propylene, and aromatic mixtures) and hydrocarbon mixtures *via* pyrolysis. In this study, the authors estimated the capital cost, operating cost, and NPVs for a base case where HDPE is converted to the products and a heat integrated case. The authors reported a capital cost of \$118.5 million for the base case and \$120.5 million for the heat integrated case. The NPV can range from \$320 million to \$450 million depending on the selling price of low MWHCs and the internal rate of return (IRR).<sup>359</sup> The study showed that plastic pyrolysis targeting multiple products could be very profitable.

**5.1.5 Commercial activities.** Table 13 lists the publicly made announcements about major plastic pyrolysis technologies that are in operation, were previously planned or are currently planned. Western Europe began to study plastic pyrolysis in the late 1970s.<sup>287</sup> The first of these plants was designed by BP in 1994. Using mixed waste packaging plastics, research on a laboratory scale was followed by demonstration on a continuous pilot plant scale (nominal 50 kg h<sup>-1</sup>) at BP's Grangemouth site. BP Chemicals, VALPAK, and Shanks & McEwan formed a collaborative initiative (POLSCO) in 1998 to study the viability of a 25 kton per year factory with a fluidized bed reactor, which would include logistical infrastructure for delivering mixed plastics from Scotland.<sup>361</sup> This plant was never built because BP claimed it would require a tipping fee of £250 per ton (\$225 per ton) to fulfill a £15–20 million (\$24.75–33 million) total investment cost of this plant.<sup>287</sup>

In Europe, there are 3 operating pyrolysis plants owned by Quantafuels and Plastic Energy. Quantafuel's first commercial production facility is in Skive, Denmark. The plant processes 20 kton per year. The liquid product is sent to BASF, who uses the liquid product to produce virgin plastic and other chemicals.<sup>362</sup> Plastic Energy currently has two plants in

Almeria (started in 2014) and Seville (started in 2017) in Spain. The plant in Seville has the ability to treat 5 kton per year.<sup>363</sup>

Several companies have announced plans in the past few years to build plastic pyrolysis plants and convert the plastic oils into aromatics/olefins by steam cracking. In Germany, SABIC and BP announced in 2021 plans to build a plastic recycling plant in Gelsenkirche.<sup>355</sup> BP will build plants to steam crack the plastic oil obtained from SABIC and forward the cracking materials to SABIC for making new plastics.<sup>355</sup> One goal of BP is to achieve 30% of propylene and ethylene produced from recycled material by 2030.<sup>364</sup> Shell plans to work with Pryme to build a plastic pyrolysis plant and produce circular chemicals in the Netherlands and Germany with the capacity of 60 kton per year in 2022.<sup>365</sup> Plastic Energy announced a collaboration with ExxonMobil in early 2021. Starting in 2023, ExxonMobil will use the plastic oil from Plastic Energy and upgrade the plastic to a naphtha-quality petrochemical feedstock.<sup>354</sup> The company has started to construct a recycling plant in France next to ExxonMobil's Notre Dame de Gravenchon petrochemical complex, which will have a capacity of 25 kton per year.<sup>366</sup> QuantaFuel plans to build a 100 kton per year plant in Sunderland UK and to work with VITOL and VITTO to build another 100 kton per year plant in Amsterdam.<sup>367,368</sup> Fuenix Ecology raised €4 million (\$4.53 million) to scale up its technology to recycle mixed plastic waste, and in a collaboration with Dow to build a plant to pyrolyze plastic in Weert, Netherlands in 2019.<sup>369,370</sup> The pyrolysis plastic oil will be sent to Dow Terneuzen, Netherlands, for steam cracking and producing virgin quality plastics.<sup>371</sup> The goal for both Dow and Fuenix is to generate 100 kton of the recycled plastics by 2025.<sup>372</sup>

In the US, Brightmark is planning to build one of the largest plastic pyrolysis plants in the world, with a scale of 100 kton per year, in Ashley, Indiana.<sup>373</sup> Freepoint Eco-Systems plan to invest \$60 million to construct a plastic pyrolysis plant in Obetz, Ohio, with a capacity of 90 kton per year. The company claims that the plant will be operating in 2023 and will be able to convert 300 tons of waste plastic into 1500 barrels of oil.<sup>374,375</sup> TotalEnergies is also working with the Freepoint Eco-Systems to build a 33 kton per year plant in Houston, Texas in mid-2024. The products will be sent to TotalEnergies' steam cracker to produce monomer and manufacture high-quality plastics.<sup>352,376</sup> Agilix and ExxonMobil created a joint venture together called Cyclyx International, which will be focused on creating novel ways to collect and pre-process massive amounts of plastic trash into feedstocks for higher-value products.<sup>374</sup>

There are also some plastic pyrolysis projects underway in Asia. Shell decided to start producing plastic oil with a capacity of 50 kton per year at Pulau Bukom, Singapore in 2023.<sup>377</sup> Plastic Energy collaborates with WWF-Indonesia and aims to help Indonesia to reduce 100 kton of plastic waste by 2025.<sup>378</sup> Insights provided by McKinsey showed that pyrolysis could be the most profitable process in the coming years.<sup>379</sup> Due to the large amounts of oil required to run the hydrocarbon





**Table 13** Commercial plastic pyrolysis plants that were previously planned, operational or shut down

Name	Plant location	Scale (kton per year)	Status	Reactor type	Feedstocks	Product	Collaborators
BP <sup>361</sup>	Grange-mouth (Polit plant)	25	1998–2000 (Design only)	Fluidized bed reactor	PP, PE, PET, PS, PVC	Hydrocarbon liquid	VALPAK, and Shanks & McEwan
BASF <sup>361</sup>	Ludwig-shafen (Polit plant)	15	1994–1996	Not reported	Not reported	Not reported	Duales System Deutschland
Agilyx <sup>376</sup>	Tigard (Polit plant)	3	Operational since 2018	Stirred tank reactor	PS	Styrene monomer	Toyo, Exxon Mobil, Braskem, AmSty, Lucite, and NextChem
Quantafuel <sup>367,339,368</sup>	Skive (Polit plant)	20	Operational since 2017	Fluidized bed reactor	HDPE, LDPE, PP, PS, and PET	Liquid oil, non-condensable gas, and carbon rich ash. The liquid oil will be used to produce virgin-quality plastic	BASF, VITOL, and VITTI
	Amsterdam	100	Under construction and plan to operate in 2023–2024				
	Sunderland	100	Under construction and plan to operate in 2024				
Pryme <sup>35,3,380</sup>	Rotterdam	40–60	Under construction and plan to operate in 2022	Fluidized bed reactor	PS, PE, and PP	Kerosine, naphtha, and wax followed with steam cracking to obtain petroleum products	Shell
Brightmark <sup>339,373,381</sup>	Asheley	100	Partially operational since 2021	Auger reactor	PET, HDPE, PVC, LDPE, PP, and PS	Ultra-low sulfur diesel, naphtha, and wax	BP, Chevron, clean fuel Partners, and Northeast Indiana Solid Waste Management District
Plastic energy <sup>354,366</sup>	Seville (Pilot plant)	5	Operational since 2017	Stirred tank reactor	LDPE, HDPE, PP, PS	Diesel and naphtha followed with steam cracking to obtain raw materials to make new plastic	SABIC, ExxonMobil, and freepoint Eco-Systems
	Le Havre	25	Design phase planned to start up in 2023				
	Almeria	Not reported	Operational since 2014				
Freepoint Eco-Systems <sup>374</sup>	Houston	33	Plan to operate in Mid-2024	Fluidized bed reactor	LDPE, HDPE, PP, PS	Synthetic oil	Plastic energy, and TotalEnergies
	Obetz	90	Plan to operate in 2023				
Shell <sup>377</sup>	Pulau Bukom	50	Under construction and plan to operate in 2022	Not reported	Not reported	Not reported	Pryme
ExxonMobil <sup>374</sup>	Baytown	30	Under construction and plan to operate in end-2022	Fluidized bed reactor	Not reported	Not reported	Cyclx, agilyx, and plastic energy

economy, the use of blends of plastic pyrolysis products and petroleum-derived feedstocks is expected to expand.<sup>305</sup>

## 5.2 Catalytic thermal decomposition of plastics

**5.2.1 Catalysts.** Numerous catalysts have been explored for catalytic pyrolysis with entire review papers written on this topic.<sup>20,382–384</sup> A large number of catalytic pyrolysis studies focus on the use of aluminosilicate materials such as amorphous  $\text{SiO}_2\text{-Al}_2\text{O}_3$ , mesoporous  $\text{SiO}_2\text{-Al}_2\text{O}_3$ , and zeolites. Aluminosilicates offer the unique advantage of having tunable acidity which can be used to direct the product selectivity of catalytic pyrolysis transformations.<sup>10</sup> By increasing the alumina content – and thus acidity – within these materials, improved selectivities towards gas fractions can be achieved, while lower acidity can yield greater liquid fractions.<sup>385</sup> Aluminosilicates can increase product quality, and reduce residue production as compared to thermal degradation.<sup>383,385–394</sup> Amorphous  $\text{SiO}_2\text{-Al}_2\text{O}_3$  lacks a pore network that could induce higher control over product selectivity.<sup>382</sup> Mesoporous catalysts have been explored for catalytic pyrolysis to increase mass-transfer.<sup>382</sup> The presence of mesopores allow for improved diffusion of the plastic molecules, which accelerate the initial rate of degradation and thus enhance plastic cracking. Both pure silica (kanemite-derived folded silica, FSM, MCM-41) and aluminosilicate (Al-MCM-41 and SBA-15) mesoporous structures have been explored for the degradation of PSW with varying success.<sup>390,392,395–400</sup> Pure silica mesoporous materials were found to yield higher quantities of liquid products – with higher selectivity towards kerosene and diesel fractions – during the catalytic pyrolysis of PE and PP as compared to thermal degradation.<sup>390,395</sup> It was found that the siloxane oxygens lining the channels of the mesopores could interact with the hydrogen atoms of the polymers to induce cracking.<sup>398</sup> The interaction allows for liquid oil product selectivity to be increased at the expense of heavy oil and wax fractions.<sup>396,399</sup> Additionally, the mild acidic character of the pure silica materials was found to enhance the cracking rate of polymers as compared to thermal degradation while also inhibiting extensive secondary cracking. As such, the all-silica mesoporous catalysts were found to be coke-resistant throughout multiple runs.<sup>390</sup>

For mesoporous aluminosilicates, the plastic decomposition product distribution was dependent on the acidity of the material. Low-acidic materials (Al-MCM-41, Al-SBA-15) have high resistance to coking and increased cracking activity compared to all-silica materials.<sup>392,400,402–404</sup> The additional acidity induced by the presence of alumina sites facilitates plastic cracking and can yield higher selectivity towards lighter hydrocarbons. For example, the product distribution for a PP/PE mixture was shifted towards  $\text{C}_6\text{--C}_{12}$  products for Al-MCM-41, while Al-SBA-15 yielded high-quality diesel oil (high selectivity towards  $\text{C}_{13}\text{--C}_{20}$  fraction, Fig. 20). However, both Al-MCM-41 and Al-SBA-15 were found to degrade a mixed plastics feed (HDPE, LDPE, PP, PE, and PS) to a similar product distribution of near equal amounts of  $\text{C}_1\text{--C}_5$ ,  $\text{C}_6\text{--C}_{12}$ , and  $\text{C}_{13}\text{--C}_{40}$  hydrocarbons.<sup>402,405</sup> The large pore size of mesoporous alumi-

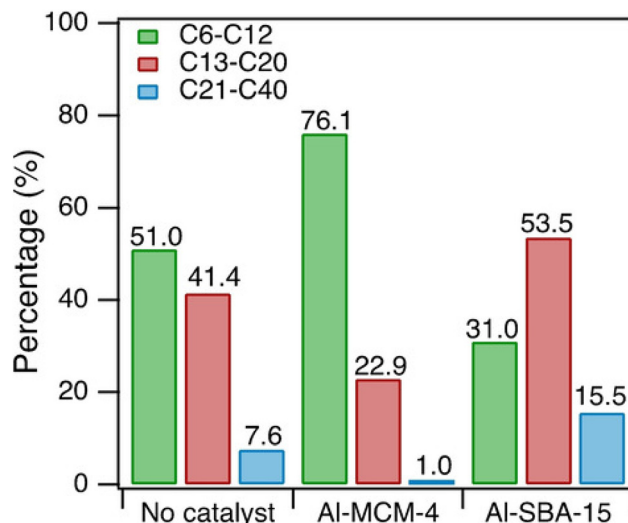


Fig. 20 Distribution of liquid and wax products for thermal pyrolysis and mesoporous aluminosilicates in the conversion of PE/PP (ratio 6 : 5). Pyrolysis experiments were conducted at 500 °C for 30 minutes using a batch reactor set up, where the catalyst-to-feedstock ratio was 0.03 : 1. Reproduced from ref. 401 with permission from Wiley-VCH, copyright 2020.

nosilicates allows for improved intercalation of polymer molecules to Brønsted acid sites but prevents the moderately cracked products from undergoing re-adsorption and secondary reactions that result in extensive cracking.<sup>406</sup> However, it was found that the promising cracking ability of mesoporous materials was only effective with polyolefin and polyaromatic PSW – polymers with other heteroatoms form coke which causes catalyst deactivation.<sup>402</sup>

While mesoporous aluminosilicates were found to be capable of producing favorable product distributions with limited amount of coke, zeolites have still been extensively explored for the catalytic pyrolysis of plastic waste.<sup>20,382</sup> Zeolite Y was found to have high cracking ability due to its high accessibility to active sites, but the larger micropores and high acidity were found to facilitate condensation and secondary reactions leading to fast deactivation.<sup>407–415</sup> Similarly, ZSM-5 has high cracking activity for polyolefins due to its strong acidity.<sup>413,416–425</sup> The microporous network within the ZSM-5 structure is ideal for the aromatization of cracked intermediates, however this precludes coke formation and fast deactivation.  $\beta$ -Zeolite yields higher gas fractions at the expense of liquid products because it is highly active for secondary reactions.<sup>389,426–431</sup> Additionally,  $\beta$ -zeolites were found to produce high quantities of residue and wax. Natural zeolites were found to have moderate cracking ability with higher selectivity towards the liquid fraction, but its efficiency was strongly correlated to the plastic/catalyst ratio.<sup>393,432–442</sup> Given the uncontrolled structure of natural zeolites, the materials contain impurities and there is little consistency amongst the materials. As such, there is high variability in the effectiveness of natural zeolites. Lastly, doped zeolites have been explored to



enhance the acidity of the material.<sup>436,443–452</sup> Doped zeolites were found to yield high selectivity towards olefinic products and were active for the removal of heteroatoms such as Br. One great challenge of the catalytic pyrolysis of plastic waste with zeolites is catalyst deactivation due to secondary coking reactions and limited diffusion of polymeric molecules into the microporous network.

Clays are another form of aluminosilicate that are of interest due to their weaker acidity, wide availability, and ability to produce medium distillate products such as diesel fuel.<sup>409,453–456</sup> Clays are composed of silica and alumina or magnesia (or both) and have a macroporous structure which induces high coke resistance and moderate polymer cracking to heavier products. Structured clays, such as pillared clays (PILC), can include heteromoiety like metal oxides (Al, Fe, Ti, and Zr) to improve the textural properties and increase catalyst acidity.<sup>453–456</sup> As such, PILCs have been found to have improved catalytic performance for HDPE and PE, as well as improved regeneration abilities. Clays, however, have lower activity due to the macroporous nature of the material, resulting in reduced contact of the feedstock with the weakly acidic sites within the structure.

Spray dried catalysts (typically Geldart Particle size A) are used in fluidized bed reactors because they are easier to flow in the fluidized bed. Spray dried catalysts (Fig. 21) are a mixture of clays or binders, zeolites, and silica-alumina matrices.<sup>457–463</sup> Spray dried catalysts can have a bimodal pore structure with micropores in the zeolite framework and mesopores in the silica-alumina matrix. It was recently determined by Weckhuysen and coworkers that, in the conversion of PP, the fluidized catalytic cracking (FCC) matrix was responsible for aromatization of cracked products and the zeolite domain was responsible for coking.<sup>457</sup> Zeolite and silica alumina catalysts can undergo structural changes during the reaction due to water vapor (dealumination) and impurities from the feed

building up on the catalyst surface. Thus, in a circulating fluidized bed reactor, such as in fluid catalytic cracking, it is important to study the “equilibrium catalyst”. It is the equilibrium catalyst which is the actual catalyst in the reactor. Studies of the effect of the equilibrium FCC catalyst on PP conversion found the same aromatic content as fresh FCC catalysts with reduced coking. The zeolite domains in an equilibrium catalyst were found to be inaccessible – resulting in reduced coking – and the FCC matrix was found to have enhanced cracking activity due to leached metal deposits. This work by Weckhuysen and co-workers suggests that the strong acidity and microporous structure of the zeolite domain within an FCC catalyst is not necessary for the aromatization of polyolefin feedstocks.<sup>457</sup> Further, the presence of zeolite domains may even be detrimental to the effectiveness of FCC catalysts for the catalytic pyrolysis of plastic waste.

Like FCC catalysts, multi-catalyst systems are zeolites mixed with MCM-41, NiO, muds, clays, salts, or metal silicates.<sup>396,464–468</sup> The systems are typically formed by either the mechanical mixing of the two separate catalysts *via* mortar and pestle or by layering the catalysts within the bed. As with other catalytic pyrolysis systems, the presence of the catalysts reduces the required temperature for polymeric degradation as compared to thermal pyrolysis.<sup>464,467</sup> The use of muds and clays with zeolites – such as a combination system of zeolite Y, metakaolin, aluminum hydroxide, and sodium silicate – has been found to improve the selectivity toward liquid products for a mixed plastic waste feed stream as compared to thermal pyrolysis.<sup>415,469,470</sup> Additionally, red mud and calcium hydroxide was found to reduce chlorine content in the products. The combination of zeolites and MCM-41 has been found to induce synergistic effects on plastic degradation, where the MCM-41 provides enhanced surface area, and the zeolite provides strong acidity.<sup>464</sup> For zeolite/MCM-41 systems, diffusional limitations were observed for the direct catalytic pyrolysis of HDPE. In two-stage pyrolytic-catalytic cracking with HZSM-5/MCM-41, a high yield of aromatic gasoline range products was formed.<sup>464</sup> Similarly, HY-zeolite/NiO was explored in a two-stage reactor.<sup>466</sup> The addition of NiO was found to increase gas selectivity at the expense of liquid products and reduce coke formation as compared to HY-zeolite alone. NiO was speculated to promote primary degradation of larger polymer fragments into radicals preventing coke deposition.<sup>466</sup> In total, composite systems can induce favorable synergistic effects that can result in a narrowed carbon number distribution of products as compared to thermal pyrolysis, however the favorable effects are highly dependent on the catalyst mixture ratio. Further, diffusional limitations are increased in composite systems given the physical mixture of varying pore networks and may require two-stage pyrolysis-catalysis.

Like composite systems, hierarchical and core-shell catalysts combine the advantageous properties of various materials into one system. Unlike composite systems, hierarchical and core-shell catalysts are contained within one structure rather than in a heterogeneous mixture or across multiple reactors. Many of the studies to date of hierarchical or core-shell cata-

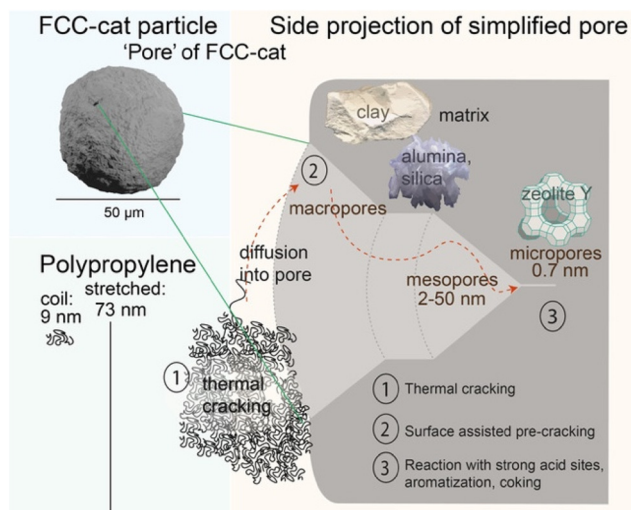


Fig. 21 Structure of a spray dried FCC catalyst. Reproduced from ref. 457 with permission from Wiley-VCH, copyright 2021.



lysts for plastic waste deconstruction combine the micropores of zeolites with secondary mesoporosity.<sup>445,446,449,450,471–481</sup> The goal is to allow for enhanced accessibility where faster intra-crystalline diffusion and lower steric hindrances occur. Catalysts such as these have been found to have higher resistance to coking and deactivation compared to traditional microporous zeolites.<sup>479</sup> Further, the secondary porosity of such materials renders improved gas and aromatic hydrocarbon production than their microporous counterpart. Hierarchical and core-shell materials are capable of supporting metals to enhance acidity and therefore activity.<sup>446,449,450,471–476,478,479</sup> However, these materials require refined and detailed synthesis – making scale up difficult – and the dual porosity must be well defined otherwise deactivation *via* coking will occur.

Silica and aluminosilicates have dominated catalytic pyrolysis because of their porous networks and acidity, however other metal oxides such as ZrO<sub>2</sub>, MgO, and CaO have shown interesting results.<sup>482–494</sup> In particular, sulfated zirconia – despite suffering from coke deactivation – has shown high cracking activity and isomerization, esterification, and hydrocracking ability.<sup>485,487,492,494</sup> By sulfating the metal oxide, the acidity of the material is enhanced, resulting in improved reactivity. Further, studies have explored promoting sulfated ZrO<sub>2</sub> with platinum and found that the material – in a two-step pyrolysis-catalytic hydrocracking process – can enhance the hydrocracking of LDPE into liquid products as compared to the non-doped material.<sup>483</sup> Other metal oxides such as MgO and CaO have been shown to reduce activation barriers and enhance selectivity toward phenolic compounds for PC catalytic pyrolysis, as well as reduce production of light gases (H<sub>2</sub>, CO<sub>2</sub>, CO, and methane) for PC and LDPE degradation.<sup>482,484,488,489,491</sup> It was determined that the basicity of CaO allowed for the reaction of CO<sub>2</sub> in the pyrolysis vapors, resulting in the production of CaCO<sub>3</sub>, while MgO was found to interact with H<sub>2</sub> and utilize the molecule for hydrogenation reactions.<sup>488,491</sup> However, CaO and MgO produce significant amounts of solid residue, where the carbonaceous char inhibited the movement of free radicals during the cracking reaction, preventing propagation and degradation of the plastic molecules.<sup>484</sup>

Outside of metal oxide catalysts, activated carbon has been tested for plastic catalytic pyrolysis but has been found to only minimally change product distribution.<sup>396,481,495–497</sup> Further, activated carbon has variable acidity – which can be modulated by the addition of different acid groups (–OH, –OOH, and –P–O) – that dictates the product distribution.<sup>396,497</sup> Weakly acidic activated carbons have been found to have high selectivity towards jet-fuel range alkanes within the liquid fraction and strongly acidic carbons (with P functionality) have improved selectivity towards jet-fuel range aromatics.<sup>481</sup> Additionally, metal-doped carbons have been utilized for PSW decomposition due to the high thermal stability of the material and the cracking ability of transition metals. For example, Pt/C and Pd/C were found to decompose PET into monocyclic compounds within the liquid fraction by improving decyclization activity and promoting thermal free radical

cracking mechanisms.<sup>498</sup> Pt/C was also found to crack the carbonaceous compounds that formed during catalytic pyrolysis of PET, further inhibiting the production of undesirable products.<sup>498</sup>

Like many of the catalysts described above, carbonates have been found to increase the rate, reduce operational temperature, and reduce residence time of plastic decomposition. However, carbonates are prone to decomposition under thermal treatment, resulting in the formation of oxide compounds and CO<sub>2</sub>. MgCO<sub>3</sub>, CoCO<sub>3</sub>, and CuCO<sub>3</sub> were all found to yield largely diesel fuel components in the liquid fraction for the catalytic pyrolysis of HDPE.<sup>499–502</sup> At the same time, gas yields were increased by 10–15% due to the decomposition of the material under reaction conditions.<sup>499</sup> The basic carbonates were hypothesized to initiate the plastic cracking mechanism *via* a different step than the acidic catalysts previously described, where the carbonates will accept a proton from a plastic defect site to create a carbocation chain rather than the catalyst donating the proton to form a carbonium molecule. The carbocation chain will undergo β-scission to form lower carbon number alkanes and alkenes, then further reaction will occur through carbonium ion attacks or interactions with the catalyst basic sites.

Ashes from plastic incineration plants have also proven to be effective in reforming plastic pyrolysis vapor using a pyrolysis-reforming reactor.<sup>503</sup> Incineration ashes contain ppm levels of metals due to metal evaporation and adsorption to the surface of ash particles during incineration. When used for in-line upgrading of plastic vapor, flying ash increased the BTX content of liquid product compared to non-catalytic upgrading. The Fe content of ash promoted the formation of monoaromatics while inhibiting the formation of polyaromatics.<sup>455,504</sup> Although the use of ash as a catalyst is attractive as it is a waste, the catalytic performance of this material is still inferior compared ZSM-5. Furthermore, pre-treatment of ashes is required to remove impurities that prevent access to active sites.

**5.2.2 Reactor design.** Two main approaches for catalytic pyrolysis have been proposed for plastic conversion: a single-stage catalytic-pyrolysis (*in situ*) process and a two-stage pyrolysis-catalysis (*ex situ*) process. In the single-stage process, the plastic waste and catalyst are directly mixed in a reactor (usually a fluidized bed reactor, Fig. 22) and heated to the degradation temperature. In the two-stage pyrolysis-catalysis process, the plastic waste is first thermally pyrolyzed and then the pyrolysis vapors are passed over a catalyst bed (which could potentially be a fixed bed reactor).<sup>505,506</sup> Fluidized beds are the most commonly used industrial reactors for processing solid materials. They have high rates of heat transfer and therefore can be scaled to larger industrial reactors.<sup>507</sup> Circulating fluidized bed reactors are commonly used in industry as they circulate the catalyst between a reaction and regeneration zone, where the coke on the catalyst can be continuously removed by oxidation. In contrast, fixed bed reactors must be shut down when the catalyst is regenerated leading to a decrease in capital efficiency. Fixed-bed catalytic reactors are preferred



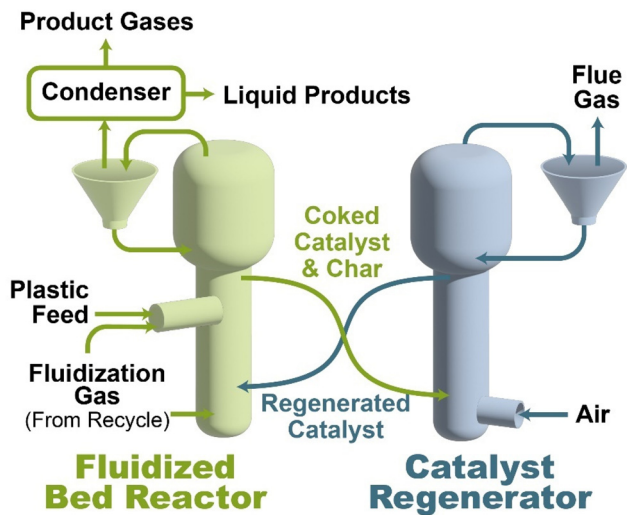


Fig. 22 Fluidized bed reactor for plastic pyrolysis.<sup>508</sup>

when no solids reactants or products are formed as they are simpler to design and operate than fluidized bed reactors. Plugging of the fixed-bed reactors is another major concern when operating with solids or in reactions that form larger amounts of coke.

**5.2.3 Commercial activities.** Anellotech, who originally developed a technology to catalytically convert biomass into aromatics called Bio-TCat, has developed a sister process that transforms plastic waste into virgin commodity chemicals using a circulating fluidized bed reactor. The process, Plas-TCat, converts mixed plastic waste into olefins and aromatics to be used as “drop in” raw materials to produce new plastics and work towards a plastic circular economy.<sup>508</sup> Plas-TCat uses a zeolite catalyst in a fluidized bed reactor to generate the desired products in a single catalytic step.<sup>508,509</sup> The technology can be used to either produce a high olefin or high aromatic product from mixed plastic wastes. It has several advantages compared to pyrolysis and steam cracking including lower capital cost, higher value of product, scalability of the fluidized bed reactor system, feedstock flexibility, and a narrower product yield.

Braskem, the leading biopolymer producer of thermoplastic polyolefins in America, has formed several partnerships to develop new catalysts for plastic catalytic upgrading.<sup>510–512</sup> Braskem is working with FCC S.A., the leading catalysts supplier of fluid catalytic cracking in the South American market, to develop new catalysts for plastic upgrading. In addition, Braskem and Encina have formed a long-term partnership to produce recycled PP. Encina development group is focusing on developing a catalytic pyrolysis process to produce BTX from plastics #3 through 7, with the focus on PP.

## 6. Liquefaction of plastics

Liquefaction typically operates at temperatures between 200–450 °C under high pressure to convert the plastic feed-

stock into a liquid oil in the liquid phase. Heterogenous or homogenous catalysts are sometimes added.<sup>513,514</sup> When liquefaction occurs in a solvent, it is called solvent liquefaction. Fuel liquids or monomers can be obtained from the liquefaction of plastics.<sup>513,515–523</sup> During liquefaction, pressurized nitrogen or other gases keep the pressure high, helping maintain the products in the liquid phase. Pressurized hydrogen enhances polymer chain cleavages, caps the chain ends with hydrogen, and produces liquids with higher H/C ratios and/or low boiling point products.<sup>521</sup> Various organic solvents, including hydrocarbons, alcohols, and water, are used to enhance the reaction rate and lower the activation energy of plastic decomposition, in addition to reducing unfavored secondary reactions for repolymerization.<sup>524–527</sup> Chemically-compatible solvents can facilitate product removal and dissolution, suppressing intermolecular coupling reactions.<sup>520</sup> Hydrogen-donating solvents can enhance product dissolution and stabilize intermediate products.<sup>518</sup>

When performed under supercritical states of solvents, solvent liquefaction also takes advantage of drastically increased reaction rates and enhanced solubilization capability of the polar and non-polar products.<sup>518,528</sup> In the case of hydrothermal liquefaction (HTL), water is a low-cost green solvent. Table 14 summarizes some of the previous work on plastic liquefaction processes, which are grouped into liquefaction using pressurized gases, HTL, and liquefaction by organic solvents with the majority of this work in stirred-tank batch reactors.

### 6.1 Products

**6.1.1 Liquefaction using pressurized gases.** Direct liquefaction of plastics using pressurized gases has been investigated since the 1990s, mainly applied to producing synthetic fuel oils from individual non-polar polymers or co-mingled waste plastics. Increasing the reaction pressure during liquefaction enhances liquid production and reduces gas formation. Hydrogen can be added to the liquefaction process to increase product yields by hydrogenating the products in a single step. Williams *et al.*<sup>523</sup> reported an increase in the oil yields from 71% to 77% for PS and 15% to 27% for PET by switching from a nitrogen to a hydrogen atmosphere, which almost entirely contributed to the decreased solid yields. In comparison, there were no significant increases in the oil yields from PE and PP by switching from a nitrogen atmosphere to hydrogen, as shown in Table 14. Liquefaction under pressurized gases also promotes the formation of aromatics from PE and PP. While PE pyrolysis at atmospheric pressure nitrogen almost exclusively produced aliphatic hydrocarbons, the oil produced using pressurized nitrogen contained 16.4% aromatics.<sup>523</sup> The increased gas pressure promoted secondary reactions of PE decomposition, such as saturation, cyclization, and isomerization.<sup>529</sup> Cyclization reactions were also promoted during hydrogen liquefaction, albeit less so than in liquefaction under nitrogen gas.<sup>523</sup> The work of Williams *et al.* also showed that hydrogen liquefaction increased the selectivity of single-ring aromatics for PS,<sup>523</sup> because the hydrogen atmosphere



Table 14 Literature reporting liquefaction of typical waste plastics (if not mentioned otherwise, assume stirred-tank batch reactors)

Type of plastics	Temp. (°C)	Pressure (MPa)	Time (h)	Concentration (%)	Solvent/gas/catalyst	Products	Oil yield (wt%)	Year	Ref.
<b>Liquefaction under pressurized gases</b>									
PE, PP, PS (continuous reactor)	400	—	—	—	w/or w/o ZSM-5	Majority aromatics, some aliphatic liquids and gases	85% (PE, PP); 90% (PS)	1992	515
MDPE, HDPE, PP, PET or mix	420–450	5	1	66% plastics in tetralin/waste oil	H <sub>2</sub> ; w/or w/o 1 wt% HZSM-5/ferrihydrite catalyst	Hydrocarbon oil and gases	w/o to with catalyst: 11 to 96% (HDPE); 83 to 98% (PP); 33 to 93% (MDPE)	1994	516
Mix of HDPE, LDPE, PET and PS	400–440	5.6	0.5–2	50% plastics in tetralin, decalin, dodecane, C <sub>12</sub> –C <sub>20</sub> alkanes	H <sub>2</sub> ; 10–20 wt% HZSM-5/FCC catalysts	Hydrocarbon oil and gases	56.2–75.8% conversion (mixture); 90–100% conversion (individual plastics)	1996	513
PS and SBR	350–450	3.45–17.23	0.25–2	1–5 wt% Fe <sub>2</sub> O <sub>3</sub> /SO <sub>4</sub> <sup>2–</sup> and ZrO <sub>2</sub> /SO <sub>4</sub> <sup>2–</sup>		Aromatics (PS); aromatics and C <sub>3</sub> –C <sub>10</sub> paraffins/cycloparaffins.	80.3% (PS); 72% (SBR)	1996	517
LDPE, PET, PVC	420–440	5.5	0.25–1	70% in tetralin	Hydrogen	C <sub>9</sub> –C <sub>40</sub> hydrocarbons and gases	59% (LDPE)	1996	518
MDPE, HDPE, PP	>420	0.68–5.5	0.3–1	30–50% in tetralin; H <sub>2</sub> or N <sub>2</sub> ; HZSM-5 or Al <sub>2</sub> O <sub>3</sub> –SiO <sub>2</sub> –ferrihydrite		Light, medium and heavy oils	>90% (all plastics)	1996	519
HDPE, PP, PB	350–450	3.5–13.8	0.5–3	n-Octadecane; H <sub>2</sub> ; 1–2 wt% Fe <sub>2</sub> O <sub>3</sub> /SO <sub>4</sub> <sup>2–</sup> and ZrO <sub>2</sub> /SO <sub>4</sub> <sup>2–</sup>		Gasoline range paraffins as major products	> 90%	1997	520
PE and PP	500	0.79	0.5	Hydrogen		Light and heavy oils	up to 60%	1998	521
Post-consumer plastic (PCW)	415–455	1.4	0.5–1	H <sub>2</sub> , 1–5 wt% of HZSM-5 and others		Higher gasoline range oil with catalysts	up to 85%	1999	522
PE, PP, PS, PVC, and PET (standalone and mixed)	500	1	1	Nitrogen and hydrogen		Hydrocarbon oil and gases with high concentrations of alkanes and single-ring aromatics	Calculated mix vs. PCW (DSD/waste Fost Plus): 72.3% vs. 32.5/64.1% (N <sub>2</sub> ); 75.12% vs. 48.2/70.6% (H <sub>2</sub> )	2007	523
<b>Hydrothermal liquefaction</b>									
HDPE	425	Corresp. to T	0.16–3	None		Light and medium oil	90.2% (120 min)	1999	524
SBR	450–686	<1000	0.022–0.5	5/10% H <sub>2</sub> O <sub>2</sub>		Light and medium HCs	25.9–66%	2002	530
<b>Hydrothermal liquefaction</b>									
HDPE	450–480	Corresp. to T	0.016–0.5	25–50	None	Light and medium oil	91.4% (460 °C, 1 min)	2004	531
PVC	200–600	1.6–55.7	1	0.1–2	None	Low-molecular weight aromatic and aliphatic compounds	179 ppm (300 °C), 396 ppm (400 °C)	2004	532
HDPE (continuous reactor)	530	25	0.02–0.07	—	None	C <sub>7</sub> –C <sub>11</sub> , C <sub>12</sub> –C <sub>18</sub> , C <sub>19</sub> –C <sub>24</sub> , >C <sub>24</sub>	79%	2007	533
Model mix of PE, PP, PS and PVC	200–400	1–5	100–200		Glass powder additive	Chlorine content after NaOH-based dechlorination	40–120 ppm in oil (negl.)	2011	534
PBT, PC, PLA, PMMA, POM, PPO, PVA, SB.	400	25	0.25	10	None	Oil%/solid%; nil/50.8 (PBT), 99.8/nil (PC), 68.5 (PET), 48/nil (PMMA), 13.7/8.1 (POM), 78.9/8.8 (PPO), 35.4/2.9 (PVA), 80.8/1.2 (SB)		2017	535
High impact PS (HIPS)	350–550	30	0.12–1	1–9	None	Ethylbenzene (51.3 wt%), toluene (14 wt%) and other polyaromatics (490 °C per 1 h)	Maximum carbon liquefaction rate of 77 wt% (490 °C, 1 h)	2019	536
PP	425–450	23	0.5–4	—	None	80% naphtha	91% (2 h per 425 °C; 1 h per 450 °C)	2019	537





Table 14 (Contd.)

Type of plastics	Temp. (°C)	Pressure (MPa)	Time (h)	Concentration (%)	Solvent/gas/catalyst	Products	Oil yield (wt%)	Year	Ref.
ABS, PA6, PA66, PET, Epoxy, PC, PUR, HDPE, PVC, LDPE, PP, PS	350	Corresp. to <i>T</i>	0.33	5.6	KOH	Bisphenol-A & phenol (PC, epoxy), caprolactam + (PA6, PA66), TE & EG (PET), TDA + (PUR) and no polyolefin-derived products		2020	538
PP, PS, PC and PET	350–450	25+	0.5–1	0.06–0.35	None	32% (PP, 425 °C, 30 min), 16% (PET, 450 °C, 30 min), 86% (PS, 350 °C, 30 min), and 60% (PC, 425 °C, 30 min).		2020	528
PC	350–450	Corresp. to <i>T</i>	0.03–1	5	None	IPP, IPrP, phenol, BPA, and other alkylphenols	57.7	2020	539
HDPE	400–450	Corresp. to <i>T</i>	0.5–4	57.1	None	Naphtha, heavy oil and heavy waxes	86–87% (425 °C, 2.5 h or 450 °C, 0.75 h)	2020	540
LDPE, HDPE	380–450	Corresp. to <i>T</i>	0.25–4	20	1% acetic acid	Alkanes, alkenes, cycloalkanes, aromatics, and negligible alcohols	85–90% (425–450 °C, 1 h)	2020	514
<b>Hydrothermal liquefaction</b>									
Mix of LLDPE and PP	400	25	1	16.67	None	Paraffins, olefins, cyclics and aromatics	90.7% (mixture); 87.04% (LLDPE); 86.42% (PP)	2021	541
A waste mixture containing polyolefins, PET, nylon, PVAc, and cellulose	340	Corresp. to <i>T</i>	5	10	2% NaOH	Aromatics, oxygenated compounds, benzoic acid, phenols, caprolactones, fatty acids, and no polyolefin-derived products	w/o/with NaOH: oil (7.7%/7.4%), solid (75.1%/65.5%), gas (11%/11%), unreacted & aqueous-phase products (6.2%/16%)	2021	542
<b>Liquefaction with other supercritical solvents</b>									
HDPE, PP and HDPE/PP mix	450–470	Corresp. to <i>T</i>	1	10%	Acetone	Aliphatic hydrocarbons	Oil yield: 88% (HDPE); 96% (PP); 90% (mix)	2021	525
PS	370	Corresp. to <i>T</i>	1.5	7–10%	<i>n</i> -Hexane	Styrene (primary); toluene and ethyl benzene (secondary)	90% conversion	2001	526
PS	340–420	Corresp. to <i>T</i>	0.25–1	—	Methanol	Styrene, toluene, ethylbenzene, dimer, and other 2-ringed aromatics	92% conversion (380 °C/15 min)	2008	527
HDPE; HDPE + spirulina microalgae	340	Corresp. to <i>T</i>	—	6–14%	Ethanol	Aliphatic hydrocarbons	7.55% (PE oil); ~50% (HDPE + spirulina)	2012	543
PS	350 (SC ethanol); 370 (HTL)	Corresp. to <i>T</i>	0.25–1.25	25–400%	Ethanol; water	Alkyls, alkenes, and aromatics (SC ethanol)	Oil yield: 84.74% (SC ethanol); 78.3% (HTL)	2020	544
HDPE + sugarcane bagasse mix	240–280	Corresp. to <i>T</i>	1–1.5	5–10%	Ethanol	Aliphatic hydrocarbons	32.3% (bio-oil yield)	2020	545 and 546

enhanced both chain cleavage and secondary saturation reactions compared to nitrogen.

Solid acid catalysts are often used during the hydrogen liquefaction of plastics. In general, the addition of catalyst lowers reaction temperature, increases conversion, and produces oils with higher light fractions. Shabtai *et al.* reported that conversion of HDPE during hydrogen liquefaction at 350 °C increased from nearly zero without a catalyst to 30% with a 17 wt% of  $\text{SO}_4/\text{ZrO}_2$  catalyst, and 64.7% using a 33%  $\text{Pt}/\text{SO}_4^{2-}/\text{ZrO}_2$  catalyst.<sup>520</sup> Much lower metal loadings were used in other related studies. For example, Zmierczak *et al.*<sup>517</sup> found catalytic hydrogen liquefaction of PS at 375 °C increased the conversion from 59.4% without a catalyst to 70.5% with a 5 wt%  $\text{Fe}_2\text{O}_3/\text{SO}_4^{2-}$  catalyst and to 80.3% with a 5 wt%  $\text{ZrO}_2/\text{SO}_4$  catalyst. Other catalysts were also evaluated for hydrogen liquefaction, as shown in Table 14. Shah *et al.* converted post-consumer plastic waste using 1 wt% HZSM-5 zeolite, a  $\text{ZrO}_2/\text{WO}_3$  catalyst, nanoscale ferrihydrite treated with citric acid, ferrihydrite containing 5% Mo, a  $\text{SiO}_2\text{-Al}_2\text{O}_3$  binary oxide, and two  $\text{TiO}_2\text{-SiO}_2$  binary oxides.<sup>522</sup> They reported that while there were no significant differences in the oil yields, the presence of ZSM-5 reduced the boiling point distribution of the oil products resulting in the most gasoline-like products. Similar results were also observed by Feng *et al.*<sup>519</sup>

Chemically compatible or hydrogen donor solvents have been used to aid the hydrogen liquefaction of plastics. For example, adding *n*-octadecane during  $\text{Pt}/\text{SO}_4^{2-}/\text{ZrO}_2$  catalyzed hydrogen liquefaction of HDPE at 350 °C increased the conversion from 64.7% without solvent to 92.5% with the solvent.<sup>520</sup> The plastic conversion in the solvent without catalyst was only 2%.<sup>520</sup> Tetralin has been studied as a hydrogen donor for coal liquefaction. As shown in Table 14, Taghiei *et al.*<sup>516</sup> reported that tetralin-aided hydrogen liquefaction of PE and PP increased the oil yield from 11% without a catalyst to 83% with a catalyst.<sup>2</sup> In contrast, the oil yield only increased from 62% to 64% for PET. Since PE and PP-derived products are non-polar hydrocarbons whereas PET-derived products are oxygenated polar products, chemical compatibility between the solvent and plastic decomposition products seemed to play a critical role in their study. Murty *et al.*<sup>518</sup> reported that PVC absorbs tetralin and that this promoted PVC decomposition. Feng *et al.*<sup>519</sup> reported that liquefaction of co-mingled waste plastics in the absence of solvent resulted in higher oil yields than the liquefaction in tetralin or waste motor oil, regardless of whether catalyst was added or not.

The liquefaction of plastics is highly sensitive to reaction temperature. Zmierczak *et al.*<sup>517</sup> reported an increase in the distillable product yield from 71% at 350 °C to 93% at 450 °C during catalytic hydrogen liquefaction of PS. Increasing temperature also increased the formation of single-ring aromatics (*i.e.*, benzene and alkylbenzenes) by further decomposing multi-ring products (*e.g.*, diphenyl or triphenyl alkenes).<sup>517</sup> However, increasing the temperature during catalytic liquefaction can also promote the cracking of liquid products to gases. Compared to catalytic liquefaction, reaction temperature seemed to have a greater effect on non-catalytic liquefaction.

Feng *et al.*<sup>519</sup> showed that the oil yield from mixed post-consumer plastics at 430 °C was only about 25% with no catalyst and 60–63 wt% with 1 wt% HZSM-5 or Al/Si as the catalyst. However, oil yields of over 90% were obtained at 460 °C both with and without catalysts.<sup>519</sup> For all cases, gasoline and kerosene fractions increased with increasing temperature.

In general, increasing reaction time increased both conversion and secondary reactions. Shabtai *et al.*<sup>520</sup> reported that increasing reaction time during catalytic hydrogen liquefaction of HDPE at 450 °C improved the conversion from 82.5% to 100% but also reduced the oil yield from 92.8% to 60.2% due to increased cracking at prolonged reaction times. A similar trend was also observed with PP.<sup>520</sup> Increasing the reaction time also enabled the complete depolymerization of PS to single ring aromatics and promoted secondary cyclization of the primary monomers to form more naphthalene and indane as reported by Zmierczak *et al.*<sup>517</sup> While the effect of hydrogen pressure is usually less significant than reaction temperature or time, it can improve both conversion and oil quality.<sup>519,520</sup> For example, Murty *et al.*<sup>518</sup> reported that the oil produced from LDPE at 440 °C using 800 psi hydrogen pressure was three times less viscous than the oil obtained using 100 psi hydrogen pressure because of the conversion from heavy oil to light oil at higher pressure. Increasing pressure also promoted single-ring aromatics and suppressed secondary cyclization during catalytic liquefaction of PS.<sup>517</sup>

Feedstock heterogeneity is the most challenging problem in converting real-world plastic wastes. Williams and Slaney<sup>523</sup> evaluated the feedstock compositional variability under comparable liquefaction in this context. They conducted non-catalytic liquefaction of a mixture containing HDPE, PP, PET, and PVC. The product yields obtained from the mixture were then compared with the theoretical product yields calculated using those obtained when their constituent polymers were independently converted under the same condition. The oil yields produced from the mixed plastics were significantly lower than the calculated yields for nitrogen and hydrogen liquefaction. The effect of feedstock preparation methods showed that the PCW prepared in Belgium by Fost Plus *via* air blowing separation (obtaining a low density fraction of PCW) produced much higher oil yields and lower solid residues than the non-plastic removed PCW prepared by water washing (Waste DSD).<sup>523</sup> Plastic wastes from Waste Fost Plus were expected to contain a high fraction of low-density plastics (LDPE, PP, and PS) and a lower fraction of high-density plastics (HDPE, PVC, and PET).<sup>523</sup> Unfortunately, the authors investigated neither the product compositions nor the possible interactions among the compositions to elaborate on the crucial results. Contaminant content in mixed plastics also had a significant detrimental impact during hydrogen liquefaction. The catalytic effect was severely hindered during Shah *et al.*'s study when the dirtier PCW prepared by dry separation was converted.<sup>522</sup> The authors found no noticeable changes in either yields or boiling point distributions of the products before and after using 1 wt% of HZSM-5 or other catalysts. In contrast, adding identical amounts of catalysts to a cleaner PCW prepared by



water washing significantly increased the gasoline fraction of the oil products.<sup>522</sup> The dirtier PCW contained slightly more N and Cl elements than the cleaner PCW (0.67% vs. 0.65% for N, 1.26% vs. 0.03% for Cl), likely from PVC and polyurethane.<sup>522</sup> Thus, catalyst deactivation by the heteroatoms Cl and N can be considered among the reasons for the reduced catalyst performance.

**6.1.2 Hydrothermal liquefaction (HTL).** Water and other solvents behave differently beyond their critical points. Above the critical point, water exhibits two-phase behavior with characteristics of both liquids and gases. When the critical state temperature and pressure are reached ( $T = 375\text{ °C}$  and  $P = 22\text{ MPa}$ ), the diffusivity, viscosity, and solubility parameters of water change, thereby inducing changes in its density, heat and mass transfer coefficients, and dielectric constant.<sup>537</sup> Supercritical water (SCW), with its excellent heat transfer properties, can be leveraged to chemically recycle waste plastics by deconstructing the plastics into their constituent monomers or other value-added chemicals, as well as hydrocarbon fuels.<sup>528</sup> This is made possible by the acid catalyst-like behavior exhibited by the SCW at high temperatures where an abundance of  $\text{H}^+$ ,  $\text{H}^+$ , and  $\text{OH}^-$  ions are produced.<sup>536</sup> HTL facilitates both ionic and free-radical reactions depending on the reaction conditions.<sup>528,538</sup>

Depending on their polymer structure, either monomers or fuel oil products are obtained during the HTL of plastics. Some step-growth polymers formed by condensation polymerization, such as PET, PC, polyamides, and polyurethane (PUR), have ether, ester, or acid amide linkages.<sup>528,535,538,539</sup> These functional groups can be hydrolyzed to rapidly depolymerize the plastics with high chemical selectivity and liquefaction efficiencies even under sub-critical conditions.<sup>528,538,539</sup> There is pronounced support for hydrogen bonding and ion solvation due to the higher density of the sub-critical water medium.<sup>528,538</sup> HTL of PUR mainly promotes monomer production. It was reported that the sub-critical liquefaction of PUR at only  $250\text{ °C}$  for 30 min produced diaminotoluene (TDA) at 72% yield along with some other aromatics and polyols.<sup>547</sup> Passosa *et al.*<sup>538</sup> reported oligomers as the primary products when PUR was converted at  $350\text{ °C}$  using fast heating rates and short residence times, suggesting partial depolymerization under such conditions. HTL of PUR produces  $\text{NH}_3$ . The solubilized  $\text{NH}_3$  then acts as a base catalyst to promote PUR decomposition.<sup>538</sup> As reported by Passosa *et al.*<sup>538</sup> and Goto *et al.*,<sup>548</sup> polyamides (PA including PA6 and PA66) were hydrolyzed during HTL at temperatures above  $300\text{ °C}$  to produce  $\epsilon$ -aminocaproic acid, which further decomposed to form  $\epsilon$ -caprolactam in nearly theoretical yield. When caprolactam was further hydrolyzed over extended reaction time, a range of water-soluble oxygenated platform chemicals were produced.<sup>538,548</sup> Passosa *et al.*<sup>538</sup> showed that adding KOH catalyst to the HTL of PA could significantly increase oil yield and promote complete depolymerization in reduced residence times. The presence of the base catalyst also accelerated the production of oxygenated products soluble in water<sup>542</sup> and increased the selectivity of polyaromatics and oxygenated compounds derived from plastics like PC and PURs.<sup>538</sup>

HTL of non-polar plastics (polyolefins and PS) usually requires supercritical or near supercritical conditions to be effective. According to Ciuffi *et al.*,<sup>542</sup> compounds from PE, PP, and PS depolymerization were absent from the liquid products obtained for subcritical HTL of mixed plastic wastes. The lack of heteroatoms (*i.e.*, polar reactive sites) in the polyolefins and PS prevents the plastics from depolymerizing under mild conditions.<sup>538,542</sup> As shown in Table 14, HTL of PS has been widely studied. Kwak *et al.*<sup>549</sup> reported the complete and nearly instantaneous conversion of PS at  $400\text{ °C}$ . Higher temperatures or prolonged reaction times at supercritical conditions will further decompose liquefied products by promoting secondary reactions. Seshasayee *et al.*<sup>528</sup> reported a decrease in PS-derived oil yield from 86.2% at  $350\text{ °C}$  to 38.3% at  $450\text{ °C}$  after 30 minutes of treatment. HTP of PS usually produces styrene monomer, ethylbenzene,  $\alpha$ -methylstyrene, styrene dimer, styrene trimer, and other dimer/trimer associated products. Toluene and ethylbenzene were the major liquid products under supercritical reaction conditions. Bai *et al.*<sup>536</sup> reported yields for toluene and ethylbenzene at  $490\text{ °C}$  to reach 14% and 51.3%, respectively.

HTL of polyolefins was conducted under supercritical conditions to produce an oil similar to naphtha. Several articles have reported 85–90% oil yields from HDPE and LDPE in supercritical HTL.<sup>514,540,541</sup> As given in Table 14, oil yields higher than 90% from HDPE were reported by Murty *et al.*<sup>518</sup> and Su *et al.*<sup>533</sup> where HTL was performed in batch reactors.<sup>524,531</sup> In comparison, the highest yield obtained using a continuous reactor system was 79% at  $530\text{ °C}$  (Table 14).<sup>533</sup> Supercritical HTL of polyolefins yields oils with a wide range of molecular weights. A narrower distribution can be obtained by increasing temperature and reaction time.<sup>531</sup> HTL of PE produces *n*-alkanes as the major products, followed by 1-alkenes and alkadienes.<sup>514,540</sup>

Intramolecular  $\beta$ -scission and intermolecular hydrogen abstraction (H abstraction) are generally considered the primary mechanisms for polyolefins to degrade during HTL. When the PE backbone undergoes homolytic cleavage, the random scission produces free radicals with a random number of carbon atoms. These radical ends can be terminated by hydrogen abstraction from within the molecule (by  $\beta$ -scission) or from other molecules (by H abstraction).<sup>550</sup> The ratio between 1-alkenes and *n*-alkanes in the product can indicate which reaction is prominent.<sup>550</sup> During HTL, polymer fragments with radical ends immediately dissolve in SCW, where large amounts of excited H radicals are available. Thus, H abstraction becomes more prominent than  $\beta$ -scission.<sup>528</sup> This is also why previous studies frequently report the 1-alkene-to-*n*-alkane ratio to be lower in HTL of PE than in thermal pyrolysis of PE.<sup>524</sup> At extended reaction times, *n*-alkanes can undergo isomerization, and alkenes can undergo secondary reactions like cyclization.<sup>540</sup> Gas production is also increased under these conditions due to increased cracking or recombination of short-chain free radicals.<sup>540</sup> Aromatization is suppressed under HTL, thus producing less char from plastics.<sup>524</sup> When HTL was conducted in a continuous or a semi-batch



reactor system, the radicals were quickly removed from the reaction region. This led to a decreased opportunity for H abstraction, producing more alkenes than *n*-alkanes.<sup>533,551</sup> In addition to promoting chain cleavage, HTL can also oxidize the hydrocarbon products to form alcohols and ketones. Products such as 2-propanol, 2-butanol, 2-propanone, and 2-butanone were found in the aqueous phase products obtained during HTP of polyolefins by Moriya *et al.*<sup>524</sup>

As shown in Table 14, oil yields up to 91% from supercritical HTL of PP were reported using reaction temperatures up to 450 °C.<sup>537</sup> The oil fraction consisted of olefins, paraffins, and cyclic and aromatic compounds, with 80–90% of these compounds in the naphtha range. The authors also reported that the PP-derived oil is comparable to gasoline in terms of their H/C and O/C ratios, boiling point range, carbon numbers, density, viscosity, and surface tension.<sup>537</sup> Similar product composition from HTL of PP was also reported by others,<sup>541</sup> presenting an opportunity for PP-derived oil to be directly used as fuel feedstocks and blendstocks without further upgrading. Zhao *et al.* studied co-conversion of LLDPE and PP by HTL at 400 °C and reported the oil yield from the plastic mixture to be higher than the yield produced by converting LLDPE or PP alone, as shown in Table 14.<sup>541</sup> In this study, PE produced more heavy oil than medium or light oils whereas PP produced equal amounts of naphtha (light oil), medium, and heavy oils. In comparison, the mixtures of PP and PE produced more heavy oil than naphtha or light oil. HTL co-conversion also increased the formation of cyclic compounds while reducing paraffin production.<sup>541</sup> Thus, relatively lower quality oil was obtained by co-conversion, although the oil yield synergistically increased.

Subcritical HTL of PVC was also investigated because hydrochloric acid, produced from the PVC, is water soluble. PVC was dechlorinated in subcritical water at 200 °C in Takeshita *et al.*'s work to yield polyenes as solid residue without producing any hazardous organochlorine compounds.<sup>532</sup> When the reaction temperature increased to 250–350 °C, a mixture of low-molecular-weight aromatic and aliphatic compounds was produced. As the temperature further increased to 400 °C, the increased production of light alkanes and alkenes was also accompanied by the formation of aliphatic ketones and oxygenated benzene compounds at higher yields.<sup>532</sup> Inside the highly acidic solution created by the PVC-derived HCl, the PVC-derived polyene can undergo cyclization, hydrolysis, oxidation, and thermal degradation.<sup>532,538</sup> As shown in Table 14, base catalysts, such as NaOH or KOH, were added during HTL of PVC to study their effect on dechlorination. Passosa *et al.*<sup>538</sup> showed that although adding KOH did not affect the oil and solid yields produced from PVC at 350 °C, it caused more chlorine to leave as Cl<sub>2</sub> gas rather than remaining in the solution as HCl.

Increasing temperature and treatment time during HTL often facilitated conversion to increase liquid and gas yields.<sup>514,524,531,539,540</sup> However, it has been noted that high reaction temperatures and a prolonged residence time can reduce the desired product yield and increase coke formation

due to over-cracking of the liquefied products.<sup>530,532,536</sup> The feedstock-to-solvent mass ratio also affected the HTL process. Increasing the feedstock mass loading caused the liquefaction reaction rate to first increase and then decrease. Increasing the solid mass loading to beyond the corresponding optimum led to increased heat transfer limitations and decreased mobility of the macromolecular free-radical fragments in the solution.<sup>539</sup> Such limitations favored undesired secondary reactions like repolymerization. Jin<sup>539</sup> *et al.* also reported that increasing temperature and mass ratio would eventually result in decreased liquefaction efficiency for the same reaction time. When high mass ratios were employed at higher reaction temperatures, increased reaction rate and higher H<sup>+</sup>/H<sup>•</sup> concentration in the solution caused the monomers and oligomers of the liquified products to undergo further cracking to form gaseous products.<sup>539</sup> The effect of pressure during HTL of plastics is generally considered less significant than reaction temperature and time, especially for continuous and semi-batch reactor systems.<sup>533</sup> Although the pressure effect was only observed in some studies, an increase in pressure increased the ion products of the water due to increased density, subsequently bolstering the cracking and hydrolysis process.<sup>536</sup> An increase in pressure also enables enhanced interaction among different reaction species, promoting cyclization, hydrolysis, oxidation, and thermal degradation all at the same time.<sup>532</sup> Depending on plastic types and the availability of reactive sites, any of these reactions may take precedence.

### 6.1.3 Liquefaction with other organic solvents.

Liquefaction of plastics in supercritical hydrocarbons and alcohol solvents has also been studied, as shown in Table 14. In general, the solvents were used to enhance product dissolution, increase reaction rates, and stabilize products. However, in these cases, the solvent is a co-reactant and the conversion of the solvent must be considered. Hwang *et al.*<sup>526</sup> reported that at least 90% of PS was converted in *n*-hexane at 370 °C, while there was almost no conversion when PS was pyrolyzed at the same temperature.

Ethanol achieves its critical states at relatively milder operating conditions, and its low dielectric constant increases the solubility of both polar and non-polar products. Furthermore, ethanol can also act as a hydrogen-donor solvent to stabilize the intermediate products and reduce repolymerization reactions. Breaking alcohol solvent at the critical state produces excessive hydrogen and hydroxyl ions, aiding the hydrogenation reactions. Ahmad *et al.* reported that the oil yield produced from PS conversion in ethanol at 350 °C was 84.74%, higher than 71% from pyrolysis at 500 °C, and 78.3% obtained using HTL at 370 °C.<sup>544</sup> Rather than producing styrene as the primary monomer, the liquid produced using ethanol solvent consisted of alkyls, alkenes, and aromatics.<sup>544</sup> Compared to PS, less liquid was produced when PE was converted in ethanol. According to Pei *et al.*, the oil yield of HDPE in 340 °C ethanol was only 7.55%.<sup>543</sup> However, co-liquefying PE with microalgae or lignocellulosic biomass in ethanol was found to synergistically increase the liquid yield because the oxygenated feedstock enhanced the thermal decomposition of PE in the



solvent probably by hydrogen abstraction from PE by the oxygenated biopolymers.<sup>545,546</sup>

Methanol is also a hydrogen donor solvent with low critical conditions. Shin and Bae reported 92% conversion for PS by treating with 380 °C methanol for 15 min.<sup>527</sup> Their comparative study showed that the activation energy for degrading PS in supercritical methanol was 117.2 kJ mol<sup>-1</sup>, lower than 132 kJ mol<sup>-1</sup> in supercritical *n*-hexane, 157 kJ mol<sup>-1</sup> with supercritical water, and 224 kJ mol<sup>-1</sup> in pyrolysis. The authors reported the hydrogenation of unsaturated products to be the predominant reaction in methanol. Besides donating hydrogen, methanol also directly reacted with styrene monomer and  $\alpha$ -methylstyrene to produce 3-phenyl propanol and 3-phenyl-1-butanol.<sup>527</sup>

## 6.2 Reactor designs

Lab-scale liquefaction studies have predominantly been carried out in batch reactors with few accounts of continuous reactor systems. Industrial-scale processes have incorporated both batch and continuous reactor designs. Stirred or agitated tank reactors are the most employed batch reactor designs at both lab and industry-scale. The different continuous reactor designs adopted for industrial-scale processes are continuous flow stirred tank, rotary kiln, fixed bed, and tubular reactors, with gravity or auger/extruder-based material feeding mechanisms.<sup>552,553</sup> Fig. 23 shows an example of an industrial-scale continuous flow reactor design.

## 6.3 Commercial activities in plastics liquefaction

**6.3.1 Hydrogenation plants in Germany.** The Vega process was initially developed to convert coal into naphtha and gas oil. This process was pioneered by Vega Oel GmbH of Germany and then later adopted to depolymerize waste plastics into syncrude, hydrogenated solid residue, and HCl if a dechlorination step was involved.<sup>552</sup> Later, in 1999, the technology was discontinued due to the higher cost involved than in more economical feedstock recycling processes and mechanical recycling.<sup>552</sup> Several other multi-stage upgrading and direct hydrogenation liquefaction projects of waste plastics were also established by German companies like RWE-Entsorgungs AG, Hiedrierwerke Zeitz GmbH and Bergakademie Freiberg, but later terminated.<sup>552</sup>

**6.3.2 Liquefaction plants in Japan.** The growth of feedstock recycling in Japan was spurred by the Plastic Containers and Packaging Recycling Law passed in 2000. This law promoted sorting at collection and recycling of plastic waste containers.<sup>553</sup> Less of the waste plastic bale materials were made available to liquefaction plants and at a higher tender price when compared to other feedstock recycling. Due to this, liquefaction had a lower combined plant capacity than other feedstock recycling approaches.<sup>553</sup> The Niigata liquefaction plant was established with a capacity of 6 kton per year with support from the Plastic Waste Management Institute (PWMI) and the city of Niigata.<sup>555,556</sup> The plant operated by Rekisei Koyu started commercial operation in April 1998 and demonstrated

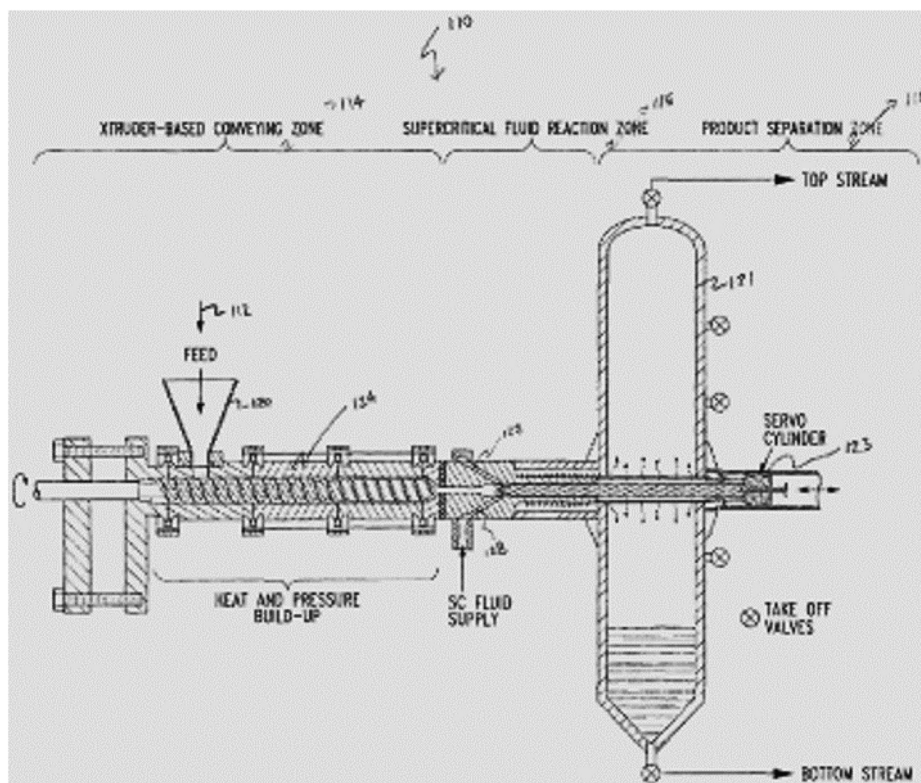


Fig. 23 Example of a continuous tubular reactor design for hydrothermal liquefaction of plastics (extracted from the US patent US 8980143B2).<sup>554</sup>



that unsegregated and contaminated household waste plastics could be converted to oil.<sup>555,556</sup> Mixed plastic bales comprising PE, PP, PS, PET, and PVC were allocated from the city of Niigata. The PWMI designed and TOSHIBA-built plant has a pretreatment stage to remove PET and other contaminants followed by a dechlorination stage. The liquefaction process occurs at 420 °C in a stirred tank reactor where 65% of the oil produced was utilized as process fuel within the plant.<sup>553,556</sup> Details for this process can be found in the 2019 PWMI annual report.<sup>557</sup>

The Sapporo Plastic Recycle Co. Ltd (SPR) was established in 2000 with the support of PWMI and Sapporo city with an initial capacity of 13.5 kton year which later grew into 14.5 kton per year.<sup>553</sup> The SPR plant treated mixed plastics at three stages. The first stage involved pretreatment, sorting and pelletizing, followed by dechlorination, which fed calcium hydroxide into the system. The third and final stage involved thermally decomposing the waste plastics in a rotary kiln reactor at 400 °C and 5 kPa overpressure to produce light, medium, and heavy fractions of oils.<sup>553,556</sup> Approximately 65% of the total oil produced was utilized as a process fuel within the plant.<sup>553</sup> Due to the tender system governed by the Japan Container and Package Recycling Association (JCPRA), only half of the baled plastics were used in the SPR liquefaction plant. Additionally, the small operation scale of the SPR plant also raised the cost of waste plastics recycling.<sup>553</sup> In Mikasa city, another large scale (6 kton per year capacity) liquefaction plant started operation in 2000 but was shut down in early 2004 due to a lack of waste plastic feedstock to process.<sup>556</sup> By 2010, all major liquefaction plants in Japan ceased, with the advanced SPR plant being the last of them. A 2019 PWMI report suggested that the need for the crude oil product to be further cracked and refined meant that the process was not commercially viable at that time.<sup>557</sup> Furthermore, these facilities are prone to fire accidents due to the risk of an explosion associated with the liquefaction reactors. Since the 2000s, liquefaction research and development have improved direct liquefaction methods to convert waste feedstocks to naphtha and diesel and thus reduced the burden for further refining. Nevertheless, the issues related to the scale of the plants and businesses remain, and any new companies adopting this technology will face difficulties.<sup>557</sup>

**6.3.3 Plants with hydrothermal liquefaction.** Licella Holdings, Australia, has carried out HTL research over the past two decades and has established the Cat-HTR technology.<sup>558</sup> The first-ever continuous-flow Cat-HTR liquefaction facility, with a capacity of 20 kton per year, was established by Licella Holdings in Australia in 2007, now operated by iQRenew.<sup>558</sup> Cat-HTR technology is being commercialized internationally via MURA Technology Ltd, Licella's global joint-venture with Armstrong Energy based in the UK.<sup>558</sup> MURA technology has proposed a process called Hydro-PRS adopting the Cat-HTR technology.<sup>559</sup> In 2021, Renew-ELP, based in the UK, started construction of a similar plant in England after obtaining a license for the Hydro-PRS process from Mura Technology.<sup>559</sup> The companies claim that mixed plastic waste with a limited

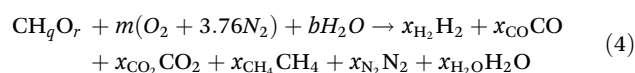
PVC content can be treated using this process. The Cat-HTR/Hydro-PRS process involved treating waste plastics or other carbonaceous feedstock at sub-critical or supercritical water to produce naphtha, distillate gas oil, heavy gas oil, and heavy wax residue.<sup>559,560</sup> Decontaminated waste plastic mixture is added to the hopper with an extruder (1), and the melted plastics exiting the hopper were pressurized (2). These molten plastics and SCW were mixed in a chamber (3) before the slurry was fed into the Cat-HTR reactors (4). Note that the Cat-HTR reactors are heated by both a heat carrier (hot water in the chamber) and an external heat exchanger. Here, the waste plastics are treated for 20–25 min at 350–420 °C and above 220 bar to produce over 85% liquid. The post-conversion contents are depressurized (5) before feeding into the flash distillation chamber, where the products are separated (6). The condensable products are then stored (7), and the gases are used as process fuel.<sup>558–560</sup> The used water after the product separation was recycled in the same system. This process operated at a waste concentration of about 70%.<sup>558,561</sup>

Another company called Aduro Clean Technologies from Canada has also developed an HTL-based commercial process. They call their process Hydrochemolytic Plastic Upcycling where the reactor operates at only 240–390 °C and takes about 25 min to completely convert the plastic mixtures.<sup>562,563</sup> According to their claim, their water-based process operates under less severe conditions and allows the manipulation of chemical reactions associated with different types of plastics to form a comprehensive approach for chemical conversion of plastics.<sup>563</sup>

## 7. Gasification of waste plastics

### 7.1 Fundamentals of gasification reactions

Gasification (or partial oxidation) of MSW converts solid waste into synthesis gas or producer gas (CO, H<sub>2</sub>, CH<sub>4</sub>) by the reaction shown in eqn (4), where CH<sub>q</sub>O<sub>r</sub> represents the feedstock; *q* and *r* are the hydrogen and oxygen to carbon ratios, respectively; *m* and *b* are the input air and steam to MSW ratios; *x<sub>i</sub>* is the mole number of molecular species *i*.<sup>564</sup> Producer gas (CO, H<sub>2</sub>, N<sub>2</sub>) is produced when air is used for the gasification while synthesis gas (CO, H<sub>2</sub>) is produced when oxygen is used for gasification. Synthesis gas can be further processed to produce a range of chemicals and fuels. MSW and mixed plastic waste can be used as the feed for gasification.<sup>565</sup> MSW gasification could be more profitable and environmentally sustainable than incineration.<sup>566,567</sup> A comparative study estimates that the global warming impacts of waste gasification with a combined cycle powerplant are over 50% lower than incineration.<sup>568</sup>



Gasification of MSW occurs above 550 °C.<sup>569</sup> The main MSW gasification products are gases including CO, H<sub>2</sub>, CO<sub>2</sub>, and CH<sub>4</sub>. Solid residues (*i.e.*, ash) are also produced. The



amount of ash depends on the equivalence ratio (*i.e.*, the ratio of oxygen in the employed oxidant and the oxygen required for complete combustion). Ash can be minimized by applying equivalence ratios between 0.25 and 0.35. Accordingly, equivalence ratios within this range are usually used in commercial reactors. Chemical thermodynamics can be used to predict the gas phase products during gasification.<sup>570,571</sup>

As shown in Table 15, at lower gasification temperatures (*i.e.*, around 600 °C) there is a significant amount of CO<sub>2</sub><sup>572</sup> formed from the highly exothermic CO oxidation (eqn (5)), the oxidation of carbon (eqn (6)) and the water-gas shift reaction (eqn (7)). These reactions are thermodynamically unfavorable at higher gasification temperatures (>700 °C) leading to a decrease in the amount of CO<sub>2</sub> produced.<sup>571,573</sup> Conversely, more CO is formed at these higher temperatures by the steam reforming of CH<sub>4</sub> (eqn (8)), steam reforming of hydrocarbons, the steam gasification of char (eqn (9)) and the dry reforming of hydrocarbons (eqn (11)) all of which are highly endothermic reactions. The Boudouard reaction (eqn (10)) is yet another highly endothermic reaction that yields CO.<sup>574</sup> Material and operational constraints such as tar condensation and accumulation<sup>575</sup> often require maintaining gas temperatures above 700 °C.

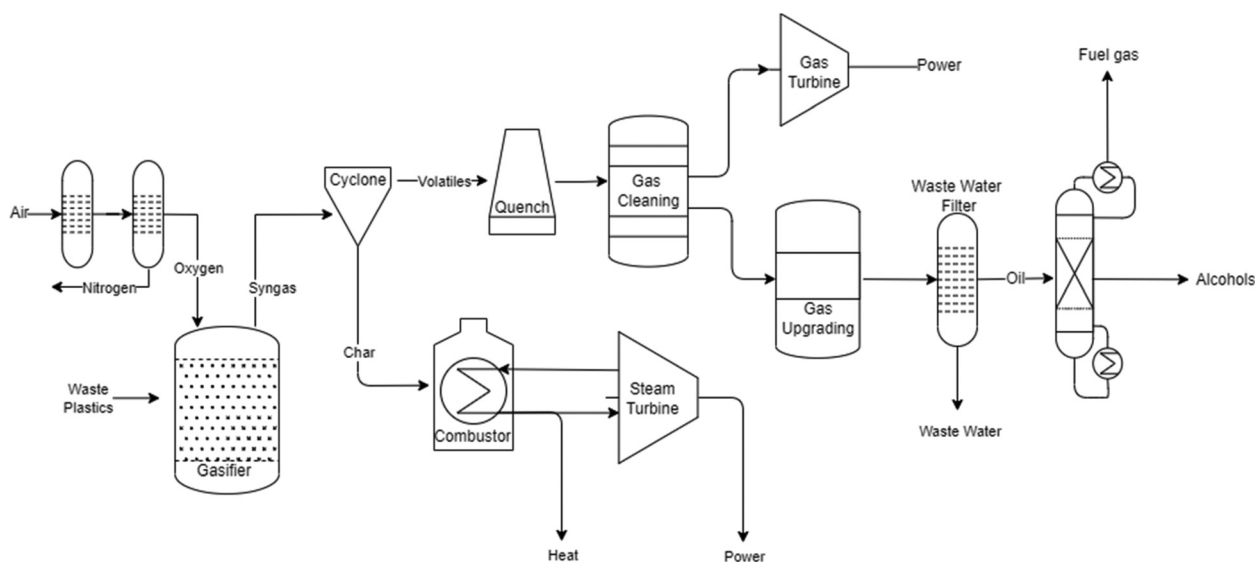
## 7.2 Waste plastic gasification process flow diagram

Fig. 24 shows a general flow diagram for waste plastic gasification processes. The feedstock is fed into a gasifier where gasification takes place. The volatiles enter a combination of physical, thermal, or chemical gas cleaning technologies where char, slags, and ash are removed. The clean syngas is then cooled in a quench unit to the temperature required for a secondary gas cleaning step. The secondary gas cleaning step removes contaminants that can impact catalyst performance, such as sulfur, halides, HCN, NH<sub>3</sub>, and tar, to levels of less than 0.1 parts per million by volume.<sup>576</sup> The cleaned syngas can either go to a turbine for power generation or for catalytic upgrading to other products. Synthetic gas consisting mostly of CO and H<sub>2</sub> is the feedstock for many catalytic synthesis systems.<sup>577,578</sup> The synthetic gas mixture can be catalytically converted to methanol and other alcohols. Platform chemicals such as ethylene, propylene, and other alkenes can be produced *via* the methanol-to-olefins process.<sup>579</sup>

The design and configuration of waste plastic gasification facilities depend on the facility scale and targeted products. Some gasification facilities combust the synthetic gas and solid by-product streams to produce combinations of heat and

**Table 15** Fundamental reactions that take place during the gasification of MSW along with the heat of reaction at standard conditions

Reaction	$\Delta H$ (kJ mol <sup>-1</sup> )	Name	Eqn
$\text{CO} + \frac{1}{2}\text{O}_2 \rightarrow \text{CO}_2$	-283.7 kJ mol <sup>-1</sup>	CO oxidation	(5)
$\text{C} + \text{O}_2 \rightarrow \text{CO}_2$	-394.1 kJ mol <sup>-1</sup>	Carbon partial oxidation	(6)
$\text{CO} + \text{H}_2\text{O} \leftrightarrow \text{CO}_2 + \text{H}_2$	-41.0 kJ mol <sup>-1</sup>	Water-gas shift	(7)
$\text{CH}_4 + \text{H}_2\text{O} \leftrightarrow \text{CO} + 3\text{H}_2$	+206.0 kJ mol <sup>-1</sup>	Methane steam reforming	(8)
$\text{C} + \text{H}_2\text{O} \leftrightarrow \text{CO} + \text{H}_2$	+131.0 kJ mol <sup>-1</sup>	Steam gasification of char	(9)
$\text{C} + \text{CO}_2 \leftrightarrow 2\text{CO}$	+172.0 kJ mol <sup>-1</sup>	Boudouard reaction	(10)
$\text{C}_x\text{H}_y + x\text{CO}_2 \leftrightarrow 2x\text{CO} + y/2\text{H}_2$	Endothermic	Dry reforming	(11)



**Fig. 24** Gasification of waste plastics and upgrading to heat, power, olefins, alcohols, and other fuels.



power. Other gasification facilities include steam generation, catalytic upgrading, and other product recovery units to improve energy efficiency and target higher-value markets.

### 7.3 Commercial activities scale

According to the Energy Information Administration (EIA), global waste gasification capacity is estimated to be less than 10 000 Megawatts thermal (MWth) compared to more than 200 000 MWth of coal gasification capacity.<sup>580</sup> Despite the low total capacity, the number of global waste gasifiers in operation is estimated to be about 100 facilities which is similar to the number of biomass and natural gas gasifiers.<sup>580</sup> These gasifiers primarily produce electricity and heat.

One of the leaders in gasification of MSW is Enerkem who is currently planning to build four commercial MSW recovery facilities. Enerkem's facility, in Québec, Canada, cost \$680 million and will convert 200 kton per year of MSW and forest residues to 125 million liters of biofuels and chemicals starting in approximately 2023. In Alberta, Canada Enerkem recently commissioned a \$50 million waste-to-biofuel facility with a capacity of 38 million liters per year.<sup>581</sup> In partnership with Shell and the Port of Rotterdam, Enerkem plans to convert about 360 kton per year of MSW to 80 kton of renewable products including aviation fuels. Finally, Enerkem, Agbar, and Repsol plan to build a facility processing 400 kton per year to 220 million liters per year of fuels in Tarragona, Spain pending final investment decisions.<sup>582</sup>

### 7.4 Techno-economic analysis

The profitability of waste plastic gasification facilities depends on several process factors and market drivers. Feedstock composition, process yields, and energy efficiency are key drivers for process performance. Feedstock tipping fees, capital costs, and market prices have a significant impact on profitability. Several studies show that waste plastic gasification is more profitable than conventional waste management practices such as incineration and landfilling.<sup>58,583,584</sup>

There are numerous techno-economic analysis studies on MSW gasification, but only a small subset focuses on waste plastic upgrading. For this review, we identified three comparative analyses that investigate the costs of waste plastic gasification as a primary strategy. Table 16 shows a summary of the key assumptions and findings from these studies.

Voss *et al.* compared the economic performance of chemical recycling and gasification to incineration as municipal waste treatment options in Germany.<sup>583</sup> In their study, they assumed that their feedstock consists of “not differentiable mixed municipal waste” and “household waste, household-type commercial waste” as defined by the European Waste Classification System.<sup>585</sup> Their MSW stream contains 6.9 wt% plastics. Most of Germany's waste streams are incinerated directly *via* combustion to produce heat and power or indirectly *via* anaerobic digestion of the organic fraction and the refuse-derived fuel (RDF) combustion. The chemical recycling scenario assumes that 1 tonne of MSW is initially mechanically separated into the organic fraction (750 kg) and RDF (250 kg). The organic fraction undergoes anaerobic digestion followed by a biogas-powered combined heat and power system. The RDF fraction is gasified to produce syngas, and the syngas is catalytically upgraded to methanol and subsequently to olefins using sodium hydroxide as the catalyst. Hydrocarbons including propylene (32 kg), ethylene (30 kg), butadiene (4.2 kg), LPG (4.0 kg), and butane (1.9 kg) are recovered in the recovery stage. The chemical recycling unit has a capital cost of \$176.6 million for a 76 kton per year facility. Under the basic scenario, this technology is not profitable. It yields a net present value of −\$180.8 million *versus* \$8927 million for direct incineration. A combination of increasing the plant scale, environmental regulations, and favorable market conditions increases the net present value to \$497.2 million.

Gregorio and Zaccariello investigated the economic performance of gasifying packaging-derived fuel (PDF) to produce power, heat and power, and district heating in Italy. PDF is a mixture of primarily plastic-derived materials. Their samples contained 53.9 wt% carbon, 7.7 wt% hydrogen, and 26.0 wt% oxygen. The material contains 0.1 wt% sulfur and 0.3 wt% chlorine, among other contaminants. The nominal capacity (4 kton per year) for the plant was 500 kilowatt-electric (kWe). Total plant costs ranged from \$5500 for the power system to \$8400 for the district heating scenario. The revenue generated from the three scenarios analyzed includes a tariff of \$0.07 per kWe delivered to the grid and \$0.09 per kWe for the sale of saturated or superheated steam production in the combined heat and power plant. Based on the revenues, the internal rate of return was estimated at 0.5% for power generation, 18.9% for district heating, and 29.8% for combined heat and power generation.<sup>584</sup>

**Table 16** Summary of techno-economic analysis estimates for waste plastic gasification

Technology	Feedstock	Major products	Region	Feed capacity (kton per year)	Capital cost (\$ million)	IRR (%)	Ref.
Chemical recycling + gasification + catalytic upgrading	MSW	Propylene, ethylene, LPG, others	Germany	76	158.2–271.2	Not reported	583
Bubbling fluidized bed gasifier	Package derived fuel	Syngas, electricity	Italy	4	0.00549–0.00841/kWe	0.5–29.8	584
Gasification to hydrocarbons	Waste polypropylene	Propylene, ethylene, aromatics	United States	100	49.09 (annualized)	16.91	58



Bora, Wang, and You compared plastic gasification to other recycling strategies. In their study, the gasifier processes plastic waste containing 84.5 wt% carbon, 13 wt% hydrogen, and 2.5 wt% oxygen. The gasification facility has a plant capacity of 100 kton per year, and an annualized capital cost of \$49.1 million. They estimated a 16.91% internal rate of return from the sale of synthetic gases.<sup>58</sup>

## 8. Dissolution-based approaches for plastics recycling

Dissolution-based approaches are methods to use solvents to separate and recycle plastics without chemically modifying their structures. The basic workflow of a dissolution-based polymer recycling process can be described as follows: first, the target polymer is selectively dissolved in a suitable solvent or solvent mixture at a defined temperature; second, the mixture is filtered to separate the solid plastic and the liquid phase that contains the solvated polymer; last, the polymer precipitates from the solution by adding an antisolvent (*i.e.*, a solvent in which the polymer is insoluble) and/or decreasing the temperature. Dissolution-based polymer recycling has several advantages over chemical or mechanical recycling methods: it produces high-quality polymers by removing impurities and additives, it can deal with multicomponent plastic mixtures by selectively dissolving a single target polymer; it does not require a high-purity input stream, and it is typically more environmentally friendly than chemical recycling.<sup>586–588</sup>

### 8.1 Thermodynamics of selective dissolution and solvent screening

The key to a dissolution-based polymer recycling process is the selection of appropriate solvents. In a selective dissolution process, the solvent should dissolve the target polymer with a sufficient solubility without dissolving other unwanted components of the input stream. Since each polymer presents unique interactions that dictate solubility, and the composition of plastic waste is often complicated, theoretical approaches are valuable for systematically identifying suitable solvents. The thermodynamics of polymer-solvent mixing is governed by the free energy of mixing (eqn (12)),<sup>589</sup> where  $\Delta G_{\text{mix}}$  is the molar Gibbs free energy of mixing,  $\Delta H_{\text{mix}}$  is the molar enthalpy of mixing,  $T$  is temperature, and  $\Delta S_{\text{mix}}$  is the molar entropy of mixing. A polymer will favorably mix with a solvent if  $\Delta G_{\text{mix}}$  is negative.

$$\Delta G_{\text{mix}} = \Delta H_{\text{mix}} - T\Delta S_{\text{mix}} \quad (12)$$

Key contributions to the Gibbs free energy of mixing can be understood using Flory–Huggins theory, a mean-field model for polymer solutions (eqn (13)),<sup>590</sup> where  $k_{\text{B}}$  is the Boltzmann constant,  $\phi$  is the volume fraction of the polymer,  $N$  is the degree of polymerization, and  $\chi$  is the Flory interaction parameter that characterizes interactions in the mixture.

$$\Delta G_{\text{mix}} = k_{\text{B}}T \left[ \frac{\phi}{N} \ln \phi + (1 - \phi) \ln(1 - \phi) + \chi \phi(1 - \phi) \right] \quad (13)$$

The  $\chi$  parameter is the critical parameter that governs how favorable a solvent system is for a selected polymer; smaller values promote mixing. The  $\chi$  parameter can be estimated by eqn (14), where  $v_0$  is the molar volume of a monomer and  $\delta_i$  is the Hildebrand solubility parameter of compound  $i$ , which is defined as the square root of the cohesive energy density. A polymer is expected to interact more favorably – and exhibit a higher solubility – in a solvent with a similar solubility parameter, reflecting the general axiom of “like dissolves like”. This conceptual framework thus highlights polymer- and solvent-specific solubility parameters as critical to the design of dissolution-based processes.

$$\chi = \frac{v_0}{k_{\text{B}}T} (\delta_{\text{polymer}} - \delta_{\text{solvent}})^2. \quad (14)$$

### 8.2 Origin of polymer dissolution and precipitation processes

The simplicity and relevancy of dissolution/precipitation for the separation and purification of polymeric materials has been demonstrated experimentally and disclosed in patents since the 1930s. For example, the dissolution and purification of condensation products, mainly polyesters, in ethyl alcohol was disclosed in a 1936 patent by Sändig.<sup>591</sup> In 1949, Young and Sparks of the Standard Oil Development Company patented a method to purify polyesters *via* the solvent-mediated separation of high-molecular weight compounds using paraffinic mineral oils.<sup>592</sup> These approaches showed the feasibility of using solvents to dissolve and purify polymerization products, giving way to the idea that this could be used to separate dissimilar polymers. In the 1970s, Seymour and Stahl demonstrated the separation of PE, PVC, PS, polyvinyl acetate (PVAC), and polymethyl methacrylate (PMMA) using a series of solvents that included toluene, methanol, and petroleum ether.<sup>593</sup> Around the same time, companies like DuPont filed patents for the recovery of solid scrap thermoplastic polymers like PET, pol(hexamethylene adipamide), poly(acrylonitrile), and poly(oxyethylene) by dissolving them in hexafluoroisopropanol.<sup>594</sup> In 1977, Monsanto patented a process for recovering solid PET, poly(cyclohexanedimethanol terephthalate), and poly(butylene terephthalate) from fibers using naphthalene as a selective solvent and dimethylformamide (DMF), water, and acetone as quenching mediums (antisolvent).<sup>595</sup>

### 8.3 Applications of dissolution-based plastic recycling

Building upon these early materials recovery and purification processes, applications of dissolution and precipitation to plastic recycling has gained interest along the years. Nauman *et al.* proposed an approach to separate plastics in physically comingled solid mixtures by selective dissolution. Single solvents were used to dissolve plastics like PS, PVC, LDPE, HDPE, and PP, at different temperatures and pressures.<sup>596,597</sup> The



process consisted of shredding the comingled solids, dissolution of the plastic, filtration, flash devolatilization, and pelletization of the separated plastic. Model experiments of plastic recycling with the dissolution/precipitation method were performed by Kampouris, Papaspyrides, and collaborators to recover PVC, LDPE, PP and PS.<sup>598–602</sup> In one study, Pappa *et al.* designed a pilot unit for the separation of LDPE/PP mixtures using the dissolution/precipitation method with xylene and 1-propanol as solvent and antisolvent, respectively. They claimed that the costs of the plastics produced from the process were comparable to those of the virgin plastics.<sup>603</sup> Regarding the impact of solvent treatment to the plastic properties, early recycling experiments with LDPE, HDPE, PET and PP showed that applying these processes once or twice did not affect the rheological, thermal, or mechanical properties of the final plastic.<sup>587,598,602,604</sup> Many of these reports established solvent/antisolvent systems for common plastics, including solvent combinations, as summarized in Table 17.

Recent and ongoing research efforts have developed dissolution/precipitation methods for increasingly complex sources of plastic waste. Researchers at the Illinois Sustainable Technology Center have developed a nontoxic energy-efficient

chemical solvent process to recover plastics from blends of electronic waste that are converted to fuel oil by pyrolysis. The process has been demonstrated at the lab scale and can produce plastics with properties similar to virgin resins and will begin a pilot-scale project depending on the performance of the recovered plastics.<sup>605–607</sup> Recently, Georgiopolou *et al.*<sup>608</sup> demonstrated a process to recycle Tetra Pak® packaging materials composed of LDPE, paperboard, and aluminum. Their approach included a hydropulping process to recycle the paper component and a dissolution/precipitation process to recover LDPE, using xylene and *i*-propanol as the solvent/antisolvent pair. Researchers at the Center for the Chemical Upcycling of Waste Plastics at the University of Wisconsin–Madison have developed a solvent-based method called Solvent-Targeted Recovery and Precipitation (STRAP) that has been demonstrated for the recycling of different post-industrial multilayer films composed of PE, EVOH, PET and EVA.<sup>609,610</sup> STRAP combines experiments, computational modeling, and process design tools to develop solvent systems to recycle multilayer plastics *via* selective dissolution. A technoeconomic analysis showed that STRAP can produce plastics at costs similar to virgin resins and can be more economically

**Table 17** Solvents/antisolvents used experimentally for the dissolution/precipitation of common plastics

Polymer	Solvent	Antisolvent	Ref.
PVC	Cyclohexanone	<i>n</i> -Hexane	601
PVC	Dichloromethane	Methanol	611
PVC	Toluene	Methanol	611
PVC	Tetrahydrofuran (THF), xylene	—	596
PS	Methyl ethyl ketone (MEK)	Methanol, <i>n</i> -hexane	599
PS	<i>p</i> -Xylene	<i>n</i> -Pentane	599
PS	Benzene, toluene	Water	600
PS	Toluene	<i>n</i> -Hexane	611
PS	Xylene	Methanol	611
PS	THF, toluene, xylene	—	596
PS	<i>p</i> -Cymene	—	612
EPS	<i>n</i> -Limonene	—	611
HDPE	Xylene	<i>n</i> -Hexane, methanol	611
HDPE	THF, toluene, xylene	—	596
HDPE, LDPE, PP	Turpentine	<i>n</i> -Hexane, petroleum ether (PetE)	613 and 614
HDPE, LDPE, PP	Turpentine/PetE	<i>n</i> -Hexane, PetE	613 and 614
HDPE, LDPE, PP	Turpentine/benzene	<i>n</i> -Hexane, PetE	613 and 614
LDPE	Xylene	<i>n</i> -Hexane	611
LDPE	THF, toluene, xylene	—	596
PE, PP, PS	<i>n</i> -Butane, propane	—	615
PP	Xylene	<i>n</i> -Hexane	611
PP	Tetrachloroethylene	—	616
PP	THF, toluene, xylene	—	596
PET	THF	—	596
PET	$\gamma$ -Valerolactone (GVL)	—	617
PET	<i>N</i> -Methyl-2-pyrrolidone (NMP)	<i>n</i> -Octane, <i>n</i> -hexane	604
PET	Diphenyl, diphenyl ether, naphthalene, methylnaphthalene, benzophenone, diphenylmethane	—	618
PET	Benzyl alcohol	Methanol	611
PC	Dichloromethane	Acetone	619
PA 6	Dimethyl sulfoxide (DMSO)	MEK	620
PA 6,6	Formic acid	MEK	620



feasible when the use of antisolvents is reduced by instead inducing precipitation *via* temperature.<sup>609</sup>

Other than targeting specific plastic components in plastic waste, solvents can also be used to extract additives from plastics or to selectively dissolve or decompose adhesives in plastic structures to trigger delamination. While these topics are out of the scope of this discussion, they have been discussed at length in recent publications.<sup>621–624</sup>

#### 8.4 Industrial demonstrations of dissolution/precipitation processes

A handful of technologies are being commercialized for the recycling of different plastic waste feeds *via* dissolution methods. Here, we focus primarily on technologies that are currently in the process of commercialization. We omit discussion of past efforts; for example, the Solvay VinylLoop process was developed to separate PVC from a polymer coating using a selective dissolution step in a proprietary solvent,<sup>625</sup> but the process ceased operations in 2018.

APK AG's NewCycling process is being demonstrated in a 8000 ton per year plant in Germany to produce polyamides (PA) and PE from PIW multilayer plastics.<sup>626–628</sup> Their technology is based on dissolving a plastic using a solvent mixture from a group of alkanes, isooctane or cycloalkanes.<sup>629</sup> The plastics are recovered from solution and then pelletized by extrusion.<sup>626,627</sup> Centrifuges separate the solids from the plastic solution and solvent.<sup>630</sup> APK AG claims that PP, PET, PS, PLA and aluminum could also be recovered with this process in the future.<sup>627</sup>

The Fraunhofer Institute is developing a solvent-based process called CreaSolv that produces plastics with comparable properties to virgin materials, effectively removing contaminants and additives.<sup>631</sup> The process is likely based on the dissolution of a target plastic, mainly polyolefins, using a solvent with a Hansen parameter  $\delta_H$  between 0.0 to 3.0 MPa<sup>1/2</sup>, selected from a group of aliphatic hydrocarbons. An antisolvent made out of mono/polyhydroxy hydrocarbons, like 1-propanol or 1,3-propanediol, with a  $\delta_H$  between 4.0 and 38.0 MPa<sup>1/2</sup> is then used to precipitate the polyolefin from the mixture.<sup>632</sup> The institute has also studied the separation of PS<sup>633</sup> and is researching the recycling of multilayer food packaging that can consist of PET, PE, PP, EVOH, PA and metalized layers.<sup>634</sup> Currently, Unilever is implementing the CreaSolv process in a 1100 ton per year demonstration plant in Indonesia to recover PE from multilayer sachets.<sup>635,636</sup> CreaSolv is also reported to have a demonstration plant in Holland to separate EPS from POP, a pilot plant for recycling packaging and automotive compounds, and a demonstration plant in Germany for multilayer films.<sup>637</sup>

PureCycle Technologies is building a 54 000 ton per year facility that uses solvents to produce PP from PIW and PCW in collaboration with P&G.<sup>638,639</sup> The method consists of contacting the plastic waste with an alkane at elevated temperatures and pressures to obtain the purified PP.<sup>640</sup> The process removes impurities, undesired colors and odors and produces PP with comparable properties to the virgin resin.<sup>639</sup> P&G has

recently filed patents with methods to separate and purify adhesives, PP, PE, PET, cellulose, and polyacrylic acid (PAA).<sup>641</sup> The company also has inventions in the purification of PE using a pressurized solvent consisting of hydrocarbons, primarily *n*-butane or pentane.<sup>642</sup> Additionally, they have a process for the separation of PS, PP, PE and poly(dimethylsiloxane) under similar conditions.<sup>615</sup>

Polystyvert developed a dissolution process to recycle different types of PS, including expanded PS, extruded PS and high-impact PS. Polystyvert operates at 125 kg per hour with an output of 600 metric tons per year.<sup>605</sup> In their technology *p*-cymene is used as a selective solvent for PS and a non-polar solvent is used as an antisolvent to precipitate the plastic and remove *p*-cymene.<sup>612</sup> Through this approach they can separate and recover PS from other materials, as only PS dissolves in the solvent and other materials float or sink in the system.<sup>643</sup>

Dissolution-based recycling processes have also been applied to textile waste. For example, Worn Again Technologies has patented a technology to recycle PET into pellets. In their process, the polyesters are dissolved in a solvent system with either benzyl acetate, benzyl benzoate, benzaldehyde, or similar solvents, precipitated by cooling of the solvent system, and then separated *via* filtration. After the plastic is separated, it is washed and dried and then molded into pellets and/or converted into fibers.<sup>644</sup> This process can be applied to cotton textiles, post-consumer PET bottles, and plastic packaging containing PET. Worn Again has also partnered with companies such as H&M and Kering to promote the reduction of textile waste.<sup>645</sup> Another start-up company, Ambercycle, has developed a technology to purify and separate polyesters from different garments and is planning a demonstration plant to produce a metric ton of recycled material per day.<sup>646,647</sup>

Other approaches are being used to recycle multilayer plastics using a combination of mechanical and solvent-mediated steps. For example, Saperatec has introduced a low-energy mechanical recycling process that involves shredding the multilayer film followed by use of surfactant-containing micro-emulsions to break up and separate the layers.<sup>648</sup> The technology separates PE and aluminum film, PP from aluminum, and PE from PP. The technology was originally developed for rigid packaging and is being extended to flexible packaging and will be demonstrated at a 17 000 ton per year facility in Germany.<sup>649</sup>

#### 8.5 Advanced solvent selection for complicated feedstocks

As presented above, several solvents and antisolvents have already been identified for many common plastics, enabling the development of dissolution/precipitation processes for single plastics by selecting solvents from past literature.<sup>588,650,651</sup> However, an ongoing challenge is solvent selection for plastic mixtures which are ubiquitous in realistic plastic waste. Multicomponent polymeric materials are often made from two or more plastics, each of which is selected to contribute its own useful properties.<sup>652</sup> For example, food packaging boxes are typically multilayer plastic films, which are extremely challenging to recycle because of their complex



compositions and the incompatibility of different polymer layers.<sup>610</sup> Dissolution-based methods are promising for recycling such materials because selective dissolution enables the separation of different plastics and is tolerant to the additives and impurities present in waste. However, due to the variety of possible plastic combinations, as well as the necessity for choosing appropriate operating temperatures for dissolution and precipitation, solvent selection for plastic mixtures is a difficult task.

Based on the thermodynamic framework described above, one method for solvent selection is to compute solubility parameters for target plastics and solvents to predict dissolution. Hildebrand solubility parameters can be applied with reasonable accuracy to predict solubility in systems dominated by non-polar interactions, but are inaccurate for mixtures with strong polar or specific interactions such as hydrogen bonds.<sup>590,653</sup> Similar to the Hildebrand solubility parameter, other parameter sets have been applied to identify solvents and antisolvents for plastics; examples include Hansen,<sup>654</sup> Kamlet-Taft,<sup>655</sup> Gutmann,<sup>656</sup> and Swain<sup>657</sup> parameters. These parameters assess the chemical similarity between species to predict dissolution behaviors.<sup>651</sup> Among them, Hansen solubility parameters (HSP) are the most widely used to select solvents for plastic dissolution.<sup>588,651,658</sup> The HSP system assigns each compound three parameters that account for dispersion ( $\delta_D$ ), polar ( $\delta_P$ ), and hydrogen-bonding ( $\delta_H$ ) interactions. Solvent-polymer interactions are measured by their distance  $R_a$  in the 3-dimensional HSP space ( $2\delta_D - \delta_P - \delta_H$  space) as shown in eqn (15).

$$R_a^2 = 4\left(\delta_D^{\text{solvent}} - \delta_D^{\text{polymer}}\right)^2 + \left(\delta_P^{\text{solvent}} - \delta_P^{\text{polymer}}\right)^2 + \left(\delta_H^{\text{solvent}} - \delta_H^{\text{polymer}}\right)^2 \quad (15)$$

Each polymer has an additional radius parameter,  $R_0$ , that defines a sphere in the HSP space. Solvents within this sphere ( $R_a/R_0 < 1$ ) are expected to dissolve the polymer, whereas solvents outside of this sphere ( $R_a/R_0 > 1$ ) are not expected to dissolve the polymer. Tabulated HSP and  $R_0$  values are available for a large number of polymers and solvents based largely on empirical data and have been used in many successful applications of solvent screening.<sup>658,659</sup>

Building upon the success of these solubility parameter methods, newer computational approaches for predicting polymer solubilities and screening solvents with minimal experimental effort have emerged in recent years. A recent example was the development of machine learning techniques for the large-scale binary classification of solvents and antisolvents for polymers, thus categorizing solvents into similar categories as HSPs. Specifically, Chandrasekaran *et al.*<sup>660</sup> developed a deep neural network to classify 24 common solvents for over 4500 homopolymers with an accuracy of 93.8%. This example demonstrates the feasibility of applying data-centric methods to rapidly screen potential polymer-solvent combinations for selective dissolution processes, although more data will be required to extend the solvent library.

The preceding techniques primarily focus on qualitatively classifying solvents and antisolvents for target polymers. However, the development of dissolution/precipitation processes requires quantitative analysis of solubilities as a function of temperature in order to assess the feasibility and economics of potential industrial-scale processes. To address this challenge, Zhou *et al.* developed a computational approach for quantitatively predicting temperature-dependent polymer solubilities using molecular-scale models.<sup>661</sup> This approach employs molecular dynamics simulations to sample polymer conformations in representative solvents. These conformations are used as input to the CONductor-like Screening MODEL for Real Solvents (COSMO-RS), a model that used quantum mechanical calculations and statistical thermodynamics methods to predict polymer solubilities through solid-liquid equilibrium calculations.<sup>610,661</sup> After initial polymer conformations are available, temperature-dependent solubilities can be obtained rapidly (~minutes). This approach was applied to screen over 500 solvent combinations for the selective dissolution of PE and EVOH and extended to develop a STRAP process for a commercial multilayer film with four polymer components.<sup>609,610,661</sup>

## 8.6 Techno-economic analysis of STRAP

A published techno-economic analysis of the STRAP process has demonstrated that plastics recovered *via* this technology can be sold at prices that are comparable to virgin resins.<sup>610</sup> Due to STRAP being a new technology, the size of the process required to achieve a competitive sell price is important, as large capital costs can make scaling up to an industrial level difficult. At a feed rate of 3000 tonnes per year, plastic recycled by the STRAP process can be sold at a minimum selling price (MSP) of \$2.18 per kg, while delivering a discounted return on investment (DROI) of 10% to investors over a 20 year lifetime. The MSP can be further reduced through optimization of STRAP design parameters, as shown in Fig. 25.<sup>609</sup>

A key feature that drives economic performance is solvent selection. A solvent with a high affinity for a target polymer can decrease the dissolution time and solvent/polymer ratio which can in turn decrease the filter equipment cost by reducing its size. A low-boiling solvent/antisolvent pair with a high relative volatility or solvent that allows for temperature-controlled precipitation can reduce the size of or eliminate the need for distillation columns.<sup>609</sup> Using less solvent, an easily separable solvent/antisolvent system, or eliminating the need for an antisolvent then reduces the quality and quantity of steam required. This illustrates that efficient solvent screening and selection is essential for establishing economic as well as technical feasibility of STRAP.

Fig. 26 shows that STRAP is far from the point of diminishing returns at a processing capacity of 3000 tonnes per year. These data indicate that there will be a significant economic incentive to scale STRAP up to larger sizes if the process is shown to be effective at smaller processing capacities. At a feed rate of 15 000 tonnes per year, the recycled plastic could be sold for \$0.95 per kg to achieve a DROI of 10% or deliver a



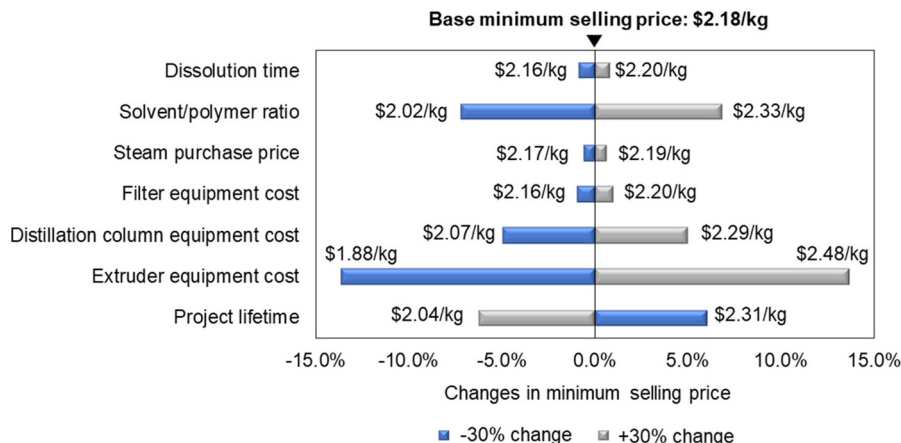


Fig. 25 Sensitivity analysis of MSP for the STRAP process. Reproduced from ref. 609 with permission from Wiley-VCH, copyright 2021.

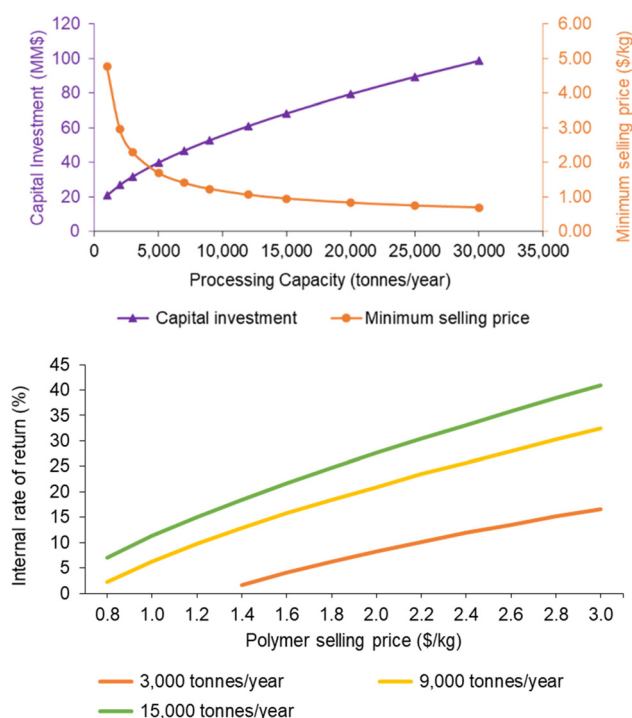


Fig. 26 Capital investment and MSP for the STRAP process as a function of feed capacity (top) and DROI as a function of MSP at three different feed capacities (bottom) Reproduced from ref. 609 with permission from Wiley-VCH, copyright 2021.

DROI of approximately 30% if the selling price of \$2.18 per kg is maintained while requiring about twice as much capital investment.<sup>610</sup> This analysis demonstrates that the process has significant economic potential and can be made even more competitive *via* process optimization and solvent selection. More broadly, this analysis, along with the commercial demonstrations described previously, supports the economic viability of dissolution-based recycling techniques.

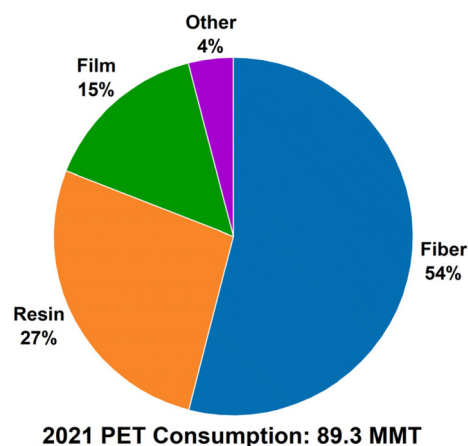


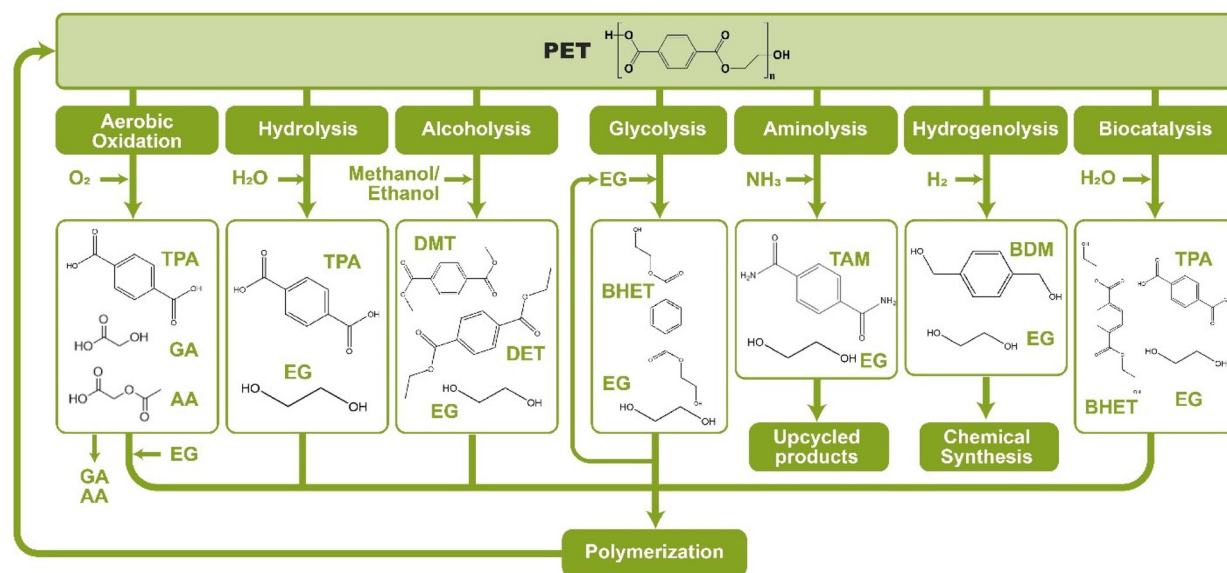
Fig. 27 Global PET consumption in 2021.

## 9. Chemical recycling of polyester to monomers

### 9.1 Chemical recycling of PET

The commercial uses of PET span a wide variety of industrial sectors, from fiber for textiles to resin for beverage bottles. In 2021, global PET consumption totaled 89.3 million metric tons (MMT) (Fig. 27). It is the fourth most consumed plastic in the world after PE, PP, and PVC.<sup>14,662,663</sup> There are many reviews in the literature summarizing recent progress in chemical plastics recycling, as well as several which focus solely on PET.<sup>17,281,663–674</sup> Chemical recycling of PET is an area of intense focus in the literature, and a comprehensive review of every report in this field is thus not attempted here. This section summarizes each strategy for PET depolymerization, with a focus on important and practical advances and their potential for industrial application. This review is organized into sections based on the approach to PET depolymerization:





**Fig. 28** Strategies for PET chemical recycling discussed in this section, and their most common products. (TPA = terephthalic acid, EG = ethylene glycol, DMT = dimethylterephthalate, DET = diethylterephthalate, BHET = bis-2-hydroxyethylterephthalate, BDM = benzenedimethanol, MHET = mono-2-hydroxyethylterephthalate.).

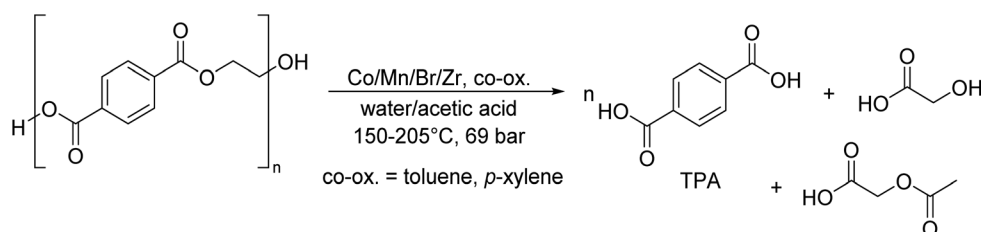
aerobic oxidation, hydrolysis, alcoholysis, glycolysis, aminolysis, hydrogenolysis, and enzymatic depolymerization (Fig. 28). Current commercial activity in chemical PET depolymerization is included at the end of this section, along with comments on the economics of these processes.

**9.1.1 Aerobic oxidation.** Aerobic oxidation of PET involves heating the polymer to high temperatures in the presence of oxygen, and sometimes a catalyst or promoter. In 1984, Jabarin and Lofgren<sup>675</sup> studied the thermal oxidation of PET and showed that it was an exothermic reaction with an activation energy lower than the thermal decomposition of PET under vacuum. At all temperatures and drying conditions studied, increased decomposition of PET was observed under air as compared to under nitrogen. However, specific products of the reaction were not identified and PET degradation was measured only by the weight loss of the sample.

Partenheimer<sup>676</sup> received a patent in 2005 for the oxidation of a wide variety of polymers using a range of simple metal salt promoters. PET sourced from blue film, recycled resin, and shirts were depolymerized as 4–20 wt% solutions in acetic acid under 1000 psia air pressure at 150–205 °C. A combi-

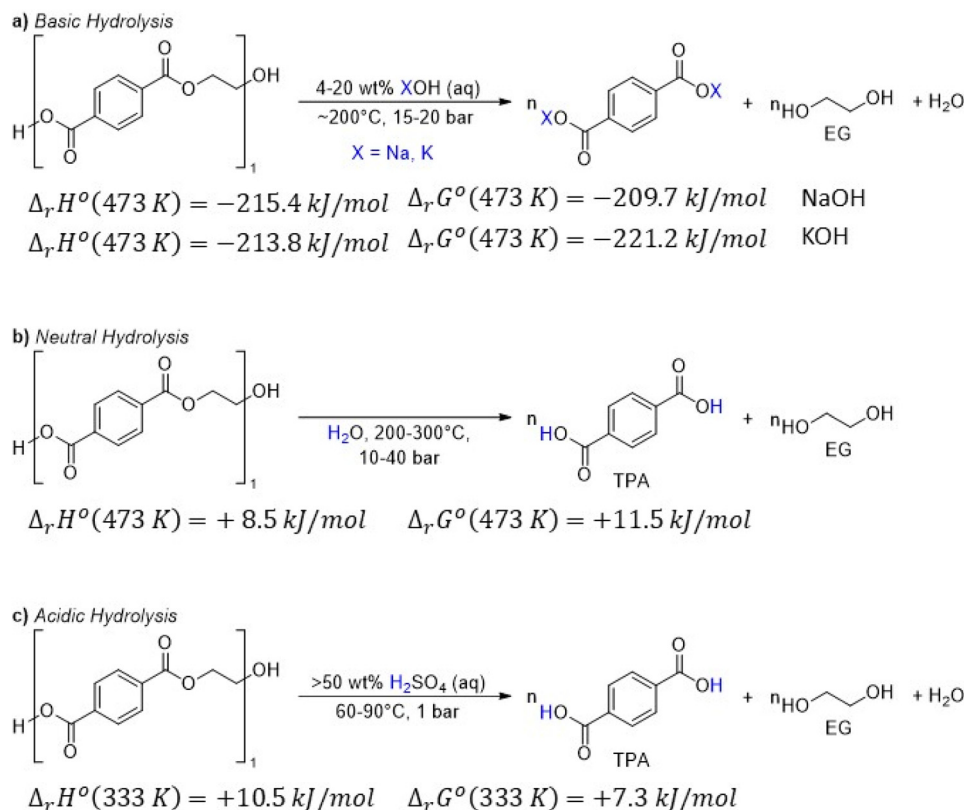
nation of Co/Mn/Br/Zr in varying ratios was used as a catalyst, and the effect of adding co-oxidants such as toluene and *p*-xylene was also investigated (Fig. 29). TPA yields of up to 100% were reached, and more efficient conversion was observed at higher temperatures, longer reaction times, higher initial PET concentrations, and in the presence of either co-oxidant. Partenheimer further published that a 56% yield of TPA could be isolated from the oxidation of PET at 190 °C in a water/acetic acid mixture using a similar Co/Mn/Br/Zr catalyst. The TPA yield increased to 100% in the presence of toluene as a co-oxidant.<sup>677</sup> This chemistry was based on an extensive review published by Partenheimer about a decade earlier on metal/bromide autoxidation of hydrocarbons.<sup>678</sup>

**9.1.2 Hydrolysis.** Hydrolytic PET depolymerization involves the reaction of the polymer in either a basic, neutral, or acidic aqueous solution. The products of PET hydrolysis are TPA and EG. One major disadvantage of hydrolysis is the large volumes of inorganic salt and aqueous waste that are generated, along with the high corrosivity of the basic and acidic systems. It has been estimated that, on an industrial scale, 20–50 L of aqueous solution would be required to hydrolyze 1 kg of post-



**Fig. 29** Typical reaction conditions and products for PET aerobic oxidation.





**Fig. 30** Typical reaction conditions and products for uncatalyzed PET (a) basic, (b) neutral, and (c) acidic hydrolysis. Calculations of enthalpy and Gibbs free energy were performed in the presence of solvent [polarizable continuum model (PCM)]. Exchange-correlation functional: B3LYP. Basis set: 6-31++g(d,p). Neutral and basic environments  $\text{H}_2\text{O}$  is the solvent – at small concentration of NaOH/KOH reactant and product species will mainly interact with  $\text{H}_2\text{O}$  molecules. Acidic environment was simulated by setting the refractive index equal to 1.3945, which corresponds to 50 wt% sulfuric acid; the result is not very sensitive to the value of dielectric constant and the one for  $\text{H}_2\text{O}$  was used (i.e., 78).

consumer PET, generating 5 kg of inorganic salt waste.<sup>679</sup> However, it is also more tolerant of post-consumer waste contaminants and other polymers than many chemical recycling strategies. Several studies are included in this section that utilize post-consumer PET sources.<sup>668,680</sup>

**9.1.2.1 Basic hydrolysis.** Basic hydrolysis is typically carried out in a 4–20 wt% solution of NaOH or KOH in water. Reaction temperatures average around 200 °C and pressures are usually 15–20 bar (Fig. 30a). The disodium or dipotassium terephthalate product must be protonated with acid after the reaction, generating stoichiometric inorganic salt waste.<sup>681</sup> LCA performed on this reaction demonstrated that decreasing the volume of water required for product purification is critical to achieve lower GHG emissions for this recycling process compared to PET incineration.<sup>679</sup> Yoshioka and coworkers evaluated a system in which PET was hydrolyzed in concentrated NaOH at 250 °C and 5 MPa  $\text{O}_2$  pressure for 5 hours. The disodium terephthalate was not oxidized under these conditions and was obtained in quantitative yields. However, EG was oxidized to oxalic acid in roughly 70% yield, generating a value-added product that could be sold to further improve the economics of this recycling strategy.<sup>682</sup>

A phase transfer catalyst such as a quaternary ammonium salt can be used to lower the temperatures and pressures

required for alkaline hydrolysis. Kosmidis and coworkers<sup>683</sup> used this strategy to isolate TPA at high purity using aqueous NaOH and catalytic trioctylmethylammonium bromide to depolymerize post-consumer PET soda bottles under atmospheric pressure and at temperatures as low as 70 °C. Similarly, microwave irradiation has been used to lower the required temperature of basic PET hydrolysis.<sup>684</sup> Khalaf and Hasan<sup>685</sup> isolated TPA from post-consumer soda bottles in almost quantitative yields after only 1 hour of irradiation in the presence of tetrabutylammonium iodide as a phase transfer catalyst. The catalyst could be recovered from the reaction mixture after product extraction, which improves the potential practicality of this method.

Hu *et al.*<sup>686</sup> found that using a mixed solvent system of an ether and an alcohol enabled complete depolymerization of PET with NaOH in 40 minutes at only 60 °C. Pure TPA and EG were easily isolated from the reaction mixture. In 2017, Essaddam<sup>687</sup> received a patent for the room temperature hydrolysis of PET. The system consisted of a nonpolar solvent such as  $\text{CH}_2\text{Cl}_2$ , which swelled the polymer, and an alcoholic solution of NaOH to hydrolyze the PET. High purity TPA could be isolated using this method in up to quantitative yields. Ügdüler and coworkers<sup>679</sup> used ethanol as a cosolvent in the



alkaline hydrolysis of PET to achieve 95% TPA yield in only 20 minutes at 80 °C. When post-consumer multilayer PET/PE trays were used as a substrate, yields were lower but still reached 45%.

**9.1.2.2 Neutral hydrolysis.** Neutral hydrolysis is in many ways preferable to basic or acidic strategies, as the solution will not require specialized reactor materials to prevent corrosion and stoichiometric salts are not required or formed in the reaction. However, this also means that impurities and additives present in the PET remain in the recycled monomer, which is not the case in TPA generated from acidic and basic hydrolysis.<sup>680,681</sup> Additionally, high temperatures and pressures are required for the reaction to run at an appreciable rate. The temperatures used are 200–300 °C, and often in the upper half of this range so the reaction runs in the melt phase of PET. Pressures of 10–40 bar are typically used, along with a large excess of water or steam (Fig. 30b). The large volume of water required leads to very dilute solutions of EG in the product mixture, which makes isolation more difficult and costly. The reaction proceeds in about 1 hour at 275 °C, and it has been proposed that the TPA formed in the reaction can catalyze the hydrolysis, rendering the reaction autocatalytic.<sup>681,688</sup>

Campanelli and coworkers<sup>689</sup> investigated possible catalytic effects in the neutral hydrolysis of PET but found that zinc salts exhibit only a minute accelerating effect on the reaction. Full conversions were only reached at temperatures above 250 °C. Xylene was utilized as a cosolvent in neutral hydrolysis, which reduced the required temperature, pressure, and volume of water in the reaction. Additionally, this strategy enabled the efficient isolation of EG as a concentrated solution in the organic layer.<sup>690</sup>

Zhang *et al.*<sup>691</sup> used a dual phase-transfer catalyst  $[(CH_3)_3N(C_{16}H_{33})]_3[PW_{12}O_{40}]$  in the neutral hydrolysis of post-consumer bottle PET at 145 °C for 3 hours to obtain TPA yields of up to 93%. The catalyst allowed the reaction to be run at much lower temperatures and could be separated from the products and recycled at least three times without any observed decrease in efficiency. Stanica-Ezeanu and Matei<sup>692</sup> found marine water to be an excellent solvent for neutral PET hydrolysis due to the presence of various metal ions that can act as catalysts. They used simple salts commonly found in the ocean, including NaCl, KHCO<sub>3</sub>, and CaCl<sub>2</sub>, as catalysts in the depolymerization of PET at 200 °C and 40 bar to obtain TPA in up to 85% isolated yield. Yields were increased at milder conditions when

more than one salt was added or when marine water was used as a catalyst.

**9.1.2.3 Acidic hydrolysis.** Several systems have been described for the acidic hydrolysis of PET in concentrated (>50 wt%) H<sub>2</sub>SO<sub>4</sub> solutions to generate high purity TPA in high yields at ambient pressures and relatively low temperatures (Fig. 30c). However, these reactions are highly impractical at scale due to the corrosivity of the solution, the need to recycle large volumes of acid, the generation of stoichiometric salt waste, and the difficulty in isolating EG from the reaction.<sup>672,681,693</sup> Yoshioka and coworkers<sup>694</sup> discovered that they could decrease the H<sub>2</sub>SO<sub>4</sub> concentration by about half and still achieve complete hydrolysis of PET to TPA in 5 hours at 150 °C. The acid was subsequently recovered by dialysis. The same group also reported that 7–13 M HNO<sub>3</sub> completely hydrolyzed PET over about 2 days at temperatures below 100 °C. The EG was simultaneously oxidized to oxalic acid, a value-added product.<sup>695</sup>

Liu *et al.*<sup>696</sup> studied the hydrolysis of PET using the ionic liquid (IL) 1-butyl-3-methylimidazolium (Bmim) chloride as the solvent and an acid-functionalized IL (1-methyl-3-(3-sulfo-propyl)-imidazolium hydrogen sulfate) as a catalyst. After 4.5 hours at 170 °C, they isolated TPA in 88% yield, and were able to recycle the ILs at least 8 times with no decrease in yield. Yang and coworkers found that TPA itself was an effective catalyst for acidic PET hydrolysis. They achieved a 95.5% yield of high purity TPA after 3 hours at 220 °C. The only workup required was a simple filtration, and the hydrolysis efficiency was maintained over 8 consecutive reaction cycles.<sup>697</sup>

**9.1.3 Alcoholysis.** Alcoholysis depolymerizes PET in the presence of alcohols to form an ester and EG (Fig. 31). Methanol and ethanol are the most common alcohols utilized in this reaction, but other alcohols can also be used.

**9.1.3.1 Methanolysis.** Methanolysis of PET produces dimethylterephthalate (DMT) and EG. DMT can be used directly in transesterification polymerization to form PET or further hydrolyzed to TPA.<sup>672,680,698</sup> However, methanolysis of post-consumer PET leads to high separation and purification costs due to the mixture of glycols, alcohols, and phthalate derivatives produced in the reaction.<sup>663</sup> Methanolysis typically operates at temperatures of 180–280 °C and pressures of 20–40 bar. The high pressures ensure that the methanol remains a liquid during the reaction. Transesterification catalysts such as zinc acetate, magnesium acetate, cobalt acetate, or lead dioxide are

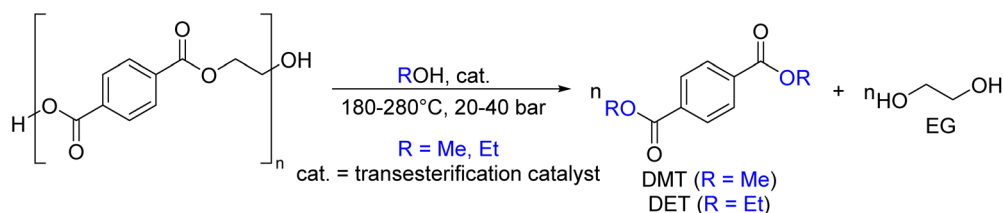


Fig. 31 Typical reaction conditions and products for PET alcoholysis.



typically used, and yields of DMT average 80–85%. This reaction can be run in continuous flow, but complex reactors are required to add feedstocks while maintaining the required high reaction pressures. In a typical continuous method, melted PET and preheated methanol are fed into an autoclave with a set residence time to complete the depolymerization, then the mixture is flowed to the bottom of a second pressurized reactor at a lower temperature so that high density impurities can be removed. After leaving the second autoclave the reaction pressure is reduced, the product mixture is further cooled in a mixer, and finally DMT is isolated by precipitation.<sup>672,680,699</sup>

Sako and coworkers<sup>700</sup> reported in 1997 that PET could be completely depolymerized to DMT, EG, and some oligomers with no catalyst in only 30 minutes in supercritical methanol. This was achieved at temperatures above 300 °C and pressures of 110 bar. Above supercritical conditions, the pressure of the reaction was not found to have a significant effect on DMT yield, however the severe conditions make this process too cost intensive for large scale use and too difficult to adapt to continuous flow.<sup>680</sup>

Kurokawa *et al.*<sup>698</sup> used the transesterification catalyst  $\text{Al}(\text{O}^i\text{Pr})_3$  to promote the methanolysis of PET from soda bottles under more mild conditions. They achieved 88% DMT and 87% EG yields in 4 : 1 methanol : toluene at 200 °C and no added pressure. Improved yields in this solvent mixture compared to pure methanol indicate that the rate of methanolysis strongly depends on PET solubility. Hofmann and coworkers<sup>701</sup> found that microwave irradiation facilitated the methanolysis of PET under even milder conditions using zinc acetate as a catalyst and  $\text{CH}_2\text{Cl}_2$  as a cosolvent to improve solubility. In only 20 minutes at 160 °C, moderate to high yields of DMT were isolated from a variety of post-consumer PET sources, including a dish detergent bottle (46% yield), a soap dispenser with a label (70% yield), and a transparent food container (98% yield).

Pham and Cho<sup>702</sup> reported that the inexpensive salt  $\text{K}_2\text{CO}_3$  catalyzes PET methanolysis at room temperature. A 93% yield of DMT was obtained after 24 hours in a mixed solvent system of 1 : 1 methanol :  $\text{CH}_2\text{Cl}_2$ . Tanaka and coworkers<sup>703</sup> developed a new strategy wherein they trapped the EG formed in the reaction as ethylene carbonate. This biased the depolymerization equilibrium towards the monomers and enabled the reaction to run in only 5 hours at ambient temperature. Various simple alkali salts were used as catalysts, and optimized yields of DMT exceeded 90% using 5 mol%  $\text{LiOMe}$ .

**9.1.3.2 Ethanolysis.** PET ethanolysis yields diethylterephthalate (DET) and EG. The strategy is similar to methanolysis in many ways but could be particularly advantageous

in countries such as Brazil where ethanol from sugarcane is cheap and abundant.<sup>704</sup>

In 2006, it was reported that PET could be completely depolymerized to its monomers in 5 hours in supercritical ethanol. At 528 °C and pressures of 76–116 bar, DET yields of 65–98% were obtained using post-consumer PET from a variety of sources including green bottles, mechanically recycled fiber, and polyester string.<sup>705</sup> Fávoro and coworkers<sup>704</sup> studied the ethanolysis of multilayer food packaging containing PET, PE, and aluminum. The material was depolymerized over 2 hours in supercritical ethanol at 255 °C and 116 bar. High purity DET was obtained in 80% yield after precipitation, and metallic aluminum could also be isolated from the reaction. Lozano-Martinez and coworkers found that the product distribution from PET ethanolysis could be changed by altering the reaction conditions. Long reaction times in supercritical ethanol generated DET as the only product, while shorter reaction times at lower temperatures and pressures led to the formation of TPA.<sup>706</sup>

Nunes *et al.*<sup>707</sup> reported that the addition of catalytic  $[\text{Bmim}][\text{BF}_4]$  reduced the required reaction time for PET depolymerization in supercritical ethanol from 6 hours to only 45 minutes. Cobalt and nickel oxides have also been found to be effective catalysts for PET ethanolysis under supercritical conditions, and provide almost quantitative yields of DET. The required reaction time was only 90 minutes with low catalyst loadings.<sup>708</sup>

**9.1.4 Glycolysis.** Glycolysis is one of the most intensely studied routes for chemical PET depolymerization, and several systems have been commercially adopted. Glycolysis involves the transesterification of PET with excess glycol, most commonly EG, to generate the corresponding ester (bis-2-hydroxyethylterephthalate, BHET, when EG is used) and EG as products (Fig. 32). Many different classes of catalysts have been studied in this reaction.<sup>663,670,709</sup> Without a catalyst, PET glycolysis requires temperatures of 200–240 °C and pressures of 2–6 bar, and high monomer yields are not obtained.<sup>681</sup> In 1991, Chen and coworkers<sup>710</sup> studied the relationship between reaction pressure and EG : PET ratio on depolymerization kinetics. Higher pressures were reported to enable faster reactions, and at higher EG concentrations BHET was in equilibrium with PET oligomers. At lower EG concentrations, no monomer was observed.

Metal acetates were first reported as PET glycolysis catalysts in 1989 and have been widely studied.<sup>709,711,712</sup> Güçlü and coworkers<sup>713</sup> used xylene to form a multiphase reaction in zinc acetate-catalyzed PET glycolysis with EG at temperatures of 170–245 °C. BHET was pulled into the xylene layer to bias the

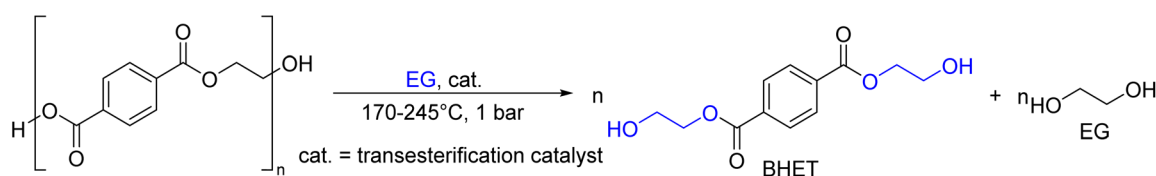


Fig. 32 Typical reaction conditions and products for PET glycolysis with EG.



equilibrium of the depolymerization and prevent oligomer formation, providing monomer in up to 80% yield. Other diols such as butanediol and triethylene glycol have also been used in PET glycolysis with zinc acetate to generate monomers and dimers.<sup>714</sup> Chen found that the optimal PET glycolysis temperature was 190 °C when using manganese acetate as a catalyst. Conversion of PET to BHET and dimer reached ~100% after 1.5 hours.<sup>715</sup> Ghaemy and Mossaddegh<sup>716</sup> used various metal acetate catalysts in the glycolysis of PET in refluxing EG. Yields of BHET reached up to 85% from both fiber and flake PET.

Troev and coworkers<sup>717</sup> demonstrated that light metal salts could also be used as glycolysis catalysts. They reported that titanium(IV) phosphate catalyzes the depolymerization of PET to BHET in up to 97% selectivity at 190 °C with a reaction time of 2.5 hours. Fang *et al.*<sup>718</sup> utilized polyoxometalates as catalysts for PET glycolysis under mild conditions. BHET was isolated in 85% yield after only 40 minutes at 190 °C and 0.018 mol% catalyst loading, with no loss in activity observed after the catalyst was recycled four times.

ILs have gained interest in the literature as catalysts for PET glycolysis due to the ease of separating the products from the reaction mixture, enabling facile catalyst recycling.<sup>719–721</sup> H. Wang *et al.*<sup>719</sup> first published the use of ILs as catalysts for PET glycolysis in 2009. They synthesized and tested several different ILs as catalysts and were able to achieve full conversion of PET to primarily BHET and some oligomers at 180 °C in 8 hours at atmospheric pressure. Higher reaction temperatures led to improved BHET selectivity. A subsequent study found that the IL could be recycled with no loss in activity.<sup>722</sup> They then found that an iron-containing IL could catalyze the depolymerization at temperatures as low as 140 °C.<sup>723</sup> Q. Wang<sup>720</sup> and coworkers studied different metal-containing ILs as PET glycolysis catalysts. They achieved isolated yields of up to 80% high purity BHET after 75 minutes at 175 °C and atmospheric pressure. Other metallic ILs have been shown to be effective catalysts for this reaction under a variety of conditions.<sup>724</sup> Yue *et al.*<sup>725</sup> used basic ILs as catalysts in PET glycolysis to isolate BHET in yields of up to 71% after 2 hours at 190 °C.

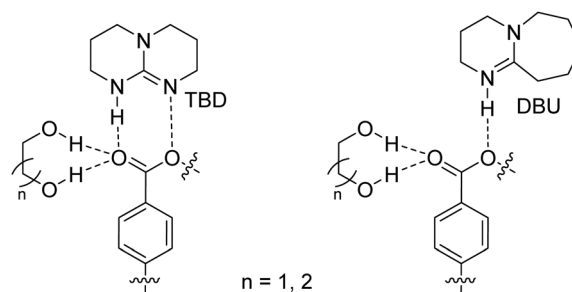
Deep eutectic solvents (DESSs) have also garnered recent interest as catalysts for PET glycolysis due to their low cost, simple synthesis, low toxicity, and other characteristics shared with ILs such as thermostability and tunability.<sup>726,727</sup> Q. Wang and coworkers first used DESSs as catalysts for PET glycolysis in 2015. Under optimized conditions of 170 °C and only 30 minutes, BHET was obtained in 83% yield. These results are similar to those obtained under supercritical conditions. The high activity is attributed to a synergistic effect between H-bonds and coordination bonds between the DES and EG. Sert *et al.*<sup>728</sup> synthesized five different DESSs to evaluate as PET glycolysis catalysts. The best catalyst tested was formed from potassium carbonate and EG, and reached isolated BHET yields of up to 88% after 2 hours at 180 °C.

A variety of different heterogeneous catalysts have also been used in the glycolysis of PET. Shukla and coworkers<sup>729</sup> used  $\beta$ - and  $\gamma$ -zeolites as catalysts for PET glycolysis in 2008. BHET yields of over 60% were reached after 8 hours in refluxing EG. Al-Sabagh *et al.*<sup>730</sup> used multiwalled carbon nanotubes doped

with  $\text{Fe}_3\text{O}_4$  as catalysts for PET glycolysis, and reported quantitative BHET yields after 2 hours at 190 °C. The catalyst was successfully recycled 8 times with no loss in activity. Verégue *et al.*<sup>731</sup> used 3 nm cobalt nanoparticles as catalysts, and isolated pure BHET without additional water in 77% yield after 3 hours at 180 °C. The catalyst could be reused at least 5 times with no drop in activity. Laldinpui and coworkers<sup>732</sup> used bamboo leaf ash as a bio-waste derived catalyst for PET glycolysis. Several metal oxides and other salts were identified in the catalyst, which provided BHET in up to 83% yield after 3 hours at 190 °C. The catalyst could be reused four times with only a slight decrease in yield, and EG was also recovered from the reactions for reuse. Z. Wang *et al.*<sup>733</sup> developed a colloidal catalyst based on graphitic carbon nitride for this reaction. 80% BHET yield was achieved in 30 minutes at 196 °C for five consecutive catalyst cycles. Several different post-consumer PET sources were successfully depolymerized to give BHET in ~80% yield, including green bottle flake, noise deadening foam, and bottle flake contaminated with PP.

IL catalysts have been tethered to heterogeneous supports to enable even more facile catalyst recovery and product isolation. Najafi-Shoa<sup>734</sup> and coworkers used a cobalt-containing IL supported on graphene to reach 95% isolated BHET yields after 3 hours at 190 °C and ambient pressure. The catalytic activity was maintained over five cycles. Al-Sabagh *et al.*<sup>735</sup> supported iron-containing ILs on bentonite to reach a maximum 44% BHET yield. Similarly, Cano *et al.* supported iron-containing ILs on silica-coated, magnetic  $\text{Fe}_3\text{O}_4$  nanoparticles. The recoverable catalyst gave quantitative BHET yields for an impressive twelve consecutive 24 hours cycles at 190 °C, and the magnetic particles greatly simplified reaction workup.<sup>736</sup>

Organocatalytic PET glycolysis was first reported in 2011 by Fukushima *et al.*<sup>737</sup> using the amine base 1,5,7-triazabicyclo[4.4.0]dec-5-ene (TBD). Isolated BHET yields of up to 78% were reached after 3.5 hours at 190 °C and atmospheric pressure, comparable to some of the most efficient metal-catalyzed reactions. A study of several other nitrogen-based catalysts led to the discovery that 1,8-diazabicyclo[5.4.0]undec-7-ene (DBU) was an even more efficient catalyst when EG was used as the glycol. Mechanistic studies revealed that EG and other short chain diols can act as cocatalysts to activate the PET ester group and assist in depolymerization (Fig. 33).<sup>738</sup> Jehanno and



**Fig. 33** Proposed mechanism of PET activation by the organic bases TBD or DBU and short chain alcohols. Longer chain alcohols cannot participate in this reaction.



coworkers<sup>739</sup> used a salt derived from TBD and methanesulfonic acid as a catalyst in PET glycolysis. 91% BHET was isolated after 2 hours at 180 °C. The catalyst could be recycled at least five times, and the monomer isolated from these reactions was used to synthesize new PET with similar thermal properties as commercial material.

Microwave irradiation is another growing strategy for facilitating PET glycolysis at milder conditions than conventional heating. Pingale and Shukla<sup>740</sup> first published in 2008 that, under otherwise identical zinc acetate-catalyzed glycolysis conditions, microwave irradiation provided the same yield of BHET in 35 minutes that conventional heating did in 8 hours. This increased efficiency was confirmed by Chaudhary *et al.*<sup>741</sup> Achilias *et al.*<sup>742</sup> studied the microwave glycolysis of PET to oligomers using diethylene glycol. They found that complete degradation was achieved in only 5 minutes at 180 °C, compared to more than 4 hours using conventional heating. Saravari *et al.*<sup>743</sup> glycolyzed PET bottles with propylene glycol under microwave irradiation with zinc acetate as a catalyst. Oligomers obtained from the reaction were reacted with linseed oil and toluene diisocyanate to obtain urethane oil with similar properties to commercially purchased material, showing the potential of this strategy for PET upcycling. Parrott<sup>744</sup> received a patent for microwave-assisted PET glycolysis in 2020. BHET yields of up to 94% were achieved in only 5 minutes of irradiation at 250 °C with 0.1 wt% zinc acetate as a catalyst. A variety of simple salt catalysts were investigated, and zinc salts were generally the most effective.

**9.1.5 Aminolysis.** Aminolysis depolymerizes PET in the presence of amines to form terephthalamides and EG. This process is more thermodynamically favored than alcoholysis or glycolysis due to the stronger amide bonds formed in the products, and so less forcing conditions can be used (Fig. 34).<sup>745</sup> The terephthalamide monomers can be used in a variety of upcycling applications, including antibacterial drugs, adhesion promoters, and as components for rigid polyurethane foams.<sup>668</sup> Aminolysis was first reported in the 1960s using a variety of primary and secondary amines.<sup>746</sup> In 2010, Soni and coworkers<sup>747</sup> depolymerized PET to terephthalamide using hydrazine in an uncatalyzed reaction at ambient temperature and pressure. After 12 hours, the product was isolated and reacted with acryloyl chloride to provide a UV curable acrylic oligomer, demonstrating a potential application of this depolymerization technique to generate upcycled products. In 2013, Bhatnagar and coworkers<sup>748</sup> working for the Indian Oil Corporation received a patent for aminolysis of virgin or post-consumer PET using (poly)amines to generate diamino

diamido mixtures with excellent bitumen anti-stripping properties. Reactions with quantitative product yield were run in xylene at 110–160 °C for 4 hours without a catalyst.

Soni and Singh reported the aminolysis of PET in the presence of aqueous methylamine or ammonia using cetyl ammonium bromide as a catalyst in 2005. They found that the catalyst reduced the required time for complete degradation to *N,N'*-dimethylterephthalamide to 45 days at 40 °C, while large PET flakes were still visible in the uncatalyzed reaction after the same time.

Ammonolysis of PET was much slower, and full depolymerization was not achieved under any tested conditions.<sup>749</sup> In 2006, Shukla and Harad<sup>750</sup> reported the aminolysis of PET using excess ethanolamine and simple catalysts including acetic acid, sodium acetate, and potassium sulfate. The product bis(2-hydroxy ethylene)terephthalamide (BHETA) was obtained in yields of up to 91% from post-consumer PET and 83% from bottle PET after 8 hours at reflux. Sodium acetate was found to give the highest yields in all reactions.

Tawfik and Eskander<sup>751</sup> used dibutyltin oxide as a catalyst in the aminolysis of PET with ethanolamine at 190 °C and ambient pressure. Pure BHETA was obtained in yields of 49–62% after 1–4 hours. Chan and coworkers<sup>752</sup> used zinc acetate as a catalyst to depolymerize post-consumer bottle PET in the presence of tri- and tetraamines. The reactions were complete in 30 minutes at 190 °C, and no purification of the polyamine products was necessary before the authors used them in crosslinking reactions with ethylene glycol diglycidyl ether to form hydrogels with potential uses in removing industrial dyes from water and other environmental and agricultural applications (Fig. 35).

Fukushima and coworkers<sup>745</sup> used TBD as a catalyst in PET aminolysis with a variety of primary amines. The terephthalamide products were obtained in moderate to high yields at reaction temperatures of 110–190 °C in less than 24 hours. The monomers have potential applications as building blocks for high performance materials with desirable thermal and mechanical properties. The same group used this catalytic system to depolymerize PET with *o*-phenylenediamine and 2-aminophenol to generate bis-benzamidazole and bis-benzoxazole, which can be used in the synthesis of medicines and high-performance polymers.<sup>753</sup>

Microwave irradiation has also been studied in PET aminolysis. Pingale and Shukla<sup>754</sup> reported the microwave-assisted aminolysis of PET using simple sodium salt catalysts and excess ethanolamine in 2009. BHETA yields of up to 90% were obtained in only 5 minutes under microwave irradiation, whereas similar yields required 8 hours using conventional heating. Cleaned post-consumer PET bottles and pristine PET



Fig. 34 Typical reaction conditions and products for PET aminolysis.



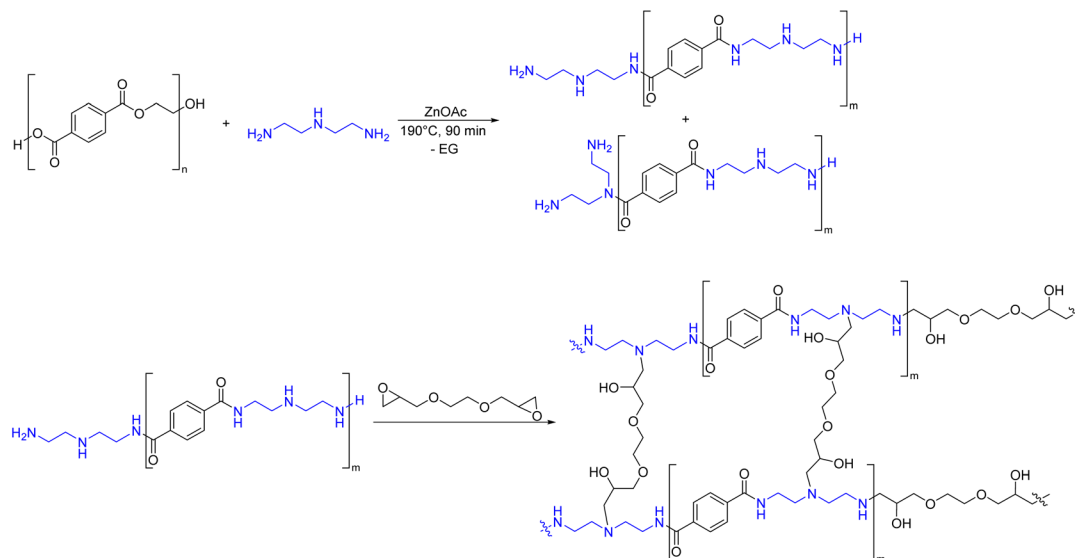


Fig. 35 Aminolysis of PET using a polyamine, followed by a crosslinking reaction to form a PET hydrogel.

fibers were both effectively depolymerized using this system. Achilias and coworkers<sup>755</sup> utilized microwave heating to quantitatively depolymerize PET to BHETA in only 5 minutes at 260 °C without the addition of a catalyst.<sup>756</sup> Hoang and Dang reported the uncatalyzed aminolysis of PET to bis(2-aminoethyl)terephthalamide and its oligomers  $\alpha,\omega$ -aminoligo(ethylene terephthalamide), but Sharma *et al.*<sup>757</sup> found that the same reaction could be carried out in only 10 minutes at 250 °C using microwave irradiation. They then used the obtained amides to synthesize bis-benzoxazines, which can be used as advanced performance thermosets.

The ammonolysis of PET involves the reaction of the monomer with excess ammonia to generate terephthalamide and EG as products. Terephthalamide can be further converted into platform chemicals *p*-xylenediamine or 1,4-bis(amino-

ethyl)cyclohexane.<sup>17</sup> A patent from 1988 describes the ammonolysis of PET under 20 bar NH<sub>3</sub> pressure at temperatures of 120–180 °C for 1–7 hours. A simple filtration and drying workup provided the product in >99% purity and >90% yield. The same patent describes the use of zinc acetate as a catalyst to facilitate the transformation at only 70 °C and provide terephthalamide in 87% yield.<sup>17</sup>

**9.1.6 Hydrogenolysis.** Hydrogenolysis reductively depolymerizes PET under H<sub>2</sub> pressure, typically forming 1,4-benzenedimethanol (BDM) and EG, and sometimes providing deoxygenated products. BDM is a platform chemical that can be used to prepare polylactide-based thermoplastic elastomers, highly cross-linked polymers, and sulfonated aromatic resins.<sup>758–760</sup> Organometallic catalysts have typically been used for these depolymerizations (Fig. 36).

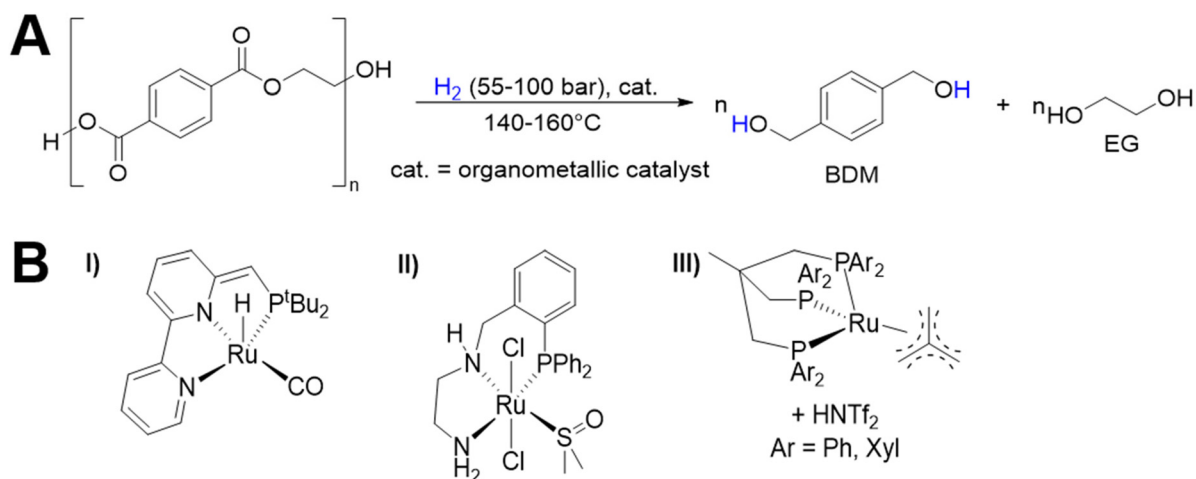


Fig. 36 (A) Typical reaction conditions and products for PET hydrogenolysis and (B) organometallic catalysts used for PET hydrogenolysis by (I) Krall *et al.*, (II) Fuentes *et al.*, and (III) Westhues *et al.*

In 2014, Krall and coworkers<sup>761</sup> found that a ruthenium pincer complex developed by Milstein could be used as a catalyst in the hydrogenolysis of PET (Fig. 36B I). At 2 mol% catalyst loading, 55 bar H<sub>2</sub>, and 160 °C in anisole/THF, quantitative conversion to BDM and EG was observed after 48 hours. Post-consumer PET soda bottles were used in these experiments without pretreatment. Fuentes *et al.*<sup>762</sup> found that a novel PNN pincer complex (Fig. 36B II) catalyzed PET hydrogenolysis with moderate BDM yields, but the catalyst was poisoned by the EG formed in the reaction. This precluded monomer yields higher than 73%. Westhues *et al.*<sup>763</sup> used a ruthenium triphos catalyst (Fig. 36B III) to depolymerize PET from a variety of sources, including water bottles, pillow filling, and a sports jersey. Reaction selectivity for BDM and EG were over 98% with most substrates, but relatively forcing conditions of 100 bar H<sub>2</sub> and 140 °C were required. An entire PET water bottle with PP cap and PE label was depolymerized without pretreatment. Quantitative conversion to BDM was observed, with no conversion of PP or PE. The other polymers could be filtered off and subsequently depolymerized.

Supported metal catalysts have also been used in PET hydrogenolysis. In 2020, Kratish *et al.*<sup>764</sup> selectively depolymerized PET to TPA and ethylene using a carbon-supported molybdenum-dioxo catalyst under only 1 bar H<sub>2</sub>. No solvent was required for the reaction, and TPA was obtained in 85% yield after 24 hours at 260 °C. The air and moisture stable catalyst could be recycled four times with no loss in activity, and the yield of TPA did not change when PET from a post-consumer beverage bottle was used as the substrate. Jing and coworkers<sup>765</sup> used a Ru/Nb<sub>2</sub>O<sub>5</sub> catalyst to convert PET to benzene, toluene, and *p*-xylene in 84% total yield. The reactions were run in octane at 280 °C and 5 bar H<sub>2</sub> for 8 hours. The catalyst also successfully depolymerized a mixture of PET, polycarbonate (PC), PS, and polyphenylene oxide to a variety of aromatic monomers in 79% overall yields, showing the viability of this system in mixed waste streams. However, a 1:1 mass ratio of polymer to catalyst was required in this system. Wu *et al.*<sup>766</sup> prepared an N-doped carbon-supported bimetallic catalyst for the conversion of PET to TPA in 91% yield in 10 hours at 260 °C and 1 bar H<sub>2</sub>. No solvent was used in the reaction, and the catalyst could be reused at least six times with no observed decrease in activity. Almost the same yield of

TPA was achieved with PET from bottles and with a mixture of PET and PP from bottles.

**9.1.7 Biocatalysis.** Given the ubiquity of natural ester-linked compounds in nature, including polymers such as cutin and suberin, enzyme catalysts have been pursued as another means to hydrolyze PET. These biocatalytic reactions have the advantage of enabling PET hydrolysis under mild conditions (30–75 °C and ambient pressure) in aqueous solutions to provide BHET, mono-2-hydroxyethylterephthalate (MHET), TPA, and EG with varying selectivity as products (Fig. 37). Many reviews have been written on this topic<sup>21,663,767–772</sup> and it is a highly active area of research, thus we only discuss highlights here.

The first report of enzymatic hydrolysis of PET was in 2005 from Müller *et al.*<sup>773</sup> wherein they showed appreciable extents of PET conversion over 3 weeks at 55 °C using a cutinase enzyme from the thermophilic bacterium *Thermobifida fusca*. This study prompted a search in genome and metagenome databases for additional cutinases capable of PET hydrolysis. In addition to the discovery and characterization of homologous enzymes from the genus *Thermobifida* and closely related bacteria,<sup>774–782</sup> Sulaiman *et al.* reported the discovery of a leaf-branch compost cutinase (LCC) that has been subsequently engineered by Tournier *et al.* for greater thermal stability and activity, enabling quantitative conversion of amorphous micronized PET substrates in 10 hours at 72 °C and enzyme loadings concomitant with industrial performance.<sup>783–785</sup> Shirke *et al.*<sup>786</sup> demonstrated that the addition of glycosylation to the LCC enzyme *via* expression in *Pichia pastoris* results in greater stabilization of the enzyme, thus highlighting the potential for post-translational modifications as another means of enzyme stabilization and engineering for industrial applicability. A similar enzyme to LCC was recently reported by Sonnendecker *et al.*<sup>787</sup> that is able to achieve similarly high PET conversion with no substrate pretreatment. Additional studies to diversify the known PET hydrolytic enzyme suite will likely be enabled by computational methods and the massive number of genome and metagenome sequences that are continuously being reported.<sup>788,789</sup>

The seminal discovery of *Ideonella sakaiensis* by Yoshida and coworkers<sup>790</sup> in 2016 highlighted that natural microbial systems are seemingly responding to the presence of PET in

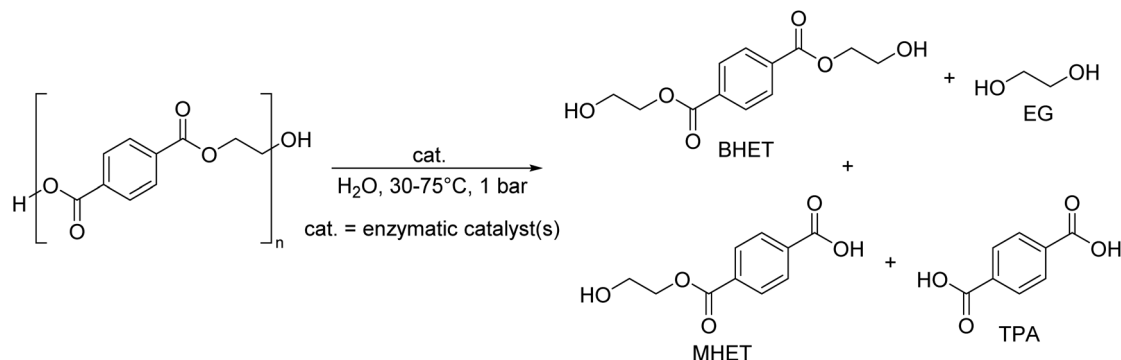


Fig. 37 Typical reaction conditions and products for enzymatic PET depolymerization.



the natural environment. In particular, *I. sakaiensis* secretes a two-enzyme system, comprising the enzymes PETase and MHETase, to fully depolymerize PET into TPA and EG *via* the intermediates BHET and MHET. This two-enzyme system has been extremely well studied to date, with structural biology techniques<sup>791–797</sup> and many types of protein engineering and evolution approaches used to improve the stability and performance particularly of the PETase enzyme.<sup>796,798,799</sup> The *I. sakaiensis* system also points to the potential utility of an enzyme cocktail for industrial application of an enzymatic recycling approach, as is common in industrial cellulose deconstruction, especially in this case to overcome product inhibition due to the buildup of MHET during enzymatic hydrolysis.<sup>783,800</sup>

Singh *et al.* recently conducted a detailed techno-economic, energy, and GHG emissions analysis of enzymatic PET recycling using the patent literature and the work from Tournier *et al.*<sup>785,800</sup> Therein, they estimated that with low-cost PET feedstocks, enzymatic recycling processes could achieve cost parity with virgin PET manufacturing at substantially reduced energy inputs and GHG emissions. This work directly highlighted two areas of prominence that merit further attention in process development for enzymatic PET recycling, which also may translate to other PET chemical recycling approaches discussed herein. Namely, it was estimated that approximately half of the energy input and GHG emissions arise from substrate pretreatment, which was modeled as thermal extrusion and cryo-grinding to yield micronized, amorphous PET. The development of enzymatic systems that can deconstruct crystalline substrates, which has been highlighted by studies as a major need for the field,<sup>787,799,801,802</sup> would thus be a major step forward for this approach. Secondly, EG recovery from

water was estimated to roughly equate to the other half of energy use and GHG emissions. Advanced approaches to separations for EG that operate in the condensed phase or employ reactive distillation may be of use to further improve this process and will likely be relevant for EG recovery in chemical solvolysis reactions as well.

## 9.2 Chemical recycling of polycarbonates and other polyester feedstocks

**9.2.1 Polycarbonates.** PC resins are generally distinguished by whether they have aliphatic or aromatic backbones. Aliphatic PC resins are not used as thermoplastics, while aromatic PCs are commonly used as engineering thermoplastics in electric and electronic equipment. Poly(BPA carbonate) (PBPAC) is the most commonly used PC and is the only PC resin that we will discuss in this section, though many chemical recycling strategies applied to PBPAC could also likely be applied to other PCs.<sup>803,804</sup> PBPAC has many desirable properties including high impact resistance and ductility, good optical clarity, flame retardancy, and relatively low production costs. Its global production has risen to 5 million tons per year.<sup>805</sup> Though commercial PC chemical recycling has not yet been realized,<sup>806</sup> many of the chemical recycling techniques discussed previously for PET have been investigated on a laboratory scale for PBPAC, including pyrolysis, hydrolysis, alcoholysis, aminolysis, and hydrogenolysis (Fig. 38).

PBPAC pyrolysis produces a large amount of char due to the flame retardancy of the polymer. Uncatalyzed pyrolysis at 300–500 °C leads to the generation of BPA and phenolic compounds as the primary liquid products, leaving behind a residue which accounts for 20–30 wt% of the starting material.<sup>804</sup> Metal chloride or oxide catalysts such as CuCl<sub>2</sub>,

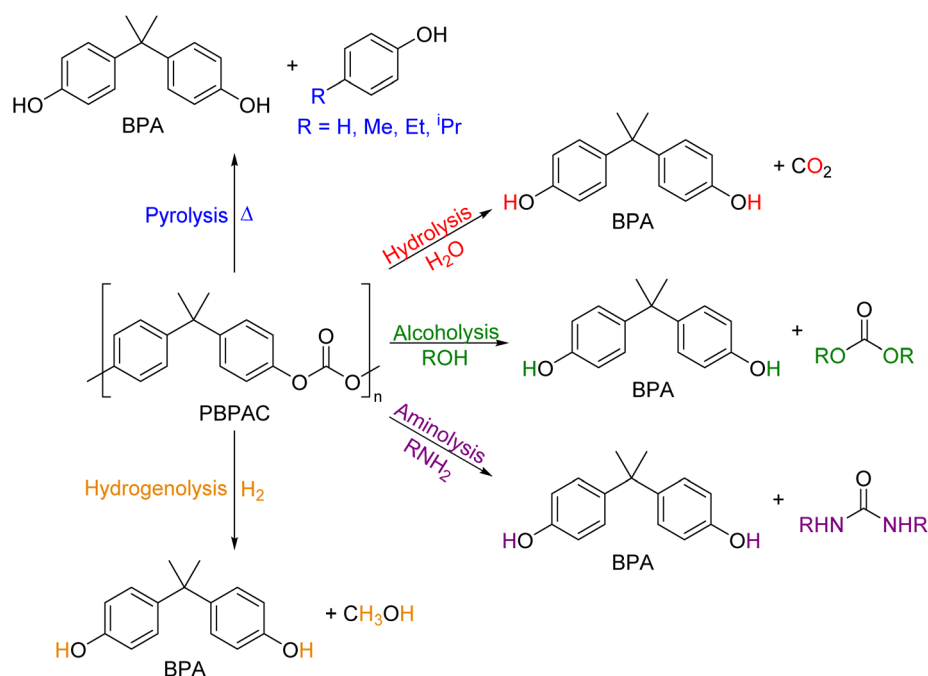


Fig. 38 Methods for the chemical depolymerization of PBPAC and their primary monomeric products.



FeCl<sub>3</sub>, ZnCl<sub>2</sub>, SnCl<sub>2</sub>, CaO, and MgO have been shown to lower the temperatures required for pyrolysis, narrow the product distribution, and decrease the amount of char waste formed in the reaction.<sup>484,488,807,808</sup> Due to the hydrophobicity of PBPA, hydrolysis of this polymer requires steam or supercritical conditions.<sup>805</sup> At temperatures above 240 °C, BPA and CO<sub>2</sub> are the primary products of PBPA hydrolysis.<sup>809–811</sup> Alkaline earth metal oxides and hydroxides, alkali hydroxides and carbonates, and rare earth triflates all catalyze PBPA hydrolysis, enabling milder reaction conditions and higher BPA yields especially when an organic cosolvent such as 1,4-dioxane is used.<sup>812–818</sup> Similar to hydrolysis of PET, ionic liquid catalysts<sup>819–821</sup> and microwave heating<sup>822,823</sup> also facilitate this reaction.

To our knowledge, PBPA alcoholysis was first reported with methanol, NaOH catalyst, and toluene cosolvent to swell the polymer and obtain BPA and methylene carbonate as products.<sup>824</sup> The reaction has since been adapted to continuous flow,<sup>825</sup> accelerated using microwave heating,<sup>823</sup> and run under supercritical conditions.<sup>826–828</sup> Alkali halide, heterogeneous, ionic liquid, and organic base catalysts have also been employed to increase yield and selectivity for BPA under milder conditions.<sup>829–837</sup> The aminolysis of PCs provides value-added ureas and BPA as products. The yield of monomeric products is increased when a diamine is used to form a stable cyclic urea.<sup>838,839</sup> An ionic liquid/ZnO nanoparticle catalyst system provides excellent BPA and urea yields with a variety of mono- and diamines.<sup>840</sup> Ammonolysis of PBPA in an aqueous ammonia solution provides BPA and urea in high yields.<sup>841,842</sup> Finally, many of the catalysts studied in PET hydrogenolysis also successfully depolymerize PCs under similar conditions to generate the corresponding alcohol monomer and methanol in high yields.<sup>761,763,765</sup>

**9.2.2 Other polyesters.** Poly(butylene terephthalate) (PBT) (Fig. 39) can be used in similar applications as PET and also as an engineering thermoplastic in rigorous mechanical profile applications such as car bumpers.<sup>14</sup> PBT resins have high strength and rigidity, low moisture absorption, and excellent electrical properties and chemical resistance.<sup>843</sup> Due to their similar chemical structures, many of the PET depolymerization strategies discussed above also successfully depolymerize PBT.

PLA is a widely used, industrially compostable bioplastic derived from the fermentation of renewable feedstocks.<sup>668</sup> PLA has good mechanical properties but a low glass transition temperature, narrow temperature-processing window, and undesirable brittleness.<sup>667</sup> Depolymerization of PLA to the

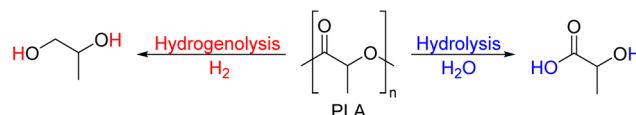


Fig. 40 Hydrolysis and hydrogenolysis of PLA to form lactic acid and propylene glycol, respectively.

lactide monomer is not possible due to side reactions including elimination to acrylic acid and epimerization.<sup>844,845</sup> The primary method used for the deconstruction of PLA on the lab scale is hydrolysis to lactic acid (Fig. 40).<sup>668</sup> Additionally, some catalysts used in the hydrogenolysis of PET are capable of reductively depolymerizing PLA to form propylene glycol in high yields.<sup>761,763</sup>

### 9.3 Commercial activity and economics

Much of the current commercial progress in PET chemical recycling is not captured in scientific publications, with patents and press announcements typically constituting the public information in this field. A recent review of advanced PET chemical recycling focuses primarily on the development of commercial processes.<sup>666</sup> At the time of publication, commercial chemical PET recycling has not yet been realized. However, many commercialization projects exist using different depolymerization chemistries and subsequent downstream purification processes.

Mechanical recycling of PET is complementary to chemical recycling processes, and both are needed to achieve a high degree of circularity in PET applications. Chemical recycling feedstocks will comprise primarily colored and/or opaque plastic bottles and polyester-based textiles that are unsuitable for the high purity standards required in mechanical recycling.<sup>662,664</sup> The availability of a high volume, low cost feedstock is critical for commercial process viability, which will require processing highly impure PET feedstocks to produce high purity, polymerization-grade monomers at scale. The quality of the output of rPET from chemical recycling is higher than that from mechanically recycled PET. This allows the rPET from chemical recycling facilities to be infinitely recyclable, whereas the rPET produced from mechanical recycling degrades during each cycle.

The commercial activity described below is in the research and development-to-pilot stage unless otherwise indicated. To our knowledge, hydrolysis, methanolysis, glycolysis, and enzymatic depolymerization are the current primary areas of commercial focus, but it is likely that additional technologies will soon emerge on the commercial landscape. The intention of the processes described here is the transformation of waste PET plastic and textiles to monomers for subsequent repolymerization to rPET with physical and mechanical properties identical to those of pristine material.

**9.3.1 Hydrolysis.** DePoly is a Swiss start-up that uses a room temperature basic hydrolysis process with TiO<sub>2</sub> or another metal oxide absorber in the presence of UV light.<sup>846</sup>

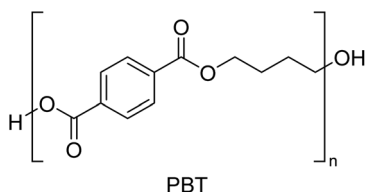


Fig. 39 Chemical structure of PBT.



The technology was originally developed at the Swiss Federal Institute of Technology Lausanne (EPFL).<sup>847</sup> Tyton BioSciences, recently renamed Circ, is a start-up based in the US which uses alkaline water at high pressure and temperature, called hydrothermal processing, to hydrolyze PET fiber to TPA, EG, and products formed from the reaction of other materials such as cotton present in the textile waste stream.<sup>848,849</sup> Gr3n, a Swiss-based start-up, announced the building of a demonstration plant in Italy in 2021. Their process features microwave-assisted hydrolysis that will be used to recycle both PET fiber and resin.<sup>850</sup>

**9.3.2 Methanolysis.** Loop Industries, a publicly traded Canadian company, has signed multiple partnerships for a global rollout of their methanolysis technology.<sup>851</sup> Using a patented process, the PET resin or fiber input is mixed with methanol, an organic swelling solvent, and an inorganic alkoxide catalyst. The reaction proceeds at a temperature below the boiling point of methanol and does not require added pressure.<sup>687</sup> At the time of writing this review, a timeline on their website states that Loop Industries has raised over \$116 million but as of yet does not have a commercial facility for their technology. Eastman Chemical has recently announced plans to build a \$250 million, 100 kton per year PET methanolysis plant in Tennessee.<sup>852</sup> They have been researching PET methanolysis for several decades, with patents in this field dating back to the early 1990s.<sup>853</sup>

**9.3.3 Glycolysis.** There are many companies working to commercialize glycolysis processes with unique process concepts. JEPLAN, a Japanese start-up, uses a metal hydroxide catalyst and EG for PET glycolysis in a pilot plant in Japan. They utilize a two-step purification process involving crystallization and distillation to produce polymerization-quality BHET.<sup>854</sup> Ioniqa, a spin-off from Eindhoven University, developed a process which features an imidazole base tethered to a magnetic iron oxide nanoparticle.<sup>855</sup> The magnetic nature of the anchored catalyst facilitates simplified catalyst removal and recovery for reuse. Ioniqa has agreements with large con-

sumer packaged goods companies in addition to PET producers and has recently announced a 10 kton per year facility.<sup>856</sup> Researchers at IBM have taken a different path to enable the facile separation and reuse of a PET glycolysis catalyst. Their process is catalyzed by a volatile organic base that can be recovered by distillation after PET depolymerization is complete.<sup>857</sup> This technology, known as VolCat (Volatile Catalyst), is being scaled up in a recently announced joint venture with several commercial partners.<sup>858</sup>

**9.3.4 Biocatalysis.** Commercial activity in biocatalytic PET depolymerization is highlighted by the publicly traded enzyme-catalyzed process from Carbios in France,<sup>785</sup> who launched a demonstration plant in 2021.<sup>859</sup> Carbios has announced partnerships including investors, end customers, enzyme producers, and process and plant designers to accelerate commercialization.<sup>860</sup> Carbios has raised over \$126 million to develop their technology,<sup>861</sup> and they currently operate a 1.2 kton per year demonstration facility with goals to build a 40 kton per year facility by 2025.<sup>862</sup>

## 10. Other catalytic approaches for plastics conversion

### 10.1 Hydrogenolysis with noble metals

Hydrogenolysis of plastics cleaves the carbon-carbon bonds in the presence of hydrogen converting the polymers into hydrocarbons (ranging from C1 to C50) typically with noble metal (*e.g.*, Ru, Pt *etc.*) catalysts. In such processes, heterogeneous catalysts are used which enables simple separation and recycling from the reactants and products.

Table 18 summarizes different technologies utilized in hydrogenolysis of waste plastics where plastics were converted in batch reactors. Ruthenium supported on metal oxides or carbon has been reported to catalyze the production of alkanes, aromatics, and liquid fuels from polyolefins (*i.e.*, LDPE, HDPE, PP), PS, and PC.<sup>863–869</sup> LDPE, HDPE, and PP can

**Table 18** Hydrogenolysis of plastics into various hydrocarbons in batch reactors

Catalyst	Polymer	Temperature (°C)	Pressure (Bar)	Time (h)	Polymer/catalyst (Mass)	Products	Ref.
Ru/CeO <sub>2</sub>	LDPE, HDPE, PP	200–240	20–60	5–24	34	Liquid fuels, waxes (C5–C45)	863
Ru/TiO <sub>2</sub>	PP	250	30	8–16	20–40	Lubricants (C20–C60), C1–C2 gases	869
Ru/Nb <sub>2</sub> O <sub>5</sub>	PET, PS, PC	200–320	3–5	12–16	1–2	Aromatic hydrocarbons	864
5Ru/C	PE, LDPE	200–225	20	16	25	Liquid alkanes (C3–C13), light gases (C1–C6)	865
5Ru/C	PP	250	35	8–24	14	Liquid alkanes (C5–C32), light gases (C1–C5)	866
Ru/FAU	LDPE, PP	300–350	50	3	50	Methane, light paraffins (C2–C11)	867
Ru/WO <sub>3</sub> /ZrO <sub>2</sub>	LDPE	250	30	2	40	Lubricants, waxes, diesel (C4–C35)	868
Ru/C	HDPE	220	30	1	2	Lubricants, liquid fuels (C6–C38)	870
Pt/WO <sub>3</sub> /ZrO <sub>2</sub> + zeolite	LDPE	250	30	2	10	Liquid fuels (C5–C22)	871
Pt/SrTiO <sub>3</sub>	PE	300	12	96	5	Lubricants, waxes ( <i>M<sub>w</sub></i> 200–1000 Da)	872
SiO <sub>2</sub> /Pt/SiO <sub>2</sub>	HDPE	300	14	24	88	Fuels, lubricants (C8–C32)	873
Pt/C	PP	300	15	24	10	Lubricants (C5–C45)	874



be converted to liquid fuel (C5–C21) and lubricants/waxes (C22–C45) at low temperature and low  $H_2$  pressure (*i.e.*, 200–250 °C, 20–30 bar) on metal oxides-supported Ru (*e.g.*, Ru/TiO<sub>2</sub>, Ru/CeO<sub>2</sub>).<sup>863,869</sup> Over multifunctional Ru/Nb<sub>2</sub>O<sub>5</sub>, monocyclic aromatics can be selectively produced from single or mixed aromatic plastics (*i.e.*, PET, PC, PS, polyphenylene oxide) at 200–320 °C in the presence of hydrogen and solvent (*e.g.*, water, octane *etc.*).<sup>864</sup> Ru hydrogenation sites with low coordination numbers (*i.e.*, 5–6) prevent the over-hydrogenating of the aromatics, while the surface Lewis acid and Brønsted acid sites on NbO<sub>x</sub> species act in concert to selectively adsorb, activate C–O bonds, and cleave C–C bonds of the plastics. The support can be adjusted to treat different plastics and obtain varied products.<sup>865–868</sup> Over Ru/WO<sub>3</sub>/ZrO<sub>2</sub>, LDPE can be converted into higher molecular weight fuels and wax/lubricant base-oils at 250 °C and 50 bar  $H_2$ .<sup>868</sup> While on Ru/FAU, methane (>97%) can be produced from PE, PP, and PS under 50 bar  $H_2$  at 300–350 °C.<sup>867</sup> Ru nanoparticles can also be supported on carbon (Ru/C) to catalyze the hydrogenolysis of LDPE, HDPE, and PP towards liquid *n*-alkanes and alkane gases (C1–C6) under mild conditions (200–250 °C, 20–50 bar  $H_2$ ).<sup>865,866</sup> In the liquid phase (water, *n*-hexane *etc.*), around 90 wt% of HDPE can be converted to liquid hydrocarbons (C8–C38) within 1 h on Ru/C catalysts at 220 °C in the presence of  $H_2$  (30 bar).<sup>870</sup>

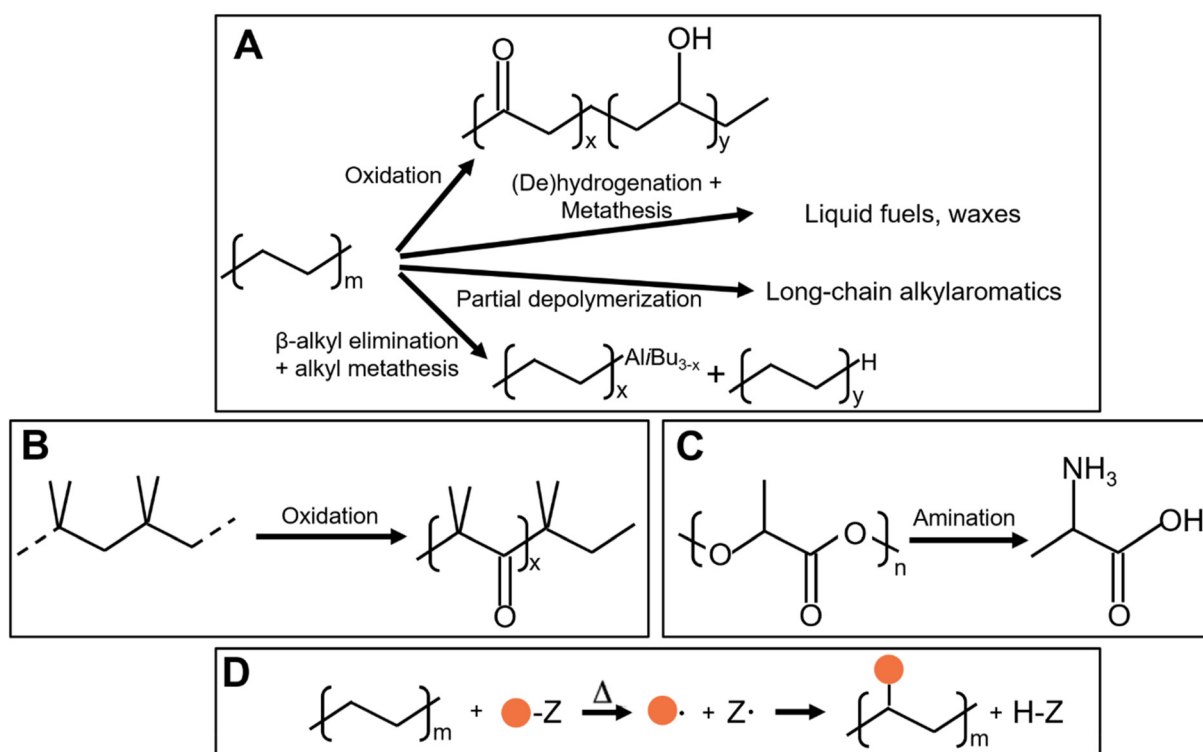
Pt-Based catalysts are another class of materials utilized in the hydrogenolysis of plastics.<sup>871–874</sup> It has been reported that PE can be converted into lubricants and waxes ( $M_w$  200–1000

Da) over platinum supported on strontium titanate or mesoporous shell/Pt/silica at 250–300 °C in the presence of  $H_2$  (10–17 bar).<sup>872,873</sup> Moreover, platinum can be supported on carbon which catalyzes the conversion of PP into liquid hydrocarbons (C5–C45),<sup>874</sup> or on WO<sub>3</sub>/ZrO<sub>2</sub> and mixed with zeolites which catalyzes the production of liquid fuels and short-chain hydrocarbons from PE, PP or PS.<sup>871</sup> The synergistic effects between platinum and supports (carbon/metal oxides) or co-catalysts (zeolites) are vital in these processes. Additionally, the hydrogenolysis of plastics can also be carried out over Al<sub>2</sub>O<sub>3</sub> or SiO<sub>2</sub> supported transition metals (Cr, Ni, Mo, Co, or Fe),<sup>875</sup> micro-mesoporous zeolites,<sup>876</sup> and other catalysts<sup>877</sup> which are not discussed here.

## 10.2 Functionalization and reactive extrusion

Another strategy to valorize plastics is the addition of other chemical groups (*e.g.*, aromatic ring, halogen, carboxylate, carbon–carbon unsaturated bond *etc.*) to these polymers *via* chemical methods (*e.g.*, oxidation, halogenation, esterification, metathesis)<sup>878,879</sup> as shown in Fig. 41. This approach is typically performed by reactive extrusion in an extruder. The products include polymers with new properties,<sup>880</sup> liquid fuels,<sup>881</sup> waxes,<sup>882</sup> and platform molecules.<sup>883</sup>

The C–H bonds in PE (HDPE, LDPE, LLDPE) can be oxidized to ketone or hydroxyl groups, which generates functionalized polymers with unique physical properties (*e.g.*, strong adhesion, ability to be painted with common paint *etc.*).<sup>880</sup> A high-valent ruthenium-oxo catalyst (polyfluorinated ruthe-



**Fig. 41** Strategies in functionalization of plastics: (A) functionalization of polyolefins; (B) oxidation of polyisobutene; (C) PLA amination; (D) reactive extrusion where orange circle represents a function group.



nium porphyrin) can be added with 2,6-dichloropyridine *N*-oxide to form esters from PE at 120 °C. The same complex can catalyze the oxidation of polyisobutene to oxo-polyisobutene (Fig. 41B) where the catalysts, reaction conditions, and oxidants are vital in selectively oxidizing the methylene positions and avoiding chain cleavage.<sup>884</sup> Reactions besides oxidation can be utilized to functionalize the plastics. Kanbur *et al.* reported that the conversion of polyolefins (PE, PP) to shorter aliphatic alkylaluminium species can be achieved *via*  $\beta$ -alkyl elimination and heterobimetallic alkyl metathesis using organozirconium catalysts and aluminum reagents at 200 °C.<sup>885</sup> The obtained shorter aliphatic alkylaluminium species can be further converted into alkyl alcohols, acids, halides, and hydrocarbons with a quenching process. Cross-alkane metathesis can convert PE into liquid fuels and waxes (short-chain linear alkanes) at 175 °C.<sup>881</sup> This process consists of three steps: (1) the dehydrogenation of PE and cofed light alkane; (2) the metathesis of olefins; (3) the hydrogenation of the obtained olefins. An iridium complex can catalyze steps 1 and 3 while  $\text{Re}_2\text{O}_7/\gamma\text{-Al}_2\text{O}_3$  catalyzes the olefin metathesis. The catalysts are compatible with various polymer additives and product distribution can be manipulated by the catalyst structure and reaction time.

Functionalized polymers can also be produced by dehydrogenation, sulfonylation, amination, and vitrimerization. Zinc sulfide is active in PP dehydrogenation<sup>886</sup> while an iridium complex can catalyze the dehydration of PE and poly(1-hexane) in the *p*-xylene and norbornene mixture.<sup>887</sup> For sulfonylation, it has been reported that PS can be sulfonated by chlorosulfonic acid, fuming/concentrated sulfuric acid, sulfur trioxide, and acetyl sulfate.<sup>888–891</sup> Tian *et al.* reported that  $\text{Ru}/\text{TiO}_2$  can catalyze the amination of ether groups in PLA in ammonia solution at 140 °C (Fig. 41C).<sup>883</sup> Alanine can be produced by this process with high selectivity in the absence of hydrogen. In most of the cases, other chemicals (*e.g.*, light alkanes, water, halogens) need to be cofed for the functionalization of the waste plastics. However, the cofed species is not necessary if the carbon and hydrogen in the polymers can be utilized. One approach is to partially depolymerize the plastics. Long-chain alkylaromatics (*ca.* C30) can be produced from PE *via* controlled depolymerization on  $\text{Pt}/\gamma\text{-Al}_2\text{O}_3$  without solvent or  $\text{H}_2$  at 280 °C.<sup>882</sup> This process couples exothermic hydrogenolysis and endothermic aromatization which enables simultaneous C–C cleavage, ring closure, and dehydrogenation under mild conditions (280 °C). Vitrimerization is a process converting polymers to vitrimers, which behave like silica,<sup>892</sup> are covalent networks and can change their topology by thermally activated bond-exchange reactions. Vitrimers can be produced from both thermoplastics (*e.g.*, PBT<sup>893</sup>) and thermoset plastics (*e.g.* polyurethane<sup>894</sup>). The key step in vitrimerization is introducing covalent adaptable networks *via* addition of catalysts or cross-linkers. Although catalyst is not necessary for vitrimerization, the properties of a catalyst-containing vitrimer can be efficiently tuned.<sup>893,895</sup>

Reactive extrusion is a commercially practiced approach to install functionality of plastics.<sup>896</sup> One example is the radical-

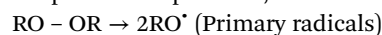
mediated addition of maleic anhydride to PE and PP.<sup>897</sup> One key step in reactive extrusion is the production of a pair of radicals which can be achieved through heating or photolysis of the reagent. One of the radicals cleaves a C–H bond in plastics and a chain transfer step can functionalize plastics (Fig. 41D). Thiocarbonyl amide reagent has been utilized to functionalize branched polyolefins.<sup>898</sup> The authors demonstrated that this metal-free C–H functionalization of isotactic PP can be performed on a decagram scale forming polymers with improved adhesion to polar substrates. Recently, another study demonstrated that an ideal reagent (*e.g.*, *O*-alkenylhydroxamate) enables slow chain transfer kinetics which provides various functionality to the backbone of plastics by other radical sources.<sup>899</sup>

The functionalization of waste polymers is being commercialized (*e.g.*, Novolooop<sup>900</sup>). The company can recycle waste LDPE, HDPE, and LLDPE. Those PE wastes are shredded, cleaned, and fed into a patented, accelerated thermal oxidative decomposition (ATOD) reactor (Fig. 42).<sup>900,901</sup> The treated PE is then heated to a temperature range from 60 to 200 °C, and oxidized into dicarboxylic acid monomers by a group of oxidation agents including oxygen, nitrous oxide, nitric oxide, and aqueous nitric acid.<sup>902</sup> The oxidized monomers are used to produce thermoplastic polyurethane (TPU).

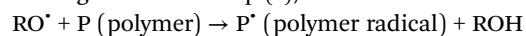
Plastic alloys are a type of functionalize plastic where different plastic materials are functionalized to create a single plastic phase.<sup>903,904</sup> The properties of the plastic alloy can be tuned by adding other materials (*e.g.*, waste fibers) which enables applications of plastic alloys in automotive, electrical & electronics, construction, home appliances, and healthcare equipment.<sup>905–908</sup> The advantages of plastic alloying are short reaction times, no need for solvents, and low operating/capital costs compared with other plastic technologies like gasification.<sup>909</sup>

Plastic alloying can introduce long chain branching of the polymer backbone to improve the properties (*e.g.* melt strength) of plastics. This approach has been used for functionalization of PP,<sup>909</sup> PE,<sup>910</sup> and polyhydroxybutyrate (PHB).<sup>906</sup> Long chain branching can be added using peroxides, which can result in increases in melt elasticity.<sup>908</sup> Long chain branching can alter physical properties such as the crystallinity and transition temperatures.<sup>911</sup> The thermophysical properties including crystallinity, melting behavior and tensile properties of HDPE were shown to be influenced by di-*tert* butyl cumyl peroxide induced cross-linking.<sup>910</sup> Dicumyl peroxide (DCP)-induced cross-linking in PE improves the melt strength and is dependent on peroxide concentration.<sup>912</sup> The lifetime of the peroxide formed from DCP is relatively close to the residence time of extrusion. The generally accepted process of peroxide induced cross-linking of polymers follows three key steps:<sup>913</sup>

(1) The primary radical formation from the thermal decomposition of peroxide,



(2) H abstraction from polymer backbone by free radicals of peroxide generated in step (1),



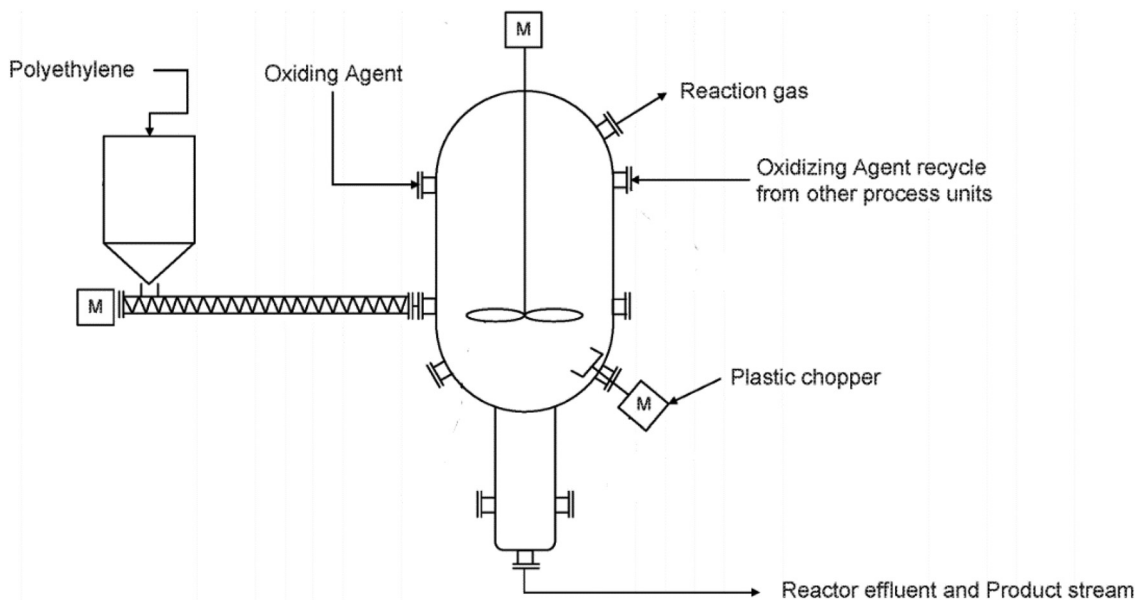


Fig. 42 The scheme of the ATOD reactor. (Extracted from the US patent US20220119616A1).<sup>902</sup>

(3) the bimolecular radical recombination of polymer radicals from step (2) to generate C–C cross-links.

$2P^{\bullet} \rightarrow P-P$  (crosslinking)

There is limited information on the chemical position(s) associated with cross-linked molecular chains to form a gel network structure. Long chain branching increases the plastic molar mass, polydispersity, melt strength and strain hardening in PP.<sup>909</sup> One key step in plastic alloying is C–H activation which can be achieved by different routes.<sup>2</sup>

Plastic alloying has been explained by inter-linking and interfacial adhesion between different polymers. Wigotsky pointed out the importance of plastic alloying to the plastic industry because of the improved physical properties of the alloys.<sup>904</sup> The compatibilizing agents in plastics act as polymeric surfactants which lowers surface tension and promotes interfacial adhesion between polymer phases in plastic alloys.<sup>914</sup> In addition to this, PP functionalization (*i.e.*, carboxylation) generates compatibilizers which can be used to produce plastic alloys.<sup>915</sup> Sakai reported a processing technology which can improve compatibility of plastic and produce plastic alloys using twin-screw extruders.<sup>916</sup> Asay *et al.* reported that PVC can be utilized to produce plastic alloys because of the varied degree of miscibility between PVC and a wide range of polymers.<sup>917,918</sup> Composite materials with improved properties can be obtained *via* addition of other materials. Kimura showed significant improvement in tensile strength by adding fillers to polyolefins.<sup>919</sup> Amor *et al.* studied the improvements of properties of PLA with biomass, demonstrating synergetic effect of small addition of PLA on the thermo-mechanical properties.<sup>920</sup> The above studies portray the importance of plastic alloying for the production of plastic and composite material products. However, these studies were all conducted with pure polymers by mixing two or three com-

ponents. Aumate *et al.* were the first to recognize that plastic waste could be also alloyed.<sup>903</sup> In their fundamental study, they simulated plastic wastes by mixing pure components of LDPE and HDPE with PP and showed the effects of the branching of PEs on mechanical properties and crystallization behavior.

Another plastic alloying approach is the “grafting onto” method which grafts the PHB polymer onto cellulose fibers through plastic alloying processing with the use of a small amount of DCP.<sup>906,908</sup> LDPE has also been shown to graft onto cellulose fibers, retaining the stiffness of cellulose and the flexibility of the polymer matrix.<sup>921</sup> When the peroxide is exposed to heat during extrusion, it will decompose into strong free radicals which tend to abstract H's from the polymer and cellulose molecular chains and initiate the grafting between the two phases in composites.

### 10.3 Microwave-assisted conversion

Microwave radiation can be applied during catalysis to heat the reaction system, shorten reaction times, and enhance the kinetics of some chemical reactions.<sup>922</sup> In conventional thermal heating processes, the whole reaction system (catalysts, reactor, diluent, feedstock *etc.*) are heated while microwave radiation enables the electromagnetic energy to be absorbed evenly and efficiently at the microwave-adsorbing points (*e.g.*, catalyst surface).<sup>922–924</sup> Furthermore, other researchers propose that the microwaves likely have intrinsic catalytic effects or assist in lowering the activation energy of the reactions.<sup>925</sup>

Microwave-assisted depolymerization and catalytic upgrading can be separated by the reactor system.<sup>491,926</sup> In microwave-assisted pyrolysis, LDPE is depolymerized into pyrolysis vapor and the microwave absorbent (*e.g.*, SiC) enables even



heating of the feedstock which promotes the formation of light olefins.<sup>491</sup> The products are then catalyzed by MgO to produce more valuable chemicals (*i.e.*, aromatics, C<sub>12+</sub> hydrocarbons) in a subsequent reactor. This process can be modified by changing the microwave absorbent to NiO and the catalyst in the separated reactor to HY zeolite which enhances the production of olefins in the pyrolysis zone and produces gasoline fuel with high yield as well as appropriate carbon number.<sup>926</sup> Microwave-assisted conversion can also be performed with catalysts in the liquid phase.<sup>927,928</sup> LDPE powder can be completely degraded in 1 h of microwave irradiation at 180 °C in the presence of dilute nitric acid solution (0.1 g mL<sup>-1</sup>).<sup>927</sup> In this process, water is used to absorb microwave energy and nitric acid catalyzes the oxidation of LDPE towards dicarboxylic acids (*e.g.*, malonic acid, succinic acid, glutaric acid *etc.*). Bäckström *et al.*<sup>928</sup> pointed out that HDPE can be converted to dicarboxylic acids with a similar approach and the obtained products can then be utilized to synthesize plasticizers. Addition of the plasticizer to PLA improves the physical properties of the polymers. Much faster degradation can be achieved *via* microwave-assisted conversion combined with appropriate catalysts. Jie and coworkers<sup>923</sup> reported that pulverized plastics (HDPE, LDPE, PP, PS) can be deconstructed into hydrogen and high-value carbon materials (*e.g.*, carbon nanotubes) in 30–90 s. FeAlO<sub>x</sub> plays a significant role in this process by both efficiently absorbing microwave energy, which initiates the physical heating process, and by catalyzing the depolymerization of the plastics.

Additionally, continuous processing and cofeeding of biomass can be applied to microwave-assisted conversion of plastics. Zhou *et al.*<sup>929</sup> reported a continuous microwave-assisted pyrolysis system which can convert HDPE and PP to gasoline-range hydrocarbons rich in aromatic hydrocarbons. The system consists of microwave heating with a SiC mixing-ball-bed and a secondary catalyst bed with ZSM-5 and can process up to 10 kg of plastics an hour with 89.6% energy efficiency. Considering the oxygen deficiency of polyolefins, it can be used as a hydrogen source to be co-processed with hydrogen-deficient biomass *via* microwave heating, thus improving the quality of the bio-oil.<sup>930,931</sup> Zeolites and metal oxides as well as the combination of these two materials have been reported to catalyze the production of hydrocarbons from a mixture of LDPE and lignin, where microwave-assisted heating is vital in achieving even and efficient internal heating.

#### 10.4 Biocatalysis

This section will focus on the biocatalysis of other plastics as the application of biocatalysis for PET depolymerization has been discussed in Section 9. The biological breakdown of plastics by enzymes refers to an attack on water immiscible plastic polymers by appropriate microflora. Plastics are degraded by microbial flora's enzymatic activity, which results in polymer chain fragmentation into monomers.<sup>932</sup> Degradation is caused by the activity of enzymes secreted by microorganisms, which use hydrocarbons in the polymer backbone as their major

carbon source.<sup>932</sup> Enzymatic plastic degradation proceeds in two steps.<sup>933</sup> The first step is the decomposition of polymers into smaller molecular compounds by attacking main chains of the polymer with abiotic and/or biotic reactions. The second step is the assimilation of the decomposed polymer (monomer, dimer, or oligomers) by means of microbials and its mineralization which creates CO<sub>2</sub>, H<sub>2</sub>O, and CH<sub>4</sub>.

The degradation of HDPE by exposure to white rot fungus, *Bjerkandera adusta* TBB-03, in a lignocellulose substrate treatment has been demonstrated.<sup>934</sup> TBB-03 is able to effectively improve laccase activity (211.4 U L<sup>-1</sup>) in the presence of ash wood chips due to a mediator resulting from lignin decomposition. The mediator is oxidized by laccase and may play a role as a strong oxidant by producing radical intermediates, which results in the significant morphological change of HDPE.

Skariyachan and coworkers reported that thermophilic consortia of *Aneurinibacillus* sp. and *Brevibacillus* sp. showed degradation potential for LDPE, HDPE and PP films and pellets.<sup>935</sup> The percentage weight reduction for LDPE, HDPE and PP strips in the consortia of isolates at 50 °C in 140 days was calculated to be 58.21%, 46.6% and 56.3%, respectively. The report on the enzymatic degradation associated with PVC was discussed by Khatoon *et al.*<sup>936</sup> *Phanerocheate chrysosporium* is able to degrade PVC film with 31% weight loss at 25 °C in the 4<sup>th</sup> week of the incubation period with the fungal strain. Furthermore, Sumathi *et al.* isolated a fungal species, *Cochilobolus* sp., for production of laccase, from plastic dumped soils and then determined the ability of the fungi to degrade low molecular weight PVC under lab conditions where the synthetic polymer served as the only carbon source for the *Cochilobolus* sp.<sup>937</sup> They observed significant differences from the FTIR, GC-MS, and SEM results in between control and *Cochilobolus* sp. treated PVC.

## 11. Conclusions and outlook

Compared to other engineered materials (*i.e.*, glass, metal, paper *etc.*), plastics are lightweight and can be easily manufactured into products for a variety of applications. Generation of plastic waste and the ratio of waste plastics in MSW have increased due to the growth of plastic production. Recycling of plastics is still far behind where it needs to be for a circular plastics economy, but improved technology is continuously being developed to efficiently increase the lifetime of plastics.

### 11.1 Collecting and sorting of waste plastics

The first step in any plastic recycling involves collecting and separating the plastics. There is an opportunity to divert more material from landfills through an upgrade in the recycling infrastructure. This can be achieved by an increase in the number of facilities, such as MRFs, or by improving process efficiency along the recycling process, such as improved sorting by adding more optical sorters. However, this will result in additional capital costs for MRFs. Education and outreach regarding recycling is also critical, as consumers need to



learn the environmental, social, and economic benefits of recycling.

The operation of a MRF presents multiple challenges. One is the difficulty in finding personnel. Another challenge is the lack of predictability of the inbound stream, as each week, the received material can fluctuate according to holidays. For example, in the period of the year close to the Thanksgiving and Christmas holidays, there is an increase in food containers (from dinner parties) and fibers (ads from the shopping season). In terms of the materials collected, some MRFs view the presence of full-body shrink sleeve labels on PET bottles and aluminum cans as a challenge, as it affects the recyclability of two significant sources of income (PET and aluminum). Other challenges include the presence of films and flexible packaging, shredded paper, and packaging with mixed types of material (e.g., plastic bottles with metal closures).<sup>938</sup>

Increased contamination of the waste material stream is also an issue, especially with material collected from areas not used to having recycling programs, which often have less awareness of the waste sorting procedures. For example, lithium batteries are a growing concern due to the danger of starting fires, with 68 incidents reported in MRFs between 2013 and 2020.<sup>939,940</sup> The challenges associated with the presence of contaminants in the bales could result in lower yields per bale, showing an opportunity to improve bale quality. Such measures would include an increase in sortation efficiency by adding more optical sorters, expansion of recycling education to reduce contamination in inbound streams, or even construction of new MRFs.

In developing countries, the waste pickers also need support. The main needs of waste pickers include improving their working conditions, learning to manage their family needs, receiving education and training, preventing violence and guidance to reduce teenage pregnancies, alcoholism and drug addiction, and training to “produce something” from the waste that gives them more income.<sup>941</sup> Some actions that would lead to fair living wage waste picking jobs include: (a) develop strategies for precise censuses of waste picker communities and to have dynamic updates of this information; (b) integrate waste pickers in the recycling value chain; (c) harmonize recycling strategies with frontier technologies and train the waste pickers; (d) develop innovative business models for MSW management with a social perspective; (e) update and enforce the legal and regulatory framework of recycling value chains in compliance with human rights of waste pickers; (f) integrate and establish social programs for waste pickers, from public, private, local, and international organizations.

### 11.2 Mechanical recycling of waste plastics

Mechanical recycling works well for a very homogeneous plastic stream like HDPE milk bottles. However, contamination and other plastics decrease the quality of the plastics produced during mechanical recycling. Some plastics cannot undergo mechanical recycling or do not flow upon heating after cure (thermosets) as they cannot tolerate thermal treatment. Multi-layered plastic products (*i.e.*, juice bottles) cannot

be mechanically recycled. These multi-layered packaging materials are more challenging to recycle as each plastic in a different layer has a different melting temperature, and different plastics are often immiscible which makes them practically non-recyclable.<sup>942</sup> Colored plastic products, for example PET containers with carbon black in them, are not detected by the sensors during the sorting stage of recycling and complicate the recycling process.<sup>943</sup> Films produce a low quality product during mechanical recycling. To improve the quality of the products from mechanical recycling, more advanced separating techniques can be used to obtain feedstock with high a degree of homogeneity. In addition, additives can be added to the extruder to improve the quality of the resin.

### 11.3 Pyrolysis, liquefaction, and gasification of waste plastics

Pyrolysis, liquefaction and gasification have the advantage of being able to process mixtures of plastics and more easily dealing with contamination than mechanical recycling. Several plastic pyrolysis approaches are being commercialized. Catalytic pyrolysis is used to increase product selectivity.<sup>944</sup>

Despite continuing advancement of the technology, commercialization of plastics pyrolysis faces significant challenges which can be addressed by further research. Better understanding of the complex reaction mechanisms controlling depolymerization of plastics could improve selectivity to desired produce molecules. Novel approaches to process intensification will be important to overcome the combination of relatively modest chemical reaction rates and heat and mass transfer limitations that characterize many pyrolysis processes. Using process intensification to achieve economies of scale, determining optimal reactor and process conditions, and securing consistent feedstock streams will increase the profitability of pyrolysis plants. In addition to this, the reactors used in pyrolysis need to be well designed to enable efficient mass and heat transfer. A better understanding of approaches to convert the plastic pyrolysis oils into chemicals, plastics and fuels is needed as steam cracking of the oil has several challenges.

Liquefaction is another technology currently being commercialized. The major challenges of liquefaction are high costs related to the equipment and operation conditions. Supercritical HTL also increases reactor corrosion. Enabling a high feedstock mass loading in the solvent without significantly affecting liquefaction efficiency is also critical, as it is less efficient to heat a large amount of solvent and convert only a small amount of plastic waste. According to Licella, feedstock loading must be sufficiently high (*i.e.*, 70%) for their Cat-HTR process to be economical. Developing an improved conversion strategy to produce higher quality products with minimal required upgrading is also essential. While lab studies indicate that feedstock compositions and reaction conditions strongly impact liquefaction product yield and quality, fewer studies discuss cross-interactions among different plastics. There is also a lack of information about the fate of contaminants and pollutants during liquefaction. HTL of polymers also promotes oxidative reactions, which become more



noticeable under supercritical conditions. The effect of oxygenated compounds on the direct use of the crude oil or during subsequent upgrading should be addressed in future studies.

Gasification of MSW shares similar challenges and opportunities as other fossil-based gasification technologies, primarily associated with the high capital cost of gasification. Converting synthetic gas to heat and power produces energy that competes with the declining costs of solar and wind power generation which are now less than \$0.04 per kW per h.<sup>945</sup> Pursuing higher-value chemicals such as ethylene which is valued at more than \$1000 per metric ton<sup>946</sup> is possible but requires several catalytic steps (methanol synthesis and methanol to olefins). The varying composition of waste plastic streams presents an additional operational and management challenge for recycling facilities. An incentive program tailored to reduce the risk of economic losses due to market price volatility could serve as a complement or alternative to environmental regulations. Waste reduction policies and incentive programs will likely spur the development of waste gasification facilities.<sup>947</sup>

#### 11.4 Dissolution-based approaches for waste plastics

Dissolution-based plastic recycling approaches can have advantages over other recycling technologies as they produce the virgin resins. Proper solvent selection for specific types of plastic waste is the key to the feasibility of dissolution-based plastic recycling. Many solvent systems for common polymers have been disclosed in the literature and in patents by different companies. However, when considering more complicated plastic waste feedstocks, advanced thermodynamic computational tools are a means to expedite the development and design of these processes. The recycled materials obtained *via* dissolution/precipitation methods could be economically competitive with virgin resins, showing the capability of these approaches to reduce plastic waste. These techniques can also be applied to complex multicomponent input streams (*e.g.*, multilayer films) which are challenging for current mechanical recycling technologies.

Several challenges remain in the design of dissolution-based recycling techniques that merit future study. The use of large amounts of solvent in these processes poses potential challenges associated with toxicity and energy consumption.<sup>631,948,949</sup> To address these concerns, methods for solvent selection based on polymer solubility can be combined with technoeconomic and life cycle analysis techniques to assess tradeoffs in solvent selection.<sup>38,47,634</sup> Another challenge is the removal of potential contaminants (*e.g.*, residual inks or retained solvent) from the recovered polymers.<sup>588,950</sup> The kinetics of dissolution also could hinder dissolution-based recycling for large amounts of plastic waste.<sup>609,651</sup> These challenges could be addressed through additional processing steps for contaminant removal or mechanical shredding prior to dissolution; such steps will require further investigation. Finally, there are opportunities to explore the integration of dissolution-based techniques with liquid-phase chemical recycling techniques.<sup>669,951</sup> For example, selective dissolution

could be used to separate target polymers from mixed plastic waste prior to their chemical depolymerization, thereby mimicking pretreatment methods utilized in biomass conversion. In this context, solvents could be selected to promote both polymer solubility and desired reaction outcomes.

#### 11.5 Chemical recycling approaches for polyesters and other plastics

New chemical recycling processes centered around catalysis are emerging. PET can be depolymerized *via* many different routes generating chemicals to produce rPET or other commodities (Fig. 28). For the hydrogenolysis of waste plastics, the product distribution can be tuned by adjusting the residence time, catalyst to polymer mass ratio, temperature, and H<sub>2</sub> pressure *etc.* Detailed reaction mechanisms for the hydrogenolysis of plastics should be elucidated to provide structure–function relationships at the molecular/atomic level which will provide insights in the rational design of new catalysts with improved efficiency or cheaper metal centers. The products from hydrogenolysis are mainly paraffins and light gases. Converting these back into plastics would involve dehydrogenation followed by steam cracking or another type of processing. The cost of H<sub>2</sub> and safety issues related to its use are major concerns in the industrialization of such processes. Continuous flow of feedstocks with uniform properties might be challenging due to the solid state of waste plastics. It would be ideal to design techniques which enable continuous feedstock flow with high polymer/catalyst ratio and short reaction times. Furthermore, noble metal centers are likely to be poisoned by the impurities in the feedstock, which also needs to be considered in the development of catalytic materials and processes for waste plastics hydrogenolysis.

In the functionalization of plastics, product selectivity and atom efficiency are two challenges since side reactions (*e.g.*, undesired chain cleavage, over-functionalized *etc.*) easily occur under reaction conditions and an excess of reactant is often required to provide the functional groups. The impurities in waste plastics likely lead to contaminated products or poison the catalysts, which should also be considered in developing these techniques. The removal of impurities in feedstocks needs significant effort in the sortation and pretreatment of waste plastics. Instead, virgin plastic resin can be utilized to manufacture some of the functionalized polymers. Besides, some of the processes need long reaction times (*i.e.*, up to 4 days), which needs to be addressed in scaling up the techniques. Plastic alloying has several advantages compared to other recycling technologies. The key advantages include: (1) little sorting is needed prior to forming the plastic alloys; (2) every type of plastic (#1–#7) can be recycled *via* this approach; (3) less manpower is needed to operate a plastic alloy facility compared to a MRF and the secondary recycling facility. Compared to pyrolysis of waste plastics, the advantages are: (1) higher ratio of the mixed plastic waste stream can be recycled; (2) fewer numbers of steps are required which results in lower capital/operating costs; and (3) higher value materials than a plastic oil can be produced. More work on this technology is



needed to understand if it can be applied to real plastic waste feedstocks, understand the relationships between the catalysts/additives and identify the properties of the plastic alloys, as well as the desirable properties of the plastic alloys.

The removal of impurities in the feedstock is also one of the challenges in microwave-assisted conversion. The impurities that can absorb microwave energy likely lead to varied local temperature, which then results in wide product distribution. Accurate parameters (*i.e.*, microwave power, radiation intensity, magnetic permeability *etc.*) need to be standardized for the development of this technique. The capital cost and energy efficiency should also be considered in scaling up microwave-assisted techniques for plastic recycling. As for the biocatalytic processes, it is important to standardize and improve the efficiency of the isolation procedure for microbial species which contain plastic degrading enzymes so that pure breeding colonies of these microorganisms can be quickly screened. Enzyme production from pure colonies can be boosted by standardizing the initial step, which enhances the overall performance of biocatalytic plastic degradation.

Overall, enhancing plastic recycling requires focused efforts, particularly in chemical recycling technologies. Efficient approaches to process waste plastics need to be developed to decrease plastic waste and pollution.

## Conflicts of interest

The authors declare conflict of interest.

## Acknowledgements

This material is based upon work supported by the U.S. Department of Energy, Office of Energy Efficiency and Renewable Energy, Bioenergy Technologies Office under Award Number DE-EE0009285. Professor G. W. Huber has an ownership interest in Anellotech, which is commercializing the PlastiCat technology described in this review paper. This paper was also supported in part by the Institute for the Advancement of Food and Nutrition Sciences (IAFNS) through a grant from the Food Packaging Safety and Sustainability Committee. IAFNS is a nonprofit science organization that pools funding from industry collaborators and advances science through the in-kind and financial contributions from public and private sector participants. We also thank Rosalind J. McKennon for her help with requiring permission for materials and Xin Zou for her help with improving figures in this paper.

## References

- 1 R. C. Thompson, S. H. Swan, C. J. Moore and F. S. Vom Saal, *Our Plastic Age*, The Royal Society Publishing, 2009, vol. 364, pp. 1973–1976.
- 2 R. Geyer, J. R. Jenna, and K. L. Law, Production, Use, and Fate of all Plastics ever Made, *Sci. Adv.*, 2017, 3(7), e1700782.
- 3 PlasticEurope Plastics – the Facts 2015 an Analysis of European Plastics Production, Demand and Waste Data, <https://plasticseurope.org/wp-content/uploads/2021/10/2015-Plastics-the-facts.pdf> (accessed Dec 06).
- 4 A. J. Ragauskas, G. W. Huber, J. Wang, A. Guss, H. M. O'Neill, C. S. K. Lin, Y. Wang, F. R. Wurm and X. Meng, *New Technologies are Needed to Improve the Recycling and Upcycling of Waste Plastics*, Wiley Online Library, 2021, vol. 14, pp. 3982–3984.
- 5 Foundation, E. M. Plastics and the Circular Economy. <https://archive.ellenmacarthurfoundation.org/explore/plastics-and-the-circular-economy> (accessed Feb 02).
- 6 J. R. Jambeck, R. Geyer, C. Wilcox, T. R. Siegler, M. Perryman, A. Andrady, R. Narayan and K. L. Law, Plastic waste inputs from land into the ocean, *Science*, 2015, 347(6223), 768–771.
- 7 National Academies of Sciences, E.; Medicine, Reckoning with the U.S. Role in Global Ocean Plastic Waste. 2021.
- 8 S. Allen, D. Allen, F. Baladima, V. Phoenix, J. Thomas, G. Le Roux and J. Sonke, Evidence of Free Tropospheric and Long-Range Transport of Microplastic at Pic Du Midi Observatory, *Nat. Commun.*, 2021, 12(1), 1–10.
- 9 United States Environmental Protection Agency Trash-Free Waters Plastic Pollution. <https://www.epa.gov/trash-free-waters/plastic-pollution> (accessed Dec 06).
- 10 C. Benson, Waste containment: Strategies and performance, *Aust. Geomech.*, 2001, 36(4), 1–25.
- 11 K. L. Law, N. Starr, T. R. Siegler, J. R. Jambeck, N. J. Mallos and G. H. Leonard, The United States' contribution of plastic waste to land and ocean, *Sci. Adv.*, 2020, 6(44), eabd0288.
- 12 HS Markit Analysis Indicates Need for Multibillion-Dollar Capital Spending to Achieve a “Circular Plastics Economy” by 2050. [https://news.ihsmarkit.com/prviewer/release\\_only/slug/bizwire-2021-10-11-ihs-markit-analysis-indicates-need-for-multibillion-dollar-capital-spending-to-achieve-a-circular-plastics-economy-by-2050](https://news.ihsmarkit.com/prviewer/release_only/slug/bizwire-2021-10-11-ihs-markit-analysis-indicates-need-for-multibillion-dollar-capital-spending-to-achieve-a-circular-plastics-economy-by-2050) (accessed Feb 02).
- 13 S. Ilias and A. Bhan, Mechanism of the Catalytic Conversion of Methanol to Hydrocarbons, *ACS Catal.*, 2013, 3(1), 18–31.
- 14 S. R. Nicholson, N. A. Rorrer, A. C. Carpenter and G. T. Beckham, Manufacturing energy and greenhouse gas emissions associated with plastics consumption, *Joule*, 2021, 5(3), 673–686.
- 15 S. D. A. Sharuddin, F. Abnisa, W. M. A. W. Daud and M. K. Aroua, A Review on Pyrolysis of Plastic Wastes, *Energy Convers. Manage.*, 2016, 115, 308–326.
- 16 S. Ügdüler, K. M. Van Geem, M. Roosen, E. I. Delbeke and S. De Meester, Challenges and Opportunities of Solvent-Based Additive Extraction Methods for Plastic Recycling, *Waste Manage.*, 2020, 104, 148–182.



- 17 V. Sinha, M. R. Patel and J. V. Patel, Pet Waste Management by Chemical Recycling: A Review, *J. Polym. Environ.*, 2010, **18**(1), 8–25.
- 18 A. Singh, N. A. Rorrer, S. R. Nicholson, E. Erickson, J. S. DesVeaux, A. F. Avelino, P. Lamers, A. Bhatt, Y. Zhang and G. Avery, Techno-Economic, Life-Cycle, and Socioeconomic Impact Analysis of Enzymatic Recycling of Poly (Ethylene Terephthalate), *Joule*, 2021, **5**(9), 2479–2503.
- 19 A. J. Martín, C. Mondelli, S. D. Jaydev and J. Pérez-Ramírez, Catalytic Processing of Plastic Waste on the Rise, *Chem*, 2021, **7**(6), 1487–1533.
- 20 L. O. Mark, M. C. Cendejas and I. Hermans, Cover Feature: The Use of Heterogeneous Catalysis in the Chemical Valorization of Plastic Waste (ChemSusChem 22/2020), *ChemSusChem*, 2020, **13**(22), 5773–5773.
- 21 L. D. Ellis, N. A. Rorrer, K. P. Sullivan, M. Otto, J. E. McGeehan, Y. Román-Leshkov, N. Wierckx and G. T. Beckham, Chemical and Biological Catalysis for Plastics Recycling and Upcycling, *Nat. Catal.*, 2021, **4**(7), 539–556.
- 22 J.-P. Lange, Managing Plastic Waste– Sorting, Recycling, Disposal, and Product Redesign, *ACS Sustainable Chem. Eng.*, 2021, **9**(47), 15722–15738.
- 23 T. A. Osswald and J. P. Hernández-Ortiz, *Polymer processing, Modeling and Simulation*, Hanser, Munich, 2006, pp. 1–651.
- 24 R. Geyer, J. R. Jambeck and K. L. Law, Production, Use, and Fate of All Plastics Ever Made, *Sci. Adv.*, 2017, **3**(7), e1700782.
- 25 A.-V. Ruzette and L. Leibler, Block copolymers in tomorrow's plastics, *Nat. Mater.*, 2005, **4**(1), 19–31.
- 26 T. Ren, M. K. Patel and K. Blok, Steam cracking and methane to olefins: Energy use, CO<sub>2</sub> emissions and production costs, *Energy*, 2008, **33**(5), 817–833.
- 27 S. S. Chadwick, *Ullmann's encyclopedia of industrial chemistry. Reference Services Review* 1988.
- 28 IHS\_Chemical, PEP Review-Ethylene Process Summary, 2015.
- 29 M. Yang and F. You, Comparative techno-economic and environmental analysis of ethylene and propylene manufacturing from wet shale gas and naphtha, *Ind. Eng. Chem. Res.*, 2017, **56**(14), 4038–4051.
- 30 E. Baur, T. A. Osswald and N. Rudolph, *Plastics Handbook*, Hanser Publications, Munich, Germany, 2019.
- 31 A. Naranjo, *Plastics testing and characterization: Industrial applications*, Hanser Verlag, 2008.
- 32 T. A. Osswald and G. Menges, *Materials science of polymers for engineers*, Carl Hanser Verlag GmbH Co KG, 2012.
- 33 F. Fleischhaker, A. P. Haehnel, A. M. Misske, M. Blanchot, S. Haremza and C. Barner-Kowollik, Glass-Transition-, Melting-, and Decomposition Temperatures of Tailored Polyacrylates and Polymethacrylates: General Trends and Structure-Property Relationships, *Macromol. Chem. Phys.*, 2014, **215**(12), 1192–1200.
- 34 IAPD Thermoplastics Rectangle. <https://www.iapd.org/ItemDetail?iProductCode=ITR> (accessed 07 Feb).
- 35 F. Perugini, M. L. Mastellone and U. Arena, A life cycle assessment of mechanical and feedstock recycling options for management of plastic packaging wastes, *Environ. Prog.*, 2005, **24**(2), 137–154.
- 36 L. Shen, E. Worrell and M. K. Patel, Open-loop recycling: A LCA case study of PET bottle-to-fibre recycling, *Resour., Conserv. Recycl.*, 2010, **55**(1), 34–52.
- 37 S. Toniolo, A. Mazzi, M. Niero, F. Zuliani and A. Scipioni, Comparative LCA to evaluate how much recycling is environmentally favourable for food packaging, *Resour., Conserv. Recycl.*, 2013, **77**, 61–68.
- 38 A. Schwarz, T. Ligthart, D. G. Bizarro, P. De Wild, B. Vreugdenhil and T. Van Harmelen, Plastic recycling in a circular economy; determining environmental performance through an LCA matrix model approach, *Waste Manage.*, 2021, **121**, 331–342.
- 39 U. Arena, M. L. Mastellone and F. Perugini, Life cycle assessment of a plastic packaging recycling system, *Int. J. Life Cycle Assess.*, 2003, **8**(2), 92–98.
- 40 D. Garraín, P. Martínez, R. Vidal and M. J. Bellés, In LCA of thermoplastics recycling, Proc. 3rd International Conference of Life Cycle Assessment. Zurich, Austria. <https://www.lcm2007.org/paper/168.pdf> accessed July, 2007; p 2008.
- 41 L. Rigamonti, M. Grosso and M. C. Sunseri, Influence of assumptions about selection and recycling efficiencies on the LCA of integrated waste management systems, *Int. J. Life Cycle Assess.*, 2009, **14**(5), 411–419.
- 42 P. N. Pressley, J. W. Levis, A. Damgaard, M. A. Barlaz and J. F. Decarolis, Analysis of material recovery facilities for use in life-cycle assessment, *Waste Manage.*, 2015, **35**, 307–317.
- 43 H. H. Khoo, LCA of plastic waste recovery into recycled materials, energy and fuels in Singapore, *Resour., Conserv. Recycl.*, 2019, **145**, 67–77.
- 44 A. Demetrious and E. Crossin, Life cycle assessment of paper and plastic packaging waste in landfill, incineration, and gasification-pyrolysis, *J. Mater. Cycles Waste Manage.*, 2019, **21**(4), 850–860.
- 45 S. Al-Salem, S. Evangelisti and P. Lettieri, Life cycle assessment of alternative technologies for municipal solid waste and plastic solid waste management in the Greater London area, *Chem. Eng. J.*, 2014, **244**, 391–402.
- 46 M. F. Cosate de Andrade, P. Souza, O. Cavalett and A. R. Morales, Life cycle assessment of poly (lactic acid)(PLA): Comparison between chemical recycling, mechanical recycling and composting, *J. Polym. Environ.*, 2016, **24**(4), 372–384.
- 47 D. Maga, M. Hiebel and N. Thonemann, Life cycle assessment of recycling options for polylactic acid, *Resour., Conserv. Recycl.*, 2019, **149**, 86–96.
- 48 N. Rudolph, R. Kiesel and C. Aumnate, *Understanding plastics recycling: Economic, ecological, and technical aspects of plastic waste handling*, Carl Hanser Verlag GmbH Co KG, 2020.



- 49 H. Jeswani, C. Krüger, M. Russ, M. Horlacher, F. Antony, S. Hann and A. Azapagic, Life cycle environmental impacts of chemical recycling via pyrolysis of mixed plastic waste in comparison with mechanical recycling and energy recovery, *Sci. Total Environ.*, 2021, **769**, 144483.
- 50 S. Kaza, L. Yao, P. Bhada-Tata and F. Van Woerden, *What a waste 2.0: a global snapshot of solid waste management to 2050*, World Bank Publications, 2018.
- 51 U.S.EPA Plastics: Material-Specific Data. <https://www.epa.gov/facts-and-figures-about-materials-waste-and-recycling/plastics-material-specific-data> (accessed Feb 02).
- 52 Parliament, E. Plastic waste and recycling in the EU: facts and figures. <https://www.europarl.europa.eu/news/en/headlines/society/20181212STO21610/plastic-waste-and-recycling-in-the-eu-facts-and-figures> (accessed Feb 1).
- 53 D. C. Wilson, L. Rodic, P. Modak, R. Soos, A. Carpintero, K. Velis, M. Iyer and O. Simonett, *Global waste management outlook*, UNEP, 2015.
- 54 Agency, U. S. E. P. Non-Hazardous Materials and Waste Management Hierarchy. <https://www.epa.gov/smm/sustainable-materials-management-non-hazardous-materials-and-waste-management-hierarchy> (accessed Dec 11).
- 55 C. A. Bareither, C. H. Benson, M. A. Barlaz, T. B. Edil and T. M. Tolaymat, Performance of North American bioreactor landfills. I: Leachate hydrology and waste settlement, *J. Environ. Eng.*, 2010, **136**(8), 824–838.
- 56 M. A. Barlaz, C. A. Bareither, A. Hossain, J. Saquing, I. Mezzari, C. H. Benson, T. M. Tolaymat and R. Yazdani, Performance of North American bioreactor landfills. II: Chemical and biological characteristics, *J. Environ. Eng.*, 2010, **136**(8), 839–853.
- 57 Agency, U. E. P. Basic information about landfill gas. <https://www.epa.gov/lmop/basic-information-about-landfill-gas> (accessed Dec 11).
- 58 R. R. Bora, R. Wang and F. You, Waste polypropylene plastic recycling toward climate change mitigation and circular economy: Energy, environmental, and techno-economic perspectives, *ACS Sustainable Chem. Eng.*, 2020, **8**(43), 16350–16363.
- 59 P. Kjeldsen, M. A. Barlaz, A. P. Rooker, A. Baun, A. Ledin and T. H. Christensen, Present and long-term composition of MSW landfill leachate: a review, *Crit. Rev. Environ. Sci. Technol.*, 2002, **32**(4), 297–336.
- 60 T. F. Stocker, D. Qin, G.-K. Plattner, M. Tignor, S. K. Allen, J. Boschung, A. Nauels, Y. Xia, V. Bex and P. M. Midgley, The physical science basis. Contribution of working group I to the fifth assessment report of the intergovernmental panel on climate change, *Comput. Geom.*, 2013, **18**(2), 95–123.
- 61 D. Mutz, D. Hengevoss, C. Hugl and T. Gross, *Waste-to-energy options in municipal solid waste management a guide for decision makers in developing and emerging countries*, Deutsche Gesellschaft für Internationale Zusammenarbeit (GIZ) GmbH, 2017.
- 62 D. Tonini, V. Martinez-Sanchez and T. F. Astrup, Material resources, energy, and nutrient recovery from waste: are waste refineries the solution for the future?, *Environ. Sci. Technol.*, 2013, **47**(15), 8962–8969.
- 63 G. Finnveden, A. Björklund, M. C. Reich, O. Eriksson and A. Sörbom, Flexible and robust strategies for waste management in Sweden, *Waste Manage.*, 2007, **27**(8), S1–S8.
- 64 T. Fruergaard and T. Astrup, Optimal utilization of waste-to-energy in an LCA perspective, *Waste Manage.*, 2011, **31**(3), 572–582.
- 65 L. Rigamonti, M. Grosso and L. Biganzoli, Environmental Assessment of Refuse-Derived Fuel Co-Combustion in a Coal-Fired Power Plant, *J. Ind. Ecol.*, 2012, **16**(5), 748–760.
- 66 A. Villar, J. J. Arribas and J. Parrondo, Waste-to-energy technologies in continuous process industries, *Clean Technol. Environ. Policy*, 2012, **14**(1), 29–39.
- 67 T. F. Astrup, D. Tonini, R. Turconi and A. Boldrin, Life cycle assessment of thermal Waste-to-Energy technologies: Review and recommendations, *Waste Manage.*, 2015, **37**, 104–115.
- 68 M. U. S. Jaganmohan, Waste Energy - Statistics & Facts. <https://www.statista.com/topics/3231/waste-energy-in-the-us/#dossierKeyfigures> (accessed Dec 08).
- 69 W. E. Council, *World energy resources: Waste to Energy*, World Energy Council London, 2016.
- 70 (UNEP), U. N. E. P, *Waste-to-Energy: Considerations for Informed Decision-Making*, 2019.
- 71 (EIA), U. S. E. I. A. U. S, Waste-to-energy (Municipal Solid Waste). <https://www.eia.gov/energyexplained/biomass/waste-to-energy.php> (accessed Dec 7).
- 72 (EPA), U. S. E. P. A. U. S, Energy Recovery from the Combustion of Municipal Solid Waste (MSW). <https://www.epa.gov/smm/energy-recovery-combustion-municipal-solid-waste-msw> (accessed Dec 9).
- 73 (OECD), O. f. E. C. a. D, Municipal Waste. [https://www.oecd-ilibrary.org/environment/data/oecd-environment-statistics/municipal-waste\\_data-00601-en](https://www.oecd-ilibrary.org/environment/data/oecd-environment-statistics/municipal-waste_data-00601-en) (accessed Dec 07).
- 74 EPA, U. National Overview: Facts and Figures on Materials, Wastes and Recycling. <https://www.epa.gov/facts-and-figures-about-materials-waste-and-recycling/national-overview-facts-and-figures-materials> (accessed Dec 06).
- 75 (DOE), U. S. D. o. E. U. S, Waste-to-Energy from Municipal Solid Wastes, 2019.
- 76 (WHO), W. H. O. Dioxins and their effects on human health. <https://www.who.int/news-room/fact-sheets/detail/dioxins-and-their-effects-on-human-health>. (accessed Feb 02).
- 77 A. Mukherjee, B. Debnath and S. K. Ghosh, A review on technologies of removal of dioxins and furans from incinerator flue gas, *Proc. Environ. Sci.*, 2016, **35**, 528–540.
- 78 Z. Hao, M. Sun, J. J. Ducoste, C. H. Benson, S. Luettich, M. J. Castaldi and M. A. Barlaz, Heat generation and accumulation in municipal solid waste landfills, *Environ. Sci. Technol.*, 2017, **51**(21), 12434–12442.
- 79 U.S.EPA, *Material Recovery Facilities for Municipal Solid Waste*, United States Environmental Protection Agency, 1991.



- 80 J. Pichtel, *Waste Management Practices: Municipal, Hazardous, and Industrial*, CRC Press, Boca Raton, FL, 2014, vol. 2.
- 81 M. L. Mastellone, R. Cremiato, L. Zaccariello and R. Lotito, Evaluation of performance indicators applied to a material recovery facility fed by mixed packaging waste, *Waste Manage.*, 2017, **64**, 3–11.
- 82 H. Damgacioglu, M. Hornilla, O. Bafail and N. Celik, Recovering value from single stream material recovery facilities – An outbound contamination analysis in Florida, *Waste Manage.*, 2020, **102**, 804–814.
- 83 D. J. Tonjes, O. Aphale, L. Clark and K. L. Thyberg, Conversion from dual stream to single stream recycling results in nuanced effects on revenues and waste stream amounts and composition, *Resour., Conserv. Recycl.*, 2018, **138**, 151–159.
- 84 G. C. Fitzgerald, J. S. Krones and N. J. Themelis, Greenhouse gas impact of dual stream and single stream collection and separation of recyclables, *Resour., Conserv. Recycl.*, 2012, **69**, 50–56.
- 85 C. Lakhan, A Comparison of Single and Multi-Stream Recycling Systems in Ontario, Canada, *Resources*, 2015, **4**(2), 384–397.
- 86 ISRI, *ISRI Scrap Specifications Circular 2021*, Institute of Scrap Recycling Industries, Washington, DC, 2021.
- 87 MRFF Flexible Packaging Recycling in Material Recovery Facilities Pilot. <https://www.materialsrecoveryforthefuture.com/wp-content/uploads/MRFF-Pilot-Report-2020-Final.pdf> (accessed 17 Dec 2021).
- 88 GBB *Supplemental Report: The Evolution of Mixed Waste Processing Facilities - Technology and Equipment Guide*, Gershman, Brickner & Bratton, Inc., The American Chemistry Council, Fairfax, VA, 2016, p. 32.
- 89 T. H. Christensen and B. Bilitewski, Mechanical Treatment: Material Recovery Facilities, in *Solid Waste Technology & Management*, ed. T. H. Christensen, John Wiley & Sons, Ltd, Chichester, 2010, pp. 349–362.
- 90 B. Bilitewski, Mechanical Treatment: Unit Processes, in *Solid Waste Technology & Management*, ed. T. H. Christensen, John Wiley & Sons, Ltd, Chichester, 2010, vol. 1, pp. 319–348.
- 91 J. Beigbeder, D. Perrin, J.-F. Mascaro and J.-M. Lopez-Cuesta, Study of the physico-chemical properties of recycled polymers from waste electrical and electronic equipment (WEEE) sorted by high resolution near infrared devices, *Resour., Conserv. Recycl.*, 2013, **78**, 105–114.
- 92 B. Eule, *Processing of Co-mingled Recyclate Material at UK Material Recycling Facilities (MRF)*, RWTH Aachen, Aachen, 2013.
- 93 K. Barker, Optical sorting advances are driving the MRF of the future. <https://www.recyclingproductnews.com/article/35838/optical-sorting-advances-are-driving-the-mrf-of-the-future> (accessed 09 Nov 2021).
- 94 Y. Zheng, J. Bai, J. Xu, X. Li and Y. Zhang, A discrimination model in waste plastics sorting using NIR hyper-spectral imaging system, *Waste Manage.*, 2018, **72**, 87–98.
- 95 G. Bonifazi and S. Serranti, in *Quality control by HyperSpectral Imaging (HSI) in solid waste recycling: logics, algorithms and procedures*, IS&T/SPIE Electronic Imaging, San Francisco, CA, SPIE: San Francisco, CA, 2014.
- 96 M. De Biasio, T. Arnold, G. McGunnigle, R. Leitner, D. Balthasar and V. Rehrmann, In *Detecting and discriminating PE and PP polymers for plastics recycling using NIR imaging spectroscopy*, SPIE Defense, Security, and Sensing, Orlando, FL, SPIE, Orlando, FL, 2010.
- 97 S. Zinchik, S. Jiang, S. Friis, F. Long, L. Høgstædt, V. M. Zavala and E. Bar-Ziv, Accurate Characterization of Mixed Plastic Waste Using Machine Learning and Fast Infrared Spectroscopy, *ACS Sustainable Chem. Eng.*, 2021, **9**(42), 14143–14151.
- 98 J. Xia, Y. Huang, Q. Li, Y. Xiong and S. Min, Convolutional neural network with near-infrared spectroscopy for plastic discrimination, *Environ. Chem. Lett.*, 2021, **19**(5), 3547–3555.
- 99 S. Zhu, H. Chen, M. Wang, X. Guo, Y. Lei and G. Jin, Plastic solid waste identification system based on near infrared spectroscopy in combination with support vector machine, *Adv. Ind. Eng. Polym. Res.*, 2019, **2**(2), 77–81.
- 100 W. A. Worrell and P. A. Vesling, *Solid Waste Engineering*, Cengage Learning, Stamford, CT, 2012.
- 101 H. Leverenz, G. Tchobanoglous and D. B. Spencer, Recycling, in *Handbook of Solid Waste Management*, ed. G. Tchobanoglous and F. Kreith, McGraw-Hill, New York, NY, 2002.
- 102 K. Maile, Baler basics. <https://www.recyclingtoday.com/article/baler-basics/> (accessed 09 Nov 2021).
- 103 APR Model Bale Specifications. <https://plasticsrecycling.org/model-bale-specifications> (accessed 09 Nov 2021).
- 104 Machinex Machinex Expands its Baler Range with the II ram Baler Series. <https://www.machinexrecycling.com/news/machinex-expands-baler-range-ii-ram-baler-series/> (accessed 11 Nov 2021).
- 105 RecyclingMarkets RecyclingMarkets.net. <https://www.recyclingmarkets.net> (accessed Feb 02).
- 106 U.S.EPA, *Advancing Sustainable Materials Management: 2018 Tables and Figures*, United States Environmental Protection Agency, 2020.
- 107 2020 U.S. Post-Consumer Plastic Recycling Survey. <https://www.lastbeachcleanup.org/usplasticrecyclingsurvey> (accessed 20 Oct 2021).
- 108 J. Hocevar, *Circular Claims Fall Flat: Comprehensive U.S. Survey of Plastics Recyclability*, Greenpeace, 2020.
- 109 D. Toto, The largest 75 MRFs in North America. <https://www.wastetodaymagazine.com/article/largest-north-american-material-recovery-facilities/> (accessed 11 Nov 2021).
- 110 WRAP Materials Facility Reporting Portal Q4 2019 – Commentary; Waste and Resources Action Programme, 2020.
- 111 M. Ali and P. Courtenay, Evaluating the progress of the UK's Material Recycling Facilities: A mini review, *Waste Manage. Res.*, 2014, **32**(12), 1149–1157.
- 112 COREPLA, *Rapporto di Sostenibilit  2020*; Consorzio Nazionale per la raccolta, il riciclo e il recupero degli imballaggi in plastica, Milan, Italy, 2020.



- 113 MISE, *Studio di fattibilità nell'ambito dell'Economia Circolare mirato al riciclo delle Plastiche Miste*, Ministero dello sviluppo economico, MISE (Italy), Roma, Italy, 2019.
- 114 Destatis Waste treatment plants 2019. <https://www.destatis.de/EN/Themes/Society-Environment/Environment/Waste-Management/Tables/waste-treatment-plants-2019.html> (accessed 11 Nov 2021).
- 115 ADEME, *Déchets chiffres-clés Édition 2020*; Agence de la transition écologique, Angers, France, 2020.
- 116 S. M. Dias, Waste pickers and cities, *Environ. Urban*, 2016, **28**(2), 375–390.
- 117 F. Gutierrez-Galicia, A. L. Coria-Paez, R. Tejeida-Padilla and E. F. Galicia-Haro, A System for the Inclusion of the Informal Recycling Sector (IRS) in Mexico City's Solid Waste Management, *Sustainability*, 2021, **13**(22), 12490.
- 118 M. Medina, Scavenger cooperatives in Asia and Latin America, *Resour., Conserv. Recycl.*, 2000, **31**(1), 51–69.
- 119 C. V. Santos and J. A. G. García, El papel de los pepenadores de materiales reciclables en la gestión de residuos sólidos: los casos de Brasil y México, *Revista Legislativa de Estudios Sociales y de Opinión Pública*, 2019, **12**(24), 87–114.
- 120 D. I. Noguera, *Life cycle assessment of PET bottle recycling: a case study for Mexico*, 2013.
- 121 M. Medina, Social Inclusion in Mexico's PET Plastic Recycling, 2013.
- 122 Análisis de costos de producción y márgenes del pet virgen y reciclado, 2011.
- 123 Compra venta de chatarra y reciclados por kilogramos, 2022.
- 124 P. Navarrete-Hernández and N. Navarrete-Hernández, Unleashing waste-pickers' potential: supporting recycling cooperatives in Santiago de Chile, *World Dev.*, 2018, **101**, 293–310.
- 125 O. Buenrostro and G. Bocco, Solid waste management in municipalities in Mexico: goals and perspectives, *Resour., Conserv. Recycl.*, 2003, **39**(3), 251–263.
- 126 V. Montiel-Corona and J. A. Guevara-García, Impulsando a México a una Cultura de Reciclaje, in *México Contemporáneo: aspectos económicos, políticos y sociales*, ed. U. Veracruzana, Universidad Veracruzana, 2018.
- 127 C. Silva-Chavez, D. Caro and M. Thomsen, Environmental Assessment of Alternatives for Biowaste Treatment in Mexico City, *Front. Energy Res.*, 2019, **7**, 30.
- 128 N. M. Jimenez-Martinez and R. Garcia-Barrios, The Zero Waste University Program in Mexico: A Model for Grassroots Innovations in Sustainability, *Sustainability*, 2020, **12**(22), 9444.
- 129 V. Montiel-Corona and J. Guevara-García, Impulsando a México a una Cultura de Reciclaje, in *México Contemporáneo: aspectos*, 2018.
- 130 C. S. Chávez, D. Caro and M. Thomsen, Environmental assessment of alternatives for biowaste treatment in Mexico City, *Front. Energy Res.*, 2019, **7**, 30.
- 131 A. Flores and O. Fairuz, *Policy mechanisms to reduce single-use plastic waste. Review of available options and their applicability in Mexico*, World Resources Institute Mexico, 2020, pp. 50.
- 132 Netherlands Enterprise Agency, *Market opportunities on Circular Economy in Mexico*, 2019.
- 133 Gobierno de México, LA LEY GENERAL DE ECONOMÍA CIRCULAR. Camara de Senadores, Ed. Gobierno de México: Diario Oficial de la Federación, 2021.
- 134 G. A. o. W. Pickers, Global Alliance of Waste Pickers. <https://globalrec.org/life-and-voices/> (accessed Aug 28).
- 135 Guidance for Industry: Use of Recycled Plastics in Food Packaging (Chemistry Considerations). U.S. Food and Drug (FDA), 2021.
- 136 N. Singh, D. Hui, R. Singh, I. P. S. Ahuja, L. Feo and F. Fraternali, Recycling of plastic solid waste: A state of art review and future applications, *Composites, Part B*, 2017, **115**, 409–422.
- 137 Mechanical Recycling; European Bioplastics (EUBP), 2020.
- 138 M. D. Jagtap, S. S. Khatavkar and T. Z. Quazi, Methods for Waste Plastic Recycling. International Journal on Recent Technologies in Mechanical and Electrical Engineering (IJRMEE) 2 (ISSN: 2349-7947), 120–122.
- 139 FDA, U., *Use of Recycled Plastics in Food Packaging: Chemistry Considerations*. Food and Drug Administration, Washington, DC, 2006.
- 140 N. Malik, P. Kumar, S. Shrivastava and S. B. Ghosh, An overview on PET waste recycling for application in packaging, *Int. J. Plast. Technol.*, 2017, **21**(1), 1–24.
- 141 C. Prakash, S. Singh, G. Krolczyk and B. Pabla, Advances in materials science and engineering, *Lect. Notes Mech. Eng.*, 2020, **10**, 978–981.
- 142 L. Fetters, D. Lohse, D. Richter, T. Witten and A. Zirkel, Connection between polymer molecular weight, density, chain dimensions, and melt viscoelastic properties, *Macromolecules*, 1994, **27**(17), 4639–4647.
- 143 R. H. Colby, L. J. Fetters and W. W. Graessley, The melt viscosity-molecular weight relationship for linear polymers, *Macromolecules*, 1987, **20**(9), 2226–2237.
- 144 R. W. Nunes, J. R. Martin and J. F. Johnson, Influence of molecular weight and molecular weight distribution on mechanical properties of polymers, *Polym. Eng. Sci.*, 1982, **22**(4), 205–228.
- 145 F. P. La Mantia, *Recycling of PVC and mixed plastic waste*, ChemTec Publishing, 1996.
- 146 M. Paci and F. La Mantia, Influence of small amounts of polyvinylchloride on the recycling of polyethyleneterephthalate, *Polym. Degrad. Stab.*, 1999, **63**(1), 11–14.
- 147 F. La Mantia, D. Curto and R. Scaffaro, Recycling of dry and wet polyamide 6, *J. Appl. Polym. Sci.*, 2002, **86**(8), 1899–1903.
- 148 P. Kumar, R. K. Yadav, R. Kumar and S. Maurya, Recycling of waste plastic using extrusion process.
- 149 K. P. Rajan, A. Gopanna and S. P. Thomas, A project based learning (PBL) Approach involving pet recycling in chemical engineering education, *Recycling*, 2019, **4**(1), 10.
- 150 B. Jabłońska, P. Kielbasa, M. Korenko and T. Drózd, Physical and chemical properties of waste from PET



- bottles washing as a component of solid fuels, *Energies*, 2019, **12**(11), 2197.
- 151 D. L. Gall, J. Ralph, T. J. Donohue and D. R. Noguera, A group of sequence-related sphingomonad enzymes catalyzes cleavage of  $\beta$ -aryl ether linkages in lignin  $\beta$ -guaiacyl and  $\beta$ -syringyl ether dimers, *Environ. Sci. Technol.*, 2014, **48**(20), 12454–12463.
  - 152 B. Brooks, K. Hays and L. Milner, *Plastics recycling, in PET and Europe lead the way*, 2019.
  - 153 S. Cruz and M. Zanin, PET recycling: Evaluation of the solid state polymerization process, *J. Appl. Polym. Sci.*, 2006, **99**(5), 2117–2123.
  - 154 F. Awaja and D. Pavel, Recycling of PET, *Eur. Polym. J.*, 2005, **41**(7), 1453–1477.
  - 155 Z. O. Schyns and M. P. Shaver, Mechanical recycling of packaging plastics: A review, *Macromol. Rapid Commun.*, 2021, **42**(3), 2000415.
  - 156 A. Brems, J. Baeyens, C. Vandecasteele and R. Dewil, Polymeric cracking of waste polyethylene terephthalate to chemicals and energy, *J. Air Waste Manage. Assoc.*, 2011, **61**(7), 721–731.
  - 157 M. Paci and F. P. La Mantia, Influence of small amounts of polyvinylchloride on the recycling of polyethyleneterephthalate, *Polym. Degrad. Stab.*, 1999, **63**(1), 11–14.
  - 158 G. W. Curtzwiler, E. B. Williams, A. L. Maples, N. W. Davis, T. L. Bahns, J. Eliseo De León and K. L. Vorst, Ultraviolet protection of recycled polyethylene terephthalate, *J. Appl. Polym. Sci.*, 2017, **134**(32), 45181.
  - 159 T. Kim and S. Jabarin, Solid-state polymerization of poly (ethylene terephthalate). II. Modeling study of the reaction kinetics and properties, *J. Appl. Polym. Sci.*, 2003, **89**(1), 213–227.
  - 160 M. Asensio, P. Esfandiari, K. Núñez, J. F. Silva, A. Marques, J. C. Merino and J. M. Pastor, Processing of pre-impregnated thermoplastic towpreg reinforced by continuous glass fibre and recycled PET by pultrusion, *Composites, Part B*, 2020, **200**, 108365.
  - 161 Unilever makes PET plastic breakthrough. <https://www.businessgrowthhub.com/green-technologies-and-services/green-intelligence/resource-library/unilever-makes-pet-plastic-breakthrough>.
  - 162 D. Toto, Indorama Ventures highlights sustainability achievements. <https://www.recyclingtoday.com/article/indorama-sustainability-report-2020-pet-recycling/>.
  - 163 Anonymous, *Guidance for industry: Use of recycled plastics in food packaging: Chemistry considerations*; U.S. Dept. of Health and Human Services, FDA, Center for Food Safety and Applied Nutrition, College Park, 2021.
  - 164 C. Marschik, B. Löw-Baselli and J. Miethlinger, in *Modeling devolatilization in single-and multi-screw extruders*, *AIP Conference Proceedings*, AIP Publishing LLC, 2017, p. 080006.
  - 165 S. Pachner, M. Aigner and J. Miethlinger, A heuristic method for modeling the initial pressure drop in melt filtration using woven screens in polymer recycling, *Polym. Eng. Sci.*, 2019, **59**(6), 1105–1113.
  - 166 M. Mousavi, *Territorial Environmental Modeling of Cement Concrete Demolition Waste (CCDW) Management with a Life Cycle Approach*, Loire Bretagne University, 2018.
  - 167 F. Tao, S. Dag, L.-W. Wang, Z. Liu, D. R. Butcher, H. Bluhm, M. Salmeron and G. A. Somorjai, Break-up of stepped platinum catalyst surfaces by high CO coverage, *Science*, 2010, **327**(5967), 850–853.
  - 168 rPET market to garner US \$12.5 billion by 2026. recycling magazine 2019.
  - 169 J. A. Brown, M. Alic and M. H. Gold, Manganese peroxidase gene transcription in *Phanerochaete chrysosporium*: Activation by manganese, *J. Bacteriol.*, 1991, **173**(13), 4101–4106.
  - 170 . 2020 PET RECYCLING REPORT. <https://napcor.com/reports-resources/>.
  - 171 Y. Wang, R. Song and D. Shen, Note: Enthalpy relaxation studies in amorphous poly (ethylene terephthalate) by Modulated DSC, *J. Macromol. Sci., Part B: Phys.*, 1998, **37**(5), 709–716.
  - 172 G. W. Curtzwiler, M. Schweitzer, Y. Li, S. Jiang and K. L. Vorst, Mixed post-consumer recycled polyolefins as a property tuning material for virgin polypropylene, *J. Cleaner Prod.*, 2019, **239**, 117978.
  - 173 G. W. Curtzwiler, E. B. Williams, E. Hurban, J. Greene and K. L. Vorst, Certification markers for empirical quantification of post-consumer recycled content in extruded polyethylene film, *Polym. Test.*, 2018, **65**, 103–110.
  - 174 S. Luzuriaga, J. Kovářová and I. Fortelný, Degradation of pre-aged polymers exposed to simulated recycling: properties and thermal stability, *Polym. Degrad. Stab.*, 2006, **91**(6), 1226–1232.
  - 175 J. M. Soto, G. Blázquez, M. Calero, L. Quesada, V. Godoy and M. Á. Martín-Lara, A real case study of mechanical recycling as an alternative for managing of polyethylene plastic film presented in mixed municipal solid waste, *J. Cleaner Prod.*, 2018, **203**, 777–787.
  - 176 Amut Friction Washer Cleans Contaminated PET Flakes. <https://www.recyclingtoday.com/article/amut-friction-recycled-pet-washing/>.
  - 177 Oh!, E. <https://www.ernestny.com/eco-oh.php> (accessed Feb 02).
  - 178 L. A. Pinheiro, M. A. Chinelatto and S. V. Canevarolo, The role of chain scission and chain branching in high density polyethylene during thermo-mechanical degradation, *Polym. Degrad. Stab.*, 2004, **86**(3), 445–453.
  - 179 P. Oblak, J. Gonzalez-Gutierrez, B. Zupančič, A. Aulova and I. Emri, Processability and mechanical properties of extensively recycled high density polyethylene, *Polym. Degrad. Stab.*, 2015, **114**, 133–145.
  - 180 K. Bhunia, S. S. Sablani, J. Tang and B. Rasco, Migration of chemical compounds from packaging polymers during microwave, conventional heat treatment, and storage, *Compr. Rev. Food Sci. Food Saf.*, 2013, **12**(5), 523–545.
  - 181 Diversion of waste from landfill in Europe. <https://www.eea.europa.eu/ims/diversion-of-waste-from-landfill>.



- 182 Anonymous Advancing Sustainable Materials Management: 2018 Fact Sheet. [https://www.epa.gov/sites/production/files/2021-01/documents/2018\\_ff\\_fact\\_sheet\\_dec\\_2020\\_fnl\\_508.pdf](https://www.epa.gov/sites/production/files/2021-01/documents/2018_ff_fact_sheet_dec_2020_fnl_508.pdf) (accessed 28 April).
- 183 S. Camarero, O. Garcia, T. Vidal, J. Colom, J. C. del Río, A. Gutiérrez, J. M. Gras, R. Monje, M. J. Martinez and Á. T Martinez, Efficient bleaching of non-wood high-quality paper pulp using laccase-mediator system, *Enzyme Microb. Technol.*, 2004, **35**(2–3), 113–120.
- 184 Z. Wen, Y. Xie, M. Chen and C. D. Dinga, China's plastic import ban increases prospects of environmental impact mitigation of plastic waste trade flow worldwide, *Nat. Commun.*, 2021, **12**(1), 1–9.
- 185 F. G. Calvo-Flores and J. A. Dobado, Lignin as renewable raw material, *ChemSusChem*, 2010, **3**(11), 1227–1235.
- 186 Plastics – the Facts 2019, 2019.
- 187 Recycled Plastics in Food Packaging, 2020.
- 188 T. D. Bugg, M. Ahmad, E. M. Hardiman and R. Rahmanpour, Pathways for degradation of lignin in bacteria and fungi, *Nat. Prod. Rep.*, 2011, **28**(12), 1883–1896.
- 189 Food Packaging Regulation in the US; foodpackaging-forum, 2013.
- 190 FDA, *Recycled Plastics in Food Packaging*, FDA, 2020.
- 191 K. A. Fenlon, A. C. Johnson, C. R. Tyler and E. M. Hill, Gas-liquid chromatography-tandem mass spectrometry methodology for the quantitation of estrogenic contaminants in bile of fish exposed to wastewater treatment works effluents and from wild populations, *J. Chromatogr., A*, 2010, **1217**(1), 112–118.
- 192 Anonymous Submissions on Post-Consumer Recycled (PCR) Plastics for Food-Contact Articles. [https://www.cfsanappsexternal.fda.gov/scripts/fdc/?set=RecycledPlastics&sort=Date\\_of\\_NOL&order=ASC&type=basic&search=](https://www.cfsanappsexternal.fda.gov/scripts/fdc/?set=RecycledPlastics&sort=Date_of_NOL&order=ASC&type=basic&search=) (accessed 11 January).
- 193 M. Lorber, A. Schecter, O. Paepke, W. Shropshire, K. Christensen and L. Birnbaum, Exposure assessment of adult intake of bisphenol A (BPA) with emphasis on canned food dietary exposures, *Environ. Int.*, 2015, **77**, 55–62.
- 194 V. S. Cecon, P. F. Da Silva, G. W. Curtzwiler and K. L. Vorst, The challenges in recycling post-consumer polyolefins for food contact applications: A review, *Resour., Conserv. Recycl.*, 2021, **167**, 105422.
- 195 M. G. Davidson, R. A. Furlong and M. C. McManus, Developments in the life cycle assessment of chemical recycling of plastic waste e A review, *J. Cleaner Prod.*, 2021, **293**, 126163.
- 196 R. K. Singh and B. Ruj, Time and temperature depended fuel gas generation from pyrolysis of real world municipal plastic waste, *Fuel*, 2016, **174**, 164–171.
- 197 H. J. Rubel, U. Jung, C. Follette, A. Meyer zum Felder, S. Appathurai and M. Benedi Diaz, *A Circular Solution to Plastic Waste*, Boston Consulting Group, 2019.
- 198 H. Jeswani, C. Kruger, M. Russ, M. Horlacher, F. Antony, S. Hann and A. Azapagic, Life cycle environmental impacts of chemical recycling via pyrolysis of mixed plastic waste in comparison with mechanical recycling and energy recovery, *Sci. Total Environ.*, 2021, **769**, 15.
- 199 W. Kaminsky and I. J. N. Zorriquetta, Catalytical and thermal pyrolysis of polyolefins, *J. Anal. Appl. Pyrolysis*, 2007, **79**(1–2 SPEC. ISS.), 368–374.
- 200 D. Zhao, X. Wang, J. B. Miller and G. W. Huber, The Chemistry and Kinetics of Polyethylene Pyrolysis: A Process to Produce Fuels and Chemicals, *ChemSusChem*, 2020, **13**(7), 1764–1774.
- 201 Y. Xue, P. Johnston and X. Bai, Effect of catalyst contact mode and gas atmosphere during catalytic pyrolysis of waste plastics, *Energy Convers. Manage.*, 2017, **142**, 441–451.
- 202 Y. Xue, S. Zhou, R. C. Brown, A. Kelkar and X. Bai, Fast pyrolysis of biomass and waste plastic in a fluidized bed reactor, *Fuel*, 2015, **156**, 40–46.
- 203 M. L. Mastellone, F. Perugini, M. Ponte and U. Arena, Fluidized bed pyrolysis of a recycled polyethylene, *Polym. Degrad. Stab.*, 2002, **76**(3), 479–487.
- 204 T. Kuroki, T. Sawaguchi, S. Niikuni and T. Ikemura, Mechanism for Long-Chain Branching in the Thermal Degradation of Linear High-Density Polyethylene, *Macromolecules*, 1982, **15**(6), 1460–1464.
- 205 L. Cheng, J. Gu, Y. Wang, J. Zhang, H. Yuan and Y. Chen, Polyethylene high-pressure pyrolysis: Better product distribution and process mechanism analysis, *Chem. Eng. J.*, 2020, **385**(September 2019), 123866–123866.
- 206 C. Berruero, E. J. Mastral, E. Esperanza and J. Ceamanos, Production of waxes and tars from the continuous pyrolysis of high density polyethylene. Influence of operation variables, *Energy Fuels*, 2002, **16**(5), 1148–1153.
- 207 S. H. Jung, M. H. Cho, B. S. Kang and J. S. Kim, Pyrolysis of a fraction of waste polypropylene and polyethylene for the recovery of BTX aromatics using a fluidized bed reactor, *Fuel Process. Technol.*, 2010, **91**(3), 277–284.
- 208 P. J. Donaj, W. Kaminsky, F. Buzeto and W. Yang, Pyrolysis of polyolefins for increasing the yield of monomers' recovery, *Waste Manage.*, 2012, **32**(5), 840–846.
- 209 A. Aboulkas, K. El harfi and A. El Bouadili, Thermal degradation behaviors of polyethylene and polypropylene. Part I: Pyrolysis kinetics and mechanisms, *Energy Convers. Manage.*, 2010, **51**(7), 1363–1369.
- 210 L. A. Wall and S. Straus, Pyrolysis of polyolefins, *J. Polym. Sci.*, 1960, **44**(144), 313–323.
- 211 J. D. Peterson, S. Vyazovkin and C. A. Wight, Kinetics of the Thermal and Thermo-Oxidative Degradation of Polystyrene, Polyethylene and Poly(propylene), *Macromol. Chem. Phys.*, 2001, **202**(6), 775–784.
- 212 R. W. J. Westerhout, J. Waanders, J. A. M. Kuipers and W. P. M. van Swaaij, Kinetics of the Low-Temperature Pyrolysis of Polyethene, Polypropene, and Polystyrene Modeling, Experimental Determination, and Comparison with Literature Models and Data, *Ind. Eng. Chem. Res.*, 1997, **36**(6), 1955–1964.
- 213 A. Marcilla, M. I. Beltrán and R. Navarro, Evolution of products during the degradation of polyethylene in a batch reactor, *J. Anal. Appl. Pyrolysis*, 2009, **86**(1), 14–21.



- 214 E. Kiran and J. K. Gillham, Pyrolysis–molecular weight chromatography: A new on–line system for analysis of polymers. II. Thermal decomposition of polyolefins: Polyethylene, polypropylene, polyisobutylene, *J. Appl. Polym. Sci.*, 1976, **20**(8), 2045–2068.
- 215 H. Bockhorn, A. Hornung, U. Hornung, P. Jakobströer and M. Kraus, Dehydrochlorination of plastic mixtures, *J. Anal. Appl. Pyrolysis*, 1999, **49**(1), 97–106.
- 216 R. P. Lattimer and W. J. Kroenke, Mechanisms of formation of volatile aromatic pyrolyzates from poly(vinyl chloride), *J. Appl. Polym. Sci.*, 1982, **27**(4), 1355–1366.
- 217 Y. Tsuchiya and K. Sumi, Thermal decomposition products of polypropylene, *J. Polym. Sci., Part A: Polym. Chem.*, 1969, **7**(7), 1599–1607.
- 218 R. P. Lattimer, Pyrolysis field ionization mass spectrometry of hydrocarbon polymers, *J. Anal. Appl. Pyrolysis*, 1997, **39**(2), 115–127.
- 219 Y. Matsuzawa, M. Ayabe, J. Nishino, N. Kubota and M. Motegi, Evaluation of char fuel ratio in municipal pyrolysis waste, *Fuel*, 2004, **83**(11–12), 1675–1687.
- 220 J. Yu, L. Sun, C. Ma, Y. Qiao and H. Yao, Thermal degradation of PVC: A review, *Waste Manage.*, 2016, **48**, 300–314.
- 221 V. V. Krongauz, Y. P. Lee and A. Bourassa, Kinetics of thermal degradation of poly(vinyl chloride): Thermogravimetry and spectroscopy, *J. Therm. Anal. Calorim.*, 2011, **106**(1), 139–149.
- 222 L. Dean, Z. Dafei and Z. Deren, Mechanism and kinetics of thermo-dehydrochlorination of poly(vinyl chloride), *Polym. Degrad. Stab.*, 1988, **22**(1), 31–41.
- 223 T. Y. Xie, A. E. Hamielec, M. Rogestadt and T. Hjertberg, Experimental investigation of vinyl chloride polymerization at high conversion: polymer microstructure and thermal stability and their relationship to polymerization conditions, *Polymer*, 1994, **35**(7), 1526–1534.
- 224 W. H. Starnes, Structural and mechanistic aspects of the thermal degradation of poly(vinyl chloride), *Prog. Polym. Sci.*, 2002, **27**(10), 2133–2170.
- 225 W. H. Starnes, Overview and assessment of recent research on the structural defects in poly(vinyl chloride), *Polym. Degrad. Stab.*, 2012, **97**(9), 1815–1821.
- 226 B. B. Troitskii, A. S. Yakhnov, M. A. Novikova, T. G. Ganyukhina and V. N. Denisova, Effect of tacticity on thermal degradation of poly(vinyl chloride), *Eur. Polym. J.*, 1997, **33**(4), 505–511.
- 227 W. H. Starnes and X. Ge, Mechanism of Autocatalysis in the Thermal Dehydrochlorination of Poly(vinyl chloride), *Macromolecules*, 2004, **37**(2), 352–359.
- 228 V. M. Yanborisov and S. S. Borisevich, Quantum-chemical modeling of the mechanism of autocatalytic dehydrochlorination of PVC, *Theor. Exp. Chem.*, 2005, **41**(6), 352–358.
- 229 T. Hjertberg and E. Sörvik, *Thermal degradation of PVC. In Degradation and Stabilisation of PVC*, Springer, 1984, pp. 21–79.
- 230 I. C. McNeill, L. Memetea and W. J. Cole, A study of the products of PVC thermal degradation, *Polym. Degrad. Stab.*, 1995, **49**(1), 181–191.
- 231 L. Ye, T. Li and L. Hong, Understanding enhanced char formation in the thermal decomposition of PVC resin: Role of intermolecular chlorine loss, *Mater. Today Commun.*, 2021, **26**, 102186.
- 232 J. Huang, X. Li, G. Zeng, X. Cheng, H. Tong and D. Wang, Thermal decomposition mechanisms of poly(vinyl chloride): A computational study, *Waste Manage.*, 2018, **76**, 483–496.
- 233 A. Lopez-Uriónabarrenechea, I. De Marco, B. M. Caballero, M. F. Laresgoiti and A. Adrados, Catalytic stepwise pyrolysis of packaging plastic waste, *J. Anal. Appl. Pyrolysis*, 2012, **96**, 54–62.
- 234 A. Guyot, Recent developments in the thermal degradation of polystyrene—A review, *Polym. Degrad. Stab.*, 1986, **15**(3), 219–235.
- 235 L. A. Wall, S. Straus, R. E. Florin and L. J. Fetters, Pyrolysis of anionic and thermally prepared polystyrenes, *J. Res. Natl. Bur. Stand., Sect. A*, 1973, **77**(1), 157–157.
- 236 G. G. Cameron and G. P. Kerr, Thermal degradation of polystyrene-II the role of abnormalities, *Eur. Polym. J.*, 1970, **6**(2), 423–433.
- 237 L. Costa, G. Camino, A. Guyot, M. Bert and A. Chiotis, The rôle of chain ends in the thermal degradation of anionic polystyrene, *Polym. Degrad. Stab.*, 1982, **4**(4), 245–260.
- 238 J. Huang, X. Li, H. Meng, H. Tong, X. Cai and J. Liu, Studies on pyrolysis mechanisms of syndiotactic polystyrene using DFT method, *Chem. Phys. Lett.*, 2020, **747**(January), 137334–137334.
- 239 A. Rahimi and J. M. García, Chemical recycling of waste plastics for new materials production, *Nat. Rev. Chem.*, 2017, **1**(6), 0046.
- 240 L. H. Buxbaum, The Degradation of Poly(ethylene terephthalate), *Angew. Chem., Int. Ed. Engl.*, 1968, **7**(3), 182–190.
- 241 G. Montaudo, C. Puglisi and F. Samperi, Primary thermal degradation mechanisms of PET and PBT, *Polym. Degrad. Stab.*, 1993, **42**(1), 13–28.
- 242 J. Huang, H. Meng, X. Luo, X. Mu, W. Xu, L. Jin and B. Lai, Insights into the thermal degradation mechanisms of polyethylene terephthalate dimer using DFT method, *Chemosphere*, 2022, **291**, 133112.
- 243 B. J. Holland and J. N. Hay, The thermal degradation of poly(vinyl acetate) measured by thermal analysis–Fourier transform infrared spectroscopy, *Polymer*, 2002, **43**(8), 2207–2211.
- 244 H. H. G. Jellinek, Thermal Degradation of Polystyrene and Polyethylene. Part III, *Journal of Polymer Science*, 1949, **4**, 13–36.
- 245 G. Lopez, M. Artetxe, M. Amutio, J. Bilbao and M. Olazar, Thermochemical routes for the valorization of waste polyolefinic plastics to produce fuels and chemicals. A review, *Renewable Sustainable Energy Rev.*, 2017, **73**, 346–368.
- 246 S. M. Al-Salem, A. Antelava, A. Constantinou, G. Manos and A. Dutta, A review on thermal and catalytic pyrolysis of plastic solid waste (PSW), *J. Environ. Manage.*, 2017, **197**, 177–198.



- 247 E. A. W. Williams and T. Paul, The Pyrolysis of Individual Plastics and a Plastic Mixture in a Fixed Bed Reactor, *J. Chem. Technol. Biotechnol.*, 1997, **70**, 9–20.
- 248 U. R. Gracida-Alvarez, M. K. Mitchell, J. C. Sacramento-Rivero and D. R. Shonnard, Effect of Temperature and Vapor Residence Time on the Micropyrolysis Products of Waste High Density Polyethylene, *Ind. Eng. Chem. Res.*, 2018, **57**(6), 1912–1923.
- 249 J. M. Russell, U. R. Gracida-Alvarez, O. Winjobi and D. R. Shonnard, Update to “Effect of Temperature and Vapor Residence Time on the Micropyrolysis Products of Waste High Density Polyethylene”, *Ind. Eng. Chem. Res.*, 2020, **59**(22), 10716–10719.
- 250 D. G. Kulas, A. Zolghadr and D. Shonnard, Micropyrolysis of Polyethylene and Polypropylene Prior to Bioconversion: The Effect of Reactor Temperature and Vapor Residence Time on Product Distribution, *ACS Sustainable Chem. Eng.*, 2021, **9**(43), 14443–14450.
- 251 G. W. Meindersma, *Extraction of aromatics from naphtha with ionic liquids : from solvent development to pilot RDC evaluation*, 2005.
- 252 D. Zhao, X. Wang, J. B. Miller and G. W. Huber, The Chemistry and Kinetics of Polyethylene Pyrolysis: A Process to Produce Fuels and Chemicals, *ChemSusChem*, 2020, **13**, 1764–1774.
- 253 I. Velghe, R. Carleer, J. Yperman and S. Schreurs, Study of the pyrolysis of municipal solid waste for the production of valuable products, *J. Anal. Appl. Pyrolysis*, 2011, **92**(2), 366–375.
- 254 J. A. Conesa, R. Font, A. Marcilla and A. N. Garcia, Pyrolysis of Polyethylene in a Fluidized Bed Reactor, *Energy Fuels*, 1994, **8**(6), 1238–1246.
- 255 S. D. Anuar Sharuddin, F. Abnisa, W. M. A. Wan Daud and M. K. Aroua, A review on pyrolysis of plastic wastes, *Energy Convers. Manage.*, 2016, **115**, 308–326.
- 256 F. J. Mastral, E. Esperanza, C. Berruenco, M. Juste and J. Ceamanos, Fluidized bed thermal degradation products of HDPE in an inert atmosphere and in air-nitrogen mixtures, *J. Anal. Appl. Pyrolysis*, 2003, **70**(1), 1–17.
- 257 D. Zhao, X. Wang, J. B. Miller and G. W. Huber, The Chemistry and Kinetics of Polyethylene Pyrolysis: A Process to Produce Fuels and Chemicals, *ChemSusChem*, 2020, **13**(7), 1764–1774.
- 258 A. López, I. De Marco, B. M. Caballero, M. F. Laresgoiti and A. Adrados, Influence of time and temperature on pyrolysis of plastic wastes in a semi-batch reactor, *Chem. Eng. J.*, 2011, **173**(1), 62–71.
- 259 S. Orozco, J. Alvarez, G. Lopez, M. Artetxe, J. Bilbao and M. Olazar, Pyrolysis of plastic wastes in a fountain confined conical spouted bed reactor: Determination of stable operating conditions, *Energy Convers. Manage.*, 2021, **229**, 113768.
- 260 M. Sogancioglu, G. Ahmetli and E. Yel, A Comparative Study on Waste Plastics Pyrolysis Liquid Products Quantity and Energy Recovery Potential, *Energy Procedia*, 2017, **118**, 221–226.
- 261 L. Soják, R. Kubinec, H. Jurdáková, E. Hájeková and M. Bajus, High resolution gas chromatographic-mass spectrometric analysis of polyethylene and polypropylene thermal cracking products, *J. Anal. Appl. Pyrolysis*, 2007, **78**(2), 387–399.
- 262 A. Demirbas, Pyrolysis of municipal plastic wastes for recovery of gasoline-range hydrocarbons, *Journal of Analytical Applied Pyrolysis*, 2004, **79**, 97–102.
- 263 K. H. Lee, Pyrolysis of municipal plastic wastes separated by difference of specific gravity, *J. Anal. Appl. Pyrolysis*, 2007, **79**, 362–367.
- 264 O. Dogu, M. Pelucchi, R. Van de Vijver, P. H. Van Steenberge, D. R. D’hooge, A. Cuoci, M. Mehl, A. Frassoldati, T. Faravelli and K. M. Van Geem, The chemistry of chemical recycling of solid plastic waste via pyrolysis and gasification: State-of-the-art, challenges, and future directions, *Prog. Energy Combust. Sci.*, 2021, **84**, 100901.
- 265 R. Miandad, M. A. Barakat, A. S. Aburizaiza, M. Rehan, I. M. I. Ismail and A. S. Nizami, Effect of plastic waste types on pyrolysis liquid oil, *Int. Biodeterior. Biodegrad.*, 2017, **119**, 239–252.
- 266 I. Maafa, Pyrolysis of Polystyrene Waste: A Review, *Polymers*, 2021, **13**(2), 225.
- 267 Y. S. Kim, G. C. Hwang, S. Y. Bae, S. C. Yi, S. K. Moon and H. Kumazawa, Pyrolysis of polystyrene in a batch-type stirred vessel, *Korean J. Chem. Eng.*, 1999, **16**(2), 161–165.
- 268 J. A. Onwudili, N. Insura, and P. T. Williams, Composition of products from the pyrolysis of polyethylene and polystyrene in a closed batch reactor: Effects of temperature and residence time, *J. Anal. Appl. Pyrolysis*, 2009, **86**, 293–303.
- 269 Y. Liu, J. Qian and J. Wang, Pyrolysis of polystyrene waste in a fluidized-bed reactor to obtain styrene monomer and gasoline fraction, *Fuel Process. Technol.*, 2000, **63**(1), 45–55.
- 270 Y. Mo, L. Zhao, Z. Wang, C.-L. Chen, G.-Y. A. Tan and J.-Y. Wang, Enhanced styrene recovery from waste polystyrene pyrolysis using response surface methodology coupled with Box–Behnken design, *Waste Manage.*, 2014, **34**(4), 763–769.
- 271 H.-W. B. Wong and J. Linda, Tertiary Resource Recovery from Waste Polymers via Pyrolysis: Neat and Binary Mixture Reactions of Polypropylene and Polystyrene, *Ind. Eng. Chem. Res.*, 2001, **40**, 4716–4723.
- 272 C. Bradley, What’s Happening in Advanced Recycling Now. <https://www.plasticstoday.com/advanced-recycling/whats-happening-advanced-recycling-now> (accessed January 15).
- 273 A. B. J. Brems, C. Vandecasteele and R. Dewil, Polymeric Cracking of Waste Polyethylene Terephthalate to Chemicals and Energy, *J. Air Waste Manage. Assoc.*, 2011, **61**(7), 721–731.
- 274 P. Das and P. Tiwari, Thermal degradation study of waste polyethylene terephthalate (PET) under inert and oxidative environments, *Thermochim. Acta*, 2019, **679**, 178340.



- 275 M. S. Qureshi, A. Oasmaa, H. Pihkola, I. Deviatkin, A. Tenhunen, J. Mannila, H. Minkkinen, M. Pohjakallio and J. Laine-Ylijoki, Pyrolysis of plastic waste: Opportunities and challenges, *J. Anal. Appl. Pyrolysis*, 2020, **152**, 104804.
- 276 H. Jia, H. Ben, Y. Luo and R. Wang, Catalytic Fast Pyrolysis of Poly (Ethylene Terephthalate) (PET) with Zeolite and Nickel Chloride, *Polymers*, 2020, **12**(3), 705.
- 277 P. T. Williams and E. Slaney, Analysis of products from the pyrolysis and liquefaction of single plastics and waste plastic mixtures, *Resour., Conserv. Recycl.*, 2007, **51**(4), 754–769.
- 278 H. Almohamadi, M. Alamoudi, U. Ahmed, R. Shamsuddin and K. Smith, Producing hydrocarbon fuel from the plastic waste: Techno-economic analysis, *Korean J. Chem. Eng.*, 2021, **38**(11), 2208–2216.
- 279 A. H. Tullo, Plastic has a problem; is chemical recycling the solution? <https://cen.acs.org/environment/recycling/Plastic-problem-chemical-recycling-solution/97/i39> (accessed January 15).
- 280 T. Thiounn and R. C. Smith, Advances and approaches for chemical recycling of plastic waste, *Journal of Polymer Science*, 2020, **58**(10), 1347–1364.
- 281 N. George and T. Kurian, Recent Developments in the Chemical Recycling of Postconsumer Poly(ethylene terephthalate) Waste, *Ind. Eng. Chem. Res.*, 2014, **53**(37), 14185–14198.
- 282 H. S. Wu, Strategic Possibility Routes of Recycled PET, *Polymers*, 2021, **13**(9), 1475.
- 283 W. Kaminsky, Chemical recycling of plastics by fluidized bed pyrolysis, *Fuel Communications*, 2021, **8**, 100023.
- 284 N. Miskolczi, L. Bartha and A. Angyal, Pyrolysis of Polyvinyl Chloride (PVC)-Containing Mixed Plastic Wastes for Recovery of Hydrocarbons, *Energy Fuels*, 2009, **23**(5), 2743–2749.
- 285 A. Buekens, Introduction to Feedstock Recycling of Plastics, in *Feedstock Recycling and Pyrolysis of Waste Plastics: Converting Waste Plastics into Diesel and Other Fuels*, John Wiley & Sons, Ltd, 2006.
- 286 A. López, I. De Marco, B. M. Caballero, M. F. Laresgoiti and A. Adrados, Dechlorination of fuels in pyrolysis of PVC containing plastic wastes, *Fuel Process. Technol.*, 2011, **92**(2), 253–260.
- 287 J. Scheirs and W. Kaminsky, *Feedstock Recycling and Pyrolysis of Waste Plastics: Converting Waste Plastics into Diesel and Other Fuels*, John Wiley & Sons, Ltd, 2006.
- 288 W. Kaminsky and H. Sinn, Pyrolysis of plastic waste and scrap tires using a fluidized-bed process, in *Thermal Conversion of Solid Wastes and Biomass*, ed. A. C. Society, 1980, vol. 130, pp. 423–439.
- 289 H. R. Sinn, W. Kaminsky and J. R. Janning, Processing of Plastic Waste and Scrap Tires into Chemical Raw Materials, Especially by Pyrolysis, *Angew. Chem., Int. Ed. Engl.*, 1976, **15**(11), 660–672.
- 290 W. Chen, S. Shi, J. Zhang, M. Chen and X. Zhou, Co-pyrolysis of waste newspaper with high-density polyethylene: Synergistic effect and oil characterization, *Energy Convers. Manage.*, 2016, **112**, 41–48.
- 291 D. V. Suriapparao, A. Yerrayya, G. Nagababu, R. K. Guduru and T. H. Kumar, Recovery of renewable aromatic and aliphatic hydrocarbon resources from microwave pyrolysis/co-pyrolysis of agro-residues and plastics wastes, *Bioresour. Technol.*, 2020, **318**, 124277.
- 292 B. B. Uzoejinwa, X. He, S. Wang, A. E. F. Abomohra, Y. Hu and Q. Wang, Co-pyrolysis of biomass and waste plastics as a thermochemical conversion technology for high-grade biofuel production: Recent progress and future directions elsewhere worldwide, *Energy Convers. Manage.*, 2018, **163**, 468–492.
- 293 Z. B. Wang, G. Kiran, T. Lei and A. K. Gupta, Co-pyrolysis of waste plastic and solid biomass for synergistic production of biofuels and chemicals - A review, *Prog. Energy Combust. Sci.*, 2021, **84**, 100899.
- 294 W. Ścierański, Migration of Sulfur and Nitrogen in the Pyrolysis Products of Waste and Contaminated Plastics, *Appl. Sci.*, 2021, **11**(10), 4374.
- 295 N. Sakthipriya, Plastic waste management: A road map to achieve circular economy and recent innovations in pyrolysis, *Sci. Total Environ.*, 2022, **809**, 151160.
- 296 L. Mingxing, W. Mei, L. Zelong and Z. Qundan, Qualitative and Quantitative Analysis of Silicon Species in Pyrolysis Oil From Waste Plastic, *Acta Pet. Sin.*, 2021, **37**(4), 909.
- 297 T. Bhaskar, T. Matsui, J. Kaneko, M. A. Uddin, A. Muto and Y. Sakata, Novel calcium based sorbent (Ca-C) for the dehalogenation (Br, Cl) process during halogenated mixed plastic (PP/PE/PS/PVC and HIPS-Br) pyrolysis, *Green Chem.*, 2002, **4**(4), 372–375.
- 298 T. A. U. M. Bhaskar, J. Kaneko, T. Matsui, A. Muto and Y. Sakata, Pyrolysis of Polypropylene/Polyethylene/Polystyrene and Polyvinylchloride Mixed Plastics using CaCO<sub>3</sub>, *Prog. Rubber, Plast. Recycl. Technol.*, 2004, **20**(2), 163–170.
- 299 B. Dou, J. Gao, S. W. Baek and X. Sha, High-Temperature HCl Removal with Sorbents in a Fixed-Bed Reactor, *Energy Fuels*, 2003, **17**(4), 874–878.
- 300 Y. Sakata, M. A. Uddin, K. Koizumi and K. Murata, Thermal degradation of polyethylene mixed with poly(vinyl chloride) and poly(ethyleneterephthalate), *Polym. Degrad. Stab.*, 1996, **53**(1), 111–117.
- 301 M. A. Uddin, Y. Sakata, Y. Shiraga, A. Muto and K. Murata, Dechlorination of Chlorine Compounds in Poly(vinyl chloride) Mixed Plastics Derived Oil by Solid Sorbents, *Ind. Eng. Chem. Res.*, 1999, **38**(4), 1406–1410.
- 302 M. Fukushima, B. Wu, H. Ibe, K. Wakai, E. Sugiyama, H. Abe, K. Kitagawa, S. Tsuruga, K. Shimura and E. Ono, Study on dechlorination technology for municipal waste plastics containing polyvinyl chloride and polyethylene terephthalate, *J. Mater. Cycles Waste Manage.*, 2010, **12**, 108–122.
- 303 A. Soler, J. Conesa and N. Ortuño, Application of Subcritical Water to Dechlorinate Polyvinyl Chloride Electric Wires, *Energies*, 2018, **11**(10), 2612.



- 304 A. Lopez-Urionabarrenechea, I. De Marco, B. M. Caballero, M. F. Laresgoiti and A. Adrados, Upgrading of chlorinated oils coming from pyrolysis of plastic waste, *Fuel Process. Technol.*, 2015, **137**, 229–239.
- 305 M. Kusenbergh, A. Eschenbacher, M. R. Djokic, A. Zayoud, K. Ragaert, S. De Meester and K. M. Van Geem, Opportunities and challenges for the application of post-consumer plastic waste pyrolysis oils as steam cracker feedstocks: To decontaminate or not to decontaminate?, *Waste Manage.*, 2022, **138**, 83–115.
- 306 J. Brock, V. Valerie and G. John, The recycling myth - Big oil's solution for plastic waste littered with failure. <https://www.reuters.com/investigates/special-report/environment-plastic-oil-recycling/> (accessed 14 January).
- 307 A. B. Koc and Y. Ali, Catalytic and thermal oxidative pyrolysis of LDPE in a continuous reactor system, *J. Anal. Appl. Pyrolysis*, 2007, **78**(1), 7–13.
- 308 R. C. Brown, Process Intensification through Directly Coupled Autothermal Operation of Chemical Reactors, *Joule*, 2020, **4**(11), 2268–2289.
- 309 J. P. Polin, C. A. Peterson, L. E. Whitmer, R. G. Smith and R. C. Brown, Process intensification of biomass fast pyrolysis through autothermal operation of a fluidized bed reactor, *Appl. Energy*, 2019, **249**, 276–285.
- 310 M. Y. Wey, C. S. Lo, S. Y. Wu and Y. T. Lee, Operating parameters of autothermal pyrolysis of plastic waste in a fluidized bed, *Waste Manage. Res.*, 1998, **16**(1), 72–81.
- 311 M. Gholizadeh, C. Li, S. Zhang, Y. Wang, S. Niu, Y. Li and X. Hu, Progress of the development of reactors for pyrolysis of municipal waste, *Sustainable Energy Fuels*, 2020, **4**(12), 5885–5915.
- 312 E. Butler, G. Devlin and K. McDonnell, Waste Polyolefins to Liquid Fuels via Pyrolysis: Review of Commercial State-of-the-Art and Recent Laboratory Research, *Waste Biomass Valorization*, 2011, **2**(3), 227–255.
- 313 D. Chen, L. Yin, H. Wang and P. He, Pyrolysis technologies for municipal solid waste: A review, *Waste Manage.*, 2014, **34**(12), 2466–2486.
- 314 S. H. Gebre, M. G. Sendeku and M. Bahri, Recent Trends in the Pyrolysis of Non-Degradable Waste Plastics, *ChemistryOpen*, 2021, **10**(12), 1202–1226.
- 315 D. Kunii and O. Levenspiel, in *Fluidization Engineering*, Butterworth-Heinemann, 2nd edn, 1991.
- 316 W. Kaminsky, The Hamburg Fluidized-bed Pyrolysis Process to Recycle Polymer Wastes and Tires, in *Feedstock Recycling and Pyrolysis of Waste Plastics: Converting Waste Plastics into Diesel and Other Fuels*, ed. Schiers and J. K. Walter, John Wiley & Sons, Ltd, 2006, pp. 475–491.
- 317 M. Predel and W. Kaminsky, Pyrolysis of mixed polyolefins in a fluidised-bed reactor and on a pyro-GC/MS to yield aliphatic waxes, *Polym. Degrad. Stab.*, 2000, **70**(3), 373–385.
- 318 W. Kaminsky and J. Franck, Monomer recovery by pyrolysis of poly(methyl methacrylate) (PMMA), *J. Anal. Appl. Pyrolysis*, 1991, **19**, 311–318.
- 319 S.-H. Jung, M.-H. Cho, B.-S. Kang and J.-S. Kim, Pyrolysis of a fraction of waste polypropylene and polyethylene for the recovery of BTX aromatics using a fluidized bed reactor, *Fuel Process. Technol.*, 2010, **91**(3), 277–284.
- 320 F. J. Mastral, E. G. P. Esperanza and M. Juste, Pyrolysis of high-density polyethylene in a fluidised bed reactor. Influence of the temperature and residence time, *J. Anal. Appl. Pyrolysis*, 2002, **63**(1), 1–15.
- 321 K. B. Park, Y. S. Jeong, B. Guzelciftci and J. S. Kim, Characteristics of a new type continuous two-stage pyrolysis of waste polyethylene, *Energy*, 2018, **166**, 343–351.
- 322 T. Yoshioka, G. Grause, C. Eger, W. Kaminsky and A. Okuwaki, Pyrolysis of poly(ethylene terephthalate) in a fluidised bed plant, *Polym. Degrad. Stab.*, 2004, **86**(3), 499–504.
- 323 U. M. Arena and M. Laura, Fluidized Bed Pyrolysis of Plastic Wastes, in *Feedstock Recycling and Pyrolysis of Waste Plastics: Converting Waste Plastics into Diesel and Other Fuels*, ed. W. K. John Scheirs, John Wiley & Sons, Ltd, 2006, pp. 435–474.
- 324 J. F. B. C. Mastral and J. Ceamanos, Modelling of the pyrolysis of high density polyethylene: Product distribution in a fluidized bed reactor, *J. Anal. Appl. Pyrolysis*, 2007, 313–322.
- 325 A. M. W. Cunliffe and T. Paul, Composition of oils derived from the batch pyrolysis of tyres, *J. Anal. Appl. Pyrolysis*, 1998, **44**(2), 131–152.
- 326 M. Arabiourrutia, G. Elordi, M. Olazar and J. Bilbao, Pyrolysis of Polyolefins in a Conical Spouted Bed Reactor: A Way to Obtain Valuable Products, in *Pyrolysis*, InTech, 2017.
- 327 M. Artetxe, G. Lopez, M. Amutio, I. Barbarias, A. Arregi, R. Aguado, J. Bilbao and M. Olazar, Styrene recovery from polystyrene by flash pyrolysis in a conical spouted bed reactor, *Waste Manage.*, 2015, **45**, 126–133.
- 328 R. Aguado, M. Olazar, B. Gaisán, R. Prieto and J. Bilbao, Kinetic Study of Polyolefin Pyrolysis in a Conical Spouted Bed Reactor, *Ind. Eng. Chem. Res.*, 2002, **41**(18), 4559–4566.
- 329 G. Elordi, M. Olazar, G. Lopez, M. Artetxe and J. Bilbao, Product Yields and Compositions in the Continuous Pyrolysis of High-Density Polyethylene in a Conical Spouted Bed Reactor, *Ind. Eng. Chem. Res.*, 2011, **50**(11), 6650–6659.
- 330 B. V. M. Csukas, N. Miskolczi, S. Balogh, A. Angyal and L. Bartha, Simplified dynamic simulation model of plastic waste pyrolysis in laboratory and pilot scale tubular reactor, *Fuel Process. Technol.*, 2013, **106**, 186–200.
- 331 B. Fekhar, V. Zsinka and N. Miskolczi, Value added hydrocarbons obtained by pyrolysis of contaminated waste plastics in horizontal tubular reactor: In situ upgrading of the products by chlorine capture, *J. Cleaner Prod.*, 2019, **241**, 118166.
- 332 W. J. Hall, N. M. M. Mitani, T. Bhaskar, A. Muto, Y. Sakata and P. T. Williams, The co-pyrolysis of flame retarded high impact polystyrene and polyolefins, *J. Anal. Appl. Pyrolysis*, 2007, **80**, 406–415.
- 333 E. Hartulistiyoso, F. A. Sigiyo and M. Yulianto, Temperature Distribution of the Plastics Pyrolysis Process



- to Produce Fuel at 450 °C, *Proc. Environ. Sci.*, 2015, **28**, 234–241.
- 334 W. K. Buah, A. M. Cunliffe and P. T. Williams, Characterization of Products from the Pyrolysis of Municipal Solid Waste, *Process Saf. Environ. Prot.*, 2007, **85**(5), 450–457.
- 335 S. Luo, B. Xiao, Z. Hu and S. Liu, Effect of particle size on pyrolysis of single-component municipal solid waste in fixed bed reactor, *Int. J. Hydrogen Energy*, 2010, **35**(1), 93–97.
- 336 F. Campuzano, R. C. Brown and J. D. Martínez, Auger reactors for pyrolysis of biomass and wastes, *Renewable Sustainable Energy Rev.*, 2019, **102**, 372–409.
- 337 S. B. H. Gephart and C. John, *Process and Apparatus for Producing Hydrocarbon Fuel from Waste Plastic*, 2015.
- 338 S. M. Al-Salem, Y. Yang, J. Wang and G. A. Leeke, Pyro-Oil and Wax Recovery from Reclaimed Plastic Waste in a Continuous Auger Pyrolysis Reactor, *Energies*, 2020, **13**(8), 2040.
- 339 J. Schabel, R. A. Schwarz, C. W. Grispin, M. A. Gencer and J. D. Hensel, Process and apparatus for producing petroleum products, *US Pat.*, 10711202, 2017.
- 340 J. Xu, J. Yu, W. He, J. Huang, J. Xu and G. Li, Recovery of carbon black from waste tire in continuous commercial rotary kiln pyrolysis reactor, *Sci. Total Environ.*, 2021, **772**, 145507.
- 341 S.-Q. Li, Q. Yao, Y. Chi, J.-H. Yan and K.-F. Cen, Pilot-Scale Pyrolysis of Scrap Tires in a Continuous Rotary Kiln Reactor, *Ind. Eng. Chem. Res.*, 2004, **43**(17), 5133–5145.
- 342 A. Prakash and R. R. Palkar, Co-processing of plastic waste in a cement kiln: a better option, *Environ. Sci. Pollut. Res.*, 2021, 1–11.
- 343 Y. J. Zhang, C. Guozhao, W. Chuanshuai, W. Yinxiang and L. Weijian, Aimin, Liquid oils produced from pyrolysis of plastic wastes with heat carrier in rotary kiln, *Fuel Process. Technol.*, 2020, 206.
- 344 F. C. S. Fantozzi, P. Bartocci and U. Desideri, Rotary Kiln Slow Pyrolysis for Syngas and Char Production from Biomass and Waste-Part I: Working Envelope of the Reactor, *J. Eng. Gas Turbines Power*, 2007, **129**, 901–907.
- 345 A. Olufemi and S. Olagboye, Thermal conversion of waste plastics into fuel oil, *Int. J. Petrochem. Sci. Eng.*, 2017, **2**(8), 252–257.
- 346 S.-S. Kim and S. Kim, Pyrolysis characteristics of polystyrene and polypropylene in a stirred batch reactor, *Chem. Eng. J.*, 2004, **98**(1–2), 53–60.
- 347 H. Smuda, *The method of obtaining liquid fuels from polyolefine wastes*, 1990.
- 348 D. McNamara, C. L. M. Murray and C. Dublin, *Conversion of Waste Plastics Material to Fuel*, 2012.
- 349 A. Brems, J. B. C. Vandecasteele and R. Dewil, Polymeric Cracking of Waste Polyethylene Terephthalate to Chemicals and Energy, *J. Air Waste Manage. Assoc.*, 2011, **61**(7), 721–731.
- 350 R. C. Brown, Process Intensification through Directly Coupled Autothermal Operation of Chemical Reactors, *Joule*, 2020, **4**, 2268–2289.
- 351 M. Blazso, Composition of Liquid Fuels Derived from the Pyrolysis of Plastics, in *Feedstock Recycling and Pyrolysis of Waste Plastics: Converting Waste Plastics into Diesel and Other Fuels*, 2006, pp. 315–344.
- 352 TotalEnergies Doubles its Recycled Plastic Production Capacity in France. <https://totalenergies.com/media/news/press-releases/totalenergies-doubles-its-recycled-plastic-production-capacity-france>.
- 353 Shell and Pryme Sign Strategic Plastic Waste to Chemicals Cooperation Agreement. <https://www.shell.com/business-customers/chemicals/media-releases/2021-media-releases/shell-and-pryme-sign-cooperation-agreement.html>.
- 354 A. H. Tullo, ExxonMobil plunges into plastics recycling. <https://cen.acs.org/environment/recycling/ExxonMobil-plunges-plastics-recycling/99/i38>.
- 355 M. Smalley, SABIC, BP collaborate at chemical complex in Germany. <https://www.recyclingtoday.com/article/sabic-bp-collaborate-chemical-complex-germany/>.
- 356 A. Fivga and I. Dimitriou, Pyrolysis of plastic waste for production of heavy fuel substitute: A techno-economic assessment, *Energy*, 2018, **149**, 865–874.
- 357 M. Larrain, S. Van Passel, G. Thomassen, U. Kresovic, N. Alderweireldt, E. Moerman and P. Billen, Economic performance of pyrolysis of mixed plastic waste: Open-loop versus closed-loop recycling, *J. Cleaner Prod.*, 2020, **270**, 122442.
- 358 J. Sahu, K. Mahalik, H. K. Nam, T. Y. Ling, T. S. Woon, M. S. bin Abdul Rahman, Y. Mohanty, N. Jayakumar and S. Jamuar, Feasibility study for catalytic cracking of waste plastic to produce fuel oil with reference to Malaysia and simulation using ASPEN Plus, *Environ. Prog. Sustainable Energy*, 2014, **33**(1), 298–307.
- 359 U. R. Gracida-Alvarez, O. Winjobi, J. C. Sacramento-Rivero and D. R. Shonnard, System Analyses of High-Value Chemicals and Fuels from a Waste High-Density Polyethylene Refinery. Part 1: Conceptual Design and Techno-Economic Assessment, *ACS Sustainable Chem. Eng.*, 2019, **7**(22), 18254–18266.
- 360 M. A. A. J. Ghodrat, D. Hagare, R. Yang and B. Samali, Economic feasibility of energy recovery from waste plastic using pyrolysis technology: an Australian perspective, *Int. J. Environ. Sci. Technol.*, 2019, **16**, 3721–3734.
- 361 A. Tukker, H. G. L. Simons and S. Wiegemasma, *Chemical Recycling of Plastics Waste (PVC and other resins)*, TNO Institute, 1999.
- 362 Y. Sakata, T. Bhaskar, M. Uddin, A. Muto and T. Matsui, Development of a catalytic dehalogenation (Cl, Br) process for municipal waste plastic-derived oil, *J. Mater. Cycles Waste Manage.*, 2003, 113–124.
- 363 Energy, P. Plastic Energy Achieves RSB Certification For Recycling Plant In Sevilla, Spain. [https://plasticenergy.com/rsb\\_certification\\_sevilla/](https://plasticenergy.com/rsb_certification_sevilla/).
- 364 Sabic bp and sabic embark on new cooperation for products from advanced plastics recycling. <https://www.sabic.com/en/news/26431-bp-and-sabic-embark-on-new-cooperation>.
- 365 Shell Plastic waste. <https://www.shell.com/sustainability/environment/plastic-waste.html>.



- 366 Energy, P. Plastic Energy Announces Final Investment Decision And Start Of Construction Works For Advanced Recycling Plant In France. [https://plasticenergy.com/plastic-energy-announces\\_fid\\_and\\_start\\_of\\_construction\\_works\\_for\\_advanced\\_recycling\\_plant\\_in\\_france/](https://plasticenergy.com/plastic-energy-announces_fid_and_start_of_construction_works_for_advanced_recycling_plant_in_france/).
- 367 Quantafuel expands into the UK to help solve plastic waste problem. <https://www.quantafuel.com/media#/pressreleases/quantafuel-expands-into-the-uk-to-help-solve-plastic-waste-problem-3130820>.
- 368 *Third Quarter 2021 Consolidated financial statements* Quantafuel ASA, Quantafuel ASA, 2021.
- 369 J. M. Lee and E. W. C. Lim, Heat Transfer in a Pulsating Turbulent Fluidized Bed, *Appl. Therm. Eng.*, 2020, **174**, 115321.
- 370 Dow and Fuenix enter into a partnership for the production of 100% circular plastic. <https://corporate.dow.com/en-us/news/press-releases/dow-and-fuenix-enter-into-a-partnership-for-the-production-of-10.html>.
- 371 Dow Terneuzen. <https://nl.dow.com/en-us/locations/terneuzen.html> (accessed 2/22).
- 372 Sandoval, D. Dow, Fuenix Ecology Group partner on plastics recycling project. <https://www.recyclingtoday.com/article/dow-to-produce-new-plastics-from-pyrolysis-oil-netherlands/> (accessed 2/22).
- 373 Ashley Plastics Renewal Facility. <https://www.brightmark.com/plastics-renewal/projects/ashley-indiana>.
- 374 ORDC Freepoint Commodities to Receive \$50,000 Grant. <https://rail.ohio.gov/wps/portal/gov/ordc/about-ordc/news-and-events/ordc-approves-grant-for-freepoint-commodities>.
- 375 Z. Xu, S. S. Kolapkar, S. Zinchik, E. Bar-Ziv and A. G. McDonald, Comprehensive kinetic study of thermal degradation of polyvinylchloride (PVC), *Polym. Degrad. Stab.*, 2020, **176**, 109148.
- 376 Energy, P. Plastic Recycling: Plastic Energy, Freepoint Eco-Systems And TotalEnergies Partner On Advanced Recycling Project In The U.S. <https://plasticenergy.com/plastic-energy-freepoint-eco-systems-totalenergies-advanced-recycling-project-in-the-us/>.
- 377 Shell Investment in shell energy and chemicals park singapore to bring circular chemicals to asia pacific customers. <https://www.shell.com.sg/media/2021-media-releases/investment-in-shell-energy-and-chemicals-park-singapore-to-bring-circular-chemicals-to-asia-pacific-customers.html>.
- 378 Energy, P. Plastic Energy Joins Forces with WWF to Combat Plastic Pollution in Indonesia. <https://plasticenergy.com/press-release-plastic-energy-join-forces-with-wwf/>.
- 379 T. M. Hundertmark, M. Mirjam, J. S. Chris, W. Theo, Christof How plastics waste recycling could transform the chemical industry. <https://www.mckinsey.com/industries/chemicals/our-insights/how-plastics-waste-recycling-could-transform-the-chemical-industry> (accessed January 14).
- 380 Pryme Q3 2021 Presentation, in *Pryme converts plastic waste into valuable products on an industrial scale*, 2021.
- 381 H. Jiang, E. Celeste and B. Stephanis, How waste solutions company Brightmark is converting plastic waste into fuel. <https://www.businessinsider.com/brightmark-plastic-waste-fuel-pollution-2020-10> (accessed 2/22).
- 382 J. Aguado, D. P. Serrano and J. M. Escola, Fuels From Waste Plastics by Thermal and Catalytic Processes: A Review, *Ind. Eng. Chem. Res.*, 2008, **47**, 7982–7992.
- 383 R. Miandad, M. A. Barakat, A. S. Aburizaiza, M. Rehan and A. S. Nizami, Catalytic pyrolysis of plastic waste: A review, *Process Saf. Environ. Prot.*, 2016, **102**, 822–838.
- 384 S. M. Al-Salem, A. Antelava, A. Constantinou, G. Manos and A. Dutta, A review on thermal and catalytic pyrolysis of plastic solid waste (PSW), *J. Environ. Manage.*, 2017, **197**, 177–198.
- 385 H. Ohkita, R. Nishiyama, Y. Tochihara, T. Mizushima, N. Kakuta, Y. Morioka, A. Ueno, Y. Namiki, S. Tanifuji, H. Katoh, H. Sunazuka, R. Nakayama and T. Kuroyanagi, Acid Properties of Silica-Alumina Catalysts and Catalytic Degradation of Polyethylene, *Ind. Eng. Chem. Res.*, 1993, **32**, 3112–3116.
- 386 G. Audisio, F. Bertini, P. L. Beltrame and P. Carniti, Catalytic Degradation of Polymers: Part III - Degradation of Polystyrene, *Polym. Degrad. Stab.*, 1990, **29**, 191–200.
- 387 A. Maity, S. Chaudhari, J. J. Titman and V. Polshettiwar, Catalytic nanosponges of acidic aluminosilicates for plastic degradation and CO<sub>2</sub> to fuel conversion, *Nat. Commun.*, 2020, **11**(1), 1–12.
- 388 R. Ochoa, H. Van Woert, W. H. Lee, R. Subramanian, E. Kugler and P. C. Eklund, Catalytic Degradation of Medium Density Polyethylene Over Silica - Alumina Supports, *Fuel Process. Technol.*, 1996, **49**, 119–136.
- 389 J. Aguado, D. P. Serrano, J. M. Escola, E. Garagorri and J. A. Fernández, Catalytic conversion of polyolefins into fuels over zeolite beta, *Polym. Degrad. Stab.*, 2000, **69**, 11–16.
- 390 M. A. Uddin, Y. Sakata, A. Muto, Y. Shiraga, K. Koizumi, Y. Kanada and K. Murata, Catalytic Degradation of Polyethylene and Polypropylene into Liquid Hydrocarbons with Mesoporous Silica, *Microporous Mesoporous Mater.*, 1998, **21**, 557–564.
- 391 Y. Sakata, M. A. Uddin and A. Muto, Degradation of Polyethylene and Polypropylene into Fuel Oil by Using Solid Acid and Non-Acid Catalysts, *J. Anal. Appl. Pyrolysis*, 1999, **51**, 135–155.
- 392 D. P. Serrano, J. Aguado and J. M. Escola, Catalytic Conversion of Polystyrene over HMCM-41, HZSM-5 and Amorphous SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>: Comparison with Thermal Cracking, *Appl. Catal., B*, 2000, **25**, 181–189.
- 393 E. Y. Hwang, J. R. Kim, J. K. Choi, H. C. Woo and D. W. Park, Performance of Acid Treated Natural Zeolites in Catalytic Degradation of Polypropylene, *J. Anal. Appl. Pyrolysis*, 2002, **62**, 351–364.
- 394 B. Roozbehani, M. Motevassel, M. Mirdrikvand, S. I. Moqadam and A. Kharaghani, Gasoline Production from a Polymeric Urban Disposal Mixture using Silica-Alumina Catalyst, *Clean Technol. Environ. Policy*, 2017, **19**, 123–136.
- 395 Y. Sakata, M. A. Uddin, A. Muto, Y. Kanada, K. Koizumi and K. Murata, Catalytic degradation of Polyethylene into



- Fuel Oil Over Mesoporous Silica (KFS-16) Catalyst, *J. Anal. Appl. Pyrolysis*, 1997, **43**, 15–25.
- 396 N. Miskolczi, C. Wu and P. T. Williams, Fuels by Waste Plastics using Activated Carbon, MCM-41, HZSM-5 and Their Mixture, *MATEC Web Conf.*, 2016, **49**, 05001.
- 397 D. Munir, F. Piepenbreier and M. R. Usman, Hydrocracking of a Plastic Mixture over Various Micro-Mesoporous Composite Zeolites, *Powder Technol.*, 2017, **316**, 542–550.
- 398 C. Ma, J. Yu, B. Wang, Z. Song, J. Xiang, S. Hu, S. Su and L. Sun, Catalytic Pyrolysis of Flame Retarded High Impact Polystyrene over Various Solid Acid Catalysts, *Fuel Process. Technol.*, 2017, **155**, 32–41.
- 399 Q. Huang, C. Liu, R. Wei and J. Wang, Experimental Study of Polyethylene Pyrolysis and Combustion over HZSM-5, HUSY, and MCM-41, *J. Hazard. Mater.*, 2017, **333**, 10–22.
- 400 S. C. Kim, B. S. Kang, B. S. Kim, Y. M. Kim, J. K. Joen and Y. K. Park, Catalytic Pyrolysis of Municipal Plastic Film Wastes over Nanoporous Al-MCM-41, *J. Nanosci. Nanotechnol.*, 2018, **18**, 1078–1082.
- 401 L. O. Mark, M. C. Cendejas and I. Hermans, The Use of Heterogeneous Catalysis in the Chemical Valorization of Plastic Waste (ChemSusChem 22/2020), *ChemSusChem*, 2020, **13**, 5773–5773.
- 402 D. P. Serrano, J. Aguado, J. M. Escola, E. Garagorri, J. M. Rodríguez, L. Morselli, G. Palazzi and R. Orsi, Feedstock Recycling of Agriculture Plastic Film Wastes by Catalytic Cracking, *Appl. Catal., B*, 2004, **49**, 257–265.
- 403 H. Juwono, L. Fauziah, I. Q. Uyun, R. Alfian, Suprpto, Y. L. Ni'Mah and I. Ulfen, Catalytic Conversion of Al-MCM-41-Ceramic on Hidrocarbon (C8 - C12) Liquid Fuel Synthesis from Polypropylene Plastic Waste, *AIP Conf. Proc.*, 2018, 2049.
- 404 P. Verma, Y. Kuwahara, K. Mori, R. Raja and H. Yamashita, Functionalized mesoporous SBA-15 silica: recent trends and catalytic applications, *Nanoscale*, 2020, **12**, 11333–11363.
- 405 K. Li, S. Lee, G. Yuan, J. Lei, S. Lin, P. Weerachanchai, Y. Yang and J.-Y. Wang, Investigation into the Catalytic Activity of Microporous and Mesoporous Catalysts in the Pyrolysis of Waste Polyethylene and Polypropylene Mixture, *Energies*, 2016, **9**, 431.
- 406 Z. Zhang, K. Gora-Marek, J. S. Watson, J. Tian, M. R. Ryder, K. A. Tarach, L. López-Pérez, J. Martínez-Triguero and I. Melián-Cabrera, Recovering Waste Plastics using Shape-Selective Nano-Scale Reactors as Catalysts, *Nat. Sustain.*, 2019, **2**, 39–42.
- 407 A. R. Songip, T. Masuda, H. Kuwahara and K. Hashimoto, Production of High-Quality Gasoline by Catalytic Cracking over Rare-Earth Metal Exchanged Y-Type Zeolites of Heavy Oil from Waste Plastics, *Energy Fuels*, 1994, **8**, 136–140.
- 408 G. Manos, A. Garforth and J. Dwyer, Catalytic Degradation of High-Density Polyethylene on an Ultrastable-Y Zeolite. Nature of Initial Polymer Reactions, Pattern of Formation of Gas and Liquid Products, and Temperature Effects, *Ind. Eng. Chem. Res.*, 2000, **39**, 1203–1208.
- 409 G. Manos, I. Y. Yusof, N. Papayannakos and N. H. Gangas, Catalytic cracking of polyethylene over clay catalysts. Comparison with an ultrastable Y zeolite, *Ind. Eng. Chem. Res.*, 2001, **40**, 2220–2225.
- 410 I. C. Neves, G. Botelho, A. V. Machado and P. Rebelo, The effect of acidity behaviour of Y zeolites on the catalytic degradation of polyethylene, *Eur. Polym. J.*, 2006, **42**, 1541–1547.
- 411 M. Davoodpour, R. Tafreshi, A. A. Khodadadi and Y. Mortazavi, Two-Stage Cracking Catalyst of Amorphous Silica-Alumina on Y Zeolite for Enhanced Product Selectivity and Suppressed Coking, *Korean J. Chem. Eng.*, 2017, **34**, 681–691.
- 412 A. A. Ajibola, J. A. Omoleye and V. E. Efevbokhan, Catalytic Cracking of Polyethylene Plastic Waste using Synthesised Zeolite Y from Nigerian Kaolin Deposit, *Appl. Petrochem. Res.*, 2018, **8**, 211–217.
- 413 N. Miskolczi, T. Juzsakova and J. Sója, Preparation and Application of Metal Loaded ZSM-5 and Y-Zeolite Catalysts for Thermo-Catalytic Pyrolysis of Real End of Life Vehicle Plastics Waste, *J. Energy Inst.*, 2019, **92**, 118–127.
- 414 B. P. S. Santos, D. D. Almeida, M. d. F. V. Marques and C. A. Henriques, Degradation of Polypropylene and Polyethylene Wastes Over HZSM-5 and USY Zeolites, *Catal. Lett.*, 2019, **149**, 798–812.
- 415 W. U. Eze, I. C. Madufor, G. N. Onyeagoro, H. C. Obasi and M. I. Ugbaja, Study on the Effect of Kankara Zeolite-Y-Based Catalyst on the Chemical Properties of Liquid Fuel from Mixed Waste Plastics (MWPs) Pyrolysis, *Polym. Bull.*, 2020, 03116.
- 416 A. Marcilla, A. Gómez, J. A. Reyes-Labarta, A. Giner and F. Hernández, Kinetic study of polypropylene pyrolysis using ZSM-5 and an equilibrium fluid catalytic cracking catalyst, *J. Anal. Appl. Pyrolysis*, 2003, **68–69**, 467–480.
- 417 Q. Zhou, L. Zheng, Y. Z. Wang, G. M. Zhao and B. Wang, Catalytic degradation of low-density polyethylene and polypropylene using modified ZSM-5 zeolites, *Polym. Degrad. Stab.*, 2004, **84**, 493–497.
- 418 J. G. A. P. Filho, E. C. Graciliano, A. O. S. Silva, M. J. B. Souza and A. S. Araujo, Thermo gravimetric kinetics of polypropylene degradation on ZSM-12 and ZSM-5 catalysts, *Catal. Today*, 2005, **107–108**, 507–512.
- 419 S. Boxiong, W. Chunfei, G. Binbin and W. Rui, Liangcai, Pyrolysis of waste tyres with zeolite USY and ZSM-5 catalysts, *Appl. Catal., B*, 2007, **73**, 150–157.
- 420 A. López, I. de Marco, B. M. Caballero, A. Adrados and M. F. Laresgoiti, Deactivation and regeneration of ZSM-5 zeolite in catalytic pyrolysis of plastic wastes, *Waste Manage.*, 2011, **31**, 1852–1858.
- 421 A. López, I. de Marco, B. M. Caballero, M. F. Laresgoiti, A. Adrados and A. Aranzabal, Catalytic pyrolysis of plastic wastes with two different types of catalysts: ZSM-5 zeolite and Red Mud, *Appl. Catal., B*, 2011, **104**, 211–219.
- 422 J. Y. Lee, S. M. Park, S. K. Saha, S. J. Cho and G. Seo, Liquid-phase degradation of polyethylene (PE) over MFI



- zeolites with mesopores: Effects of the structure of PE and the characteristics of mesopores, *Appl. Catal., B*, 2011, **108–109**, 61–71.
- 423 A. Coelho, L. Costa, M. M. Marques, I. M. Fonseca, M. A. Lemos and F. Lemos, The effect of ZSM-5 zeolite acidity on the catalytic degradation of high-density polyethylene using simultaneous DSC/TG analysis, *Appl. Catal., A*, 2012, **413–414**, 183–191.
- 424 N. Carmo, D. Afonso, E. Santos, I. Fonseca, F. Lemos and M. A. Lemos, Coprocessing of Waste Plastic and Hydrocarbons over MFI (HZSM-5), *Int. J. Chem. Kinet.*, 2016, **48**, 329–336.
- 425 Y. Zhao, Z. Ye, H. Zhang, Y. Zhang and Y. Tang, Facile Fabrication and Morphology Regulation of Crossed MFI Zeolite with Improved Performance on LDPE Cracking, *Ind. Eng. Chem. Res.*, 2019, **58**, 13174–13181.
- 426 A. Marcilla, A. Gómez-Siurana and F. Valdés, Catalytic Cracking of Low-Density Polyethylene over H-Beta and HZSM-5 Zeolites: Influence of the External Surface. Kinetic Model, *Polym. Degrad. Stab.*, 2007, **92**, 197–204.
- 427 M. S. Renzini, L. C. Lerici, U. Sedran and L. B. Pierella, Stability of ZSM-11 and BETA zeolites during the catalytic cracking of low-density polyethylene, *J. Anal. Appl. Pyrolysis*, 2011, **92**, 450–455.
- 428 K. Wanchai and A. Chaisuwan, Catalytic Cracking of Polypropylene Waste over Zeolite Beta, *J. Chem. Mater. Res.*, 2013, **3**, 2225–2956.
- 429 H. W. Lee, S. J. Choi, J. K. Jeon, S. H. Park, S. C. Jung and Y. K. Park, Catalytic conversion of waste particle board and polypropylene over H-beta and HY zeolites, *Renewable Energy*, 2015, **79**, 9–13.
- 430 D. Munir, H. Amer, R. Aslam, M. Bououdina and M. R. Usman, Composite Zeolite Beta Catalysts for Catalytic Hydrocracking of Plastic Waste to Liquid Fuels, *Mater. Renewable Sustainable Energy Rev.*, 2020, **9**, 9.
- 431 K. Pyra, K. A. Tarach, E. Janiszewska, D. Majda and K. Góra-Marek, Evaluation of the Textural Parameters of Zeolite Beta in LDPE Catalytic Degradation: Thermogravimetric Analysis Coupled with FTIR Operando Studies, *Molecules*, 2020, **25**(4), 926.
- 432 S. Y. Lee, J. H. Yoon, J. R. Kim and D. W. Park, Catalytic Degradation of Polystyrene over Natural Clinoptilolite Zeolite, *Polym. Degrad. Stab.*, 2001, **74**, 297–305.
- 433 S. Salamah, D. Azhari and A. Mitanto, Pyrolysis of Ethylene Vinyl Acetate Polymer by Natural Zeolite Catalyst as an Alternative Fuel, *Adv. Eng. Res.*, 2019, **189**, 54–59.
- 434 E. Erawati, Hamid and R. D. Permatasari, Pyrolysis of Polypropylene Waste with Natural Zeolite as Catalyst, *AIP Conf. Proc.*, 2019, **2114**, 050019.
- 435 S. Jin, K. Cui, H. Guan, M. Yang, L. Liu and C. Lan, Preparation of mesoporous MCM-41 from natural sepiolite and its catalytic activity of cracking waste polystyrene plastics, *Appl. Clay Sci.*, 2012, **56**, 1–6.
- 436 W. Sriningsih, M. G. Saerodji, W. Trisunaryanti, R. Armunanto and I. I. Falah, Fuel Production from LDPE Plastic Waste over Natural Zeolite Supported Ni, Ni-Mo, Co and Co-Mo Metals, *Procedia Environ. Sci.*, 2014, **20**, 215–224.
- 437 I. Borovanska, M. L. Cerrada, P. Zipper and S. Djoumaliisky, Recycled Polyolefin Blends: Effect of Modified Natural Zeolite on their Properties and Morphology, *Polym.-Plast. Technol. Eng.*, 2016, **55**, 486–497.
- 438 L. G. Mssina, P. R. Bonelli and A. L. Cukierman, *In situ* Catalytic Pyrolysis of Peanut Shells Using Modified Natural Zeolite, *Fuel Process. Technol.*, 2017, **159**, 160–167.
- 439 S. Salamah and A. Aktawan, Product Distribution of Pyrolysis of Polystyrene Foam Waste using Catalyst of Natural Zeolite and Nickel/Silica, *IOP Conf. Series: Earth and Envir. Sci.*, 2018, 175.
- 440 P. Kusumo, A. Romli, M. I. Aulia and E. M. Yanuar, Fuel Oil from Municipal Plastic Waste through Pyrolysis with and without Natural Zeolite as Catalysts, *E3S Web Conf.*, 2018, **73**, 01021.
- 441 E. Erawati, H. Hamid and A. A. Ilma, Pyrolysis Process of Mixed Polypropylene (PP) and High-Density Polyethylene (HDPE) Waste with Natural Zeolite as Catalyst, *Molekul*, 2018, **13**, 106.
- 442 I. N. Meshkova, T. M. Ushakova, V. G. Grinev, V. A. Nikashina and L. A. Novokshonova, Use of Synthetic and Natural Zeolites for Fabricating Immobilized Olefin Polymerization Catalysts and Polyolefin-Based Composite Materials, *Pet. Chem.*, 2019, **59**, 831–837.
- 443 W. Ding, J. Liang and L. L. Anderson, Hydrocracking and Hydroisomerization of High-Density Polyethylene and Waste Plastic over Zeolite and Silica - Alumina-Supported Ni and Ni-Mo Sulfides, *Energy Fuels*, 1997, **11**, 1219–1223.
- 444 T. Isoda, S. Maemoto, K. Kusakabe and S. Morooka, Hydrocracking of pyrenes over a nickel-supported Y-zeolite catalyst and an assessment of the reaction mechanism based on MD calculations, *Energy Fuels*, 1999, **13**, 617–623.
- 445 A. Eschenbacher, F. Goodarzi, R. J. Varghese, K. Enemark-Rasmussen, S. Kegnaes, M. S. Abbas-Abadi and K. M. Van Geem, Boron-Modified Mesoporous ZSM-5 for the Conversion of Pyrolysis Vapors from LDPE and Mixed Polyolefins: Maximizing the C2-C4Olefin Yield with Minimal Carbon Footprint, *ACS Sustainable Chem. Eng.*, 2021, **9**, 14618–14630.
- 446 J. M. Escola, J. Aguado, D. P. Serrano, A. García, A. Peral, L. Briones, R. Calvo and E. Fernandez, Catalytic Hydroreforming of the Polyethylene Thermal Cracking Oil over Ni Supported Hierarchical Zeolites and Mesoporous Aluminosilicates, *Appl. Catal., B*, 2011, **106**, 405–415.
- 447 E. G. Fuentes-Ordóñez, J. A. Salbidegoitia, J. L. Ayastuy, M. A. Gutiérrez-Ortiz, M. P. González-Marcos and J. R. González-Velasco, High external surface Pt/zeolite catalysts for improving polystyrene hydrocracking, *Catal. Today*, 2014, **227**, 163–170.
- 448 E. G. Fuentes-Ordóñez, J. A. Salbidegoitia, M. P. González-Marcos, J. L. Ayastuy, M. A. Gutiérrez-Ortiz and



- J. R. González-Velasco, Pt/ITQ-6 zeolite as a bifunctional catalyst for hydrocracking of waste plastics containing polystyrene, *J. Mater. Cycles Waste Manage.*, 2015, **17**, 465–475.
- 449 D. P. Serrano, J. M. Escola, L. Briones, S. Medina and A. Martínez, Hydroreforming of the oils from LDPE thermal cracking over Ni-Ru and Ru supported over hierarchical Beta zeolite, *Fuel*, 2015, **144**, 287–294.
- 450 D. P. Serrano, J. M. Escola, L. Briones and M. Arroyo, Hydroprocessing of the LDPE Thermal Cracking Oil into Transportation Fuels over Pd Supported on Hierarchical ZSM-5 Catalyst, *Fuel*, 2017, **206**, 190–198.
- 451 A. Hijazi, A. A. H. Al-Muhtaseb, S. Aouad, M. N. Ahmad and J. Zeaiter, Pyrolysis of Waste Rubber Tires with Palladium Doped Zeolite, *J. Environ. Chem. Eng.*, 2019, **7**, 103451.
- 452 K. Pyra, K. A. Tarach, A. Srebowata, I. Melián-Cabrera and K. Góra-Marek, Pd-Modified Beta Zeolite for Modulated Hydro-Cracking of Low-Density Polyethylene into a Paraffinic-Rich Hydrocarbon Fuel, *Appl. Catal., B*, 2020, 119070.
- 453 G. Manos, I. Y. Yusof, N. H. Gangas and N. Papayannakos, Tertiary Recycling of Polyethylene to Hydrocarbon Fuel by Catalytic Cracking Over Aluminum Pillared Clays, *Energy Fuels*, 2002, **16**, 485–489.
- 454 A. De Stefanis, P. Cafarelli, F. Gallese, E. Borsella, A. Nana and G. Perez, Catalytic Pyrolysis of Polyethylene: A Comparison Between Pillared and Restructured Clays, *J. Anal. Appl. Pyrolysis*, 2013, **104**, 479–484.
- 455 K. Li, J. Lei, G. Yuan, P. Weerachanchai, J. Y. Wang, J. Zhao and Y. Yang, Fe-, Ti-, Zr- and Al-Pillared Clays for Efficient Catalytic Pyrolysis of Mixed Plastics, *Chem. Eng. J.*, 2017, **317**, 800–809.
- 456 V. Patil, S. Adhikari and P. Cross, Co-pyrolysis of lignin and plastics using red clay as catalyst in a micro-pyrolyzer, *Bioresour. Technol.*, 2018, **270**, 311–319.
- 457 I. Vollmer, M. J. Jenks, R. Mayorga González, F. Meirer and B. M. Weckhuysen, Plastic Waste Conversion over a Refinery Waste Catalyst, *Angew. Chem.*, 2021, **133**, 16237–16244.
- 458 S. C. Cardona and A. Corma, Tertiary Recycling of Polypropylene by Catalytic Cracking in a Semibatch Stirred Reactor. Use of Spent Equilibrium FCC Commercial Catalyst, *Appl. Catal., B*, 2000, **25**, 151–162.
- 459 K. H. Lee, N. S. Noh, D. H. Shin and Y. Seo, Comparison of Plastic Types for Catalytic Degradation of Waste Plastics into Liquid Product with Spent FCC Catalyst, *Polym. Degrad. Stab.*, 2002, **78**, 539–544.
- 460 Y. H. Lin and M. H. Yang, Catalytic pyrolysis of polyolefin waste into valuable hydrocarbons over reused catalyst from refinery FCC units, *Appl. Catal., A*, 2007, **328**, 132–139.
- 461 E. Rodríguez, R. Palos, A. Gutiérrez, F. J. Vela, J. M. Arandes and J. Bilbao, Effect of the FCC Equilibrium Catalyst Properties and of the Cracking Temperature on the Production of Fuel from HDPE Pyrolysis Waxes, *Energy Fuels*, 2019, **33**, 5191–5199.
- 462 E. Rodríguez, G. Elordi, J. Valecillos, S. Izaddoust, J. Bilbao, J. M. Arandes and P. Castaño, Coke Deposition and Product Distribution in the Co-Cracking of Waste Polyolefin Derived Streams and Vacuum Gas Oil Under FCC Unit Conditions, *Fuel Process. Technol.*, 2019, **192**, 130–139.
- 463 K. Praveen Kumar and S. Srinivas, Catalytic Co-pyrolysis of Biomass and Plastics (Polypropylene and Polystyrene) Using Spent FCC Catalyst, *Energy Fuels*, 2020, **34**, 460–473.
- 464 D. K. Ratnasari, M. A. Nahil and P. T. Williams, Catalytic Pyrolysis of Waste Plastics using Staged Catalysis for Production of Gasoline Range Hydrocarbon Oils, *J. Anal. Appl. Pyrolysis*, 2017, **124**, 631–637.
- 465 D. Munir and M. R. Usman, Catalytic Hydrolysis of a Model Municipal Waste Plastic Mixture over Composite USY/SBA-16 Catalysts, *J. Anal. Appl. Pyrolysis*, 2018, **135**, 44–53.
- 466 K. Ding, S. Liu, Y. Huang, S. Liu, N. Zhou, P. Peng, Y. Wang, P. Chen and R. Ruan, Catalytic Microwave-Assisted Pyrolysis of Plastic Waste over NiO and HY for Gasoline-Range Hydrocarbons Production, *Energy Convers. Manage.*, 2019, **196**, 1316–1325.
- 467 M. J. B. de Souza, T. H. A. Silva, T. R. S. Ribeiro, A. O. S. da Silva and A. M. G. Pedrosa, Thermal and Catalytic Pyrolysis of Polyvinyl Chloride using Micro/Mesoporous ZSM-35/MCM-41 Catalysts, *J. Therm. Anal. Calorim.*, 2020, **140**, 167–175.
- 468 M. Pires, M. Murariu, A. M. Cardoso, L. Bonnaud and P. Dubois, Thermal Degradation of Poly(lactic acid)-Zeolite Composites Produced by Melt-Blending, *Polym. Bull.*, 2020, **77**, 2111–2137.
- 469 P. Sudarsanam, E. Peeters, E. V. Makshina, V. I. Parvulescu and B. F. Sels, Advances in porous and nanoscale catalysts for viable biomass conversion, *Chem. Soc. Rev.*, 2019, **48**, 2366–2421.
- 470 B. Fekhar, V. Zsinka and N. Miskolczi, Value Added Hydrocarbons Obtained by Pyrolysis of Contaminated Waste Plastics in Horizontal Tubular Reactor: In Situ Upgrading of the Products by Chlorine Capture, *J. Cleaner Prod.*, 2019, **241**, 118166.
- 471 J. Pérez-Ramírez, C. H. Christensen, K. Egeblad, C. H. Christensen and J. C. Groen, Hierarchical zeolites: Enhanced utilisation of microporous crystals in catalysis by advances in materials design, *Chem. Soc. Rev.*, 2008, **37**, 2530–2542.
- 472 R. Zou, Y. Wang, L. Jiang, Z. Yu, Y. Zhao, Q. Wu, L. Dai, L. Ke, Y. Liu and R. Ruan, Microwave-assisted co-pyrolysis of lignin and waste oil catalyzed by hierarchical ZSM-5/MCM-41 catalyst to produce aromatic hydrocarbons, *Bioresour. Technol.*, 2019, **289**, 121609.
- 473 Y. M. Kim, J. Jeong, S. Ryu, H. W. Lee, J. S. Jung, M. Z. Siddiqui, S. C. Jung, J. K. Jeon, J. Jae and Y. K. Park, Catalytic pyrolysis of wood polymer composites over hier-



- archical mesoporous zeolites, *Energy Convers. Manage.*, 2019, **195**, 727–737.
- 474 B. J. B. Silva, L. V. Sousa, L. R. A. Sarmento, S. L. Alencar, P. H. L. Quintela and A. O. S. Silva, Kinetic Study of Thermocatalytic Degradation of UHMWPE over Microporous and Hierarchical ZSM-23 Zeolite, *Appl. Catal., B*, 2020, **267**, 118699.
- 475 Z. Li, Z. Zhong, B. Zhang, W. Wang, G. V. S. Seufitelli and F. L. P. Resende, Catalytic fast co-pyrolysis of waste greenhouse plastic films and rice husk using hierarchical micro-mesoporous composite molecular sieve, *Waste Manage.*, 2020, **102**, 561–568.
- 476 J. Aguado, D. P. Serrano, J. M. Escola and L. Briones, Deactivation and regeneration of a Ni supported hierarchical Beta zeolite catalyst used in the hydroreforming of the oil produced by LDPE thermal cracking, *Fuel*, 2013, **109**, 679–686.
- 477 W. Namchot and S. Jitkarnka, Catalytic pyrolysis of waste tire using HY/MCM-41 core-shell composite, *J. Anal. Appl. Pyrolysis*, 2016, **121**, 297–306.
- 478 V. P. S. Caldeira, A. Peral, M. Linares, A. S. Araujo, R. A. Garcia-Muñoz and D. P. Serrano, Properties of Hierarchical Beta Zeolites Prepared from Protozeolitic Nanounits for the Catalytic Cracking of High Density Polyethylene, *Appl. Catal., A*, 2017, **531**, 187–196.
- 479 K. A. Tarach, K. Pyra, S. Siles, I. Melián-Cabrera and K. Góra-Marek, Operando Study Reveals the Superior Cracking Activity and Stability of Hierarchical ZSM-5 Catalyst for the Cracking of Low-Density Polyethylene, *ChemSusChem*, 2019, **12**, 633–638.
- 480 S. L. Wu, J. H. Kuo and M. Y. Wey, Thermal degradation of waste plastics in a two-stage pyrolysis-catalysis reactor over core-shell type catalyst, *J. Anal. Appl. Pyrolysis*, 2019, **142**, 104641.
- 481 Y. Zhang, D. Duan, H. Lei, E. Villota and R. Ruan, Jet Fuel Production from Waste Plastics via Catalytic Pyrolysis with Activated Carbons, *Appl. Energy*, 2019, **251**, 113337.
- 482 C. Wu and P. T. Williams, A Novel Ni-Mg-Al-CaO Catalyst with the Dual Functions of Catalysis and CO<sub>2</sub> Sorption for H<sub>2</sub> Production from the Pyrolysis-Gasification of Polypropylene, *Fuel*, 2010, **89**, 1435–1441.
- 483 M. Busto, C. R. Vera and J. M. Grau, Optimal process conditions for the isomerization-cracking of long-chain n-paraffins to high octane isomerizate gasoline over Pt/SO<sub>4</sub>2–ZrO<sub>2</sub> catalysts, *Fuel Process. Technol.*, 2011, **92**, 1675–1684.
- 484 M. N. Siddiqui, E. V. Antonakou, H. H. Redhwi and D. S. Achilias, Kinetic analysis of thermal and catalytic degradation of polymers found in waste electric and electronic equipment, *Thermochim. Acta*, 2019, **675**, 69–76.
- 485 M. N. Almustapha, M. Farooq, M. L. Mohammed, M. Farhan, M. Imran and J. M. Andresen, Modification of Acidic and Textural Properties of a Sulphated Zirconia Catalyst for Efficient Conversion of High-Density Polyethylene into Liquid Fuel, *Environ. Sci. Pollut. Res.*, 2020, **27**, 55–65.
- 486 C. A. Veses, R. Date, R. Date, A. Date and N. Mv, From Laboratory Scale to Pilot Plant: Evaluation of the Catalytic Co-Pyrolysis of Grape Seeds and Polystyrene Wastes with CaO, *Catal. Today*, 2020, **379**, 87–95.
- 487 A. Patel, V. Brahmkhatri and N. Singh, Biodiesel Production by Esterification of Free Fatty Acid over Sulfated Zirconia, *Renewable Energy*, 2013, **51**, 227–233.
- 488 E. V. Antonakou, K. G. Kalogiannis, S. D. Stefanidis, S. A. Karakoulia, K. S. Triantafyllidis, A. A. Lappas and D. S. Achilias, Catalytic and thermal pyrolysis of polycarbonate in a fixed-bed reactor: The effect of catalysts on products yields and composition, *Polym. Degrad. Stab.*, 2014, **110**, 482–491.
- 489 S. Kumagai, I. Hasegawa, G. Grause, T. Kameda and T. Yoshioka, Thermal Decomposition of Individual and Mixed Plastics in the Presence of CaO or Ca(OH)<sub>2</sub>, *J. Anal. Appl. Pyrolysis*, 2015, **113**, 584–590.
- 490 M. S. Khan, M. Sohail and N. S. Khattak, Conversion of Mixed Low-Density Polyethylene Wastes into Liquid Fuel by Novel CaO/SiO<sub>2</sub> Catalyst, *J. Polym. Environ.*, 2016, **24**, 255–263.
- 491 L. Fan, Y. Zhang, S. Liu, N. Zhou, P. Chen, Y. Liu, Y. Wang, P. Peng, Y. Cheng and M. Addy, Ex-Situ Catalytic Upgrading of Vapors from Microwave-Assisted Pyrolysis of Low-Density Polyethylene with MgO, *Energy Convers. Manage.*, 2017, **149**, 432–441.
- 492 M. Utami, K. Wijaya and W. Trisunaryanti, Pt-Promoted Sulfated Zirconia as Catalyst for Hydrocracking of LDPE Plastic Waste into Liquid Fuels, *Mater. Chem. Phys.*, 2018, **213**, 548–555.
- 493 M. Nadjib, T. H. A. Santosa, A. Zuniardi and R. Shihabudin, Properties of co-pyrolysed palm kernel shell and plastic grocery bag with CaO as catalyst, *IOP Conference Series: Earth and Environmental Science*, 2018, **209**.
- 494 L. S. Diaz-Silvarrey, A. McMahon and A. N. Phan, Benzoic Acid Recovery via Waste Poly(ethylene terephthalate) (PET) Catalytic Pyrolysis using Sulphated Zirconia Catalyst, *J. Anal. Appl. Pyrolysis*, 2018, **134**, 621–631.
- 495 Y. Uemichi, Y. Makino and T. Kanazuka, Degradation of Polyethylene to Aromatic Hydrocarbons Over Metal-Supported Activated Carbon Catalysts, *J. Anal. Appl. Pyrolysis*, 1989, **14**, 331–344.
- 496 N. Miskolczi, C. Wu and P. T. Williams, Pyrolysis of Waste Plastics Using Catalysts: Activated Carbon, MCM-41 and HZSM-5, *Int. J. Chem. Eng. Appl.*, 2017, **8**, 67–74.
- 497 K. Sun, Q. Huang, X. Meng, Y. Chi and J. Yan, Catalytic Pyrolysis of Waste Polyethylene into Aromatics by H<sub>3</sub>PO<sub>4</sub>-Activated Carbon, *Energy Fuels*, 2018, **32**, 9772–9781.
- 498 S. Kim, C. Park and J. Lee, Reduction of Polycyclic Compounds and Biphenyls Generated by Pyrolysis of Industrial Plastic Waste by Using Supported Metal Catalysts: A Case Study of Polyethylene Terephthalate Treatment, *J. Hazard. Mater.*, 2020, **392**, 122464.
- 499 B. Kunwar, B. R. Moser, S. R. Chandrasekaran, N. Rajagopalan and B. K. Sharma, Catalytic and Thermal



- Depolymerization of Low Value Post-Consumer High Density Polyethylene Plastic, *Energy*, 2016, **111**, 884–892.
- 500 M. V. Singh, Waste and Virgin High-Density Poly(ethylene) into Renewable Hydrocarbons Fuel by Pyrolysis-Catalytic Cracking with a CoCO<sub>3</sub> Catalyst, *J. Anal. Appl. Pyrolysis*, 2018, **134**, 150–161.
- 501 M. V. Singh, S. Kumar and M. Sarker, Waste HD-PE plastic, Deformation into Liquid Hydrocarbon Fuel using Pyrolysis-Catalytic Cracking with a CuCO<sub>3</sub> Catalyst, *Sustainable Energy Fuels*, 2018, **2**, 1057–1068.
- 502 M. V. Singh, Deformation of Virgin HD-PE, PP and Waste PP Plastics into Green Fuel via a Pyrolysis-Catalytic using a NiCO<sub>3</sub> Catalyst, *Indian Chem. Eng.*, 2019, **61**, 254–268.
- 503 A. Ahamed, L. Liang, W. P. Chan, P. C. K. Tan, N. T. X. Yip, J. Bobacka, A. Veksha, K. Yin and G. Lisak, In situ catalytic reforming of plastic pyrolysis vapors using MSW incineration ashes, *Environ. Pollut.*, 2021, **276**, 116681.
- 504 H. Persson, I. Duman, S. Wang, L. J. Pettersson and W. Yang, Catalytic pyrolysis over transition metal-modified zeolites: A comparative study between catalyst activity and deactivation, *J. Anal. Appl. Pyrolysis*, 2019, **138**, 54–61.
- 505 F. J. Mastral, E. Esperanza, P. García and M. Juste, Pyrolysis of high-density polyethylene in a fluidised bed reactor. Influence of the temperature and residence time, *J. Anal. Appl. Pyrolysis*, 2002, **63**, 1–15.
- 506 Y. Xue, P. Johnston and X. Bai, Effect of catalyst contact mode and gas atmosphere during catalytic pyrolysis of waste plastics, *Energy Convers. Manage.*, 2017, **142**, 441–451.
- 507 D. Kunii and O. Levenspiel, *Fluidization engineering*, Butterworth-Heinemann, Boston, London, 1991.
- 508 Anellotech New Anellotech technology tackles plastics pollution by recycling plastic waste into chemicals. <https://anellotech.com/press/new-anellotech-technology-tackles-plastics-pollution-recycling-plastic-waste-chemicals#:~:text=Pearl%20River%2C%20NY%20%E2%80%93%20December%206,to%20make%20new%2C%20virgin%20plastics>. (accessed Feb 02).
- 509 D. Sudolsky, Commercializing Renewable Aromatics for Biofuels, Biobased Chemicals and Plastics Chemical Recycling, *Ind. Biotechnol.*, 2019, **15**, 330–333.
- 510 Braskem advances in research into chemical recycling of plastics. <https://www.braskem.com.br/news-detail/braskem-advances-in-research-into-chemical-recycling-of-plastics> (accessed Feb 02).
- 511 Goldsberry, C. Braskem America, Encina Partner to Develop Circular Polypropylene Feedstock. <https://www.plasticstoday.com/advanced-recycling/braskem-america-encina-partner-develop-circular-polypropylene-feedstock> (accessed Feb 02).
- 512 CALIENDO, H. Encina Turning Plastic Waste Into Renewable Base Chemicals and Fuels. <https://www.pton-line.com/news/encina-turning-plastic-waste-into-renewable-base-chemicals-and-fuels#:~:text=Encina%20is%20a%20company%20emerging,fuels%20for%20the%20circular%20economy.&text=Encina%20has%20developed%20a%20process,plastic%20waste%20through%20catalytic%20pyrolysis>. (accessed Feb 02).
- 513 M. Luo and C. W. Curtis, Effect of reaction parameters and catalyst type on waste plastics liquefaction and coprocessing with coal, *Fuel Process. Technol.*, 1996, **49**, 177–196.
- 514 M. Čolnik, P. Kotnik, Ž. Knez and M. Škerget, Hydrothermal decomposition of polyethylene waste to hydrocarbons rich oil, *J. Supercrit. Fluids*, 2020, **169**, 105136.
- 515 T. Hirota and F. N. Fagan, Liquefaction of Plastics, *Makromol. Chem., Macromol. Symp.*, 1992, **57**, 161–173.
- 516 M. M. Taghiei, Z. Feng, F. E. Huggins and G. P. Huffman, Coliquefaction of Waste Plastics with Coal, *Energy Fuels*, 1994, **8**, 1228–1232.
- 517 W. Zmierzak, X. Xiao and J. Shabtai, Depolymerization-liquefaction of plastics and rubbers. 2. Polystyrenes and styrene-butadiene copolymers, *Fuel Process. Technol.*, 1996, **49**, 31–48.
- 518 M. V. S. Murty, P. Rangarajan, E. A. Grulke and D. Bhattacharyya, Thermal degradation/hydrogenation of commodity plastics and characterization of their liquefaction products, *Fuel Process. Technol.*, 1996, **49**, 75–90.
- 519 Z. Feng, J. Rockwell, D. Bailey and G. Huffman, Direct liquefaction of waste plastics and coliquefaction of coal-plastic mixtures, *Fuel Process. Technol.*, 1996, **49**, 17–30.
- 520 J. Shabtai, X. Xiao and W. Zmierzak, Depolymerization-liquefaction of plastics and rubbers. 1. Polyethylene, polypropylene, and polybutadiene, *Energy Fuels*, 1997, **11**, 76–87.
- 521 P. K. Ramdoss and A. R. Tarrer, High-temperature liquefaction of waste plastics, *Fuel*, 1998, **77**, 293–299.
- 522 N. Shah, J. Rockwell and G. P. Huffman, Conversion of waste plastic to oil: Direct liquefaction versus pyrolysis and hydroprocessing, *Energy Fuels*, 1999, **13**, 832–838.
- 523 P. T. Williams and E. Slaney, Analysis of products from the pyrolysis and liquefaction of single plastics and waste plastic mixtures, *Resour., Conserv. Recycl.*, 2007, **51**, 754–769.
- 524 T. Moriya and H. Enomoto, Characteristics of polyethylene cracking in supercritical water compared to thermal cracking, *Polym. Degrad. Stab.*, 1999, **65**, 373–386.
- 525 G. C. Hwang, K. H. Kim, S. Y. Bae, S. C. Yi and H. Kumazawa, Degradation of High Density Polyethylene, Polypropylene and Their Mixtures in Supercritical Acetone, *Korean J. Chem. Eng.*, 2001, **18**, 396–401.
- 526 G. C. Hwang, J. H. Choi, S. Y. Bae and H. Kumazawa, Degradation of Polystyrene in Supercritical n-Hexane, *Korean J. Chem. Eng.*, 2001, **18**, 854–861.
- 527 H. Y. Shin and S. Y. Bae, Thermal decomposition of polystyrene in supercritical methanol, *J. Appl. Polym. Sci.*, 2008, **108**, 3467–3472.
- 528 M. S. Seshasayee and P. E. Savage, Oil from plastic via hydrothermal liquefaction: Production and characterization, *Appl. Energy*, 2020, **278**, 115673.



- 529 S. H. Ng, H. Seoud, M. Stanciulescu and Y. Sugimoto, Conversion of Polyethylene to Transportation Fuels through Pyrolysis and Catalytic Cracking, *Energy Fuels*, 1995, **9**, 735–742.
- 530 Z. Fang and J. A. Koziński, A study of rubber liquefaction in supercritical water using DAC-stereomicroscopy and FT-IR spectrometry, *Fuel*, 2002, **81**, 935–945.
- 531 X. Su, Y. Zhao, R. Zhang and J. Bi, Investigation on degradation of polyethylene to oils in supercritical water, *Fuel Process. Technol.*, 2004, **85**, 1249–1258.
- 532 Y. Takeshita, K. Kato, K. Takahashi, Y. Sato and S. Nishi, Basic study on treatment of waste polyvinyl chloride plastics by hydrothermal decomposition in subcritical and supercritical regions, *J. Supercrit. Fluids*, 2004, **31**, 185–193.
- 533 H. f. Zhang, X. l. Su, D. k. Sun, R. Zhang and J. c. Bi, Investigation on degradation of polyethylene to oil in a continuous supercritical water reactor, *J. Fuel Chem. Technol.*, 2007, **35**, 487–491.
- 534 M. Sugano, T. Shimizu, A. Komatsu, Y. Kakuta and K. Hirano, Liquefaction and dechlorination of hydrothermally treated waste mixture containing plastics with glass powder, *Environ. Sci. Technol.*, 2011, **45**, 2493–2497.
- 535 T. H. Pedersen and F. Conti, Improving the circular economy via hydrothermal processing of high-density waste plastics, *Waste Manage.*, 2017, **68**, 24–31.
- 536 B. Bai, H. Jin, C. Fan, C. Cao, W. Wei and W. Cao, Experimental investigation on liquefaction of plastic waste to oil in supercritical water, *Waste Manage.*, 2019, **89**, 247–253.
- 537 W. T. Chen, K. Jin and N. H. Linda Wang, Use of Supercritical Water for the Liquefaction of Polypropylene into Oil, *ACS Sustainable Chem. Eng.*, 2019, **7**, 3749–3758.
- 538 J. S. dos Passosa, M. Glasius and P. Biller, Screening of common synthetic polymers for depolymerization by subcritical hydrothermal liquefaction, *Process Saf. Environ. Prot.*, 2020, **139**, 371–379.
- 539 H. Jin, B. Bai, W. Wei, Y. Chen, Z. Ge and J. Shi, Hydrothermal Liquefaction of Polycarbonate (PC) Plastics in Sub-/Supercritical Water and Reaction Pathway Exploration, *ACS Sustainable Chem. Eng.*, 2020, **8**, 7039–7050.
- 540 K. Jin, P. Vozka, G. Kilaz, W. T. Chen and N. H. L. Wang, Conversion of polyethylene waste into clean fuels and waxes via hydrothermal processing (HTP), *Fuel*, 2020, **273**, 1–11.
- 541 P. Zhao, Z. Yuan, J. Zhang, X. Song, C. Wang, Q. Guo and A. J. Ragauskas, Supercritical water co-liquefaction of LLDPE and PP into oil: Properties and synergy, *Sustainable Energy Fuels*, 2021, **5**, 575–583.
- 542 B. Ciuffi, L. Rosi, E. Miliotti, G. Lotti, A. M. Rizzo and D. Chiaramonti, Batch Hydrothermal liquefaction of end-of-life plastic and oil characterization, *E3S Web Conf.*, 2021, **238**, 0–4.
- 543 X. Pei, X. Yuan, G. Zeng, H. Huang, J. Wang, H. Li and H. Zhu, Co-liquefaction of microalgae and synthetic polymer mixture in sub- and supercritical ethanol, *Fuel Process. Technol.*, 2012, **93**, 35–44.
- 544 N. Ahmad, N. Ahmad, I. M. Maafa, U. Ahmed, P. Akhter, N. Shehzad, U. e. s. Amjad and M. Hussain, Thermal conversion of polystyrene plastic waste to liquid fuel via ethanolysis, *Fuel*, 2020, **279**, 118498.
- 545 H. A. Baloch, S. Nizamuddin, M. T. H. Siddiqui, N. M. Mubarak, S. Mazari, G. J. Griffin and M. P. Srinivasan, Co-liquefaction of synthetic polyethylene and polyethylene bags with sugarcane bagasse under supercritical conditions: A comparative study, *Renewable Energy*, 2020, **162**, 2397–2407.
- 546 H. A. Baloch, M. T. H. Siddiqui, S. Nizamuddin, N. M. Mubarak, M. Khalid, M. P. Srinivasan and G. J. Griffin, Solvothermal co-liquefaction of sugarcane bagasse and polyethylene under sub-supercritical conditions: Optimization of process parameters, *Process Saf. Environ. Prot.*, 2020, **137**, 300–311.
- 547 Z. Dai, B. Hatano, J. I. Kadokawa and H. Tagaya, Effect of diaminotoluene on the decomposition of polyurethane foam waste in superheated water, *Polym. Degrad. Stab.*, 2002, **76**, 179–184.
- 548 M. Goto, M. Sasaki and T. Hirose, Reactions of polymers in supercritical fluids for chemical recycling of waste plastics, *J. Mater. Sci.*, 2006, **41**, 1509–1515.
- 549 H. Kwak, H. Y. Shin, S. Y. Bae and H. Kumazawa, Characteristics and kinetics of degradation of polystyrene in supercritical water, *J. Appl. Polym. Sci.*, 2006, **101**, 695–700.
- 550 M. Watanabe, H. Hirakoso, S. Sawamoto, T. Adschiri and K. Arai, Polyethylene conversion in supercritical water, *J. Supercrit. Fluids*, 1998, **13**, 247–252.
- 551 M. Sugano, A. Komatsu, M. Yamamoto, M. Kumagai, T. Shimizu, K. Hirano and K. Mashimo, Liquefaction process for a hydrothermally treated waste mixture containing plastics, *J. Mater. Cycles Waste Manage.*, 2009, **11**, 27–31.
- 552 A. Tukker, H. De Groot, L. Simons and S. Wiegiersma, *Chemical Recycling of Plastics Waste (PVC and other resins)*, Delft, Netherlands, 1999.
- 553 A. Okuwaki, T. Yoshioka, M. Asai, H. Tachibana, K. Wakai and K. Tada, The Liquefaction of Plastic Containers and Packaging in Japan, in *Feedstock Recycling and Pyrolysis of Waste Plastics: Converting Waste Plastics into Diesel and Other Fuels*, ed. J. Scheirs and W. Kaminsky, John Wiley & Sons, 2006, pp. 665–708.
- 554 T. E. Loop, J. D. Flynn, G. Allan, S. C. Van Swearingen and K. O. Gaw, Biomass and waste plastics depolymerization machine and methods via supercritical water, *US Pat.*, XTRUDX Technologies Inc, 8980143, 2015.
- 555 Y. Ishihara, K. Saido and T. Kuroki, Economic evaluation of small liquefaction plants for waste plastics, *Sekiyu Gakkaishi*, 2003, **46**, 77–83.
- 556 A. Okuwaki, Feedstock recycling of plastics in Japan, *Polym. Degrad. Stab.*, 2004, **85**, 981–988.
- 557 Plastic Waste Management Institute, *An Introduction to Plastic Recycling*, Tokyo, Japan, 2019, pp. 21–22.



- 558 Licella Holdings Cat-HTR™: A Bridge to a lower carbon future, Sydney, Australia, 2019.
- 559 Mura Technology Limited Hydro-PRS Technology. <https://muratechnology.com/technology/> (accessed 2022-01-18).
- 560 Licella Holdings Plastic Waste – Advanced Recycling Feasibility Study, Geelong-Altona Industrial Corridor, Sydney, Australia, 2021; pp. 26–38.
- 561 Licella Holdings Plastics Cat-HTR™. <https://www.licella.com/solutions/plastic/> (accessed 2022-01-18).
- 562 Aduro Clean Technologies Inc. Valuable 21st century resources from plastic waste and other low-value feedstocks. <https://adurocleantech.com/about-us/> (accessed 2022-01-18).
- 563 Aduro Clean Technologies Inc. Hydrochemolytic Plastic Upcycling. <https://adurocleantech.com/hpu/> (accessed 2022-01-18).
- 564 S. Jarunthammachote and A. Dutta, Thermodynamic equilibrium model and second law analysis of a down-draft waste gasifier, *Energy*, 2007, **32**(9), 1660–1669.
- 565 U. Arena, Process and technological aspects of municipal solid waste gasification. A review, *Waste Manage.*, 2012, **32**(4), 625–639.
- 566 U. Arena, M. L. Mastellone and F. Perugini, The environmental performance of alternative solid waste management options: a life cycle assessment study, *Chem. Eng. J.*, 2003, **96**(1–3), 207–222.
- 567 C. H. Bartholomew and R. J. Farrauto, *Fundamentals of industrial catalytic processes*, John Wiley & Sons, 2011.
- 568 J. Dong, Y. Tang, A. Nzihou, Y. Chi, E. Weiss-Hortala and M. Ni, Life cycle assessment of pyrolysis, gasification and incineration waste-to-energy technologies: Theoretical analysis and case study of commercial plants, *Sci. Total Environ.*, 2018, **626**, 744–753.
- 569 Y.-C. Seo, M. T. Alam and W.-S. Yang, in *Gasification of Municipal Solid Waste*, ed. Y. Yun, InTech, 2018, pp. 115–136.
- 570 F. N. a. Sidek, Review on effects of gasifying agents, temperature and equivalence ratio in biomass gasification process, *IOP Conference Series: Materials Science and Engineering*, 2020, **863**(1), p. 012028.
- 571 P. Xu, Y. Jin and Y. Cheng, Thermodynamic Analysis of the Gasification of Municipal Solid Waste, *Engineering*, 2017, **3**(3), 416–422.
- 572 L. Zhao, H. Wang, S. Qing and H. Liu, Characteristics of gaseous product from municipal solid waste gasification with hot blast furnace slag, *J. Nat. Gas Chem.*, 2010, **19**(4), 403–408.
- 573 H. A. Arafat and K. Ijjakli, Modeling and comparative assessment of municipal solid waste gasification for energy production, *Waste Manage.*, 2013, **33**(8), 1704–1713.
- 574 S. Chen, A. Meng, Y. Long, H. Zhou, Q. Li and Y. Zhang, TGA pyrolysis and gasification of combustible municipal solid waste, *J. Energy Inst.*, 2015, **88**(3), 332–343.
- 575 M. Cortazar, J. Alvarez, G. Lopez, M. Amutio, L. Santamaria, J. Bilbao and M. Olazar, Role of temperature on gasification performance and tar composition in a fountain enhanced conical spouted bed reactor, *Energy Convers. Manage.*, 2018, **171**, 1589–1597.
- 576 R. C. Brown, *Thermochemical processing of biomass: conversion into fuels, chemicals and power*, John Wiley & Sons, 2019.
- 577 G. W. Huber, S. Iborra and A. Corma, Synthesis of transportation fuels from biomass: chemistry, catalysts, and engineering, *Chem. Rev.*, 2006, **106**(9), 4044–4098.
- 578 A. Bolt, I. Dincer and M. Agelin-Chaab, A critical review of synthetic natural gas production techniques and technologies, *J. Nat. Gas Sci. Eng.*, 2020, 103670.
- 579 M. R. Gogate, Methanol-to-olefins process technology: current status and future prospects, *Pet. Sci. Technol.*, 2019, **37**(5), 559–565.
- 580 C. Higman, State of the gasification industry: Worldwide gasification and syngas databases 2016 update. Available at <https://www.gasification-syngas.org/uploads/downloads/2016-presentations/2016-Wed-Higman.pdf>. Accessed June 2016, 8, 2017.
- 581 Edmonton to be Site of World's First Industrial Scale Municipal Waste-to-Ethanol Facility. <https://www.theauto-channel.com/news/2008/06/26/091250.html> (accessed Feb 02).
- 582 Enkern project pipeline worldwide. <https://enkern.com/company/facilities-projects/> (accessed Feb 02).
- 583 R. Voss, R. P. Lee, L. Seidl, F. Keller and M. Frhling, Global warming potential and economic performance of gasification-based chemical recycling and incineration pathways for residual municipal solid waste treatment in Germany, *Waste Manage.*, 2021, **134**, 206–219.
- 584 F. Di Gregorio and L. Zaccariello, Fluidized bed gasification of a packaging derived fuel: energetic, environmental and economic performances comparison for waste-to-energy plants, *Energy*, 2012, **42**(1), 331–341.
- 585 J. Daniel-Gromke, N. Rensberg, V. Denysenko, M. Trommler, T. Reinholz, K. Vller, M. Beil and W. Beyrich, Anlagenbestand Biogas und Biomethan-Biogaserzeugung und-nutzung in Deutschland, *DBFZ Rep.*, 2017, (30), 7.
- 586 S. Billiet and S. R. Trenor, 100th Anniversary of Macromolecular Science Viewpoint: Needs for Plastics Packaging Circularity, *ACS Macro Lett.*, 2020, **9**(9), 1376–1390.
- 587 J. G. Poulakis and C. D. Papaspyrides, The dissolution/precipitation technique applied on high density polyethylene: I. Model recycling experiments, *Adv. Polym. Technol.*, 1995, **14**, 237–242.
- 588 D. Triebert, H. Hanel, M. Bundt and K. Wahnig, Solvent-Based Recycling, in *Circular Economy of Polymers: Topics in Recycling Technologies*, ACS Publications, 2021, pp. 33–59.
- 589 J. Brandrup, E. H. Immergut, E. A. Grulke, A. Abe and D. R. Bloch, *Polymer handbook*, Wiley, New York, 1999, vol. 89.
- 590 M. Rubinstein and R. H. Colby, *Polymer physics*, Oxford university press, 2003.
- 591 K. Sändig, Process for producing particularly stable condensation products, US2061635, 1936.



- 592 D. W. Young and W. J. Sparks, Preparation of purified polyesters, US2491350, 1949.
- 593 R. B. Seymour and G. A. Stahl, Separation of waste plastics: An experiment in solvent fractionation J, *Chem. Educ.*, 1976, **53**(10), 653.
- 594 J. Teti, Process for polymer recovery, US3696058, 1972.
- 595 N. C. Sidebotham, P. D. Shoemaker and C. W. Young, Polyester polymer recovery, US4064079, 1977.
- 596 E. B. Nauman and J. C. Lynch, Polymer recycling by selective dissolution, US5198471, 1993.
- 597 E. B. Nauman and J. C. Lynch, Polymer recycling by selective dissolution, US5278282, 1994.
- 598 J. G. Poulakis and C. D. Papaspyrides, Recycling of polypropylene by the dissolution/reprecipitation technique: I. A model study, *Resour., Conserv. Recycl.*, 1997, **20**(1), 31–41.
- 599 E. M. Kampouris, C. D. Papaspyrides and C. N. Lekakou, A model process for scrap polystyrene foam by means of solvent systems, *Conserv. Recycl.*, 1987, **10**(4), 315–319.
- 600 E. M. Kampouris, C. D. Papaspyrides and C. N. Lekakou, A Model Process for the Solvent Recycling of Polystyrene, *Polym. Eng. Sci.*, 1988, **28**(8), 534–537.
- 601 E. M. Kampouris, D. C. Diakoulaki and C. D. Papaspyrides, Solvent Recycling of Rigid Poly(Vinyl Chloride) Bottles, *J. Vinyl Technol.*, 1986, **8**(2), 79–82.
- 602 C. D. Papaspyrides, J. G. Poulakis and P. C. Varelides, A model recycling process for low density polyethylene, *Resour., Conserv. Recycl.*, 1994, **12**(3–4), 177–184.
- 603 G. Pappa, C. Boukouvalas, C. Giannaris, N. Ntaras, V. Zografos, K. Magoulas, A. Lygeros and D. Tassios, The selective dissolution/precipitation technique for polymer recycling: a pilot unit application, *Resour., Conserv. Recycl.*, 2001, **34**(1), 33–44.
- 604 J. G. Poulakis; and C. D. Papaspyrides, Dissolution/Reprecipitation: A Model Process for PET Bottle Recycling, *J. Appl. Polym. Sci.*, 2001, **81**, 91–95.
- 605 Accelerating circular supply chains for plastics: A landscape of transformational technologies that stop plastic waste, keep materials in pay and grow markets. <https://www.closedlooppartners.com/research/advancing-circular-systems-for-plastics/>.
- 606 B. K. C. Sharma, Sraaam Beneficial Use of Plastic Wastes. <https://hdl.handle.net/2142/113454> (accessed Feb 02).
- 607 S. R. Chandrasekaran, S. Avasarala, D. Murali, N. Rajagopalan and B. K. Sharma, Materials and energy recovery from e-waste plastics, *ACS Sustainable Chem. Eng.*, 2018, **6**(4), 4594–4602.
- 608 I. Georgiopoulou, G. D. Pappa, S. N. Vouyiouka and K. Magoulas, Recycling of post-consumer multilayer Tetra Pak® packaging with the Selective Dissolution-Precipitation process, *Resour., Conserv. Recycl.*, 2021, **165**, 105268.
- 609 K. L. Sánchez-Rivera, P. Zhou, M. S. Kim, L. D. González Chávez, S. Grey, K. Nelson, S. C. Wang, I. Hermans, V. M. Zavala and R. C. Van Lehn, Reducing Antisolvent Use in the STRAP Process by Enabling a Temperature-Controlled Polymer Dissolution and Precipitation for the Recycling of Multilayer Plastic Films, *ChemSusChem*, 2021, **14**(19), 4317–4329.
- 610 T. W. Walker, N. Frelka, Z. Shen, A. K. Chew, J. Banick, S. Grey, M. S. Kim, J. A. Dumesic, R. C. Van Lehn and G. W. Huber, Recycling of multilayer plastic packaging materials by solvent-targeted recovery and precipitation, *Sci. Adv.*, 2020, **6**(47), eaba7599.
- 611 D. S. Achilias, A. Giannoulis and G. Z. Papageorgiou, Recycling of polymers from plastic packaging materials using the dissolution–reprecipitation technique, *Polym. Bull.*, 2009, **63**(3), 449–465.
- 612 R. Côté, Processes for recycling polystyrene waste, US20200165407A1, 2019.
- 613 A. J. Hadi, G. F. Najmuldeen and K. B. Yusoh, Dissolution/reprecipitation technique for waste polyolefin recycling using new pure and blend organic solvents, *J. Polym. Eng.*, 2013, **33**(5), 471–481.
- 614 A. J. Hadi, G. F. Najmuldeen and I. Ahmed, Polyolefins Waste Materials Reconditioning Using Dissolution/Reprecipitation Method, *APCBEE Proc.*, 2012, **3**, 281–286.
- 615 J. M. Layman, D. I. Collias, H. Schonemann and K. Williams, Method for purifying reclaimed polymers, US10961366, 2021.
- 616 K. F. Drain, W. R. Murphy and M. S. Otterburn, A solvent technique for the recycling of polypropylene—degradation on recycling, *Conserv. Recycl.*, 1983, **6**(3), 123–137.
- 617 W. Chen, Y. Yang, X. Lan, B. Zhang, X. Zhang and T. Mu, Biomass-derived  $\gamma$ -valerolactone: efficient dissolution and accelerated alkaline hydrolysis of polyethylene terephthalate, *Green Chem.*, 2021, **23**(11), 4065–4073.
- 618 E. Siggel and J. Klein, Dissolution and purification of polyethylene terephthalate, US2762788, 1956.
- 619 G. S. Weeden Jr., N. H. Soepriatna and N. H. Wang, Method for efficient recovery of high-purity polycarbonates from electronic waste, *Environ. Sci. Technol.*, 2015, **49**(4), 2425–2433.
- 620 C. Kartalis, J. Poulakis, C. Tsenoglou and C. Papaspyrides, Pure component recovery from polyamide 6/6 6 mixtures by selective dissolution and reprecipitation, *J. Appl. Polym. Sci.*, 2002, **86**(8), 1924–1930.
- 621 S. Ugduler, K. M. Van Geem, M. Roosen, E. I. P. Delbeke and S. De Meester, Challenges and opportunities of solvent-based additive extraction methods for plastic recycling, *Waste Manage.*, 2020, **104**, 148–182.
- 622 K. Kaiser, M. Schmid and M. Schlummer, Recycling of Polymer-Based Multilayer Packaging: A Review, *Recycling*, 2018, **3**(1), 1.
- 623 S. Ugduler, T. De Somer, K. M. Van Geem, M. Roosen, A. Kulawig, R. Leineweber and S. De Meester, Towards a Better Understanding of Delamination of Multilayer Flexible Packaging Films by Carboxylic Acids, *ChemSusChem*, 2021, **14**(19), 4198–4213.
- 624 O. Horodytska, F. J. Valdés and A. Fullana, Plastic flexible films waste management—A state of art review, *Waste Manage.*, 2018, **77**, 413–425.



- 625 T. Bauer, H.-G. Krebber, C. Nover and R. Saffert, Process for the recovery of a polymer from a polymer coating on a support. November 3, 2005 2005.
- 626 K. Wohnig, *Sustainable Plastic Innovation: Closing the Loop*, GPCA PlastiCon, 2018.
- 627 M. Niaounakis, *Recycling of Flexible Plastic Packaging*, William Andrew, 2020.
- 628 R. Coker, APK deploys downstream melt processing system. [https://www.brazilianplastics.com/edicao00/02\\_December2019.html#:~:text=December%204%2C%202019%3A%20APK%20AG,properties%20close%20to%20virgin%20resin](https://www.brazilianplastics.com/edicao00/02_December2019.html#:~:text=December%204%2C%202019%3A%20APK%20AG,properties%20close%20to%20virgin%20resin). (accessed March 17, 2022).
- 629 K. Wohnig, M. Kaina, M. Fleig and H. Hanel, Solvent and method for dissolving a plastic from a solid within a suspension, DE102016015198A1, 2018.
- 630 K. Wohnig, M. Kaina, M. Fleig and J. Jeschke, Gas-tight centrifuge for separating solids from a polymer solution, and method for separating solids from a polymer solution, DE102016015197A1, 2018.
- 631 C. P. Ashcroft, P. J. Dunn, J. D. Hayler and A. S. Wells, Survey of solvent usage in papers published in organic process research & development 1997–2012, *Org. Process Res. Dev.*, 2015, **19**(7), 740–747.
- 632 A. Mäurer, M. Schlummer, F. Knappich, T. Fell, A. Berrang and R. Leizinger, Method for Recycling Polyolefin Containing Waste, EP3305839 A1, 2018.
- 633 A. Maeurer, M. Schlummer and O. Beck, Methods for recycling plastic materials and use thereof, US8138232B2, 2006.
- 634 F. P. Byrne, S. Jin, G. Paggiola, T. H. Petchey, J. H. Clark, T. J. Farmer, A. J. Hunt, C. Robert McElroy and J. Sherwood, Tools and techniques for solvent selection: green solvent selection guides, *Sustainable Chem. Processes*, 2016, **4**(1), 1–24.
- 635 Plasteurope VINYLLOOP: Closure of operation in Italy/Phthalates issue under REACH brings down European PVC recycling project. [https://www.plasteurope.com/news/Closure\\_of\\_operation\\_in\\_Italy\\_Phthalates\\_issue\\_under\\_REACH\\_brings\\_down\\_VINYLLOOP/](https://www.plasteurope.com/news/Closure_of_operation_in_Italy_Phthalates_issue_under_REACH_brings_down_VINYLLOOP/) (accessed Feb 1).
- 636 Caliendo, H., Unilever Introduces Process to Recycle Multilayer Sachets. <https://www.ptonline.com/blog/post/unilever-introduces-process-to-recycle-multilayer-sachets> (accessed March 6, 2022).
- 637 Plastic Recycling Plants. <https://www.creacycle.de/en/crea-solv-plants.html> (accessed February 15, 2022).
- 638 J. M. Layman, M. Gunnerson, H. Schonemann and K. Williams, *Method for purifying contaminated polypropylene*, 2017.
- 639 PureCycle Technologies transforms end-of-life carpet into its UPRP resin. <https://www.recyclingtoday.com/article/purecycle-trials-carpet-recycling-using-pandg-technology/> (accessed March 21, 2022).
- 640 J. Layman, M. Gunnerson, E. Bond, A. Neltner and J. Hosmer, Articles of reclaimed polypropylene compositions, WO2017/003802A1, 2017.
- 641 J. M. Layman, D. I. Collias, H. Schonemann and K. Williams, *Method for separating and purifying polymers from reclaimed product*, US11008433, 2021.
- 642 J. M. Layman, D. I. Collias, H. Schonemann and K. Williams, *Method for purifying reclaimed polyethylene*, US10941269, 2021.
- 643 Polystyrene recycling <https://www.polystyvert.com/en/technology/>.
- 644 A. Walker, Process for extracting polyester from an article, WO2014/045062A1, 2013.
- 645 Worn Again Technologies <https://wornagain.co.uk/>.
- 646 P. Patel, Shay Sethi talks about the future of fabric recycling. *Chemical & Engineering News*, March 15, 2021.
- 647 Ambercycling. <https://ambercycle.com/technology> (accessed 15 February, 2022).
- 648 T. A. Cooper, in *Developments in End of Life Technologies for Flexible Packaging: Multilayer Films, Barrier Structures and Pouches*, Society of Plastics Engineers. Flex Pack Con., Myrtle Beach, NC, October 8 2019, ARGO Group International Myrtle Beach, NC, 2019.
- 649 Plant & Service. <https://www.saperatec.de/en/plant-service.html> (accessed March 26, 2022).
- 650 D. R. Bloch, *Solvents and non solvents for polymers*, The Wiley Database of Polymer Properties, 2003.
- 651 Y.-B. Zhao, X.-D. Lv and H.-G. Ni, Solvent-based separation and recycling of waste plastics: A review, *Chemosphere*, 2018, **209**, 707–720.
- 652 J. K. Kim, S. Thomas and P. Saha, *Multicomponent Polymeric Materials*, Springer, 2016, vol. 223.
- 653 B. A. Miller-Chou and J. L. Koenig, A review of polymer dissolution, *Prog. Polym. Sci.*, 2003, **28**(8), 1223–1270.
- 654 C. M. Hansen, *The three dimensional solubility parameter*, Danish Technical, Copenhagen, 1967, vol. 14.
- 655 R. W. Taft, J.-L. M. Abboud, M. J. Kamlet and M. H. Abraham, Linear solvation energy relations, *J. Solution Chem.*, 1985, **14**(3), 153–186.
- 656 V. Gutmann, Empirical parameters for donor and acceptor properties of solvents, *Electrochim. Acta*, 1976, **21**(9), 661–670.
- 657 C. G. Swain, M. S. Swain, A. L. Powell and S. Alunni, Solvent effects on chemical reactivity. Evaluation of anion- and cation-solvation components, *J. Am. Chem. Soc.*, 1983, **105**(3), 502–513.
- 658 C. M. Hansen, *Hansen solubility parameters: a user's handbook*, CRC press, 2007.
- 659 S. Abbott and C. M. Hansen, *Hansen solubility parameters in practice*, Hansen-Solubility, 2008.
- 660 A. Chandrasekaran, C. Kim, S. Venkatram and R. Ramprasad, A deep learning solvent-selection paradigm powered by a massive solvent/nonsolvent database for polymers, *Macromolecules*, 2020, **53**(12), 4764–4769.
- 661 P. Zhou, K. L. Sánchez-Rivera, G. W. Huber and R. C. Van Lehn, Computational Approach for Rapidly Predicting Temperature-Dependent Polymer Solubilities Using Molecular-Scale Models, *ChemSusChem*, 2021, **14**(19), 4307–4316.



- 662 A.-S. Bescond and A. Pujari, *PET Polymer*, IHS Markit, 2020.
- 663 A. J. Martín, C. Mondelli, S. D. Jaydev and J. Pérez-Ramírez, Catalytic processing of plastic waste on the rise, *Chem*, 2021, 7(6), 1487–1533.
- 664 *Recycling of polyethylene terephthalate bottles*, ed. S. Thomas, A. V. Rane, K. Kanny, V. K. Abitha and M. G. Thomas, William Andrew, Oxford, 2018.
- 665 S. M. Al-Salem, P. Lettieri and J. Baeyens, Recycling and recovery routes of plastic solid waste (PSW): A review, *Waste Manage.*, 2009, 29(10), 2625–2643.
- 666 R. D. Allen and M. I. James, Chemical Recycling of PET, in *Circular Economy of Polymers: Topics in Recycling Technologies*, American Chemical Society, 2021, vol. 1391, pp. 61–80.
- 667 G. W. Coates and Y. D. Y. L. Getzler, Chemical recycling to monomer for an ideal, circular polymer economy, *Nat. Rev. Mater.*, 2020, 5(7), 501–516.
- 668 J. Payne and M. D. Jones, The Chemical Recycling of Polyesters for a Circular Plastics Economy: Challenges and Emerging Opportunities, *ChemSusChem*, 2021, 14(19), 4041–4070.
- 669 K. Ragaert, L. Delva and K. Van Geem, Mechanical and chemical recycling of solid plastic waste, *Waste Manage.*, 2017, 69, 24–58.
- 670 A. B. Raheem, Z. Z. Noor, A. Hassan, M. K. Abd Hamid, S. A. Samsudin and A. H. Sabeen, Current developments in chemical recycling of post-consumer polyethylene terephthalate wastes for new materials production: A review, *J. Cleaner Prod.*, 2019, 225, 1052–1064.
- 671 I. Vollmer, M. J. F. Jenks, M. C. P. Roelands, R. J. White, T. van Harmelen, P. de Wild, G. P. van der Laan, F. Meirer, J. T. F. Keurentjes and B. M. Weckhuysen, Beyond Mechanical Recycling: Giving New Life to Plastic Waste, *Angew. Chem., Int. Ed.*, 2020, 59(36), 15402–15423.
- 672 D. Paszun and T. Spychar, Chemical Recycling of Poly(ethylene terephthalate), *Ind. Eng. Chem. Res.*, 1997, 36(4), 1373–1383.
- 673 S. R. Nicholson, J. E. Rorrer, A. Singh, M. O. Konev, N. A. Rorrer, A. C. Carpenter, A. J. Jacobsen, Y. Román-Leshkov and G. T. Beckham, The critical role of process analysis in chemical recycling and upcycling of waste plastics, *Annu. Rev. Chem. Biomol. Eng.*, 2022, 13, <https://assets.amazon.science/5a/a7/aa47ad51471-ba07a68b8cfc69240/the-critical-role-of-process-analysis-in-chemical-recycling-and-upcycling-of-waste-plastics.pdf>.
- 674 B. Geyer, G. Lorenz and A. Kandelbauer, Recycling of poly(ethylene terephthalate) – A review focusing on chemical methods, *EXPRESS Polym. Lett.*, 2016, 10, 559–586.
- 675 S. A. Jabarin and E. A. Lofgren, Thermal stability of polyethylene terephthalate, *Polym. Eng. Sci.*, 1984, 24(13), 1056–1063.
- 676 W. Partenheimer, Transformation of Polymers to Useful Chemical Oxidation, US6,958,373B2, 2005.
- 677 W. Partenheimer, Valuable oxygenates by aerobic oxidation of polymers using metal/bromide homogeneous catalysts, *Catal. Today*, 2003, 81(2), 117–135.
- 678 W. Partenheimer, Methodology and scope of metal/bromide autoxidation of hydrocarbons, *Catal. Today*, 1995, 23(2), 69–158.
- 679 S. Ügdüler, K. M. Van Geem, R. Denolf, M. Roosen, N. Mys, K. Ragaert and S. De Meester, Towards closed-loop recycling of multilayer and coloured PET plastic waste by alkaline hydrolysis, *Green Chem.*, 2020, 22(16), 5376–5394.
- 680 M. Han, 5 - Depolymerization of PET Bottle via Methanolysis and Hydrolysis, in *Recycling of Polyethylene Terephthalate Bottles*, ed. S. Thomas, A. Rane, K. V. K. A. Kanny and M. G. Thomas, William Andrew Publishing, 2019, pp. 85–108.
- 681 G. P. Karayannidis and D. S. Achilias, Chemical Recycling of Poly(ethylene terephthalate), *Macromol. Mater. Eng.*, 2007, 292(2), 128–146.
- 682 T. Yoshioka, M. Ota and A. Okuwaki, Conversion of a Used Poly(ethylene terephthalate) Bottle into Oxalic Acid and Terephthalic Acid by Oxygen Oxidation in Alkaline Solutions at Elevated Temperatures, *Ind. Eng. Chem. Res.*, 2003, 42(4), 675–679.
- 683 V. A. Kosmidis, D. S. Achilias and G. P. Karayannidis, Poly(ethylene terephthalate) Recycling and Recovery of Pure Terephthalic Acid. Kinetics of a Phase Transfer Catalyzed Alkaline Hydrolysis, *Macromol. Mater. Eng.*, 2001, 286(10), 640–647.
- 684 M. N. Siddiqui, D. S. Achilias, H. H. Redhwi, D. N. Bikiaris, K. A. G. Katsogiannis and G. P. Karayannidis, Hydrolytic Depolymerization of PET in a Microwave Reactor, *Macromol. Mater. Eng.*, 2010, 295(6), 575–584.
- 685 H. I. Khalaf and O. A. Hasan, Effect of quaternary ammonium salt as a phase transfer catalyst for the microwave depolymerization of polyethylene terephthalate waste bottles, *Chem. Eng. J.*, 2012, 192, 45–48.
- 686 L.-C. Hu, A. Oku, E. Yamada and K. Tomari, Alkali-Decomposition of Poly(ethylene terephthalate) in Mixed Media of Nonaqueous Alcohol and Ether. Study on Recycling of Poly(ethylene terephthalate), *Polym. J.*, 1997, 29(9), 708–712.
- 687 H. Essaddam, Polyethylene terephthalate depolymerization, US9,550,713B1, 2017.
- 688 C.-Y. Kao, B.-Z. Wan and W.-H. Cheng, Kinetics of Hydrolytic Depolymerization of Melt Poly(ethylene terephthalate), *Ind. Eng. Chem. Res.*, 1998, 37(4), 1228–1234.
- 689 J. R. Campanelli, D. G. Cooper and M. R. Kamal, Catalyzed hydrolysis of polyethylene terephthalate melts, *J. Appl. Polym. Sci.*, 1994, 53(8), 985–991.
- 690 G. Güçlü, T. Yalçınyuva, S. Özgümüş and M. Orbay, Hydrolysis of waste polyethylene terephthalate and characterization of products by differential scanning calorimetry, *Thermochim. Acta*, 2003, 404(1), 193–205.
- 691 L. Zhang, J. Gao, J. Zou and F. Yi, Hydrolysis of poly(ethylene terephthalate) waste bottles in the presence of dual functional phase transfer catalysts, *J. Appl. Polym. Sci.*, 2013, 130(4), 2790–2795.



- 692 D. Stanica-Ezeanu and D. Matei, Natural depolymerization of waste poly(ethylene terephthalate) by neutral hydrolysis in marine water, *Sci. Rep.*, 2021, **11**(1), 4431.
- 693 G. Brown and R. O'Brien, Method for recovering terephthalic acid and ethylene glycol from polyester materials, US3,952,053A, 1976.
- 694 T. Yoshioka, T. Sato and A. Okuwaki, Hydrolysis of waste PET by sulfuric acid at 150 °C for a chemical recycling, *J. Appl. Polym. Sci.*, 1994, **52**(9), 1353–1355.
- 695 T. Yoshioka, N. Okayama and A. Okuwaki, Kinetics of Hydrolysis of PET Powder in Nitric Acid by a Modified Shrinking-Core Model, *Ind. Eng. Chem. Res.*, 1998, **37**(2), 336–340.
- 696 F. Liu, X. Cui, S. Yu, Z. Li and X. Ge, Hydrolysis reaction of poly(ethylene terephthalate) using ionic liquids as solvent and catalyst, *J. Appl. Polym. Sci.*, 2009, **114**(6), 3561–3565.
- 697 W. Yang, R. Liu, C. Li, Y. Song and C. Hu, Hydrolysis of waste polyethylene terephthalate catalyzed by easily recyclable terephthalic acid, *Waste Manage.*, 2021, **135**, 267–274.
- 698 H. Kurokawa, M.-a. Ohshima, K. Sugiyama and H. Miura, Methanolysis of polyethylene terephthalate (PET) in the presence of aluminium triisopropoxide catalyst to form dimethyl terephthalate and ethylene glycol, *Polym. Degrad. Stab.*, 2003, **79**(3), 529–533.
- 699 S. Enthaler, Zinc-Catalyzed Depolymerization Reactions, *Zinc Catal.*, 2015, 207–218.
- 700 T. Sako, T. Sugeta, K. Otake, N. Nakazawa, M. Sato, K. Namiki and M. Tsugumi, Depolymerization of Polyethylene Terephthalate to Monomers with Supercritical Methanol, *J. Chem. Eng. Jpn.*, 1997, **30**(2), 342–346.
- 701 M. Hofmann, J. Sundermeier, C. Alberti and S. Enthaler, Zinc(II) acetate Catalyzed Depolymerization of Poly(ethylene terephthalate), *ChemistrySelect*, 2020, **5**(32), 10010–10014.
- 702 D. D. Pham and J. Cho, Low-energy catalytic methanolysis of poly(ethyleneterephthalate), *Green Chem.*, 2021, **23**(1), 511–525.
- 703 S. Tanaka, J. Sato and Y. Nakajima, Capturing ethylene glycol with dimethyl carbonate towards depolymerisation of polyethylene terephthalate at ambient temperature, *Green Chem.*, 2021, 9412–9416.
- 704 S. L. Fávoro, A. R. Freitas, T. A. Ganzerli, A. G. B. Pereira, A. L. Cardozo, O. Baron, E. C. Muniz, E. M. Giroto and E. Radovanovic, PET and aluminum recycling from multi-layer food packaging using supercritical ethanol, *J. Supercrit. Fluids*, 2013, **75**, 138–143.
- 705 R. E. N. De Castro, G. J. Vidotti, A. F. Rubira and E. C. Muniz, Depolymerization of poly(ethylene terephthalate) wastes using ethanol and ethanol/water in supercritical conditions, *J. Appl. Polym. Sci.*, 2006, **101**(3), 2009–2016.
- 706 P. Lozano-Martinez, T. Torres-Zapata and N. Martin-Sanchez, Directing Depolymerization of PET with Subcritical and Supercritical Ethanol to Different Monomers through Changes in Operation Conditions, *ACS Sustainable Chem. Eng.*, 2021, **9**(29), 9846–9853.
- 707 C. S. Nunes, M. J. Vieira da Silva, D. Cristina da Silva, A. d. R. Freitas, F. A. Rosa, A. F. Rubira and E. C. Muniz, PET depolymerisation in supercritical ethanol catalysed by [Bmim][BF<sub>4</sub>], *RSC Adv.*, 2014, **4**(39), 20308–20316.
- 708 J. R. Fernandes, L. P. Amaro, E. C. Muniz, S. L. Favaro and E. Radovanovic, PET depolymerization in supercritical ethanol conditions catalysed by nanoparticles of metal oxides, *J. Supercrit. Fluids*, 2020, **158**, 104715.
- 709 J. Xin, Q. Zhang, J. Huang, R. Huang, Q. Z. Jaffery, D. Yan, Q. Zhou, J. Xu and X. Lu, Progress in the catalytic glycolysis of polyethylene terephthalate, *J. Environ. Manage.*, 2021, **296**, 113267.
- 710 J. Y. Chen, C. F. Ou, Y. C. Hu and C. C. Lin, Depolymerization of poly(ethylene terephthalate) resin under pressure, *J. Appl. Polym. Sci.*, 1991, **42**(6), 1501–1507.
- 711 U. R. Vaidya and V. M. Nadkarni, Polyester polyols from glycolized PET waste: Effect of glycol type on kinetics of polyesterification, *J. Appl. Polym. Sci.*, 1989, **38**(6), 1179–1190.
- 712 S. Baliga and W. T. Wong, Depolymerization of poly(ethylene terephthalate) recycled from post-consumer soft-drink bottles, *J. Polym. Sci., Part A: Polym. Chem.*, 1989, **27**(6), 2071–2082.
- 713 G. Güçlü, A. Kaşgöz, S. Özbudak, S. Özgümüş and M. Orbay, Glycolysis of poly(ethylene terephthalate) wastes in xylene, *J. Appl. Polym. Sci.*, 1998, **69**(12), 2311–2319.
- 714 S. H. Mansour and N. E. Ikladios, Depolymerization of poly(ethylene terephthalate) wastes using 1,4-butanediol and triethylene glycol, *Polym. Test.*, 2002, **21**(5), 497–505.
- 715 C.-H. Chen, Study of glycolysis of poly(ethylene terephthalate) recycled from postconsumer soft-drink bottles. III. Further investigation, *J. Appl. Polym. Sci.*, 2003, **87**(12), 2004–2010.
- 716 M. Ghaemy and K. Mossaddegh, Depolymerisation of poly(ethylene terephthalate) fibre wastes using ethylene glycol, *Polym. Degrad. Stab.*, 2005, **90**(3), 570–576.
- 717 K. Troev, G. Grancharov, R. Tsevi and I. Gitsov, A novel catalyst for the glycolysis of poly(ethylene terephthalate), *J. Appl. Polym. Sci.*, 2003, **90**(4), 1148–1152.
- 718 P. Fang, B. Liu, J. Xu, Q. Zhou, S. Zhang, J. Ma and X. Lu, High-efficiency glycolysis of poly(ethylene terephthalate) by sandwich-structure polyoxometalate catalyst with two active sites, *Polym. Degrad. Stab.*, 2018, **156**, 22–31.
- 719 H. Wang, Y. Liu, Z. Li, X. Zhang, S. Zhang and Y. Zhang, Glycolysis of poly(ethylene terephthalate) catalyzed by ionic liquids, *Eur. Polym. J.*, 2009, **45**(5), 1535–1544.
- 720 Q. Wang, X. Lu, X. Zhou, M. Zhu, H. He and X. Zhang, 1-Allyl-3-methylimidazolium halometallate ionic liquids as efficient catalysts for the glycolysis of poly(ethylene terephthalate), *J. Appl. Polym. Sci.*, 2013, **129**(6), 3574–3581.
- 721 M. Khoonkari, A. H. Haghighi, Y. Sefidbakht, K. Shekoohi and A. Ghaderian, Chemical Recycling of PET Wastes with Different Catalysts, *Int. J. Polym. Sci.*, 2015, **2015**, 124524.



- 722 H. Wang, Z. Li, Y. Liu, X. Zhang and S. Zhang, Degradation of poly(ethylene terephthalate) using ionic liquids, *Green Chem.*, 2009, **11**(10), 1568–1575.
- 723 H. Wang, R. Yan, Z. Li, X. Zhang and S. Zhang, Fe-containing magnetic ionic liquid as an effective catalyst for the glycolysis of poly(ethylene terephthalate), *Catal. Commun.*, 2010, **11**(8), 763–767.
- 724 S. Cot, M. K. Leu, A. Kalamiotis, G. Dimitrakis, V. Sans, I. de Pedro and I. Cano, An Oxalate-Bridged Binuclear Iron(III) Ionic Liquid for the Highly Efficient Glycolysis of Polyethylene Terephthalate under Microwave Irradiation, *ChemPlusChem*, 2019, **84**(7), 786–793.
- 725 Q. F. Yue, C. X. Wang, L. N. Zhang, Y. Ni and Y. X. Jin, Glycolysis of poly(ethylene terephthalate) (PET) using basic ionic liquids as catalysts, *Polym. Degrad. Stab.*, 2011, **96**(4), 399–403.
- 726 A. P. Abbott, E. I. Ahmed, R. C. Harris and K. S. Ryder, Evaluating water miscible deep eutectic solvents (DESS) and ionic liquids as potential lubricants, *Green Chem.*, 2014, **16**(9), 4156–4161.
- 727 D. V. Wagle, H. Zhao and G. A. Baker, Deep Eutectic Solvents: Sustainable Media for Nanoscale and Functional Materials, *Acc. Chem. Res.*, 2014, **47**(8), 2299–2308.
- 728 E. Sert, E. Yilmaz and F. S. Atalay, Chemical Recycling of Polyethylene Terephthalate by Glycolysis Using Deep Eutectic Solvents, *J. Polym. Environ.*, 2019, **27**(12), 2956–2962.
- 729 S. R. Shukla, V. Palekar and N. Pingale, Zeolite catalyzed glycolysis of poly(ethylene terephthalate) bottle waste, *J. Appl. Polym. Sci.*, 2008, **110**(1), 501–506.
- 730 A. M. Al-Sabagh, F. Z. Yehia, D. R. K. Harding, G. Eshaq and A. E. ElMetwally, Fe<sub>3</sub>O<sub>4</sub>-boosted MWCNT as an efficient sustainable catalyst for PET glycolysis, *Green Chem.*, 2016, **18**(14), 3997–4003.
- 731 F. R. Veregue, C. T. Pereira da Silva, M. P. Moisés, J. G. Meneguín, M. R. Guilherme, P. A. Arroyo, S. L. Favaro, E. Radovanovic, E. M. Giroto and A. W. Rinaldi, Ultrasmall Cobalt Nanoparticles as a Catalyst for PET Glycolysis: A Green Protocol for Pure Hydroxyethyl Terephthalate Precipitation without Water, *ACS Sustainable Chem. Eng.*, 2018, **6**(9), 12017–12024.
- 732 Z. Laldinpuii, S. Lalmangaihzuale, Z. Pachuau and K. Vanlaldinpuia, Depolymerization of poly(ethylene terephthalate) waste with biomass-waste derived recyclable heterogeneous catalyst, *Waste Manage.*, 2021, **126**, 1–10.
- 733 Z. Wang, Y. Wang, S. Xu, Y. Jin, Z. Tang, G. Xiao and H. Su, A pseudo-homogeneous system for PET glycolysis using a colloidal catalyst of graphite carbon nitride in ethylene glycol, *Polym. Degrad. Stab.*, 2021, **190**, 109638.
- 734 S. Najafi-Shoa, M. Barikani, M. Ehsani and M. Ghaffari, Cobalt-based ionic liquid grafted on graphene as a heterogeneous catalyst for poly (ethylene terephthalate) glycolysis, *Polym. Degrad. Stab.*, 2021, **192**, 109691.
- 735 A. M. Al-Sabagh, F. Z. Yehia, G. Eshaq and A. E. ElMetwally, Ionic Liquid-Coordinated Ferrous Acetate Complex Immobilized on Bentonite As a Novel Separable Catalyst for PET Glycolysis, *Ind. Eng. Chem. Res.*, 2015, **54**(50), 12474–12481.
- 736 I. Cano, C. Martin, J. A. Fernandes, R. W. Lodge, J. Dupont, F. A. Casado-Carmona, R. Lucena, S. Cardenas, V. Sans and I. de Pedro, Paramagnetic ionic liquid-coated SiO<sub>2</sub>@Fe<sub>3</sub>O<sub>4</sub> nanoparticles—The next generation of magnetically recoverable nanocatalysts applied in the glycolysis of PET, *Appl. Catal., B*, 2020, **260**, 118110.
- 737 K. Fukushima, O. Coulembier, J. M. Lecuyer, H. A. Almegren, A. M. Alabdulrahman, F. D. Alsewaleim, M. A. McNeil, P. Dubois, R. M. Waymouth, H. W. Horn, J. E. Rice and J. L. Hedrick, Organocatalytic depolymerization of poly(ethylene terephthalate), *J. Polym. Sci., Part A: Polym. Chem.*, 2011, **49**(5), 1273–1281.
- 738 K. Fukushima, D. J. Coady, G. O. Jones, H. A. Almegren, A. M. Alabdulrahman, F. D. Alsewaleim, H. W. Horn, J. E. Rice and J. L. Hedrick, Unexpected efficiency of cyclic amidine catalysts in depolymerizing poly(ethylene terephthalate), *J. Polym. Sci., Part A: Polym. Chem.*, 2013, **51**(7), 1606–1611.
- 739 C. Jehanno, I. Flores, A. P. Dove, A. J. Müller, F. Ruipérez and H. Sardon, Organocatalysed depolymerisation of PET in a fully sustainable cycle using thermally stable protic ionic salt, *Green Chem.*, 2018, **20**(6), 1205–1212.
- 740 N. D. Pingale and S. R. Shukla, Microwave assisted eco-friendly recycling of poly (ethylene terephthalate) bottle waste, *Eur. Polym. J.*, 2008, **44**(12), 4151–4156.
- 741 S. Chaudhary, P. Surekha, D. Kumar, C. Rajagopal and P. K. Roy, Microwave assisted glycolysis of poly(ethylene terephthalate) for preparation of polyester polyols, *J. Appl. Polym. Sci.*, 2013, **129**(5), 2779–2788.
- 742 D. S. Achilias, H. H. Redhwi, M. N. Siddiqui, A. K. Nikolaidis, D. N. Bikiaris and G. P. Karayannidis, Glycolytic depolymerization of PET waste in a microwave reactor, *J. Appl. Polym. Sci.*, 2010, **118**(5), 3066–3073.
- 743 O. Saravari, P. Potiyaraj and S. Phunphoem, Preparation of Urethane Oils from Microwave-Assisted Glycolyzed Products of Waste PET Bottles, *Energy Procedia*, 2011, **9**, 491–497.
- 744 M. Parrott, Chemical recycling of polyethylene terephthalate by microwave irradiation, US10,858,493B2, 2020.
- 745 K. Fukushima, J. M. Lecuyer, D. S. Wei, H. W. Horn, G. O. Jones, H. A. Al-Megren, A. M. Alabdulrahman, F. D. Alsewaleim, M. A. McNeil, J. E. Rice and J. L. Hedrick, Advanced chemical recycling of poly(ethylene terephthalate) through organocatalytic aminolysis, *Polym. Chem.*, 2013, **4**(5), 1610–1616.
- 746 H. Zahn and H. Pfeifer, Aminolysis of polyethylene terephthalate, *Polymer*, 1963, **4**, 429–432.
- 747 R. K. Soni, M. Teotia and K. Dutt, Studies on synthesis and characterization of a novel acrylic aromatic amide oligomer of aminolysed endproducts generated from pet waste with hydrazine monohydrate and its photocuring with acrylate monomers, *J. Appl. Polym. Sci.*, 2010, **118**(2), 638–645.



- 748 A. Bhatnagar, R. Padhan, A. Gupta and K. Agadi, An environment friendly method for disposal of waste plastics through conversion of polyethylene terephthalate (pet) polymers to anti-stripping compounds, *WO2013/118057A1*, 2013.
- 749 R. K. Soni and S. Singh, Synthesis and characterization of terephthalamides from poly(ethylene terephthalate) waste, *J. Appl. Polym. Sci.*, 2005, **96**(5), 1515–1528.
- 750 S. R. Shukla and A. M. Harad, Aminolysis of polyethylene terephthalate waste, *Polym. Degrad. Stab.*, 2006, **91**(8), 1850–1854.
- 751 M. E. Tawfik and S. B. Eskander, Chemical recycling of poly(ethylene terephthalate) waste using ethanolamine. Sorting of the end products, *Polym. Degrad. Stab.*, 2010, **95**(2), 187–194.
- 752 K. Chan and A. Zinchenko, Conversion of waste bottles' PET to a hydrogel adsorbent via PET aminolysis, *J. Environ. Chem. Eng.*, 2021, **9**(5), 106129.
- 753 K. Fukushima, G. O. Jones, H. W. Horn, J. E. Rice, T. Kato and J. L. Hedrick, Formation of bis-benzimidazole and bis-benzoxazole through organocatalytic depolymerization of poly(ethylene terephthalate) and its mechanism, *Polym. Chem.*, 2020, **11**(30), 4904–4913.
- 754 N. D. Pingale and S. R. Shukla, Microwave-assisted aminolytic depolymerization of PET waste, *Eur. Polym. J.*, 2009, **45**(9), 2695–2700.
- 755 C. N. Hoang and Y. H. Dang, Aminolysis of poly(ethylene terephthalate) waste with ethylenediamine and characterization of  $\alpha,\omega$ -diamine products, *Polym. Degrad. Stab.*, 2013, **98**(3), 697–708.
- 756 D. S. Achilias, G. P. Tsintzou, A. K. Nikolaidis, D. N. Bikiaris and G. P. Karayannidis, Aminolytic depolymerization of poly(ethylene terephthalate) waste in a microwave reactor, *Polym. Int.*, 2011, **60**(3), 500–506.
- 757 P. Sharma, B. Lochab, D. Kumar and P. K. Roy, Sustainable Bis-benzoxazines from Cardanol and PET-Derived Terephthalamides, *ACS Sustainable Chem. Eng.*, 2016, **4**(3), 1085–1093.
- 758 M. T. Martello and M. A. Hillmyer, Polylactide-Poly(6-methyl- $\epsilon$ -caprolactone)-Polylactide Thermoplastic Elastomers, *Macromolecules*, 2011, **44**(21), 8537–8545.
- 759 K. Tanemura, T. Suzuki, Y. Nishida and T. Horaguchi, Synthesis of the sulfonated condensed polynuclear aromatic (S-COPNA) resins as strong protonic acids, *Tetrahedron*, 2011, **67**(6), 1314–1319.
- 760 Y. Luo, S. Zhang, Y. Ma, W. Wang and B. Tan, Microporous organic polymers synthesized by self-condensation of aromatic hydroxymethyl monomers, *Polym. Chem.*, 2013, **4**(4), 1126–1131.
- 761 E. M. Krall, T. W. Klein, R. J. Andersen, A. J. Nett, R. W. Glasgow, D. S. Reader, B. C. Dauphinais, S. P. Mc Ilrath, A. A. Fischer, M. J. Carney, D. J. Hudson and N. J. Robertson, Controlled hydrogenative depolymerization of polyesters and polycarbonates catalyzed by ruthenium(II) PNN pincer complexes, *Chem. Commun.*, 2014, **50**(38), 4884–4887.
- 762 J. A. Fuentes, S. M. Smith, M. T. Scharbert, I. Carpenter, D. B. Cordes, A. M. Z. Slawin and M. L. Clarke, On the Functional Group Tolerance of Ester Hydrogenation and Polyester Depolymerisation Catalysed by Ruthenium Complexes of Tridentate Aminophosphine Ligands, *Chem. – Eur. J.*, 2015, **21**(30), 10851–10860.
- 763 S. Westhues, J. Idel and J. Klankermayer, Molecular catalyst systems as key enablers for tailored polyesters and polycarbonate recycling concepts, *Sci. Adv.*, 2018, **4**(8), eaat9669.
- 764 Y. Kratish, J. Li, S. Liu, Y. Gao and T. J. Marks, Polyethylene Terephthalate Deconstruction Catalyzed by a Carbon-Supported Single-Site Molybdenum-Dioxo Complex, *Angew. Chem., Int. Ed.*, 2020, **59**(45), 19857–19861.
- 765 Y. Jing, Y. Wang, S. Furukawa, J. Xia, C. Sun, M. J. Hülsey, H. Wang, Y. Guo, X. Liu and N. Yan, Towards the Circular Economy: Converting Aromatic Plastic Waste Back to Arenes over a Ru/Nb<sub>2</sub>O<sub>5</sub> Catalyst, *Angew. Chem., Int. Ed.*, 2021, **60**(10), 5527–5535.
- 766 P. Wu, G. Lu and C. Cai, Cobalt-molybdenum synergistic catalysis for the hydrogenolysis of terephthalate-based polyesters, *Green Chem.*, 2021, **23**(21), 8666–8672.
- 767 R. Wei and W. Zimmermann, Biocatalysis as a green route for recycling the recalcitrant plastic polyethylene terephthalate, *Microb. Biotechnol.*, 2017, **10**(6), 1302–1307.
- 768 N. Wierckx, M. A. Prieto, P. Pomposiello, V. de Lorenzo, K. O'Connor and L. M. Blank, Plastic waste as a novel substrate for industrial biotechnology, *Microb. Biotechnol.*, 2015, **8**(6), 900–903.
- 769 I. Taniguchi, S. Yoshida, K. Hiraga, K. Miyamoto, Y. Kimura and K. Oda, Biodegradation of PET: Current Status and Application Aspects, *ACS Catal.*, 2019, **9**(5), 4089–4105.
- 770 F. Kawai, T. Kawabata and M. Oda, Current State and Perspectives Related to the Polyethylene Terephthalate Hydrolases Available for Biorecycling, *ACS Sustainable Chem. Eng.*, 2020, **8**(24), 8894–8908.
- 771 R. Wei, T. Tiso, J. Bertling, K. O'Connor, L. M. Blank and U. T. Bornscheuer, Possibilities and limitations of biotechnological plastic degradation and recycling, *Nat. Catal.*, 2020, **3**(11), 867–871.
- 772 A. Carniel, V. d. A. Waldow and A. M. d. Castro, A comprehensive and critical review on key elements to implement enzymatic PET depolymerization for recycling purposes, *Biotechnol. Adv.*, 2021, **52**, 107811.
- 773 R.-J. Müller, H. Schrader, J. Profe, K. Dresler and W.-D. Deckwer, Enzymatic Degradation of Poly(ethylene terephthalate): Rapid Hydrolyse using a Hydrolase from *T. fusca*, *Macromol. Rapid Commun.*, 2005, **26**(17), 1400–1405.
- 774 X. Hu, U. Thumarat, X. Zhang, M. Tang and F. Kawai, Diversity of polyester-degrading bacteria in compost and molecular analysis of a thermoactive esterase from *Thermobifida alba* AHK119, *Appl. Microbiol. Biotechnol.*, 2010, **87**(2), 771–779.



- 775 D. Ribitsch, E. H. Acero, K. Greimel, A. Dellacher, S. Zitzenbacher, A. Marold, R. D. Rodriguez, G. Steinkellner, K. Gruber, H. Schwab and G. M. Guebitz, A New Esterase from *Thermobifida halotolerans* Hydrolyses Polyethylene Terephthalate (PET) and Polylactic Acid (PLA), *Polymers*, 2012, **4**(1), 617–629.
- 776 D. Ribitsch, E. H. Acero, K. Greimel, I. Eiteljoerg, E. Trotscha, G. Freddi, H. Schwab and G. M. Guebitz, Characterization of a new cutinase from *Thermobifida alba* for PET-surface hydrolysis, *Biocatal. Biotransform.*, 2012, **30**(1), 2–9.
- 777 C. Roth, R. Wei, T. Oeser, J. Then, C. Föllner, W. Zimmermann and N. Sträter, Structural and functional studies on a thermostable polyethylene terephthalate degrading hydrolase from *Thermobifida fusca*, *Appl. Microbiol. Biotechnol.*, 2014, **98**(18), 7815–7823.
- 778 Å.M Ronkvist, W. Xie, W. Lu and R. A. Gross, Cutinase-Catalyzed Hydrolysis of Poly(ethylene terephthalate), *Macromolecules*, 2009, **42**(14), 5128–5138.
- 779 C. Silva, S. Da, N. Silva, T. Matamá, R. Araújo, M. Martins, S. Chen, J. Chen, J. Wu, M. Casal and A. Cavaco-Paulo, Engineered *Thermobifida fusca* cutinase with increased activity on polyester substrates, *Biotechnol. J.*, 2011, **6**(10), 1230–1239.
- 780 E. Herrero Acero, D. Ribitsch, A. Dellacher, S. Zitzenbacher, A. Marold, G. Steinkellner, K. Gruber, H. Schwab and G. M. Guebitz, Surface engineering of a cutinase from *Thermobifida cellulositica* for improved polyester hydrolysis, *Biotechnol. Bioeng.*, 2013, **110**(10), 2581–2590.
- 781 J. Then, R. Wei, T. Oeser, M. Barth, M. R. Belisário-Ferrari, J. Schmidt and W. Zimmermann, Ca<sup>2+</sup> and Mg<sup>2+</sup> binding site engineering increases the degradation of polyethylene terephthalate films by polyester hydrolases from *Thermobifida fusca*, *Biotechnol. J.*, 2015, **10**(4), 592–598.
- 782 M. Furukawa, N. Kawakami, A. Tomizawa and K. Miyamoto, Efficient Degradation of Poly(ethylene terephthalate) with *Thermobifida fusca* Cutinase Exhibiting Improved Catalytic Activity Generated using Mutagenesis and Additive-based Approaches, *Sci. Rep.*, 2019, **9**(1), 16038.
- 783 C. M. Payne, B. C. Knott, H. B. Mayes, H. Hansson, M. E. Himmel, M. Sandgren, J. Ståhlberg and G. T. Beckham, Fungal Cellulases., *Chem. Rev.*, 2015, **115**(3), 1308–1448.
- 784 S. Sulaiman, S. Yamato, E. Kanaya, J. Kim, Y. Koga, K. Tanako and S. Kanaya, Isolation of a novel cutinase homolog with polyethylene terephthalate-degrading activity from leaf-branch compost by using a metagenomic approach, *Appl. Environ. Microbiol.*, 2012, **78**(5), 1556–1562.
- 785 V. Tournier, C. M. Topham, A. Gilles, B. David, C. Folgoas, E. Moya-Leclair, E. Kamionka, M. L. Desrousseaux, H. Texier, S. Gavalda, M. Cot, E. Guémard, M. Dalibey, J. Nomme, G. Cioci, S. Barbe, M. Chateau, I. André, S. Duquesne and A. Marty, An engineered PET depolymerase to break down and recycle plastic bottles, *Nature*, 2020, **580**(7802), 216–219.
- 786 A. N. Shirke, C. White, J. A. Englaender, A. Zwarycz, G. L. Butterfoss, R. J. Linhardt and R. A. Gross, Stabilizing Leaf and Branch Compost Cutinase (LCC) with Glycosylation: Mechanism and Effect on PET Hydrolysis, *Biochemistry*, 2018, **57**(7), 1190–1200.
- 787 C. Sonnendecker, J. Oeser, P. K. Richter, P. Hille, Z. Zhao, C. Fischer, H. Lippold, P. Blázquez-Sánchez, F. Engelberger, C. A. Ramírez-Sarmiento, T. Oeser, Y. Lihanova, R. Frank, H.-G. Jahnke, S. Billig, B. Abel, N. Sträter, J. Matysik and W. Zimmermann, Low Carbon Footprint Recycling of Post-Consumer PET Plastic with a Metagenomic Polyester Hydrolase, *ChemSusChem*, 2021, **15**(9), e202101062.
- 788 D. Danso, J. Chow and W. Streit, Plastics: Environmental and biotechnological perspectives on microbial degradation, *Appl. Environ. Microbiol.*, 2019, **85**(19), e01095–e01019.
- 789 D. Danso, C. Schmeisser, J. Chow, W. Zimmermann, R. Wei, C. Leggewie, X. Li, T. Hazen and W. Streit, New insights into the function and global distribution of polyethylene terephthalate (PET)-degrading bacteria and enzymes in marine and terrestrial metagenomes, *Appl. Environ. Microbiol.*, 2018, **84**(8), e02773–e02717.
- 790 S. Yoshida, K. Hiraga, T. Takehana, I. Taniguchi, H. Yamaji, Y. Maeda, K. Toyohara, K. Miyamoto, Y. Kimura and K. Oda, A bacterium that degrades and assimilates poly(ethylene terephthalate), *Science*, 2016, **351**(6278), 1196–1199.
- 791 X. Han, W. Liu, J.-W. Huang, J. Ma, Y. Zheng, T.-P. Ko, L. Xu, Y.-S. Cheng, C.-C. Chen and R.-T. Guo, Structural insight into catalytic mechanism of PET hydrolase, *Nat. Commun.*, 2017, **8**(1), 2106.
- 792 H. P. Austin, M. D. Allen, B. S. Donohoe, N. A. Rorrer, F. L. Kearns, R. L. Silveira, B. C. Pollard, G. Dominick, R. Duman, K. El Omari, V. Mykhaylyk, A. Wagner, W. E. Michener, A. Amore, M. S. Skaf, M. F. Crowley, A. W. Thorne, C. W. Johnson, H. L. Woodcock, J. E. McGeehan and G. T. Beckham, Characterization and engineering of a plastic-degrading aromatic polyesterase, *Proc. Natl. Acad. Sci. U. S. A.*, 2018, **115**(19), E4350.
- 793 T. Fecker, P. Galaz-Davison, F. Engelberger, Y. Narui, M. Sotomayor, L. P. Parra and C. A. Ramírez-Sarmiento, Active Site Flexibility as a Hallmark for Efficient PET Degradation by *I. sakaiensis* PETase, *Biophys. J.*, 2018, **114**(6), 1302–1312.
- 794 S. Joo, I. J. Cho, H. Seo, H. F. Son, H.-Y. Sagong, T. J. Shin, S. Y. Choi, S. Y. Lee and K.-J. Kim, Structural insight into molecular mechanism of poly(ethylene terephthalate) degradation, *Nat. Commun.*, 2018, **9**(1), 382.
- 795 G. J. Palm, L. Reisky, D. Böttcher, H. Müller, E. A. P. Michels, M. C. Walczak, L. Berndt, M. S. Weiss, U. T. Bornscheuer and G. Weber, Structure of the plastic-degrading *Ideonella sakaiensis* MHETase bound to a substrate, *Nat. Commun.*, 2019, **10**(1), 1717.



- 796 H. F. Son, I. J. Cho, S. Joo, H. Seo, H.-Y. Sagong, S. Y. Choi, S. Y. Lee and K.-J. Kim, Rational Protein Engineering of Thermo-Stable PETase from *Ideonella sakaiensis* for Highly Efficient PET Degradation, *ACS Catal.*, 2019, **9**(4), 3519–3526.
- 797 B. C. Knott, E. Erickson, M. D. Allen, J. E. Gado, R. Graham, F. L. Kearns, I. Pardo, E. Topuzlu, J. J. Anderson, H. P. Austin, G. Dominick, C. W. Johnson, N. A. Rorrer, C. J. Szostkiewicz, V. Copié, C. M. Payne, H. L. Woodcock, B. S. Donohoe, G. T. Beckham and J. E. McGeehan, Characterization and engineering of a two-enzyme system for plastics depolymerization, *Proc. Natl. Acad. Sci. U. S. A.*, 2020, **117**(41), 25476.
- 798 Y. Cui, Y. Chen, X. Liu, S. Dong, Y. e. Tian, Y. Qiao, R. Mitra, J. Han, C. Li, X. Han, W. Liu, Q. Chen, W. Wei, X. Wang, W. Du, S. Tang, H. Xiang, H. Liu, Y. Liang, K. N. Houk and B. Wu, Computational Redesign of a PETase for Plastic Biodegradation under Ambient Condition by the GRAPE Strategy, *ACS Catal.*, 2021, **11**(3), 1340–1350.
- 799 H. Lu, D. J. Diaz, N. J. Czarnecki, C. Zhu, W. Kim, R. Shroff, D. J. Acosta, B. Alexander, H. Cole, Y. J. Zhang, N. Lynd, A. D. Ellington and H. S. Alper, Deep learning redesign of PETase for practical PET degrading applications, *bioRxiv*, 2021, DOI: [10.1101/2021.10.10.463845](https://doi.org/10.1101/2021.10.10.463845).
- 800 A. Singh, N. A. Rorrer, S. R. Nicholson, E. Erickson, J. S. DesVeaux, A. F. T. Avelino, P. Lamers, A. Bhatt, Y. Zhang, G. Avery, L. Tao, A. R. Pickford, A. C. Carpenter, J. E. McGeehan and G. T. Beckham, Techno-economic, life-cycle, and socio-economic impact analysis of enzymatic recycling of poly(ethylene terephthalate), *Joule*, 2021, **5**(9), 2479–2503.
- 801 E. Erickson, T. J. Shakespeare, F. Bratti, B. L. Buss, R. Graham, M. A. Hawkins, G. König, W. E. Michener, J. Miscall, K. J. Ramirez, N. A. Rorrer, M. Zahn, A. R. Pickford, J. E. McGeehan and G. T. Beckham, Comparative Performance of PETase as a Function of Reaction Conditions, Substrate Properties, and Product Accumulation, *ChemSusChem*, 2021, e202101932.
- 802 R. Wei, D. Breite, C. Song, D. Gräsing, T. Ploss, P. Hille, R. Schwerdtfeger, J. Matysik, A. Schulze and W. Zimmermann, Biocatalytic Degradation Efficiency of Postconsumer Polyethylene Terephthalate Packaging Determined by Their Polymer Microstructures, *Adv. Sci.*, 2019, **6**(14), 1900491.
- 803 M. C. Delpech, F. M. B. Coutinho and M. E. S. Habibe, Bisphenol A-based polycarbonates: characterization of commercial samples, *Polym. Test.*, 2002, **21**(2), 155–161.
- 804 E. V. Antonakou and D. S. Achilias, Recent Advances in Polycarbonate Recycling: A Review of Degradation Methods and Their Mechanisms, *Waste Biomass Valorization*, 2013, **4**(1), 9–21.
- 805 J. G. Kim, Chemical recycling of poly(bisphenol A carbonate), *Polym. Chem.*, 2020, **11**(30), 4830–4849.
- 806 R. Geyer, J. R. Jambeck and K. L. Law, Production, use, and fate of all plastics ever made, *Sci. Adv.*, 2017, **3**(7), e1700782.
- 807 M. Blazsó, Thermal decomposition of polymers modified by catalytic effects of copper and iron chlorides, *J. Anal. Appl. Pyrolysis*, 1999, **51**(1), 73–88.
- 808 S.-J. Chiu, S.-H. Chen and C.-T. Tsai, Effect of metal chlorides on thermal degradation of (waste) polycarbonate, *Waste Manage.*, 2006, **26**(3), 252–259.
- 809 B. Subramaniam and M. A. McHugh, Reactions in supercritical fluids - a review, *Ind. Eng. Chem. Process Des. Dev.*, 1986, **25**(1), 1–12.
- 810 M. Watanabe, Y. Matsuo, T. Matsushita, H. Inomata, T. Miyake and K. Hironaka, Chemical recycling of polycarbonate in high pressure high temperature steam at 573 K, *Polym. Degrad. Stab.*, 2009, **94**(12), 2157–2162.
- 811 H. Weingärtner and E. U. Franck, Supercritical Water as a Solvent, *Angew. Chem., Int. Ed.*, 2005, **44**(18), 2672–2692.
- 812 T. Yoshioka, K. Sugawara, T. Mizoguchi and A. Okuwaki, Chemical Recycling of Polycarbonate to Raw Materials by Thermal Decomposition with Calcium Hydroxide/Steam, *Chem. Lett.*, 2005, **34**(3), 282–283.
- 813 G. Grause, K. Sugawara, T. Mizoguchi and T. Yoshioka, Pyrolytic hydrolysis of polycarbonate in the presence of earth-alkali oxides and hydroxides, *Polym. Degrad. Stab.*, 2009, **94**(7), 1119–1124.
- 814 G. Grause, R. Kärrbrant, T. Kameda and T. Yoshioka, Steam Hydrolysis of Poly(bisphenol A carbonate) in a Fluidized Bed Reactor, *Ind. Eng. Chem. Res.*, 2014, **53**(11), 4215–4223.
- 815 G. O. Jones, A. Yuen, R. J. Wojtecki, J. L. Hedrick and J. M. García, Computational and experimental investigations of one-step conversion of poly(carbonate)s into value-added poly(aryl ether sulfone)s, *Proc. Natl. Acad. Sci. U. S. A.*, 2016, **113**(28), 7722.
- 816 Y. Huang, S. Liu and Z. Pan, Effects of plastic additives on depolymerization of polycarbonate in sub-critical water, *Polym. Degrad. Stab.*, 2011, **96**(8), 1405–1410.
- 817 G. Grause, N. Tsukada, W. J. Hall, T. Kameda, P. T. Williams and T. Yoshioka, High-value products from the catalytic hydrolysis of polycarbonate waste, *Polym. J.*, 2010, **42**(6), 438–442.
- 818 E. Quaranta, Rare Earth metal triflates  $M(O_3SCF_3)_3$  ( $M=Sc, Yb, La$ ) as Lewis acid catalysts of depolymerization of poly-(bisphenol A carbonate) via hydrolytic cleavage of carbonate moiety: Catalytic activity of  $La(O_3SCF_3)_3$ , *Appl. Catal., B*, 2017, **206**, 233–241.
- 819 X. Song, F. Liu, L. Li, X. Yang, S. Yu and X. Ge, Hydrolysis of polycarbonate catalyzed by ionic liquid  $[Bmim][Ac]$ , *J. Hazard. Mater.*, 2013, **244–245**, 204–208.
- 820 L. Li, F. Liu, Z. Li, X. Song and S. Yu, Hydrolysis of polycarbonate using ionic liquid  $[Bmim][Cl]$  as solvent and catalyst, *Fibers Polym.*, 2013, **14**(3), 365–368.
- 821 M. Liu, J. Guo, Y. Gu, J. Gao and F. Liu, Degradation of waste polycarbonate via hydrolytic strategy to recover monomer (bisphenol A) catalyzed by DBU-based ionic liquids under metal- and solvent-free conditions, *Polym. Degrad. Stab.*, 2018, **157**, 9–14.



- 822 G. P. Tsintzou and D. S. Achilias, Chemical Recycling of Polycarbonate Based Wastes Using Alkaline Hydrolysis Under Microwave Irradiation, *Waste Biomass Valorization*, 2013, **4**(1), 3–7.
- 823 L. Rosi, M. Bartoli, A. Undri, M. Frediani and P. Frediani, Synthesis of dianols or BPA through catalytic hydrolysis/glycolysis of waste polycarbonates using a microwave heating, *J. Mol. Catal. A: Chem.*, 2015, **408**, 278–286.
- 824 L.-C. Hu, A. Oku and E. Yamada, Alkali-catalyzed methanolysis of polycarbonate. A study on recycling of bisphenol A and dimethyl carbonate, *Polymer*, 1998, **39**(16), 3841–3845.
- 825 R. Piñero, J. García and M. J. Cocero, Chemical recycling of polycarbonate in a semi-continuous lab-plant. A green route with methanol and methanol–water mixtures, *Green Chem.*, 2005, **7**(5), 380–387.
- 826 L. Chen, Y. Wu, Y. Ni, K. Huang and Z. Zhu, Depolymerization of polycarbonate in critical region of methanol, *Acta Sci. Circumstantiae*, 2004, **24**(1), 60–64.
- 827 H. Jie, H. Ke, Z. Qing, C. Lei, W. Yongqiang and Z. Zibin, Study on depolymerization of polycarbonate in supercritical ethanol, *Polym. Degrad. Stab.*, 2006, **91**(10), 2307–2314.
- 828 D. Kim, B.-k. Kim, Y. Cho, M. Han and B.-S. Kim, Kinetics of Polycarbonate Glycolysis in Ethylene Glycol, *Ind. Eng. Chem. Res.*, 2009, **48**(2), 685–691.
- 829 B. G. G. Lohmeijer, R. C. Pratt, F. Leibfarth, J. W. Logan, D. A. Long, A. P. Dove, F. Nederberg, J. Choi, C. Wade, R. M. Waymouth and J. L. Hedrick, Guanidine and Amidine Organocatalysts for Ring-Opening Polymerization of Cyclic Esters, *Macromolecules*, 2006, **39**(25), 8574–8583.
- 830 E. Quaranta, D. Sgherza and G. Tartaro, Depolymerization of poly(bisphenol A carbonate) under mild conditions by solvent-free alcoholysis catalyzed by 1,8-diazabicyclo[5.4.0]undec-7-ene as a recyclable organocatalyst: a route to chemical recycling of waste polycarbonate, *Green Chem.*, 2017, **19**(22), 5422–5434.
- 831 E. Quaranta, C. C. Minischetti and G. Tartaro, Chemical Recycling of Poly(bisphenol A carbonate) by Glycolysis under 1,8-Diazabicyclo[5.4.0]undec-7-ene Catalysis, *ACS Omega*, 2018, **3**(7), 7261–7268.
- 832 C. Alberti and S. Enthaler, Depolymerization of End-of-Life Poly(bisphenol A carbonate) via Alkali-Metal-Halide-Catalyzed Methanolysis, *Asian J. Org. Chem.*, 2020, **9**(3), 359–363.
- 833 W. Huang, H. Wang, W. Hu, D. Yang, S. Yu, F. Liu and X. Song, Degradation of polycarbonate to produce bisphenol A catalyzed by imidazolium-based DESs under metal- and solvent-free conditions, *RSC Adv.*, 2021, **11**(3), 1595–1604.
- 834 F. Liu, Y. Xiao, X. Sun, G. Qin, X. Song and Y. Liu, Synergistic catalysis over hollow CeO<sub>2</sub>-CaO-ZrO<sub>2</sub> nanostructure for polycarbonate methanolysis with methanol, *Chem. Eng. J.*, 2019, **369**, 205–214.
- 835 M. Liu, J. Guo, Y. Gu, J. Gao, F. Liu and S. Yu, Pushing the Limits in Alcoholysis of Waste Polycarbonate with DBU-Based Ionic Liquids under Metal- and Solvent-Free Conditions, *ACS Sustainable Chem. Eng.*, 2018, **6**(10), 13114–13121.
- 836 F. Liu, J. Guo, P. Zhao, M. Jia, M. Liu and J. Gao, Novel succinimide-based ionic liquids as efficient and sustainable media for methanolysis of polycarbonate to recover bisphenol A (BPA) under mild conditions, *Polym. Degrad. Stab.*, 2019, **169**, 108996.
- 837 F. Liu, Z. Li, S. Yu, X. Cui and X. Ge, Environmentally benign methanolysis of polycarbonate to recover bisphenol A and dimethyl carbonate in ionic liquids, *J. Hazard. Mater.*, 2010, **174**(1), 872–875.
- 838 S. Hata, H. Goto, E. Yamada and A. Oku, Chemical conversion of poly(carbonate) to 1,3-dimethyl-2-imidazolidinone (DMI) and bisphenol A: a practical approach to the chemical recycling of plastic wastes, *Polymer*, 2002, **43**(7), 2109–2116.
- 839 S. Nakano and T. Kato, A new process for producing polyamide from polyester. *J. Polym. Sci., Part A: Polym. Chem.*, 1999, **37**(10), 1413–1423.
- 840 F. Iannone, M. Casiello, A. Monopoli, P. Cotugno, M. C. Sportelli, R. A. Picca, N. Cioffi, M. M. Dell'Anna and A. Nacci, Ionic liquids/ZnO nanoparticles as recyclable catalyst for polycarbonate depolymerization, *J. Mol. Catal. A: Chem.*, 2017, **426**, 107–116.
- 841 K. Hatakeyama, T. Kojima and T. Funazukuri, Chemical recycling of polycarbonate in dilute aqueous ammonia solution under hydrothermal conditions, *J. Mater. Cycles Waste Manage.*, 2014, **16**(1), 124–130.
- 842 R. Arai, K. Zenda, K. Hatakeyama, K. Yui and T. Funazukuri, Reaction kinetics of hydrothermal depolymerization of poly(ethylene naphthalate), poly(ethylene terephthalate), and polycarbonate with aqueous ammonia solution, *Chem. Eng. Sci.*, 2010, **65**(1), 36–41.
- 843 H. J. Radusch, Poly(Butylene Terephthalate), *Handbook of Thermoplastic Polyesters*, 2002, pp. 389–419.
- 844 F. G. Terrade, J. van Krieken, B. J. V. Verkuilj and E. Bouwman, Catalytic Cracking of Lactide and Poly(Lactic Acid) to Acrylic Acid at Low Temperatures, *ChemSusChem*, 2017, **10**(9), 1904–1908.
- 845 I. A. Shuklov, H. Jiao, J. Schulze, W. Tietz, K. Kühlein and A. Börner, Studies on the epimerization of diastereomeric lactides, *Tetrahedron Lett.*, 2011, **52**(9), 1027–1030.
- 846 Technology: Simple Sustainable Recycling. <https://www.depoly.ch> (accessed 01/08/22).
- 847 S. L. Anderson, C. P. Ireland, B. Smit and K. Stylianou, Degradation of plastic materials into terephthalic acid (tpa), ethylene glycol and/or other monomers that form the plastic materials, WO2020/173961A1, 2020.
- 848 F. G. Barla, T. Showalter, H. S. Su, J. Jones and I. Bobe, Methods for recycling cotton and polyester fibers from waste textiles, US10,501,599B2, 2020.
- 849 . Threading Together the Future of Circular Fashion. <https://circ.earth/> (accessed Feb 02, 2022).
- 850 Moving from Linear to Circular. <https://gr3n-recycling.com/technology.html> (accessed 01/08/22).



- 851 Making Cutting Edge Science an Everyday Reality. <https://www.loopindustries.com/en/about> (accessed 01/08/22).
- 852 J. Paben, Eastman offers details on \$250M depolymerization plant. <https://resource-recycling.com/plastics/2021/02/03/eastman-offers-details-on-250m-depolymerization-plant/> (accessed 01/08/22).
- 853 A. Naujokas and K. Ryan, Recovery process for ethylene glycol and dimethylterephthalate, US5,051,528A, 1991.
- 854 BRING Technology. <https://www.jeplan.co.jp/en/technology/> (accessed 01/08/22).
- 855 T. Hooghoudt, V. Pilippi and M. V. Artigas, Polymer Degradation, US2018/0037710A1, 2019.
- 856 Ioniqa takes first 10 kiloton PET upcycling factory into operation. <https://ioniqa.com/ioniqa-takes-first-10-kiloton-pet-upcycling-factory-into-operation/> (accessed 01/08/22).
- 857 R. D. Allen, K. M. Bajjuri, J. L. Hedrick, G. Breyta and C. E. Larson, Methods and materials for depolymerizing polyesters, US9,255,194B2, 2015.
- 858 Technip Energies, IBM and Under Armour form joint venture to advance the possibilities of plastics recycling technology. <https://www.technipenergies.com/media/news/technip-energies-ibm-under-armour-form-joint-venture-advance-possibilities-plastics-recycling> (accessed 01/08/22).
- 859 Enzymatic Recycling: Removing the Constraints of Current Processes. <https://www.carbios.com/en/enzymatic-recycling/> (accessed 01/08/22).
- 860 Our Partners. <https://www.carbios.com/en/partnering/> (accessed 01/08/22).
- 861 F. Akoueson, C. Chbib, S. Monchy, I. Paul-Pont, P. Doyen, A. Dehaut and G. Duflos, Identification and quantification of plastic additives using pyrolysis-GC/MS: A review, *Sci. Total Environ.*, 2021, 773, 145073.
- 862 Technip announces successful launch of Carbios industrial demonstration plant. <https://www.hydrocarbonprocessing.com/news/2021/11/technip-announces-successful-launch-of-carbios-industrial-demonstration-plant> (accessed 01/19/2022).
- 863 Y. Nakaji, M. Tamura, S. Miyaoka, S. Kumagai, M. Tanji, Y. Nakagawa, T. Yoshioka and K. Tomishige, Low-Temperature Catalytic Upgrading of Waste Polyolefinic Plastics into Liquid Fuels and Waxes, *Appl. Catal., B*, 2021, 285, 119805.
- 864 Y. Jing, Y. Wang, S. Furukawa, J. Xia, C. Sun, M. J. Hülsey, H. Wang, Y. Guo, X. Liu and N. Yan, Towards the Circular Economy: Converting Aromatic Plastic Waste Back to Arenes over a Ru/Nb2O5 Catalyst, *Angew. Chem.*, 2021, 133(10), 5587–5595.
- 865 J. E. Rorrer, G. T. Beckham and Y. Román-Leshkov, Conversion of Polyolefin Waste to Liquid Alkanes with Ru-Based Catalysts under Mild Conditions, *JACS Au*, 2020, 1(1), 8–12.
- 866 J. E. Rorrer, C. Troyano-Valls, G. T. Beckham and Y. Román-Leshkov, Hydrogenolysis of Polypropylene and Mixed Polyolefin Plastic Waste over Ru/C to Produce Liquid Alkanes, *ACS Sustainable Chem. Eng.*, 2021, 9(35), 11661–11666.
- 867 W.-T. Lee, F. D. Bobbink, A. P. van Muyden, K.-H. Lin, C. Corminboeuf, R. R. Zamani and P. J. Dyson, Catalytic Hydrocracking of Synthetic Polymers into Grid-Compatible Gas Streams, *Cell Rep. Phys. Sci.*, 2021, 2(2), 100332.
- 868 C. Wang, T. Xie, P. A. Kots, B. C. Vance, K. Yu, P. Kumar, J. Fu, S. Liu, G. Tsilomelekis and E. A. Stach, Polyethylene Hydrogenolysis at Mild Conditions over Ruthenium on Tungstated Zirconia, *JACS Au*, 2021, 1(9), 1422–1434.
- 869 P. A. Kots, S. Liu, B. C. Vance, C. Wang, J. D. Sheehan and D. G. Vlachos, Polypropylene Plastic Waste Conversion to Lubricants over Ru/TiO2 Catalysts, *ACS Catal.*, 2021, 11, 8104–8115.
- 870 C. Jia, S. Xie, W. Zhang, N. N. Intan, J. Sampath, J. Pfandtner and H. Lin, Deconstruction of high-density polyethylene into liquid hydrocarbon fuels and lubricants by hydrogenolysis over Ru catalyst, *Chem. Catal.*, 2021, 437–455.
- 871 S. Liu, P. A. Kots, B. C. Vance, A. Danielson and D. G. Vlachos, Plastic waste to fuels by hydrocracking at mild conditions, *Sci. Adv.*, 2021, 7(17), eabf8283.
- 872 G. Celik, R. M. Kennedy, R. A. Hackler, M. Ferrandon, A. Tennakoon, S. Patnaik, A. M. LaPointe, S. C. Ammal, A. Heyden and F. A. Perras, Upcycling Single-Use Polyethylene into High-Quality Liquid Products, *ACS Cent. Sci.*, 2019, 5(11), 1795–1803.
- 873 A. Tennakoon, X. Wu, A. L. Paterson, S. Patnaik, Y. Pei, A. M. LaPointe, S. C. Ammal, R. A. Hackler, A. Heyden and I. I. Slowing, Catalytic Upcycling of High-Density Polyethylene via a Processive Mechanism, *Nat. Catal.*, 2020, 3(11), 893–901.
- 874 S. D. Jaydev, A. J. Martin and J. Pérez-Ramírez, Direct Conversion of Polypropylene into Liquid Hydrocarbons on Carbon-Supported Platinum Catalysts, *ChemSusChem*, 2021, 5179–5185.
- 875 J. Kijeński and T. Kaczorek, Catalytic degradation of polystyrene-Rapid Communication, *Polimery*, 2005, 50(1), 60–63.
- 876 D. Munir, F. Piepenbreier and M. R. Usman, Hydrocracking of a plastic mixture over various micro-mesoporous composite zeolites, *Powder Technol.*, 2017, 316, 542–550.
- 877 D. Munir, M. F. Irfan and M. R. Usman, Hydrocracking of virgin and waste plastics: A detailed review, *Renewable Sustainable Energy Rev.*, 2018, 90, 490–515.
- 878 C. W. Yeung, J. Y. Teo, X. J. Loh and J. Y. Lim, Polyolefins and Polystyrene as Chemical Resources for a Sustainable Future: Challenges, Advances, and Prospects, *ACS Mater. Lett.*, 2021, 3, 1660–1676.
- 879 J. B. Williamson, S. E. Lewis, R. R. Johnson III, I. M. Manning and F. A. Leibfarth, C–H Functionalization of Commodity Polymers, *Angew. Chem., Int. Ed.*, 2019, 58(26), 8654–8668.
- 880 L. Chen, K. G. Malollari, A. Uliana, D. Sanchez, P. B. Messersmith and J. F. Hartwig, Selective, Catalytic Oxidations of C–H Bonds in Polyethylenes Produce



- Functional Materials with Enhanced Adhesion, *Chem*, 2021, 7(1), 137–145.
- 881 X. Jia, C. Qin, T. Friedberger, Z. Guan and Z. Huang, Efficient and Selective Degradation of Polyethylenes into Liquid Fuels and Waxes under Mild Conditions, *Sci. Adv.*, 2016, 2(6), e1501591.
- 882 F. Zhang, M. Zeng, R. D. Yappert, J. Sun, Y.-H. Lee, A. M. LaPointe, B. Peters, M. M. Abu-Omar and S. L. Scott, Polyethylene Upcycling to Long-Chain Alkylaromatics by Tandem Hydrogenolysis/Aromatization, *Science*, 2020, 370(6515), 437–441.
- 883 S. Tian, Y. Jiao, Z. Gao, Y. Xu, L. Fu, H. Fu, W. Zhou, C. Hu, G. Liu and M. Wang, Catalytic Amination of Polylactic Acid to Alanine, *J. Am. Chem. Soc.*, 2021, 16358–16363.
- 884 L. Chen, K. G. Malollari, A. Uliana and J. F. Hartwig, Ruthenium-Catalyzed, Chemoselective and Regioselective Oxidation of Polyisobutene, *J. Am. Chem. Soc.*, 2021, 143(12), 4531–4535.
- 885 U. Kanbur, G. Zang, A. L. Paterson, P. Chatterjee, R. A. Hackler, M. Delferro, I. I. Slowing, F. A. Perras, P. Sun and A. D. Sadow, Catalytic Carbon-Carbon Bond Cleavage and Carbon-Element Bond Formation Give New Life for Polyolefins as Biodegradable Surfactants, *Chem*, 2021, 7(5), 1347–1362.
- 886 J. De Andrés, A. Aguilar and J. Domenech, Kinetic Study of the Catalytic Effect of Zinc(II) Ion on the Dehydrogenation of Atactic Polypropylene by Sulfur, *J. Macromol. Sci., Chem.*, 1990, 27(2), 213–223.
- 887 A. Ray, K. Zhu, Y. V. Kissin, A. E. Cherian, G. W. Coates and A. S. Goldman, Dehydrogenation of Aliphatic Polyolefins Catalyzed by Pincer-Ligated Iridium Complexes, *Chem. Commun.*, 2005, (27), 3388–3390.
- 888 D. Brown and R. Lowry, Molecular Weight Standards from Sulfonation of Polystyrene, *J. Polym. Sci., Polym. Chem. Ed.*, 1979, 17(4), 1039–1046.
- 889 J. E. Coughlin, A. Reisch, M. Z. Markarian and J. B. Schlenoff, Sulfonation of Polystyrene: Toward the “Ideal” Polyelectrolyte, *J. Polym. Sci., Part A: Polym. Chem.*, 2013, 51(11), 2416–2424.
- 890 F. Kučera and J. Jančář, Preliminary Study of Sulfonation of Polystyrene by Homogeneous and Heterogeneous Reaction, *Chem. Pap.*, 1996, 50(4), 224–227.
- 891 F. Kučera and J. Jančář, Homogeneous and Heterogeneous Sulfonation of Polymers: a Review, *Polym. Eng. Sci.*, 1998, 38(5), 783–792.
- 892 D. Montarnal, M. Capelot, F. Tournilhac and L. Leibler, Silica-Like Malleable Materials from Permanent Organic Networks, *Science*, 2011, 334(6058), 965–968.
- 893 Y. Zhou, R. Groote, J. G. Goossens, R. P. Sijbesma and J. P. Heuts, Tuning PBT Vitriimer Properties by Controlling the Dynamics of the Adaptable Network, *Polym. Chem.*, 2019, 10(1), 136–144.
- 894 L. Yue, V. S. Bonab, D. Yuan, A. Patel, V. Karimkhani and I. Manas-Zloczower, Vitriimerization: A Novel Concept to Reprocess and Recycle Thermoset Waste via Dynamic Chemistry, *Global Challenges*, 2019, 3(7), 1800076.
- 895 W. Denissen, J. M. Winne and F. E. Du Prez, Vitrimers: Permanent Organic Networks with Glass-Like Fluidity, *Chem. Sci.*, 2016, 7(1), 30–38.
- 896 C. Hopmann, M. Adamy and A. Cohnen, Introduction to reactive extrusion, *Reactive Extrusion: Principles and Applications*, 2017, pp. 1–10.
- 897 D. Shi, J. Yang, Z. Yao, Y. Wang, H. Huang, W. Jing, J. Yin and G. Costa, Functionalization of isotactic polypropylene with maleic anhydride by reactive extrusion: mechanism of melt grafting, *Polymer*, 2001, 42(13), 5549–5557.
- 898 J. B. Williamson, C. G. Na, R. R. Johnson III, W. F. Daniel, E. J. Alexanian and F. A. Leibfarth, Chemo- and regio-selective functionalization of isotactic polypropylene: A mechanistic and structure–property study, *J. Am. Chem. Soc.*, 2019, 141(32), 12815–12823.
- 899 T. J. Fazekas, J. W. Alty, E. K. Neidhart, A. S. Miller, F. A. Leibfarth and E. J. Alexanian, Diversification of aliphatic C–H bonds in small molecules and polyolefins through radical chain transfer, *Science*, 2022, 375(6580), 545–550.
- 900 M. Butcher, Novolooop says it's worked out how to upcycle plastic waste, raises \$11M Series A. [https://techcrunch.com/2022/02/14/novolooop-says-its-worked-out-how-to-upcycle-plastic-waste-raises-11m-series-a/?guccounter=1&guce\\_referrer=aHR0cHM6Ly93d3cubm92b2xvb3AuY29tLw&guce\\_referrer\\_sig=AQAAAE528UVdX0V9achO5yivPIUNGIZR1f8PLRKsCcthW3CsLPIoejxo919ff-v3V1VOzHfddFhDZTejDx-7tT3B77CJjysbfjTz0R-hEz6Ri0wVOiLkEYHLfRKK4BX1cV-E8uQyaMk91b0EYbwOmzpH7GiDocq-P0j-NO3CZ49bX4xH](https://techcrunch.com/2022/02/14/novolooop-says-its-worked-out-how-to-upcycle-plastic-waste-raises-11m-series-a/?guccounter=1&guce_referrer=aHR0cHM6Ly93d3cubm92b2xvb3AuY29tLw&guce_referrer_sig=AQAAAE528UVdX0V9achO5yivPIUNGIZR1f8PLRKsCcthW3CsLPIoejxo919ff-v3V1VOzHfddFhDZTejDx-7tT3B77CJjysbfjTz0R-hEz6Ri0wVOiLkEYHLfRKK4BX1cV-E8uQyaMk91b0EYbwOmzpH7GiDocq-P0j-NO3CZ49bX4xH).
- 901 Novolooop upcycling. <https://www.novolooop.com/technology> (accessed 2/22/2022).
- 902 J. Y. Yao, Y. W. Wang, T. Muppaneni, R. Shrestha, J. L. Roy and G. D. Figuly, Methods for the decomposition of contaminated plastic, *Waste*, 2020, 1–57.
- 903 C. Aumnate, N. Rudolph and M. Sarmadi, Recycling of polypropylene/polyethylene blends: Effect of chain structure on the crystallization behaviors, *Polymers*, 2019, 11(9), 1456.
- 904 V. Wigotsky, Alloys and blends home in on demanding design specs, *Plast. Eng.*, 1988, 44(11), 25–32.
- 905 L. Wei, A. McDonald, C. Freitag and J. Morrell, Effects of wood fiber esterification on properties, weatherability and biodegradability of wood plastic composites, *Polym. Degrad. Stab.*, 2013, 98, 1348–1361.
- 906 L. Wei, A. McDonald and N. Stark, Grafting of Bacterial Polyhydroxybutyrate (PHB) onto Cellulose via In Situ Reactive Extrusion with Dicumyl Peroxide, *Biomacromolecules*, 2015, 16, 1040–1049.
- 907 L. Wei and A. McDonald, Peroxide induced cross-linking by reactive melt processing of two biopolyesters: Poly(3-hydroxybutyrate) and poly(lactic acid) to improve their melting processability, *J. Appl. Polym. Sci.*, 2015, 132, 41724.



- 908 L. Wei, N. Stark and A. McDonald, Interfacial improvements in biocomposites based on poly(3-hydroxybutyrate) and poly(3-hydroxybutyrate-co-3-hydroxyvalerate) bioplastics reinforced and grafted with  $\alpha$ -cellulose fiber, *Green Chem.*, 2015, **17**, 4800–4814.
- 909 S. Stanic, T. Koch, K. Schmid, S. Knaus and V.-M. Archodoulaki, Upcycling of polypropylene with various concentrations of peroxydicarbonate and dilauroyl peroxide and two processing steps, *J. Appl. Polym. Sci.*, 2021, e50659.
- 910 H. Khonakdar, J. Morshedien, U. Wagenknecht and S. Jafari, An investigation of chemical crosslinking effect on properties of high-density polyethylene, *Polymer*, 2003, **44**, 4301–4309.
- 911 R. Rasal, A. Janorkar and D. Hirt, Poly(lactic acid) modifications, *Prog. Polym. Sci.*, 2010, **35**, 338–356.
- 912 H. Zhou, Z. Wang, G. Xu, X. Wang, B. Wen and S. Jin, Preparation of Crosslinked High density Polyethylene Foam Using Supercritical CO<sub>2</sub> as Blowing Agent, *Cell. Polym.*, 2017, **36**(4), 167–182.
- 913 M. Takamura, T. Nakamura, S. Kawaguchi, T. Takahashi and K. Koyama, Molecular characterization and crystallization behavior of peroxide-induced slightly crosslinked poly(L-lactide) during extrusion, *Polym. J.*, 2010, **42**, 600–608.
- 914 N. Gaylord, Compatibilizing agents: Structure and function in polyblends, *J. Macromol. Sci., Chem.*, 1989, **26**, 1211–1229.
- 915 S. C. Manning and R. B. Moore, Carboxylation of polypropylene by reactive extrusion with functionalized peroxides for use as a compatibilizer in polypropylene/polyamide-6, 6 blends, *J. Vinyl Addit. Technol.*, 1997, **3**(2), 184–189.
- 916 T. Sakai, Report on the state of the art: Reactive processing using twin-screw extruders, *Adv. Polym. Technol.*, 1991, **11**, 99–108.
- 917 R. Asay, M. Hein and D. Wharry, Blends and alloys of vinyl—technology and applications, *J. Vinyl Addit. Technol.*, 1993, **15**, 76–81.
- 918 M. Hein, Elastomeric alloys of PVC, *J. Vinyl Addit. Technol.*, 1994, **16**, 208–212.
- 919 Y. Kimura, Co-rotating Twin Screw Extruder Compounding Technologies, *Plast. Eng.*, 2014, **70**, 32–36.
- 920 A. Amor, N. Okhay, A. Guinault, G. Miquelard-Garnier, C. Sollogoub and M. Gervais, Combined compatibilization and plasticization effect of low molecular weight poly (Lactic acid) in poly(lactic acid)/poly(3-hydroxybutyrate-co-3-hydroxyvalerate) blends, *EXPRESS Polym. Lett.*, 2018, **12**, 114–125.
- 921 S. Sapieha, P. Allard and Y. Zang, Dicumyl peroxide-modified cellulose/LLDPE composites, *J. Appl. Polym. Sci.*, 1990, **41**, 2019–2048.
- 922 S. Horikoshi and N. Serpone, Role of Microwaves in Heterogeneous Catalytic Systems, *Catal. Sci. Technol.*, 2014, **4**(5), 1197–1210.
- 923 X. Jie, W. Li, D. Slocombe, Y. Gao, I. Banerjee, S. Gonzalez-Cortes, B. Yao, H. AlMegren, S. Alshihri and J. Dilworth, Microwave-Initiated Catalytic Deconstruction of Plastic Waste into Hydrogen and High-Value Carbons, *Nat. Catal.*, 2020, **3**(11), 902–912.
- 924 C. Ludlow-Palafox and H. A. Chase, Microwave-Induced Pyrolysis of Plastic Wastes, *Ind. Eng. Chem. Res.*, 2001, **40**(22), 4749–4756.
- 925 V. Palma, D. Barba, M. Cortese, M. Martino, S. Renda and E. Meloni, Microwaves and Heterogeneous Catalysis: A Review on Selected Catalytic Processes, *Catalysts*, 2020, **10**(2), 246.
- 926 K. Ding, S. Liu, Y. Huang, S. Liu, N. Zhou, P. Peng, Y. Wang, P. Chen and R. Ruan, Catalytic Microwave-Assisted Pyrolysis of Plastic Waste over NiO and HY for Gasoline-Range Hydrocarbons Production, *Energy Convers. Manage.*, 2019, **196**, 1316–1325.
- 927 E. Bäckström, K. Odelius and M. Hakkarainen, Trash to Treasure: Microwave-Assisted Conversion of Polyethylene to Functional Chemicals, *Ind. Eng. Chem. Res.*, 2017, **56**(50), 14814–14821.
- 928 E. Bäckström, K. Odelius and M. Hakkarainen, Designed from Recycled: Turning Polyethylene Waste to Covalently Attached Polylactide Plasticizers, *ACS Sustainable Chem. Eng.*, 2019, **7**(12), 11004–11013.
- 929 N. Zhou, L. Dai, Y. Lyu, H. Li, W. Deng, F. Guo, P. Chen, H. Lei and R. Ruan, Catalytic Pyrolysis of Plastic Wastes in a Continuous Microwave Assisted Pyrolysis System for Fuel Production, *Chem. Eng. J.*, 2021, **418**, 129412.
- 930 Q. Bu, Y. Liu, J. Liang, H. M. Morgan Jr., L. Yan, F. Xu and H. Mao, Microwave-Assisted Co-Pyrolysis of Microwave Torrefied Biomass with Waste Plastics using ZSM-5 as a Catalyst for High Quality Bio-Oil, *J. Anal. Appl. Pyrolysis*, 2018, **134**, 536–543.
- 931 L. Fan, P. Chen, Y. Zhang, S. Liu, Y. Liu, Y. Wang, L. Dai and R. Ruan, Fast Microwave-Assisted Catalytic Co-Pyrolysis of Lignin and Low-Density Polyethylene with HZSM-5 and MgO for Improved Bio-Oil Yield and Quality, *Bioresour. Technol.*, 2017, **225**, 199–205.
- 932 N. Mohanan, Z. Montazer, P. K. Sharma and D. B. Levin, Microbial and enzymatic degradation of synthetic plastics, *Front. Microbiol.*, 2020, **11**, 2837.
- 933 M. Suzuki, Y. Tachibana and K.-i. Kasuya, Biodegradability of poly (3-hydroxyalkanoate) and poly ( $\epsilon$ -caprolactone) via biological carbon cycles in marine environments, *Polym. J.*, 2021, **53**(1), 47–66.
- 934 B. R. Kang, S. B. Kim, H. A. Song and T. K. Lee, Accelerating the biodegradation of high-density polyethylene (HDPE) using *Bjerkandera adusta* TBB-03 and lignocellulose substrates, *Microorganisms*, 2019, **7**(9), 304.
- 935 S. Skariyachan, A. A. Patil, A. Shankar, M. Manjunath, N. Bachappanavar and S. Kiran, Enhanced polymer degradation of polyethylene and polypropylene by novel thermophilic consortia of *Brevibacillus* sps. and *Aneurinibacillus* sp. screened from waste management



- landfills and sewage treatment plants, *Polym. Degrad. Stab.*, 2018, **149**, 52–68.
- 936 N. Khatoon, A. Jamal and M. I. Ali, Lignin peroxidase isoenzyme: a novel approach to biodegrade the toxic synthetic polymer waste, *Environ. Technol.*, 2019, **40**(11), 1366–1375.
- 937 T. Sumathi, B. Viswanath, A. Sri Lakshmi and D. SaiGopal, Production of laccase by *Cochliobolus* sp. isolated from plastic dumped soils and their ability to degrade low molecular weight PVC, *Biochem. Res. Int.*, 2016, 2016.
- 938 ASTRX *ASTRX Review of Material Flow at MRFs and Reprocessors; Sustainable Packaging Coalition and The Recycling Partnership*, 2018.
- 939 Staub, C. MRF operator: Lithium-ion batteries are ‘ticking time bombs’. <https://resource-recycling.com/recycling/2021/04/13/mrf-operator-lithium-ion-batteries-are-ticking-time-bombs/> (accessed 15 Nov 2021).
- 940 U.S.EPA, *An Analysis of Lithium-ion Battery Fires in Waste Management and Recycling*; United States Environmental Protection Agency, 2021.
- 941 CEDOC. *Proyecto diagnóstico participativo situacional y propuesta de programa de intervención con Mujeres Pепенadoras de la Unidad Habitacional Manuel M. López, Tláhuac* 2014.
- 942 N. C. Maragou, A. Makri, E. N. Lampi, N. S. Thomaidis and M. A. Koupparis, Migration of bisphenol A from polycarbonate baby bottles under real use conditions, *Food Addit. Contam., Part A*, 2008, **25**(3), 373–383.
- 943 D. Chiche and J.-M. Schweitzer, Investigation of competitive COS and HCN hydrolysis reactions upon an industrial catalyst: Langmuir-Hinshelwood kinetics modeling, *Appl. Catal., B*, 2017, **205**, 189–200.
- 944 J. Aguado, D. P. Serrano and J. M. Escola, Fuels from Waste Plastics by Thermal and Catalytic Processes: A Review, *Ind. Eng. Chem. Res.*, 2008, **47**(21), 7982–7992.
- 945 E. Asmelash, G. Prakash, R. Gorini and D. Gielen, Role of IRENA for global transition to 100% renewable energy, in *Accelerating the transition to a 100% renewable energy era*, Springer, 2020; pp. 51–71.
- 946 L., F. Price of ethylene worldwide from 2017 to 2021. <https://www.statista.com/statistics/1170573/price-ethylene-forecast-globally/#:~:text=The%20average%20price%20of%20ethylene,comparison%20with%20the%20previous%20year.> (accessed Feb 02).
- 947 C. Mukherjee, J. Denney, E. Mbonimpa, J. Slagley and R. Bhowmik, A review on municipal solid waste-to-energy trends in the USA, *Renewable Sustainable Energy Rev.*, 2020, **119**, 109512.
- 948 S. Das, C. Liang and J. B. Dunn, Life Cycle Assessment of Polymers and Their Recycling, in *Circular Economy of Polymers: Topics in Recycling Technologies*, ACS Publications, 2021, pp. 143–170.
- 949 P. G. Jessop, Searching for green solvents, *Green Chem.*, 2011, **13**(6), 1391–1398.
- 950 J. García-Turiel and B. Jérôme, Solvent retention in thin polymer films studied by gas chromatography, *Colloid Polym. Sci.*, 2007, **285**(14), 1617–1623.
- 951 I. Vollmer, M. J. Jenks, M. C. Roelands, R. J. White, T. van Harmelen, P. de Wild, G. P. van Der Laan, F. Meirer, J. T. Keurentjes and B. M. Weckhuysen, Beyond mechanical recycling: Giving new life to plastic waste, *Angew. Chem., Int. Ed.*, 2020, **59**(36), 15402–15423.

