

# Single catalyst particle diagnostics in a microreactor for performing multiphase hydrogenation reactions†

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Since inter- and intra-particle heterogeneities in catalyst particles are more the rule than the exception, it is advantageous to perform high-throughput screening for the activity of single catalyst particles. A multiphase system (gas/liquid/solid) is developed, where droplet-based microfluidics and optical detection are combined for the analysis of single catalyst particles by safely performing a hydrogenation study on in-house synthesized hollow Pd/SiO<sub>2</sub> catalyst microparticles, in a polydimethylsiloxane (PDMS) microreactor. A two-phase segmented flow system of particle-containing droplets is combined with a parallel gas-reactant channel separated from the flow channel by a 50 μm thick gas permeable PDMS wall. In this paper, the developed microreactor system is showcased by monitoring the Pd-catalyzed hydrogenation of methylene blue. A discoloration of blue to brown visualizes the hydrogenation activity happening in a high-throughput fashion on the single Pd/SiO<sub>2</sub> spherical catalyst microparticles, which are encapsulated in 50 nL-sized droplets. By measuring the reagent concentration at various spots along the length of the channel the reaction time can be determined, which is proportional to the residence time in the channel. The developed experimental platform opens new possibilities for single catalyst particle diagnostics in a multiphase environment.

## Introduction

In the search for more effective catalysts and reaction conditions, the use of high-throughput experimentation to monitor catalyst performance on a single particle level has gained increasing interest over the last decades.<sup>1–4</sup> A growing field of

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research that has shown great potential for these types of experiments is lab-on-a-chip, and in particular droplet-based microfluidics.<sup>5–7</sup> When using two immiscible fluids and specific geometries such as a T-junction or flow focusing geometry, droplets can be created by a combination of surface tension and shear forces.<sup>8</sup> Due to the low Reynolds numbers in microfluidic channels, the droplets are typically monodisperse and equally spaced, and do not merge when traveling through the microreactor. With all kinds of external forces (*e.g.*, electric, magnetic, acoustic) the droplets can be manipulated, offering the possibility for more complex chemistry or droplet sorting.<sup>9</sup> Furthermore, the use of droplets compartmentalizes reagents and products, and thus prevents Taylor dispersion or lateral mixing. The droplet compartments prevent dispersion along the length of the channel due to the parabolic flow profile, as observed in single phase flow.<sup>8</sup> In these droplets, single catalyst particles can be encapsulated to perform high-throughput screening of their catalytic activity.

Droplet microfluidics aimed at single particle or single cell diagnostics has mainly been used for biochemical assays, such as the study of single cells or rapid screening for the discovery of new enzymes.<sup>10–12</sup> One of the main advantages of droplet microfluidics is that the before-mentioned droplets with a single cell or particle, act as pico-/nanoliter sized reaction vessels, *i.e.*, “nanoreactors”. The use of optically-transparent reactor materials, such as polydimethylsiloxane (PDMS) or glass,<sup>13</sup> allows for *in situ* micro- and/or spectroscopic measurements within these droplets.

When we perform a catalytic reaction inside droplets that contain a catalyst particle, we can detect the activity of each catalyst particle, by measuring for example induced fluorescence, a specific color change or distinctive Raman or IR bands in the droplet. With an optical or spectroscopic detection method along the channel, the products formed per single particle can be analyzed by measuring all droplets passing through the detector.<sup>14</sup> This opens possibilities for the characterization of catalyst particles in liquid-phase reactions. However, a large class of heterogeneous catalytic reactions involve not only a liquid-phase and a solid-phase, but also a gas phase. This class of reactions brings an extra challenge to the field of microfluidics: not much work has been done on the combined control of both liquids, solids and gases. Recent work on the control of multiphase reactions in microfluidic devices has focused on the immobilization of a heterogeneous catalyst either as a packed-bed or as a coating on the channel interior.<sup>15–18</sup> Mixed feeds with gas slugs in a liquid flow were used to create a multiphase system. However, the precise control of gas slugs in a liquid flow has proven to be difficult, due to different forces other than the shear force and interfacial tension, that contribute to the formation and stabilization of liquid droplets.<sup>19</sup> Although, adding a surfactant to the liquid-phase helps to increase flow stability,<sup>20</sup> it is still difficult to get monodisperse gas slugs or droplets at fixed flow rates for both phases.<sup>21</sup> This motivates researchers to use a microreactor with gas-permeable channel walls. In this way, we can form stable liquid “nanoreactor” droplets with encapsulated catalyst particles in an immiscible and non-reactive oil phase. Gases can diffuse through the permeable reactor into the droplets, thereby creating a multiphase (gas/liquid/solid) environment. Gas permeable liquids with low solubility for gases, such as fluorinated oil, can be used as the continuous phase to increase the gas flux towards the droplet.



In this work, a PDMS microreactor has been developed with three parallel channels, as schematically shown in Fig. 1, to perform gas/liquid/solid catalytic reactions for the diagnostics of single catalyst particles. PDMS is a flexible polymer that is often used for the fabrication of microfluidic systems, since the fabrication of PDMS microreactors utilizes soft lithography which is relatively cheap and easy.<sup>22</sup> Furthermore, it is known that PDMS has a high permeability to gases, such as  $H_2$  and  $O_2$ , which is used to our advantage. The outer channels, as shown in Fig. 1, are used for the flow of  $H_2$  that permeates through the PDMS walls and reaches the central liquid channel. In this liquid channel droplets of methylene blue (MB) dissolved in ethanol, containing single particles of a Pd-catalyst, flow in a continuous fluorinated oil phase. As a proof of principle reaction, the hydrogenation of MB to leuco-MB that discolors from blue to colorless is performed.<sup>23</sup> This reaction is catalyzed by 40  $\mu m$  sized hollow spherical Pd/SiO<sub>2</sub> particles encapsulated in the MB/ethanol droplets. The droplets that flow through the reactor channel, have identical residence times at any chosen position along the length of the channel. This allows *in situ* analysis of the ongoing reaction, by measuring the color of the droplet at various spots along the length of the channel.

## Results and discussion

### Microreactor design and fabrication

The PDMS microreactor, as shown in Fig. 2, was designed to benefit from the gas-permeability of PDMS: a thin wall of 50  $\mu m$  between the gas and the droplet channel allows for fast diffusion of  $H_2$  to the liquid droplets with reactant and catalyst. The hydrogenation reaction can only take place when the three phases meet (the solid catalyst particle, the liquid MB in ethanol and the gaseous  $H_2$ ) and

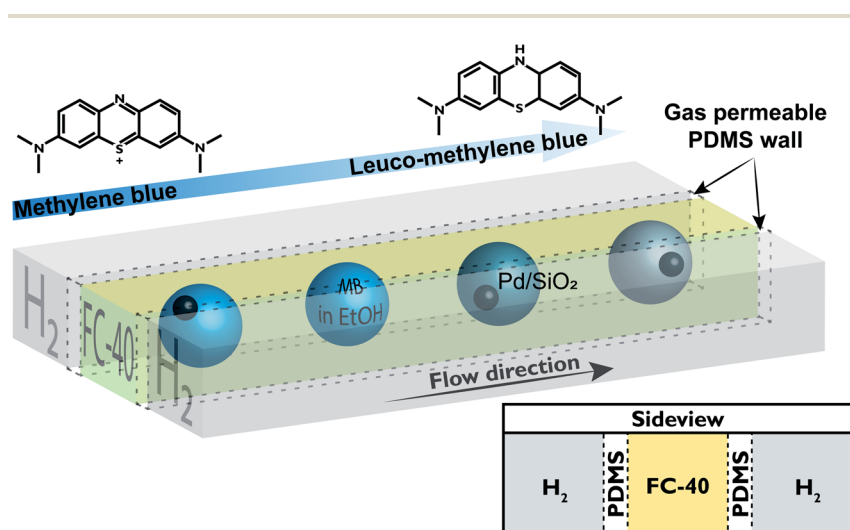


Fig. 1 Schematic representation of a polydimethylsiloxane (PDMS) microreactor with three parallel channels separated by 50  $\mu m$  thick walls.  $H_2$  can diffuse through the walls and hydrogenate methylene blue (MB) to leuco-MB in the presence of Pd/SiO<sub>2</sub> particles in ethanol droplets.



## Faraday Discussions

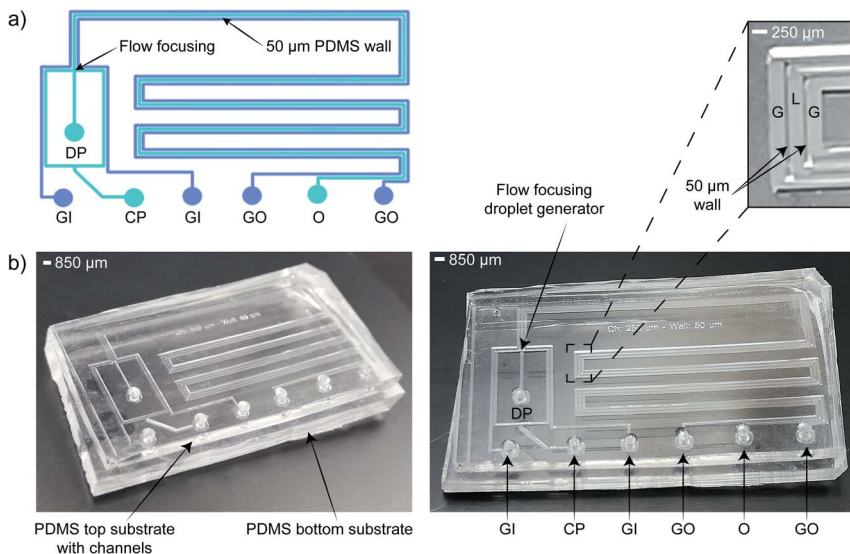


Fig. 2 A schematic representation (a) and images (b) of the polydimethylsiloxane (PDMS) microreactor ( $2 \times 1$  cm length and width) and of the channel system showing the gas inlet (GI), continuous phase inlet (CP), droplet phase inlet (DP), gas outlet (GO) and fluidic outlet (O). The zoomed-in image shows the gas (G) and liquid (L) channels, the  $50 \mu\text{m}$  thin PDMS wall that separates the gas and liquid channels is shown. All channels are  $250 \mu\text{m}$  wide and deep.

therefore starts when the catalyst particle-containing droplets enter the liquid microchannel ( $250 \times 250 \mu\text{m}$  width and depth) surrounded by two  $\text{H}_2$  gas channels with similar cross-sectional dimensions. Ethanol droplets (containing MB) are created *via* a flow focusing geometry using a fluorinated hydrocarbon oil, FC-40, as the continuous phase. The droplets of  $\sim 50$  nL travel through the microreactor in 45 s with a total flow rate of  $7.5 \mu\text{L min}^{-1}$ .

For the hydrogenation to take place, the gaseous  $\text{H}_2$  has to travel from the gas channels through the PDMS wall and the fluorinated oil (FC-40) continuous phase before it reaches the ethanol droplet. It is important that the  $50 \mu\text{m}$  thick PDMS wall does not interfere too much with the  $\text{H}_2$  diffusion in ethanol, to prevent a change in reaction kinetics due to mass transport limitations. Fig. 3a schematically shows which factors influence the concentration of  $\text{H}_2$  in the ethanol droplet. For a flow with spherical droplets, the continuous phase is wetting the channel walls, whereas the droplet phase is non-wetting. This leads to the formation of a thin stagnant film of oil between the ethanol droplet and the PDMS wall. Fig. 3b shows that the droplets in the microreactor system are slugs rather than spherical droplets.<sup>24</sup> Based on the small contact angle between the non-wetting slug and the wall, we assume that there is a nanometer thick (but invisible) layer of FC-40 between the droplet and the PDMS. Since FC-40 has a high  $\text{H}_2$  gas permeability (similar to PDMS),<sup>25</sup> consequently there is no diffusion limitation caused by the FC-40 film. From this, we concluded that  $\text{H}_2$  must first diffuse into and through the PDMS wall before it can enter the ethanol droplet containing the catalyst. From Table 1, it can be observed that the diffusivity ( $D$ ) of  $\text{H}_2$  through



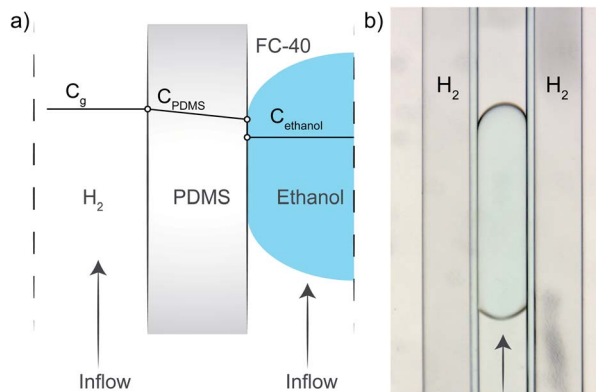


Fig. 3 Simplified/schematic representation of the  $H_2$  concentrations in the different compartments of the microreactor (a), and a microscope image of one droplet (b). The ethanol droplets partially wet the polydimethylsiloxane (PDMS) wall and are therefore considered as 'slugs'. Due to the high diffusivity of  $H_2$  through PDMS ( $1.4 \times 10^4 \text{ m}^2 \text{ s}^{-1}$ ), with respect to ethanol ( $1.49 \times 10^2 \text{ m}^2 \text{ s}^{-1}$ ), the limiting diffusion step is for  $H_2$  to enter the ethanol droplet.<sup>27,28</sup>

**Table 1** Diffusion ( $D$ ) and solubility ( $S$ ) parameters of  $H_2$  in polydimethylsiloxane (PDMS) and ethanol

	$D \text{ (m}^2 \text{ s}^{-1}\text{)}$	$S \text{ (}\times 10^5 \text{ Pa)}$
PDMS	$1.40 \times 10^4$ (ref. 27)	20.3 (ref. 27)
Ethanol	$1.49 \times 10^2$ (ref. 28)	452 (ref. 29)

PDMS is a factor 100 higher than that of  $H_2$  through ethanol. Inside the PDMS wall and the ethanol droplet, the solubility follows Henry's law. The solubility ( $S$ ) parameter of  $H_2$  is 200 times higher in ethanol compared to PDMS.

The high diffusivity, but low  $H_2$  solubility in PDMS results in the fast transport of  $H_2$  through the PDMS membrane. In ethanol, the  $H_2$  diffusivity is lower, but its solubility is higher compared to PDMS, leading to  $H_2$ -saturated ethanol droplets. Therefore, it is assumed that the PDMS does not introduce significant diffusion limitations. Within the droplets, chaotic advection causes fast mixing,<sup>26</sup> leading to a homogeneous and constant  $H_2$  concentration.

Fig. 3a sketches the situation where the ethanol droplet is completely saturated with  $H_2$  and homogeneously mixed, therefore there is a discontinuity in the simplified representation at the PDMS-droplet interface. When the ethanol concentration in the droplet becomes lower because the  $H_2$  reacts with MB on the Pd catalyst,  $H_2$  can diffuse from the PDMS and dissolve into the ethanol droplet again.

### Catalytic hydrogenation of methylene blue

The developed PDMS microreactor was tested for the hydrogenation of MB (blue) into leuco-MB (colorless). As the catalyst, we have opted for Pd supported on hollow  $\text{SiO}_2$  spheres  $40 \mu\text{m}$  in diameter. We have selected Pd as the active metal



because of its known activity towards hydrogenation reactions. An added benefit is its stability in air. After a reduction step, the formed Pd particles are not prone to oxidation and can, therefore, easily be transferred through or stored in air. Our microreactor setup lacks options for *in situ* catalyst reduction steps, thus a stable and robust catalyst system is vital. The hollow core of the silica particles lowers their weight by a factor 10 approximately (bulk density of  $0.2 \text{ mg L}^{-1}$  vs. skeletal density  $2.5 \text{ mg L}^{-1}$ ), to improve their flow through the microchannel. In general, catalyst particles with much higher densities than the surrounding liquid have difficulty moving inside microfluidic channels, as they tend to sink to the bottom due to gravity.<sup>30</sup> Once stuck at the channel bottom, heavy catalyst particles cannot easily be removed because it is expected that they stick to the PDMS. Since catalyst support materials often have a higher density compared to the liquid reactants, this sinking is an important factor in microfluidic single particle diagnostics. The prepared catalyst was characterized with scanning electron microscopy (SEM), X-ray diffraction (XRD), transmission electron microscopy (TEM) and  $\text{N}_2$ -physorption. SEM and TEM images can be found in Fig. 4a and b, respectively. With SEM, the external surface and morphology was investigated. It was found that the structure and shape of the spherical  $\text{SiO}_2$  particles was intact after the preparation of the catalyst. The  $40 \mu\text{m}$  porous  $\text{SiO}_2$  microparticles were too big to analyze with TEM, but after crushing them, the remaining fragments could be analyzed to determine the Pd dispersion and nanoparticle size. On average, the Pd nanoparticles are  $\sim 25\text{--}30 \text{ nm}$ . The particle size distribution is large, but their dispersion over the  $\text{SiO}_2$  support is homogeneous, as can be seen in Fig. 4d. In the XRD (Fig. 4c), diffraction peaks allocated to crystalline Pd were found, and with the Scherrer equation using the Full Width Half Maximum (FWHM) of the XRD

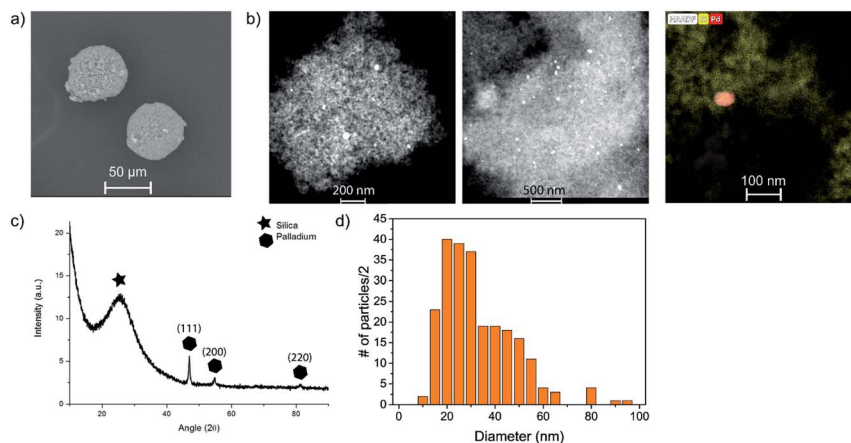


Fig. 4 Scanning electron microscopy (SEM) images in backscatter mode of the catalyst prepared (a), shows an intact spherical shape and large Pd clusters. Transmission electron microscopy (TEM) images in STEM mode (b), of the crushed spheres show homogeneously distributed Pd nanoparticles. In the X-ray diffraction (XRD) pattern (c), peaks corresponding to silica and Pd are assigned. The particle size distribution (d), as determined from multiple TEM images is large. The total number of measured particles  $\sim 130$ . Two sides were measured for each particle: the values on the y-axis should be divided by two for the actual number of particles measured.



peaks, an average crystallite size of  $\sim 25$  nm could be determined. The BET surface area of the particles was calculated to be  $\sim 180$  m<sup>2</sup> g<sup>-1</sup>. To perform the hydrogenation reaction inside the droplet microreactor, a setup was built with a vertically mounted syringe pump to benefit from gravitational forces acting on the catalyst particles. A shaker was connected to the tip of the syringe, inducing vibrations in the tubing and a stir bar was added to the syringe to disperse the particles in the ethanol solution. Both measures are a precaution against particle sedimentation in the syringe or tubing. A detailed image of the setup is given in Fig. 5. The droplets were followed with optical microscopy to monitor the color change of all droplets that contained catalyst particles.

As part of the experimental setup, the catalyst particles were added to the MB-ethanol syringe prior to starting the flows. Since no reaction can happen before the particles have entered the microreactor, due to the absence of H<sub>2</sub> in the glass syringe, we have a well-defined starting time for the reaction ( $t_0$ ). Interestingly, after adding the Pd/SiO<sub>2</sub> to a 20 ppm solution of MB in ethanol, a rapid color change of the fresh catalyst was observed from brown to blue, due to the adsorption of MB. Fig. 6 shows two microscopy images of the catalyst before and after adsorption of MB. This color change is advantageous for the catalyst characterization: the blue particles should return to their original brown color upon hydrogenation. This color change effect is expected to be more pronounced compared to a discoloration of the light blue color of the MB droplet itself and therefore easier to detect. As a proof of concept experiment, droplets containing blue Pd/SiO<sub>2</sub> particles were followed over time, without any liquid flow, leading to stagnant droplets. It can be seen in Fig. 7 that after starting the H<sub>2</sub> flow the red/green/blue (RGB) values, representing the color of the particle, reach a plateau over time. During the experiments a H<sub>2</sub> sensor (Industrial Scientific Pro Gas Badge) is put next to the microreactor for safety reasons. The minimum amount it can detect is 1 ppm and during all experiments, this level is never reached.

These results show the working principle of the PDMS hydrogenation microreactor: H<sub>2</sub> can diffuse through the PDMS wall and dissolves in the reactant droplet. However, for single particle diagnostics, these experiments should be

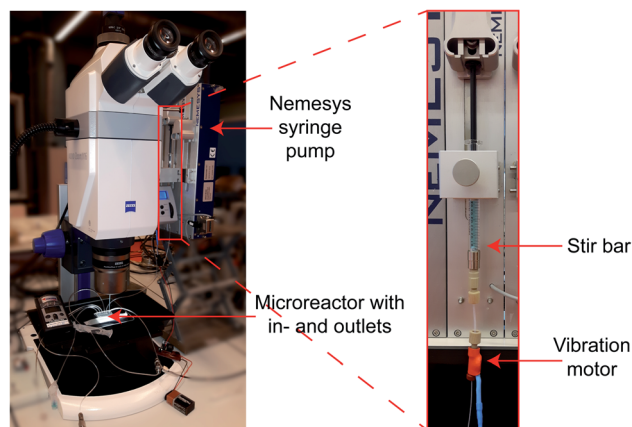


Fig. 5 Images of the microscope setup with vertical syringe pump, syringe with stir bar and vibration motor for optimal conditions to encapsulate solid particles in droplets.



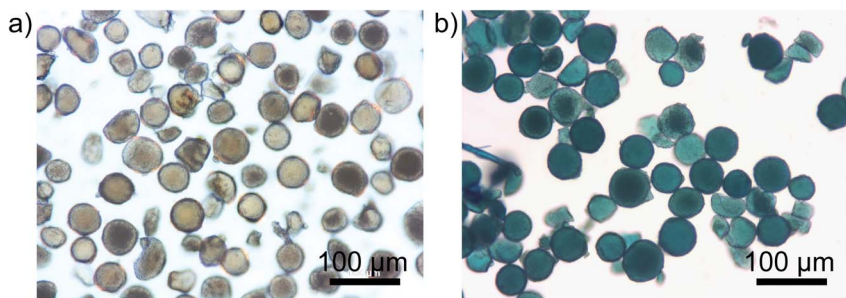


Fig. 6 Two optical images of Pd/SiO<sub>2</sub> before (a) and after (b) adding them to 20 ppm methylene blue (MB) in ethanol. The blue color is caused by adsorption of MB on the surface of the solid particles.

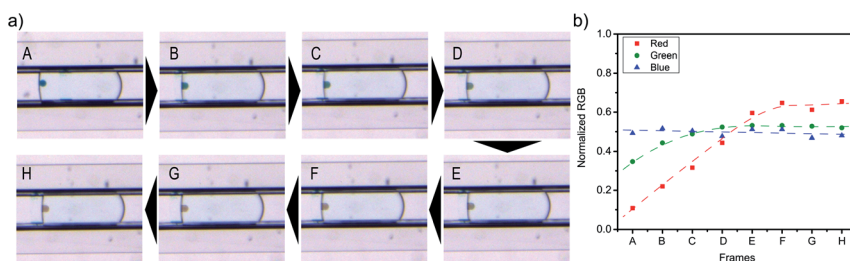


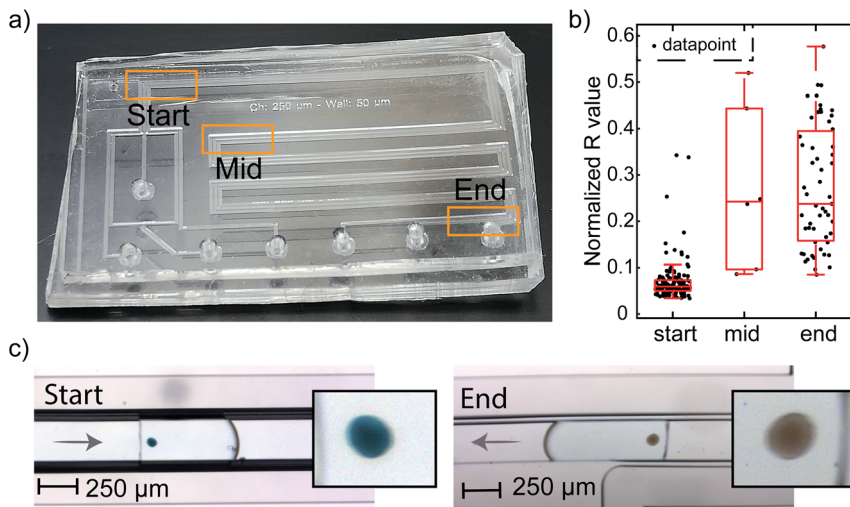
Fig. 7 Separate frames (a); with an interval of 1.3 s each, going from A to H) show a rapid particle discoloration from blue to brown when the droplets are exposed to a H<sub>2</sub> flow via the adjacent gas channels. The plot (b) shows the changes in the RGB channels per frame.

performed in flow. Therefore, the same hydrogenation of MB was performed at a total flow of 7.5  $\mu\text{L min}^{-1}$ , leading to a droplet formation rate of 1 droplet per s and a residence time of 45 s in the microchannel. The analysis of particles in flow is more difficult compared to the static experiment. Therefore, three monitoring regions for characterization were defined at the start, middle and the end of the microchannel (Fig. 8a). In this way, all particles can be analyzed for three different reaction times. Fig. 8c shows two sets of images of Pd/SiO<sub>2</sub> in a MB–ethanol droplet recorded at the start and end regions.

Indeed, the blue color of the particles at the start of the channel has disappeared towards the end of the channel. From these results, we conclude that H<sub>2</sub> also permeates the PDMS wall, dissolves in the ethanol droplet and participates in the reaction when the droplets experience a flow. Thus, our microreactor design is working: within the 45 s residence time ( $t_r$ ) in the microchannel, the MB hydrogenates to the colorless leuco-MB. To support these findings, control experiments without H<sub>2</sub> or the active catalyst are performed: the particles stay blue during their residence in the microchannel. These results are shown in Fig. S1.† The color change is most visible for the more concentrated MB, adsorbed on the particles. Empty droplets contain the same initial concentration of MB as droplets containing a particle. However, the concentration in the droplets is too low to be visible in the images and both empty droplets and particle containing droplets appear ‘white’ and have no discernable color change in the RGB level. With the







**Fig. 8** The measurement positions on the microreactor are shown in (a), where the normalized red ( $R$ ) levels with respect to the background polydimethylsiloxane (PDMS) signal of particles in droplets at the start, middle and end of the reaction channel are given in a boxplot (b). Particles are blue at the start of the reaction channel ((c), left) and reddish/brown near the end of the reaction channel ((c), right) due to hydrogenation of methylene blue (MB) to the colorless leuco-MB. The arrow indicates the flow direction. The number of particles measured at the start, middle and end are 128, 6 and 55, respectively. The horizontal spread in data points is done for visibility purposes only and contains no other information.

presented setup, the encapsulation of particles in droplets was relatively straightforward. However, fluctuating concentrations of particles near the inlet of the microreactor often led to multiple particles per droplet, as can be seen in Movies M1–M4.†

For the flow experiments, a statistically relevant analysis was performed by monitoring the RGB levels of the acquired movies in Matlab. The movies were screened for the presence of catalyst particles in a droplet using a small window at three positions on the microreactor (start, middle, and end) as indicated in Fig. 8a. Fig. S2† shows three examples of particles found at these different locations. Matlab processing was used to find the frames containing particles. The RGB values of all particles were collected using a line profile positioned perpendicular to the flow direction. From these line profiles, it can be clearly seen that the particles have lower RGB values than the background. The lowest 10 RGB values of each particle are summed and averaged to obtain the RGB value for a particle at each position. This tracking allowed for an evaluation of the RGB levels for each particle. Fig. 8b shows a boxplot of red levels for multiple particles at the start, middle and at the end of the flow channel. The datapoints obtained from the Matlab script are plotted on top of the boxplot. Only the red value is shown, as that is the value with the most distinctive change upon discoloration, as shown in Fig. 7. The values are normalized with respect to a reference position on the PDMS, denoted as background. From this plot, the color change of Pd/SiO<sub>2</sub> catalyst particles flowing through the microchannel is clearly visible. At the start, the blue particles show low red values, whereas the brown



particles at the middle and end show high red values. For the middle region, only a few particles (*i.e.*, 6) could be measured, leading to less sound statistics. However, due to the similar red color value in the box plot at the middle compared to the end position, it is concluded that the hydrogenation has already been completed at the middle position (54 mm after droplet formation and exposure to  $H_2$ ).

Interestingly, this hydrogenation is a fast reaction and does not need the full residence time of 45 s (when using a total flow of  $7.5 \mu\text{L min}^{-1}$ ) in the microreactor to be completed. Due to the gradual color change from blue to brown, it is difficult to pinpoint the exact position in the microreactor where the hydrogenation is completed, but it is approximated that the reaction is completed within 10 s, because the red value of the particle does not change after this point, as shown in Fig. 7, from frame F onwards. Movies M1 to M4† show hydrogenations at different

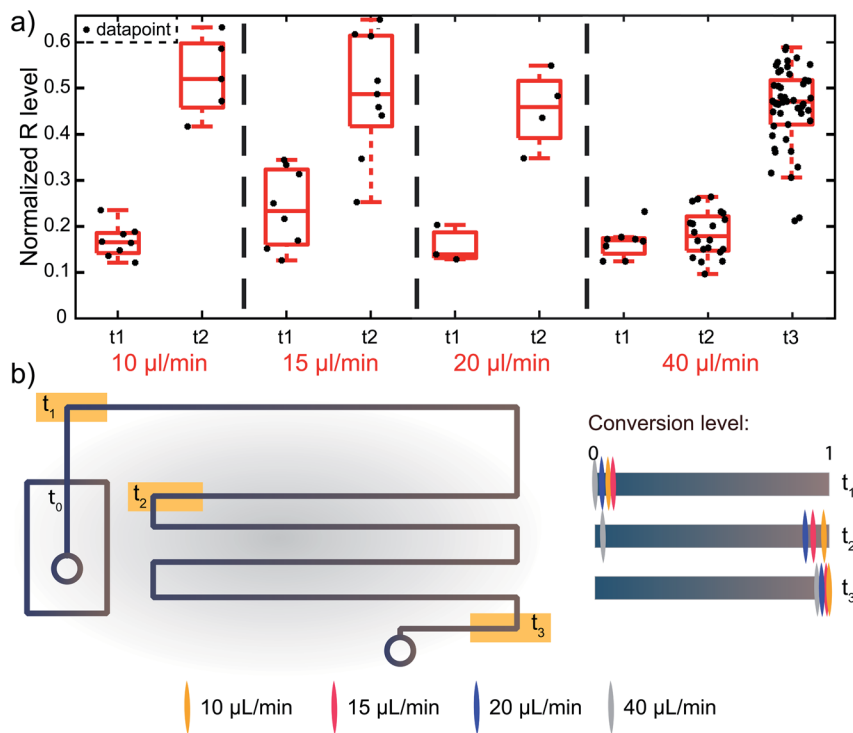


Fig. 9 The start ( $t_1$ : 6.8 mm after droplet formation), middle ( $t_2$ : 53.8 mm after droplet formation) and end ( $t_3$ : 123.4 mm after droplet formation) regions are analyzed at different flow rates and a boxplot of the red values for all flow rates and positions is shown. The total flow rates are given, the ratio of the continuous phase (CP) vs. droplet phase (DP) phase is 1 : 1. For the fastest rate (total flow of  $40 \mu\text{L min}^{-1}$ ) also the end region is analyzed, because for this flow rate there is a clear difference between the end and middle. The graphical representation of the results (b) shows that at higher flow rates, the reaction is completed more down-stream in the microchannel. The number of particles ( $n$ ) analyzed for each flow rate and position are  $n = 8$  and  $n = 5$  at  $t_1$  and  $t_2$ , respectively, for  $10 \mu\text{L min}^{-1}$ ;  $n = 8$  and  $n = 9$  at  $t_1$  and  $t_2$ , respectively, for  $15 \mu\text{L min}^{-1}$ ;  $n = 3$  and  $n = 4$  at  $t_1$  and  $t_2$ , respectively, for  $20 \mu\text{L min}^{-1}$ ; and  $n = 8$ ,  $n = 20$  and  $n = 46$  at  $t_1$ ,  $t_2$  and  $t_3$ , respectively, for  $40 \mu\text{L min}^{-1}$ . The horizontal spread in datapoints is done for visibility purposes only and contains no other information.



total flow speeds and indicate the position where the hydrogenation is complete. For a total flow of  $7.5 \mu\text{L min}^{-1}$ ,  $\sim 1$  droplet per second passes the analysis region. For high-throughput experimentation it holds that it is better to use a higher flowrate. Increasing the flowrate to  $40 \mu\text{L min}^{-1}$  leads to larger, but less stable droplets (Movie M4†), but the hydrogenation still takes place and the droplet size does not seem to affect the reaction kinetics. Fig. 9 shows the red color values for the start and middle of the reaction channel, for four different flow rates. It can be seen that up to a total flow of  $20 \mu\text{L min}^{-1}$  (10/10, w/o), the reaction has completed by the mid-region of the microreactor. For a total flow of  $40 \mu\text{L min}^{-1}$  (20/20, w/o), the residence time of a droplet in the microreactor is decreased to 8.5 s. At this flow rate, the full channel length is needed for completion of the reaction, meaning that the reaction time for the hydrogenation of MB, at these conditions, is  $\pm 8$  s. Therefore, the end position is also measured at this flow rate.

## Conclusions

In this work, we show the proof of concept of a PDMS microreactor for high-throughput, multiphase catalytic reactions, demonstrating the liquid-phase hydrogenation of MB. A liquid channel with Pd/SiO<sub>2</sub> particles of 40  $\mu\text{m}$  encapsulated in droplets containing 20 ppm MB in ethanol are flanked by two gas channels with H<sub>2</sub>, separated with 50  $\mu\text{m}$  PDMS walls. Due to the high permeability of PDMS, H<sub>2</sub> diffuses into the liquid channels and facilitates the Pd-catalyzed hydrogenation of MB at room temperature. In approximately 8 s the reaction completes, as concluded from the discoloration of the particles in droplets going from blue (due to adsorbed MB) to brown (their original color). Droplets containing single particles could be analyzed individually to allow for the diagnostics of multiple heterogeneous catalyst particles, as opposed to the use of packed-bed or wall-coated reactors. This newly developed microreactor has, therefore, proven to be useful for the single particle diagnostics of catalyst particles in complex multiphase reactions. With this we have a new diagnostics tool in hand to improve the statistical relevance of single catalyst particle analysis and bridge the gap towards bulk characterization. In addition, a safe and relatively easy method has been demonstrated to work with H<sub>2</sub>, as no H<sub>2</sub> leak was detected by a commercial sensor during any of the experiments, and only small amounts of gas are involved. Furthermore, by placing the PDMS chip on a heating stage, reactions at elevated temperatures can be performed. The thermal stability of crosslinked PDMS allows for heating up to 400 °C before it starts to degrade,<sup>31</sup> but in this situation more problems arise, such as the boiling of solvents or a non-uniform heating of the microreactor. In addition, the optical properties of PDMS allow reactions to be monitored with visible (laser) light, therefore allowing users to perform *in situ* UV-vis or Raman spectroscopy. These techniques should be optimized in a way that they can work fast and can detect individual droplets at high flow rates. Finally, more sophisticated microreactor designs with microfluidic droplet sorters can be implemented to sort the catalyst particles of interest.

## Experimental

### Microreactor fabrication

Microreactors were fabricated in PDMS with standard soft- and photolithography methods, as described elsewhere.<sup>32</sup> The SU-8 mold was made in the



cleanroom of the MESA+ Nanolab at the University of Twente. SU-8 photoresist was spin-coated on a silicon substrate (P-type <100>, single side polished, 500  $\mu\text{m}$ ) and patterned with a photomask by exposure to UV-light. Structures with a height and width of 250  $\mu\text{m}$  for both the gas channels and the liquid channel were created. The spacing between the gas and liquid channel is 50  $\mu\text{m}$ . This mold was used to fabricate the inverse replica in PDMS. A liquid mixture of the base- and curing agent (10 : 1, Sylgard 184, Dow Corning) was degassed and poured over the molds. After thermally curing the PDMS at 60  $^{\circ}\text{C}$  for 3 h, the layer was peeled from the master. Inlet and outlet holes of 1 mm diameter are punched into the PDMS after which it was treated in an  $\text{O}_2$  plasma oven for 2 min and subsequently bonded to another flat layer of PDMS acting as a bottom substrate, followed by heating the assembled microreactor to 60  $^{\circ}\text{C}$  for 30 min. Bonding of the structured PDMS slab to the flat bottom slab had to be carried out carefully, to prevent distortion and collapse of the relatively flexible thin PDMS walls. A chip yield of approximately 75% has been achieved. In total, 20 chips have been fabricated and tested.

### Catalyst preparation and characterization

Pd was deposited on hollow spherical 40  $\mu\text{m}$   $\text{SiO}_2$  particles (Materium450) *via* incipient wetness impregnation of a 6 mM solution of  $\text{PdCl}_2$  in ethanol. After an equilibrium period of 8 h, the ethanol was slowly evaporated by heating the mixture at 60  $^{\circ}\text{C}$ . After carefully drying the particles, the sample was calcined and reduced in a flow of air and  $\text{H}_2$  consecutively. The prepared catalyst was characterized with powder XRD, SEM and  $\text{N}_2$ -physisorption. The crystalline phase of the Pd/ $\text{SiO}_2$  catalyst was measured using a Bruker-AXS D2 Phaser equipped with a Co  $K\alpha$  radiation source ( $\lambda = 1.78897 \text{ \AA}$ ) with  $2\theta$  from 10–90 $^{\circ}$  (increments of 0.1 and scan steps of 1 s). SEM images were collected in back-scattered electron mode using a Phenom table top machine. For TEM, a diluted sample of the crushed Pd/ $\text{SiO}_2$  in ethanol was drop-casted on lacey copper carbon grids (van Loenen Instruments, 300 mesh grid). The samples were analyzed with a ThermoFisher Scientific Talos F200X equipped with an X-FEG electron source operated at 200 kV. Energy-dispersive X-ray spectroscopy (EDX) images were made using the same apparatus with a Super-X<sup>TM</sup> EDX detector in STEM mode. A Micromeritics TriStar 300 V6.08 A was used for  $\text{N}_2$ -physisorption measurements at 77 K. The BET equation was used to obtain the specific surface areas. The catalyst particles were added to a syringe with 20 ppm MB in ethanol at a low concentration: 1 mg in 1 mL. This low concentration was needed to increase the possibility of having one particle per droplet, as the amount of particles per droplet follows the Poisson distribution.<sup>33</sup> The blue MB quickly adsorbs on the surface of the silica spheres, leaving blue particles in a pale blue liquid. After entering the microchannel, the droplets with blue Pd/ $\text{SiO}_2$  particles flow in between the two gas channels of the  $\text{H}_2$  supply.

### Microfluidic reaction: chemicals and materials

The microreactor was designed with three parallel channels, a center-channel for the liquids and two surrounding channels for the gas (all channels have a depth and width of 250  $\mu\text{m}$ ).  $\text{H}_2$  was flushed through the gas channels at 0.75  $\text{mL min}^{-1}$



total flow (using a Bronkhorst mass flow controller of 0–1 mL min<sup>-1</sup>). In the liquid channel 20 ppm MB in ethanol droplets (with the added catalyst) in a continuous phase of the fluorinated FC-40 oil were created. FEP polymer tubing from IDEX-HS (ID = 500 μm, OD = 1/16") in combination with Hamilton syringes (1000 μL) and a Nemesys (Cetoni) syringe pump were used to create droplets. Flow rates were varied between 2.5 to 20 μL min<sup>-1</sup> and 5 to 20 μL min<sup>-1</sup> for the ethanol (dispersed phase) and fluorinated oil (continuous phase), respectively. Microscopy images were made and data acquisition was done with a Zeiss Axio Zoom.V16 microscope using bottom illumination, equipped with a PlanNeoFluar Z 1× zoom objective and an Axiocam 105 color camera.

## Matlab data analysis

All movies acquired were screened for the presence of catalyst particles in a droplet, using a small window at three positions of the microreactor (start, middle, and end). Fig. S2† shows three examples of particles found at these locations. To find the center of the particles, all red values in the window are added column-wise and then multiplied by -1. The result is the bottom row of images in Fig. S2.† Here it can be seen that the position of the particle results in a peak, because the red values are significantly lower for the particle than for the background. The presence of a droplet interface also results in a peak, but by looking at the width of the peak as well, they can be filtered from actual particles. The findpeaks function in Matlab is used to find the position of the particle peak. With this position a line (yellow line in Fig. S2†) can be drawn over the middle of the particle, plotting the RGB values along this line, as seen in the top row of images in Fig. S2.†

## Conflicts of interest

There are no conflicts to declare.

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