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Recent progress in monolithic two-terminal perovskite-based triple-junction solar cells

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Multi-junction solar cells are the most famous approach to overcome the power conversion efficiency (PCE) limit of single-junction solar cells. Metal halide perovskite absorber materials offer low-cost fabrication and tunable bandgap that make them suitable candidates for multi-junction applications. Perovskite-based dual-junction solar cells have already shown impressive PCE improvement in recent years. As a next step, triple-junction structures can allow for further PCE increase; however, research on triple-junction solar cells with perovskite materials is still at an early stage. In this review, we present the status of three monolithic perovskite-based triple-junction technologies available: perovskite/perovskite/silicon, perovskite/perovskite/perovskite, and perovskite/perovskite/organic solar cells. First, an overview of the potential of these solar cell types based on simulation is given. Further, a summary of scientific and experimental challenges in the field as well as strategies to achieve suitable absorber materials and contact layers that can be implemented in these structures are presented. Finally, global cell characterization of triple-junction solar cells together with a guideline on correct measurement of this type of solar cells are discussed.

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Broader context

Tackling climate change requires transformation of global energy from conventional fossil fuels toward cleaner sources. This is achievable through electrification of energy demand as well as increasing the share of renewable sources for electricity production. Among all the renewable energy sources, photovoltaics (PV) plays a crucial role. Even though the electricity share of the PV is only 4.5%, its world installed capacity has reached 1 TWdc and is further growing. Entering the terawatt scale raises the need for reducing the cost of PV technology. Therefore, increasing the efficiency of the PV module is more important than ever. To do so, multi-junction solar cells have proven to be the most attractive option, yet development of efficient and low-cost subcells is necessary. In this regard, metal halide perovskite is one of the most promising candidates with perovskite/silicon holding the dual-junction record efficiency. Improving this efficiency further is possible by increasing the number of junctions to three as it has been demonstrated by III-V semiconductor materials. Realizing the triple-junction solar cell with perovskite material comes with several challenges and requirements which we have outlined in this review.

1. Introduction

The most famous approach to overcome the efficiency limit of single-junction solar cells and achieve efficient usage of the solar spectrum is the use of multi-junction solar cells. In this approach, solar cells with different bandgaps are stacked on top of each other in a bandgap descending order with the highest

bandgap solar cell facing the sun. This way, the top solar cell absorbs the high energy photons up to its bandgap and the lower energy photons are transmitted to reach the underlying subcells with lower bandgaps. This reduces the thermalization losses and leads to better harvesting of the solar spectrum. Fig. 1a shows this principle for the case of triple-junction solar cells.

According to simulation by Philipps *et al.*, the highest theoretical PCE that can be achieved in a detailed balance limit (Auger recombination is not taken into account) by a dual-junction solar cell is 45.9% under Air Mass 1.5 global (AM 1.5g) spectrum.¹ This PCE limit can be exceeded by increasing the number of junctions in a solar cell. However, as shown in Fig. 1b the incremental increase becomes lower towards more junctions. Furthermore, the additional junctions introduce new

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Fig. 1 (a) Use of the solar spectrum by a triple-junction solar cell consisting of a silicon bottom cell, a 1.50 eV middle cell (e.g. GaInAsP), and a 2.00 eV top cell (e.g. AlGaInP). The transmission and thermalisation losses are reduced compared to single-junction and dual-junction solar cells. (b) Theoretical efficiency of multi-junction solar cells in the radiative limit as a function of the number of junctions. The optimum bandgap combination is given for the maximum PCE under the AM 1.5g spectrum. The gain in efficiency becomes lower by increasing the number of junctions. Data taken from ref. 1.

challenges in terms of processing, choice of materials and interaction between the layers. Thus, triple-junction solar cells are a reasonable approach to achieve a good balance between efficiency potential, processing, and device complexity.

So far, highly efficient triple-junction solar cells are made of III–V semiconductor materials and are commercially available for concentrator photovoltaic and space application. Triple-junction solar cells using III–V materials reached 39.5% efficiency for a gallium indium phosphide (GaInP) top cell, gallium indium arsenide (GaInAs)/gallium arsenide phosphide (GaAsP) quantum well middle cell, and GaInAs bottom cell under the AM 1.5g spectrum.² This exceeded the previous record of a sextuple-junction solar cell and made the triple-junction solar cell the most efficient non-concentrated terrestrial PV technology to date. Cells made from III–V compound semiconductor absorbers are highly efficient thanks to the low defect density that can be achieved in the single-crystalline materials and due to the direct

nature of their bandgap. However, they require expensive deposition techniques such as metalorganic or hydride vapor phase epitaxy (MOVPE, HVPE) or molecular beam epitaxy (MBE) to achieve the required high crystal quality. The high production costs prevent these technologies from entering the terrestrial photovoltaic markets and consequently limit them to concentrator photovoltaic and space application where the high efficiency is the decisive factor. Several works have been done to couple III–V materials on a silicon bottom cell to reduce the cost and to benefit from the fact that the photovoltaic (PV) market is dominated by crystalline silicon. For the first time in 2013 Derendorf *et al.* reported successful integration of GaInP/GaAs/silicon in a triple-junction structure using wafer bonding.³ A record efficiency of 35.9% was achieved in 2021 for this type of solar cell.⁴ Technologically, wafer bonding is not favorable as it is an expensive serial process and requires an extra chemical-mechanical polishing (CMP) step.⁵ However, direct growth of III–V materials



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Fig. 3 Theoretical efficiencies in the radiative limit for triple-junction solar cells for a bottom cell absorber with a bandgap of (a) 1.00 eV, (b) 1.10 eV, (c) 1.20 eV, and (d) 1.30 eV. The optimum top and middle cell bandgaps in each case are (a) 1.94 eV and 1.42 eV, (b) 2.00 eV and 1.49 eV, (c) 2.06 eV and 1.57 eV, and (d) 2.13 eV and 1.66 eV.

Table 1 The optimum bandgap combinations to achieve highest theoretical PCE in a triple-junction solar cell with respect to the choice of the bottom cell

Bottom cell (eV)	Middle cell (eV)	Top cell (eV)
1.00	1.42	1.94
1.10	1.49	2.00
1.20	1.57	2.06
1.30	1.66	2.13

be current matched in the field as the spectra and temperature variations affect the bandgaps of the subcells in different ways.^{30–32} Furthermore, in a two-terminal configuration, the voltage of the final device is the sum of the voltages of all subcells. This means that to ensure highest voltage in the multi-junction solar cell, first the voltage deficit (*i.e.*, $V_{\text{deficit}} = E_g/q - V_{\text{OC}}$, where E_g is the bandgap, q is the electron elementary charge and V_{OC} the open-circuit voltage) of the individual subcells should be minimized and second lossless interconnection layers between the subcells are required.

So far, this introduction covered the potential of triple-junction solar cells based on simulation. Realization of such photovoltaic devices with maximum possible output in real lab conditions demands consideration of practical factors and limitations. Beyond optimization of individual layers, the processing sequence and layer interactions of the whole multilayer stack strongly influence the final device performance. Thus, a thorough analysis and comparison of the approaches taken for realizing the proof of

concepts of these new technologies as well as follow-up studies are needed to allow fast technological development. This paper discusses the progress in engineering of monolithic perovskite-based triple-junction solar cells comprehensively. First, device architectures and interlayers used in current reported perovskite-based triple-junction solar cells including their photovoltaic parameters are summarized. Then, a review of perovskite absorbers suitable for middle cell and top cell together with details on bandgap tuning of perovskites, different deposition techniques, challenges associated with each type of the perovskite absorber, as well as possible strategies to tackle them are presented. In addition, we discuss the available materials and methods that are used for the recombination layers between perovskite subcells. Lastly, precise characterization of triple-junction solar cells based on the publications from current state-of-the-art III-V triple-junction technologies is addressed. Special emphasis is placed on potential uncertainties arising from measurements, along with suggestions on how to avoid them in research laboratories.

2. Perovskite-based triple-junction solar cells: categories and status

A monolithically integrated multi-junction solar cell consists of many layers processed sequentially on top of each other with different deposition methods. Process compatibility of each layer with its underlying layer is therefore of great importance.





Fig. 4 Simulated external quantum efficiency (EQE) and current density–voltage (jV) curves for maximum practical PCE (a) 36.6% for an all-perovskite triple-junction solar cell with perovskite's bandgaps of 1.22 eV, 1.58 eV, and 2.04 eV for the subcells and (b) 38.8% for a perovskite/perovskite/silicon triple-junction solar cell with bandgaps of 1.44 eV and 1.95 eV for perovskite subcells. Reproduced with permission from ref. 27, Copyright © 2017, American Chemical Society.

For example, solvent orthogonality, possible processing damage as well as thermal budget of the bottom layers should be considered when processing subsequent layers. Moreover, addition of each subcell increases the number of layers, which consequently introduces new challenges.

Multi-junction solar cells can be divided into superstrate or substrate configuration (Fig. 5) depending on the type of bottom solar cell technology. In case of thin film bottom solar cells, such as in all-perovskite and perovskite/perovskite/organic solar cells, the superstrate configuration is used; solar cells are deposited on a glass (or foil) which is flipped and facing the sun in the final device. In case of wafer-based bottom solar cells, such as in perovskite/perovskite/silicon, the substrate configuration is used; the bottom cell wafer itself acts as the substrate and subsequent layers are processed on top. Consequently, the processing order of the absorbers is different. In the superstrate configuration, perovskites are processed in bandgap descending order and highest restrictions concerning process compatibility apply for the low bandgap perovskite absorber. In the substrate configuration, perovskite middle and top cells are processed successively on top of the bottom solar cell wafer. Highest

restrictions concerning compatibility, such as annealing temperature and possible solution damage to the underlying layers apply for the processing of high-bandgap perovskite top cell. One example is high-temperature annealed nickel oxide (NiO_x), that cannot be implemented as charge transport layer on top of another perovskite subcell. In addition, the first processed subcell (high bandgap in the superstrate and low bandgap in substrate configuration) must sustain several harsh conditions involved in the deposition of the top layers such as annealing steps, sputtering, *etc.* More discussion on fabrication of respective perovskite layers is presented in Section 3 and 4.

Moreover, perovskite solar cells can be classified by their order of deposition of the electron (n) and hole (p) transport and the perovskite absorber (i) layers into n–i–p (electron transport layer (ETL) deposited first) and p–i–n (hole transport layer (HTL) deposited first) device architectures. The work on perovskite/silicon tandem solar cells started on n–i–p architecture.³³ However, the research focus changed toward the p–i–n structure due to an optically more favorable front contact, ease of fabrication and upscaling.

Similarly, the very first report on all-perovskite triple-junction solar cells in 2019 by McMeekin *et al.* had an n–i–p





Fig. 5 Schematic illustration of monofacial perovskite-based triple-junction solar cells with (top) superstrate configuration and (bottom) substrate configuration. Perovskite subcells are in p–i–n architecture. Some of the common materials for each layer together with their deposition techniques are shown. The processing of substrate configuration starts with bottom cell (lowest bandgap subcell) while for superstrate configuration the top cell (the highest bandgap subcell) is processed first. The main limitations of the processes are highlighted.

configuration implementing $\text{FA}_{0.83}\text{Cs}_{0.17}\text{Pb}(\text{Br}_{0.70}\text{I}_{0.30})_3$ (1.94 eV), MAPbI_3 (1.55 eV) and $\text{MAPb}_{0.75}\text{Sn}_{0.25}\text{I}_3$ (1.34 eV) perovskite absorbers.²³ This work remains the only perovskite-based triple-junction solar cell with n–i–p architecture. Another exceptional approach regarding solar cell fabrication was that all the layers except for the silver electrode were solution-processed; even the indium tin oxide (ITO) recombination layer which is usually deposited *via* sputtering was replaced by spin coated ITO nanoparticles. Their strategy to overcome solvent compatibility issue was to change the conventional mixture of dimethylformamide/dimethyl

sulfoxide (DMF/DMSO) as perovskite solvent to a new acetonitrile/methylamine (ACN/MA) solvent system for both low bandgap and middle bandgap perovskites. However, the change in solvent system yielded a reduced PCE. The triple-junction solar cell reached a PCE of 6.7% with an open-circuit voltage (V_{OC}) of 2.70 V. The limited PCE mainly arose from low short-circuit current density (j_{SC}) of 8.3 mA cm^{-2} limited by the low bandgap bottom cell, as well as a low fill factor (FF) of 43.0%. Other possible factors limiting the performance of this structure could be high parasitic absorption, especially in the 60 nm thick





Fig. 6 Structure evolution and cross sectional SEM images of perovskite-based triple-junction solar cells. Reproduced with permission from ref. 14–17, 22–26. Copyright © 2018, American Chemical Society. Copyright © 2019 Published by Elsevier Inc. Copyright © 2020, Wang *et al.*, Published by Springer Nature, Copyright © 2020, American Chemical Society, Copyright © 2022, American Chemical Society, Copyright © 2022, American Chemical Society, Copyright © 2023, Wang *et al.* under exclusive licence to Springer Nature Limited, Copyright © 2023, American Chemical Society, Copyright © 2023 Heydarian *et al.*, Published by American Chemical Society.

bandgap of the top cell is kept at 1.80 eV, the middle cell bandgap should be lowered to ~ 1.40 eV to achieve current matching at a j_{SC} of ~ 12.2 mA cm $^{-2}$ for a flat silicon bottom cell and a $j_{SC} > 13.0$ mA cm $^{-2}$ for a both-side textured bottom cell.

In 2022, Zheng *et al.* achieved 20.1% PCE for a perovskite/perovskite/silicon triple-junction solar cell.¹⁷ In contrast to the previous work, they employed solution-based spin coated perovskite absorbers on a SHJ bottom cell with flat front side and textured rear surface. Their champion device was based on a FA_{0.9}CS_{0.1}PbI₃ (1.55 eV) middle cell absorber and FA_{0.80}CS_{0.20}Pb(I_{0.45}Br_{0.55})₃ (1.90 eV) top cell absorber and reached 20.1% PCE, 86.0% FF and 8.5 mA cm $^{-2}$ j_{SC} with a V_{OC} of 2.74 V. The cell showed acceptable stability measured for more than 40 s at maximum power point. In this work, 1 nm of Au was used as recombination layer between the perovskite subcells. The top perovskite absorber layer had a higher bandgap compared to the previous publication. This bandgap combinations for perovskite middle and top cells are closer to the optimum values suggested by simulations. As an antireflection layer, textured polydimethylsiloxane (PDMS) was used at the front side of the device. Overall, current matching was still not achieved in this work and the perovskite middle cell limited the j_{SC} of the device.

Very recently, Choi *et al.* reported on a 22.2% perovskite/perovskite/silicon triple-junction solar cell¹⁵ on a flat front side

and textured rear side SHJ. Perovskite middle and top cells in this work were Cs_{0.10}FA_{0.85}MA_{0.05}PbI₃ (1.56 eV) and MAPb(I_{0.50}Br_{0.35}Cl_{0.15})₃ (1.96 eV), respectively. To avoid the solvent damage while processing the perovskite top cell, they followed a similar approach as the first all-perovskite triple-junction solar cell by McMeekin *et al.*²³ They employed ACN/MA solvent system instead of DMF/DMSO for the top perovskite which was removed immediately after spin coating and prevented solvent penetration to the underlying layers. By taking advantage of this optimization, the perovskite top cell was fabricated without the ALD SnO_x protection layer. Similar to the record all-perovskite triple-junction work,¹⁴ here PEIE was spin coated on top of C₆₀. In addition, they employed a high-quality high bandgap perovskite achieved *via* additive engineering by adding urea into their perovskite precursor solution. With these two optimizations, the best performing cell showed 22.2% PCE, 78.6% FF and 10.2 mA cm $^{-2}$ j_{SC} with a V_{OC} of 2.78 V. The cell showed satisfactory stability for 600 s measured at maximum power point in ambient atmosphere at room temperature. The j_{SC} of the final device was limited by the middle cell.

Our team recently fabricated perovskite/perovskite/silicon triple-junction solar cell with 20.0% PCE. A SHJ cell with flat front and textured rear side was employed as the bottom cell and perovskite middle and top cells were in p–i–n configuration





Fig. 7 (a) ABX_3 structure of perovskite material where A is a monovalent organic or inorganic cation such as methylammonium (MA), formamidinium (FA), and cesium (Cs). B is typically divalent lead (Pb) or tin (Sn) and X is a halide, mostly iodide (I) and bromide (Br) or a combination of them. (b) Perovskite bandgap tunability in the range from 1.2 eV to 3.1 eV. The bandgap range suitable for top cell, middle cell and bottom cell are highlighted by blue, green and red background accordingly. Adapted with permission from ref. 40 and 47 Copyright © 2020 Elsevier Inc and ref. 47 available from: <https://doi.org/10.1021/nl5048779>, Copyright © 2019 American Chemical Society.

(MA), formamidinium (FA), and cesium (Cs). B is typically divalent lead (Pb) or tin (Sn) and X is a halide, mostly iodide (I) and bromide (Br) or a combination of them.⁷ One outstanding property of metal halide perovskite is their bandgap tunability, which makes them ideal to be used in multi-junction solar cells. The perovskite's bandgap can be tuned from 1.2 eV to 3.1 eV⁴⁰ by compositional engineering *via* cation or halide substitution (Fig. 7).^{34,40–43}

Primarily, the perovskite's bandgap is determined by the B- and X-site ions forming a $[BX_6]$ octahedral framework. The valence band maximum (VBM) consists of B-s and X-p orbital coupling, while CBM consists mainly of B-p orbital contribution.⁴⁴ The A-site cation has ionic character and its electronic states do not contribute to the VBM or CBM.⁴⁵ Nonetheless, the A cation can influence the $[BX_6]$ framework sterically or electrostatically. In this way, expansion or tilting of the lattice structure can lead to changes in the bandgap.⁴⁶ Depending on the B-site cation used (Pb or Sn), smaller cations on the A-site ($Cs < MA < FA$) can either increase or reduce the bandgap.⁴⁶ Most commonly, A- and X-sites are tuned at the same time to adjust the bandgap and ensure phase stability of the final composition.

The first reported perovskite solar cell was $MAPbI_3$ absorber with a bandgap of 1.55 eV,⁴⁸ however it is not regarded as promising middle cell absorber due to poor moisture and thermal stability above 85 °C.⁴⁹ Improved performance as well as chemical and thermal stability have been achieved for multi cation (Cs/MA/FA) multi halide (Br/I) perovskite compositions that are now widely used in the community.⁵⁰

3.1 Middle perovskite subcell in current triple-junction solar cells

The record PCE of p–i–n perovskite single-junction solar cells is 24.7% using a triple cation double halide absorber with a $Cs_{0.05}(FA_{0.95}MA_{0.05})_{0.95}Pb(I_{0.95}Br_{0.05})_3$ composition and a 1.55 eV bandgap.⁵¹ Currently the perovskite middle cells in reported triple-junction solar cells have bandgaps in the range of 1.55 eV to 1.62 eV. Table 3 summarizes compositions and bandgaps of

the middle perovskite absorbers implemented in current triple-junction solar cells, as well as device structures and jV performances of respective single-junction solar cells.

As mentioned before, so far, the reported perovskite/perovskite/silicon triple-junction solar cells suffer from current mismatch in a way that the middle cell is limiting the overall current of the device and highest current is being generated in the silicon bottom cell. For improved current matching, reducing the bandgap of the middle cell perovskite absorber is required. In the following sections, we discuss the two most promising perovskite candidates with bandgap lower than 1.50 eV.

3.2 Strategies for stable $FAPbI_3$ perovskite with bandgap of 1.47 eV

Compared to $MAPbI_3$, implementing FA on the A-site allows to form a nearly cubic structure, a reduced bandgap (1.47 eV), and improved thermal stability.^{52,53} Moreover, its bandgap is ideal to be used as middle cell absorber in a triple-junction structure with a 1.12 eV bottom cell. The work on $FAPbI_3$ solar cell has mostly been in the n–i–p architecture which holds the record single-junction perovskite solar cell with a PCE of 25.8%.⁵⁴ Despite the relatively fewer works on the $FAPbI_3$ based p–i–n solar cells, recently an impressive PCE of 24.1%⁵⁵ has been reported, which is promising for multi-junction solar cell's application.

The major challenge of $FAPbI_3$ perovskite lies in its limited structural stability. Due to disordered FA-I ion interaction, the asymmetrical FA cation takes an off-centered position, which results in the formation of a trigonal instead of a cubic structure. Experimentally, a 1D yellow non-perovskite polymorph (yellow δ -phase) is formed for usual low-temperature annealing around ~ 100 °C. Annealing at 160 °C allows to form the desired cubic phase (black α -phase),⁵⁶ which could harm temperature-sensitive underlying layers. Moreover, exposure to ambient environment, particularly high humidity, can trigger the phase transition from black α - to yellow δ -phase.⁵⁶

Fig. 8 shows the PCE evolution of $FAPbI_3$ perovskites for n–i–p and p–i–n structures.



Table 3 j_V performance, perovskite composition, bandgap, absorber layer thickness, and device structure of perovskite single-junction solar cells with middle perovskite absorber used in perovskite-based triple-junction solar cells in literature. Single-junction solar cell values for the first perovskite/perovskite/silicon solar cell are not available (due to the fully textured design and respective optimization of processes on textured silicon bottom solar cells)²²

Year	2019	2020	2020	2022	2022	2022	2023	2023	2023
Composition	MAPbI ₃	F _{A0.66} MA _{0.34} ⁺ PbI _{2.85} Br _{0.15}	C _{S0.05} FA _{0.95} ⁻ PbI _{2.55} Br _{0.45}	C _{S0.1} FA _{0.9} PbI ₃	C _{S0.15} MA _{0.15} FA _{0.70} ⁻ PbI _{2.85} Br _{0.15} ³	C _{S0.05} FA _{0.9} MA _{0.05} ⁻ PbI _{2.95} Br _{0.1} ³	C _{S0.1} FA _{0.88} MA _{0.05} ⁻ PbI ₃	C _{S0.05} (FA _{0.9} MA _{0.1}) _{0.95} ⁻ PbI _{2.95} Br _{0.05} ³	
Bandgap (eV)	1.57	1.57	1.60	1.55	1.62	1.60	1.56	1.56	
Structure	Glass/FTO/SnO ₂ /perovskite/PTAA/PCBM/perovskite/C60/BCP/Al	Glass/ITO/PTAA/perovskite/C60/BCP/Al	Glass/ITO/NiO _x /PTAA/perovskite/C60/BCP/Cu	Glass/ITO/HTL/perovskite/LiF/C60/BCP/Cu	Glass/ITO/NiO _x /Me-4PACz/perovskite/PEAI-EDAI ₂ /PCBM/PEIE/SnO ₂ /Ag	Glass/ITO/PTAA/PFN-perovskite/C60/PTAA/PFN-perovskite/C60/PEIE/Ag	Glass/ITO/PTAA/PFN-perovskite/C60/SnO _x /Ag	Glass/ITO/PTAA/PFN-perovskite/C60/SnO _x /Ag	
Molarity (M)	1.03 : 1 MAI:PbI ₂	NA	1.40	1.50	1.25	1.50	1.20	1.20	
Thickness (nm)	530	450	280	NA	NA	780	450	450	
PCE (%)	15.3	16.5	19.4	18.1	21.0	21.1	20.1	15.6	
FF (%)	70.0	76.0	80.2	78.0	79.4	77.3	80.3	77.2	
J_{SC} (mA cm ⁻²)	20.8	21.0	22.4	23.3	22.4	22.5	24.5	19.8	
V_{OC} (V)	1.06	1.03	1.08	1.01	1.18	1.20	1.04	1.02	
Top cell in	Pero/pero/pero	Pero/pero/pero	Pero/pero/pero	Pero/pero/silicon	Pero/pero/organic	Pero/pero/pero	Pero/pero/silicon	Pero/pero/silicon	
Ref.	23	25	24	17	16	14	15	26	



Fig. 8 PCE evolution of FAPbI₃ solar cells in p-i-n and n-i-p configuration discussed in this review for different strategies that resulted in efficient solar cells and improved stability (red: compositional engineering, orange: deposition technique, green: additive engineering, blue: surface and interface passivation and purple: charge transport layer). Data for n-i-p configuration are taken from ref. 54 and 57–64 and for p-i-n configuration from ref. 55 and 65–68. Certified values are marked with #.

In order to improve the stability of FAPbI₃ and achieve the black perovskite phase at low annealing temperature several strategies have been reported in the literature, which we briefly summarize below:

(1) Compositional engineering: the most famous approach to stabilize the black α -phase is alloying a small concentration of cations and anions with smaller ionic radius such as MA, Cs and Br to the composition. For example, Lee *et al.* showed that by adding a small amount of CsI to FAPbI₃, a black perovskite phase can be formed even prior to the annealing step.⁶⁹ This approach however has the drawback of increasing the bandgap of perovskite. Min *et al.* reported stable α -FAPbI₃ by incorporation of small amount of methylenediammonium dichloride (MDACL₂) into perovskite lattice. The film annealed for 10 minutes at 150 °C, showed almost identical bandgap compared to the control film, and the corresponding solar cell delivered 23.7% certified efficiency. This perovskite solar cell retained 90% of its PCE for 20 h in air under 150 °C with no encapsulation.⁵⁸ Moreover, non-stoichiometric modified precursors have shown several advantages in film quality of different perovskite compositions. For FAPbI₃ perovskite, excess FAI resulted in formation of the black film at low annealing temperature of 60 °C⁷⁰ or even without annealing at room temperature.⁷¹ Zhang *et al.* systematically studied the effect of excess PbI₂ in FAPbI₃ precursor solution and found that it reduced charge trap densities and prolonged charge carrier lifetimes.⁶⁶ Previous studies have confirmed the impact of excess PbI₂ in passivating the grain boundaries of perovskite.⁷²

(2) Deposition technique: the fabrication method employed to deposit the perovskite layer is known to influence film crystallization. Instead of common one-step spin coating



Fig. 9 General approaches reported in literature to improve performance and stability of FAPbI₃ perovskite solar cells. (a) FAPbI₃ and FA_{0.9}Cs_{0.1}PbI₃ films with different annealing temperatures, (b) Top view SEM images of FAPbI₃ and FA_{0.9}Cs_{0.1}PbI₃ and (c) normalized PCE of their respective solar cells without encapsulation measured over time in ambient. Cs incorporation resulted in formation of black perovskite even at room temperature. FA_{0.9}Cs_{0.1}PbI₃ has improved film quality and stability compared to pure FAPbI₃. Reproduced with permission from ref. 69. Copyright © 2015 WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim. (d) Schematic illustration of perovskite processing of FAPbI₃ solar cells processed with 2-step deposition method using dynamic



spin coating for the organic salt and statistical photovoltaic parameters (j_{sc} , PCE, FF and V_{oc}) of FAPbI₃ solar cells comparing static and dynamic spin coating for organic salt deposition. Reproduced with permission from ref. 74. Copyright © 2022, Rights managed by AIP Publishing. (e) Schematic illustration of evaporation method for processing of FAPbI₃ and respective FAPbI₃ film processed on large area with this method. Black FAPbI₃ is formed after 1 minute annealing at 170 °C. Reproduced with permission from ref. 75 Copyright © 2017, American Chemical Society. (f) XRD measurement of fresh and aged FAPbI₃ films with and without MAFA additive and (g) operational and thermal stability of FAPbI₃ solar cells with and without MAFA additive. Adding MAFA into perovskite precursor leads to excellent phase stability for 500 h and the corresponding solar cell exhibited improved operational stability. Reproduced with permission from ref. 55. Copyright © 2023 Wiley-VCH GmbH. (h) Top view SEM images of FAPbI₃ films with and without passivation with CPAH, (i) XRD measurement of fresh and aged FAPbI₃ films with and without CPAH treatment and (j) operational and thermal stability of FAPbI₃ solar cells with and without passivation. Passivating the perovskite surface with CPAH resulted in phase stability for 48 h and the corresponding solar cell exhibited improved operational stability. Reproduced with permission from ref. 77. Copyright © 2021 Elsevier Ltd. All rights reserved. (k) PCE of FAPbI₃ solar cell in p-i-n configuration using different HTLs and varied annealing temperature along with the trap density calculated for perovskite films on different HTLs and (l) perovskite films with different HTLs kept under 70% RH and 120 °C condition. Solar cell with MeO-2PACz as HTL indicated highest PCE and lowest trap density. The FAPbI₃ perovskite deposited on MeO-2PACz was more stable compared to other HTLs. Reproduced with permission from ref. 66. Copyright © 2022 Wiley-VCH GmbH.



Fig. 10 Composition, bandgap and PCE evolution of Sn-containing perovskites discussed in this review for different strategies that resulted in efficient solar cells and improved stability (red: compositional engineering, orange: deposition technique, green: additive engineering, blue: surface and interface passivation and purple: charge transport layer). Data are taken from ref. 84–92. Certified values are marked with #.

above 1.35 eV suitable for the middle cell in triple-junction devices. Among them, pure Sn perovskite with FASnI₃ composition could be an attractive option. First, its bandgap of ~1.40 eV is suitable for the middle cell of triple-junction solar cell especially on top of silicon bottom cell, and secondly, employing such Pb-free perovskite in multi-junction solar cell relaxes the concern regarding the toxicity of Pb. However, the maximum certified PCE reported so far for FASnI₃ solar cell is 14.1%⁹² which lags behind the performance of pure Pb and Pb–Sn perovskites.

In general, there are two major challenges associated with Sn-containing perovskite. First, Sn²⁺ can easily be oxidized to Sn⁴⁺ in the presence of small amounts of oxygen leading to defect formation that reduces carrier lifetime.⁹³ Second, due to non-uniform nucleation and fast crystallization of Sn-containing perovskite, fabrication of high-quality, homogeneous, compact, and pinhole-free film is more challenging compared to pure Pb perovskite.^{91,94} Such non-ideal perovskite films with defects and large number of

grain boundaries in turn accelerate the oxidation of Sn²⁺. Klug *et al.* reported that the photoluminescence intensity of perovskite film decreased by orders of magnitude when replacing only 1% of the Pb with Sn in the composition, which proves the challenges on the way of bringing Sn-based perovskite to the level of pure Pb perovskite.⁹⁵

Some strategies reported in literature to overcome these challenges are:

(1) Compositional engineering: perovskite composition and solution preparation have a crucial impact on the quality of the perovskite film in general and consequently the device performance. This is particularly critical in the case of Sn-based perovskites since they are prone to defects as discussed before. Usually, the perovskite solution is prepared by dissolving the precursor powders in an appropriate solvent. Liao *et al.* introduced a new precursor system by preparing FASnI₃ and MAPbI₃ precursor solutions separately and mixed them subsequently at different molar ratios. The fabricated (FASnI₃)_{0.6}(MAPbI₃)_{0.4} perovskite films showed dense grains with no visible pinholes.⁹⁶ Li *et al.* demonstrated that incorporation of Br in mixed Pb–Sn perovskite improves perovskite film quality and effectively passivates the grain boundaries. Optimizing Br concentration to 6% led to 19.0% PCE.⁸⁹ In another approach incorporation of Cs into FA_{0.8}MA_{0.2}Sn_{0.5}Pb_{0.5}I₃ perovskite improved the operational stability and for the optimum Cs content of 2.5%, PCE of 18.2% was reported.⁹⁷

(2) Deposition technique: as discussed in the previous section, fabrication method can have a huge impact on morphology of the formed perovskite film. Abdollahi Nejang *et al.* introduced processing of Sn-containing perovskite films *via* the vacuum-assisted growth control (VAGC). In this method, instead of using an antisolvent, a vacuum chamber is used to remove the solvents from the film. As a result of process optimization, homogeneous pinhole-free perovskite layers with large grains were achieved.⁹⁴ Werner *et al.* employed the gas quenching method, in which a flow of nitrogen is used to remove the solvent from the film. Sn-containing perovskite films processed with N₂ quenching also showed uniform, pinhole-free morphology.⁹¹ The improvement in morphology was shown to reduce defects at the grain boundaries and is a crucial factor to improve the performance and stability of Sn-containing perovskites.⁹⁸

(3) Additive engineering: introducing inorganic Sn halide additives SnX₂ (X = F, Cl, Br, I) into the precursor solution has



widely been reported to limit the oxidation by reducing the formation of Sn vacancies. For example, employing SnF₂ additive resulted in better crystallization and formation of pinhole-free perovskite layer.⁹⁹ Incorporation of a small amount of metallic Sn powder not only helps to lower the oxidation of Sn²⁺ to Sn⁴⁺ but also is a step further and can convert Sn⁴⁺ back to Sn²⁺.⁸⁷ Organic additives such as Guanidinium thiocyanate (GuaSCN)¹⁰⁰ and methylammonium thiocyanate (MASCN)¹⁰¹ have also been reported to increase the perovskite grain size and reduce the grain boundaries. In addition Sn²⁺ and SCN⁻ interaction has shown to inhibit the degradation of Pb–Sn perovskite precursor.¹⁰¹ Xiao *et al.* added zwitterionic antioxidant into the perovskite precursor solution.⁸⁶ The zwitterionic molecules hindered Sn²⁺ oxidation and passivated defects at the surface and grain boundaries of mixed Pb–Sn perovskite films, leading to certified PCE of 20.7%.⁸⁶ Furthermore, introducing hydrazine sulfate (HS) additive into Sn-containing perovskite has been found to slow down the crystallization. This in turn resulted in homogeneous distribution of elements and high quality perovskite film which led to 23.2% PCE.¹⁰² Very recently 23.7% PCE was achieved for Pb–Sn perovskite by improving the film quality through addition of octyl ammonium tetrafluoroborate (OABF₄) into the perovskite precursor.⁸⁴

(4) Interfacial and surface passivation: oxidation of Sn mostly occurs at the perovskite surface. Therefore, passivating the surface with different treatment methods such as forming 2D/3D structure can protect the perovskite surface and reduce the degradation rate by blocking the diffusion of oxygen into the grains. Kapil *et al.* studied the effect of surface treatment of Pb–Sn perovskite with ethylenediamine (EDA). They showed that the EDA treated perovskite films had reduced Sn⁴⁺ concentration on their surface compared to the non-treated films. The champion cell with optimum EDA concentration showed 21.7% PCE.¹⁰³ Hu *et al.* passivated top surface of Pb–Sn perovskite with ethylenediammonium iodide (EDAI₂) and achieved 23.6% PCE.⁸⁵ Passivated samples showed improved stability with 80% of the PCE retained after measuring for 200 h in inert atmosphere. In another study, passivating the surface and grain boundaries of Pb–Sn perovskite with phenethylamine acetate (PEAAc) effectively hindered the oxidation of Sn²⁺. In addition, this surface modification improved the band alignment of perovskite and ETL.¹⁰⁴

(5) Charge transport layer: the charge transport layer plays an important role for the stability of Sn-containing perovskite solar cells. PEDOT:PSS is the most widely used HTL in p–i–n configuration for Pb–Sn perovskite solar cells. However, stability of solar cells employing this HTL is a concern due to its hygroscopic and acidic nature. Ghimire *et al.* employed a PEDOT:PSS/PTAA bilayer in their Pb–Sn perovskite which resulted in improved morphology and larger grain size. Moreover, due to hydrophobic nature of PTAA, devices incorporating this bilayer as the HTL, exhibited significantly improved stability when compared to those using PEDOT:PSS.¹⁰⁵ Kapil *et al.* achieved 23.3% efficiency by employing a 2PACz/methyl phosphonic acid (MPA) bilayer as HTL in Pb–Sn perovskite. Perovskite films with 2PACz/MPA showed much slower oxidation rate.⁹⁰ Pitaro *et al.* compared

the formation of Pb–Sn perovskite on PEDOT:PSS, 2PACz and Br-2PACz. Their findings revealed that Br passivates the halogen vacancies at the perovskite/HTL interface. In addition, perovskite layers deposited on Br-2PACz exhibited better crystallinity. Consequently, solar cells utilizing Br-2PACz demonstrated superior performance and stability compared to PEDOT:PSS and 2PACz.¹⁰⁶ In a later study they improved the wetting of the Sn-based perovskite on SAM by deposition of a carbazole alkylammonium iodide derivative (4CzNH₃I) layer on top of Br-2PACz (Fig. 11).¹⁰⁷

Several reviews have summarized the progress of Pb–Sn perovskite solar cells^{82,108} with focus on bandgap tuning and their application in all-perovskite tandem solar cells,¹⁰⁹ stability issues and how to overcome them¹¹⁰ as well as their optoelectronic properties.¹¹¹

4. Suitable perovskite absorbers for top cell application

The bandgap required for the top cell in a triple-junction device is in the range of 1.85 eV to 2.15 eV depending on the choice of the other two subcells (see Section 1). So far, the focus of the research on high bandgap perovskite (HBG) in perovskite community has been mostly on the bandgap range suitable for dual-junction application (1.60–1.70 eV) and compositions with bandgaps greater than that have been explored relatively little.

4.1 Strategies for stable mixed cation mixed halide perovskite with bandgaps above 1.75 eV

In a mixed cation (mainly Cs/MA/FA) mixed halide (mainly Br/I) perovskite composition, the most common practice to increase the perovskites' bandgap is by increasing the amount of Br and/or Cs in the composition, which results in around 0.06 eV and 0.02 eV increase in bandgap by each 10% increase in Br and Cs content, respectively.^{41,43} However, the effective Br tuning introduces defect-assisted photo-induced phase segregation, which can be regarded as one of the key challenges associated with HBG perovskite. For the first time Hoke *et al.* reported that HBG perovskites with halide mixture of Br and I in the composition with Br/I > 20% segregate into Br-rich and I-rich regions upon continuous illumination¹¹² (Fig. 12a). This phenomenon is also attributed to ion migration in mixed halide perovskite, where the generated electric field from electrical biasing breaks the halide's bond and leads to phase segregation as a result of this ionic movement.¹¹³ This goes along with a deficit in open-circuit voltage.¹¹² In addition to phase segregation, non-radiative recombination losses and the non-ideal energetic band alignment between the perovskite and the charge transport layers limit the V_{OC} of the final device¹¹⁴ (Fig. 12b and c). Therefore, high V_{OC} deficit is reported for HBG perovskites (Fig. 12d).

In order to tackle the above-mentioned issues and improve the V_{OC} in respective compositions several strategies have been reported in literature, which we briefly summarize below.

(1) Compositional engineering: the composition of HBG perovskites is an important factor influencing device performance





Fig. 11 General approaches reported in literature to improve performance and stability of Pb-Sn perovskite solar cells. (a) AFM images of Pb-Sn perovskite and (b) statistical photovoltaic parameters (J_{sc} , V_{OC} , FF, and PCE) of Pb-Sn perovskite with different Br concentrations. Br incorporation resulted in larger grain size, and the highest PCE is achieved for solar cells with 6% Br concentration. Reproduced with permission from ref. 89 Copyright © 2018 WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim. (c) Schematic illustration of deposition of Pb-Sn perovskite with VAGC and (d) top view and



cross sectional SEM images of perovskite films processed with antisolvent and VAGC methods. Perovskite processed with VAGC had larger grains compared to the film processed with antisolvent. Reproduced from ref. 94 Copyright © 2019 Abdollahi Nejang *et al.* Published by WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim under the Creative Commons CC BY. (e) Aging Pb–Sn perovskite precursor solution with and without MASCN additive. (f) Top view and cross sectional SEM images of perovskite films with different concentrations of MASCN and (g) normalized PCE of the solar cells with and without MASCN additive as a function of precursor solution aging time. Pb–Sn precursor solution with additive showed no oxidation after 50 minutes exposure to air. Enlarged grain size is achieved for the films with additive in the precursor. Reproduced with permission from ref. 101 Copyright © 2018 WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim. (h) XPS measurement of untreated and EDA coated Pb–Sn perovskite films, (i) top view SEM images of perovskite surface and (j) jV characteristic of solar cells with no passivation and passivated with different concentration of EDA. Non-treated perovskite contains higher concentration of Sn⁴⁺ compared to the treated surface. Better film quality is achieved with EDA treatment. 0.1 mM was found to be optimum EDA concentration resulting in maximum PCE. Reproduced with permission from ref. 103. Copyright © 2021 Wiley-VCH GmbH. (k) Top view SEM images of Pb–Sn perovskite deposited on PEDOT:PSS and PEDOT:PSS/PTAA bilayer. Hydrophobic nature of PTAA compared to PEDOT:PSS resulted in larger grain size formation. Reproduced with permission from ref. 105. Copyright © 2022 Wiley-VCH GmbH. (l) Statistical PCE and stability of Pb–Sn perovskite with PEDOT:PSS, 2PACz and Br-2PACz as HTL. Devices with Br-2PACz exhibited higher PCE and stability. Reproduced from ref. 106. Copyright 2023 © Royal Society of Chemistry under Creative Commons Attribution-NonCommercial 3.0 Unported Licence.



Fig. 12 Origin of V_{oc} limitation in HBG perovskite solar cells. (a) Phase segregation of mixed halide high bandgap perovskite. Reproduced from ref. 112 Copyright © 2015, The Royal Society of Chemistry used under a Creative Commons Attribution CC BY 3.0. (b) V_{oc} loss of a solar cell due to non-radiative recombination loss. Reproduced from ref. 115. Copyright © 2020, Springer Nature Limited. (c) Band diagram of perovskite and its charge transport layers showing a band misalignment for 1.8 eV perovskite due to the fact that the HTL and ETL were optimized for 1.6 eV perovskite. Reproduced from ref. 114 Copyright © 2023, Caprioglio *et al.* under a Creative Commons Attribution CC BY and (d) V_{oc} of some of the high bandgap perovskite solar cells discussed in this review as a function of the reported bandgaps. The discrepancy between V_{oc} and bandgap increases for high bandgap perovskite solar cells.

and stability as each composition may induce a different electronic and crystal structure. Therefore, perovskites with same bandgap and different compositions do not necessarily exhibit similar trap states in their films. Bush *et al.* studied a wide range of double

cation (FA/Cs)/double halide (Br/I) perovskite compositions and found that increasing the bandgap should not only be relied on Br content. Increasing the Cs content allows to reduce the Br content (to a certain extent) while maintaining similar bandgap and





Fig. 13 Approaches reported in literature which successfully suppressed the light-induced phase segregation, non-radiative recombination and energetic band misalignment that improved the V_{OC} and consequently the performance of high bandgap perovskite solar cells. (a) Top view and cross-sectional SEM images of 1.78 eV perovskite films and (b) schematic structure of perovskite solar cell, statistical PCE as well as operational stability over time for perovskite solar cells with and without Rb in the composition. Reproduced with permission from ref. 116. Incorporation of Rb resulted in better film quality, increase in PCE and long term stability. Copyright © 2021 Wiley-VCH GmbH. (c) Top view and cross-sectional SEM images and XRD patterns





Fig. 14 Approaches reported in literature which successfully improved performance and stability of all-inorganic perovskite. (a) PL measurements of $\text{CsPbI}_{1.75}\text{Br}_{1.25}$ and $\text{Rb}_{0.15}\text{Cs}_{0.85}\text{PbI}_{1.75}\text{Br}_{1.25}$ perovskites. Reproduced with permission from ref. 14. Copyright © 2023, Wang *et al.* under exclusive license to Springer Nature Limited. (b) Statistical PCE, stabilized j_{sc} as well as long term stability of the all-inorganic perovskite solar cells with and without Rb in the composition. Better performance, photostability and long-term stability is achieved by incorporation of Rb. Reproduced with permission from ref. 143. Copyright © 2020 WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim. (c) Schematic illustration of dynamic hot-air assisted deposition technique, optical and top view SEM images of CsPbI_2Br perovskite processed with and without hot air quenching indicating improved film quality for samples prepared by dynamic hot-air assisted method. Reproduced with permission from ref. 147. Copyright © 2020 Elsevier Inc. (d) Schematic illustration of evaporation deposition of CsPbBr_3 and top view SEM images of CsPbBr_3 with different evaporation rates. The best film with large grain size is achieved for 5 \AA s^{-1} evaporation rate. Reproduced with permission from ref. 148. Copyright © 2018 WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim. (e) Images of CsPbI_2Br films with different amount of CaCl_2 additive over time stored at humidity of 40%, together with stabilized j_{sc} and j/V curves of the corresponding solar cells. Samples with high CaCl_2 concentration are more stable under humidity. Highest PCE is achieved for 0.5% CaCl_2 amount. Reproduced with permission from ref. 151. Copyright © 2020 WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim. (f) Images of CsPbI_2Br films with different passivation over time stored at humidity range from 25% to more than 60% as well as long-term stability of their corresponding solar cells. Passivated films showed better stability compared to non-passivated films under humidity. Best stability is achieved for PEACl treatment. Reproduced with permission from ref. 153. Copyright © 2018 WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim.



improved photostability under illumination.¹⁴ In the record perovskite/perovskite/silicon triple-junction solar cell, a triple halide perovskite composition of $\text{MAPb}(\text{I}_{0.50}\text{Br}_{0.35}\text{Cl}_{0.15})_3$ with 1.96 eV bandgap was employed. Urea was added to the perovskite solution to improve crystallinity and achieve a high-quality perovskite film with large grains without pinholes. Consequently, the performance of the high bandgap perovskite cell significantly improved from 6.4% to 13.9%. The main improvement came from increase in (j_{SC}) in the presence of the urea additive, which they attributed to the enhanced thin-film crystallinity and light absorption.¹⁵ We used a $\text{Cs}_{0.05}(\text{FA}_{0.55}\text{MA}_{0.45})_{0.95}\text{Pb}(\text{I}_{0.55}\text{Br}_{0.45})_3$ perovskite composition with 1.83 eV bandgap as top cell absorber of perovskite/perovskite/silicon triple-junction cell. A dynamic gas quenching method was used to prevent solvent damage to the already deposited layers. The perovskite film deposited by the adapted method showed homogeneous and compact morphology with improved crystallinity.²⁶

A comprehensive overview on high bandgap perovskite solar cells can be found in the recent review papers.^{157,158}

5. Recombination layer between the perovskite subcells

In monolithic multi-junction solar cells, the subcells are connected in series through recombination layers. The recombination layer has shown to be one of the key factors influencing the performance of tandem solar cells as its electro-optical properties directly affect all photovoltaic parameters (j_{SC} , V_{OC} and FF) of the device.^{159,160} In a perovskite solar cell, electrons are extracted through an ETL, and holes are extracted through an HTL. In electrically series-connected perovskite subcells without any additional layer, the ETL and HTL of the subcells get in contact. However, there is usually a difference between the work functions of the middle cell's ETL and top cell's HTL.¹⁶¹ Therefore, directly connecting these two layers from different subcells introduce a barrier at this interface^{160,161} and has shown to result in S-shape jV curves and reduced FF of the device.¹⁶² Hence, introducing an additional layer between the subcells with a suitable work function could reduce the mentioned gap and provide recombination sites for the collected charge

carriers at HTL and ETL of different subcells. There are several properties that a recombination layer between perovskite subcells must fulfill (Fig. 15) which can be categorized as follows:

1. Electrical requirements

- As the subcells are electrically connected in monolithic multi-junction solar cells, the recombination layer must have low contact resistance.

- It also requires low lateral conductivity to avoid current diffusion.

2. Optical requirements

- The parasitic absorption of this additional layer should be minimum to transmit the light to the underlying subcell. Given the bandgap combinations of the subcells in the dual-junction solar cell, the recombination layer needs to be transmitting especially in the infra-red (IR) range. This spectrum of interest is broader for the recombination layer between the top and middle cell in triple-junction solar cells and is not limited to IR region.

3. Processing requirements

- To avoid possible damages during the processing of the top layers, the recombination layer must protect the layers underneath.

- The processing of the recombination layer itself needs to be compatible in order not to damage the underlying layers.

Generally, there are two common approaches for the recombination layer between the subcells in perovskite-based multi-junction solar cells. Either employing a transparent conductive oxide (TCO) such as sputtered indium tin oxide (ITO) and indium zinc oxide (IZO) or ultrathin metal layer such as gold (Au) and silver (Ag).

A thick layer of sputtered ITO ($\sim 100\text{--}120$ nm) has been used as recombination layer between the perovskite subcells in early reports on all-perovskite dual-junction solar cells.^{163,164} In the first proof of concept perovskite/perovskite/silicon triple-junction cell, Werner *et al.* followed a similar approach and employed 150 nm IZO as the recombination layer between the perovskite middle cell and top cell.²² However, the thick TCO layers have several drawbacks such as low sheet resistance which has shown to result in shunting the solar cells.¹⁶⁵ Such thick layers are also optically poor due to high parasitic absorption and possible back reflection.



Fig. 15 Schematic of relevant electrical, optical and processing requirements for the monolithic connection of perovskite subcells.



Most of the recent, highly efficient all-perovskite dual-junction solar cells including the current certified record, employed 1 nm evaporated gold (Au) as recombination layer in their structure.^{10,120,166} The advantages of evaporated metal

layer are its damage-free deposition method compared to sputtering as well as its very high conductivity. However, this layer should be kept as thin as possible (~ 1 nm) to minimize parasitic absorption. Later, TCO layers with reduced thickness



Fig. 16 Replacing metal layer with thin TCO as recombination layer. (a) Schematic structure of perovskite/organic dual-junction solar cell with four types of recombination layers and their corresponding jV curves and (b) comparison of transmittance and reflectance of the tested recombination layers. Reproduced with permission from ref. 162. Copyright © 2022, Springer Nature. (c) Schematic structure of perovskite/organic dual-junction solar cell with different thicknesses of ALD deposited InO_x as recombination layer and their corresponding jV curves. (d) Diode characteristic of (SnO_x)/(InO_x)/(MoO_x). (e) Comparison of transmittance of ~ 1.5 nm of InO_x and 1 nm Ag, and EQE of the organic bottom cell with 1.5 nm of InO_x and 1 nm Ag as recombination layer. Reproduced with permission from ref. 129 Copyright © 2022, Springer Nature. (f) Schematic structure of perovskite/perovskite/silicon triple-junction solar cell with Au/PTAA and ITO/2PACz as interconnection layers and their corresponding jV curves and (g) comparison of transmittance, reflectance and absorbance of the 1 nm of Au with 15 nm of ITO. Reproduced with permission from ref. 26 Copyright © 2023 Heydarian et al., Published by American Chemical Society. Under a Creative Commons Attribution CC-BY-NC-ND 4.0. All examples indicate improved optical properties of the recombination layer upon replacing the metal layer with thin TCO. Improved electrical property is achieved by optimizing the thickness of the TCO layer.



were employed. Abdollahi Nejang *et al.* showed that 15 nm of ITO is still optically favorable compared to 1 nm Au, and their all-perovskite dual-junction solar cell exhibited 0.9 mA cm^{-2} increase in j_{SC} upon replacing Au with ITO as recombination layer.¹⁶⁵ We observed similar behavior in our perovskite/perovskite/silicon triple-junction solar cell where the j_{SC} of the device was severely limited by the middle cell. By replacing the Au with an ITO between the perovskite middle cell and top cell, more light was transmitted to middle cell which improved the j_{SC} of the final triple-junction solar cell (Fig. 16f and g).²⁶ Chen *et al.* developed a recombination layer based on a 4 nm IZO on perovskite/organic tandem solar cell (Fig. 16a and b).¹⁶² The perovskite/perovskite/organic triple-junction solar cell also employed only 2 nm IZO as the recombination layer between perovskite middle cell and top cell.¹⁶ Palmstrom *et al.* attempted to produce recombination layer-free all-perovskite dual-junction solar cells. However, based on their results at least 5–15 nm of IZO is needed to achieve high FF.³⁸ Brinkmann *et al.* demonstrated perovskite/organic dual-junction solar cell with only 1.5 nm indium oxide (InO_x) as recombination layer (Fig. 16c–e). Deposition by ALD instead of sputtering enabled formation of such thin and yet conformal InO_x layer.¹²⁹ Commonly, to avoid sputter damage, a buffer layer is deposited prior to sputtering of the TCO layers, which is usually a SnO_x layer deposited by ALD. This additional layer also helps to prevent the penetration of solvent during the solution-based processing of the subsequent layers.²⁶ Beyond this, Choi *et al.* fabricated perovskite/perovskite/silicon triple-junction solar cells without the SnO_x buffer layer.¹⁵ To enable fabrication of ALD free interconnection layer, Polyethylenimine ethoxylated (PEIE) in methanol was first spin coated on C_{60} similar to the approach outlined in ref. 14 and 38. Subsequently 20 nm ITO was sputtered on top of the PEIE coated stack. However, to remove the ALD buffer layer, firstly, development of a soft sputtering process is required. Secondly, in the absence of a solvent barrier layer, alternative strategies such as change of the perovskite solvent system^{15,23} or employing evaporation technique is required for processing of the perovskite layer on top.

Recently, a 23.7% efficient all-perovskite dual-junction solar cell with no TCO or metal based recombination layer was reported by directly contacting the SnO_x buffer layer and the HTL (PEDOT:PSS) of the low bandgap perovskite.¹⁶⁷ Even though this work highlights the potential of a simplified recombination layer, further study is needed to assess the possible formation of a Schottky barrier when the SnO_x and other HTL materials get in contact. Future work should focus on developing an ideal recombination layer between the subcells in multi-junction solar cells. In addition to the high parasitic absorption, taking the production cost into account, gold is the least favorable material to be used and material availability of both gold and indium are critical. Another motivation to avoid using a metal layer, especially in the substrate configuration (Fig. 5) where HBG perovskite is processed on top of the recombination layer, is that the common self-assembled monolayer (SAM) hole transport materials for HBG perovskites (see Section 4) cannot directly be deposited on metal as they require hydroxyl (–OH) groups to

bind to in a condensation reaction.¹⁶⁸ In that respect the surface of the recombination layer should provide sufficient –OH groups to ensure homogeneous coverage of SAM.

Research on alternative indium-free recombination layers such as aluminum-doped zinc oxide (AZO) is ongoing. For example zinc oxide (ZnO)/AZO has been used as recombination layer in copper indium selenium (CuInSe_2)/perovskite dual-junction solar cell.¹⁶⁹ AZO has also been employed as front contact of SHJ solar cells¹⁷⁰ which opens up the window for replacing the common TCO recombination layer between silicon and perovskite subcells. In addition, according to Messmer *et al.* the final cost of the solar cell significantly drops by replacing ITO layer with AZO.¹⁷¹

Finally, it is important to mention that optimizing the recombination layer between two subcells in a triple-junction solar cell is complex as one cannot evaluate the quality of the recombination layer independent from the effect of the connection to the third subcell.

6. Characterization of triple-junction solar cells

Precise characterization of solar cells is highly important in research and development. Solar cell's performance data reported in literature are mainly from in-house measurements. While for single-junction solar cells the measurement approach and interpretation of data is more straightforward, a sophisticated procedure is needed for multi-junction solar cells, especially in two-terminal structures where no direct electrical access to the individual subcells is possible and additional effects such as luminescent coupling can occur for current mismatched subcells. This gets more challenging by adding to the number of junctions. Even though perovskite-based triple-junction solar cells are at the early stage of development, there is extensive research and well-established measurement standards for multi-junction solar cells based on III–V materials,^{172–177} from which the perovskite community can benefit.

6.1 External quantum efficiency (EQE) measurement

The general method for correct EQE measurement of monolithically series-connected solar cells has been first presented by Burdick and Glatfelter in 1986 for a-Si/Si dual-junction solar cells¹⁷⁸ and was extended for a GaInP/GaInAs/Ge triple-junction solar cell by Meusel *et al.*¹⁷³ The method is used to characterize multi-junction devices independent of their material. In summary, the EQE of each subcell in a two-terminal triple-junction solar cell can be measured individually provided that the subcell of interest limits the overall current. To achieve this, the solar cell is illuminated with spectrally selective bias lights to saturate the other subcells so that they generate larger photocurrents than the subcell under test. The suitable selective bias light depends on the spectral responses of the subcells and can be provided by wavelength specific bias lights such as LEDs or the use of optical filters in combination with broadband light sources.¹⁷⁹ In addition, to determine the EQE correctly, the subcell under test needs to operate at its



short-circuit condition, therefore an external voltage equal to the sum of the voltages of the other two subcells under the bias light condition needs to be applied. Estimating the appropriate bias voltage value requires further effort as the exact values of the subcell voltages at this low irradiance are often not known and in this case the procedure described in International Electrotechnical Commission (IEC) should be followed.¹⁷⁹

One common challenge in EQE measurement of multi-junction solar cells are measurement artifacts.^{174,175} Subcell properties (e.g., low parallel resistance (R_p), early reverse breakdown and high radiative recombination) in combination with non-correct measurement settings (bias voltage, spectrally tuned bias light) can cause interaction between them during measurement which introduce undesired measurement artifacts such that the EQE of other subcells appears in the measured EQE-data of the subcell of interest. At the same time the absolute EQE of the measured subcell is lower than expected. This effect usually happens when the solar cells have low parallel resistance or low breakdown voltages leading to a change in operating voltage during measurement.¹⁷³ In addition, the luminescence coupling is another source of artifact in EQE measurement of multi-junction solar cells.^{176,180} However, EQE measurement of perovskite-based multi-junction solar cells with artifacts caused by luminescent coupling has not been reported yet. Therefore, in the following we will focus on artifacts caused by low parallel resistance or low breakdown voltage. This is one of the major challenges associated with EQE measurement of multi-junction solar cells that is widely discussed for III–V based multi-junction solar cells (Fig. 17a).¹⁷³ The measurement artifact can be corrected mathematically as described in ref. 174 and 175. However, it has been shown by Reichmuth *et al.* that the typical correction procedure based on the assumption of a uniform R_p might lead to deviations from the true EQE.¹⁸¹ These lateral effects may become more relevant for industrial-size solar cells.

For the case of perovskite/perovskite/silicon triple-junction solar cells, we have observed this effect in our lab when

measuring the EQE of a silicon bottom cell in which the artifact in the spectral response range of the top and middle cells (300–750 nm) is visible (Fig. 17b) and also the as-measured EQE curve of the middle cell shows an artifact in the spectral response range of the bottom cell (800–1200 nm) (Fig. 17b). The artifacts have been corrected with the method described in ref. 174. In summary, for the case of middle cell, a scaling factor (S) is determined to bring the EQE of the bottom cell to the level of the artifact at 800–1200 nm. Then the scaled curve is subtracted from the measured EQE to remove the artifact. Additionally, the measured EQE up to 800 nm is divided by $(1 - S)$. Similar procedure is applied to correct the EQE of the bottom cell.

Apart from the common challenges described above, several other factors and measurement conditions are shown to have an impact on the absolute EQE of perovskite solar cells due to their dynamic effects.¹⁸² Mundus *et al.* investigated the non-linearity of various single-junction perovskite solar cells and showed that the j_{SC} has non-linear behavior with respect to the irradiance leading to a dependency of the EQE on bias illumination intensity.^{183,184} Mercaldo *et al.* reported similar effect.¹⁸⁴ Other parameters such as chopper wheel frequency,^{184–188} preconditioning of the cell¹⁸⁷ and applied bias voltage are also reported to affect the absolute EQE.¹⁸⁷ Also, the common approach to measure the EQE with a monochromatic beam smaller than the active area of the solar cell can cause deviations in the signal compared to when illuminating the whole area including all metallization, the edges and spatially different absorber thickness, radiative properties *etc.*¹⁸¹ Therefore, calculating the generated current from measured EQE data obtained for individual subcells is not straightforward. Consequently, determining the current matching situation of the perovskite-based multi-junction solar cells from EQE measurement can result in misinterpretation.¹⁸⁹ An alternative approach based on spectrometric characterization for precise determination of current matching could in the future be used for perovskite-based triple-junction solar cells.¹⁷² This approach has been successfully applied on perovskite/silicon dual-junction solar cells.¹⁸⁹



Fig. 17 (a) Measurement artifact at spectral response (SR) range of top cell during EQE measurements of the germanium (Ge) bottom cell of a III–V/III–V/Ge triple-junction solar cell. With permission from ref. 173 Copyright © 2003 John Wiley & Sons, Ltd. (b) EQE curves of a perovskite/perovskite/silicon triple-junction solar cell measured at Fraunhofer ISE CaLab. Artifacts are visible for both middle cell and bottom cell EQEs. The EQE measurements with artifacts and the corrected curves are presented.



6.2 Current density–voltage (jV) measurement

Accurate jV measurement of multi-junction solar cells require a different procedure than that necessary for the characterization of single-junction solar cells. In the case of single-junction solar cells, the difference between the AM 1.5g reference spectrum and the simulator spectrum can be calculated with the mismatch factor and the intensity (often of a single broad band lamp) is set for the specific solar cell under test. For multi-junction solar cells however, the simple intensity variation of a single lamp will for most cases not reach AM 1.5g reference conditions within all subcells. Although a solar simulator might be classified to have a closely matched spectrum, even small spectral differences will lead to incorrect subcell currents. Therefore, also the relative spectral irradiance of the solar simulator needs to be tuned based on the spectral response of each solar cell individually (usually with multiple light-sources).^{172,190}

For multi-junction solar cells, the solar simulator spectrum needs to generate the same current in each subcell as under the reference spectrum (normally the AM 1.5g spectrum). That means, in case of triple-junction solar cells the following equation system must be fulfilled:

$$\begin{aligned} j_{\text{top}}^{\text{simulator}} &= j_{\text{top}}^{\text{AM 1.5g}} \\ j_{\text{middle}}^{\text{simulator}} &= j_{\text{middle}}^{\text{AM 1.5g}} \\ j_{\text{bottom}}^{\text{simulator}} &= j_{\text{bottom}}^{\text{AM 1.5g}} \end{aligned}$$

For this system of equations to be solvable at least three spectral channels are needed. Hence, a correct jV measurement of any type of triple-junction solar cell is only possible either with solar simulator that is equipped with three or more light sources which can be adjusted individually or with using different optical filters.^{172,177,191} The International Electrotechnical Commission (IEC) in its standard IEC60904-1-1 states maximum allowed deviations for the above equations by defining a factor Z_i for each subcell “i” to quantify how much the spectral irradiance of the subcell under test differs from AM 1.5g reference irradiance.¹⁹¹ The standard in its current form (2017) allows for 3% deviations from reference irradiance, however it also states, that maximum 1% deviations should be aimed for, since for series-connected multi-junction devices the FF and thus the efficiency is sensitively affected by spectral changes and measurement results could be significantly misleading. There is no easy straightforward correction procedure inherently in this regard. The uncertainty for setting the above equations affects the jV parameter as described by Reichmuth *et al.*¹⁹² So far the triple-junction solar cells reported in literature are measured with two lamp solar simulators such as tungsten-halogen²⁵ and halogen-xenon solar simulators,^{22,24} or with a one lamp solar simulator.¹⁷ In the first all-perovskite triple-junction solar cell, measurements were done with a xenon lamp solar simulator, but a mismatch correction factor was applied, which reduced the final efficiency from 9.9% to the reported value of 6.7%.²³ This significant difference shows the importance of accurate measurements. For the measurement of perovskite/perovskite/silicon triple-junction solar cell

in our group, the above mentioned requirements were fulfilled.²⁶ The jV measurement was performed with LED-based solar simulator. The spectrum of the solar simulator was adjusted based on the SR of the three subcells using the method developed in ref. 193. It must be noted that direct comparison between the performance of published perovskite-based triple-junction solar cells is difficult as there is only one certified measurement among them.¹⁴

Since research on triple-junction solar cells is at an early stage, following the IEC measurement procedure for measurements in the research labs is necessary for comparison between reported data and therefore increase the reliability of this emerging photovoltaic technology.

Here we summarize the measurement protocol of Fraunhofer ISE CalLab using three light source solar simulator:

I. SR measurement of the individual subcells.

II. Solving the following equation system based on the discussed conditions.

$$\begin{aligned} C_{\text{top}}A_1 \int s_{\text{top}}(\lambda)e_1(\lambda)d\lambda + C_{\text{top}}A_2 \int s_{\text{top}}(\lambda)e_2(\lambda)d\lambda \\ + C_{\text{top}}A_3 \int s_{\text{top}}(\lambda)e_3(\lambda)d\lambda &= C_{\text{top}} \int s_{\text{top}}(\lambda)E_{\text{AM1.5g}}(\lambda)d\lambda \\ C_{\text{mid}}A_1 \int s_{\text{mid}}(\lambda)e_1(\lambda)d\lambda + C_{\text{mid}}A_2 \int s_{\text{mid}}(\lambda)e_2(\lambda)d\lambda \\ + C_{\text{mid}}A_3 \int s_{\text{mid}}(\lambda)e_3(\lambda)d\lambda &= C_{\text{mid}} \int s_{\text{mid}}(\lambda)E_{\text{AM1.5g}}(\lambda)d\lambda \\ C_{\text{bot}}A_1 \int s_{\text{bot}}(\lambda)e_1(\lambda)d\lambda + C_{\text{bot}}A_2 \int s_{\text{bot}}(\lambda)e_2(\lambda)d\lambda \\ + C_{\text{bot}}A_3 \int s_{\text{bot}}(\lambda)e_3(\lambda)d\lambda &= C_{\text{bot}} \int s_{\text{bot}}(\lambda)E_{\text{AM1.5g}}(\lambda)d\lambda \end{aligned}$$

where s_{top} , s_{mid} and s_{bot} are the as-measured spectral responses (relative SR) and C_{top} , C_{mid} and C_{bot} are the scaling factors which will be cancelled out. This means that only relative SR are needed for correct adjustment of the solar simulator. e_1 , e_2 and e_3 are the spectrum of each lamp and $E_{\text{AM 1.5g}}$ is the AM 1.5g spectrum. The intensities of the three light sources are then adjusted according to A_1 , A_2 and A_3 .

III. In case of measuring perovskite-based solar cells, measurements should be performed in forward and reverse scan directions.

IV. Reporting stabilized PCE determined from fixed voltage or maximum power point (MPP) tracking.

7. Summary and outlook

While the highly efficient perovskite-based dual-junction solar cells especially on silicon bottom cells have already shown to be an attractive option for further efficiency improvement of future PV modules, perovskite-based triple-junction solar cells have the potential to surpass the efficiency limit of dual-junction solar cells. So far, the perovskite community has mostly focused on the optimization of single and dual-junction solar cells and limited effort has been spent on development of triple-junction solar cells using perovskite semiconductors. Therefore, the PCE



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Conflicts of interest

The authors declare no competing financial interest.

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