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Tailoring dielectric properties using designed polymer-grafted ZnO nanoparticles in silicone rubber†

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Polymer grafts were used to tailor the interphases between ZnO nanoparticles (NPs) and silicone matrices. The final electrical properties of the nanocomposites were tuned by the grafted interphases, by controlling the inter-particle distance and the NP-morphology. The nanocomposites can be used in electrical applications where control of the resistivity is desired. Hansen's solubility parameters were used to select a semi-compatible polymer for grafting to obtain anisotropic NP morphologies in silicone, and the grafted NPs self-assembled into various morphologies inside the silicone matrices. The morphologies in the semi-compatible nanocomposites could be tuned by steering the graft length of poly(*n*-butyl methacrylate) *via* entropic matrix-graft wetting using surface-initiated atom-transfer radical polymerization. Image analysis models were developed to calculate the radius of primary NPs, the fraction of aggregates, the dispersion, and the face-to-face distance of NPs. The dielectric properties of the nanocomposites were related to the morphology and the face-to-face distance of the NPs. The dielectric losses, above 100 Hz, for nanocomposites with grafted NPs were approximately one decade lower than those of pristine NPs. The isotropic nanocomposites increased the resistivity up to 100 times compared to that of neat silicone rubber, due to the trapping of charge carriers by the interphase of dispersed NPs and nanoclusters. On the other hand, the resistivity of anisotropic nanocomposites decreased 10–100 times when the inter-particle distance in continuous agglomerates was close to the hopping distance of charge carriers. The electrical breakdown strength increased for compatible isotropic nanocomposites, and the temperature dependence of the resistivity and the activation energy were ~50% lower in the nanocomposites with grafted NPs. These flexible dielectric nanocomposites are promising candidates for low-loss high-voltage transmission cable accessories, mobile electronic devices, wearables and sensors.

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1. Introduction

A sustainable society requires renewable generation of electric power and reduced energy consumption *via* improved energy efficiency. More efficient electrical insulation systems need a range of mechanical and electrical properties. Tailored materials are of interest for specific applications, leading to

components with smaller size, and better reliability and efficiency. This is of current importance, for example for integrating distant renewable energy resources. Polymeric materials are being used as the main insulation of power cables, cable accessories and cable joints. They are also found as insulation in generators and motors. Further, flexible polymer nanocomposites are being considered as insulation materials for mobile electronic devices, so-called wearables, since they are known to be durable and elastic, and to have potentially tunable properties.^{1–3} Nanoparticles (NPs) are especially interesting as they might exhibit different or additional features than their corresponding bulk phase.⁴ Nanocomposites containing SiO₂ nanoparticles (NPs), grown *in situ* in polyester-amide,⁵ or dispersed in polyester⁶ or polyamide-imide,⁷ show excellent resistance against partial discharges and are used as insulation for electrical motors. The addition of SiO₂, TiO₂ or MgO NPs to polyethylene (PE) resulted in cable-insulation materials with higher electric breakdown strength^{8,9} or reduced space-charge

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accumulation.¹⁰ More recently, Hedenqvist *et al.*¹¹ and Olsson *et al.*¹² have reported the efficient trapping of charge carriers by the interphases of ZnO and MgO nanoclusters in low-density PE, which increased the resistivity by one or two decades at low filling ratios (3 wt%). Previously, Wang *et al.*¹³ demonstrated that silicone rubbers filled with reduced graphene oxide (rGO) exhibited a non-linear increase in conductivity with increasing electrical field and that the composites exhibited lower conductivity compared to the neat silicone rubber matrix at low fields. These properties were tailored by varying the oxidation state and volume fraction of rGO. Thus, the dielectric properties of nanocomposites strongly depend on the dispersion of NPs and their percolation point, as well as on the interface and the interphase of the NPs. It is therefore desirable to control the surface characteristics of the NPs.

Significant efforts have been made to control the surface chemistry of NPs using Surface-Initiated Reversible Deactivation Radical Polymerization (SI-RDRP) techniques,^{14–16} including Surface-Initiated Atomic Transfer Radical Polymerization (SI-ATRP^{17–25}) and others.^{16,26–30} The task of controlling the surface chemistry of the NPs has recently been expanded from obtaining merely well-dispersed systems to being able to arrange the NPs in various self-assembled morphologies.^{31–33} The grafting density (σ), the curvature of the NP (α), and the ratio N_M/N_g (where N_M and N_g are respectively the degrees of polymerization of the polymer matrix and of the grafts) are three parameters entropically related to the wetting of the grafts by the matrix and thus to the NP morphology in the nanocomposite. In homopolymer nanocomposites, the entropic parameters are known to determine the formation of spherical aggregates, strings, sheets, phase-separation or well-dispersed particles in the matrix.^{32–35} On the other hand, the wetting of two different types of polymers in a “multi-polymer” nanocomposite is strongly affected, or even dominated, by enthalpic interactions (including the Flory–Huggins parameter (χ) and the graft penetration).^{36–38} Due to the increasing complexity of the enthalpic compatibility of grafts and matrix, anisotropic particle morphologies of multi-polymer nanocomposites have received little attention experimentally and are therefore not as well understood as homopolymer nanocomposites.³² However, by using Hansen’s solubility parameters (HSPs), the enthalpic compatibility (solubility) of polymers can be described in an elegant and reasonably simple way, with the advantage of including specific interactions, such as hydrogen-bonds, intermolecular dipolar forces and dispersion forces.³⁹ HSPs are usually used to predict the behaviour of polymers or NPs in different solvents,⁴⁰ but in this study they have been used to describe the compatibility between the graft and the matrix, to assess the ability of the polymeric matrix to entangle with semi-compatible polymer grafts.

In the current study, we aim at investigating the possibility to tune the electrical properties of nanocomposites by tailoring the interphase of ZnO NPs. We designed compatible and semi-compatible nanocomposite systems by the use of HSPs. The nanocomposites were composed of highly pure, commercially available ZnO NPs grafted with poly(*n*-butyl methacrylate) with controlled graft lengths mixed with silicone elastomer matrices

(PDMS or silicone rubber) commonly used as outdoor insulation of high-voltage components and cable joints, but of growing interest for soft electronics. We characterized interparticle distances of annealed grafted ZnO NPs, various NP-morphologies in silicone matrices and how they depend on the N_M/N_g and σ . Finally, we investigated how the morphology of NPs influenced the dielectric properties (*e.g.* resistivity, electric constant, and losses) below, at and above the glass transition temperature of the grafts ($T_g \approx 20$ °C).⁴¹

2. Experimental methods

2.1 Materials

ZnO NPs produced by flame spray pyrolysis (NanoGard® manufactured by Nanophase®) were purchased as a white powder from Alfa Aesar® (Lancashire, UK) with a specific surface area of $16 \text{ m}^2 \text{ g}^{-1}$ determined by BET, which corresponds to an average diameter of 67 nm, and a second ZnO nanopowder produced by wet-precipitation from a ZnO-salt precursor (MKN-ZnO-030) was purchased from MKnano® (Mississauga, Canada) with an average particle diameter of 30 nm. The purity and dielectric properties of the two types of ZnO NPs are compared in the ESI†. Polydimethylsiloxane (PDMS, M_n : 62.7 kDa, visc: 10 000 mPa s, 0.1 eq. vinyl), trimethylsiloxy-terminated cross-linker (poly((6.5%)methylhydrosiloxane-*co*-(93.5%)dimethylsiloxane), $M_n = 1.9\text{--}2$ kDa) and Pt-catalyst (0.001 M platinum(0)-1,3-divinyl-1,1,3,3-tetramethyl-disiloxane complex in silicone oil) were purchased from ABCR GmbH & Co (Karlsruhe, Germany). A Sylgard® 184 Silicone Elastomer Kit (A-component: ($M_n \approx 40$ kDa, visc: 4000–6000 mPa s) and B-component: catalyst and cross-linker (M_n : 5 kDa, 1300 mPa s)) was purchased from Dow Corning. (3-Aminopropyl)triethoxysilane (APTES, 98%), 2-bromoisobutyl bromide (α -BiB, 98%), ethyl-2-bromoisobutyl bromide (E-BiB, 98%), copper(I) bromide (Cu(I)Br, 98%), copper(II) bromide (Cu(II)Br₂, 99%), 4-(dimethyl amino) pyridine (DMAP, 99%), triethyl amine (TEA, 99%), 1,1,4,7,10,10-hexamethyltriethylenetetramine (HMTETA, 97%), tetrabutylammonium fluoride in tetrahydrofuran (TBAF, 1 M), potassium hydrogen phosphate (K₂HPO₄, 97%) and a ninhydrin test-kit (Kaiser-test) were used as received from Sigma Aldrich. *n*-Butyl methacrylate (BMA, 99%) was destabilized prior to use by passing it through a neutral Al₂O₃ column. Ethanol (EtOH, 96%), tetrahydrofuran (THF, analytical grade) and toluene (HPLC-grade) were used without further purification.

2.2 Synthesis

2.2.1 Silanization and immobilization of initiators onto ZnO NPs to produce ZnO-Br. The ZnO NPs were dried under vacuum at 190 °C, dispersed in a mixture of deionized water and ethanol (1 : 1 by vol.) and silanized using APTES prior to the immobilization of ATRP-initiators (α -BiB). The silanization procedure to obtain ZnO-APTES, and the subsequent immobilization procedure to obtain ZnO-Br, were both performed according to previous work^{42,43} and are described in more detail in the ESI† The average amount of Br-groups was 0.021 $\mu\text{mol Br}$ per mg of ZnO-Br, according to the mass loss detected by TGA.



2.2.2 Grafting from ZnO–Br by SI-ATRP to produce ZnO-g-PBMA. To obtain different graft lengths of PBMA, the reaction time was varied from 70 min to 24 h. The SI-ATRP was conducted in the presence of free initiators (E-BiB). As an example, in the polymerization procedure, the following molar ratios were used: 700 : 1 : 0.8 : 0.2 : 0.9 : 0.1 for [BMA] : [HMTETA] : [CuBr] : [CuBr₂] : [E-BiB] : [ZnO–Br]. Dispersed ZnO–Br (~0.4 g, 8.9 μmol Br) in 15 mL toluene was added to a 50 mL round-bottomed flask at 0 °C equipped with a rubber septum. BMA (10 mL, 63 mmol) was added to the flask together with HMTETA (24 μL, 90 μmol) and E-BiB (12 μL, 81 μmol). The mixture was degassed by two cycles of vacuum/backfilling with argon. Subsequently, Cu(I)Br (10 mg, 72 μmol) and Cu(II)Br₂ (4.0 mg, 18 μmol) were added under argon flow, followed by degassing in two additional cycles of vacuum/argon. The polymerization was conducted at 60 °C in an oil bath, and quenched by letting air in and by cooling on an ice-bath. ZnO-g-PBMA was purified by five successive centrifugation/re-dispersion cycles, described in detail in the ESI.† The purified ZnO-g-PBMA was stored in THF. A fraction (~100 mg) of ZnO-g-PBMA was dried in a vacuum oven at 50 °C overnight, and the dried ZnO-g-PBMA was characterized by FTIR, TGA, UV-Vis and TEM. The free PBMA was dissolved in THF and passed through a basic Al₂O₃-column to remove the Cu-catalyst and was dried in a vacuum oven at 50 °C and characterized by DMF-SEC. The PBMA grafts were cleaved from ZnO-g-PBMA using TBAF as a cleaving agent as in our previous work.^{42,43} A more detailed description of the cleaving procedure is presented in the ESI.†

2.2.3 Preparation and curing of nanocomposites. Nanocomposite films were cast in silanized glass discs (chlorotrimethylsilane) or polystyrene cups with diameters of 3 or 3.4 cm. The samples were degassed for 30 min under vacuum prior to curing at 60 °C for 24 h. The thickness of the samples was ~300 or ~600 μm.

2.2.3.1 1.5 vol% ZnO NPs in PDMS elastomer. Vinyl-terminated PDMS was used as laboratory grade silicone resin. Suspended or dry ZnO NPs (1.5 vol% ≈ 8.4 wt% inorganic content) were mixed with the PDMS at 70 °C for 2–3 days, while the solvent was removed. Thereafter, the trimethylsiloxy terminated cross-linker was added in small excess together with the Pt-catalyst. The PDMS and cross-linker were mixed in a ratio of 92.3 : 7.7 wt% with a few drops (~20 mg) of catalyst.

2.2.3.2 2.5 vol% ZnO NPs in silicone rubber. Sylgard® 184 was used as a commercial grade of silicone rubber as it contains fumed silica. In general, the A-component was mixed with 2.5 vol% (≈ 14 wt%) suspended or dry ZnO NPs (excluding the coating). The mixture was left at 70 °C for 2–3 days before curing by mixing with the B-component containing the cross-linker and the Pt-catalyst, the ratio of A to B being 10 : 1.

2.3 Models and methods

2.3.1 Hansen's solubility parameters (HSPs). The miscibility of two chemical species can be predicted using Hansen's solubility parameters (HSPs).³⁹ Three parameters (δ_D , δ_P , δ_H) are assigned to each molecule, where δ_D is the energy from dispersion forces between the molecules, δ_P is the energy from

dipolar intermolecular forces, and δ_H is the energy from hydrogen bonds between molecules. The three parameters are expressed in MPa^{0.5}, and they can be used as coordinates in a three-dimensional (Hansen) space. If two chemicals are closer in the Hansen space than the interaction radius R_0 of the solvent, the chemicals are more compatible and likely to dissolve each other. Thus, R_0 determines the size of the sphere in Hansen space, while the parameters δ_D , δ_P , δ_H determine the position. The centre-to-centre distance (R_a) between two spheres in the Hansen space is calculated according to:

$$R_a^2 = 4(\delta_{D1} - \delta_{D2})^2 + (\delta_{P1} - \delta_{P2})^2 + (\delta_{H1} - \delta_{H2})^2 \quad (1)$$

The relative energy difference (RED) of the system is obtained by dividing R_a by R_0 . If RED < 1 the polymers are compatible, if RED = 1 the polymers are semi-compatible and if RED > 1 the polymers are incompatible. A table with HSP values for silicone, ZnO, PBMA and THF are presented in the ESI (Table S1†).

2.3.2 Particle agglomeration and dispersion. To obtain a quantitative assessment of the dispersion of NPs, we used four dispersion analysis methods, developed and implemented in Matlab®. Electron microscope images of pristine, silanized and polymer-grafted ZnO NPs were imported to ImageJ®, where the contrast was enhanced so that the NPs were clearly distinguishable as black spots on a white background. Several images with different thresholds were merged, and artefacts were eliminated by restricting the maximum, minimum size and elongation. The centre-of-mass and the area were exported to Matlab for analysis. For simplicity, the NPs were treated as spheres. The radius distribution and the average centre-to-centre and face-to-face distances were calculated with a bootstrap statistics strategy using 1000 Bootstrap iterations.⁴² Repeating boundary conditions were applied on the borders of the image. The four dispersion analysis methods A–D are described as follows:

(A) The fraction of agglomerates ($\theta_{\text{aggl},A}$) was obtained by identifying all NPs with a radius larger than a cut-off radius defined as twice the predefined radius ($\langle r_{0A} \rangle$) of the primary NPs (*i.e.* $r_{\text{cutoff}} = 2\langle r_{0A} \rangle$), calculating the area of these agglomerates and normalizing by dividing by the total area of all the NPs. When $\theta_{\text{aggl},A} = 0\%$, no agglomeration is observed, while $\theta_{\text{aggl},A} = 100\%$ means that all the primary NPs are agglomerated. If the size distribution of the primary NPs is relatively low, this method provides a good estimate of the fraction of agglomerates greater than r_{cutoff} .

(B) A second fraction of agglomerates was obtained from the radius distribution curve. An estimate of the “mean radius” of the primary NPs ($\langle r_{0B} \rangle$) was obtained as the radius of the highest (and usually first) peak of the bootstrapped radius distribution histogram. The data-points below $\langle r_{0A} \rangle$ were mirror-imaged, and a bell-shaped first order Gaussian function was fitted to the data. This Gaussian fit often corresponds to the size distribution of primary NPs. A second order Gaussian fit was also added, corresponding to small agglomerates. The areas of primary NPs (A_{prim}) and of small agglomerates (A_{small}) as well as the total area (A_{tot}) were calculated as:



$$A = \sum_{j=1}^n \pi r_j^2 \frac{P(r_j)}{n} \quad (2)$$

where $P(r_j)$ is the radius-dependent probability of each curve, r_j is the NP radius of bucket j , and n is the total number of buckets in the histogram. The total fraction of agglomerates is thus defined as $\theta_{\text{aggl},B} = 1 - A_{\text{prim}}/A_{\text{tot}}$. As in method A, $\theta_{\text{aggl},B} = 0\%$ means no agglomeration, while a value of 100% means that all the primary NPs are agglomerated. Homogeneously distributed clusters close to the size of large primary NPs could potentially be considered as primary NPs with this method. The method is free from arbitrary model parameters.

(C) The relative cluster size was obtained by calculating the “average radius” ($\langle r \rangle$) in the micrographs and dividing by the “mean radius” of primary NPs ($\langle r_{0B} \rangle$, from method B) giving the relative average radius $r_{\text{rel},B} = \langle r \rangle / \langle r_{0B} \rangle$. If $r_{\text{rel},B}$ is close to or equal to 1, less agglomeration is present, while a higher $r_{\text{rel},B}$ value indicates more agglomeration. This strategy is robust, relatively easy to implement and does not use any arbitrary model parameters. However, in the case of homogeneously sized nanoclusters and very few primary NPs, the $r_{\text{rel},B}$ value underestimates the ratio of agglomerates. Therefore, it is valuable to compare $r_{\text{rel},B}$ with $r_{\text{rel},A} = \langle r \rangle / \langle r_{0A} \rangle$. Method C is considered more reliable than the methods A and B when most clusters are slightly larger than or slightly smaller than the r_{cutoff} .

(D) The face-to-face (or centre-to-centre) 2D-distances between NPs were compared to the corresponding theoretical distances for randomly positioned, dispersed spheres. The latter distances were calculated on 2D-slices cut from Monte-Carlo generated 3D-geometries of composites with non-intersecting, randomly positioned spherical fillers.⁴² The theoretical (2D) centre-to-centre distance for a system with equally sized particles with diameter 1 is described as a function of volume filler fraction ϕ as

$$D_{\text{cci}}^1(\phi) = \left(\frac{a_i}{1 + b_i \times \phi} \right)^{c_i} + d_i \quad (3)$$

where the subscript i corresponds to the i^{th} neighbour. The values used were $a = 131.57$, $b = 73\,978$, $c = 0.5622$, $d = 0.5353$ for the nearest neighbour and $a = 509.02$, $b = 30\,746$, $c = 0.4994$, $d = 0.01020$ for the 51st nearest neighbor.⁴² To obtain distances for systems with particle diameters other than 1, $D_{\text{cci}}^1(\phi)$ was multiplied by the diameter of the primary NPs. When method B is used to calculate the radius of the primary NPs, the theoretical centre-to-centre distance thus becomes $\check{D}_{\text{cci},B} = 2\langle r_{0B} \rangle D_{\text{cci}}^1(\phi)$ and the theoretical face-to-face distance is $\check{D}_{\text{ffi},B} = \check{D}_{\text{cci}} - 2\langle r_{0B} \rangle$.

If the primary NPs are clearly distinguishable, the ratio $\Delta_{\text{cci},B} = \langle D_{\text{cci}} \rangle / \check{D}_{\text{cci},B}$ of the distance $\langle D_{\text{cci}} \rangle$ and the analytical distance $\check{D}_{\text{cci},B}$ will decrease with decreasing dispersion, but if the primary NPs within the agglomerates are not treated as separated, $\Delta_{\text{cci},B}$ will instead increase with decreasing dispersion. This can be handled by introducing the cut-off radius (r_{cutoff}) from method A and treating the observed NPs with a radius larger than r_{cutoff} as clusters of adjacent NPs on a honey comb

lattice.¹² All the distances and the average radius are then recalculated. With this adjustment, a value of the ratio $\Delta_{\text{cci},D}$ less than 1 corresponds to a poorer dispersion, while a value of $\Delta_{\text{cci},D}$ greater than 1 corresponds to a better dispersion. The same applies for the new face-to-face ratio $\Delta_{\text{ffi},B}$. When experimental distances are compared with theoretical, it is important to use the volume filler fraction (ϕ) calculated from the micrograph to avoid systematic errors introduced due to visibility differences of NPs in cross-sections, deposited or microtomed samples.

2.4 Instrumentation and characterization methods

Fourier Transform Infrared spectroscopy (FTIR, 4000–600 cm^{-1}) was carried out with a Perkin-Elmer Spectrum 2000 FTIR instrument equipped with a MKII Golden Gate, single reflection ATR system (Specac Ltd, London, UK). The ATR-crystal was a MKII heated diamond 45° ATR top-plate.

A Kaiser-test kit, containing phenol (~80% in ethanol), potassium cyanide in H_2O : pyridine, and ninhydrin (6% in ethanol), was used to determine the concentration of primary amines on ZnO-APTES using a Cary UV-Vis Spectrophotometer with CaryWinUV software detecting the absorbance at 576 nm, which is associated with the amine-ninhydrin-complex concentration.^{44,45}

Thermogravimetric analysis (TGA) was performed on a Mettler Toledo TGA/DSC1, using STARe software to process the data. The samples were heated from 50 to 700 °C in ceramic cups at a rate of 10 °C min^{-1} in N_2 (flow rate 50 mL min^{-1}).

Transmission electron microscopy (TEM) of ZnO NPs was performed using a Hitachi HT7700 TEM at 100 kV accelerating voltage. Diluted suspensions (<0.1 mg mL^{-1}) of unmodified or modified NPs in EtOH or THF were applied on ultrathin carbon-coated copper grids (Ted Pella, Inc.) and examined in the microscope after drying.

A Hitachi S-4800 field emission scanning and transmission electron microscope (SEM/STEM) was used to study cross-sections of composites prepared by freeze-fracturing in liquid nitrogen and dispersions of pristine and modified NPs applied onto ultrathin carbon coated copper grids (TED Pella, Inc.).

DMF-SEC was carried out using a TOSOH EcoSEC HLC-8320GPC system equipped with an EcoSEC RI detector, three columns (PSS PFG 5 μm ; Microguard, 100 Å, and 300 Å) columns (M_w resolving range: 0.1–300 kDa) from PSS GmbH, using DMF (0.2 mL min^{-1}) with 0.01 M LiBr as the mobile phase at 50 °C. A conventional calibration method was used utilizing poly(methyl methacrylate) standards. Corrections for flow rate fluctuations were applied using toluene as an internal standard. PSS WinGPCUnity software version 7.2 was used to process the data.

2.4.1 Dielectric characterization. All the samples were conditioned at 23 °C and 0% RH for at least two days prior to dielectric characterization measurements. The contact pressure was 4 kPa for the electrode and 23 kPa for the guard. Soft and smooth rubber films ensured good contact to the electrodes without significant deformation. Relative permittivity and dielectric loss-tangent were measured using an insulation



diagnostic analyser (Megger IDAX300) with its output voltage connected to a large planar electrode below the sample, and its input connected to a guarded brass electrode with a diameter of 20 mm and a guard gap of 0.15 mm, above the sample. Dry samples were tested inside a climate chamber (Weiss Technik) set to 20 °C or 50 °C at 0% of RH. The voltage was sinusoidal at 200 V (peak) with frequencies sweeping from 10 kHz to 0.01 Hz. This type of measurement includes the effects of polarization, capacitance, and conduction. Resistivity was measured inside a climate chamber (CTS C-20/350) at -10 °C, 23 °C, and 50 °C. The samples were positioned on top of a high-voltage electrode connected to a Heinzinger PNC5 high-voltage DC power-supply outside the chamber. The brass electrode used for permittivity measurements was positioned on top of the film and connected to a Keithley 6512 electrometer. The polarization process took place under a constant DC electric field for 12 min. The resistivity was calculated based on the final polarization current. Electrical breakdown tests were performed on film samples between two spherical electrodes (6 mm in diameter), immersed in silicone oil. An AC voltage at 50 Hz was applied between the electrodes, starting at zero and increasing at 1 kV s⁻¹ peak value, in the style of method 'A' in ASTM D149-97a. The electrodes were adjusted to provide sufficient force to prevent the sample from sliding between the electrodes. The sample thickness was measured with a Mitotoyo ABS Digimatic Indicator ID-SX (6 mm in diameter) at each tested site and the measured value was used to divide the recorded breakdown voltage.

3. Results and discussion

The major advantage, as well as challenge, of NPs is the control of the chemistry of their large specific surface area. The manufacturing of pure NPs with a defined size and surface chemistry on a large scale is still a significant challenge. Today, a range of commercial ZnO NPs of various purities and surface reactivities are available, but the presence of organic remnants may affect any subsequent surface modification and thus the final properties of nanocomposites. Therefore, two types of commercially available ZnO NPs were compared (see the section "Comparison of commercial ZnO NPs" in the ESI†) and it was found that the organic content of ZnO NPs produced by flame-spray pyrolysis⁴⁶ was 10 times less than that of ZnO NPs produced by salt-precipitation, which also contained residual salt-precursors⁴⁷ detected by FTIR and TGA (Fig. S1 and S2†). Further, the resistivity of a silicone rubber with ZnO NPs containing salt-precursors and pure ZnO NPs was ~10¹⁰ Ωm and ~10¹⁴ Ωm, respectively (Fig. S3†). The chemically pure, non-porous and highly crystalline ZnO NPs produced by flame-spray pyrolysis were therefore selected for this study. Micrometer sized ZnO particles (and bulk ZnO) are known to be semi-conductors with properties depending on doping elements and grain-boundaries.^{48,49} However, flame-sprayed, highly pure ZnO NPs neither contain doping elements nor large grain-boundaries. Low filling fractions of pure metal-oxide NPs have significantly reduced the conductivity by the trapping of charge carriers.^{11,12} The trapping has mainly been attributed to "deep

traps" on the NP-interface;⁵⁰ the induction of dipoles;⁵¹ and the scattering or charge differences by the NP-polymer interphase.^{8,52} In this study, we designed the interphase of flame-sprayed pristine ZnO NPs⁴⁶ by silanization and controlled polymer grafting in order to tune the dielectric properties of polymer nanocomposites.

3.1 Detection of accessible amines of ZnO-APTES

ZnO NPs were silanized by aminopropyltriethoxysilane (APTES) (Fig. S4a†). The accessible primary amines of the silane coating were monitored by spectrophotometry (at 570 nm) through the formation of the Ruhemanns-Blue complex with ninhydrin, using the Kaiser-test (Fig. S4b†).^{44,45} The concentration of primary amines was shown to be directly related to the final graft density, as the ninhydrin-complex detects the most accessible amines.⁴² The amine density was calculated using Lambert-Beer's law as previously described by Malmström *et al.*⁴² and was found to be 0.08 ± 0.01 amines nm⁻².

3.2 Characterization of ZnO-g-PBMA and free PBMA

Prior to the controlled grafting of PBMA from ZnO NPs, ATRP-initiators were immobilized on the primary amines of ZnO-APTES by the formation of an amide-bond (ZnO-Br, Fig. 1) as described in previous reports (see the ESI†).^{42,43} In this study, the SI-ATRP grafting was conducted from the end group of ZnO-Br in the presence of a sacrificial initiator to allow fast and easy characterization of the polymerization (Fig. 1).

The PBMA-grafts were cleaved and the degrafted NPs characterized by FTIR (Fig. 2). FTIR-spectra of ZnO-APTES, ZnO-Br and grafted ZnO NPs showed the absorbance peaks of amines, amides, and carboxyl groups or their absence in pristine and degrafted ZnO NPs at 1800–1500 cm⁻¹ (Fig. 2 enlarged image) and the characteristic absorbance of C-H around 2930 cm⁻¹, which confirms the successful surface modification of the NPs (Fig. 2).

According to TGA, the concentration of immobilized initiators on ZnO-Br was 0.021 μmol Br per mg of ZnO-Br, which is equal to 0.8 initiators nm⁻². The concentration of initiators was ten times higher than the determined amount of available amines and can be explained by the greater accessibility of the initiators compared to that of the bulky ninhydrin-complex; the initiators are able to reach primary amines deeper inside the "gooey-layer" of silane, as suggested by Malmström *et al.*⁴²

The free polymers were characterized by DMF-SEC and their average molar masses were compared to those of the cleaved chains (Table 1, Fig. S5 and S6†). The narrow dispersities indicate good control (Table 1). Free PBMA-chains were slightly longer and exhibited a slightly more narrow size distribution than the cleaved PBMA-grafts, in agreement with grafting from cellulose substrates.⁵³

According to the thermograms, the content of volatile organics increased with each surface modification, and the mass-losses are displayed next to the sample names in Fig. S7.† The average graft density of ~0.08 grafts nm⁻² was confirmed from the correlation between the molar mass of cleaved grafts and the organic mass losses, and this is equal to a grafting



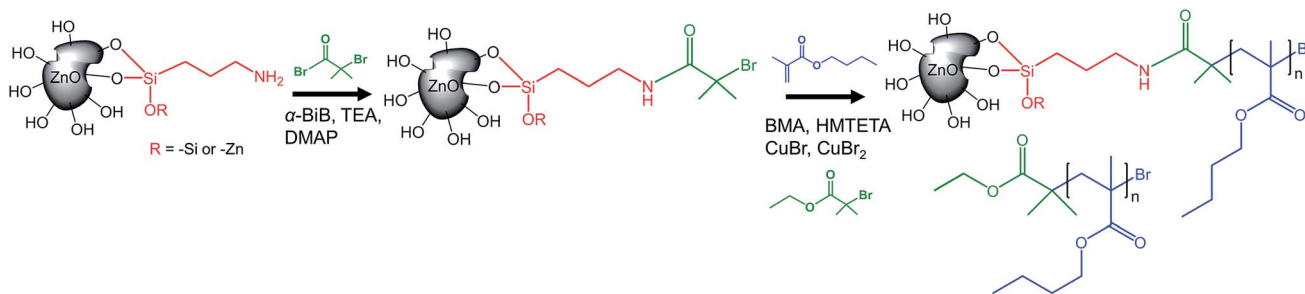


Fig. 1 The immobilization of the ATRP-initiator (green), and the surface-initiated grafting of BMA (blue) from ZnO-APTES and ZnO-Br, respectively. The free chains of PBMA are simultaneously polymerized from the sacrificial initiator by ATRP in parallel with the grafting reaction.

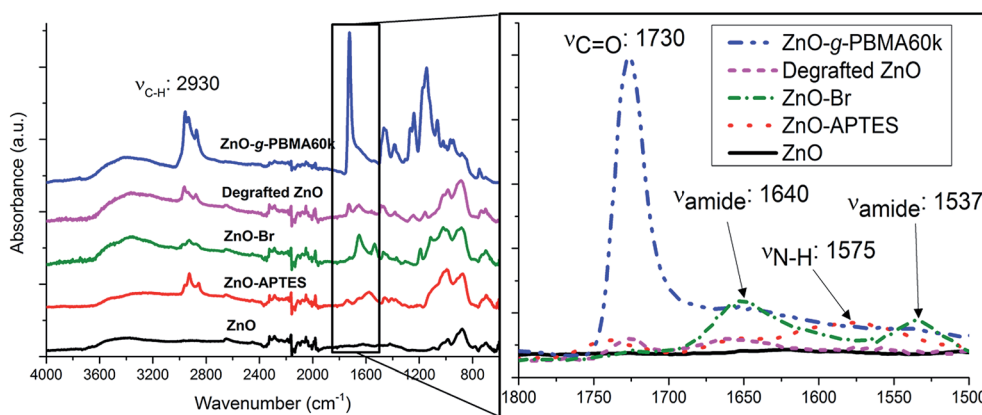


Fig. 2 FTIR spectra of ZnO, ZnO-APTES, ZnO-Br, ZnO-g-PBMA60k and degrafted ZnO between 4000 and 600 cm^{-1} . Spectra have been vertically scaled and offset for clarity. The enlarged spectrum shows detailed overlapping spectra between 1800 and 1500 cm^{-1} without offset.

efficiency of $\sim 10\%$. The calculated molar mass of grafts (M_g) and the degree of polymerization of the grafts (N_g) in Table 1 were obtained from the grafting density and the organic content according to eqn (S1) in the ESI.†

Finally, the band gaps of pristine ZnO, ZnO-g-PBMA10k and ZnO-g-PBMA60k (Table S2†) were calculated according to eqn (S2) in the ESI,† using the absorption peak obtained by UV-Vis spectroscopy, Fig. S8.† The tiny red-shift of grafted ZnO NPs indicated that the band gaps did not significantly change with surface grafting and thus remained constant at ~ 3.3 eV.

3.3 Dispersion of ZnO, ZnO-APTES and ZnO-g-PBMA

It is challenging to determine the distribution of primary NPs and the fraction of agglomerates from SEM and TEM images, or

dynamic light scattering, especially from NPs with a broad size distribution. The size of smaller agglomerates (nanoclusters) may be similar to that of larger primary NPs, which creates the illusion of well-dispersed NPs at low magnification, when in fact small agglomerates are present. Another difficulty is in distinguishing between agglomerates and clusters of individually separated NPs. To improve and to simplify the distinction between single NPs and agglomerates, we developed four methods to assess the radius and the dispersion of NPs considering different aspects. Methods A and B determine the respective fractions of agglomerates ($\theta_{\text{aggl},A}$ and $\theta_{\text{aggl},B}$) by using either the user-defined cut-off radius (r_{cutoff}) or the “mean radius” (r_{0B}) at the highest peak of the distribution histogram. Method A is reliable for detecting both homogeneously

Table 1 Comparison of molar masses and dispersities of free PBMA-chains, cleaved PBMA-grafts and calculated average molar masses of PBMA and correlating degree of polymerization

Name of NPs	Free PBMA		Cleaved grafts		Calculated	
	M_w (g mol^{-1})	D_M	M_w (g mol^{-1})	D_M	M_g (g mol^{-1})	N_g
ZnO-g-PBMA10k	13 000	1.18	9000	1.09	10 000	70
ZnO-g-PBMA50k	54 000	1.12	50 000	1.19	47 000	331
ZnO-g-PBMA60k	68 000	1.17	60 000	1.25	61 000	429
ZnO-g-PBMA80k	101 000	1.22	74 000	1.30	83 000	584



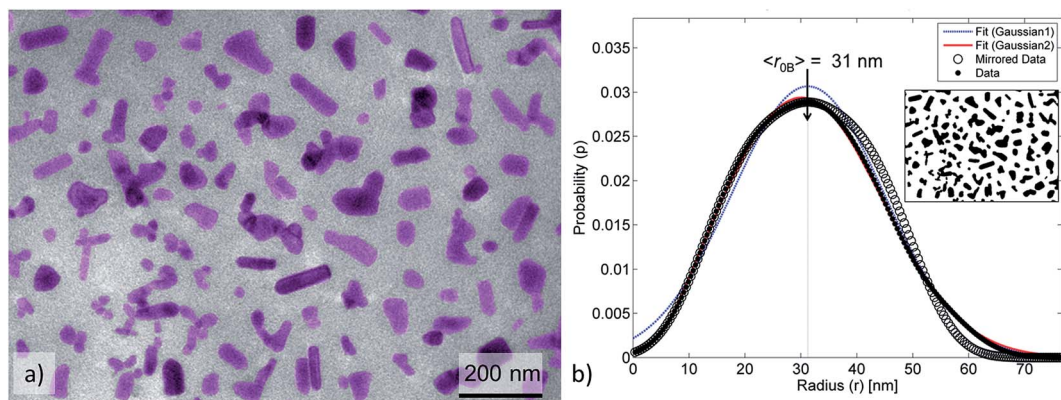


Fig. 3 (a) TEM images of an annealed and densely packed film of ZnO-g-PBMA80k with computer-assisted coloring of ZnO NPs. (b) Fitting of the NP-size by a first and a second order Gaussian distribution and calculation of average radius.

distributed agglomerates and heterogeneously distributed well-separated NPs, but it is dependent on the user-defined r_{cutoff} unlike method B. Method C describes two ways to determine the average radius ($\langle r \rangle$) relative to the radii determined by methods A and B ($r_{\text{rel,A}}$ and $r_{\text{rel,B}}$). Method C has been found to be more robust for the detection of nanoclusters that are slightly smaller or slightly larger than the r_{cutoff} . Method D calculates the face-to-face distance (D_{ff1}), the centre-to-centre distance (D_{cci}), and the deviation ratios (Δ_{ff1} and Δ_{cci}) relative to a completely randomized dispersion. These versatile analytical methods can be applied to AFM, TEM, SEM and STEM images.

3.3.1 Primary particle size and face-to-face distance of annealed ZnO-g-PBMAs. In order to determine the size and the face-to-face distance (D_{ff1}) of packed ZnO NPs prior to the mixing into PDMS matrices, suspensions of dispersed grafted NPs were deposited on TEM-grids, and annealed at 80 °C for 3 h. Annealed ZnO-g-PBMAs with longer PBMA-grafts exhibited an efficient face-to-face separation, and restriction of percolation, as they formed films with individually separated and densely packed NPs (~28 vol%), see Fig. 3. Therefore, ZnO-g-PBMA60k and ZnO-g-PBMA80k were used to determine the average radius ($\langle r \rangle$) of primary NPs, and thus the r_{cutoff} (Table 2). According to methods A and B, the average radius of primary NPs was 31–35 nm, in accordance with the value of 33.5 nm given by the

supplier. In some images (Fig. 3), method A did not detect any agglomerates ($\theta_{\text{aggl0,A}}$), whereas 0–5% agglomerates were detected by method B ($\theta_{\text{aggl0,B}}$), which indicates the benefit of method B, without arbitrary parameters.

The annealed ZnO-g-PBMAs with short grafts (ZnO-g-PBMA10k) did not form continuous films, but frequently separated the NP-cores of agglomerated nanoclusters (Fig. 4c). Both the face-to-face distance (D_{ff1}) to the closest neighbour ($D_{\text{ff1,D}}$) and the corresponding deviation ratio ($\Delta_{\text{ff1,D}}$) increased with graft length, using the honeycomb packing strategy of method D (Table 2). Deviation ratios as high as 14 indicate good fitting to a densely packed honeycomb structure despite the heterogeneous geometries of the ZnO NPs.

3.3.2 Fraction of agglomerates, average radii and distribution of non-annealed NPs. TEM and STEM images of non-annealed ZnO, ZnO-APTES and ZnO-g-PBMAs were studied and compared by methods A–D and provided a better insight into the spontaneous agglomeration caused by the long-range (polar) and short-range (vdW) interactions of the samples (Fig. 4). The images at different magnifications (1.5k to 40k), were transformed into high-contrast images, and the fractions of agglomerates, the radii, the relative radii, the face-to-face distances, and the deviation ratios (Table 2), as well as the size distributions of primary NPs and the agglomerate ratio were calculated by methods A–D (Fig. 5).

Table 2 Fraction of agglomerates, average and mean radius, relative radii, face-to-face distance and deviation ratio to the closest neighbor for ZnO, ZnO-APTES and ZnO-g-PBMA (10k, 60k and 80k). Numbers with * include only data from annealed samples

Name of the NP	Method A	Method B	Method C		Method D			
	Fraction of agglomerates (%)	Fraction of agglomerates (%)	Average radius (nm)	Mean radius (nm)	Relative average radius	Face-to-face distance (nm)	Face-to-face deviation ratio	
	$\theta_{\text{aggl0,A}}$	$\theta_{\text{aggl0,B}}$	$\langle r \rangle$	$\langle r_{0B} \rangle$	$r_{\text{rel,A}}$	$r_{\text{rel,B}}$	$D_{\text{ff1,D}}$	$\Delta_{\text{ff1,D}}$
ZnO	90	90	60–70	30–40	2.0	2.0	—	0.4–0.5
ZnO-APTES	80–90	0–50	70–90	70–90	2.4	1.1	—	0.1–0.3
ZnO-g-PBMA10k	30–70	70–80	40–50	20–40	1.3	1.5	6–8*	0.3–0.6
ZnO-g-PBMA60k	0–50	0–60	30–60	20–50	1.2	1.1	21–22*	0.8–11
ZnO-g-PBMA80k	0–30	0–40	30–40	30–40	1.1	1.1	26–28*	1.1–14



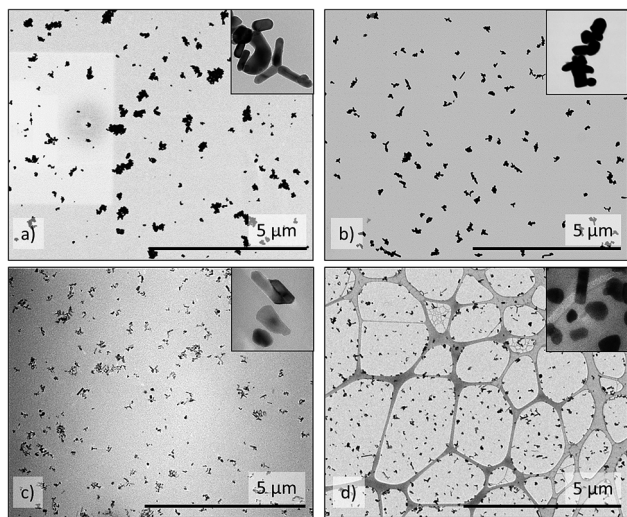


Fig. 4 Transmission images of agglomerates and primary particles of (a) pristine ZnO NPs, (b) ZnO-APTES, (c) ZnO-*g*-PBMA10k and (d) ZnO-*g*-PBMA80k. The inset pictures of annealed samples are 200 nm wide.

For pristine ZnO NPs, methods A and B successfully determined similar fractions of agglomerates ($\sim 90\%$, Table 2) despite the heterogeneous geometry of the NPs (Fig. 4a and 5a).

The large amount of agglomerates indicated strong NP-NP attraction (polarity). The average radius ($\langle r \rangle$) was approximately twice as large as the radius of the primary ZnO NPs.

The ZnO-APTES formed homogeneously distributed nanoclusters with agglomerated cores classified as 80–90% agglomerates (Fig. 4b) and only a few primary NPs (Fig. 5b). The formation of nanoclusters was detected by method A (as $\theta_{\text{aggl},A} \gg \theta_{\text{aggl},B}$) and confirmed by method C (since $r_{\text{rel},A} \gg r_{\text{rel},B}$), and was probably an effect of insufficient shielding of short-range core-core attractions during drying (Table 2). The agglomerates and distribution of ZnO-*g*-PBMA10k appeared very differently compared to ZnO-APTES (Fig. 4c and 5c). Both the radii ($\langle r_{0B} \rangle$ and $\langle r \rangle$) were close to the radius of the primary NPs (~ 33.5 nm), and thus described individual NPs separated from the closest neighbours (Table 2). The fractions of agglomeration were different ($\theta_{\text{aggl},A} < \theta_{\text{aggl},B}$), while the relative radii were similar ($\langle r_{\text{rel},A} \approx \langle r_{\text{rel},B} \rangle$), indicating a heterogeneous distribution of nanoclusters. The large variations in face-to-face distances of primary NPs within and between nanoclusters suggested that some core-core attraction between ZnO-*g*-PBMA10k remained during drying, although the grafts prevented complete core-core agglomeration.

Multiple images of annealed and non-annealed NPs with long grafts (ZnO-*g*-PBMA60k and ZnO-*g*-PBMA80k) displayed

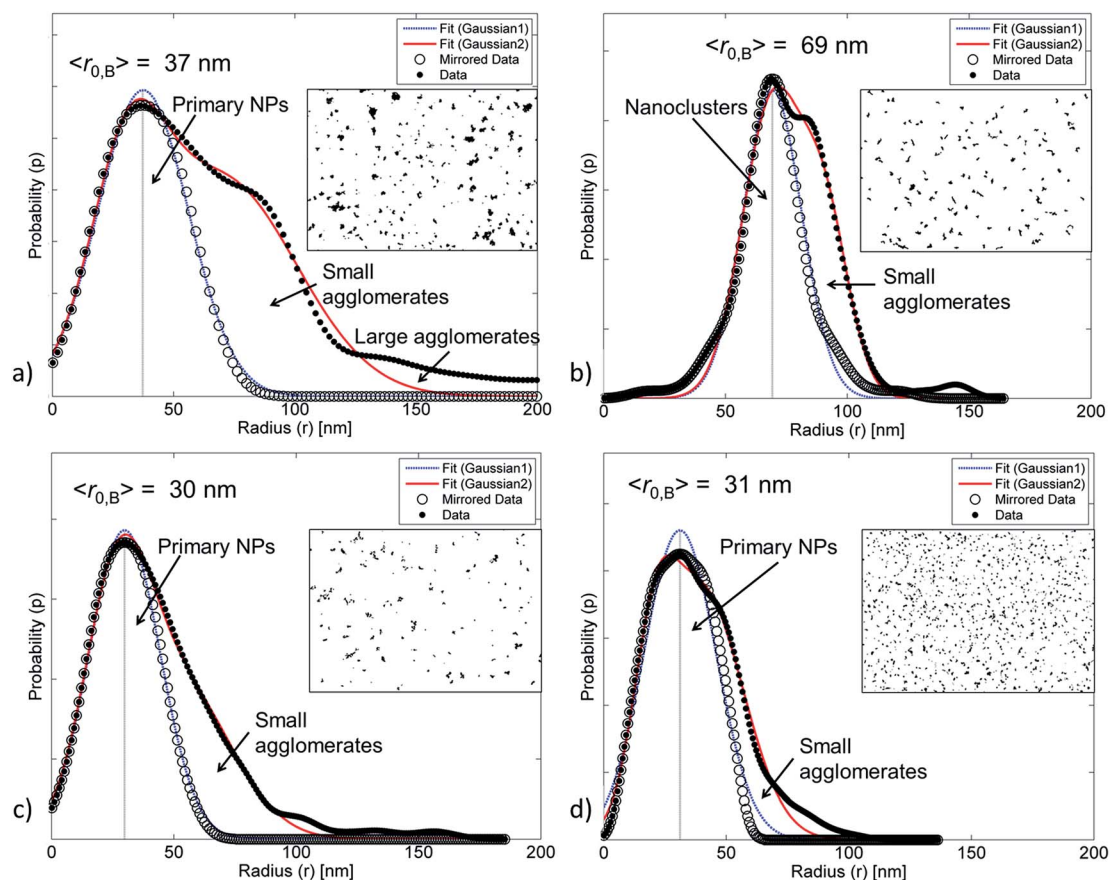


Fig. 5 The size distribution and the mean radius calculated from transmission images of (a) ZnO NPs, (b) ZnO-APTES, (c) ZnO-*g*-PBMA10k and (d) ZnO-*g*-PBMA80k. The arrows show the areas under the curves, representing the fraction of primary NPs, small and large agglomerates. The inset images are 12 μm wide cut-outs of the full images for simplified comparison.



Table 3 Names of the nanocomposites with grafted NPs, the N_M of the silicone matrices, the filling content of ZnO NPs, and the ratios of N_M/N_g

Name of the nanocomposite	Silicone matrix		ZnO NP content		N_M/N_g
		N_M	vol%	wt%	
<i>1.5ZnO-g-PBMA10k</i>	PDMS	847	1.5	8.4	12
<i>2.5ZnO-g-PBMA10k</i>	Silicone rubber	550	2.5	14	8
<i>1.5ZnO-g-PBMA60k</i>	PDMS	847	1.5	8.4	2
<i>2.5ZnO-g-PBMA80k</i>	Silicone rubber	550	2.5	14	0.9

similar radii ($\langle r \rangle \approx \langle r_{0B} \rangle$), equal to the radius of primary NPs. The fractions $\theta_{\text{aggl},A}$ and $\theta_{\text{aggl},B}$ were similar and low, and the relative radii were close to 1 (Table 2), suggesting good dispersion of the NPs. The face-to-face deviation ratio ($\Delta_{\text{ff},D}$) ranged from 0.8 to 11 for ZnO-g-PBMA60k and from 1.1 to 14 for ZnO-g-PBMA80k, indicating ordered separation of the NP cores by the grafts (Fig. 4d and 5d). The longer grafts effectively shielded both the short-range and long-range core-core attractions and thus formed well-dispersed primary NPs with a minor fraction of nanoclusters.

3.4 Morphologies of nanocomposites

To manufacture flexible dielectric nanocomposites, the ZnO NPs were mixed into silicone rubbers, commonly used in HV cable accessories (cable joints and terminations).^{54,55}

Two grades of silicone matrices were used, a pure laboratory grade of PDMS with a high degree of polymerization ($N_M = 847$) and a commercial silicone rubber (Sylgard® 184) with $N_M \approx 550$ prior to curing. The degree of polymerization of the grafts (N_g) on ZnO-g-PBMAs was varied in order to change the ratio of N_M/N_g to entropically favour different morphologies (Table 3). A rule of thumb for homopolymer nanocomposites is that a ratio of N_M/N_g less than 1 entropically favours dispersed NPs, while $N_M/N_g > 1$ causes phase separation, depending on the graft density and the curvature of the NPs.

The compatibility between PBMA-grafted NPs and silicone elastomers was investigated using Hansen's solubility parameters (HSPs) in order to estimate the enthalpic compatibility between the PBMA-grafts or pristine ZnO NPs and the silicone matrices. HSPs were selected because they account for interaction parameters such as hydrogen-bonds, dipolar intermolecular forces, and dispersion forces.³⁹ According to the HSPs (Table S1†), the ZnO NPs are compatible with silicone as the relative energy difference (RED) is less than 1 (Fig. 6a), which should give nanocomposites with a random or isotropic distribution of NPs. However, the RED for the PBMA-grafts and the silicone is equal to 1.09 which suggests that a semi-compatible "multi-polymer" nanocomposite will be obtained, as RED is approx. equal to 1 (Fig. 6b).

3.4.1 Nanocomposites of PDMS elastomer with 1.5 vol% NPs. Multiple films of neat PDMS elastomer (PDMS) and nanocomposites (*1.5ZnO*, *1.5ZnO-APTES*, *1.5ZnO-g-PBMA10k*, and *1.5ZnO-g-PBMA60k*) were prepared and subsequently cured to verify the reproducibility. Sample names in italics refer to films. The visual appearance was found to vary depending on the surface chemistry of the NPs (Fig. 7). The nanocomposites (0.6–0.7 mm thick) exhibited a drop in transmittance below 400 nm due to the absorbance of ZnO NPs (Fig. S9a†).

The nanocomposite films containing pristine ZnO NPs (*1.5ZnO*) were homogeneous and white translucent, while *1.5ZnO-APTES* and *1.5ZnO-g-PBMA10k* were more transparent

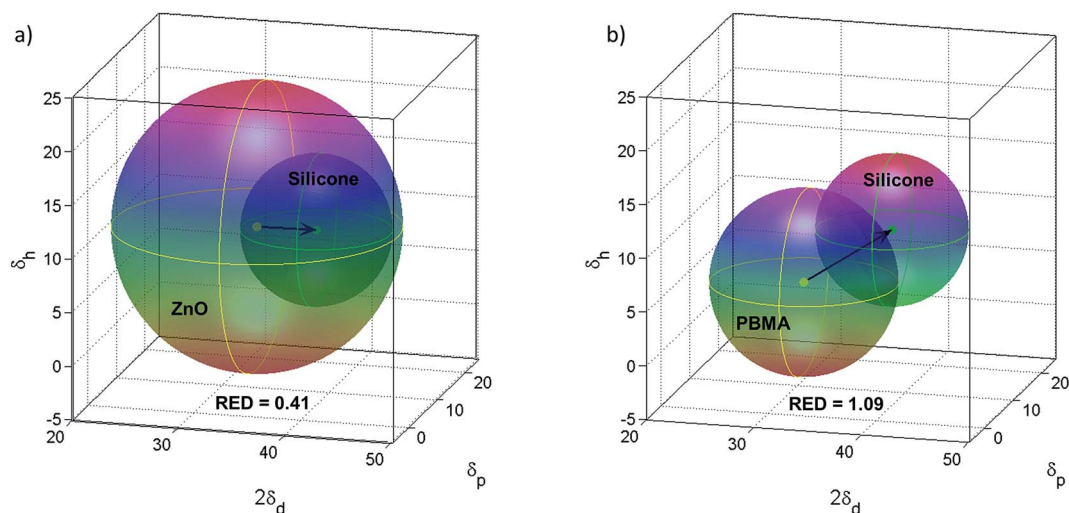


Fig. 6 (a) Hansen's solubility parameters for ZnO in silicone resin give RED = 0.41 indicating compatibility. (b) HSPs for PBMA in silicone resin indicate semi-compatibility as RED = 1.09.



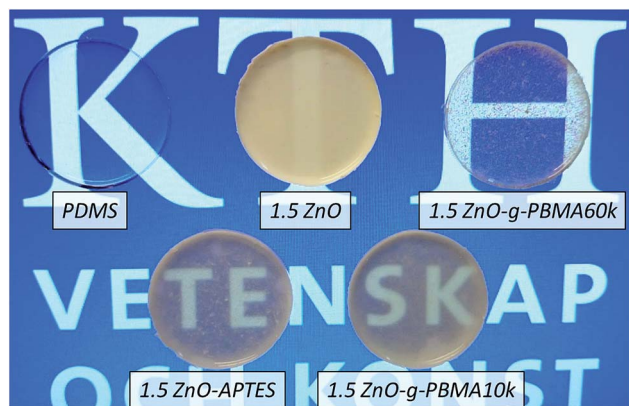


Fig. 7 Photo of neat PDMS and nanocomposites containing 1.5 vol% of ZnO NPs, ZnO-APTES, ZnO-g-PBMA10k or ZnO-g-PBMA60k.

and heterogeneous. The *1.5ZnO-g-PBMA60k* samples contained regions of NPs separated by almost completely transparent regions providing the highest transmittance among the nanocomposites (Fig. 7 and S9a[†]). The increase in transparency of coated ZnO NPs can be explained by a combination of matching of the refractive indices⁴³ and regions containing few NPs.

Cross-sections of *1.5ZnO* revealed randomized isotropic distributions of NPs and small nanoclusters incorporated in the PDMS-matrix (Fig. S10[†]), as an effect of the enthalpic compatibility between ZnO-NPs and the silicone matrix, according to the HSPs (Fig. 6). Cross-sections of *1.5ZnO-g-PBMA10k*, with N_M/N_g equal to 12 (Table 1) expectedly formed phase-separated rounded agglomerates of grafted NPs, as the short grafts were

entropically unable to be wetted by the much longer polymer matrix. More surprisingly, minor regions of distributed NPs were also present (Fig. 8a and b), and might be an effect of the semi-efficient shielding of the enthalpic interactions between the ZnO NPs and the silicone matrix, in agreement with the heterogeneous dispersions of ZnO-g-PBMA10k (Fig. 4c and 5c). Cross-sections of *1.5ZnO-g-PBMA60k* ($N_M/N_g = 2$) formed continuous superstructures of well-separated film-forming NPs (Fig. 8c and d and S11[†]). The long grafts appeared to entangle mainly with the other PBMA-grafts and partly with the matrix, as $N_M > N_g$, and formed continuous non-spherical agglomerates. This indicates that the initially well-dispersed ZnO-g-PBMA60k (in THF) self-assembled into superstructures of NPs during the thermal treatment of the films prior to curing. The interphase of grafts and matrix appeared to be seamless and the ZnO-cores were clearly separated by the grafts in agreement with annealed NPs (Fig. 3).

3.4.2 Nanocomposites of silicone rubber with 2.5 vol% NPs. The neat Sylgard® 184 (*silicone rubber*) and nanocomposites containing 2.5 vol% ZnO NPs (*2.5ZnO*), ZnO-g-PBMA10k (*2.5ZnO-g-PBMA10k*) and ZnO-g-PBMA80k (*2.5ZnO-g-PBMA80k*) were reproducibly prepared as white or white-translucent films (Fig. S9b[†]) similar to the nanocomposites with 1.5 vol% NPs, but they exhibited different NP morphologies (Fig. 9).

Cross-sections of *2.5ZnO-g-PBMA10k* ($N_M/N_g \approx 8$) showed the anticipated formation of large rounded and elongated agglomerates of closely packed NPs (6–8 nm). Some of the agglomerates percolated and formed superstructures of several hundred microns in size containing islands of neat silicone

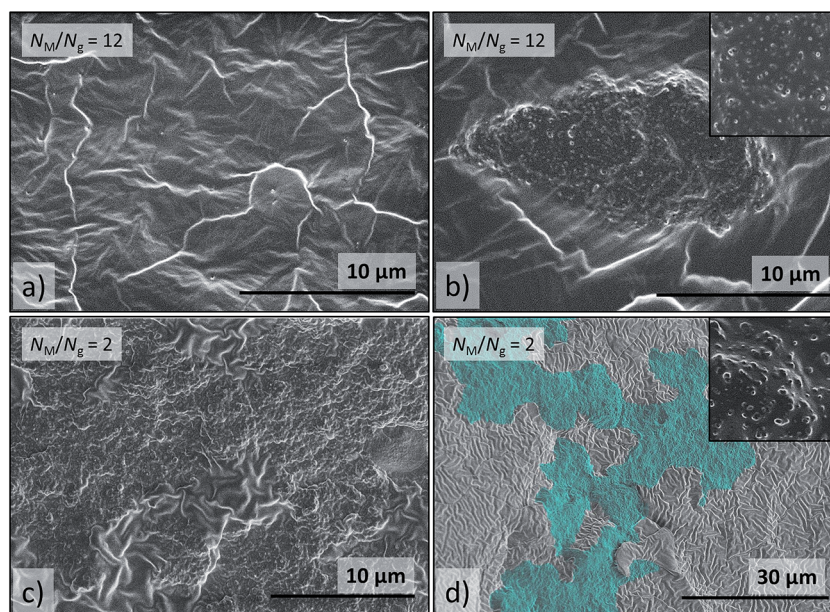


Fig. 8 SEM images of cross-sections of (a) and (b) *1.5ZnO-g-PBMA10k* ($N_M/N_g = 12$) and (c) and (d) *1.5ZnO-g-PBMA60k* ($N_M/N_g = 2$). (a) Region with low concentration of dispersed ZnO-g-PBMA10k, (b) a large spherical agglomerate of separated ZnO-g-PBMA10k, (c) continuous non-spherical agglomerate of ZnO-g-PBMA60k, (d) superstructure of ZnO-g-PBMA60k digitally highlighted in blue using Adobe Photoshop® for clarification. The original image is available in the ESI.† The inset pictures are 2 μm wide and show well-separated grafted NP cores of the agglomerates.



3.5 Dielectric properties of silicone nanocomposites

The dielectric properties of the sample films were characterized multiple times under dry conditions at temperatures below, at and above the T_g of the PBMA-grafts. The dielectric losses, the relative permittivity and the resistivity were linked to the NP-morphologies and the face-to-face distance of the NPs, while the breakdown strength was dependent on the NP-matrix compatibility (Fig. S12†).^{3,61} The breakdown strength was improved by the addition of compatible, highly pure ZnO NPs (despite the relatively large filling content), while it decreased with increasing graft-length for the semi-compatible PBMA-grafted NPs. Importantly, all breakdown voltage levels were well above the E-fields used in high-voltage cable accessories, joints, and rotating machines.

The focus of this study is the correlation of the dielectric losses and the resistivity with the NP-morphologies, the surface grafting and the inter-particle distances, which are described in the following sections.

3.5.1 Dielectric spectroscopy of PDMS samples with 1.5 vol% NPs. The dielectric properties of *PDMS*, *1.5ZnO*, *1.5ZnO-g-PBMA10k* and *1.5ZnO-g-PBMA60k* were evaluated at 20 °C and 50 °C (Fig. 11).

For *PDMS*, the real part of the relative permittivity ($\epsilon'_{r,PDMS} \approx 3$) exhibited no significant frequency dependence and was found to be slightly lower at 50 °C,⁶² due to a reduction in the number of aligned dipoles in *PDMS*. With the addition of pristine ZnO NPs (*1.5ZnO*), the ϵ'_r increased at 20 °C as an effect of the higher ϵ'_r of the NPs ($\epsilon'_{r,ZnO} \approx 8.5$).⁶³ The ϵ'_r was about the same for all the nanocomposites and may be an effect of the absence of impurities, doping agent and grain-boundaries of the highly pure, flame-sprayed ZnO NPs⁴⁶ (Fig. S1 and S2†). However, the ZnO-*g*-PBMA were slightly frequency dependent.

The dielectric loss ($\tan \delta = \epsilon''_r / \epsilon'_r$, where ϵ''_r is the imaginary component of ϵ'_r) of *PDMS* was low and made it possible to investigate the effect of added nanofillers (Fig. 11b and d). The $\tan \delta$ of *PDMS* increased with temperature at low frequencies and the slope originating from DC conduction was shifted towards higher frequencies at 50 °C. The addition of pristine ZnO NPs (*1.5ZnO*) led to a higher and constant $\tan \delta$ above 0.1 Hz, while $\tan \delta$ at 50 °C decreased at higher frequencies.

At both 20 and 50 °C, the addition of grafted NPs introduced a frequency-dependent $\tan \delta$, which resulted in lower losses at higher frequencies than with pristine ZnO NPs. This effect is attributed to the absence of polar groups (–OH and moisture) at the interface of the ZnO-*g*-PBMA. At 20 °C, the

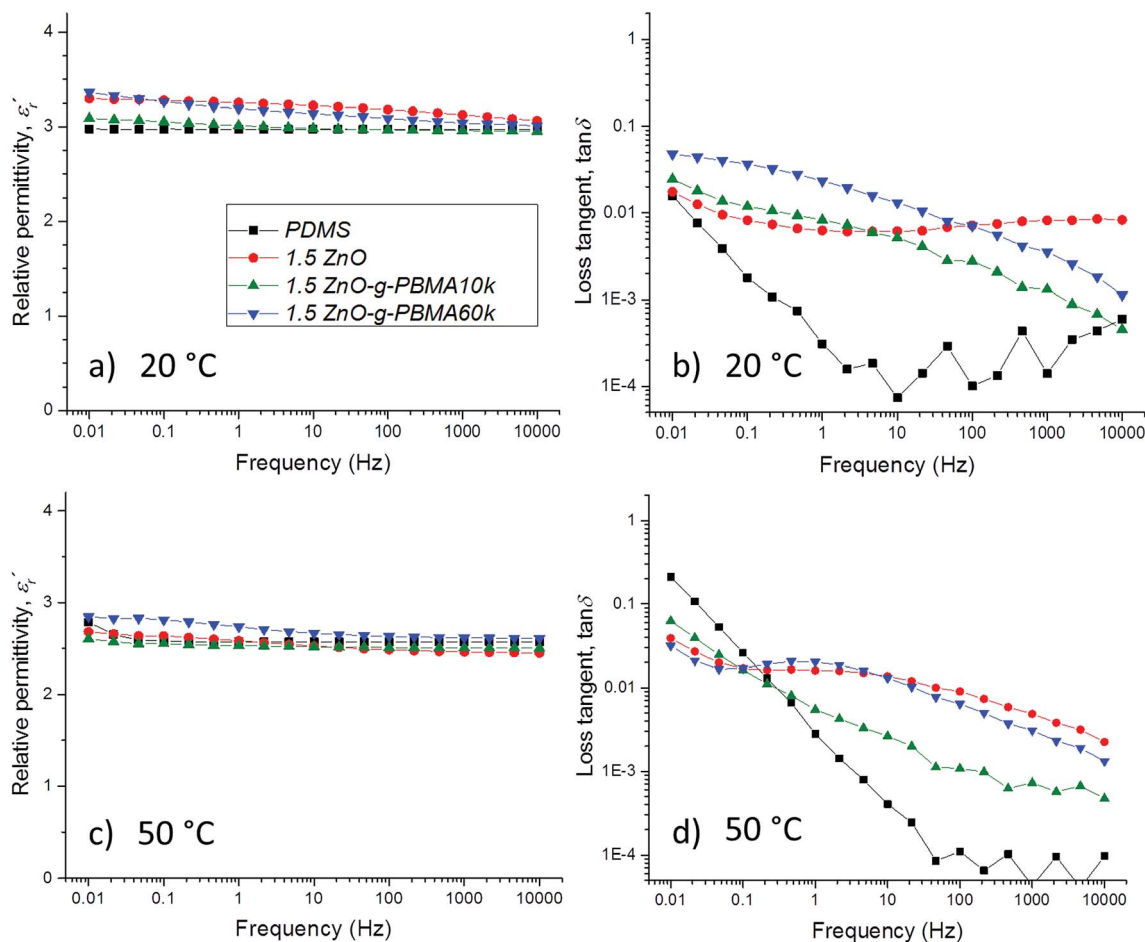


Fig. 11 Dielectric spectroscopy data of neat *PDMS*, *1.5ZnO*, *1.5ZnO-g-PBMA10k* and *1.5ZnO-g-PBMA60k* at 20 °C (a and b) and at 50 °C (c and d). Fig. (a) and (c) show the relative permittivity, ϵ'_r versus frequency, and (b) and (d) the loss tangent, $\tan \delta$ versus frequency.



1.5ZnO-g-PBMA60k suffered greater losses at low frequencies than 1.5ZnO-g-PBMA10k . This may be attributed to the slower orientation of entangled long PBMA-grafts in the superstructures of 1.5ZnO-g-PBMA60k . However, at $50\text{ }^\circ\text{C}$ and at low frequencies, $\tan\delta$ decreased and 1.5ZnO-g-PBMA60k exhibited the lowest losses of all the samples (Fig. 11d). The non-linear behaviour of the $\tan\delta$ may be an effect of the glass transition of the entangled long PBMA-grafts, and the lower DC conductivity can be explained by the face-to-face distance of 21–22 nm (Table 2), which is longer than the hopping distance of charge carriers (<10 nm) according to Wang *et al.*⁶⁴

3.5.2 Dielectric spectroscopy of silicone rubber samples with 2.5 vol% NPs. To evaluate the effect of NPs in a commercial grade of silicone rubber, Sylgard® 184 was used. It was observed that the neat silicone rubber (*silicone rubber*) had a significantly higher dielectric loss than PDMS (Fig. 11b and d and 12b and d), which is probably a result of the reinforcing silica filler. Therefore, a higher filling ratio of NPs was used than in the PDMS-based nanocomposites. Dielectric spectroscopy data of *silicone rubber*, 2.5ZnO , 2.5ZnO-g-PBMA10k , and 2.5ZnO-g-PBMA80k at $20\text{ }^\circ\text{C}$ and $50\text{ }^\circ\text{C}$ are shown in Fig. 12.

The ϵ'_r of *silicone rubber* was observed to be similar to that of PDMS (Fig. 11a and c and 12a and c). However, the increase in

ϵ'_r below 0.1 Hz, observed for *silicone rubber*, and also for 2.5ZnO-g-PBMA10k (Fig. 12a and c), has previously been explained by a “quasi-DC” conduction double-layer effect,^{52,65} due to the formation of small “capacitors”, or dipoles, as the charges are located on opposite sides of the NPs (*i.e.* fumed silica or ZnO-g-PBMA10k). The slope of $\tan\delta$ in *silicone rubber* and 2.5ZnO-g-PBMA10k was close to -1 below ~ 50 Hz. The 2.5ZnO-g-PBMA10k exhibited the highest $\tan\delta$ below ~ 50 Hz, and an increase in the DC conductivity, caused by the superstructures with face-to-face distances close to the hopping distance (<10 nm) (Fig. 12b and d).⁶⁴ However, above ~ 50 Hz, the $\tan\delta$ can be significantly reduced in agreement with what was seen for 1.5ZnO-g-PBMA10k and 1.5ZnO-g-PBMA60k .

The isotropic morphology of NPs in 2.5ZnO and 2.5ZnO-g-PBMA80k effectively reduced the “quasi-DC” effect, since the dispersed NP-interphases immobilize the charge carriers (Fig. 12c and d). For 2.5ZnO , $\tan\delta$ was constant over the investigated frequency range and showed the highest value at 10 kHz and among the lowest at 0.01 Hz (less DC conduction). The 2.5ZnO-g-PBMA80k (containing dispersed grafted NPs) exhibited a low $\tan\delta$ at both low and high frequencies.

3.5.3 Relationship between the relative dielectric losses and the NP morphology. The $\tan\delta$ values of 1.5ZnO-g-PBMA10k ,

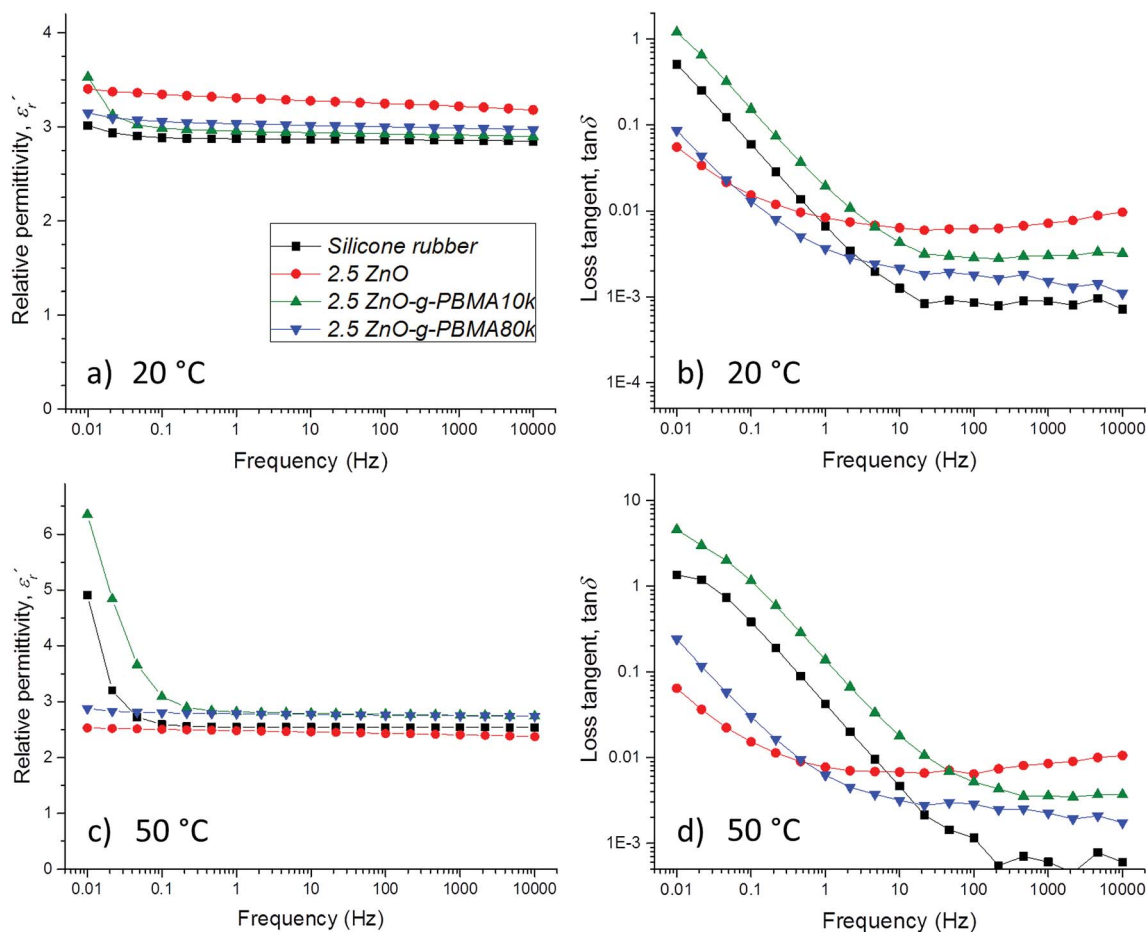


Fig. 12 Dielectric spectroscopy data of *silicone rubber*, 2.5ZnO , 2.5ZnO-g-PBMA10k and 2.5ZnO-g-PBMA80k at $20\text{ }^\circ\text{C}$ (a and b), and $50\text{ }^\circ\text{C}$ (c and d). Fig. (a) and (c) display the relative permittivity, ϵ'_r versus frequency, and (b) and (d) the loss tangent, $\tan\delta$ versus frequency.



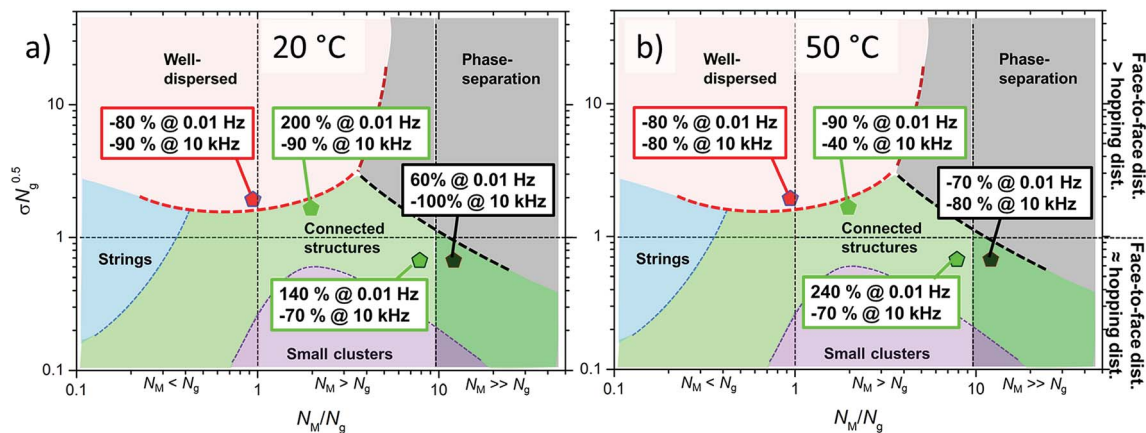


Fig. 13 The relative loss tangent as a percentage at 0.01 Hz and 10 kHz for the nanocomposites with grafted NPs at 20 °C (a) and 50 °C (b).

1.5ZnO-g-PBMA60k, *2.5ZnO-g-PBMA10k* and *2.5ZnO-g-PBMA80k* were compared with $\tan \delta$ of their corresponding neat silicone at 0.01 Hz, expressed as percentages. Because of the large scattering in $\tan \delta$ of neat silicone at 10 kHz (close to the noise-level of the instrument), the samples were compared with their corresponding nanocomposites with pristine NPs, in order to quantify the effect of the PBMA-grafts. The relative $\tan \delta$, as

a percentage, was related to the morphology and the face-to-face distance of the NPs at 20 °C and 50 °C (Fig. 13). All four nanocomposites with grafted NPs exhibited lower losses at 10 kHz at both temperatures, due to the less polar interphases of ZnO-*g*-PBMA than pristine ZnO NPs. The relative $\tan \delta$ at 10 kHz decreased at 50 °C for all four samples. The *2.5ZnO-g-PBMA80k* exhibited 80–90% lower relative losses at both frequencies and

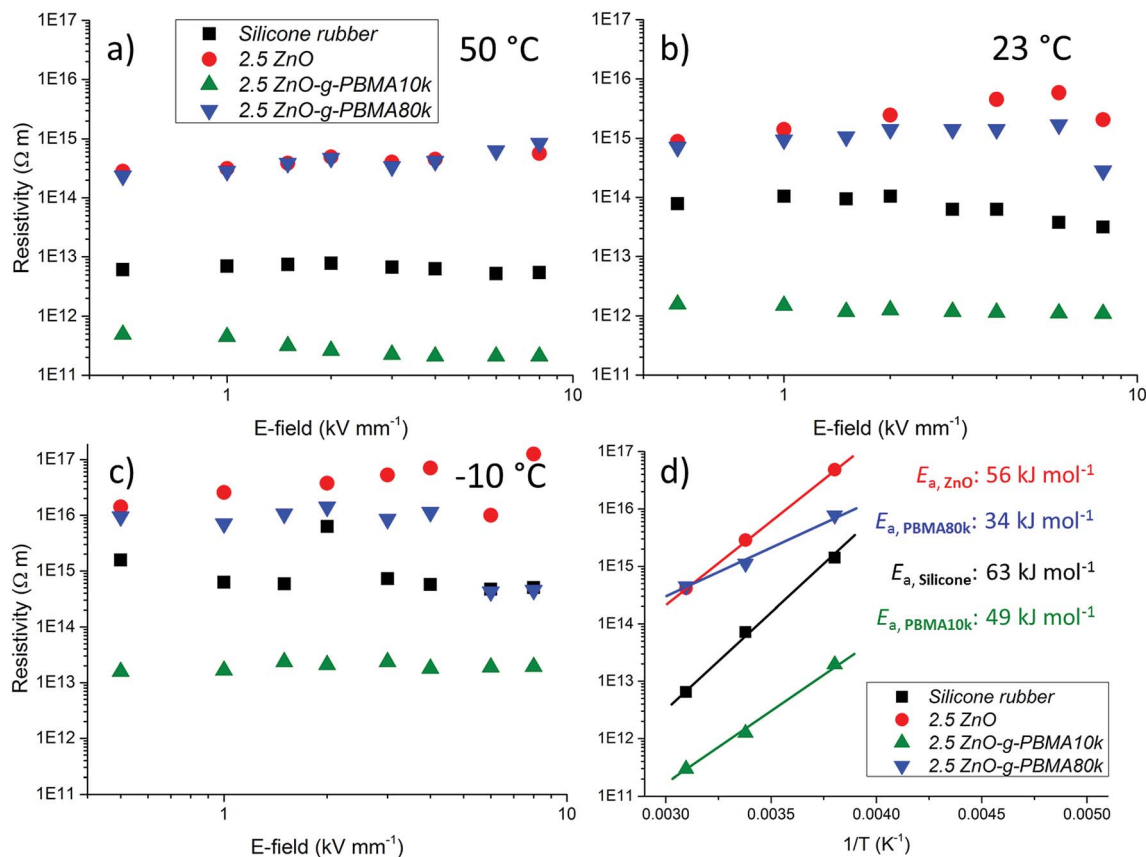


Fig. 14 Resistivity data for *silicone rubber*, *2.5ZnO*, *2.5ZnO-g-PBMA10k* and *2.5ZnO-g-PBMA80k* at (a) 50 °C, (b) 23 °C and (c) –10 °C. (d) The logarithmic average resistivity plotted against $1/T$. Curve fitting gives the slopes corresponding to the temperature dependence of the resistivity and the activation energy of the materials.



temperatures. At low frequencies, the interphase of the well-dispersed grafted NPs efficiently trapped charge carriers, and at high frequencies the dielectric loss was lower, due to a reduced amount of polar groups and moisture.

At 0.01 Hz, the *2.5ZnO-g-PBMA10k* with connected structures exhibited large relative losses at both 20 °C and 50 °C, in contrast to *1.5ZnO-g-PBMA60k* with connected structures and the phase-separated *1.5ZnO-g-PBMA10k*, both of which exhibited lower relative losses at 50 °C. The large relative loss tangent (240%) and increased DC-conductivity of *2.5ZnO-g-PBMA10k* at 50 °C were an effect of the morphologies and short face-to-face distance of the ZnO-cores (<10 nm) (Fig. 13). The interesting dielectric properties obtained at low frequencies were complemented by DC resistivity measurements to gain more insight into the conduction mechanisms.

3.5.4 Resistivity measurements of silicone rubber containing 2.5 vol% NPs. The resistivities of *silicone rubber*, *2.5ZnO*, *2.5ZnO-g-PBMA10k*, and *2.5ZnO-g-PBMA80k* at different electric fields (0.2–8 kV mm⁻¹) are shown in Fig. 14. The samples were tested above (50 °C), around (23 °C) and below (−10 °C) the *T_g* of PBMA. The scatter in data could, however, be up to one decade at high resistivities (>10¹⁶ Ω m), due to the low signal-to-noise ratio.

It was concluded that all the evaluated materials essentially exhibited a resistivity independent of the applied electric field within the evaluated interval, and the resistivity increased with decreasing temperature. The isotropic nanocomposites with dispersed NPs (*2.5ZnO* and *2.5ZnO-g-PBMA80k*) had a higher resistivity than the *silicone rubber* (Fig. 14), indicating a trapping of charge carriers by the interphase of the well-dispersed NPs, despite the high filling ratio. These findings are in agreement with the reported higher resistivities of LDPE-nanocomposites with ZnO NPs.¹¹ The enhanced resistivity indicates that ZnO-g-PBMA80k was still readily available for trapping of charge carriers.

The lower resistivity of *2.5ZnO-g-PBMA10k* (Fig. 14) is most likely an effect of the connected structures with the short face-to-face distances (6–8 nm), in the range for efficient hopping of charge carriers (Fig. 13).⁶⁴ This may be compared with the longer face-to-face distance of 26–28 nm for the *2.5ZnO-g-PBMA80k*. We verified that the observed reduction in resistivity was not caused by ionic contamination (Fig. S3†) by reproducing the synthesis and evaluating the effect of different cleaning approaches. The pure interphases of NPs were confirmed by the greater resistivity of *2.5ZnO-g-PBMA80k*.

Since it is considered important to obtain stable dielectric properties over a large temperature interval for high voltage dielectrics and electronic applications, the temperature dependence of the resistivity was calculated using the Arrhenius equation. The temperature dependence of the resistivity and the activation energy (*E_a*) were obtained by curve fitting of the logarithmic resistivities *versus* *T*⁻¹, where the slopes correspond to the *E_a/R* (Fig. 14d and S13a†). The temperature dependence of the resistivity decreased for the nanocomposites compared to *silicone rubber*. The lowest *E_a* was obtained for *2.5ZnO-g-PBMA80k* followed by *2.5ZnO-g-PBMA10k* and *2.5ZnO* (Fig. 14d and S13b†).

4. Conclusion

For the first time, Hansen's solubility parameters (HSPs) have been directly applied to predict the compatibility between the polymer grafts on NPs and polymer matrices. By using HSPs, we designed nanocomposites with semi-compatible polymer grafts and matrices in order to obtain various NP morphologies, ranging from spherical agglomerates *via* continuous superstructures to well-dispersed NPs. We discovered that the morphology of the NPs in a semi-compatible nanocomposite is strongly affected by the entropic wetting of the grafts by the matrix (*N_M/N_g* ratio) similar to homopolymer nanocomposites. This indicates that the morphology of ZnO NPs and thus, the dielectric properties of the nanocomposites can be tuned by controlling the graft length and the *N_M/N_g* ratio. Further, the resistivity of anisotropic nanocomposites containing connected morphologies is dependent on the tunable face-to-face distance of the NP-cores, as the resistivity decreased when the distance was close to the hopping distance (<10 nm). Image analysis models were developed to improve the characterization of NPs and their distribution, by calculating the face-to-face distance, the radius of the primary NPs, and the fraction of agglomerates.

More specifically, we obtained nanocomposites of commercial silicone with low dielectric loss where the resistivity increased up to 100 times. The interphase of well-dispersed grafted NPs provides a unique combination of high resistivity, by the trapping of charge carriers, and low dielectric loss at higher frequencies, due to the absence of polar groups and moisture. The well-dispersed pristine ZnO NPs improved the electrical breakdown strength of silicone due to their large and compatible NP–matrix interphase. Further, the thermal dependence of the DC resistivity was reduced by up to 50% for nanocomposites compared to neat silicone rubber.

We believe that these tunable properties of silicone based nanocomposites with semi-compatible polymer grafts are highly versatile and promising materials for low-loss high-voltage transmission cable accessories, as well as for flexible-dielectric materials for mobile electronic devices, wearables and sensors.

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