

# A case study on tap water quality in large buildings recommissioned after extended closure due to the COVID-19 pandemic

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This study examined the water chemical quality deterioration in ten large buildings after prolonged stagnation due to COVID-19 pandemic and evaluated the effectiveness of two different flushing practices in taking the fresh drinking water to the building plumbing. This study could be beneficial in preparation for many situations that cause stagnation events not just pandemics such as; holidays, long weekends, long breaks due to breaks in the semester, renovation work of a building, maybe even other emergency response situations.

# A case study on tap water quality in large buildings recommissioned after extended closure due to the COVID-19 pandemic

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The extensive building closures due to the unprecedented COVID-19 pandemic resulted in long-term water stagnation within the plumbing of large buildings. This study examined water chemical quality deterioration in ten large buildings after prolonged stagnation caused by the closure of a university campus in response to the COVID-19 pandemic. The volume-based and constant-duration flushing protocols were implemented to replace stagnant water with fresh drinking water. The effectiveness of developed water flushing protocols was examined by monitoring the disinfectant residuals, heavy metals concentrations and temperature for water samples collected from the buildings' Point of Entry (POE) and select water fixtures. More than 14 m<sup>3</sup> of water were flushed in all ten large buildings. The results demonstrated a significantly greater average total chlorine residual concentration in POE's water samples collected after flushing (1.1 mg/L) compared to the stagnant condition (0.6 mg/L). For water samples collected from fixtures during the extended stagnation, chlorine was absent in 71% of samples from academic buildings and and 69% of samples from athletic buildings. The effectiveness of flushing practices is underscored by increasing the median total chlorine concentration from <0.1 to 1.0 mg/L in academic buildings and from <0.1 to 0.75 mg/L in athletic buildings Furthermore, the concentrations of Pb, Zn, and Cu had decreased following the water flushing, but the concentration of Fe had increased in some buildings. This study could be beneficial to prepare for prolonged water stagnation events including but not limited to pandemics.

# Introduction

The COVID-19, the severe respiratory disease caused by SARS-CoV-2, was first reported in Wuhan, China, in late 2019.<sup>1</sup> Within only a few months, this highly transmissible and deadly virus spread across many regions and impacted millions of people around the world as a serious global public health problem.<sup>2</sup> To reduce the rapid transmission of COVID-19, many countries took strict actions to encourage a significant portion of their populations to stay home.<sup>3-5</sup> Globally, millions of schools, office buildings, and non-essential businesses such as restaurants, music and movie theatres, clubs, and indoor sports centers were closed to an unprecedented extent and at an unprecedented speed.<sup>3,6,7</sup> These extensive building closures substantially impacted the water use and resulted in an extended drinking water stagnation within the plumbing of the commercial, educational, and athletic buildings.<sup>8,9</sup> Although some of the stay-at-home orders/advisories were lifted within several weeks, and some commercial buildings were reopened at reduced capacity, many recreational centers, schools, college, and university buildings remained closed or reopened only for essential workers.<sup>10</sup> The zero- or reduced-occupancy in these large buildings has resulted in prolonged stagnation of drinking water in the buildings' plumbing.<sup>11</sup> Prolonged water stagnation within a building's plumbing raised substantial concerns regarding the water's microbial content and chemical quality deterioration.<sup>12,13</sup> The recent field studies that evaluated the water chemical quality variations due to the stagnation within the building plumbing mostly focused on the

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residential buildings.<sup>12–16</sup> Prolonged stagnation in commercial buildings yields an increased rate of disinfectant decay,<sup>17</sup> enhanced heavy metals leaching (e.g. Pb, Cu, Zn, Fe) from metallic pipes and fittings,<sup>13,18,19</sup> and greater microbial growth<sup>20</sup> within potable water.<sup>21</sup>

Multiple water flushing guidelines for building recommissioning were developed by federal, state, and local agencies during the COVID-19 pandemic to mitigate the adverse impacts caused by prolonged stagnation.<sup>22-24</sup> These guidelines generally suggest simple flushing practices for both hot and cold water by replacing the stagnant water with fresh tap water (finished water from the distribution network).<sup>25</sup> However, more complex practices like shock disinfection (using elevated water temperatures and high disinfectant concentrations)<sup>26-28</sup> were recommended as the remediation for Legionella colonization. Although many of the guidelines recommend water flushing for a certain duration of time (e.g., 10 min, 20 min),<sup>29,30</sup> additional water quality monitoring (e.g., disinfectant residuals) should be conducted to ensure the fresh tap water is replacing the stagnant water. However, no systematic studies have been conducted to evaluate the efficiency of the proposed guidelines under pandemic conditions when the human resources, supplies, and access to the building information are limited. As shown in Figure 1, following the COVID-19 disease spread in Shelby County, Tennessee (TN), in mid-March 2020, the University had extended the spring break to March 22nd, then transitioned to online instruction like thousands of other academic institutions in the U.S. After the rapid transition, only essential employees continued to work on campus until June 3rd, 2020. At this point, approximately 25% of the University employees were allowed to work on campus, and certain educational,

recreational, and office buildings were completely closed. Only a fraction of the athletic department's staff, football staff, and football student-athletes were allowed to return to the campus for training and competition. This zero or low occupancy in university buildings raised concerns regarding the tap water quality deterioration due to prolonged water stagnation in the plumbing. Thus, as an immediate response to these concerns, an intensive water chemical quality investigation and building water plumbing recommissioning were conducted during the COVID-19 pandemic (April-June 2020) at ten large buildings on campus to ensure the safety of the tap water. In this study, recommissioning was considered as buildings' reopening after extended closure and concentrates on restoring the tap water quality to the regular water use condition.<sup>8</sup> The specific objectives of this study are to (1) examine the water chemical quality in the large buildings after prolonged stagnation caused by the COVID-19 pandemic, (2) implement the volume-based and constant-duration flushing protocols to replace the stagnant water with fresh tap water, and (3) evaluate the effectiveness of developed water flushing protocols in promoting the water chemical quality.

# Experimental

# Study site, water sampling campaign, and water quality monitoring

In this study, the first draw water samples were collected during the buildings' closure or low occupancy in seven academic [B1-B7] and three athletic buildings [A1-A3] at a university campus in Tennessee, USA. In the academic buildings, consisting mainly of classrooms and office spaces, the water fixtures were mostly faucets in restrooms and water coolers. In athletic buildings A1, there were offices, classrooms, gym, and indoor courts, in A3 in addition to offices, there were some training rooms, locker rooms, equipment storage, and support rooms and had greater number of shower fixtures compared to the academic buildings, and A2 was mainly comprised of athletic offices. The studied buildings were between 38 and 70 years old. The locations of the sampled buildings are shown in Figure SI-1. More information regarding the buildings is provided in Supplementary file (SI-1).

A same municipal water treatment plant supplies groundwater that has been chlorinated, aerated, filtered, and chlorinated again with free chlorine for secondary disinfection

to all target buildings. Orthophosphate was also added as a corrosion inhibitor before the water distribution. The chemical quality of finished water supplied by the local water utility is shown in Table SI-1. As buildings were locked during the study, each person needed to use the ID card to access most of buildings. The number of access through the building was used as an indicator of occupancy in buildings during the extended stagnation and after flushing. The buildings access data indicated that occupancy of buildings was changed during the study. Although it should be noted the building access may show the multi entry by a single person, however its overall trend could represent the variation of buildings occupancy under pandemic. As shown in Table SI-2, the number of people accessing building A1 was increased by more than three time as we conducted this building recommissioning. We have also been told that the number of people in building A3 was increased from 20 to 130 during the study. With having the remote learning through the campus, the occupancy was increased more significantly in athletic buildings. We also found increased access to buildings B1, B3, B4, B6, and B7, while the access to buildings B2 and B5 had decreased slightly. After conducting the water flushing, water samples were collected at select cold and hot water fixtures in all ten buildings to ensure the effectiveness of the flushing practices in delivering the fresh drinking water into the building plumbing. The fixtures' flow rates varied from 1.5 to 2.5 LPM during water sampling. The water samples were first collected at the building point of entry (POE) and then collected sequentially at both cold and hot water fixtures along the building plumbing (as the distance from the POE increased). After extended stagnation the water samples were collected from POE outlets after 5 min to represent the water that enters the building. The water sampling was conducted by collecting 10 mL water samples from cold and hot water fixtures for onsite measurements of total chlorine residuals. Moreover, in five of these buildings [A1, A3, B3, B4, B6], after collection of water sample for chlorine residuals, 60 mL water samples were collected for measurement of pH, temperature, and dissolved oxygen (DO), then 50 mL samples were collected in polypropylene tubes for total lead (Pb), total copper (Cu), total zinc (Zn), and total iron (Fe) quantification,

and two 40 mL amber vials were filled with the water from hot and cold water fixtures for Total Organic Carbon (TOC) concentration measurements. Water pH was measured onsite using a Fisherbrand<sup>™</sup> accumet<sup>™</sup> XL600 pH Meter. DO was



**Figure 1:** The timeline demonstrating the occupancy variation, water sampling, and buildings recommissioning (flushing) at the university campus

Building		Athletic		Academic						
Label	A1	A2	A3	B1	B2	B3	B4	B5	B6	B7
# Floors	3	2	2	1	4	5	4	4	2	3
Total area (m <sup>2</sup> )	14,388	4,804	7,751	3,883	8,660	7,739	7,877	5,750	1,198	2,916
Year built	1951	1983	1971	1963	1967	1973	1930	1966	1971	1958
# WHT <sup>a</sup>	1	2	6	2	1	1	3	1	1	1
Vol. WHT <sup>b</sup> (m <sup>3</sup> )	0.1	0.3	1.5	0.2	0.3	0.8	0.2	0.2	0.2	0.2
Type of Pipes	GIP <sup>c</sup>	CP <sup>d</sup>	СР	СР	СР	СР	СР	СР	GIP	GIP
# Cold water taps	23	8	37	32	41	8	8	23	10	6
# Hot water taps	3	8	15	15	11	16	6	8	5	12
# Water coolers	9	4	14	30	8	4	3	8	4	2
As-built availability	Yes	Yes	Yes	Yes	Yes	Yes	No	Yes	Yes	Yes
POE flushing duration (min)	35	10	15	45	105	10	15	80	na <sup>e</sup>	5
Diameter of service line (in)	2	2.5	2.5	4	4	4	3	4	2.5	2
Outlet access at POE during stagnation	Yes	Yes	Yes	No	Yes	Yes	Yes	Yes	No	Yes
Outlet access at POE during flushing	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	No	Yes
Minimum plumbing flushing duration (min)	479	186	379	342	396	239	200	195	152	188
Estimated water volume in plumbing (m <sup>3</sup> )	2.0	0.7	3.2	1.0	1.5	1.7	ne <sup>f</sup>	1.0	1.1	0.7
Total collected samples	44	40	80	86	62	74	32	52	22	54

**Table-1:** The specifications of studied buildings (<sup>a</sup>water heater tank; <sup>b</sup>volume of water heater tank; <sup>c</sup>galvanized iron pipe, <sup>d</sup>copper pipe, <sup>e</sup>no access; <sup>f</sup>no estimation; <sup>g</sup> Ductile iron, <sup>h</sup>estimated value)

measured using an Oakton DO450 Meter Kit. For preservation, the water samples were acidified to 2% by nitric acid (Fisher Chemical, technical grade) after the samples were transported to the lab. The water samples that were collected for TOC

measurements were transferred in ice to the lab, where Na<sub>2</sub>S<sub>2</sub>O<sub>3</sub> (6 mg) was immediately added to them. Information regarding the field and trip blanks are provided in supplemental file (SI-2). The local certified analytical lab measured the Zn, Cu, Pb, and Fe via Inductively Coupled Plasma Mass Spectrometry (ICP-MS) according to the US EPA method 200.8. The minimum detection limits (MDLs) for Zn, Cu, Pb, and Fe were 14.3 µg/L, 0.6 µg/L, 0.02 µg/L, and 20.9 µg/L, respectively. The minimum quantification limits (MQLs) for Zn, Cu, Pb, and Fe were 20 µg/L, 1.0 µg/L, 0.5 µg/L, and 100 µg/L, respectively. The TOC concentration was measured using a TOC-V CSN Shimadzu TOC analyzer in accordance with US EPA method 415.1. The instrument was calibrated from 0.0 to 25.0 mg TOC/L using HOOCC6H4COOK ( $r^2$  0.999). A HACH<sup>®</sup> Pocket Colorimeter<sup>™</sup> II,

Chlorine was used to measure the total chlorine residual using the DPD colorimetry method (MDL=0.1 mg/L).

#### Water flushing procedures

The water flushing was conducted to deliver water with a sufficient level of disinfectant residuals (total chlorine residuals >0.9 mg/L) to the buildings' POE and  $1^{st}$  hot water fixture in the buildings. Two distinct water flushing protocols were developed to replace the stagnant water in the buildings' plumbing with the fresh drinking water from distribution system.

#### Water flushing at POEs

The water was flushed at the POE's of 9 buildings using the water outlet located in the buildings' utility room. We

considered the service line as the pipe that connected the water distribution main to the building POE. The service lines' dimensions were identified from as-builts. The pipes used for the service line in all buildings were ductile iron. We have used the plumbing as-built drawing and the water distribution network outline to identify the dimensions. The water flow rates in the POE's were measured on site and varied from 15 to 60 LPM. However, we have calculated the volume of water in the service line, but he concentration of the total chlorine residuals was measured onsite in the water samples collected consecutively from the buildings' POE's to ensure that fresh drinking water entered the buildings' POE's prior to conducting the water flushing inside the buildings. The water flushing at POE was stopped when total chlorine residuals exceeded the 0.9 mg/L. For building B6, that we did not have access to the POE, we have flushed the water that was stagnant in the service line using the closest cold water fixture to the building POE.

#### Water Heater Tanks

The water heater tanks (WHTs) were expected to have a large amount of sediment as they were in service for many years.<sup>33,34</sup> Thus, they were not drained during our building recommissioning effort. Their complete draining may have resulted in resuspension of their sediment, and subsequent deposition into the hot water plumbing. Opening several hot water fixtures at the same time could have resulted in insufficient water pressure within the plumbing system. Thus, the incomplete flushing may result in redeposition of dislodged particles onto the other segments of the building plumbing.<sup>8</sup> Due to the lack of appropriate personal protective equipment (N-95 facemasks), the research team exited the room during flushing the hot water fixtures and did not flush the washroom showers during this study. In lieu of draining the hot water tanks (HWT), the hot water was flushed at the fixture closest to the HWT. The volume of water contained within the HWT and the hot water plumbing leading to the first hot water fixture was considered when calculating the minimum flushing duration (MFD<sub>Hot</sub>) as shown in equation (1), where VHWT is the volume of the HWT. Despite the MFD<sub>Hot</sub> estimation, the total chlorine residual in the hot water samples collected from the first hot water fixture did not increase significantly while flushing. Thus, the water flushing was continued beyond the MFD<sub>Hot</sub>, and the chlorine residuals were monitored over the flushing duration until total chlorine residual increased to greater than 0.9 mg/L. However, for four buildings (A1, A3, B1, B3) were not able to meet this condition. Flushing the hot water for more than two hours in buildings B1 and A3 only increased the total chlorine concentrations to 0.6 mg/L and 0.7 mg/L, respectively. The duration of flushing at the first hot water fixture and the total chlorine residual after flushing is shown in Table SI-3.

$$MFD_{Hot} = \frac{V_{HWT}(m^3)}{q(L/min)} + \frac{\pi \times (d(cm))^2 \times l(m) \times 0.1}{4q (L/min)}$$
(1)

#### Volume-based flushing

The volume-based flushing procedure was applied for the nine buildings with as-built plumbing drawings available. For volume-based flushing, the minimum duration was calculated based on the time required to flush the specific volume of water that is present within the pipes between fixtures as it is shown in **Figure 2.** After flushing the POE and HWT, the subsequent hot and cold water fixtures were flushed individually and sequentially beginning from the fixture closest to the POE. The minimum flushing duration (MFD) was calculated according to the Equation (2) <sup>32</sup> using the length (I) and diameter (d) of the water pipe, and the water flow rate (Q).<sup>32</sup> The faucet's water flow rate was measured before the



**Figure 2:** The schematic demonstrating the water flushing sequence, POE: Point of Entry, CWF: Cold water fixture, HWF: Hot water fixture, HWT: Hot Water Tank, Vol: Volume, TCR: Total Chlorine Residuals concentration



**Figure 3:** The variation of total chlorine residuals at the academic and athletic buildings' POEs over the time (MDL=0.1 mg/L)

flushing. Prior to flushing, the fixtures' aerators were removed and cleaned where possible. The shear forces applied during water flushing could resuspend some particulate matters and detach the biofilm from the pipe surface. These contaminants may accumulate in the aerator and gradually release the heavy metals (e.g., Pb, Cu) and cause microbial contamination of tap water. To prevent this contamination, the aerators were removed before flushing and cleaned and returned to the faucets after flushing. The pipe diameter and length were identified using the plumbing as-built drawings. The fixtures' flow rates varied from 1.5 to 7.5 LPM. The water coolers were flushed for a constant duration of 5 min.

$$MFD (min) = \frac{Volume}{Flow Rate} = \frac{\pi \times (d(cm))^2 \times l(m) \times 0.1}{4Q (L/min)}$$
(2)

The level of disinfectant residuals was monitored in select cold and hot water fixtures at buildings A1, A3, and B7 for up to 12 days after flushing to identify the disinfectant residual decay behaviour under low water use condition.

## **Constant duration flushing**

Constant-duration flushing was applied for the academic building (B4) without an as-built drawing. The water heater tank was flushed for 60 min and the total chlorine residual was increased from 0.4 mg/L to 1.0 mg/L. The cold and hot water fixtures located on the first and second floors [closer to the POE] were flushed for 5 min, and the cold and hot water

fixtures on the third and fourth floors that [further from the POE] were flushed for 10 minutes.<sup>35</sup> The water coolers were flushed for a constant duration of 5 min.

### Statistical analysis

The IBM SPSS software, version 26 was used for the statistical analysis. The normality of water quality data was examined using the Kolmogorov-Smirnov test.<sup>36,37</sup> The paired t-test and the non-parametric test of independent-samples median test were applied to identify the significant differences between the water quality data with the normal distributed and non-normal distributed water quality parameters, respectively. A type I error of 0.05 was selected as the significance level for all tests.

# **Results and Discussion**

#### Water chemical quality at the buildings' point of entry (POE)

In this study we monitored the total chlorine residuals as an indicator of the water quality. The average total chlorine residual concentration in the water samples collected from buildings' POE's during extended stagnation was 0.6 mg/L. It should be noted that, there was no access to the POE of building B1 during stagnation, and also no access to POE in building B6 during both stagnation and flushing. The POE at all other buildings were accessible. This implies that despite the low water use due to the low occupancy, the water mains present on campus delivered relatively fresh drinking water to the buildings. However, the very small distance (0.3 mile) of the campus to the water treatment plant may have resulted in a lower water age at this campus compared to the other parts of distribution system and therefore the chlorine concentrations might be higher as they have not decayed in the distribution system over time. This average concentration of total chlorine residual was increased to 1.1 mg/L after flushing (p-value<0.05). The POE's flushing durations varied from 5 min to 105 min. This significant increase in the total chlorine residual concentration underscores

the success of the flushing protocols in conveying the fresh drinking water from adjacent water mains into the buildings' POE's. We have also monitored the variations of total chlorine residuals as a function of flushing duration at POEs in seven buildings. As shown in Figure 3, the initial total chlorine residual concentration was greater than 0.6 mg/L in buildings B2, B3, B7, and A2. Thus, after a relatively short duration of water flushing (<15 min), the total chlorine residual concentration exceeded 1.0 mg/L. For Building B2, the initial total chlorine concentration of 0.9 mg/L increased to 1.0 mg/L after 15 min, which remained almost constant after flushing for 90 min, and eventually has reached the maximum value of 1.3 mg/L after 105 min of water flushing. No total chlorine residuals were found in samples collected initially at the buildings B1 and B5; it took 45 min and 80 min, to reach the 1.0 mg/L threshold level of total chlorine residuals in these buildings' POEs. The buildings' occupancy, service line dimensions and flow rates, outline, dimensions of water mains around the buildings, and rate of water consumption in surrounding buildings connected to the same water main may have influenced the rate of delivering the fresh water into the buildings' POE.

Monitoring the DO and TOC concentration at the POE's of four buildings (A1, A3, B3, B4) revealed no significant difference due to the flushing. The Pb concentration in water samples collected during the extended stagnation period from POE's at buildings A1 and A3 exceeded the United States Environmental Protection Agency (USEPA) action level of 15  $\mu$ g/L. The POE access line was absent in these two buildings, so the water outlets used to collect these water samples were hose bibs and might have contributed to this lead release. No label was found on the water outlets indicating the National Sanitation Foundation (NSF) International certification or lead-free features.<sup>13</sup> Greater Pb [1.5-27.5  $\mu$ g/L], Zn [40.0-348.0  $\mu$ g/L], Fe [226.0-2160.0  $\mu$ g/L], and Cu [58.8-814.0  $\mu$ g/L] concentrations were found in the water samples collected from POE's during

 Table 2: The summary of water chemical quality at the buildings' POE (\*samples collected from 8 POEs during the extended stagnation)

Water Quality Parameter			рН	DO (%)	Temp (ºC)	Total	тос	Zn	Fe	Cu	Pb	
Statistic Parameter						Chlorine (mg/L)	(mg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	
Before	nir		Mean	6.9	31.8	20.6	0.7	5.2	125.7	949.5	289.1	14.7
	issio	-	STD	0.5	17.0	0.5	0.4	0.3	148.5	906.8	360.4	14.7
	omm	a	Minimum	6.5	17.0	19.8	0.3	5.0	40.0	226.0	47.6	1.5
	Rec		Maximum	7.7	55.2	20.9	1.3	5.6	348.0	2160.0	814.0	27.5
After	:ommissionin		Mean	7.1	34.5	21.8	1.1	5.6	4.4	104.4	19.8	3.2
		В	STD	0.3	3.4	1.5	0.2	0.4	8.8	78.0	15.5	4.7
			Minimum	6.7	31.0	20.4	0.9	5.3	0.0	42.6	7.1	0.7
	Rec		Maximum	7.3	38.2	24.0	1.6	6.1	17.5	213.0	39.5	10.3
		Num	n. of buildings	4.0	4.0	4.0	9.0*	4.0	4.0	4.0	4.0	4.0
% Change of Mean				2%	8%	6%	57%	8%	-96%	-89%	-93%	-78%

the extended water stagnation period compared to after flushing. The Pb [0.7-10.3  $\mu$ g/L], Zn [<14.3-17.5], Fe [42.6-213.0], and Cu [7.1-24.7] concentrations were reduced after flushing the POEs. Following the buildings closure, the Fe concentration in the POE water samples from buildings A3 and B3 exceeded the USEPA Secondary Maximum Contaminant Level (SMCL) of 300  $\mu$ g/L. These buildings had ductile iron

service lines and had a maximum iron concentration of 2,160  $\mu$ g/L. However, following the water flushing no water samples exceeded this limit. The summary of water chemical quality at the POE's is shown in **Table 2**.

Impacts of water flushing on disinfectant residuals inside the buildings

The results demonstrated absence of total chlorine residuals (<0.1 mg/L) in 69% and 71% of first draw water samples collected during the extended water stagnation from the academic and athletic buildings, respectively. According to the Tennessee Department of Environment of Conservation, the residual free chlorine concentration should not be less than 0.2 mg/L in more than 5% of samples collected each month for two consecutive months for public water systems.<sup>38</sup> Although, in this study we have not measured the free chlorine residuals, but when the total chlorine residuals is less than 0.2 mg/L, the free chlorine should be less than this limit. As reported by the literature, several chemical reactions that occur within the bulk water and pipe wall result in chlorine decay. Water stagnation within the building plumbing could accelerate the disinfectant residual decay as the pipe materials, biofilm, corrosion deposits, inorganic scale, and natural organic matter present in the plumbing system consume the chlorine residuals.<sup>39,40</sup> After conducting the buildings' recommissioning, the total chlorine residuals were below the detection limit in one hot water sample (faucet) that was flushed according to the volume-based method and underscores it's limitation. Moreover, one cold water sample that was collected from a cooler in building A3 after 5 min flushing also showed the absence of chlorine residuals, which shows sometimes the constant duration of flushing does not replace the stagnant water with fresh tap water. The renovations in buildings' plumbing which have not been marked in as-built drawings may result in a discrepancy between the estimated volume of water and the actual volume of water in the pipes. Despite this minor limitation, conducting the flushing practices has increased the median total chlorine concentration from <0.1 to 1.0 mg/L in academic buildings, and from <0.1 to 0.75 mg/L in athletic building (pvalue<0.05). This finding confirms the effectiveness of developing detailed flushing protocols despite their minor limitations. The constant-duration flushing in building B4 has

academic buildings that were flushed according to the volumebased procedure. As shown in Figure 4, the total chlorine residual concentration was greater in water entering the buildings at the POE's than at the water at the fixtures inside the athletic and academic buildings. The small diameter plumbing within the building provided a large surface area to volume ratio as compared to the POE and increased the rate of chlorine decay within the building.<sup>41</sup> The median total chlorine residual concentration in cold water samples collected from academic buildings during the extended water stagnation period was significantly greater than that of the hot water samples (p-value<0.05). Flushing yielded 23% and 37% greater total chlorine residual in the cold water samples compared to the hot water samples in academic and athletic buildings (pvalue<0.05), because elevated temperatures in hot water tanks accelerated the chlorine decay.<sup>41</sup> After flushing, the median chlorine residual concentrations for both cold (pvalue<0.05) and hot water samples (p-value>0.05) were lower in the athletic buildings compared to the academic buildings. The majority of buildings remained at low occupancy even after recommissioning. According to the buildings access information and our survey, the occupancy was increased significantly in buildings A1 and A3 which were athletic facilities. Thus, as shown in Figure 5, follow-up disinfectant residuals monitoring was conducted in multiple cold and hot water fixtures in select buildings to identify the disinfectant decay behaviour under limited occupancy conditions. Twelve days after recommissioning building B7, the total chlorine residual concentration was 0.2 mg/L in one of the cold water fixtures despite its low occupancy (38 access/month). On the other hand, although building A3 maintained significant occupancy (130 people), the total chlorine residuals had depleted to below the detection limit (0.1 mg/L) in less than 4 days. In general, the chlorine residuals dissipated more rapidly in the hot water fixtures compared to the cold water fixtures.<sup>42</sup> Despite, the increased occupancy in buildings A1 and A3, the



**Figure 4:** Total chlorine residuals in cold and hot water samples collected from seven academic and three athletic buildings (a) after extended stagnation and (b) after water flushing, red dotted line represents the median total chlorine concentration at buildings POE, within each box horizontal black lines denote the median values, boxes extended from first to third quartile of each group distribution, X represents the mean, the whiskers extended from min to maximum, dots denote the outlier data, (MDL=0.1 mg/L).

significantly increased the median total chlorine concentration from <0.1 to 1.0 mg/L, which was similar to the other

total chlorine residuals was depleted to below the detection limit as early as one day after recommissioning in the hot



**Figure 5:** The total chlorine residuals concentration (mg/L) over the time after buildings (A1, A3, and B7) recommissioning, blue line represents the cold water and red line represents the hot water, each dot represents one water sampling event (MDL=0.1 mg/L).

water fixtures. Thus, as suggested by the literature, routine water flushing could be used as an effective tool to better maintain the drinking water quality within the large buildings.<sup>11</sup> The plumbing materials were Galvanized iron pipe (GIP) in buildings A1 and B7, however it was copper (CP) in building A3. Although the literature suggested a faster chlorine decay in GIP compared to CP,<sup>41</sup> due to the complexity of building plumbing and variation in building occupancy, this trend was not observed herein.

#### Water pH, temperature, DO level and TOC concentrations



**Figure 6:** DO% at academic (B3, B4, B6) and athletic buildings (A1, A3) before flushing (BF) and after flushing (AF), within each box horizontal black lines denote the median values, boxes extended from first to third quartile of each group distribution, x represents the mean, the whiskers extended from min to maximum, dots denote the outlier data.

For the two academic buildings with the CP plumbing (B3 and B4), the average pH values were lower (*p*-value<0.05) during the extended water stagnation (6.9 and 7.4) than they were after flushing (7.4 and 7.8). Low pH increases the potential for heavy metals to be released into the water.<sup>43</sup> However, the average pH for the academic building with GIP plumbing (B6) decreased from 8.1 to 7.8 following the flushing (*p*-value<0.05). The cathodic and anodic reactions occur within the metallic water pipes have been

identified as reasons behind the pH variations under stagnant condition.<sup>44</sup> Previous authors have reported an increase in pH up to 2.3 units as water had stagnated in old iron pipe.<sup>45-47</sup> No significant change was found in the pH levels of water samples collected from athletic buildings after implementing the flushing practices. Among the buildings with copper plumbing, the median pH value for water samples collected in building B4 was significantly greater than median pH value for water samples collected in building B3 after

extended stagnation (*p*-value<0.05) and in building A3 after flushing (*p*-value<0.05). As was expected, the median temperature of hot water samples increased to 41.2 °C and 36.3 °C in both academic and athletic buildings due to the water flushing (*p*-value<0.05). The constant-duration flushing in building B4 has increased the median temperature for hot water samples by 17 C° (22°C  $\rightarrow$  39°C), however the temperature was increased by 19 °C (22°C  $\rightarrow$  41°C) for other academic buildings that were recommissioned according to

the volume-based. As shown in Figure 6, the median values of DO% in academic and athletic buildings increased significantly from 29% and 11% to 37% and 39%, respectively after conducting the water flushing practices (*p*-value<0.05). The median DO% in building B4 was increased from 19% to 39% after conducting the constant-duration flushing, however it was increased from 30% to 37% in water samples collected from other academic buildings that were flushed according to volume-based procedure. The constant-

duration flushing in building B4 has increased the median temperature for hot water samples by 17 C° (22°C  $\rightarrow$  39°C), however the temperature was increased by 19 °C (22°C  $\rightarrow$  41°C) for other academic buildings that were recommissioned according to the volume-based. The median TOC concentration slightly increased from 5.2 mg/L to 5.5 mg/L in water samples collected from academic buildings and increased from 5.3 mg/L to 5.8 mg/L in water samples collected from athletic buildings due to the buildings



**Figure 7:** The box and whisker plots for total Cu, Zn, and Fe concentrations in water samples collected after extended stagnation (a, c, e) and after buildings recommissioning (b, d, f) from academic (B3,B4,B6) and athletic buildings (A1, A3), outliers are not shown, within each box horizontal black lines denote the median values, boxes extended from first to third quartile of each group distribution, X represents the mean, the whiskers extended from min to maximum, dots denote the outlier data.

recommissioning (*p*-value<0.05). The increased shear forces experienced during flushing may have dislodged any biofilms that had accumulated on the inner pipe surface.<sup>12</sup>

#### Heavy metals concentrations

The total Pb, Cu, Zn, and Fe concentrations were monitored in the water samples collected from cold and hot water fixtures in three academic buildings [B3, B4, B6] and two athletic buildings [A1, A3]. The median Pb concentration in water samples collected from water fixtures in both academic and athletic buildings during the extended water stagnation and after flushing were significantly low (<1.0  $\mu$ g/L). Of the 116 water samples that were collected in the buildings during extended water stagnation period, only four water samples exceeded the USPEA action level for Pb (ranging from 15.2  $\mu$ g/L to 129.0  $\mu$ g/L). However, after the buildings' recommissioning, only one water sample (60.3 µg/L) exceeded the Pb limit. This sample was collected after flushing the water, however this fixture had a very low Pb concentration (1.4  $\mu$ g/L) during the extended stagnation. Thus, this quantified Pb might be the particle released from upstream plumbing due to the shear forces applied during the flushing practices. Since these buildings were originally constructed (1930-1973) several years before issuing the original Lead Contamination and Control Act (LCCA),<sup>48</sup> it is reasonable to assume that there might be some lead-containing plumbing components present within the building. Furthermore, the GIP plumbing present in buildings B6 and A1 might have contributed to the Pb release into the water.<sup>49</sup> The zinc used during the galvanizing process typically contains a minimum of 0.5% lead, and this lead could be released into the water over a long-term basis.<sup>50-52</sup> The lead levels that were identified in this study during both extended stagnation and after flushing were significantly were smaller that values reported for some U.S. schools (up to 18,800  $\mu\text{g/L})^{49}$  and Canadian's large administrative and training buildings (up to 23,000  $\mu g/L),^{53}$  elementary schools, day cares, and other large buildings (up to 13,200 µg/L).<sup>54</sup> As shown in Figure 7 (a,b), the median concentration of Cu in the water samples collected from cold (362 µg/L) fixtures in athletic buildings during extended stagnation were significantly greater than cold (179  $\mu$ g/L) water samples collected in the academic buildings (p-value<0.05). Three water samples in one of the athletic buildings (A3) with CP plumbing exceeded the USEPA

SMCL for Cu (1.0 mg/L). None of collected water samples exceeded the USEPA SMCL limit for Zn (5.0 mg/L). The maximum Zn concentrations in water samples collected from academic and athletic buildings after extended stagnation duration were found as 3,290 µg/L (cold water) and 4,260 µg/L (cold water), respectively. However, following implementation of flushing practices the maximum Zn concentration reduced to 254  $\mu$ g/L (hot water) and 1,100  $\mu$ g/L (hot water), in the academic and athletic buildings, respectively. Occurrence of these maximum values in hot water following the flushing practices demonstrates the possible resuspension of metals from the hot water tank into the tap water. The constantduration flushing in building B4 has decreased the median Cu concentration from 65  $\mu$ g/L to 41  $\mu$ g/L, and the volume-based flushing reduced it from 186 µg/L to 23 µg/L in other sampled academic buildings (B3 and B6). As shown in Figure 7(c,d), the median Zn concentrations in hot and cold water samples collected from academic and cold water in athletic buildings reduced significantly due to the building were recommissioning (*p*-value<0.05). The constant-duration flushing in building B4 has decreased the median Zn concentration from 115 µg/L to 15 µg/L, and the volume-based flushing reduced it from 75 µg/L to <14 µg/L in other sampled academic buildings (B3 and B6). As shown in Figure 7(e,f), 14.8% of water samples collected in the buildings during the extended water stagnation period exceeded the USEPA SMCL of 300 µg/L for iron. Furthermore, the maximum Fe concentrations in academic and athletic buildings were 3,590  $\mu$ g/L (hot water) and 2,610  $\mu$ g/L (cold water), respectively. However, after building recommissioning, the Fe concentration in only 4.7% of collected water samples exceeded the SMCL limit. The constant-duration flushing in building B4 has increased the median Fe concentration from 31  $\mu$ g/L to 47  $\mu$ g/L, and the volume-based flushing increased it from 30  $\mu$ g/L to 43  $\mu$ g/L in other sampled academic buildings (B3 and B6). The maximum Fe concentration reduced to 204  $\mu$ g/L (hot water) in academic buildings, but it increased to 4,450  $\mu$ g/L (hot water) in an athletic building (A1) with GIP plumbing. This elevated Fe concentration might have originated from a particulate Fe dislodged from the corroded surface of GIP pipes due to the shear forces applied during the water flushing.55

The flow regime, dissolved oxygen, and disinfectant residuals are critical parameters influencing the metal scale stability and consequently the metal release behavior.40,56 The dissolved oxygen and free chlorine residuals are the predominant oxidants present within the potable water system. Under stagnant or low flow conditions, the corroded metal surfaces rapidly consume the dissolved oxygen and free chlorines that are present in the water adjacent to the pipe surface.<sup>56</sup> Depletion of oxidants in water creates a reducing environment, where the scales stability is decreasing and a more porous scale surface is formed which promotes releasing the dissolved metals to the bulk water.<sup>45</sup> Inversely, under high flow condition a sufficient level of oxidants are delivered to the metallic scale which enhances their oxidation and formation of stable denser shells.<sup>45,57,58</sup> The Kuch reactions result in ferrous iron release from the pipe scale under reducing condition.<sup>45</sup> These reactions are shown in Figure 8 Furthermore, the flowing water provided by the municipal water treatment



**Figure 8:** Schematic demonstrating the galvanic cell reactions occur under regular water use and no water use conditions

plant continuously supplies the orthophosphate inhibitors (1 mg/L) to the pipe scale, promoting the protective film which reduced the metal release to the water. However, the extended water stagnation within the plumbing enhances the consumption of inhibitor residuals and reduces their effectiveness.<sup>59,60</sup> The water pH and alkalinity are significant factors influencing the metal leaching from plumbing components.<sup>61</sup>The supplied water had a low alkalinity (53 mg/L as CaCO<sub>3</sub>) and relatively neutral pH (7.2). Its pH was changed drastically (6.6-9.9) as water conveyed through the building plumbing system. The prior studies that investigated the metal release under short term stagnation periods revealed that alkalinity up to 75 mg/L as CaCO<sub>3</sub> and increased pH values to reduce the corrosion.<sup>62</sup> However, the systematic investigations should be conducted to identify the interrelated influence of water chemistry parameters on heavy metals leaching from plumbing materials under prolonged water stagnation.

No/low water use condition  $Fe(s) \leftrightarrow Fe^{2+} + 2e^-$  (Anodic Reaction)  $2Fe00H(s) + 2H^+ + 2e^- \leftrightarrow 2Fe^{2+} + 40H^-$  (Cathodic Reaction)

#### Regular water use

 $Fe(s) \leftrightarrow Fe^{2+} + 2e^-$  (Anodic Reaction)  $O_2(g) + 4H^+(aq) + 4e^- \leftrightarrow 2H_2O(I)$  (Cathodic Reaction)

#### Evaluation of the efficiency of buildings' flushing practices

Although the USEPA recommends a flow rate of at least 3.0 LPM when flushing a fixture,<sup>63</sup> the first hot water outlet after the water heater tank with a low flow rate as low as 1.5 LPM - resulted in a time-consuming flushing process. As our previous study demonstrated, running several water fixtures simultaneously results in a lower flow rate or zero flow rate in some fixtures and reduces the effectiveness of water flushing.<sup>63</sup> With flushing only one cold and one hot water



**Figure 9:** (a) %reduction of median metal concentrations (b) %increase of median temperature, and (c) %water samples with total chlorine residuals <0.2 mg/L due to buildings recommissioning.

fixture at a time, we maximized the water flow rate and promoted the effectiveness of water flushing. We have considered the total chlorine concentration of 0.2 mg/L as our threshold to evaluate the effectiveness of applied flushing protocols. However, it should be mentioned that the complexity of the building plumbing and the various occupancies in these buildings, makes the comparison of these flushing protocols challenging. The percentage of water samples with total chlorine residuals less than 0.2 mg/L collected during the extended stagnation was compared with those values after conducting the flushing practices (Figure 9a). The total chlorine residual during the extended stagnation period was less than 0.2 mg/L in 58% to 100% of water samples collected from the target buildings. However, by conducting the volume-based flushing practices, these percentages were reduced to 0% to 4.5% in the target buildings. For building B4, which was flushed according to the constant duration-approach, this percentage was reduced from 73% to 8.3%. This study showed that both flushing protocols increased the chlorine residuals in tap water significantly. However, comparison of two methods is challenging as only one building was flushed according to the constant-duration protocol. The constant-duration flushing procedure may not replace the stagnant water completely due to the various building types, the plumbing's complexity, and the range of the fixtures' flowrates. One the other hand, developing the volume-based flushing protocols is timeconsuming and requires some background knowledge to read the plumbing as-built drawing and calculate the minimum duration of flushing. The percent increase in temperature of hot water samples due to the water flushing was calculated for the water samples collected from both academic and athletic buildings. As shown in Figure 9b, the greatest temperature increase (>90%) was found for hot water samples collected from building B3. This could imply the success of implemented flushing practice in removing the stagnant water from taps as also was confirmed by the chlorine measurements. However, it should be mentioned that in some buildings like A1 and B4, there point of use instant water heaters that impacted the water temperature during flushing that hot water taps. Future investigations should be conducted to identify the effective flushing practices for instant water heaters. As shown in Figure 9c, the concentrations of Zn and Cu decreased in all five buildings. However, in four of these buildings, the Fe concentrations increased by 27% to 214%. This finding underscores the possible incomplete water flushing in these buildings as the particulate Fe species that separated from the plumbing components were not fully removed from the plumbing system during the flushing. The potable water pipes in three of these buildings were CP whereas the other building had GIP pipes. Thus, the Fe could have originated from the GIP plumbing, the service line, or the finished water. The metallic deposits that had loosely adhered to the plumbing walls before flushing had scoured out of the plumbing surfaces during flushing, and may have redeposited in the low flow sections of the plumbing (e.g. dead ends) via gravitational settling.64,65 Thus, appropriate water velocity during flushing should be maintained to retain a suspension of the

particulates which later will be released to the drain.<sup>65</sup> However, an elevated water velocity during the flushing also poses the risk for scouring off of the protective scale from the metallic pipe surfaces.

#### Conclusion

This study was conducted to examine the influence of buildings recommissioning on the chemical quality of drinking water in ten large buildings after prolonged water stagnation caused by zero occupancy or low occupancy in response to the COVID-19 pandemic. The results demonstrated extensive absence of disinfectant residuals, low DO levels, and elevated heavy metals in water samples collected during the extended water stagnation. The buildings recommissioning was conducted by flushing the fire hydrants, POE's, and water fixtures according to the volume-based and constant-duration flushing protocols. The results highlighted the success of implemented flushing protocols by increasing the disinfectant residual content of the tap water and reducing the Zn, Cu, and Pb concentrations in the water samples. However, for a few buildings the Fe concentrations increased as the shear forces resulted from water flushing might have scoured the loose iron corrosion products out of the pipe surface. This study only focused on flushing the water fixtures such as faucets and cooler whereas building recommissioning might be more effective if the toilets, showers, and outside spigots were also flushed. It should be noted that volume estimations may not represent the real volume of water in the plumbing, as this estimation relies on the original plumbing as-built drawing. However, the large buildings may have gone through multiple renovations and maintenance operations that could have altered the plumbing configurations and dimensions. Thus, a water quality monitoring parameter, such as measuring the disinfectant residuals concentration following the flushing, should be conducted to confirm the presence of fresh drinking water in the fixtures.

# **Author Contributions**

Maryam Salehi: Investigation, Analysis, Writing Original Draft, Reviewing and Editing, Visualization, Supervision; Dave DeSimone: Investigation, Reviewing and Editing; Khashayar Aghilinasrollahabadi: Investigation; Tanvir Ahamed: Investigation

# **Conflicts of interest**

There are no conflicts to declare.

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