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Sorption kinetics of metallic and organic contaminants on micro- and nanoplastics: remarkable dependence of the intraparticulate contaminant diffusion coefficient on the particle size and potential role of polymer crystallinity†

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We developed a mechanistic diffusion model to describe the sorption kinetics of metallic and organic contaminants on nano- and micro-plastics. The framework implements bulk depletion processes, transient fluxes, and fully adaptable particle/water boundary conditions, *i.e.* not only the typically assumed simple linear Henry regime, which is not applicable to many contaminant-particle situations. Thus, our model represents a flexible and comprehensive theory for the analysis of contaminant sorption kinetics, which goes well beyond the traditional empirical pseudo first or second order kinetic equations. We applied the model to the analysis of a large body of literature data on the equilibrium and kinetic features of sorption of a wide range of contaminants by diverse types and sizes of plastic particles. Results establish the paramount importance of sorption boundary conditions (Henry, Langmuir, or Langmuir–Freundlich) and reveal interesting and often overlooked sorption features that depend on the plastic particle size and the extent to which the target compound is depleted in the bulk medium. The greater degree of polymer crystallinity reported for smaller particles may underlie our findings that the intraparticulate contaminant diffusion coefficient decreases with a decreasing particle size. We establish a universal law to predict the sorption kinetics and diffusion of any compound within any plastic phase, which has far reaching importance across many domains relevant to the environment and human health.

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Environmental significance

Plastic particles interact with many other environmental contaminants, including inorganic compounds (*e.g.* metal ions) and organic compounds (*e.g.* pesticides and pharmaceuticals). Such interactions modify water quality and have consequences for risk assessment of plastic pollution. Notably, the rate at which contaminants are distributed within plastic particles is fundamental for understanding the potential environmental and health impacts of micro- and nanoplastics. We show that the size of plastic particles is the most important factor.

1. Introduction

The ubiquitous presence of micro- and nano-plastic particles in the environment has raised concerns about their potential impacts on aquatic and terrestrial ecosystems. Plastic particles, together with their associated polymer additives, exert a range of adverse effects on biota at all trophic levels.^{1–4} In addition, plastic particles interact with and modify the chemical speciation and bioavailability of a wide range of inorganic and organic

contaminants as well as other essential compounds in the environment. Knowledge of the thermodynamic and kinetic features of plastic particle interactions with essential and toxic compounds is thus fundamental for robust risk assessment of micro-/nano-plastics and determination of water quality. Conflicting reports in the literature on the potential of plastic particles to mitigate^{5–7} or exacerbate^{8–10} the bioaccumulation and/or toxicity of compounds reflect the general lack of consideration of the kinetics of the underlying processes and the involved timescales.

To date, most studies have interpreted the sorption kinetics of compounds on plastic particles with empirical (pseudo-) first or second order kinetics.^{11–14} Although some of these empirical models also refer to intraparticulate diffusion, most do not provide a value for the pertaining diffusion coefficient.^{15–19} In cases where diffusion coefficients of organic compounds in

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plastics have been reported, there are conflicting reports on the dependence of such values on the type of organic compound or its molar mass, with the relationship depending on the nature of the polymer (amorphous *vs.* glassy) and its extent of hydration.^{20–23} Any molar mass dependence of the intraparticle diffusion coefficient is greater for glassy, dry polymers.²¹

We previously developed an interpretation framework to describe the sorption kinetics of compounds on plastic particles in aqueous media by separate and coupled considerations of the transient and steady-state diffusion processes.²⁴ This framework, built upon the empirical 2-compartment model by Bayen *et al.*,²⁵ formulates the relaxation of the former diffusion process toward a steady state in the form of an *ad hoc* exponential decay function. It is further restricted to cases where the sorption isotherm verifies linearity, *i.e.* the so-called Henry sorption regime. The present work extends this approach to a fully rigorous numerical solution of the governing Fickian transfer equations that define the distribution of target compounds at the surface and in the body of plastic particles. The approach adopted herein is valid for all spatial scales and time scales, from nano to micro-sized particles, and it implements, over the time course of the sorption, the most appropriate surface sorption boundary in the form of a linear (Henry), Langmuir, or Langmuir–Freundlich isotherm. Furthermore, the extent to which the target compound is depleted in the bulk aqueous medium during the sorption process is considered. Based on this theory, which formulates the intricate coupling between bulk depletion, surface adsorption and diffusion-driven intraparticle accumulation of contaminants over time, a robust algorithm is developed to recover consistently measured equilibrium and kinetic sorption data for contaminant/plastic systems. Our approach is successfully applied to interpret more than 100 literature data sets covering a large range of contaminants (metals and organics), polymer compositions and sizes of the plastic particles. The results demonstrate a remarkable law that connects the intraparticle contaminant diffusion coefficient and plastic particle size regardless of the contaminant and particle chemistry considered.

2. Materials and methods

2.1 Theoretical framework

In what follows, we consider the sorption of metallic or organic contaminants, collectively denoted by X, on spherical plastic particles of radius a and volume V_p , present at a volume fraction φ in a dispersing aqueous medium (Fig. 1). We detail the expressions for spherical particles because most suitable experimental data are for this geometry. By properly accounting for geometry in the flux expressions, the theory can be applied to fibres, films, *etc.* To connect the relevant spatial scales of the problem, *i.e.* from the particle dispersion scale (Fig. 1A) to the levels of a single plastic particle (Fig. 1B) and the interface it forms with the medium (Fig. 1C), particles are distributed according to a Kuwabara representation (Fig. 1A), where they are surrounded by a virtual cell of radius r_c such that the particle/solution volume ratio in that cell equates φ , leading to $r_c = a\varphi^{-1/3}$.^{26–28} We further adopt the radial coordinate system, r ,

with the origin at the particle center (Fig. 1B). Under the conditions of interest, particle dispersion is diluted so that $\varphi \ll 1$ or $r_c/a \gg 1$. A glossary of symbols is reported in the ESI.†

In our previous study, we showed that intraparticle diffusion limits the overall kinetics of contaminant accumulation by plastic particles,²⁴ *i.e.* there is no diffusion limitation in the extraparticle region. This property is reflected by the value of the intraparticle diffusion coefficient of X, $D_{X,p}$ ($\text{m}^2 \text{s}^{-1}$), which is orders of magnitude lower than the one operational in the aqueous extraparticle region, $D_{X,w}$ ($\text{m}^2 \text{s}^{-1}$).^{20,21} Accordingly, we consider herein that equilibrium conditions hold in the extraparticle zone. This setting is validated by comparison with experimental data detailed below and by comparison between the relevant timescales for intra- and extraparticle diffusion. It indicates that the experimentally observed timescales for sorption are orders of magnitude greater than those that would be operational if diffusion in the extraparticle region is limiting.

Accordingly, the kinetics of X sorption by the plastic particles is mediated solely by the intraparticle diffusion process, and throughout the intraparticle accumulation, the concentration of X at the particle surface ($r = a$) is systematically in equilibrium with the one far from the particle. Let $c_{X,w}(a < r \leq r_c, t)$ denote the extraparticle concentration of X at time t and position r . Then, we have $c_{X,w}(r, t) = c_{X,w}^*(t)$, where $c_{X,w}^*(t)$ is the concentration of X in bulk medium, with $c_{X,w}^{*,0} = c_{X,w}^*(t = 0)$ the initial concentration of X therein. $c_{X,w}^*(t)$ may decrease with time depending on the extent of depletion of X in the bulk medium owing to intraparticle X accumulation and ensuing removal from the medium (Fig. 1). Equilibrium in the extraparticle region imposes that the concentration of X on the polymer side of the particle/solution interface is related to the concentration of X at the solution side of that interface according to an equilibrium partitioning relationship (isotherm) of the form (Fig. 1C):

$$c_{X,p}(r = a, t) = f_{i = H, L, LF}(c_{X,w}^*(t)) \quad (1)$$

where $c_{X,p}(0 \leq r \leq a, t)$ denotes the intraparticle concentration of X at t and r , and $f_{i = H, L, LF}(c_{X,w}^*(t))$ denotes the expression of Henry ($i = H$), Langmuir ($i = L$) or Langmuir–Freundlich ($i = LF$) surface adsorption isotherm. The nature of the isotherm obviously depends on the X contaminant–plastic particle system considered. Developed formulations of $f_{i = H, L, LF}(c_{X,w}^*(t))$ are written according to

$$f_H(c_{X,w}^*(t)) = K_{p,w}^H c_{X,w}^*(t), \quad (2a)$$

$$f_L(c_{X,w}^*(t)) = \frac{K_{p,w}^L c_{X,w}^*(t)}{1 + K_{p,w}^L c_{X,w}^*(t)} c_{X,p}^{\text{max},s}, \quad (2b)$$

$$f_{LF}(c_{X,w}^*(t)) = \frac{(K_{p,w}^{LF} c_{X,w}^*(t))^{1/p_{LF}}}{1 + (K_{p,w}^{LF} c_{X,w}^*(t))^{1/p_{LF}}} c_{X,p}^{\text{max},s}, \quad (2c)$$

where $K_{p,w}^H$ (dimensionless), $K_{p,w}^L$ ($\text{mol}^{-1} \text{m}^3$) and $K_{p,w}^{LF}$ ($\text{mol}^{-1} \text{m}^3$) are the partition coefficients of X at the polymer/water



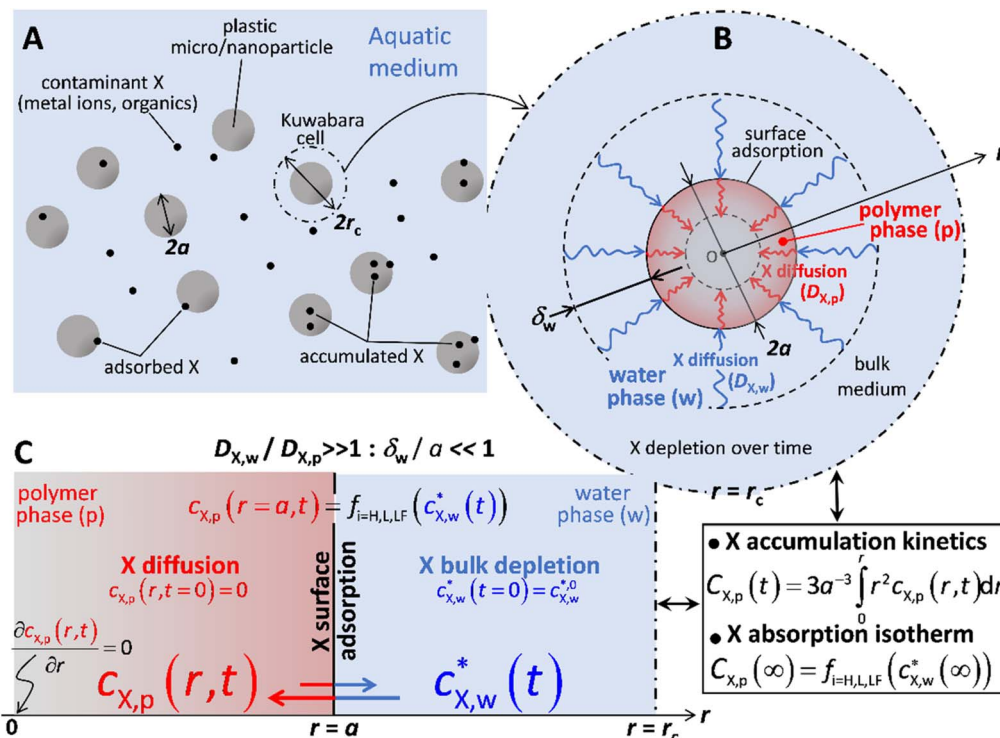


Fig. 1 Schematic view of the processes considered in the numerical analysis of the sorption kinetics of metal ions and organic molecules (collectively denoted by X) on micro- and nano-plastics, showing (A) the system at the level of the bulk dispersion, (B) processes considered at the individual particle level, and (C) the particle/water interface. All symbols are defined in the main text and glossary. Briefly, $D_{X,w}$ and $D_{X,p}$ are the diffusion coefficients of X operational in the extraparticulate aqueous medium and in the plastic particle body, respectively; a is the particle radius; δ_w is the extraparticulate diffusion layer thickness; $c_{X,w}(r, t)$ and $c_{X,p}(r, t)$ are the local concentrations of X at the radial position r and time t in the water and polymer phase, respectively; $c_{X,w}^*(t)$ is the bulk concentration of X in the medium at t ; and $C_{X,p}(t)$ corresponds to the overall concentration of X in the plastic particle at t . Panel (C) specifies the boundaries adopted at the particle center, at the particle/solution interface and in the bulk medium positioned at $r = 0$, $r = a$ and $r = r_c$, respectively, with r_c the radius of the Kuwabara cell. The scheme is not to scale. See details in the text.

interface (Fig. 1C), $1/p_{LF}$ is the heterogeneity parameter in the Langmuir-Freundlich isotherm with values between 0 and 1, and $c_{X,p}^{\max,s}$ is the maximum surface sorption capacity (relevant for $i = L, LF$). We note that the equilibrium partition coefficients derived herein are effective rather than intrinsic chemical values, *i.e.* they include any physical electrostatic and/or hydrophobic interaction contributions to the stability of the contaminant-plastic particle system, and thus are inherently functions of the medium composition (pH, ionic strength, *etc.*). However, in terms of the dynamic features, there is no significant effect of the various interaction contributions to the effective equilibrium partition coefficients on the diffusional properties of the contaminants as long as the length scale over which these contributing interactions operate is much smaller than the particle size. The rationale for this argument is provided in our previous work²⁹ and is supported by the data analysed herein (see Results and discussion).

The intraparticulate time-dependent concentration profile of X, $c_{X,p}(0 < r \leq a, t)$ is defined by the transient Fick diffusion equation:

$$\frac{\partial c_{X,p}(r, t)}{\partial t} = D_{X,p} \left[\frac{\partial^2 c_{X,p}(r, t)}{\partial r^2} + \frac{2\gamma}{r} \frac{\partial c_{X,p}(r, t)}{\partial r} \right], \quad (3)$$

where $\gamma = 1$ and $\gamma = 0$ hold for spherical and linear diffusion, respectively. Intraparticulate diffusion within a spherical particle is inherently convergent towards a point, *i.e.* the center of the particle body. Thus, spherical diffusion necessarily applies. However, if the particle body contains zones that are inaccessible to the diffusing contaminant X, the effective size of the “point” to which X diffuses increases. In such a case, depending on the size of the inaccessible intraparticulate zones and the thickness of the intraparticulate diffusion layer, linear diffusion may be operational. The boundaries associated with the partial differential eqn (3) are

$$c_{X,p}(0 \leq r \leq a, t = 0) = 0 \quad (4)$$

which defines the initial situation in which particles are free of X,

$$\left. \frac{\partial c_{X,p}(r, t)}{\partial r} \right|_{r=0} = 0 \quad (5)$$

This is derived from the symmetry of the concentration profile at the particle center $r = 0$, and the remaining boundary is provided by the surface isotherm condition given by eqn (1) and (2).



The mass balance condition of X in the Kuwabara cell of radius r_c is further written as follows:

$$4\pi \int_a^{r_c} [c_{x,w}(r, t) - c_{x,w}(r, t=0)] r^2 dr = -4\pi a^2 D_{X,p} \int_0^t \left(\frac{\partial c_{X,p}(r, t)}{\partial r} \Big|_{r=a} \right) dt, \quad (6)$$

where the left side corresponds to the amount of X removed from the extraparticulate region between $t = 0$ and t , and the right side is the integral over time of the X accumulation flux at the particle surface $r = a$, which corresponds to the amount of accumulated X at t . Differentiating eqn (6) with respect to time and using the relation $c_{x,w}(r, t) = c_{x,w}^*(t)$, we obtain the following equation after rearrangements:

$$\frac{dc_{x,w}^*(t)}{dt} = -\frac{3D_{X,p}}{a} \frac{\varphi}{1-\varphi} \frac{\partial c_{X,p}(r, t)}{\partial r} \Big|_{r=a}, \quad (7)$$

which couples the bulk depletion rate and X concentration gradient at the particle surface.

The set of eqn (1)–(5) and (7) defines the time-dependent distribution of X in the particle body, $c_{x,p}(r, t)$, in the aqueous medium, $c_{x,w}^*(t)$, and at the particle surface, $c_{x,p}(r = a, t)$, from the initial stage of the accumulation process to the equilibrium regime achieved at $t \rightarrow \infty$ by the partitioning of X between the intraparticulate polymer phase and aqueous medium. At any t , the overall concentration of X within the particles, denoted as $C_{X,p}(t)$, results from the following spatial integral of $c_{x,p}(r, t)$:

$$C_{X,p}(t) = \frac{4\pi}{V_p} \int_0^a r^2 c_{X,p}(r, t) dr. \quad (8)$$

The dependence of $C_{X,p}$ on time t featured by eqn (8) describes the X sorption kinetics on the plastic particles. For the sake of notational simplicity, we introduce the equilibrium concentrations $c_{x,w}^{*,eq} = c_{x,w}^*(t \rightarrow \infty)$, and $C_{X,p}^{eq} = C_{X,p}(t \rightarrow \infty)$. It is straightforward to verify that the X sorption isotherm must comply with the formulations:

$$C_{X,p}^{eq} = \frac{4\pi}{V_p} \int_0^a r^2 c_{X,p}(r, t \rightarrow \infty) dr = f_{i=H, L, LF} \left(c_{x,w}^{*,eq} \right), \quad (9a, b)$$

where eqn (9a) and (9b) refer to the first and second equality, respectively.

We verified that the decrease in $c_{x,w}^*(t)$ with time obtained from the numerical solution to eqn (1)–(5) and (7) could be properly fitted using the empirical relationship:

$$c_{x,w}^*(t) / c_{x,w}^{*,0} = 1 + \left(c_{x,w}^{*,eq} / c_{x,w}^{*,0} - 1 \right) [1 - \exp(-t/\tau_{depl})]^{\sigma_{depl}}, \quad (10)$$

where τ_{depl} (s) is the depletion timescale and σ_{depl} (dimensionless) is an empirical adjustment factor. Finally, the release kinetics of X from the particle (when dispersed in a medium initially free of X) can be formulated according to Crank's equation:³⁰

$$R_X(t) / R_X(t \rightarrow \infty) = 1 - \frac{6}{\pi^2} \sum_{n=1}^{\infty} \frac{1}{n^2} \exp(-n^2 \pi^2 D_{X,p} t / a^2), \quad (11)$$

where $R_X(t)$ is the release amount of X at time t .

2.2 Numerical analysis

Eqn (1)–(5) and (7) were written in terms of the reduced space and time variables $\bar{r} = r/a$ ($0 \leq \bar{r} \leq 1$) and $\bar{t} = t/(\beta\tau)$ ($0 \leq \bar{t} \leq 1$), respectively, where $\tau = a^2/D_{X,p}$ (s) is the intraparticulate diffusion timescale and β is a factor chosen for t to cover a range of desired values. Eqn (1)–(5) and (7) were made fully dimensionless with the further introduction of the scaled concentrations $\bar{c}_{x,w}^*(\bar{t}) = c_{x,w}^*(\bar{t})/c_{x,w}^{*,0}$ and $\bar{c}_{x,p}(\bar{r}, \bar{t}) = c_{x,p}(\bar{r}, \bar{t})/c_{X,p}^{norm; i=H, L, LF}$, where $c_{X,p}^{norm; i=H, L, LF}$ is defined by $c_{X,p}^{norm; i=H} = K_{p,w}^H c_{x,w}^{*,0}$ and $c_{X,p}^{norm; i=L, LF} = c_{X,p}^{max, s}$. The dimensionless forms of eqn (1)–(5) and (7) are specified by eqn (S1)–(S5) in ESI† Knowing the particle volume fraction φ , the particle radius a and the value of γ (0 or 1), the above nondimensionalisation procedure demonstrates that X partitioning is fully determined upon specification of the model equilibrium parameters $K_{p,w}^{i=H, L, LF}$, $1/p_{LF}$ (relevant for $i = LF$) and $c_{X,p}^{max, s}$ (relevant for $i = L, LF$), and the diffusion timescale $\tau = a^2/D_{X,p}$. Reduced eqn (S1)–(S5)† were subsequently discretized in the time domain according to the implicit Euler method³¹ and written as a function of the discretized concentrations denoted by $\bar{c}_{x,p}(\bar{r}, \bar{t} = \bar{t}_k) = \bar{c}_{x,p}^{(k)}(\bar{r})$ and $\bar{c}_{x,w}^*(\bar{t}_k) = \bar{c}_{x,w}^{*(k)}$ (both dimensionless), where the integer k runs from 1 to $N \gg 1$, and $\bar{t}_k = (k-1)\Delta\bar{t}$ is the discretized time with $\Delta\bar{t} = 1/(N-1)$ as the timestep adopted in the discretization scheme (eqn (S6)–(S10)†). The method leads in turn to the formulation of a set of $N-1$ space-dependent recursive differential equations of the second order defining the concentration profiles $\bar{c}_{x,p}^{(k=2, \dots, N)}(\bar{r})$ (eqn (S7)†), with $2(N-1)$ boundaries derived from eqn (1) and (5) applicable at $\bar{r} = 1$ and $\bar{r} = 0$, respectively (eqn (S6) and (S9) in ESI†). Starting with the initial condition $\bar{c}_{x,p}^{(k=1)}(0 \leq \bar{r} \leq 1) = 0$ and $\bar{c}_{x,w}^{*(k=1)} = 1$ (eqn (S8) and (S11) in ESI†), and using the discretized form of the dimensionless mass balance condition formulated by eqn (7) (eqn (S10) in ESI†), the set of recursive differential equations was solved iteratively for $k = 2, \dots, N$ using COLSYS collocation algorithm,^{32,33} which already proves its high efficiency in various complex modeling settings.^{34–36} The procedure calls for the solution $\{\bar{c}_{x,p}^{(k-1)}(\bar{r}), \bar{c}_{x,w}^{*(k-1)}\}$ obtained at step $k-1$ to find the concentration and bulk depletion profiles $\{\bar{c}_{x,p}^{(k)}(\bar{r}), \bar{c}_{x,w}^{*(k)}\}$ at step k (see details in ESI†). After the completion of the iteration and knowledge of the intraparticulate concentration profiles at any time $t_{k=1, \dots, N}$, the kinetics of X sorption, $C_{X,p}(t = t_{k=1, \dots, N})$, was evaluated by eqn (8) with the spatial integral estimated by applying the rectangle method. The convergence of the numerical results was achieved within a satisfactory delay (tens of seconds to mins) for $N \geq 1500$. The robustness and validity of the adopted algorithm were further addressed by verifying that the outcomes were independent of the values adopted for N and β , and we systematically checked the expected equivalency between eqn (9a) and (9b). The full numerics was implemented in a FORTRAN program called PLASTX, which could generate all relevant outputs of the problem (including $C_{X,p}(t)$, $C_{X,p}^{eq}$, $c_{x,p}(r, t)$ and $c_{x,w}^*(t)$) from a proper specification of the required model inputs (including τ and isotherm model descriptors).



2.3 Fitting of X isotherm and X sorption kinetic data

The flowchart describing the steps involved in fitting the X sorption isotherm and X intraparticulate accumulation data is shown in Fig. S1 in ESI.† The isotherm and sorption kinetic data were first selected from the literature according to the criteria detailed in the next section (step 1). The nature of the relevant isotherm (*i.e.* $i = H, L$ or LF) and the corresponding parameter descriptors $K_{p,w}^{i=H,L,LF}$, $1/p_{LF}$ and/or $c_{X,p}^{\max,s}$ were then evaluated by fitting the isotherm data to eqn (1) and (2) according to the Levenberg–Marquardt procedure and minimization of residues (step 2). In step 3, knowing the best isotherm type and its related theoretical descriptors (evaluated in step 2), the sorption kinetic data were fitted upon adjustment of the diffusion time scale τ using PLASTX code coupled with the freely available software PEST,³⁷ an open source program for model parameter estimation and uncertainty analysis. We summarize in Fig. S1† the various phases of the iterative dialog between PLASTX and PEST as well as the in- and out-information fluxes exchanged between these two programs until sorption data fitting is achieved within the prescribed convergence criterion. The coupled PLASTX-PEST-based method is directly inspired by our previous work on the modeling and fitting of proton adsorption isotherms on particulate organic matter, where PEST was adopted in combination with the involved numerical evaluation of particle electrostatics.^{35,38} The reader is referred to ref. 35 and

38 for details on PEST implementation. Finally, we emphasize that the fitting by the coupled PLASTX-PEST codes of some of the selected X sorption kinetic data required for the adjustment of τ and of the interfacial X partition coefficient $K_{p,w}^{i=H,L,LF}$ to a value that differed from the one derived in step 1. The flexibility of PLASTX-PEST easily allows the specification of the parameters to be adjusted to reach data fitting and those fixed by the user at prescribed values (Fig. S1†).

2.4 Data selection

We selected sufficiently documented literature data for which both equilibrium isotherm and sorption kinetics were reported for pristine plastic particles of spherical or approximately spherical geometry.^{11–13,16,39–67} The data (109 individual kinetic curves in total) correspond to the sorption of a wide variety of metal ions and organic compounds by a broad range of polymer types. The considered contaminants, (i), and polymers, (ii), include (but are not restricted to) (i) Cd(II), Cu(II), Pb(II), tetracycline, sulfamethoxazole, ciprofloxacin, atrazine, carbamazepine, triclosan, triadimefon, fluoranthene, phenanthrene, naphthalene, fluorene, *etc.*, and (ii) polystyrene, polyvinyl chloride, polyurethane, polypropylene, polyethylene, *etc.* In all cases, the plastic particles were the only complexants present in the aqueous media, *i.e.* considering chemical speciation dynamics in the dissolved aqueous phase is immaterial for



Fig. 2 Equilibrium and kinetic features of a system with low depletion of X in the bulk solution: sorption of benzophenone on polyethylene particles ($a = 2.75 \times 10^{-4}$ m). The panels correspond to (A) the equilibrium sorption isotherm; (B) kinetic sorption curves; (C) solution depletion profile; and (D) temporal evolution of the normalized intraparticulate concentration profiles, with the direction of increasing time indicated by the arrow. In (D), the timescale between the two plotted concentration profiles is $\Delta t = 3588$ s, starting at $t = 3588$ s. The condition at $t = 0$ (not shown) corresponds to plastic particles free of contaminants and to the initial bulk medium condition $c_{X,w}^*(t = 0) = c_{X,w}^{*,0}$. The Langmuir isotherm best described the equilibrium data, and τ was the only parameter optimized to fit the sorption curves (see Table S1† for the pertaining parameters). The isotherm curve (A) shows the experimental data (black circles)¹² and the best fit obtained according to the Langmuir sorption isotherm (eqn (1)–(2b), red curve, adjusted parameters: $K_{p,w}^1$ and $c_{X,p}^{\max,s}$); the kinetic sorption curve (B) shows the experimental data (black circles)¹² and the numerically computed values, eqn (1)–(2b), (3)–(5), (7) and (8) (red curve); and the depletion profile (C) shows the values obtained from numerical computation, eqn (1)–(2b), (3)–(5) and (7) (red curve). The maximal extent of bulk depletion is 6.3% in the kinetic sorption data, and from the fitted τ of 108.5 h, the derived diffusion coefficient is $D_{X,p} = 1.94 \times 10^{-15}$ m² s⁻¹.



present purposes. The reader is referred to Table S1† for exhaustive lists. The results encompass cases in which the equilibrium sorption data were best described by linear (Henry), Langmuir, and Langmuir–Freundlich isotherms (see Table S1†). We excluded studies in which the particle size was not reported or only poorly documented,^{18,68} those which reported only kinetic data (*i.e.* no corresponding equilibrium isotherms),^{69,70} cases where very few time points were recorded in the kinetic regime,^{71,72} and those which exhibited gross inconsistencies between the kinetic and equilibrium data.^{73–75}

In cases where the particle size was reported as a range of radii, computations were performed for the smallest and largest values, and both results are presented in Table S1.† A density of unity was assumed for all polymers for computing particle volume fractions, ϕ , and for converting reported sorbed concentrations (typically given in mass units) to units of mol m^{-3} . The uncertainty on the fitted parameters (Table S1†) was estimated by the 95% confidence intervals computed by PEST.³⁷ The confidence limits by PEST provide only an indication of parameter uncertainty, as they rely on a linearity assumption that may not extend as far in the parameter space as the confidence limits themselves.³⁷ The normalized root-mean-square error (NRMSE: the lower the better), derived from the sum of squared weighted residuals,²⁴ is used as a measure of the goodness-of-fit of the model to the kinetic curves.

3. Results and discussion

3.1 Model description of experimental sorption curves

The details of the systems considered herein and the results of the data fitting, including the NRMSE values and parameter confidence intervals by PEST, are presented in Table S1.† In many cases (57 out of 109), for all types of isotherm considered, the model provided a very good fit to the kinetic data by optimizing a single parameter, namely the characteristic diffusion time, $\tau = a^2/D_{X,p}$, from which the diffusion coefficient $D_{X,p}$ was derived (see Theory). In the remaining cases, allowing the thermodynamic partitioning constant $K_{p,w}^H$, $K_{p,w}^L$ or $K_{p,w}^{L,F}$ (depending on the system) to be adjusted (together with τ) in the kinetic fitting improved the fit to the data. All the cases (with only 1 exception; see Table S1†) were fitted with $\gamma = 1$ (spherical diffusion). Because intraparticle diffusion is the limiting step in the accumulation of X ($D_{X,p} \ll D_{X,w}$), the almost exclusive applicability of spherical diffusion is in line with the size and shape of the particles considered herein, implying that the entire volume of the particle body is accessible to X (see brief discussion in Theory on this issue). The model considers the extent to which the target compound X is depleted in the bulk aqueous medium throughout the sorption process. Good fits to the experimental data were obtained even in cases where significant bulk depletion occurred. We highlight that in



Fig. 3 Equilibrium and kinetic features of a system with considerable depletion of X in the bulk solution: sorption of naphthalene on polyethylene terephthalate particles ($a = 1.5 \times 10^{-3}$ m). The panels correspond to (A) equilibrium sorption isotherm; (B) kinetic sorption curves; (C) solution depletion profile; and (D) temporal evolution of the normalized intraparticle concentration profiles, with the direction of increasing time indicated by the arrow. In (D), the timescale between two plotted concentration profiles is $\Delta t = 16\,021$ s, starting at $t = 16\,021$ s. The condition at $t = 0$ (not shown) corresponds to plastic particles free of contaminants and to the initial bulk medium condition $c_{X,w}^*(t=0) = c_{X,w}^{*0}$. The Langmuir isotherm best described the equilibrium data, and τ was the only parameter optimized to fit the sorption curves (see Table S1† for the pertaining parameters). The isotherm curve (A) shows the experimental data (black circles)⁵⁹ and the best fit obtained according to the Langmuir sorption isotherm (eqn (1)–(2b), red curve, adjusted parameters: $K_{p,w}^L$ and $c_{X,p}^{\text{max},s}$); the kinetic sorption curve (B) shows the experimental data (black circles)⁵⁹ and numerically computed values, eqn (1)–(2b), (3)–(5), (7) and (8) (red curve); and the depletion profile (C) shows the values obtained from numerical computation, eqn (1)–(2b), (3)–(5), (7) (red curve). The maximal extent of bulk depletion is 87% in the kinetic sorption data, and from the fitted τ of 2225.2 h, the derived diffusion coefficient is $D_{X,p} = 2.81 \times 10^{-13} \text{ m}^2 \text{ s}^{-1}$.



contrast to a previous study on planar polymer discs, which accounted for depletion only in the case of a linear sorption isotherm,²⁰ our approach is applicable to any type of sorption isotherm. The power and genericity of our approach are illustrated by examples for each type of isotherm considered, for cases where there is negligible or considerable depletion of X in the bulk solution, and for systems in which satisfactory fit to the kinetic data was attained by varying only τ or by concomitant variation of both τ and $K_{p,w}^{i=H,L,LF}$. In the case of systems described by the Langmuir isotherm ($i = L$), and τ the sole parameter varied in the kinetic fitting, results for the situation where bulk depletion of X is negligible (3%) are illustrated in Fig. 2, and those for considerable bulk depletion of X (87%) are shown in Fig. 3. In detail, the experimental sorption isotherms and the accumulation kinetic curves are shown together with their corresponding fits in Fig. 2A–3A and Fig. 2B–3B, respectively, while computed bulk depletion and intraparticle concentration profiles are reported as functions of time in Fig. 2C–3C and Fig. 2D–3D, respectively.

The cross-over of the intraparticle concentration profiles shown in Fig. 3D is a consequence of depletion in the bulk medium and highlights the coupling between bulk depletion kinetics and accumulation by/diffusion within the plastic particle over time. Furthermore, in the depletive case, the presence of a gradient in the intraparticle concentration profile at the longest experimental time (96 h; Fig. 3D) suggests that equilibrium was not attained, in line with the ongoing bulk depletion (Fig. 3C) and the ongoing increase in $C_{x,p}$ with time in the kinetic sorption curve (Fig. 3B).

The ESI† detailed for other contaminant/plastic particle systems has corresponding results for the linear (Henry) isotherm (non-depletive cases: $K_{p,w}^H$ obtained from the fitting of sorption isotherm is fixed for the fitting of the kinetic sorption data, Fig. S2†; $K_{p,w}^H$ is varied (together with τ) for the fitting of the kinetic sorption data, Fig. S3†; depletive cases: $K_{p,w}^H$ fixed,

Fig. S4†; $K_{p,w}^H$ varied, Fig. S5†), the Langmuir isotherm (non-depletive: $K_{p,w}^L$ varied, Fig. S6†; depletive: $K_{p,w}^L$ varied, Fig. S7†), and the Langmuir–Freundlich isotherm (non-depletive: $K_{p,w}^{LF}$ fixed, Fig. S8†; we found no examples for the case where $K_{p,w}^{LF}$ is varied, nor any depletive cases for this isotherm). Also shown is the benzophenone-3/polystyrene particles system in which, for a given particle volume fraction, the extent of bulk depletion increases with decreasing particle size (Fig. S9†).¹² In each case, the equilibrium sorption isotherm, kinetic sorption curve, temporal bulk solution depletion profile, and temporal evolution of the intraparticle concentration profiles are shown.

3.2 Derived intraparticle diffusion coefficients

To practically analyze all the data sets herein, the magnitude of the computed diffusion timescale, τ , lies in the range of 15–500 h without a clear well-defined connection to the particle radius (Fig. S10†). An illustrative example of the sorption of benzophenone-3 on a series of different-sized polystyrene particles is shown in Fig. 4. Timescales in the range of tens to hundreds of hours confirm our previous finding,²⁴ that is intraparticle diffusion is the process that controls the overall rate of the sorption process. If diffusion in the extraparticle medium towards the particle surface would be the rate limiting step in surface adsorption, then the process would occur on much faster timescales, and would result in faster kinetics being observed as the particle radius decreases (it is recalled that $D_{x,p} \ll D_{x,w}$).²⁴ Instead, although the timescale of sorption is practically independent of particle radius (Fig. 4), the thermodynamic equilibrium parameters for a given polymer and target compound are size dependent, that is, $c_{x,p}^{\max,s}$ is typically greater for smaller particle radii,^{12,58,76} which likely reflects the greater contribution of surface sorption relative to intraparticle accumulation as particle size decreases.



Fig. 4 Temporal sorption of benzophenone by polystyrene particles with a range of radii, a , showing (A) normalized, $C_{x,p}(t)/C_{x,p}^{\text{eq}}$, and (B) original data. Experimental data¹² are shown as points, and the numerically computed fits to the data are shown as dashed curves (see Table S1† for parameters used in the computations). The surface area/volume ratio is a factor of 5 greater for $a = 250$ nm *cf.* $a = 125$ μm , and the corresponding $c_{x,p}^{\max,s}$ is a factor of 1.8 greater.



The experimental volume fraction, ϕ , used in the data sets we successfully analyzed was generally less than 5×10^{-3} (Table S1†). In cases where very high particle volume fractions were used in the measurements, there is a likelihood that plastic particle aggregates will be present, whose temporal accumulation of X will necessarily differ from that of the individual dispersed particles, *i.e.* the nature of the diffusion process in aggregates changes because the effective size of the object has changed. This issue can be explored by performing computations with artificially lower volume fractions. We found no suitably documented examples to robustly illustrate this point. In one case,⁷⁷ the kinetic data (obtained at an experimental $\phi = 0.02$) were better described by an artificially lower volume fraction ($\phi = 0.006$), but the corresponding equilibrium isotherm data were obviously erroneous. Furthermore, we qualitatively expect that part of the volume fraction within particle aggregates will be inaccessible to the contaminant, resulting in an increased tendency for linear diffusion to become operational. This aspect can be investigated by comparing the fits to the data obtained for $\gamma = 1$ (spherical

diffusion) versus $\gamma = 0$ (linear diffusion) (see the Theory section). Analysis of data⁷⁸ obtained at an experimental ϕ of 0.01 provides a convincing illustration of this effect. The kinetic data are best described by linear diffusion being operational ($\gamma = 0$), Fig. S11.†

We highlight that the particle radius is not used in the fitting process. Characterization of the particle size distribution and evaluation of the colloidal stability properties of the plastic particles against aggregation are fundamental determinants of the interplay between, and the proper interpretation of, the thermodynamic and kinetic features of contaminant sorption.

The derived $D_{x,p}$ is found to be largely independent of the molar mass of the contaminant X in the range *ca.* 100 to 400 g mol⁻¹ (Fig. S12†). All the data sets analyzed herein correspond to measurements in aqueous dispersions. There are disparate literature reports on the dependence of $D_{x,p}$ on molar mass depending on the crystallinity of the polymer and its degree of hydration.^{20–23} In the case of a polystyrene disc in aqueous media, $D_{x,p}$ was found to be similar (*ca.* 3×10^{-16} m² s⁻¹) for 22 compounds with molar mass in the range 180–400 g mol⁻¹.²⁰



Fig. 5 Log–log plot of the intraparticle diffusion coefficient, $D_{x,p}$, as a function of particle radius, a . Symbols correspond to the analyzed data sets as detailed in the legend; the linear regression line through all of the data is shown as a black dashed curve. Abbreviations: PS = polystyrene; PVC = polyvinyl chloride; PLA = polylactic acid; PU = polyurethane; PP = polypropylene; PE = polyethylene; PBAT = polybutylene adipate terephthalate; PET = polyethylene terephthalate; PA = polyamide; PBS = polybutylene succinate; BTR = 1H-benzotriazole; 1-OH-BTR = 1-hydroxy-benzotriazole; STTR = 5-methyl-1H-benzotriazole; XTR = 5,6-dimethyl-1H-benzotriazole; 5-chloro-1H-BTR = 5-chloro-1H-benzotriazole; 2-OH-BTH = 2-hydroxy-benzothiazole; 2-MeS-BTH = 2-methylthio-benzothiazole; 2-NH₂-BTH = 2-amino-benzothiazole.



analyzed data sets. The convergence of the normalized kinetic sorption curves to a common master curve (Fig. 6) underscores the lack of dependence on the kinetic timescale (τ) on the particle size a , thereby evidencing the dependence of $D_{x,p}$ on a .

When data are compared at the same particle radius (or film thickness), the intraparticulate diffusion coefficients reported by others for polymer spheres and films^{20,79–85} (determined by various means),^{80,86–88} and those derived *via* our previous explicit separation and coupling of the transient and steady-state processes,²⁴ are of a comparable order of magnitude as those determined herein (Fig. S16†). Any differences reflect the assumptions made in the derivation of the $D_{x,p}$ values with regard to the pertaining spatial scale and the way in which the transient and steady-state processes are treated. We highlight that the numerical approach presented herein is the most rigorous and fundamental physicochemical model of the processes involved.

These remarkable results suggest that the diverse plastic particles considered in the analysis share similar structural properties. More explicitly, because diffusion occurs almost exclusively within the amorphous polymer zones,^{89,90} our findings imply that the size and distribution of the crystalline phase as well as the relative proportions of the crystalline and amorphous zones are similar across polymer types over the pertaining particle size range. The decrease in $D_{x,p}$ with decreasing particle radius implies a concomitant increase in polymer crystallinity, which is in line with literature reports; for example, polypropylene nanospheres exhibit 76% crystallinity, while microspheres exhibit 59% crystallinity.⁹¹ The greater scatter in the data for particle radii greater than 10 μm (Fig. 5) is in part a consequence of the greater amount of data available in this size range but may also reflect differences in the relative

amounts and distribution of the crystalline and amorphous phases in larger particle bodies and across polymer types.

In support of our findings, there is a body of literature showing that for polymer thin films, $D_{x,p}$ decreases with decreasing film thickness,^{80,92–100} and for spherical particles, there is a report of $D_{x,p}$ decreasing with decreasing particle radius.⁸⁰ In the case of thin plastic films, the decrease in $D_{x,p}$ with decreasing film thickness has been ascribed variously to an increasing density of the polymer chains in progressively thinner films,¹⁰¹ or the film thickness dependence of the distribution, orientation and size of the crystalline zones in the polymer matrix,^{96,98} or a reduction in the accessibility of the polymer free volume with decreasing film thickness.¹⁰² It is noteworthy that for the penetration of solvents into a dry polymer, a plot of $\log(D_{x,p})$ as a function of $\log(\text{polymer film thickness})$ has a slope of approximately 2.⁹⁷ In the case of spherical geometry, scrutiny of particles synthesized with a given size *versus* those generated by crushing of larger items might give insight into the potential relevance of factors, such as size-dependent polymer crystallinity. However, we could not find sufficient data to draw conclusions: the majority of the data we analyzed correspond to particles that were synthesized with a given size; the few cases where particles were generated by crushing of larger objects fall in a narrow size range (37 μm to 125 μm),^{40,43,57,62,63} and the derived $D_{x,p}$ values lie in the same range as those derived from non-crushed particles (Fig. 5).

The remarkable universal law that we have established enables the prediction of the sorption and release kinetics and intraparticulate diffusion of any compound in any type of polymeric particle as a function of particle size. It follows that, for the typical case of distributed particle sizes, the corresponding diffusion coefficient distribution and characteristic diffusion timescale distribution can be computed. With regard

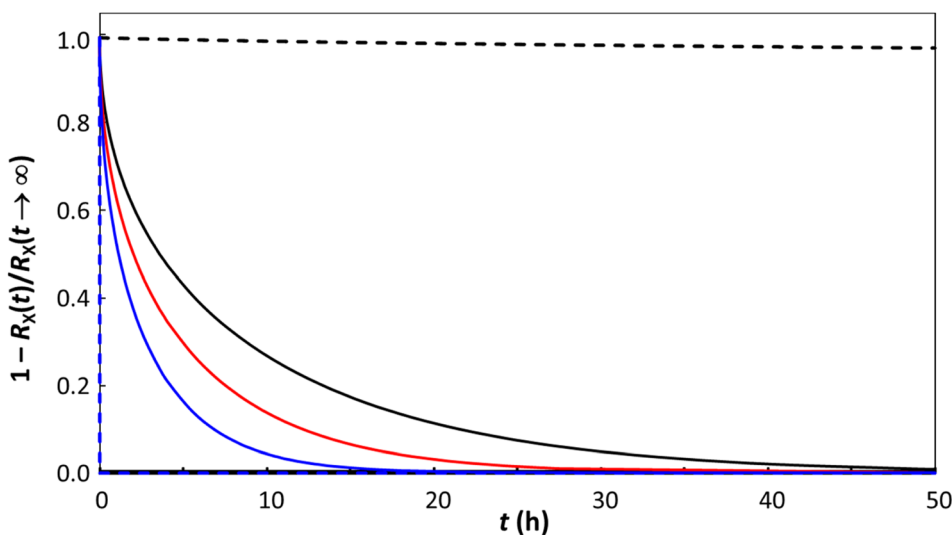


Fig. 7 Time evolution of the release, R_x , of compound X from spherical plastic particles. The curves were computed using eqn (11). Solid curves show the results for the herein identified particle size dependence of $D_{x,p}$ (obtained from the line of best fit through the data shown in Fig. 5) corresponding to (i) $a = 10^{-4}$ m, $D_{x,p} = 2.36 \times 10^{-14}$ m² s⁻¹, black solid curve; (ii) $a = 10^{-6}$ m, $D_{x,p} = 4.19 \times 10^{-18}$ m² s⁻¹, red solid curve; and (iii) $a = 10^{-8}$ m, $D_{x,p} = 7.46 \times 10^{-22}$ m² s⁻¹, blue solid curve. Dashed curves show the results for $D_{x,p}$ fixed at 4.19×10^{-18} m² s⁻¹ for $a = 10^{-4}$ m (black dashed curve) and $a = 10^{-8}$ m (blue dashed curve).



to contaminant release kinetics, our previous work,^{103,104} which assumed that $D_{X,p}$ is invariant with particle size, predicted that contaminants are released faster as the size of the plastic particles decreases, in line with the trends reported in the literature.^{105,106} The striking particle size dependence of $D_{X,p}$ identified herein provides a moderated view of the particle size dependence of contaminant release rates. Using the particle size dependence of $D_{X,p}$ (Fig. 5), the release rate of X from a spherical particle (eqn (11)) is indeed predicted to increase with decreasing particle size albeit less drastically than would be the case if $D_{X,p}$ is independent of particle size (Fig. 7).

4. Conclusions

The theory presented herein and applied to the analysis of contaminant sorption kinetics by plastic particles offers a flexible and comprehensive approach that goes well beyond the traditional empirical pseudo first or second order kinetic equations. We tentatively propose that the observed decrease in the intraparticulate diffusion coefficient with decreasing particle size is related to relative increases in the proportions of the crystalline zones (as well as their size and distribution) compared to the amorphous zones in smaller particles. Although, owing to the availability of sufficient experimental data, we have considered (approximately) spherical particles, we highlight that the theory is generically applicable to any type of particle (fibre, film, etc.), with proper accounting for the geometry involved in the flux expressions. Our approach provides dynamic level considerations relevant to environmental risk assessment, e.g. predicting the chemical speciation and bioavailability of contaminants associated with plastic particles, and human health, e.g. optimization of polymeric drug delivery systems and assessment of the migration of compounds in/out of plastic medical devices and food contact materials. Future work will use various strategies^{107,108} to extend the theory and numerical interpretative scheme to describe additional environmentally relevant scenarios, including (i) the impacts of contaminant speciation, i.e. chemical kinetic terms with the associated possibility for diffusional transport limitation in the extraparticulate phase (which may be of particular importance in soil and sediment matrices); (ii) the impact of (fully relaxed) force field interactions, while still including the fundamental transient features of the diffusional transport; (iii) time-dependent diffusional processes due to, for example, the build-up of a restricting layer of the accumulated contaminant itself,¹⁰⁹ or aggregation concomitant with sorption; and (iv) modification of the pristine polymer interfacial zone due to e.g. the presence of biofilms.

Data availability

The data supporting this article have been included as part of the ESI.†

Conflicts of interest

There are no conflicts to declare.

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