

Cite this: *Nanoscale*, 2021, 13, 17504

## Dual-site electrocatalytic nitrate reduction to ammonia on oxygen vacancy-enriched and Pd-decorated MnO<sub>2</sub> nanosheets†

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Electrocatalytic nitrate reduction (NRR) represents one promising alternative to the Haber–Bosch process for NH<sub>3</sub> production due to the lower reaction energy barrier compared to N<sub>2</sub> reduction and the potential recycling of nitrogen source from nitrate wastewater. The metal oxides with oxygen vacancy (O<sub>v</sub>) display high NH<sub>3</sub> selectivities in NRR (NO<sub>2</sub><sup>−</sup>/N<sub>2</sub> as side products), but the complexity in O<sub>v</sub> enrichment and the inferior hydrogen adsorption on oxides make NRR an inefficient process. Herein, one superior dual-site NRR electrocatalyst that is composed of O<sub>v</sub>-enriched MnO<sub>2</sub> nanosheets (MnO<sub>2</sub>-O<sub>v</sub>) and Pd nanoparticles (deposited on MnO<sub>2</sub>) is constructed over the three-dimensional porous nickel foam (Pd-MnO<sub>2</sub>-O<sub>v</sub>/Ni foam). In a continuous-flow reaction cell, this electrode delivers a NO<sub>3</sub><sup>−</sup>-N conversion rate of 642 mg N m<sup>−2</sup><sub>electrode</sub> h<sup>−1</sup> and a NH<sub>3</sub> selectivity of 87.64% at −0.85 V vs. Ag/AgCl when feeding 22.5 mg L<sup>−1</sup> of NO<sub>3</sub><sup>−</sup>-N (0.875 mL min<sup>−1</sup>), outperforming the Pd/Ni foam (369 mg N m<sup>−2</sup><sub>electrode</sub> h<sup>−1</sup>, 85.02%) and MnO<sub>2</sub>-O<sub>v</sub>/Ni foam (118 mg N m<sup>−2</sup><sub>electrode</sub> h<sup>−1</sup>, 32.25%). Increasing the feeding NO<sub>3</sub><sup>−</sup>-N concentration and flow rate to 180.0 mg L<sup>−1</sup> and 2.81 mL min<sup>−1</sup> can further lift the conversion rate to 1933 and 1171 mg N m<sup>−2</sup><sub>electrode</sub> h<sup>−1</sup>, respectively. The combination of experimental characterizations and theoretical calculations reveal that the MnO<sub>2</sub>-O<sub>v</sub> adsorbs, immobilizes, and activates the NO<sub>3</sub><sup>−</sup> and N-intermediates, while the Pd supplies the O<sub>v</sub> sites with sufficient adsorbed hydrogen (H\*) for both the NRR and O<sub>v</sub> refreshment. Our work presents a good example of utilizing dual-site catalysis in the highly selective conversion of NO<sub>3</sub><sup>−</sup> to NH<sub>3</sub> that is important for nitrate pollution abatement, nitrogen resource recycling, as well as sustainable NH<sub>3</sub> production.

 Received 30th July 2021,  
Accepted 1st October 2021  
DOI: 10.1039/d1nr04962c

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## 1. Introduction

Ammonia (NH<sub>3</sub>) is one important raw chemical with huge demand in the fertilizer, polymer, pharmaceutical, and explosive industries.<sup>1</sup> It is also a carbon-free hydrogen carrier that shows promise as a substituent for H<sub>2</sub> fuel in the upcoming renewable energy era.<sup>2</sup> Currently, the industrial production of NH<sub>3</sub> relies on the Haber–Bosch process that proceeds by the reaction of N<sub>2</sub> and H<sub>2</sub> under high temperatures (500 °C) and pressures (>150 bar).<sup>3</sup> Albeit the considerable yield, this process with the harsh reaction condition is considered to be unsustainable in the context of energy saving and environ-

mental protection. Photo-/electrocatalytic N<sub>2</sub> fixation with H<sub>2</sub>O as the hydrogen source offers a green and sustainable way for NH<sub>3</sub> production, but the yield is far from satisfying due to the chemical inertness of N<sub>2</sub> (the triple bond energy reaches 940.95 kJ mol<sup>−1</sup>).<sup>4–6</sup> Recently, a novel route for NH<sub>3</sub> production by electrocatalytic nitrate reduction (NRR) is proposed.<sup>7,8</sup> This route is considered promising as (i) the nitrate reduction to NH<sub>3</sub> is more energy-efficient compared to N<sub>2</sub> reduction,<sup>9</sup> and (ii) potential recycling of the nitrogen source from environmental pollutants, such as the NO<sub>x</sub> (one gaseous pollutant that can be readily oxidized to nitrate)<sup>6</sup> and nitrite/nitrate in wastewater.<sup>10–12</sup> The catalyst is the core of the NRR system, determining both the kinetics and the product selectivity towards NH<sub>3</sub> rather than NO<sub>2</sub><sup>−</sup>, N<sub>2</sub>, or N<sub>2</sub>O.<sup>13,14</sup> Among the tested catalysts, the transition metal oxides (such as CuO, FeO<sub>x</sub>, and TiO<sub>2</sub>) are gaining intensive attention due to their impressive NRR performances.<sup>15–17</sup> Some researchers evidenced that these oxides were partially reduced during NRR, forming oxygen vacancies (O<sub>v</sub>) at the surface coupled with the low-valent metal ions (*e.g.* Cu<sup>+</sup> in CuO-O<sub>v</sub>, Ti<sup>3+</sup> in TiO<sub>2</sub>-O<sub>v</sub>).<sup>15,16</sup> They then proposed from theoretical calculations that NO<sub>3</sub><sup>−</sup> was highly inclined to be harvested

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†Electronic supplementary information (ESI) available. See DOI: 10.1039/d1nr04962c

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and immobilized at the  $O_v$  site with its oxygen atom filling in the vacancy, which restrained the migration of N-intermediates and their coupling to form  $N_2$  or  $N_2O$ . Furthermore, such an adsorption model enabled the activation of N–O bonds, promoting  $NO_3^-$  conversion.<sup>18</sup>

Albeit the unique role of  $O_v$  in NRR has been unveiled, its function is far from being fully exploited. Two aspects can be further improved: (i)  $O_v$  enrichment in the oxide ( $MO_x$ ). The formation of  $O_v$  requires the metal M of two or more oxidative valences (e.g.,  $Ti^{3+}/Ti^{4+}$  in  $TiO_2-O_v$  and  $Cu^+/Cu^{2+}$  in  $CuO-O_v$ ). In general,  $O_v$  in  $MO_x$  can be readily enriched when M binds with more oxygen (i.e., a larger value of  $x$ ) in the initial fine oxide, owns more accessible oxidative valences, and can be reduced to the low valence under the NRR conditions.<sup>19,20</sup> The Mn in  $MnO_2$  has a valence of +4, and can be readily reduced to +2/+3 due to the corresponding positive redox potential (Table S1†). In this case, we believe more  $O_v$  can be readily formed in  $MnO_2$ , and the resultant  $MnO_2-O_v$  is expected to afford a better NRR performance.<sup>21</sup> (ii) Sufficient supply of hydrogen ( $H^*$ ) for NRR and  $O_v$  refreshment. The  $NH_3$  formation requires the  $H^*$  to combine with N-intermediates, while the  $O_v$  refreshment also requires the  $H^*$  to remove the oxygen/nitrogen species that fill the  $O_v$  during NRR. In general, the oxide is inferior in  $H^*$  adsorption,<sup>22,23</sup> and a more negative potential has to be employed to polarize the catalyst, which not only raises the energy consumption but also challenges the electrode stability (e.g.,  $-1.3$  V vs. SCE for  $FeNiO_x-O_v$ <sup>15</sup> and  $-1.6$  V vs. SCE for  $TiO_2-O_v$ <sup>17</sup>). The metallic palladium (Pd) is known as an excellent material for  $H$  adsorption.<sup>24,25</sup> We, therefore, propose that the coupling of the oxygen-deficient oxide and Pd can perform as one robust dual-site NRR electrocatalyst with high  $NH_3$  selectivity, in which the  $O_v$  serves to harvest, immobilize, and activate the  $NO_3^-$ , while the Pd supplies the  $O_v$  site with sufficient  $H^*$  from the aqueous solution. The dual-site catalysis has collected much success in heterogeneous catalytic reaction, but never reported in NRR.<sup>26–28</sup>

To confirm our hypothesis, a novel dual-site electrocatalyst that is composed of  $O_v$ -enriched  $MnO_2$  nanosheets ( $MnO_2-O_v$ ) and Pd nanoparticles (deposited on  $MnO_2$ ) was constructed over the three-dimensional porous nickel foam (Pd- $MnO_2-O_v$ /Ni foam). Its NRR performances, including the  $NO_3^-$ -N conversion rate,  $NH_3$ -N selectivity, and faradaic current efficiency, were tested in a continuous flow reactor and compared with those of Pd/Ni foam and  $MnO_2-O_v$ /Ni foam. Impacts of the  $NO_3^-$ -N feeding concentration, flow rate, solution pH, Pd loading mass, coexisting anions, and dissolved organic organisms on the NRR performances of Pd- $MnO_2-O_v$ /Ni foam were also investigated. Finally, how the dual sites work in the selective conversion of  $NO_3^-$  to  $NH_3$  is discussed with the aid of density functional theory (DFT) calculations.

## 2. Experimental methods

### 2.1. Materials

Analytical grade sodium nitrate ( $NaNO_3$ ), sodium nitrite ( $NaNO_2$ ), sodium sulfate ( $Na_2SO_4$ ), ammonium sulfate

( $(NH_4)_2SO_4$ ), anhydrous ethanol, sodium chloride (NaCl), humic acid, sodium hydroxide, hydrochloric acid, titanium trichloride ( $TiCl_3$ ), potassium bromide (KBr), potassium bromate ( $KBrO_3$ ), sulfamic acid ( $NH_2SO_3H$ ), sodium carbonate ( $Na_2CO_3$ ), sodium tetrachloropalladium ( $Na_2PdCl_4$ ), sodium sulfite ( $Na_2SO_3$ ), and potassium permanganate ( $KMnO_4$ ) were obtained from the Sinopharm group chemical reagent Co., Ltd, China. The 3D porous Ni foam substrate (110 pores per linear inch, surface density:  $380$  g  $m^{-2}$ , thickness: 0.5 mm) was provided by Kunshan Tengerhui Electronic Technology Co., Ltd, China.

### 2.2. Synthesis of the electrode

For the synthesis of Pd- $MnO_2-O_v$ /Ni foam electrode, a Ni foam piece with a size of  $35$  mm  $\times$   $35$  mm  $\times$   $0.5$  mm and pre-cleaned by ethanol was placed in a Teflon-lined stainless-steel autoclave that contains 40 mL of  $KMnO_4$  aqueous solution (1.5 mM). The mixture was kept in an oven at  $160$  °C for 24 h to induce the growth of  $MnO_2$  on the Ni foam. Once being washed with de-ionized water at room temperature, the as-prepared  $MnO_2$ /Ni foam was subjected to a reduction current ( $-8.0$  mA) in 10 mM of NaCl solution for 20 min to enrich the  $O_v$  on  $MnO_2$  ( $MnO_2-O_v$ /Ni foam, and the plotting of working potential versus reduction time can be seen in Fig. S1†). The as-synthesized  $MnO_2-O_v$ /Ni foam was then immediately immersed in a  $Na_2PdCl_4$  solution (1.0 mM, 100 mL) for 4.0 h to deposit Pd on the  $MnO_2-O_v$  sheet. In comparison, the cleaned Ni foam with pre-reduction at  $-8.0$  mA for 20 min was immersed in  $Na_2PdCl_4$  solution (1.0 mM, 100 mL) for 4.0 h to produce the Pd/Ni foam.

### 2.3. NRR test

A sealed continuous-flow reaction cell with separated cathode and anode chambers by a cation-exchange membrane was customized for the NRR test. Two working electrodes (32 mm in diameter) were placed in the cathode chamber with a distance of 1.0 cm, and their working potentials were referred to the same Ag/AgCl wire (3.0 M KCl, 0.201 V vs. standard hydrogen electrode at 25 °C). One Pt foil was placed in the anode chamber as the counter electrode. The argon-saturated influent with 50 mM of  $Na_2SO_4$  and a certain amount of  $NO_3^-$ -N was pumped to the cathode chamber, and the NRR occurred when the effluent penetrated the working electrode. The feed in the anode chamber was only the argon-saturated 50 mM  $Na_2SO_4$  solution, and the oxygen evolution reaction occurred on the Pt foil. The concentrations (mg N  $mL^{-1}$ ) of  $NO_3^-$ -N ( $C_{NO_3^-N}$ ),  $NO_2^-$ -N ( $C_{NO_2^-N}$ ), and  $NH_3$ -N ( $C_{NH_3-N}$ ), in the inlet and outlet flow of the cathode chamber were quantified to calculate the  $NO_3^-$ -N conversion efficiency ( $\eta$ , 100%) and rate ( $r$ , mg N  $m^{-2}$   $_{electrode}$   $h^{-1}$ ), the product distribution (the decreased total N mass in solution after NRR is attributed to the escape of N in terms of  $N_2$ <sup>15,29</sup>),  $NH_3$ -N selectivity ( $S_{NH_3-N}$ , 100%), and the faradaic current efficiency (FE%, 100%):

$$\eta_{NO_3^-N} = (C_{in,NO_3^-N} - C_{out,NO_3^-N}) / C_{in,NO_3^-N} \times 100\% \quad (1)$$

$$r_{NO_3^-N} = (C_{in,NO_3^-N} - C_{out,NO_3^-N}) \times Q/A \times 60 \quad (2)$$

$$S_{\text{NH}_3^-} = C_{\text{out,NH}_3^-} / (C_{\text{in,NO}_3^-} - C_{\text{out,NO}_3^-}) \times 100 \quad (3)$$

$$\text{FE}\% = (n_1 \times C_{\text{out,NO}_2^-} + n_2 \times C_{\text{out,NH}_3^-} + n_3 \times C_{\text{out,N}_2^-}) \times Q \times F / (M \times I) \times 10 \quad (4)$$

$$C_{\text{out,N}_2^-} = (C_{\text{in,NO}_3^-} - C_{\text{out,NO}_3^-} - C_{\text{out,NO}_2^-} - C_{\text{out,NH}_3^-}) / 2 \quad (5)$$

where  $Q$ ,  $F$ ,  $M$ ,  $A$ , and  $I$  refer to the flowing rate of the influent ( $\text{mL min}^{-1}$ ), Faraday constant ( $96\,500 \text{ C mol}^{-1}$ ), molar mass of the element  $N$  ( $14\,000 \text{ mg mol}^{-1}$ ), geometric surface area of the electrode ( $\text{m}^2$ ), and current (A), respectively.  $n$  refers to the number of electrons transferred in the conversion of  $\text{NO}_3^-$ -N to the corresponding nitrogen species (2, 5, and 8 for  $\text{NO}_2^-$ -N,  $\text{N}_2$ -N, and  $\text{NH}_3$ -N, respectively).

#### 2.4. DFT calculation

Spin-polarized density functional theory (DFT) calculations were carried out by the Perdew–Burke–Ernzerhof (PBE) functional within generalized gradient approximation (GGA), using the Vienna *ab initio* Simulation Package (VASP 5.4.1).<sup>30–32</sup> The kinetic energy cut off was set at 400 eV. The (111) facet-terminated  $2 \times 2$  supercell containing 48 Pd atoms and the (001) facet-terminated supercell containing 136 atoms (including 32 Mn, 76 O, 4 K, and 24 H) were constructed to model Pd and  $\delta\text{-MnO}_2$ , respectively. One oxygen atom was removed from the outermost layer of the  $\delta\text{-MnO}_2$  (001) facet to generate  $\text{MnO}_2\text{-O}_v$ . The vacuum space along the  $z$  direction was set to 15 Å, avoiding the interactions between two slab models. One layer at the bottom was fixed at the lattice position, while the remaining atomic layers and the adsorbed molecules were fully relaxed. Brillouin zone integrations were performed using Monkhorst–Pack grids of  $3 \times 3 \times 1$  for all the slab calculations with Gaussian smearing  $\sigma = 0.1 \text{ eV}$ . All the structural optimizations were converged at  $0.05 \text{ eV \AA}^{-1}$ . The solvation effect was precluded since the ignorable energy change was witnessed.<sup>33,34</sup> Grimme's DFT-D3 method was incorporated to implement the van der Waals correction.<sup>35</sup>

The adsorption energy ( $E_{\text{ads}}$ ) is defined as

$$E_{\text{ads}} = E_{\text{tot}} - (E_{\text{sub}} + E_{\text{mol}}) \quad (6)$$

where  $E_{\text{tot}}$ ,  $E_{\text{sub}}$ , and  $E_{\text{mol}}$  depict the total energy of the adsorption complex, the substrate, and the isolated adsorbed molecules, respectively.

The free energies in the electrochemical reaction pathways were calculated based on the computational hydrogen electrode (CHE) model proposed by Nørskov and co-workers. The change in the Gibbs free energy ( $\Delta G$ ) for each reaction step is given as follows:<sup>36</sup>

$$\Delta G = \Delta E + \Delta \text{ZPE} - T\Delta S + \Delta U + \Delta \text{pH} \quad (7)$$

where  $\Delta E$  is the energy change between the reactant and product obtained from DFT calculations.  $\Delta \text{ZPE}$  is the change in zero-point energy, and  $T$  and  $\Delta S$  denote the temperature and change of entropy, respectively. Here,  $T = 298 \text{ K}$  was considered.  $\Delta \text{pH}$  is the free energy correction of pH, calculated by

$\Delta \text{pH} = kT \ln 10 \times \text{pH}$ , and the pH value is zero in this work. Additionally, the Gibbs free-energy diagrams were estimated under zero potential ( $U = 0$ ).

## 3. Results and discussion

### 3.1. Synthesis and characterization of the Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam electrode

The Pd/MnO<sub>2</sub>-O<sub>v</sub> nanosheets grown on the 3D-porous Ni foam were synthesized *via* a three-step approach: (i) growth of the uniform MnO<sub>2</sub> sheet array on the skeleton of Ni foam (MnO<sub>2</sub>/Ni foam); (ii) enrichment of O<sub>v</sub> on MnO<sub>2</sub> nanosheets *via* an electrochemical reduction method (MnO<sub>2</sub>-O<sub>v</sub>/Ni foam); (iii) further decoration of Pd NPs (Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam). Fig. 1a–d present the representative SEM images of Ni foam, MnO<sub>2</sub>/Ni foam, MnO<sub>2</sub>-O<sub>v</sub>/Ni foam, and Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam. As observed, MnO<sub>2</sub> grows on the smooth skeleton surface of Ni foam and displays a unique intersecting ribbon-like sheet structure. This structure is well preserved during the O<sub>v</sub> construction and Pd NP decoration. The Pd NPs are evenly deposited at the sheet surface with little agglomeration. The EDS elemental mapping results in Fig. 1e further demonstrate the even distribution of Pd, Mn, O, and Ni on the skeleton of Ni foam. In Fig. 1f, the HRTEM image of the Pd–MnO<sub>2</sub>-O<sub>v</sub> sheet



**Fig. 1** Representative SEM images of (a) Ni foam, (b) MnO<sub>2</sub>/Ni foam, (c) MnO<sub>2</sub>-O<sub>v</sub>/Ni foam, and (d) Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam; (e) EDS elemental mapping of Pd, Mn, O, and Ni for Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam; (f) TEM image of Pd/MnO<sub>2</sub>-O<sub>v</sub> nanosheet (inset is the corresponding HRTEM image); (g) XRD patterns of electrodes; (h) EPR spectra and (i) high-resolution O 1s XPS spectra for different electrodes.

that is scraped from the Ni foam further evidences the intense and even deposition of Pd NPs with a mean size of 1.4 nm on the MnO<sub>2</sub> nanosheet (the NPs display clear lattice fringes with a consistent spacing of 0.238 nm, corresponding to the (111) facet of metallic Pd phase).<sup>37</sup> As a comparison, Pd NPs were also deposited over the Ni foam (Pd/Ni foam). The SEM image in Fig. S2a† evidences the larger and aggregated Pd particles (~20 nm) as well as some Ni(OH)<sub>2</sub> nanosheet assemblies. This structure is also verified by the TEM image of the particle that was scraped from the Pd/Ni foam (Fig. S2b†).

The XRD patterns of the MnO<sub>2</sub>/Ni foam, Pd/Ni foam, and Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam in Fig. 1g point to the δ-form of MnO<sub>2</sub> (PDFcard #80-1098) and the metallic crystal phase of Pd (PDFcard #05-0681) in all these samples.<sup>38,39</sup> No Ni(OH)<sub>2</sub> phase is discerned possibly due to its low content. The characteristic diffraction peaks for MnO<sub>2</sub> become inconspicuous in the Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam, possibly due to the crystallinity reduction of MnO<sub>2</sub> after the O<sub>v</sub> introduction or the dense cover of Pd NPs. The ICP analyses reveal that the Pd mass loading on Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam and Pd/Ni foam are similar at 1.6 mg cm<sup>-3</sup>. The presence of O<sub>v</sub> in the MnO<sub>2</sub>-O<sub>v</sub>/Ni foam, Pd/Ni foam, and Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam are evidenced by the strong EPR signal at around *g* = 2.0037 in their spectra (Fig. 1h) as well as the O 1s XPS peak at 530.4 eV (Fig. 1i).<sup>40</sup> The presence of O<sub>v</sub> on Pd/Ni foam can be ascribed to the involvement of the Ni(OH)<sub>2</sub> species. Fig. 1i also shows that the Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam carries a larger number of O<sub>v</sub> than the Pd/Ni foam (35.25% vs. 26.75%), consistent with our speculation that O<sub>v</sub> is more readily formed on MnO<sub>2</sub>.

### 3.2. NRR performance

The NRR performances of Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam, Pd/Ni foam, and MnO<sub>2</sub>-O<sub>v</sub>/Ni foam electrodes were tested and compared. Given the inherent 3D porous structure of the foam, a continuous-flow reaction cell was customized with the effluent penetrating the electrode, as schemed in Fig. 2a, which allows sufficient mass transfer of NO<sub>3</sub><sup>-</sup>-N around the active sites. Two parallel working electrodes with a distance of 1.0 cm were set to enhance the NRR. Fig. 2b plots the *C*/*C*<sub>0</sub> of NO<sub>3</sub><sup>-</sup>-N in the effluent as a function of electrolysis time under a working potential of -0.85 V, a flow rate of 0.875 mL min<sup>-1</sup>, and a feeding NO<sub>3</sub><sup>-</sup>-N concentration of 22.5 mg L<sup>-1</sup>, by which the NO<sub>3</sub><sup>-</sup>-N conversion efficiency and the rate at the steady state for the electrode can be calculated. As observed, the Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam affords both the largest NO<sub>3</sub><sup>-</sup>-N conversion efficiency of 90.61% and conversion rate of 642 mg N m<sup>-2</sup><sub>electrode</sub> h<sup>-1</sup>, of which the conversion rate is almost 1.7 and 5.7 times that of the Pd/Ni foam (369 mg N m<sup>-2</sup><sub>electrode</sub> h<sup>-1</sup>) and Pd-free MnO<sub>2</sub>-O<sub>v</sub>/Ni foam (118 mg N m<sup>-2</sup><sub>electrode</sub> h<sup>-1</sup>), respectively. As shown by the product distribution in Fig. 2c, NH<sub>3</sub>-N is the leading product on both the Pd/Ni foam and Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam electrode with a selectivity of 85.02% and 87.64%, respectively, while only a negligible amount of NO<sub>2</sub><sup>-</sup>-N is tracked (3.72 and 0.25% in product). However, on MnO<sub>2</sub>-O<sub>v</sub>/Ni foam, only 34.5% of the NO<sub>3</sub><sup>-</sup> is converted to NH<sub>3</sub> (another 30.2% to NO<sub>2</sub><sup>-</sup> and the rest to N<sub>2</sub>), which confirms the critical role of Pd in the

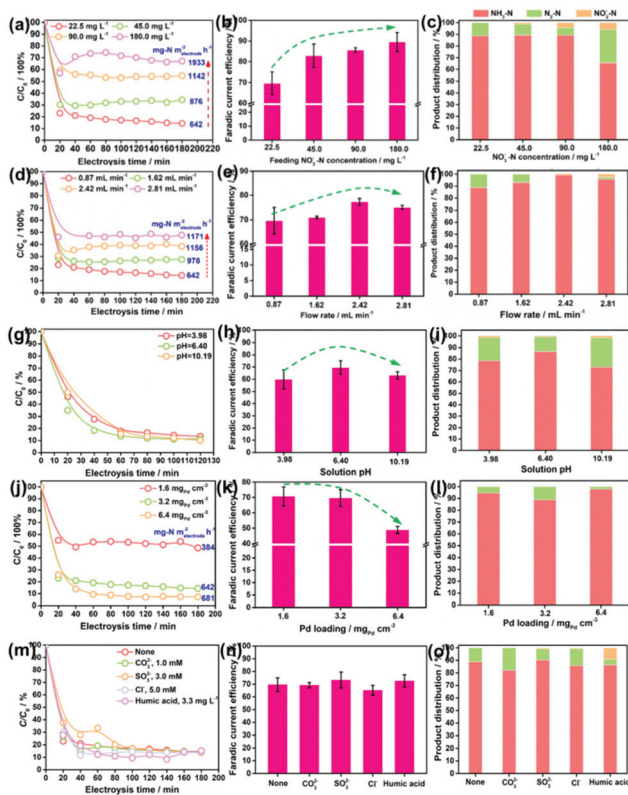


**Fig. 2** (a) Schematic description of the sealed continuous-flow reaction cell; (b) plots of *C*/*C*<sub>0</sub> as a function of the reaction time; (c) product distribution in the outlet flow at the steady state (note that the present product distribution is an average of the ones determined during the 480 min of NRR in at least three repeated tests, the same below); (d) faradaic current efficiency for the NRR on MnO<sub>2</sub>-O<sub>v</sub>/Ni foam, Pd/Ni foam, and Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam.

fast and deep reduction of NO<sub>3</sub><sup>-</sup> to NH<sub>3</sub>. Here, the NH<sub>3</sub> is believed to originate from the NO<sub>3</sub><sup>-</sup> conversion rather than the N<sub>2</sub> reduction or other impurities in the water as no NH<sub>3</sub> is detected once the NO<sub>3</sub><sup>-</sup>-free solution is fed in the flow. Fig. 2d shows that the faradaic current efficiencies for all three electrodes are smaller than 100% due to the side hydrogen evolution reaction (HER). However, the values for the Pd/Ni foam and Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam electrodes are relatively high, approaching 70%.

Impacts of the feeding NO<sub>3</sub><sup>-</sup>-N concentration, the flowing rate, the solution pH, and the Pd loading on the NRR performances of the Pd–MnO<sub>2</sub>-O<sub>v</sub>/Ni foam electrode were investigated. Fig. 3a evidences the decrease in the NO<sub>3</sub><sup>-</sup>-N conversion efficiency from 87.06% to 32.87% while the increase in the conversion rate from 642 to 1933 mg N m<sup>-2</sup><sub>electrode</sub> h<sup>-1</sup> with the feeding NO<sub>3</sub><sup>-</sup>-N concentration rising from 22.5 to 180.0 mg L<sup>-1</sup>. Fig. 3b shows that the faradaic current efficiency keeps growing with the increment in NO<sub>3</sub><sup>-</sup>-N concentration and reaches the peak of 89.5% by feeding 180 mg L<sup>-1</sup> NO<sub>3</sub><sup>-</sup>-N. It is therefore suggested that the active sites are more specific to the NRR over HER with more NO<sub>3</sub><sup>-</sup>-N supplied. The NH<sub>3</sub> selectivity is kept at a high value of around 90% with 22.5–90.0 mg L<sup>-1</sup> NO<sub>3</sub><sup>-</sup>-N in the influent (Fig. 3c), while it sharply drops to 55.45% with 180.0 mg L<sup>-1</sup> NO<sub>3</sub><sup>-</sup>-N. Correspondingly, the N<sub>2</sub> yield rises. According to the previous work, the decreased NH<sub>3</sub> yield and the enhanced N<sub>2</sub> formation can be attributed to the enlarged N-intermediate/H\* (N/H) ratio on catalyst surface when feeding a larger concentration of NO<sub>3</sub><sup>-</sup>-N.<sup>41,42</sup>

Fig. 3d reveals that an increase in the flow rate from 0.87 to 2.81 mL min<sup>-1</sup> reduces the NO<sub>3</sub><sup>-</sup>-N removal efficiency from 87.06% to 52.02%, but raises the NO<sub>3</sub><sup>-</sup>-N conversion rate from 642 to 1171 mg N m<sup>-2</sup><sub>electrode</sub> h<sup>-1</sup>. This is rationalized by the



**Fig. 3** Impacts of (a–c) the feeding  $\text{NO}_3^-$ -N concentration, (d–f) flow rate, (g–i) pH, (j–l) Pd loading, and (m–o) co-existing anions and dissolved organics on the  $\text{NO}_3^-$ -N conversion rate, faradaic current efficiency, and product distribution in NRR.

fact that under the larger flow rate, more  $\text{NO}_3^-$  pass by the electrode but stay in a shorter time. Accordingly, a larger proportion of  $\text{NO}_3^-$  incline to flow through the electrode before being reduced, leading to the increased  $\text{NO}_3^-$  residues in the effluent. Despite these, the absolute amount of the converted  $\text{NO}_3^-$ -N is increased as the active sites are feed with more  $\text{NO}_3^-$ -N under the larger flow rate. Fig. 3e and f show that with the increase in flow rate, both the faradaic current efficiency and the  $\text{NH}_3$  selectivity in the product grow, reach the peak at  $2.42 \text{ mL min}^{-1}$  and then decrease. Some  $\text{NO}_2^-$ -N is even detected at  $2.81 \text{ mL min}^{-1}$ . Therefore, it is suggested that the uplift of the flow rate but in a suitable range is conducive to acquire pure  $\text{NH}_3$ -N.

Fig. 3g shows that the solution pH has little effect on both the  $\text{NO}_3^-$ -N conversion efficiency and rate of the electrode. This is beyond expectation as many previous reports have demonstrated that an acidic condition is beneficial to NRR by affording sufficient protons and alleviating the potential poisoning of active sites (e.g.,  $\text{O}_v$  and the Pd sites) by  $\text{OH}^-$ . This inconsistency might be attributed to the overdose of active sites on the electrode when subjected to the low  $\text{NO}_3^-$ -N load, which dilutes the effect of pH. Fig. 3h and i demonstrate that the faradaic current efficiency and the  $\text{NH}_3$  selectivity are maximized at nearly neutral conditions. As observed in Fig. 3i, the

drop in  $\text{NH}_3$  selectivity primarily originates from the increased  $\text{N}_2$  yield. The enhanced  $\text{N}_2$  production in the acidic condition can be ascribed to the formation of  $\text{HNO}_{3(\text{aq})}$  that readily accumulates and is reduced on the catalyst in comparison to  $\text{NO}_3^-$ ,<sup>43</sup> which contributes to increasing the N/H ratio on electrode, promoting  $\text{N}_2$  formation. The enhanced  $\text{N}_2$  production in the alkaline condition can be attributed to the intensified poisoning of  $\text{O}_v$  by  $\text{OH}^-$  (Fig. S3†). As a result, the NRR primarily occurs on Pd, which, as we know, is one excellent metal to trigger the  $\text{N}_2$  formation.<sup>44</sup>

Fig. 3j reveals that an increment in the Pd loading boosts the  $\text{NO}_3^-$ -N conversion on the electrode under a  $\text{NO}_3^-$ -N feeding concentration of  $22.5 \text{ mg L}^{-1}$ , which further confirms the critical role of Pd in  $\text{NO}_3^-$ -N conversion. Fig. 3k shows that faradaic current efficiency decreases under a larger Pd loading, which results from the enhanced side HER that wastes more electrons. Fig. 3l shows that the moderate Pd loading of  $3.2 \text{ mg}_{\text{Pd}} \text{ cm}^{-3}$  gives rise to the poorest  $\text{NH}_3$  selectivity. As Pd occupies the  $\text{O}_v$  sites during the deposition process, we attribute the higher  $\text{NH}_3$  selectivity at the lower Pd loading to the larger number of  $\text{O}_v$ , which survived at the surface, promoting  $\text{NH}_3$  formation. The higher  $\text{NH}_3$  selectivity at the higher Pd loading is rationalized by the fact that more  $\text{H}^*$  are exported to the  $\text{O}_v$  for  $\text{NO}_3^-$  reduction, and the resultant smaller N/H ratio is conducive to  $\text{NH}_3$  formation.

Given the presence of various anions and dissolved organics in natural water, their impacts on the NRR performances of Pd- $\text{MnO}_2$ - $\text{O}_v$ /Ni foam electrodes have to be considered. The carbonate ( $\text{CO}_3^{2-}$ , 1.0 mM), sulfite ( $\text{SO}_3^{2-}$ , 3.0 mM), and chloridion ( $\text{Cl}^-$ , 5.0 mM) are selected as the probe anions,<sup>45</sup> while the humic acid ( $3.3 \text{ mg L}^{-1}$ ) is selected to represent the dissolved organics.<sup>46</sup> Intriguingly, insignificant differences in the  $\text{NO}_3^-$ -N conversion rate, faradaic current efficiency, and  $\text{NH}_3$  selectivity are observed in Fig. 3m–o after the introduction of anions and humic acid, suggesting the relatively strong resistance of our electrode to the disturbance from natural water environments. The humic acid exhibits some detrimental effects as the  $\text{NO}_2^-$  residues increase to 9.87%. It hints that a lower organic content in water is conducive to the efficient and complete conversion of  $\text{NO}_3^-$  to  $\text{NH}_3$ .

### 3.3. The dual-site catalysis mechanism

As observed, the Pd- $\text{MnO}_2$ - $\text{O}_v$ /Ni foam delivers both the high  $\text{NO}_3^-$  conversion rate and  $\text{NH}_3$  selectivity, which can be expected by the proposed dual-site reaction mechanism that the  $\text{O}_v$  site adsorbs and activates  $\text{NO}_3^-$  while the Pd site generates  $\text{H}^*$  and exports them to the  $\text{O}_v$  site for NRR. To confirm this mechanism, DFT calculations on the adsorption energy of  $\text{H}^*$ ,  $\text{N}^*$ , and  $\text{O}^*$ , as well as the Gibbs free energy changes for the  $\text{NO}_3^-$  conversion to  $\text{NH}_3$  and  $\text{N}_2$  on  $\text{MnO}_2$ ,  $\text{MnO}_2$ - $\text{O}_v$ , and Pd surfaces, were performed. The  $\delta$ - $\text{MnO}_2$  (001) surfaces without and with one  $\text{O}_v$  are chosen to model fine  $\text{MnO}_2$  and  $\text{MnO}_2$ - $\text{O}_v$ , while Pd (111) is selected as the active Pd surface. Fig. S3† reveals that the  $\text{H}^*$  adsorption on  $\text{MnO}_2$ - $\text{O}_v$  is much weaker than that on Pd, confirming the better performance of Pd in proton harvest (the over-strong H adsorption on fine

MnO<sub>2</sub> can be ascribed to the formation of –OH groups. This H species is inert and cannot be used in NRR). Combining these calculation results with the poor NRR performance of the single MnO<sub>2</sub>-O<sub>v</sub> in Fig. 2b, we are ascertained that the H\* required for NRR is primarily provided by Pd.

Fig. 4a and b compare the Gibbs free energy changes ( $\Delta G$ ) of the elementary reactions occurring during the NO<sub>3</sub><sup>-</sup> conversion to N<sub>2</sub> and NH<sub>3</sub> on Pd (111) and MnO<sub>2</sub>-O<sub>v</sub> (001), respectively. The N-intermediates and elementary reactions are set according to the literature.<sup>14,47,48</sup> Basically, the NRR can be divided into two stages: (I) NO<sub>3</sub><sup>-</sup> adsorption and its conversion to NO<sub>2</sub><sup>\*</sup>, which is well-known as the rate-determining step of NRR; (II) NO<sub>2</sub><sup>\*</sup> conversion to N<sub>2</sub> or NH<sub>3</sub>, which is considered as the determinant of product selectivity. As observed, the process I on the MnO<sub>2</sub>-O<sub>v</sub> surface is spontaneous with an overall negative  $\Delta G$  of -3.56 eV, while that on the Pd surface has to overcome an energy barrier of 0.51 eV (0.48 eV for NO<sub>3</sub><sup>-</sup> adsorption and 0.03 eV for NO<sub>3</sub><sup>\*</sup> hydrogenation). More intriguingly, O<sub>v</sub> is found to have the ability to grab one O atom from both NO<sub>3</sub><sup>\*</sup> and NO<sub>2</sub><sup>\*</sup> and complete the NO<sub>3</sub><sup>\*</sup>-NO\* conversion along with their adsorption processes. All these calculation results clearly verify that NO<sub>3</sub><sup>-</sup> is preferred to be adsorbed and activated on MnO<sub>2</sub>-O<sub>v</sub> rather than the Pd site. It should be mentioned that O<sub>v</sub> is filled by the oxygen atoms during the NO<sub>3</sub><sup>-</sup>/NO<sub>2</sub><sup>\*</sup> activation and should be regenerated under the synergy of polarization potential and H\* by overcoming an energy barrier of 0.87 eV ((1.23-0.36) eV).

In stage II, the NO\* on MnO<sub>2</sub>-O<sub>v</sub> is ready to be deeply hydrogenated to NH<sub>3</sub><sup>\*</sup> in an energetically favored pathway of NO\* → NOH\* → N\* → NH\* → NH<sub>2</sub><sup>\*</sup> → NH<sub>3</sub><sup>\*</sup> with the  $\Delta G$  of all the steps displaying negative values. The N<sub>2</sub> formation is relatively difficult as the N\*-N\* pairing requires extra energy of 0.43 eV. In comparison, the NO<sub>2</sub><sup>\*</sup> conversion to NH<sub>3</sub> and N<sub>2</sub> on Pd (111) experiences similar energy profiles, pointing to the rela-

tively poor product selectivity to NH<sub>3</sub> or N<sub>2</sub> on the Pd site. This is consistent with the previous reports that a mixed product of NH<sub>3</sub> and N<sub>2</sub> can be formed on Pd-based catalysts.<sup>49,50</sup> Combining the calculation results with the high NH<sub>3</sub> selectivity of Pd-MnO<sub>2</sub>-O<sub>v</sub> in Fig. 2c, we are ascertained that the O<sub>v</sub> site is the active center for the selective conversion of NO<sub>3</sub><sup>-</sup> to NH<sub>3</sub>.

We also examined the adsorption energies of N\* and O\* on MnO-O<sub>v</sub> and Pd, and the results in Fig. 4c and d reveal the much stronger adsorption of O\* and N\* on the O<sub>v</sub> site of MnO<sub>2</sub>-O<sub>v</sub> than that on Pd. Given the linear scale of the adsorption energies for N-intermediates with that for either an oxygen or nitrogen atom,<sup>51,52</sup> all the N-intermediates are believed to be preferably immobilized and reduced at the O<sub>v</sub> site during NRR, which reduces their encountering possibilities and contributes to high NH<sub>3</sub> selectivity.

On the basis of all the above, we firmly believe the dual-site NRR mechanism on MnO<sub>2</sub>-O<sub>v</sub>-Pd, which is schematically described in Fig. 4e. The O<sub>v</sub> serves to adsorb, immobilize, and activate the NO<sub>3</sub><sup>-</sup> and N-intermediates, while Pd supplies the O<sub>v</sub> with sufficient H\* for both the NRR and O<sub>v</sub> refreshment. Such a dual-site NRR mechanism accounts for both the efficient NRR and the high NH<sub>3</sub> selectivity.

## 4. Conclusions

This work demonstrates the superior performance of the three-dimensional porous Pd-MnO<sub>2</sub>-O<sub>v</sub>/Ni foam electrode for NRR. In a continuous-flow reaction cell, it delivers a substantial NO<sub>3</sub><sup>-</sup>-N conversion rate of 642 mg N m<sup>-2</sup> electrode h<sup>-1</sup> and a NH<sub>3</sub> selectivity of 87.64% under -0.85 V when feeding a 22.5 mg L<sup>-1</sup> NO<sub>3</sub><sup>-</sup>-N solution at a rate of 0.875 mL min<sup>-1</sup>, outperforming the Pd/Ni foam (369 mg N m<sup>-2</sup> electrode h<sup>-1</sup>, 84.02%) and MnO<sub>2</sub>-O<sub>v</sub>/Ni foam (118 mg N m<sup>-2</sup> electrode h<sup>-1</sup>, 32.25%). Combining the experimental characterizations and the theoretical calculations, we confirm the dual-site NRR process on Pd-MnO<sub>2</sub>-O<sub>v</sub>, in which the MnO<sub>2</sub>-O<sub>v</sub> serves to adsorb, immobilize, and activate the NO<sub>3</sub><sup>-</sup> and the N-intermediates, while Pd supplies the O<sub>v</sub> with sufficient H\* for both the NRR and O<sub>v</sub> refreshment. This work highlights the critical role of dual-site catalysis in the efficient and selective nitrate conversion to NH<sub>3</sub>, paving the way for utilizing dual-site catalysis in both the nitrate pollution abatement and nitrogen resource recycling from nitrate wastewater.

## Conflicts of interest

The authors declare no competing financial interest.

## Acknowledgements

We acknowledge the funding support from the National Natural Science Foundation of China (2217061059 and 51978110), the Program for the Top Young Talents of



Fig. 4 The reaction energy diagram for the conversion of NO<sub>3</sub><sup>-</sup> to N<sub>2</sub> and NH<sub>3</sub> over (a) clean MnO<sub>2</sub>-O<sub>v</sub> (001) and (b) Pd (111) facet; adsorption energies of (c) one oxygen atom and (d) one nitrogen atom on MnO<sub>2</sub>-O<sub>v</sub> (001) and Pd (111) facets; (e) schematic illustration of the MnO<sub>2</sub>-O<sub>v</sub>-Pd dual-site NRR mechanism for a high NH<sub>3</sub> selectivity.

Chongqing, Innovation group of new technologies for industrial pollution control of Chongqing Education Commission (CXQT19023), and Science and Technology Research Program of Chongqing Municipal Education Commission (KJQN201800829 and KJZD-K202000802).

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