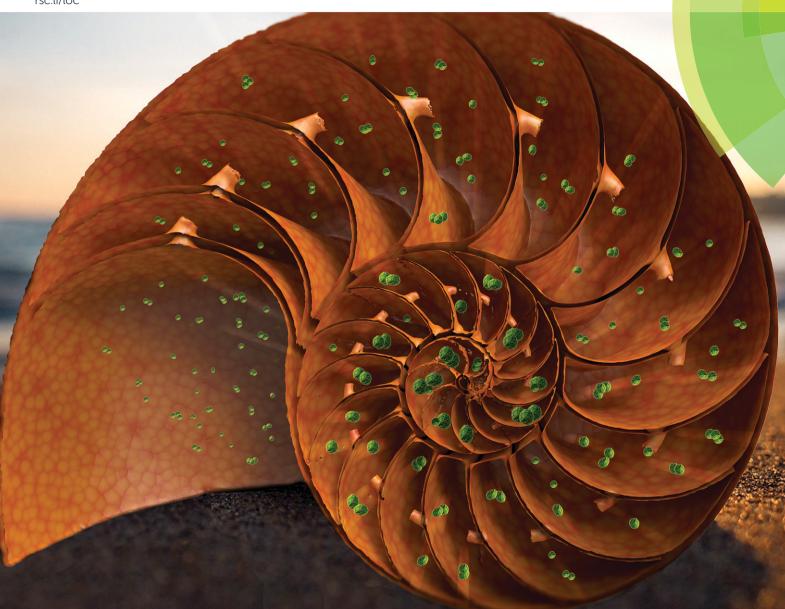
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# Flocculation on a chip: a novel screening approach to determine floc growth rates and select flocculating agents†

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Flocculation is a key purification step in cell-based processes for the food and pharmaceutical industry where the removal of cells and cellular debris is aided by adding flocculating agents. However, finding the best suited flocculating agent and optimal conditions to achieve rapid and effective flocculation is a nontrivial task. In conventional analytical systems, turbulent mixing creates a dynamic equilibrium between floc growth and breakage, constraining the determination of floc formation rates. Furthermore, these systems typically rely on end-point measurements only. We have successfully developed for the first time a microfluidic system for the study of flocculation under well controlled conditions. In our microfluidic device (μFLOC), floc sizes and growth rates were monitored in real time using high-speed imaging and computational image analysis. The on-line and in situ detection allowed quantification of floc sizes and their growth kinetics. This eliminated the issues of sample handling, sample dispersion, and end-point measurements. We demonstrated the power of this approach by quantifying the growth rates of floc formation under forty different growth conditions by varying industrially relevant flocculating agents (pDADMAC, PEI, PEG), their concentration and dosage. Growth rates between 12.2 µm s<sup>-1</sup> for a strongly cationic flocculant (pDADMAC) and 0.6 µm s<sup>-1</sup> for a non-ionic flocculant (PEG) were observed, demonstrating the potential to rank flocculating conditions in a quantitative way. We have therefore created a screening tool to efficiently compare flocculating agents and rapidly find the best flocculating condition, which will significantly accelerate early bioprocess development.

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#### 1. Introduction

The pressure to decrease operation costs and to increase the efficiency of existing industrial bioprocesses has led to a renewed interest in flocculation. 1,2 During flocculation, colloidal particles are selectively aggregated with the aid of a flocculating agent and then subsequently settle under the influence of gravity.3,4 In industrial bioprocesses, this selective removal of key impurities is applied to remove cells and cellular debris from the fermentation medium during primary recovery, i.e. before further purification steps yield the desired product. Intensified fermentation processes have led to higher cell densities, and have thus increased the load on the downstream purification steps, putting higher demands on flocculation as the solid-liquid clarification step. An increased puri-

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fication performance in a primary recovery step such as flocculation improves the efficacy of all subsequent downstream unit operation steps which in turn lowers the overall operational costs of bioprocesses.<sup>5-10</sup>

Flocculation is a highly dynamic process which is typically initiated with the addition of a flocculating agent, the flocculant, to a suspension. The majority of flocculation processes use a polymeric flocculant, such as polyethylenimine, polyethylene glycol, or chitosan. The flocculant then adsorbs onto the colloidal particles, i.e. in the case of an industrial bioprocess onto the cells and the cellular debris. Once adsorbed, the polymer re-conforms to attain an energy-minimised state with the colloid. As these new individual entities collide with each other, they form larger aggregates called flocs, for example due to charge or bridging effects. Flocs that settle faster facilitate the removal in settlement tanks. It is therefore critical to understand floc growth and the physical characteristics of flocs to enhance removal efficiency. However, these depend on a number of process parameters. The growth rate of the flocs is known to depend strongly on the dosage of the flocculants, 2,11,12 on their physical properties, such as charge densities and molecular weight, but also on the properties of

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the solution they are in, for example its pH and ionic strength.<sup>11</sup> Additionally, hydrodynamic shear stress plays an important role in flocculation. Shear stress can affect adsorption and collision rates but can also lead to floc breakage. 1,3,11,13 Under turbulent mixing, floc growth and floc breakage are typically in a dynamic equilibrium, and their individual rates are thus difficult to discern.

A variety of analytical methods to size and count flocs have been established. Light microscopy alone, 14,15 or enhanced with image processing methods to avoid microscopist bias, 16,17 is per se a non-destructive measurement method, vet suffers from the distortion that occurs in the sample preparation stage; flocs must be removed ex situ from the suspension, and thus they aggregate, settle or break before they can actually be sized and counted. This limitation also applies for all electron microscopy methods. 18,19 Similarly, methods involving light transmission or scattering offer quick and non-invasive detection of a broad band of floc sizes, but do not allow in situ characterisation and quantification of floc morphology. To monitor flocs in situ, digital image analyses with CCD cameras have been applied, but there are limitations which relate to the magnifications available from the CCD camera lens. Individual particle sensors based either on optical or electrical detection, e.g. the coulter principle,<sup>2</sup> are reliable, but the size of the aperture narrows the sizes of flocs that can be detected, and can induce floc breakage itself. Additionally, for electrical detection, flocs must be suspended in an electrolyte solution which itself can impact on the shape and the porosity of the flocs. Light scattering methods apply Lorenz-Mie and Fraunhofer diffraction theory particle size distributions from determine signals. 11,14,20-22 As they can be implemented recirculation systems, where a pump flows the flocs from the flocculation vessel to the analytical part and back, they offer continuous monitoring which provides statistical rigor. However, sample dispersion and pumping can affect the floc size, thus these methods are not strictly in situ either. Finally, focused-beam reflectance measurement (FBRM) methods<sup>23</sup> are probes that can be directly immersed in a stirred suspended fluid, and thus offer true in situ detection, but require a high particle velocity to produce an optimal detection result. However, in stirred vessels, shear rates vary significantly with location, and it is thus not possible to study flocgrowth mechanisms under controlled conditions. To further our understanding of floc-growth mechanisms, there is thus clearly a need for a flocculator capable of operating at steadystate and with a fine control over the flocculation microenvironment, whilst offering both in situ and on-line detection of floc-growth.

In this contribution, we present for the first time a microfluidic approach to analyse flocculation. We hypothesised that the laminar flow conditions afforded by microfluidic devices and their ease of coupling with light microscopy would allow investigation of floc formation and floc growth independent from floc breakage and floc ageing phases. Saccharomyces cerevisiae was selected as a model system due to its widespread use in the biotechnology industry, particularly for the study of flocculation, and several commercially available flocculants were evaluated. To study flocculation growth kinetics in situ and in real-time, the microfluidic device was combined with high-speed imaging and flocculation kinetics were studied for forty different conditions. The growth analysis of individual flocs obtained by this new screening tool, as opposed to the population analysis approach typical of conventional systems, will allow rapid selection of flocculating agents and conditions for early process development, which is relevant for both microbial fermentation<sup>21</sup> and mammalian cell processes.24-26

# 2. Experimental

#### 2.1. Device fabrication

The microfluidic flocculation device (µFLOC) was designed using SolidWorks® (Dassault Systèmes SolidWorks Corporation, USA) and fabricated out of 1.5 mm thick poly(methyl methacrylate) sheet (PMMA, 824-480, RS Components Ltd., UK) using a micro milling machine (Folken IND, USA). The PMMA layers were thermo-compression bonded at 105 °C for 1 hour. Bonding strength was tested as described in O'Sullivan et al., 2012.27

#### 2.2. Mixing characterisation

Mixing was characterized by analysing a sequence of images taken of a coloured dye when mixing with water. This was performed by injecting a solution of 4 mM Allura Red (Sigma Aldrich, UK) and Milli-Q® water (Millipore Ltd, UK) into the focusing stream and sheath stream inlets, respectively, and vice versa. The µFLOC was placed on a motorised stage of an inverted microscope (Nikon Ti-E, Nikon UK Ltd., UK) equipped with a colour CCD camera (DS Fi-1, Nikon UK Ltd., UK).

Bright field images were captured at 30 W illumination  $(2560 \times 1920 \text{ pixels})$  at different locations of the  $\mu$ FLOC and at 10× magnification. A computational script was developed in Python for image analysis, calculating the mixing time based on absorbance values<sup>28</sup> (ESI† A). Experiments were performed in triplicates.

#### 2.3. Flocculation of Saccharomyces cerevisiae

2.3.1. Materials used for flocculation. Saccharomyces cerevisiae was supplied by DCL CraftBake yeast (JW Pike, London, UK). S. cerevisiae was suspended in 100 mM di-sodium/ potassium phosphate buffer to a final yeast concentration of 250 mg mL<sup>-1</sup> (packed weight). The yeast suspension was homogenised using a Manton-Gaulin homogeniser (Lab 60, APV-SPX Ltd., UK) at 500 bar, 5 passes, 4 °C.11 The resulting homogenate was used for the flocculation experiments, and the pH adjusted to the required value using either 2 M HCl or 2 M NaOH.

2.3.2. Flocculation of yeast homogenate. Flocculation was performed by the addition of different flocculants (Table 1)

Table 1 List of flocculants employed to flocculate Saccharomyces cerevisiae homogenates with their respective molecular weight, size and cationic charge densities (CD). CD provides indication whether a polyelectrolyte flocculant is strongly or weakly ionic, which affects the flocculation process.<sup>29</sup> Flocculant concentrations were varied between 5 and 25  $g_{flocculant}$   $kg^{-1}_{packed\ yeast}$  (0.125 to 0.625% w/v, respectively) at pH 7.4, and the pH varied between 5 and 7.5 at a concentration of 20 g<sub>flocculant</sub> kg<sup>-1</sup><sub>packed yeast</sub>

Flocculant	Molecular weight (kDa)	Size <sup>a</sup> (nm)	Cationic charge densities (mol%)	Cationic charge densities (mEq g <sup>-1</sup> )	Supplier
PEI (99% w/v)	10	6	20-45 (ref. 30)	20 (ref. 31)	Alfa Aesar, USA
PEI (30% w/v)	70	15.9			
PEI (30% w/v)	50-100	13.4-19			
PEG (100% w/v)	6	4.6	_	_	VWR Chemicals, UK
PEG (100% w/v)	100	19			Alfa Aesar, USA
pDADMAC (35% w/v)	<100	<19	100 (ref. 29)	6.2 (ref. 29)	Sigma-Aldrich, UK
pDADMAC (20% w/v)	200-350	26.8-35.5			
pDADMAC (20% w/v)	400-500	37.9-42.4			

<sup>&</sup>lt;sup>a</sup> Size measured assuming zero charge density.<sup>29</sup> Note: PEI - polyethylenimine; PEG - polyethylene glycol; pDADMAC poly(diallyldimethylammonium chloride). For all flocculants, the concentrations listed represent the concentration of the stock solution.

at concentrations between 5 and 25 g<sub>flocculant</sub> kg<sup>-1</sup><sub>packed yeast</sub> (0.125 to 0.625\% w/v, respectively) at pH 7.4. Experiments were also performed between pH 5 and 7.5 at a fixed concentration of 20 g<sub>flocculant</sub> kg<sup>-1</sup><sub>packed yeast</sub>. To validate the μFLOC, flocculation experiments were performed (i) at a fixed pH 7.4, varying the concentration of PEI (50-100 kDa) in solution between 5 and 25g<sub>PEI</sub> kg<sup>-1</sup><sub>packed yeast</sub>, and (ii) at a fixed concentration of PEI (50-100 kDa) of 20 g<sub>PEI</sub> kg<sup>-1</sup><sub>packed yeast</sub>, varying the pH between 5 and 7.5.

2.3.3. Flocculation of yeast homogenate in the µFLOC. Flocculant and yeast homogenate solutions were contained in 10 mL sterile Plastipak syringes with Luer-locks (BD, UK). Both solutions were pumped into the µFLOC using syringe pumps (KDS200, KD Scientific Inc., Massachusetts, USA; and Aladdin, WPI Ltd., Hertfordshire, UK). The syringes were connected to the µFLOC by a 20 cm polytetrafluoroethylene (PTFE) tubing (S1810-10, OD 1/16 inch, Bola, Germany) and with M6 interconnects (P207X, Upchurch Scientific, USA). The flocculant was added to the side inlet (sheath flow) while the yeast homogenate was added to the centre inlet (focussed flow). Flow rates of 75 μL min<sup>-1</sup> and 85 μL min<sup>-1</sup> were used for the focussed and the sheath flow inlets, respectively. Samples were collected and analysed by laser diffraction (section 2.4.1.) and in situ image analysis (section 2.4.2.).

2.3.4. Bench-scale yeast homogenate flocculation. Flocculation studies were performed under similar conditions as in section 2.3.3. Briefly, 20 mL of yeast homogenate and PEI solutions (each) were added to a 50 mL centrifuge tube (BD, UK). Tubes were mixed by gentle tube inversion<sup>11</sup> for approximately half a minute (around 30 times, minimum shear rate = 35 s<sup>-1</sup> assuming laminar flow). Samples were collected and analysed by laser diffraction (section 2.4.1.), within approximately one minute after flocculant addition.

#### 2.4. Analytical methods

2.4.1. Laser diffraction particle sizing. A Mastersizer 2000 (Malvern Instruments Ltd., UK) was used to analyse the floc diameter. Samples were dispersed in Milli-Q® water (Millipore Ltd, UK). The Mastersizer has an external dispersion unit (Hydro SM-A, Malvern Instruments Ltd., UK) which cycles the samples to be analysed through the instrument.

The uFLOC was connected to the dispersion unit with a 10 cm long PTFE tube (ID = 0.8 mm, S1810-10, Bola, Germany). Samples from the bench-scale studies (section 2.3.4.) were added manually directly into the dispersion unit with the aid of a Pasteur pipette.

Experiments were repeated at least 5 times with each sample being measured three times by the instrument. Floc diameters were calculated using the Fraunhofer model, and reported as calculated averages (volume basis) from the three measurements. Particle size distribution (PSD) is given in % volume. Refractive indices (RI) of 1.59 and 1.33 were used, corresponding to S. cerevisiae homogenate (as for latex particles<sup>21</sup>) and Milli-Q® water,<sup>32</sup> respectively.

**2.4.2. Floc surface-charge analysis.** The zeta potential  $(\zeta)$  of the flocs were measured by electrophoretic light scattering (Zetasizer Nano ZS, Malvern Instruments Ltd., UK) using a transparent and disposable zeta cell (DTS 1070, Malvern Instruments Ltd., UK).

The µFLOC was connected to the disposable zeta cell by PTFE tubing (ID = 0.8 mm, S1810-10, Bola, Germany). Fluid flow was stopped prior to the measurements. Samples from the bench-scale studies were manually added into the zeta cell using a Pasteur pipette as in section 2.4.1. Measurements were performed in triplicates, and electrophoretic mobility readings of the instrument indicated that no sedimentation was occurring. Calculations were automatically made using the Zetasizer software 6.20 (Malvern Instruments Ltd., UK).

2.4.3. High-speed particle imaging and image analysis. For automated floc size measurements, the µFLOC was placed on a motorised stage of an inverted microscope (Eclipse Ti-E, Nikon UK Ltd., UK) equipped with a high-speed camera (MC-1, Photron USA Inc., California, USA). Images were captured (512 × 512 pixels) at 2000 frames per second (fps) at different locations of the device with an exposure time of 16.67 µs, at 10× magnification. Imaging was performed for 4 seconds, generating ~8000 images per location.

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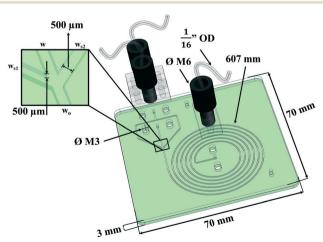
A computational script was developed for image analysis calculating the area occupied by the flocs (ESI† B). Briefly, the floc-area measured in pixels2 was converted to µm2 and used to determine the equivalent circular diameter. To create PSDs in terms of % volume (to be comparable with the lightscattering instrument), a histogram of the number of flocs was generated. The histogram containing hundred equalsized bins between 0 µm and the largest particle-size was transformed to a % number. The % number was converted into % volume by multiplying this value by the volume of a sphere at the corresponding particle size (histogram bin size) and the resulting PSDs were plotted using OriginPro 8.6 software (OriginLab Corporation, Massachusetts, USA).

2.4.4. Statistical analysis. Statistical analysis was performed using one-way ANOVA. Statistical differences between groups from the same experimental set were determined using Turkey post-hoc test. A p-value  $\leq 0.05$  was considered significant. All analyses were completed using SPSS Statistics software (IBM Corp, Armonk, NY, USA). All results were expressed as the mean and plus or minus one standard deviation.

# 3. Results

#### 3.1. Microfluidic device design

The microfluidic device (µFLOC) was comprised of a ψ-shaped hydrodynamic focussing inlet evolving into a 607 mm long inwards spiralling channel with the width (w) and depth (d) of the channels being 0.5 mm (Fig. 1). The micromachined poly(methyl methacrylate) (PMMA) substrate was sealed with a second PMMA layer with through holes for the inlet and outlet, using thermo-compression bonding. The bond strength was tested to resist up to 1.5 bar, while the theoretical pressure drop within the channels was only around 9.4 mbar. At the flow rates used for flocculation ex-



1 Microfluidic flocculation device (µFLOC). representation of the 607 mm long  $\mu$ FLOC comprising of a  $\psi$ -shaped hydrodynamic focussing inlet. The channels have an aspect ratio of 1. The width of the channel after the inlet  $(w_0)$  is 500  $\mu$ m.

periments, the calculated mixing time  $(t_{mix})$  and mixing length  $(z_{mix})$  were 7.5 s and 80.3 mm, respectively.

#### 3.2. Zeta potential analysis

The zeta potential  $(\zeta)$  analysis of the flocs showed strong similarity between the µFLOC and the bench-scale measurements under varying pH and polyethylenimine (PEI) concentrations (Fig. 2). A decrease in the  $\zeta$  potential values was observed with increasing pH at both scales for a flocculant concentration of 20  $g_{PEI}$  kg<sup>-1</sup><sub>packed yeast</sub>. From pH 5 to 7.5, the  $\zeta$ potentials decreased from 20.6 mV to -1.02 mV, and from 16.4 mV to -0.67 mV, in the bench-scale and in the μFLOC, respectively. Over this pH range, there is no parity between the scales, but a good linear correlation ( $R^2 = 0.96$ ). The point of zero mobility falls between pH 7.0 and pH 7.5 (Fig. 2A). At pH 7.4, for varying concentrations of PEI (5-20 g<sub>PEI</sub>  $kg^{-1}_{packed veast}$ ), there is a better linear correlation ( $R^2 = 0.99$ ) between the two  $\zeta$  potentials (Fig. 2B), and the point of zero mobility lies between 15 g<sub>PEI</sub> kg<sup>-1</sup><sub>packed yeast</sub> and 20 g<sub>PEI</sub>  $kg^{-1}_{packed\ veast}$ . With increasing concentrations of PEI, the  $\zeta$ potentials increased from -11.4 mV to 1.38 and from -15.7 mV to 1.79 mV in the bench-scale and the μFLOC, respectively. Similar results and correlations of  $\zeta$  potential values can be found in previously published work.<sup>11</sup>

#### 3.3. Off-line floc size characterisation

Off-line floc size measurements were performed using a laser-scattering instrument (Mastersizer) and compared with bench-scale results (Fig. 3). Two parameters were tested, pH and PEI concentrations (Fig. 3A and B), and their influence was similar in both systems ( $p \le 0.05$ ). The floc size increased in both systems with increasing pH (from 5 to 7.5) observing a similar trend in the d(0.5) (size of a floc which is the 50th percentile of the volume distribution or mass median diameter) and d(0.9) (the size which is the 90th percentile of the volume distribution). However, floc sizes were consistently larger in the µFLOC device, reaching a maximum of 51.6  $\pm$  1.7  $\mu$ m at pH 7.5, in comparison with 29.4  $\pm$  1.7  $\mu$ m at the bench-scale (Fig. 3A).

Under varying PEI concentrations (Fig. 3B), a maximum floc size was obtained at 20  $g_{PEI}$   $kg^{-1}_{packed\ yeast}$ , and pH 7.4, reaching a size of 55.3  $\pm$  6.7  $\mu m$  and 23.7  $\pm$  1.1  $\mu m$ , in the μFLOC and bench-scale, respectively.

The particle size distribution (PSD) of both systems was significantly distinct (Fig. 3C). Two different populations can be observed for the bench-scale experiments, one with an average floc size of  $\sim 3 \mu m$  and another with an average size of approximately 25 µm. With increasing concentrations of PEI, a shift of the smaller population occurred towards the larger particle size until only one population of flocs was observed (ESI† C). In the µFLOC a single PSD population with a broad size distribution was observed. The PSD did not change significantly with increasing concentrations of PEI (ESI† C).

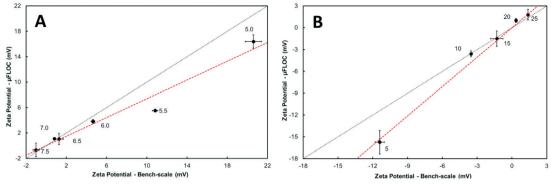


Fig. 2 Zeta potential of Saccharomyces cerevisiae in the microfluidic flocculation device (μFLOC) and bench-scale measurements. (A) - Parity analysis between the μFLOC and bench-scale measurements at different values of pH (5-7.5, data labels). The concentration of flocculant, PEI (MW 50-100 kDa), was 20 g kg<sup>-1</sup>packed yeast. (B) Parity analysis between the μFLOC and bench-scale measurements at pH 7.4 with different concentrations of the flocculant, PEI (MW 50-100 kDa), in the range of 5-20 g  ${\rm kg}^{-1}_{\rm packed\ yeast}$  (data labels). The dashed lines (red) denote the linear trend line between the two scales. Experiments were performed in triplicates, error bars represent plus or minus one standard deviation.

#### 3.4. Real-time observation of flocs in the µFLOC

The floc characterisation presented in the previous sections was performed with flocs obtained at the outlet of the µFLOC device, i.e. they were likely influenced by sample handling and preparation for the detection with the Mastersizer. To enable in situ floc size measurements and to calculate the growth kinetics of flocs formed in the µFLOC, flocs were imaged *via* a high-speed camera, at different locations  $(x_1, \dots x_7)$ , i.e. for different mean residence times (Fig. 4A). Floc sizes increased steadily along the microfluidic channel, as seen for example in Fig. 4B for 20 g<sub>PEI</sub> kg<sup>-1</sup><sub>packed yeast</sub> at pH 7. We then employed the µFLOC and image analysis to measure floc sizes and to quantify floc growth rates for different concentrations of PEI at pH 7.4. The floc sizes ranged from approximately 50  $\mu$ m (at position  $x_1$ ) to a maximum of approximately 250 μm (Fig. 5). Up to a size of 250 μm, which corresponds to half the channel width, the flocs increased linearly with distance in the channel (with coefficients of determination,  $R^2$ , approaching 1). Beyond this size, the growth plateaued (Fig. 5B). With increased loading of PEI, the growth rate increased from 3.1 to 8.8 µm s<sup>-1</sup> for PEI concentrations of 5 to 25 g<sub>PEI</sub> kg<sup>-1</sup><sub>packed yeast</sub>. A linear regression thus represents a convenient way to analyse the impact of the flocculating agent on floc growth.

#### 3.5. Floc growth kinetics with different flocculants

To further evaluate the utility of µFLOC, we studied the impact of different flocculating agents on floc-growth in the device. For this set of experiments, we exposed the yeast homogenate to the cationic flocculants poly-(diallyldimethylammonium chloride) (pDADMAC) and PEI, and to the non-ionic flocculant polyethylene glycol (PEG). Different molecular weights and different concentrations were applied for each of the three flocculants. The results of the 40 different conditions and the corresponding measured growth rates are summarised in Table 2. The choice of flocculating agent, molecular weight and concentration all had their influence on growth rates. Higher rates were obtained at high flocculant concentrations and higher molecular weight, reaching a maximum of 12.2 μm s<sup>-1</sup> with pDADMAC (400-500 kDa), at 25 g<sub>pDADMAC</sub> kg<sup>-1</sup><sub>packed yeast</sub>. At this concentration, the floc sizes attained a plateau at 200 µm. A solution of branched PEI with a broad molecular weight range (500-100 kDa) showed the highest growth rate (8.8 μm s<sup>-1</sup> at 25 g<sub>PEI</sub> kg<sup>-1</sup><sub>packed yeast</sub>) in comparison with two other linear PEI flocculants of molecular weights 10 kDa (3.1  $\mu m \text{ s}^{-1}$  at 15  $g_{PEI}$  $kg^{-1}_{packed\ yeast}$ ) and 70 kDa (5.6  $\mu m\ s^{-1}$  at 25  $g_{PEI}$ kg<sup>-1</sup><sub>packed yeast</sub>). PEG, a non-ionic polymer, did not follow this trend. The maximum growth rate observed, 0.6 µm s<sup>-1</sup>, was obtained using 100 KDa PEG at 25 g<sub>PEG</sub> kg<sup>-1</sup><sub>packed yeast</sub>.

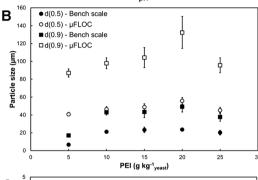
#### 4. Discussion

We set out to develop a platform to study flocculation by integrating high-speed imaging and computational analysis with a microfluidic device. Microfluidic devices nowadays are wellestablished experimental tools for process characterisation due to the precise control over the microenvironment and the possibility to integrate analytical tools.<sup>33–36</sup> These systems have been used extensively to study upstream bioprocessing steps, 37-41 but the number of reports of microfluidic devices developed to study process optimisation of downstream processing steps, such as purification and separation of biomolecules, is still limited. 27,42-48 In downstream bioprocessing, flocculation has attracted renewed interest but suitable analytical tools to comprehensively understand the flocculation mechanism have been absent. The precise control over the microenvironment afforded by microfluidic devices opened up an opportunity to investigate, for the first time, the formation and growth of flocs independently from floc breakage and ageing phases.

Yeast homogenate and flocculant were brought into contact in a controlled way in the microfluidic flocculation device (µFLOC) by hydrodynamic focussing, with the flocs growing in the long spiral-shaped channel (Fig. 1). Fresh

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 d(0.5) - Bench scale od(0.5) - µFLOC ■d(0.9) - Bench scale Ļ □d(0.9) - µFLOC Particle size (µm) 7.5 ●d(0.5) - Bench scale Od(0.5) - uFLOC 140



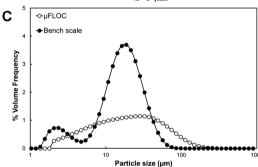


Fig. 3 Saccharomyces cerevisiae floc size characterisation using laserscattering in the microfluidic flocculation device (µFLOC) and benchscale measurements. (A) Particle size variation with pH. The concentration of flocculant, PEI (MW 50-100 kDa), was 20 g kg<sup>-1</sup><sub>packed yeast</sub>. (B) Particle size variation at pH 7.4 with different concentration of the flocculant, PEI (MW 50-100 kDa), in the range of 5-20 g kg<sup>-1</sup><sub>packed yeast</sub>. Error bars represent one standard deviation about the mean of five independent data points (n = 5). (C) Particle size distributions (PSD) of flocs from the  $\mu$ FLOC and bench-scale experiments for 20 q<sub>PEI</sub> kg<sup>-1</sup><sub>packed yeast</sub> at pH 7.4.

flocculant molecules were constantly supplied from the sheath flow streams to the centre stream wherein the flocgrowth occurred. The spiral-shaped channel had a relatively large cross-sectional area with an aspect ratio of 1 thus avoiding restrictions on floc-growth, for example due to channel walls, during the floc-formation and early growth phase. Dean numbers (De) calculated for the µFLOC varied from 0.008 (spiralling channel close to the outlet, radius of 10 mm) to 0.011 (close to the inlet, radius of 21 mm), thus the effect from Dean flow was negligible.49 Furthermore, the compact footprint afforded by the spiralling channel facilitated the coupling with light microscopy, enabling the visual observation of floc-formation and growth as the flocs travelled along the channel (Fig. 4).

Validation experiments performed with the µFLOC showed a decrease in the  $\zeta$  potential with increasing pH values. This indicated that the configuration of polyethylenimine (PEI) strands became more energy stabilised as the pH shifted from 5 to 7.5, 50,51 enhancing the rate of flocculation at nearzero mobility (Fig. 2). (Energy stabilisation is the relaxation or re-conformation of an already adsorbed flocculant; it has a significant effect on flocculation rates and determines whether charge neutralisation or polymer-bridging is the dominant mechanism<sup>50</sup>). This is also supported by the increasing floc sizes (Fig. 3A). This energy stabilisation of PEI leads to an increase in the electrostatic attraction in the microenvironment and higher surface site coverage, thereby enhancing the rate of flocculation. An exact parity was not observed between the µFLOC and bench-scale experiments, for both pH and PEI. Lower  $\zeta$  potentials were observed in the uFLOC and can be attributed to either the difference in the measurement setup or the difference in the concentration profiles of flocculants in the liquid bulk. For the former, samples from the bench-scale were manually added with a Pasteur pipette, whereas the outlet of the uFLOC was connected directly to the cuvette in the Zetasizer, preventing sedimentation of the flocs in the measurement cuvette. Furthermore, a focussed flow within the µFLOC which leads to the formation of larger flocs could have led to the depletion of the cationic flocculants in the bulk. In contrast, higher  $\zeta$  potential values were consistently recorded at the bench-scale. A uniform mixing homogeneity leading to the formation of smaller flocs may have resulted in a higher concentration of cationic flocculant in the liquid bulk. Even though these are possible explanations for the lack of exact parity, it should be noted that there is a strong linear correlation between the uFLOC and the bench-scale experiments for both pH and PEI. There is thus no other effect apart from pH and flocculant dosage that affects the  $\zeta$  potential, underlining the validity of the microfluidic approach to analyse flocculation.

Higher floc sizes were observed in the µFLOC compared to the bench-scale, which agrees with the lower zeta potential in the µFLOC (Fig. 3). This can also be attributed to negligible breakage in the µFLOC device, indicated by the low shear rate (80 s<sup>-1</sup>; ESI† D) as compared to values typically encountered in batch flocculation systems, such as systems comprising of a 6-blade Rushton turbine (>200 s<sup>-1</sup>).<sup>21</sup> After mixing, all the PEI strands are bound to the yeast homogenate particles. This results in a prolonged growth phase which ultimately leads to the formation of larger particles without the flocs suffering breakage (for the PSDs of flocs measured in situ in the µFLOC see ESI† E). This is further corroborated by the plateauing observed in particle size at approx. 250 µm, when the flocs in the µFLOC were monitored by image analysis (Fig. 5). Flocs larger than 250 µm were exposed to increasing shear rates closer to the walls, and hence growth continued only in the direction of the flow (ESI† D). Floc sizes above 300 µm were therefore disregarded from the growth kinetics calculations. Similarly, a filter was implemented for flocs smaller than 5 µm to facilitate image analysis.

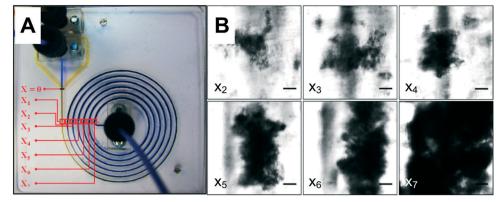


Fig. 4 (A) Photograph of the microfluidic flocculation device (µFLOC) filled with coloured dyes showing the seven positions where flocs were imaged along the channel. The x positions from the point of confluence (x = 0 mm) are  $x_1 = 14$ ,  $x_2 = 143$ ,  $x_3 = 259$ ,  $x_4 = 363$ ,  $x_5 = 454$ ,  $x_6 = 533$ , and  $x_7$  = 599 mm. (B) S. cerevisiae flocs formed along the  $\mu$ FLOC, from  $x_2$  to  $x_7$ . Images were taken at 2000 fps and 16.67  $\mu$ s exposure time. Scale bars represent 50 µm.

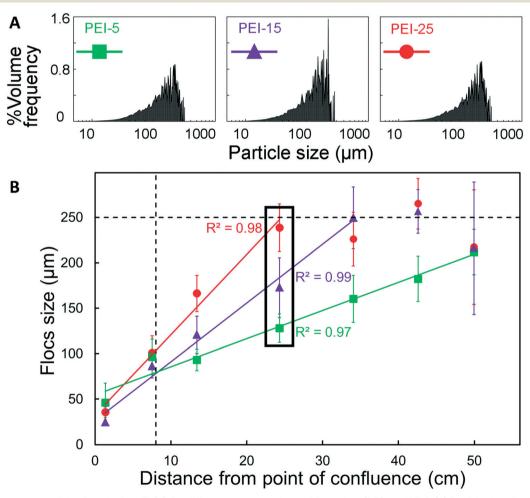


Fig. 5 Saccharomyces cerevisiae flocs in the μFLOC for different concentrations of flocculant (PEI) at pH 7.4. (A) Particle size distributions (PSD) of S. cerevisiae flocs in the presence of 5, 15 and 25 g  $kg^{-1}_{packed yeast}$  of PEI (MW 50-100 kDa). (B) Floc growth recorded along the length of the  $\mu$ FLOC for different imaging positions  $(x_1,...x_7)$  and different concentrations of PEI, i.e. 5 (green), 15 (purple) and 25 (red)  $g_{PEI}$   $kg^{-1}_{packed\ yeast}$ . The data points represent the average of the d(0.9) flocs. Full lines represent linear regression ( $R^2 > 0.97$  for all three concentrations) which are a convenient way to analyse floc growth. Growth of flocs plateaued as the particle sizes approached 250 µm; dashed vertical and dashed horizontal lines indicate the points where complete mixing is achieved and half of the channel width (250 µm), respectively. Error bars represent one standard deviation about the mean of five independent data points (n = 5). The data points shown within the box with black lines correspond to the d(0.9) values of the PSD in (A).

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Table 2 Flocculation growth rates of yeast homogenate with different flocculants obtained in the microfluidic flocculation device (μFLOC). The concentration and the molecular weights of the flocculants were varied

		Flocculatio					
Flocculant		Flocculant concentrations (g <sub>flocculant</sub> kg <sup>-1</sup> <sub>packed yeast</sub> )					
	Mol. wt (kDa)	5	10	15	20	25	
PEG	6	0.3	$0^a$	$0^a$	0.5	0.2	
	100	$0^a$	$0^a$	$0^a$	$0^a$	0.6	
PEI	10	1.5	2.9	3.1	3.1	2.6	
	70	3.0	4.5	4.3	3.9	5.6	
	50-100	3.1	4.9	6.5	6.0	8.8	
pDADMAC	<100	3.6	1.3	5.1	6.9	7.6	
	200-350	0.4	3.2	8.3	10.7	8.1	
	400-500	4.5	3.8	10.2	9.3	12.2	

PEG - polyethylene glycol, PEI - polyethylenimine, pDADMAC - poly(diallyldimethylammonium chloride). <sup>a</sup> The growth rate of 0 μm s<sup>-1</sup> indicates that an increase in floc size was not observed.

Two distinct size populations were seen in the PSD in the bench-scale, with the floc population at 3 µm shifting towards the larger floc population with increasing PEI concentration (Fig. 3C). From a flocculation point of view, this indicates a reduction in the charge-imbalance between the cationic polymer and anionic cell homogenate. 11,50,52 The shift in the PSD peaks also demonstrates the change in the flocculation mechanism.<sup>52</sup> A low surface site coverage of colloidal particles by the flocculant (5-15 kg<sup>-1</sup><sub>packed yeast</sub>) leads to the destabilisation of the particles, whereas at higher surface site coverage (at 20-25 g kg<sup>-1</sup>packed yeast), the colloidal particles are sterically stabilised. In contrast, the presence of only a single size (mono-modal) population in the µFLOC can be attributed to a nucleation zone near the centre of the channel formed by the hydrodynamic focussing. This yields a high-concentration region of oppositely charged particles increasing the proximity between the flocculant and the yeast homogenate. Furthermore, the presence of convective forces (Pe = 2500) facilitates the adsorption of flocculants onto the cell suspension in this nucleation zone. There were no other observable effects within the current device & buffer system that affected the zeta potential of flocs, underlining the validity of the µFLOC to analyse flocculation.

Flocculation growth rates are known to be influenced by the charge density, concentration and molecular weight of the flocculant. In particular, the charge density decides the optimum dosage concentration for the charge neutralisation mechanism and typically, concentrations of 0.1 to 0.2 mg  $L^{-1}$ are used,29 while the molecular weight of the polymer influences the polymer bridging mechanism. PEI carries a high cationic charge density53 and is affected by the pH and the ionic strength of the aqueous medium. 31,51,54 pDADMAC has a higher cationic charge density than PEI, having a value of 100 mol%.29 PEG, on the contrary, is a non-ionic polymer and its action is attributed to its capability to alter the interactions of cells and proteins with water, and also between each other.55 Therefore, one would expect the highest growth rates for pDADMAC, followed by PEI, with little growth when PEG is used.

Forty different conditions were evaluated with the μFLOC. As can be seen from Table 2, the highest growth rates in the μFLOC were measured for pDADMAC, followed by PEI. No growth or low growth rates were recorded for PEG. Furthermore, in general, when the dosage was increased a higher growth rate was detected. The growth rates measured with the uFLOC are therefore consistent with the effects of charge density, concentration and molecular weight of the flocculant. In some cases, for example for PEI (10 kDa) and pDADMAC (200-350 kDa), increasing the concentration of the flocculant above 20 g<sub>flocculant</sub> kg<sup>-1</sup><sub>packed yeast</sub> did not yield a higher growth rate, revealing the optimal point of flocculation. Addition of flocculants beyond the optimal level hinders the flocculation process, due to charge imbalance and electrostatic repulsion between the excess flocculants and the ones adsorbed. The uFLOC thus allows rapid and inexpensive screening of new flocculants and cell suspensions, and offers growth-kinetics based ranking of flocculating conditions in a quantitative way.

In the future, this device could also be employed to further our model understanding of flocculation and colloidal science.56 The most widely used model for flocculation is the classical expression of Smoluchowski's equation 4,57,58 for hetero-aggregation. This expression is governed by two aspects, perikinetic (due to Brownian motion and diffusive adsorption, leading to attachment) and orthokinetic flocculation (transport of flocculants due to shear). While solving the classical form of the Smoluchowski's equation, one typically assumes that a) the collision efficiency is equal to unity (i.e. any collision between two particles will lead to the formation of an aggregate), b) flow is laminar (laminar shear stress profile), c) floc breakage does not occur, d) all particles are monodisperse, e) all particles are spherical, and f) collision occurs only between two particles. 4,59 By isolating floc growth from breakage with the µFLOC, we have developed a device for which the assumptions a) to c) hold. The other assumptions are particle specific and are difficult, if not impossible to fulfill with biological systems. By implementing additional monitoring capabilities, such as in situ dynamic light scattering (DLS), floc sizes (and their aggregation) in the micron

and sub-micron range, i.e. in the range of particle sizes for which models based on the Smoluchowski's equation have typically been applied (primary flocculation phase), could be detected. For larger floc sizes, i.e. the secondary flocculation phase, current models are typically limited to extrapolating from Smoluchowski's model, using for example population balancing methods. With our device, however, we do not have to resort to such approaches, since floc growth kinetics for floc sizes above 50 µm are directly accessible. Thus, with additional detection capabilities, the µFLOC could be employed to describe and verify models for both primary and secondary flocculation phases.

#### 5. Conclusions

We successfully developed for the first time a microfluidic device for flocculation analysis, the µFLOC, and we have shown for the first time on-line and in situ detection and quantification of floc sizes and of growth kinetics of floc formation. Real-time monitoring of floc formation was enabled by combining the µFLOC with high-speed imaging and related image processing. The obtained time-course values for floc formation represents a degree of monitoring not attainable with traditional macroscopic systems, which rely on sample dispersion and sample handling steps, and largely depend on end-point measurements. The fine control over the fluid flow afforded by microfluidics facilitated the observation of individual flocs, decoupled the growth phase from the breakage phase of flocs, and therefore enabled quantification of flocculation growth. The µFLOC was challenged with a set of industrially relevant flocculation agents to study the impact of charge density, molecular weight and concentration on the flocculation in forty different growth conditions.

We have therefore established and characterised a new screening tool for the rapid and cost-effective analysis of flocculation processes from tiny amounts of flocculating reagents and cell material. This novel tool enables both the rapid testing of new flocculant formulations and the determination of process conditions to achieve rapid and effective flocculation, which thus far has been a tedious and expensive task for bioprocess engineers. Only one flow rate was required to evaluate forty different growth conditions, yet flow rates could easily be changed to analyse a broader range of flocculating agents, conditions and shear rates (for example to promote floc breakage). Measuring the sizes of the sub-micron particles in the sample suspension, a critical feature to fully understand flocculation processes, is currently outside the detection limit of the developed optical methodology, but could be implemented by incorporating an in situ dynamic light scattering (DLS) technique with our device. This may then also open the opportunity to derive more accurate mechanistic models of flocculation. In the future, we envisage that this tool will be employed to rapidly establish a ranking of different flocculation conditions for microbial fermentation and mammalian cell cultures, which can then subsequently be verified at larger scales.

### Conflicts of interest

There are no conflicts of interest to declare.

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## References

- 1 N. B. Wyatt, T. J. O'Hern, B. Shelden, L. G. Hughes and L. A. Mondy, Biotechnol. Bioeng., 2013, 110, 3156-3163.
- 2 S. Mondal, Y. K. Leong, J. L. Liow and S. R. Wickramasinghe, Powder Technol., 2013, 235, 426-430.
- 3 V. K. La Mer and R. H. Smellie Jr., Clays Clay Miner., 1960, 9, 295-314.
- 4 D. N. Thomas, S. J. Judd and N. Fawcett, Water Res., 1999, 33, 1579-1592.
- 5 D. E. Salt, S. Hay, O. R. T. Thomas, M. Hoare and P. Dunnill, Enzyme Microb. Technol., 1995, 17, 107-113.
- 6 A. Berrill, S. V. Ho and D. G. Bracewell, Biotechnol. Prog., 2008, 24, 426-431.
- 7 P. Milburn, J. Bonnerjea, M. Hoare and P. Dunnill, Enzyme Microb. Technol., 1990, 12, 527-532.
- 8 R. M. Cordes, W. B. Sims and C. E. Glatz, Biotechnol. Prog., 1990, 6, 283-285.
- 9 G. B. Habib, I. Holwill and M. Hoare, J. Biotechnol., 1997, 59,
- 10 S. R. Wickramasinghe, Y.-K. Leong, S. Mondal and J.-L. Liow, Adv. Powder Technol., 2010, 21, 374-379.
- 11 D. E. Salt, A. C. Bentham, S. Hay, A. Idris, J. Gregory, M. Hoare and P. Dunnill, Bioprocess Eng., 1996, 15, 71.
- 12 P. Narong and A. E. James, Colloids Surf., A, 2006, 274, 130-137.
- 13 J. Gregory, Colloids Surf., 1988, 31, 231-253.
- G. Espuny Garcia del Real, J. Davies and D. G. Bracewell, Biotechnol. Bioeng., 2014, 111, 2486-2498.
- 15 L. Sadasivan and C. A. Neyra, J. Bacteriol., 1985, 163, 716-723.
- 16 A. Vicente, J. M. Meinders and J. A. Teixeira, Biotechnol. Bioeng., 1996, 51, 673-678.
- 17 M. Zelger, S. Pan, A. Jungbauer and R. Hahn, Process Biochem., 2016, 51, 1610-1621.
- 18 S. Sharma, C.-L. Lin and J. D. Miller, Miner. Eng., 2017, 101,
- 19 R. Kothari, V. V. Pathak, A. Pandey, S. Ahmad, C. Srivastava and V. V. Tyagi, Bioresour. Technol., 2017, 225, 84-89.
- 20 Y. Zhou and G. V. Franks, *Langmuir*, 2006, 22, 6775–6786.

- 21 A. Chatel, P. Kumpalume and M. Hoare, *Biotechnol. Bioeng.*, 2014, 111, 913–924.
- 22 N. B. Wyatt, L. M. Gloe, P. V. Brady, J. C. Hewson, A. M. Grillet, M. G. Hankins and P. I. Pohl, *Biotechnol. Bioeng.*, 2012, 109, 493–501.
- 23 R. Ferron and S. Shah, Transp. Res. Rec., 2010, 2141, 89-91.
- 24 Y. K. Kang, J. Hamzik, M. Felo, B. Qi, J. Lee, S. Ng, G. Liebisch, B. Shanehsaz, N. Singh, K. Persaud, D. L. Ludwig and P. Balderes, *Biotechnol. Bioeng.*, 2013, 110, 2928–2937.
- 25 N. Singh, K. Pizzelli, J. K. Romero, J. Chrostowski, G. Evangelist, J. Hamzik, N. Soice and K. S. Cheng, *Biotechnol. Bioeng.*, 2013, 110, 1964–1972.
- 26 S. Akeprathumchai, B. Han, S. R. Wickramasinghe, J. O. Carlson, P. Czermak and K. Preiβ, *Biotechnol. Bioeng.*, 2004, 88, 880–889.
- 27 B. O'Sullivan, H. Al-Bahrani, J. Lawrence, M. Campos, A. Cázares, F. Baganz, R. Wohlgemuth, H. C. Hailes and N. Szita, *J. Mol. Catal. B: Enzym.*, 2012, 77, 1–8.
- 28 M. H. V. Werts, V. Raimbault, R. Texier-Picard, R. Poizat, O. Français, L. Griscom and J. R. G. Navarro, *Lab Chip*, 2012, 12, 808.
- 29 B. Bolto and J. Gregory, Water Res., 2007, 41, 2301-2324.
- 30 J. Suh, H.-J. Paik and B. K. Hwang, *Bioorg. Chem.*, 1994, 22, 318–327.
- 31 M. Neu, D. Fischer and T. Kissel, *J. Gene Med.*, 2005, 7, 992–1009.
- 32 A. D. Anastasiou, C. Makatsoris, A. Gavriilidis and A. A. Mouza, *Exp. Therm. Fluid Sci.*, 2013, 44, 90–99.
- 33 M. P. C. Marques and P. Fernandes, *Molecules*, 2011, 16, 8368–8401.
- 34 M. R. Leyden, R. J. Messinger, C. Schuman, T. Sharf, V. T. Remcho, T. M. Squires and E. D. Minot, *Lab Chip*, 2012, 12, 954–959.
- 35 Q.-S. Kang, X.-F. Shen, N.-N. Hu, M.-J. Hu, H. Liao, H.-Z. Wang, Z.-K. He and W.-H. Huang, *Analyst*, 2013, 138, 2613–2619.
- 36 N. Jaccard, R. J. Macown, A. Super, L. D. Griffin, F. S. Veraitch and N. Szita, *J. Lab. Autom.*, 2014, 19, 437–443.
- 37 D. Schäpper, M. N. H. Z. Alam, N. Szita, A. Eliasson Lantz and K. V. Gernaey, *Anal. Bioanal. Chem.*, 2009, 395, 679–695.
- 38 A. Zanzotto, N. Szita, P. Boccazzi, P. Lessard, A. J. Sinskey and K. F. Jensen, *Biotechnol. Bioeng.*, 2004, 87, 243–254.
- 39 T. V. Kirk and N. Szita, Biotechnol. Bioeng., 2013, 110, 1005–1019.

- 40 M. J. Davies, D. N. Nesbeth and N. Szita, *Chim. Oggi*, 2013, 31, 46–49.
- 41 P. Gruber, M. P. C. Marques, P. Sulzer, R. Wohlgemuth, T. Mayr, F. Baganz and N. Szita, *Biotechnol. J.*, 2017, 1600475.
- 42 M. S. Shapiro, S. J. Haswell, G. J. Lye and D. G. Bracewell, *Biotechnol. Prog.*, 2009, 25, 277–285.
- 43 J. Wen, E. W. Wilker, M. B. Yaffe and K. F. Jensen, *Anal. Chem.*, 2010, **82**, 1253–1260.
- 44 H. Yang, J. M. Mudrik, M. J. Jebrail and A. R. Wheeler, *Anal. Chem.*, 2011, 83, 3824–3830.
- 45 N. Assmann, A. Ładosz and P. Rudolf von Rohr, Chem. Eng. Technol., 2013, 36, 921–936.
- 46 J. Huft, C. A. Haynes and C. L. Hansen, *Anal. Chem.*, 2013, 85, 2999–3005.
- 47 P. Vázquez-Villegas, E. Ouellet, C. González, F. Ruiz-Ruiz, M. Rito-Palomares, C. A. Haynes and O. Aguilar, *Lab Chip*, 2016, 16, 2662–2672.
- 48 M. P. C. Marques and N. Szita, Curr. Opin. Chem. Eng., 2017, 18, 61-68.
- 49 D. Di Carlo, D. Irimia, R. G. Tompkins and M. Toner, *Proc. Natl. Acad. Sci. U. S. A.*, 2007, **104**, 18892–18897.
- 50 J. Gregory and S. Barany, Adv. Colloid Interface Sci., 2011, 169, 1-12.
- 51 R. Mészáros, I. Varga and T. Gilányi, *Langmuir*, 2004, 20, 5026–5029.
- 52 S. Barany and A. Szepesszentgyörgyi, *Adv. Colloid Interface Sci.*, 2004, 111, 117–129.
- 53 M. X. Tang and F. C. Szoka, Gene Ther., 1997, 4, 823-832.
- 54 Z. R. Amin, M. Rahimizadeh, H. Eshghi, A. Dehshahri and M. Ramezani, *Iran. J. Basic Med. Sci.*, 2013, 16, 150–156.
- 55 J. Israelachvili, Proc. Natl. Acad. Sci. U. S. A., 1997, 94, 8378–8379.
- 56 J. C. Berg, An Introduction to Interfaces & Colloids: The Bridge to Nanoscience, World Scientific Publishing Co. Pte. Ltd., New Jersey, 2010, illustrate.
- 57 K. Rahn-Chique, A. M. Puertas, M. S. Romero-Cano, C. Rojas and G. Urbina-Villalba, *Adv. Colloid Interface Sci.*, 2012, 178, 1–20.
- 58 S. K. Friedlander and C. S. Wang, J. Colloid Interface Sci., 1967, 24, 170–179.
- 59 S. R. Wickramasinghe, B. Han, S. Akeprathumchai, A. Jaganjac and X. Qian, *Powder Technol.*, 2005, **156**, 146–153.