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Many industry applications require electronic circuits and systems to operate at high temperatures over 150 °C. Although planar micro-supercapacitors (MSCs) have great potential for miniaturized on-chip integrated energy storage components, most of the present devices can only operate at low temperatures (<100 °C). In this work, we have demonstrated a facile process to fabricate activated graphene-based MSCs that can work at temperatures as high as 150 °C with high areal capacitance over 10 mF cm<sup>-2</sup> and good cycling performance. Remarkably, the devices exhibit no capacitance degradation during temperature cycling between 25 °C and 150 °C, thanks to the thermal stability of the active components.

The rapid development of a variety of industries, such as aerospace, avionics, automotive, down-hole oil and gas has driven the demand for high-temperature electronics that is able to work at ambient temperatures higher than 150 °C.<sup>1</sup> To fulfil this requirement circuits and systems based on conventional silicon complementary metal-oxide-semiconductor (CMOS) technology must be uprated to working beyond their temperature specifications. In recent years, silicon carbide (SiC) CMOS electronics have been demonstrated as a promising alternative to silicon CMOS technology and proven to function at temperatures up to 500 °C.<sup>2</sup> However, one critical limitation for the future implementation of these circuits and systems arises from the compliance of the power supply with the high temperature environment, since most energy storage devices operate at temperatures no higher than 60 °C.<sup>3</sup> Meanwhile, the continuous miniaturization of electronics raises the demand for on-chip integrated power sources as well.<sup>4</sup> As a result, on-chip

## Facile fabrication of graphene-based high-performance microsupercapacitors operating at a high temperature of 150 °C†

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integrated power supply with the capability of operating at high temperatures is highly desired for many future electronics.

Planar microsupercapacitors (MSCs) are envisioned as promising candidates for on-chip integrated energy storage components<sup>4</sup> because of their high power density, rapid charge-discharge and long cycle life. Several studies have demonstrated different high-temperature MSCs working at temperatures above 60 °C.<sup>5-7</sup> However, to the best of our knowledge, the operating temperature of the existing MSCs has not gone beyond 100 °C. Typically, supercapacitors comprise two sets of separate current collectors and active electrodes immersed in a common electrolyte yet electrically separated by a porous membrane.<sup>8</sup> In order to enable the entire device to work at high temperatures, all the components must possess good thermal stability. So far various materials have been developed for different components to increase the operating temperature of conventional (stacked) batteries and supercapacitors,<sup>9</sup> such as molten salts,<sup>10</sup> ceramics,<sup>11</sup> and room-temperature ionic liquids (RTILs)<sup>12,13</sup> for high-temperature electrolytes, clay material for high-temperature separators,<sup>12</sup> and biochar<sup>14</sup> and transition metal sulfides<sup>10</sup> for high-temperature electrodes. However, it is still challenging to integrate the compatible components to fabricate high-performance MSCs in a simple manner. The key process for the fabrication of MSCs is the patterning of active electrode materials into small interdigitated structures.<sup>4</sup> Most simple patterning techniques, such as various printing processes,<sup>15-17</sup> require polymeric binders to increase the uniformity and stability of both the initial inks or slurries during the fabrication process and the final electrodes in a harsh operating environment. However, the binders will cause device failure during high-temperature operation.<sup>7</sup> On the other hand, the demonstrated techniques to fabricate binder-free MSC electrodes, such as electrophoretic deposition<sup>5</sup> and vacuum filtration,<sup>6</sup> suffer from complicated processing or limited electrode thickness (active material loading) which results in low areal capacitance and energy density, key characteristic properties of MSCs.<sup>4</sup>

In this work, we report a facile process to fabricate MSCs that can operate at temperatures up to 150 °C with good cycle

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lifetime and high areal capacitance over  $10 \text{ mF cm}^{-2}$ . The fabrication of the MSC electrodes relies on our previously reported high-concentration aqueous inks of activated graphene.<sup>18</sup> In contrast to many other graphene inks, which often use polymeric binders for stabilization,<sup>15,16</sup> our activated graphene inks use graphene oxide as the surfactant, fumed silica as the rheology modifier, and carbon nanotubes (CNTs) as the conductive binder to improve mechanical and electrical contacts between the grains of activated graphene. The electrically insulating graphene oxide is reduced to conductive reduced graphene oxide (rGO) after the post-deposition annealing to further improve the electrical conductivity. It is important to note that all the additives (rGO, CNTs and fumed silica) and the activated graphene have excellent thermal stability at high temperatures over  $400^\circ\text{C}$ , which offers great opportunities for us to fabricate stable electrodes for high-temperature MSCs. In particular, the obtained highly concentrated ( $20 \text{ mg mL}^{-1}$ ), viscous (over  $10^4 \text{ Pa s}$ ) and stable water-based activated graphene inks<sup>18,19</sup> enable us to fabricate high-performance MSCs through four simple steps: (1) drop casting of electrode materials, (2) drying and annealing, (3) direct laser patterning through laser scribing, and (4) drop casting of electrolytes, as illustrated in Fig. 1a. The high viscosity and high concentration of the graphene inks make it convenient to fabricate uniform thick (in the range of  $25\text{--}50 \mu\text{m}$ , Fig. 1e and S2†) graphene electrode films with a sheet resistance of  $9.3 \Omega \text{ sq}^{-1}$  simply through drop casting. In practice, to further improve the patternability, a small amount ( $10 \text{ mg mL}^{-1}$ ) of sacrificial viscosifier, xanthan gum, was added to the activated

graphene inks to further increase the ink viscosity. After the ink dried, the obtained electrode films were annealed at  $300^\circ\text{C}$  in air for 30 minutes to remove the xanthan gum, reduce the graphene oxide and enhance the thermal stability of the electrodes. Afterwards, direct laser scribing was used to pattern the electrode films into interdigitated structures (Fig. 1a and c) with a finger width of 1 mm, an inter-finger gap of  $500 \mu\text{m}$  and a total footprint area of  $0.6 \text{ cm}^2$  (including the gap region). Finally, an ionogel based on a mixture of poly(vinylidenefluoride-*co*-hexafluoropropylene) (PVDF-HFP) and a RTIL, 1-butyl-3-methylimidazolium tetrafluoroborate (BMIM-BF<sub>4</sub>) in acetone was drop cast onto the electrodes to form the final MSCs, benefiting from the good thermal stability of both PVDF-HFP and BMIM-BF<sub>4</sub>. The details of the device fabrication are described in the ESI.†

To study the thermal stability of the MSCs, high temperature measurements were performed on a Signatone S-1060R 4" Hot Chuck with a temperature accuracy of  $1^\circ\text{C}$ . Cyclic voltammetry (CV), electrochemical impedance spectroscopy (EIS) and galvanostatic charge–discharge (GCD) analyses were performed and measured at  $25, 50, 100$  and  $150^\circ\text{C}$ , respectively. Fig. 2a shows the CV curves for the MSCs at scan rates ranging from 5 to  $250 \text{ mV s}^{-1}$  at  $25^\circ\text{C}$ . The device exhibits rectangular profiles at low scan rates  $<50 \text{ mV s}^{-1}$ , indicating the electrical double layer capacitive behaviour. However, at high scan rates  $>100 \text{ mV s}^{-1}$ , the CV profile becomes lens-like. The relatively high series resistance degrades the device performance at high scan rates. In contrast, as shown in Fig. 2b, the CV curves at  $150^\circ\text{C}$  retain good rectangularity even at high scan rates, pointing to the

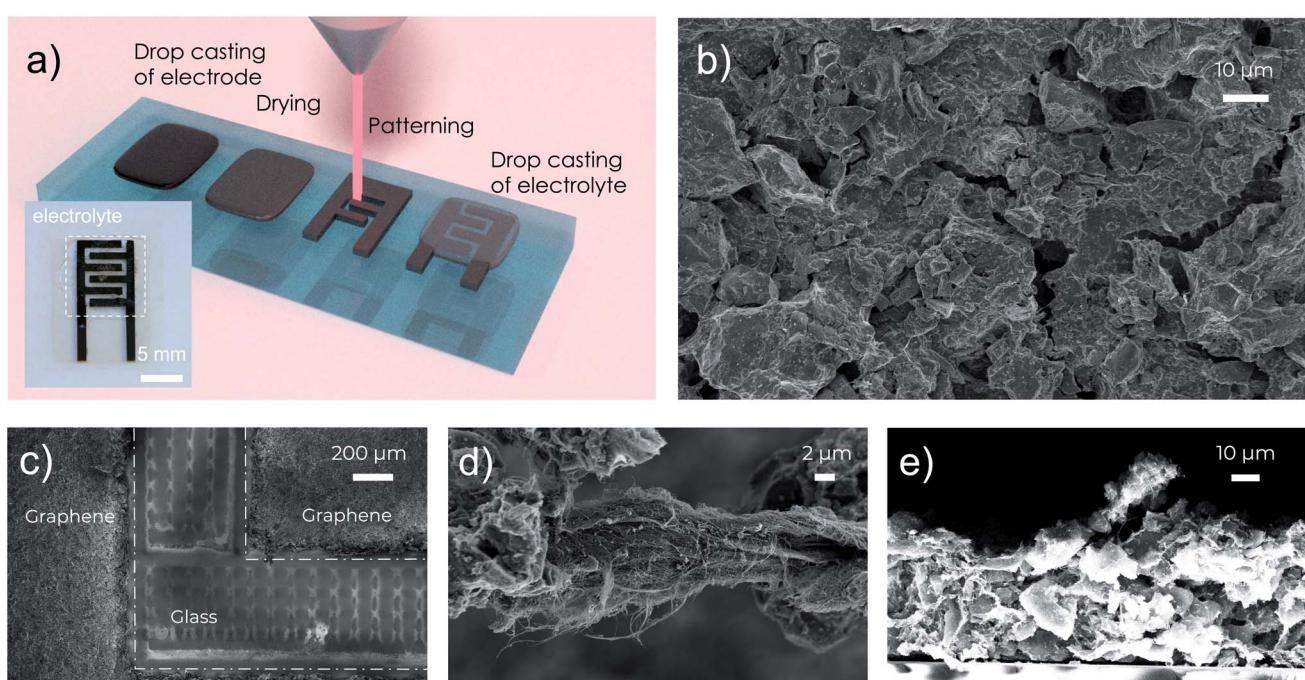


Fig. 1 The fabrication of the high-temperature MSCs on a glass substrate. (a) Schematic of step-by-step fabrication of the MSCs. Inset at the left-bottom corner: photograph of a final MSC with a drop-cast gel electrolyte. (b) SEM image of the graphene electrode. (c) SEM image of the inter-finger gap of an MSC patterned through direct laser scribing. (d) SEM image of the carbon nanotube binder protruding from some electrode surface after patterning. (e) SEM image of a cross-section of the activated graphene electrode.



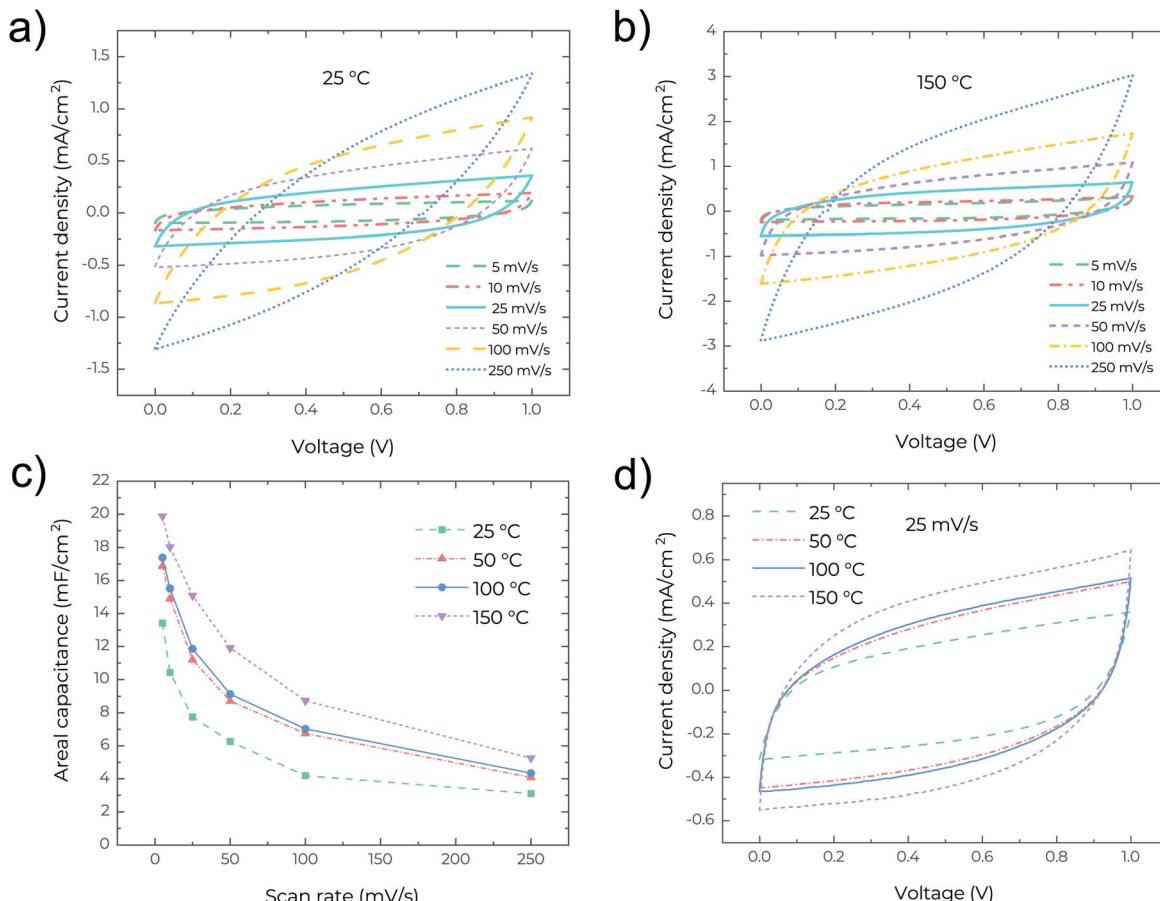


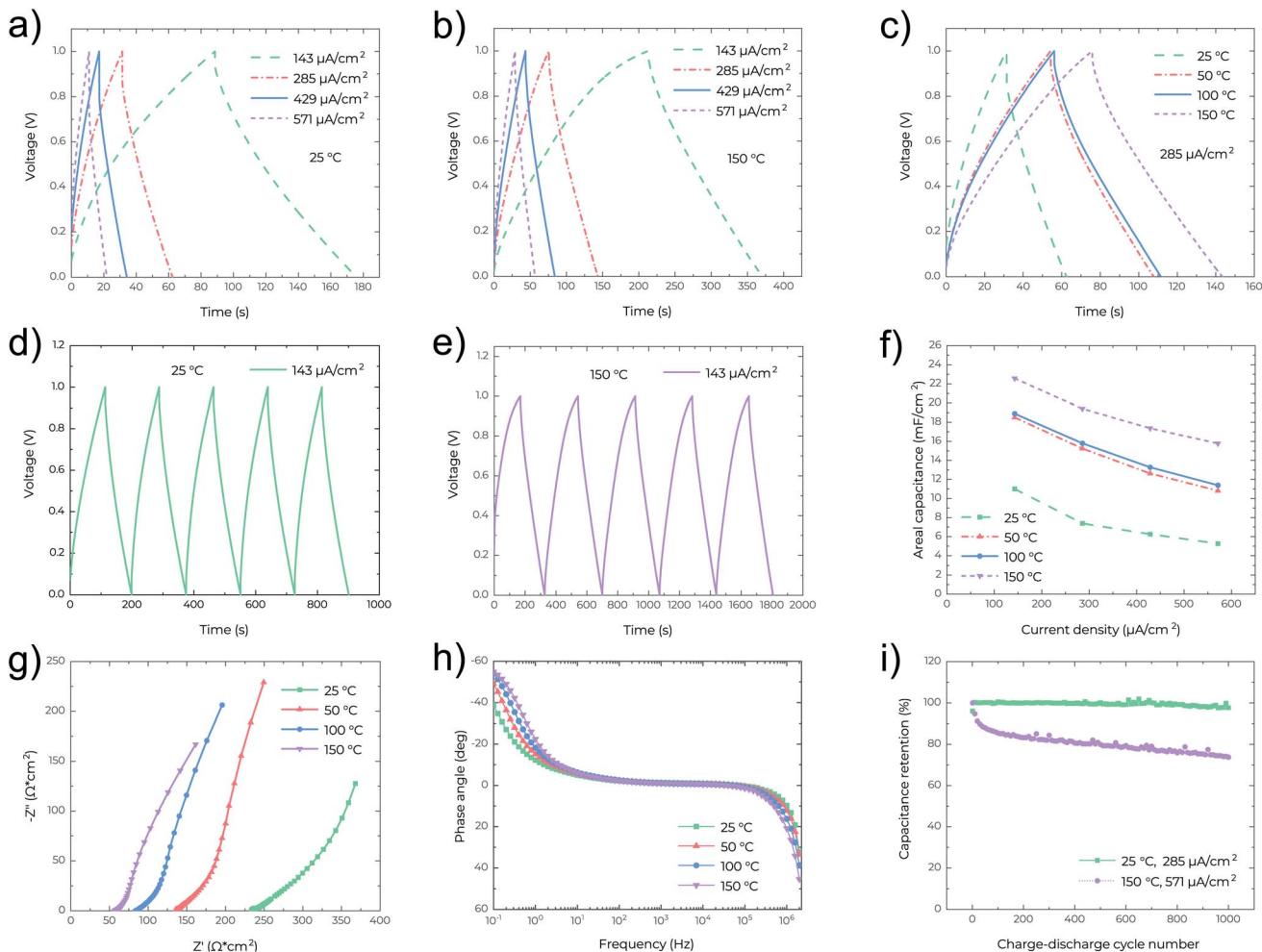
Fig. 2 CV performance of the MSCs. (a and b) CV curves at different scan rates for the MSCs measured at (a) 25 °C and (b) 150 °C. (c) Areal capacitances extracted from CV curves at different operating temperatures and scan rates. (d) CV curves obtained at a scan rate of  $25 \text{ mV s}^{-1}$  at different operating temperatures.

capability of the MSCs working at temperatures as high as 150 °C and with higher performance. Fig. 2c presents the areal capacitance measured at different temperatures and scan rates and clearly confirms the increase of areal capacitance with increasing temperature. Remarkably, a high areal capacitance of about  $20 \text{ mF cm}^{-2}$  is obtained for the MSCs operating at 150 °C and at a scan rate of  $5 \text{ mV s}^{-1}$ . This performance is even superior to many MSCs reported recently that can only operate at low temperature  $<60$  °C. The high areal capacitance is related to the very high surface area ( $\sim 2700 \text{ m}^2 \text{ g}^{-1}$ ) of the precursor activated graphene.<sup>18</sup> The temperature-dependent areal capacitance is also confirmed in Fig. 2d where the rectangular CV profile (measured at a scan rate of  $25 \text{ mV s}^{-1}$ ) enlarges with the increase of temperature. In general, the ionic conductivity of the gel electrolyte increases with temperature due to the reduced viscosity and follows the Arrhenius-type thermally activated behavior,<sup>20</sup> which is likely the cause of an increase in areal capacitance with increasing operating temperature of the MSCs.

In Fig. 3a–e the nearly symmetrical and triangular profile of the GCD curves at different current densities and temperatures confirms the electrical double layer behaviour of the MSCs. For the given current densities, the discharge times are increased almost twice when the operating temperature increases from

25 °C (Fig. 3a) to 150 °C (Fig. 3b), as also confirmed in Fig. 3c. In Fig. 3c, at the same current density, the IR drop also decreases from 0.13 V at 25 °C to 0.04 V at 150 °C, confirming again the reduced resistance of the MSCs at high temperature. Fig. 3f shows that the areal capacitance significantly increases with temperature, consistent with the results obtained from the CV analysis (Fig. 2c). The highest capacitance of  $22.5 \text{ mF cm}^{-2}$  was attained at 150 °C and measured at a current density of  $143 \mu\text{A cm}^{-2}$ . EIS characterization was also performed to analyze the capacitive behavior of the MSCs. In Fig. 3g, the Nyquist plots indicate that the series resistance of the MSC decreases with temperature from  $233 \text{ ohm cm}^2$  at 25 °C to  $57 \text{ ohm cm}^2$  at 150 °C. At the low-frequency region, the Nyquist plots are nearly vertical at all temperatures indicating ideal capacitive behavior, while at the mid-frequency region, the parts for the 45° Warburg-type impedance element shrink with the increasing temperature, which implies fast ion diffusion at high temperature.<sup>21,22</sup> In Fig. 3h the Bode phase plots also show that the characteristic frequency (at which the impedance phase angle is  $-45^\circ$ )<sup>15</sup> increases with temperature, confirming lower series resistance and hence higher electrochemical performance of the MSC at high temperature. Fig. 3i outlines the cycling behaviour of MSCs at different temperatures. After 1000 cycles,





**Fig. 3** GCD and EIS performance of the MSCs. (a and b) GCD curves at different current densities operating at (a) 25 °C and (b) 150 °C. (c) GCD curves measured at different temperatures at the same current density of 285  $\mu\text{A cm}^{-2}$ . (d and e) 5 cycles of GCD measurement of MSCs operating at (d) 25 °C and (e) 150 °C and at a current density of 143  $\mu\text{A cm}^{-2}$ . (f) Temperature dependence of the areal capacitance measured at different current densities. (g) Nyquist plots and (h) Bode phase plots for the MSCs at different operating temperatures. (i) Capacitance retention of the MSCs over 1000 GCD cycles measured at 285  $\mu\text{A cm}^{-2}$  at 25 °C and at 571  $\mu\text{A cm}^{-2}$  at 150 °C.

97.6% of the capacitance is retained at 25 °C and 73.7% at 150 °C. It is worth mentioning that most probably this is the first demonstration of the cycling performance of MSCs at a high temperature of 150 °C. The relatively poor cycling performance (73.7% capacitance retention after 1000 cycles) is likely due to the limited thermal stability of PVDF-HFP in the electrolyte. Another important reason is that the cycling test at 150 °C is at a high current density of 571  $\mu\text{A cm}^{-2}$ .

To further underline the thermal stability of the MSCs, the cycling performance against temperature change was also studied. Fig. 4a shows the recoverability of the device performance upon one cycle of temperature change at different scan rates. It is clear that at all scan rates the areal capacitance increases with temperature, and returns to the initial values once the MSCs cool down. This indicates high repeatability of the device performance with the temperature change in any direction. Fig. 4b presents the repeatability of the areal capacitance after 5 full temperature cycles (each cycle consists of a temperature increase from 25 °C to 150 °C and a following

cooling down from 150 °C to 25 °C). After every temperature cycle, the areal capacitance can retain its initial values. This can be confirmed in Fig. 4c where the CV curves are indistinguishable between different temperature cycles. All these verify the excellent performance reliability and thermal stability of the MSCs.

One of the specific features of the RTIL-based electrolytes is their ability to operate within a wide voltage window, which leads to much higher energy density.<sup>23</sup> Fig. S5a and b† show the CV curves of the MSCs for a range of voltage windows at 25 °C and 150 °C, respectively. After increasing the voltage window from 1.0 V to 2.0 V, the CV curves retain the good rectangularity. Furthermore, it is possible to increase areal capacitance by increasing the operating voltage window at both 25 °C and 150 °C (Fig. S5c†). At 150 °C, when the voltage window increases from 1.0 V to 2.0 V, the areal capacitance (at a scan rate of 25  $\text{mV s}^{-1}$ ) increases from 15.1  $\text{mF cm}^{-2}$  to 19.4  $\text{mF cm}^{-2}$ , corresponding to an increase of areal energy density from 2.1  $\mu\text{W h cm}^{-2}$  to 10.8  $\mu\text{W h cm}^{-2}$ , and an increase of areal power density

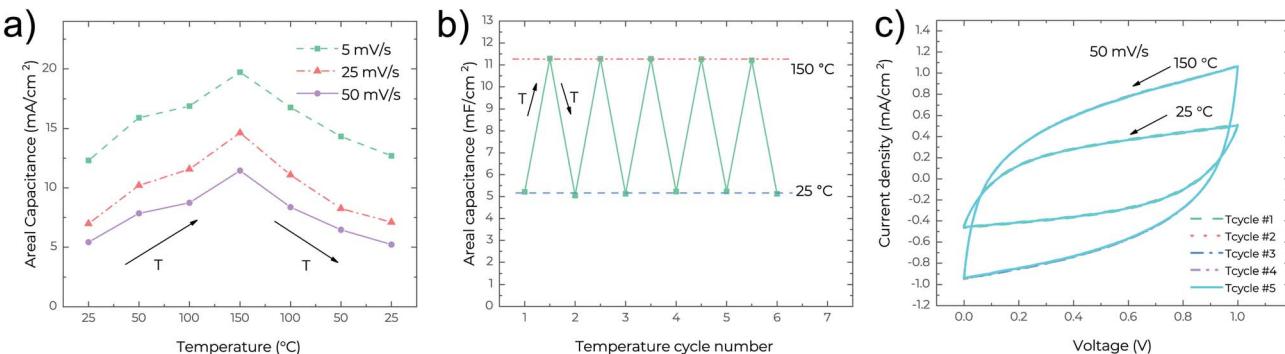


Fig. 4 Temperature cycling performance of the MSCs. (a) Areal capacitance of an MSC varying with temperature. (b) Areal capacitance varying with temperature change between 25 °C and 150 °C over 5 cycles. (c) CV curves at 50 mV s<sup>-1</sup> at 25 °C and 150 °C during the temperature cycling tests.

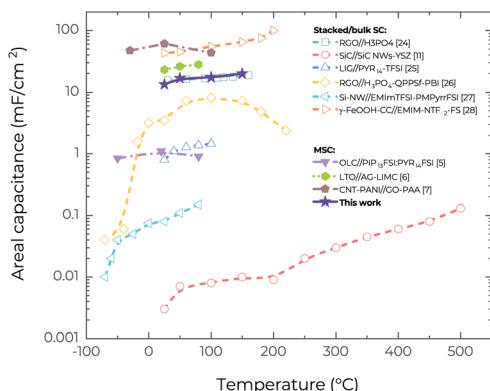


Fig. 5 Comparison of the areal capacitance of high-temperature supercapacitors in the literature to date, including both planar MSCs and stacked supercapacitors. Here, the areal capacitance for this work is in the voltage window of 1.0 V.

from 0.19 mW cm<sup>-2</sup> to 0.49 mW cm<sup>-2</sup>. However, additional research is still needed to confirm the reliability of the working voltage of 2.0 V at 150 °C because in the GCD characterization (Fig. S6†) it is difficult to charge the devices to 2.0 V at a medium current density of 285 μA cm<sup>-2</sup> whereas they can be readily charged to 1.0 V even at a lower current density of 143 μA cm<sup>-2</sup> (Fig. 3e). Fig. 5 compares the temperature-dependent areal capacitance of our MSCs with that of other reported planar MSCs and stacked supercapacitors in the literature.<sup>5-7,11,24-28</sup> It is clear that our MSCs exhibit both larger areal capacitance (for the values obtained from the voltage window of 1.0 V) and higher operating temperature than most other supercapacitors, in spite of their facile fabrication process.

## Conclusions

In conclusion, combining our previously developed ink based on high surface area activated graphene with direct laser scribing and ionogel electrolytes, we have developed a facile technique to fabricate MSCs that can operate at high temperatures up to 150 °C. The devices exhibit good thermal stability under both cyclic charging/discharging test and cyclic

temperature change test when charged up to 1.0 V. Likely for the first time, we have demonstrated that the MSCs can be charged and discharged at 150 °C for 1000 cycles with capacitance retention of 74% at a high current density of 571 μA cm<sup>-2</sup>. At 150 °C, the MSCs can also be readily operated in the voltage window of 1.0 V, resulting in a large areal capacitance of 15.1 mF cm<sup>-2</sup>, a high areal energy density of over 2 μW h cm<sup>-2</sup> and a high areal power density of about 0.2 mW cm<sup>-2</sup>. The performance is superior to that of most other reported MSCs in the literature that can only operate at low temperatures. Therefore, our MSCs have great potential to serve as the on-chip integrated energy storage components for future electronics that operate in high temperature environments.

## Conflicts of interest

There are no conflicts to declare.

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