

# Fast and selective separation of carbon dioxide from dilute streams by pressure swing adsorption using solid ionic liquids

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The need to create a new approach to carbon capture processes that are economically viable has led to the design and synthesis of sorbents that selectively capture carbon dioxide by physisorption. Solid Ionic Liquids (SolILs) were targeted because of their tunable properties and solid form under operational conditions. Molecular modelling was used to identify candidate SolILs and a number of materials based on the low cost, environmentally friendly acetate anion were selected. The materials showed excellent selectivity for carbon dioxide over nitrogen and oxygen and moderate sorption capacity. However, the rate of capture was extremely fast, in the order of a few seconds for a complete adsorb-desorb cycle, under pressure swing conditions from 1 to 10 bar. This showed the importance of rate of sorption cycling over capacity and demonstrates that smaller inventories of sorbents and smaller process equipment are required to capture low concentration CO<sub>2</sub> streams. Concentrated CO<sub>2</sub> was isolated by releasing the pressure back to atmospheric. The low volatility and thermal stability of SolILs mean that both plant costs and materials costs can be reduced and plant size considerably reduced.

## Introduction

One of the key challenges facing Carbon Capture and Storage (CCS), and indeed any carbon dioxide emission mitigation strategy, is the separation and purification of carbon dioxide from dilute gas streams. This is because over 90% of stationary CO<sub>2</sub> emissions sources emit CO<sub>2</sub> at concentrations of 15% volume or less, of which approximately 25% have CO<sub>2</sub> at concentrations of 8.5% volume or less.<sup>1</sup>

In most cases, the primary gas with which the CO<sub>2</sub> is mixed is nitrogen, requiring any capture process to show high selectivity towards CO<sub>2</sub>. This has naturally been the primary advantage of existing CO<sub>2</sub> capture methods using

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aqueous solutions of amines such as monoethanolamine (MEA).<sup>2</sup> Amine capture is a chemisorption process where an exothermic reaction with CO<sub>2</sub> to form carbamate salts gives rise to the high selectivity for the gas over nitrogen. Other oxygenated gases remain problematic, especially nitrogen oxide decomposition gases.<sup>3</sup>

In recent years there has been a move away from amine sorbents because of their thermal degradation and evaporative loss in the desorption process. The high selectivity for CO<sub>2</sub> is the reason behind this. Because a stable salt is produced in the capture phase, considerable energy is required to release the concentrated gas. Adsorption occurs typically at 50 °C with desorption at 130 °C in a temperature swing process. Furthermore, because of issues relating to viscosity and corrosion, the concentration of MEA is typically only 30% in an aqueous solution. Therefore, energy is required to raise the temperature of a solution that is 70% water, and so alternatives to amine capture must be pursued. It is important to recognise that any chemisorption approach requires significant desorption energy so future carbon capture processes need to have a stronger focus on technologies where physisorption is the primary process, and where sorbents are solvent-free.

When considering physisorption processes for CO<sub>2</sub> capture, ionic liquids (ILs) have emerged over the last decade to be particularly prominent as an area of active research. These molecular organic salts (MOSs) show the high selectivity behaviour that is required for effective CO<sub>2</sub> separation and are inherently tuneable in their syntheses to allow for task-specific compounds to be developed.<sup>4</sup> Furthermore they have the benefit of low vapour pressures at room temperature and therefore show negligible volatility. Many are also chemically stable below 200 °C.<sup>5</sup>

One of the two key issues that hampers CO<sub>2</sub> adsorption by Room Temperature Ionic Liquids (RTILs), however, is the extremely low rate of CO<sub>2</sub> diffusion through the bulk liquid. When compared with aqueous amine systems, CO<sub>2</sub> diffuses through even low-viscosity ionic liquids 19 orders of magnitude slower.<sup>6</sup> This shortfall can be somewhat remedied by the use of diluents such as water, alcohols or other amine agents used as solvents.<sup>7</sup> However, such approaches undermine some of the advantages that ionic liquids have in terms of recyclability and vapour pressure. This additionally excludes ionic liquid types that are not compatible with such dilution approaches due to solubility or stability issues, particularly common in the presence of water.

The extremely slow diffusion coefficient of RTILs combined with their relatively high cost, especially in comparison with MEA, has had an impact on their commercial deployment. While it is difficult to accurately gauge the costs per tonne of ionic liquid once large scale production is considered, the slow diffusion coefficient would require very large inventories of ionic liquid to be used in a capture plant to maintain acceptable capture levels from a given CO<sub>2</sub> point source. This has cost implications when dealing with relatively expensive sorbents, but also would likely inflate the capture plant footprint. The importance of plant footprints is further underlined in that space to accommodate large capture plant footprints is a major hurdle even for traditional MEA capture processes, which enjoy the benefits of much higher diffusion coefficients than RTILs.<sup>8</sup> Therefore, capture using ILs will require novel gas-ionic liquid contacting methods in order to bypass the slow uptake step. The UK Government announced



in November 2015 that state funding for the commercialisation of CCS had been withdrawn, and this was clearly reiterated in the House of Commons by the Prime Minister in December 2015 in a response to a question on CCS.<sup>9</sup> However, The Committee on Climate Change responded that CCS was still needed in order to meet the commitments to the Paris Agreement from COP21 and to fulfil the requirements of the Fifth Carbon Budget. The Committee said that in order to achieve CCS there was a need to “develop urgently a new approach to CCS in the UK”. This would therefore suggest a move away from current amine separation approaches to more efficient and lower energy separation methods. Gas–solid separations could therefore be a way forward.

## Solid ionic liquids and pressure swing separation

Ionic liquids are arbitrarily described as organic salts with melting points below 120–140 °C.<sup>10</sup> While RTILs exist as perhaps the most widely known of this group of organic salts, often ignored are ionic liquids with melting points significantly above room temperature. These may be given the somewhat contradictory name of Solid Ionic Liquids (SoILs, not to be confused with Supported Ionic Liquids, SILs) and may, by virtue of being solids, present advantages in allowing access to large ionic surface areas and a reduction in diffusion concerns. This effect has been previously observed with Poly Ionic Liquids (PILs), which have been tested for CO<sub>2</sub> adsorption, showing significantly faster uptake rates, and which could be considered a subset of SoILs.<sup>11</sup>

Unfortunately using SoILs will reduce total uptake capacity as not all parts of the SoIL will have access to the gas interface surface, due to the crystalline nature of the SoIL particles. This will, as in the case of the RTIL sorbent systems, require a larger sorbent inventory to be used for a given CO<sub>2</sub> point source, unless higher capacities can be achieved. Therefore, higher pressures or partial pressures of CO<sub>2</sub> will be required to ensure the maximum possible CO<sub>2</sub> capacity per unit mass of the sorbent. Taking all these limitations into consideration, this supports the use of pressure swing separation technologies.

This may be an advantage as the changes in pressure needed for pressure swing capture can be carried out very quickly, allowing the capture plant to more effectively utilise the SoIL's rapid uptake rate. By comparison, temperature swing processes will have either a significant thermal lag between each adsorption and desorption cycle, or will require a large proportion of the sorbent inventory to be undergoing regeneration at any given time.<sup>12</sup> Therefore, the combination of a fast uptake and desorption rate and rapid pressurisation and depressurisation allows more CO<sub>2</sub> to be captured with less sorbent.

On a plant scale, more rapid cycle times will offer benefits in terms of flexibility and responsiveness to changes in input gas concentrations, flow rates and sorbent capacity. These features may become increasingly important as intermittent renewable energy accounts for larger proportions of electrical energy production, requiring increased use of load-following power plants.<sup>13</sup> In comparison, MEA systems with effective cycle times as long as multiple hours per cycle have already been identified as having potential stability issues, particularly when exposed to changes in gas flow rates.<sup>14</sup>

Alongside faster cycle times and the associated benefits in responsiveness and sorbent costs discussed above, pressure swing separation has an additional



potential benefit of shrinking the capture plant footprint significantly. However, this will be dependent on sorbent particle size, operating pressure and cycle time. For example, larger particles increase the maximum possible column height while higher operating pressures and shorter cycle times shrink column sizes (while potentially increasing minimum column wall thickness).<sup>15</sup>

## Energy cost of pressure swing separation

The potential benefits of pressure swing separation of CO<sub>2</sub> must be offset against the energy costs of the feed gas compression. To explore these potential costs, a model pressure swing capture system was constructed using a range of operating pressures (15–40 bar) and separation profiles based on experimental data gathered from initial experiments to yield a >90% CO<sub>2</sub> output stream. These results compared favourably with existing literature data concerning the energetic costs of various capture methods including amine capture, membrane separation and vacuum swing separation, as shown in Fig. 1. Furthermore, the range of results given by our model of 888–1540 MJ/tCO<sub>2</sub> were in broad agreement with previously published models involving pressure swing CO<sub>2</sub> separation.

It must be noted that only total energy requirements are used as the basis of comparison in Fig. 1. From a cost perspective the differences between the value of thermal energy used by a temperature–swing system and the electrical energy used by a pressure–swing capture system may be quite large, especially in situations where surplus thermal energy is available. This would potentially narrow the gap between the two approaches.

In addition to pressurisation energy cost, the thermal performance of the sorbent must be taken into account in a pressure swing adsorber due to the



Fig. 1 Comparison of calculated energy costs of different CO<sub>2</sub> capture methods: MEA,<sup>16</sup> advanced amine,<sup>17</sup> membrane,<sup>18</sup> vacuum swing.<sup>19</sup> High pressure swing was calculated from the preliminary process model [see main text] and was found to be in agreement with literature values.<sup>20</sup> Minimum thermodynamic separation costs were calculated from entropy of de-mixing.



temperature changes when adiabatic pressurisation occurs. While highly compressed gases can easily be shown to reach extreme temperatures, the use of rapid pressurisation and depressurisation cycles would allow for a pseudo steady-state scenario where the SoILs only reach moderate temperatures. Despite this, physisorption processes are typically particularly sensitive to changes in temperature due to the weak bonding interaction and hence the performance of these sorbents must also be tested at elevated temperatures.

As a relatively unexplored but potentially highly effective and efficient method for carbon dioxide capture, a selection of simple ammonium SoILs, anticipated to be low-cost, were synthesised and tested at a variety of scales with a specific focus on uptake kinetics and gas sorption selectivity. An imidazolium-IL and two PILs as well as their monomer forms were also tested for comparison. Where possible, the anion used was acetate, which has previously been shown to enable a high degree of CO<sub>2</sub> solubility in RTILs and minimises cost by avoiding more complex anions such as PF<sub>6</sub>, BF<sub>4</sub> and NTf<sub>2</sub>, which are typically used to promote low melting points.<sup>21</sup> A preliminary computational simulation was carried out to determine interaction energies between the ILs and CO<sub>2</sub>. These showed that acetate was a good candidate anion as it gave a moderate binding energy with CO<sub>2</sub>, indicating reasonable selectivity but with low-energy regenerative desorption of the gas.

## Experimental

Computer simulations were carried out on a Windows XP PC using Avogadro modelling software. The ion pairs of the ILs were constructed using the molecular editor and the geometry was optimised using firstly the Universal Force Field (UFF) and then the MMFF94s (Merck Molecular FF) force field to refine interaction potentials. A CO<sub>2</sub> molecule was then constructed in the same modelling environment and the system was optimised using the MMFF94s FF which gave the intermolecular interaction energies and the distortion in the CO<sub>2</sub> molecule. The global energy minimum was obtained by moving the CO<sub>2</sub> molecule over the surface of the IL and then optimising at the appropriate location. From this the binding energy was obtained as well as the O–C–O dihedral angle. This was performed over a range of anions and cations in order to select suitable candidates for synthesis and evaluation. Calculation of the Single Point Energy (SPE) of the test complex was used in the calculation of the Binding Energy (BE). The BE is calculated using the sum of the SPEs of the tested ion and CO<sub>2</sub> subtracted from the SPE of the complex, as shown in eqn (1).

$$\Delta E = E([\text{complex}]) - (E([\text{ion}]) + E([\text{CO}_2])) \quad (1)$$

All amines, alkyl halide reagents, tetraethylammonium bromide (N<sub>2222</sub> Br) and tetrabutylammonium bromide (N<sub>4444</sub> Br) were purchased at the highest available purity from Sigma Aldrich and used without further purification. Amine quaternisation reactions were carried out using Schlenk-line techniques under an inert (N<sub>2</sub>) atmosphere unless otherwise indicated. Reactions using photosensitive reagents such as methyl iodide were carried out using aluminium foil protection on the exterior of the reaction vessel. All solvents were HPLC grade. CO<sub>2</sub>, N<sub>2</sub> and argon were supplied by BOC-Linde.



Small scale adsorption and densitometry studies were carried out using a Hiden Isochema IGA-0002 adsorption apparatus with a pressure range of 0–10 bar. Larger scale and higher pressure adsorption experiments were carried out using a bespoke packed-bed column constructed from Swagelok™ piping using a Jasco PU-1580-CO<sub>2</sub> supercritical carbon dioxide pump, a Jasco BP-1580-81 back pressure regulator, an Omega PX409USB High Accuracy Pressure Transducer and an AND GF-1000 High Capacity 3 decimal place balance. <sup>1</sup>H NMR spectra were recorded using a Bruker Avance 400 MHz spectrometer using tetramethyl silane as the internal standard.

### General synthesis of halide SoILs

An oven-dried 2-neck 100 mL round bottom flask was charged with tertiary amine (2 mmol) dissolved in diethyl ether (25 mL) under an atmosphere of N<sub>2</sub> using Schlenk-Line techniques. The appropriate alkyl halide (2.2 mmol) was then carefully added with rigorous stirring at room temperature for 16 hours. In all cases except with N<sub>1888</sub> I, a white precipitate was observed to form over several hours. The range of cations used which yielded SoILs is shown in Fig. 2. Each sample was then evaporated to dryness using rotary evaporation before being washed three times with hexane to remove trace unreacted amine and alkyl

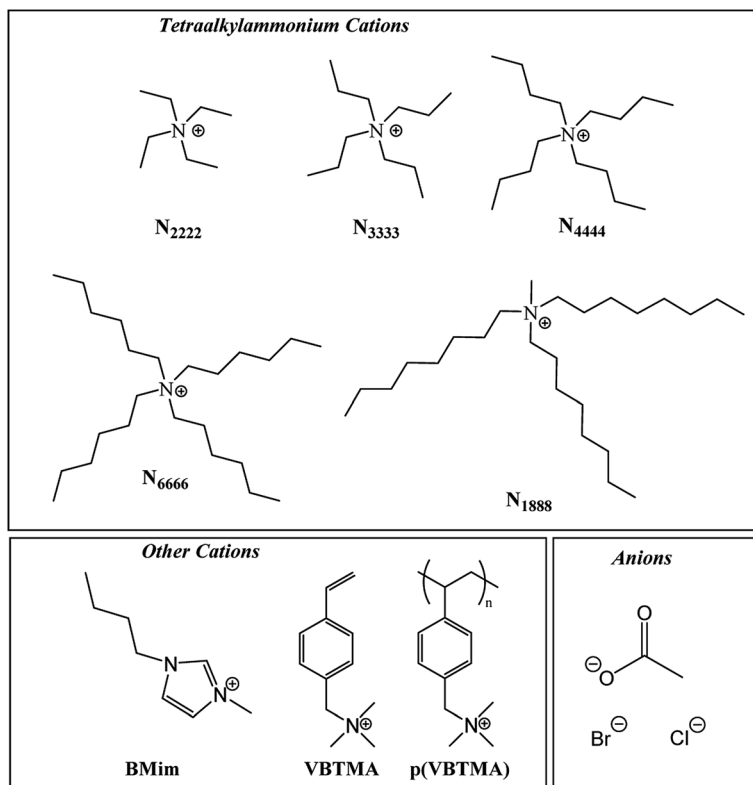


Fig. 2 The selection of tetraalkylammonium, imidazolium and polymeric/monomeric compounds synthesised which yielded solid organic salts at room temperature.



halide. SoILs were then isolated in high yield as white crystalline solids. Before IGA analysis, the SoILs were ground to fine powders using a pestle and mortar and stored in a vacuum desiccator.

### General procedure for synthesis of acetate SoILs

A 0.1 M aqueous solution of the appropriate tetraalkylammonium halide salt of the desired product was prepared, then slowly passed through a column of Amberlite™ IRN78 hydroxide form resin, which had been freshly-regenerated using 1 M high purity aqueous sodium hydroxide and then thoroughly washed to remove any sodium salts. After passing through the column, the resulting aqueous tetraalkylammonium hydroxide solution was immediately mixed with excess acetic acid. This was done to prevent decomposition of the ammonium hydroxide species, which are typically unstable. The product mixture was then tested for residual halide species by shaking a sample with aqueous silver nitrate. If no precipitate was observed, the sample was dried by rotary evaporation. Isopropanol and heptane were used sequentially to assist in the removal of water and excess acetic acid by azeotropic distillation. Isolated dry tetraalkylammonium acetate was then ground to a fine powder in a pestle and mortar and re-dried under high vacuum.

### General procedure for small scale testing on IGA-0002

A small SoIL or PIL sample (<100 mg) was loaded into the IGA sample chamber using a stainless steel mesh cup. The samples were re-dried to remove moisture from atmospheric exposure by sequential flow of dry nitrogen streams at 60 °C and high vacuum until no weight drop over time was observed. Samples were then evacuated to high vacuum for 4 hours and the dry mass was recorded. After first measuring sample density using argon as an inert gas, CO<sub>2</sub> was introduced at a ramp rate of 180 mbar min<sup>-1</sup>. At each pressure interval, the CO<sub>2</sub> pressure was maintained for a period of 50 minutes to equilibrate. This process was repeated for each point up to the maximum operating pressure of 10 bar. The sample was then evacuated to high vacuum for an additional 4 hours until the sample returned to its starting weight before the same pressure ramp profile was used with N<sub>2</sub>. Density data and raw uptake data were then used to apply a buoyancy correction proportional to the applied pressure under isothermal conditions, with the assumption of the adsorbed gas density equalling the density of the corresponding gas in liquid state.<sup>22</sup> In cases where the mass of adsorbed gas was significantly less than the buoyancy effect of that gas at a given pressure, a simplified correction assuming zero gas adsorption was performed. The uptake results using this approximation were then used for recalculation of the buoyancy effect accounting for adsorbed gas density. This unavoidable approximation may marginally underestimate gas uptake, dependent on pressure, but will only apply when gas uptake is already very small.

### General procedure for high pressure testing

The pre-dried SoIL was tightly packed into a 7 cm, 12.7 mm diameter pipe with 0.5 g quartz wool wadding packed into either end. This is labelled in Fig. 3 as the packed adsorber. The sample was then re-dried under vacuum and heated nitrogen as in the small scale testing. The adsorber assembly, including both



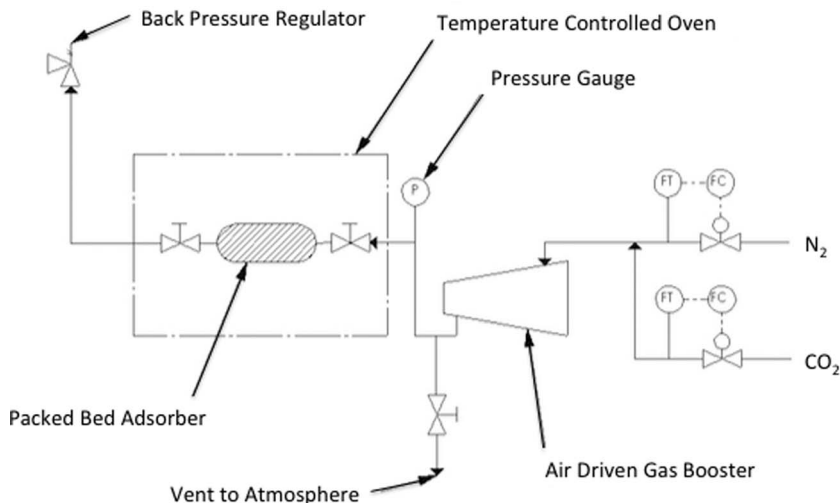


Fig. 3 Process flow diagram of high pressure testing apparatus.

valves either side of the adsorber, was detached and then measured gravimetrically using a high capacity 3 decimal place balance. Changes in weight from gas adsorption were measured similarly. The void spacing within the adsorber column was calculated using idealised packing equations.<sup>23</sup> This approach was validated by comparison with volumetric gas measurement using nitrogen on samples shown to have negligible nitrogen sorption capacity.

Uptake rate results were measured using short exposure times limited by pressure transducer response rate and manual speed. Desorption rates were measured by on-balance depressurisation timed using a stopwatch.

## Results and discussion

### Computer modelling

A number of anions and cations were investigated to determine their interactions with CO<sub>2</sub>. In the case of cations, the interaction was between the oxygen on the gas and the positive charge centre on the organic cation. Short intermolecular lengths were observed for ethylmethylimidazolium ions (2.38 Å) and tetraalkylammonium ions (2.50 Å). The CO<sub>2</sub> molecule occupied a geometry approximately orthogonal to the cation (shown in Fig. 4 for Emim<sup>+</sup>) exposing the C=O bond for interactions with the anion. Because the interaction is between the cation and the oxygen on CO<sub>2</sub> there is no distortion of the molecule, suggesting that the cation does not promote CO<sub>2</sub> activation but that it does stabilise the ion-gas complex. Similar studies showed one of the best anions to be acetate, with a binding energy for the IL to CO<sub>2</sub> of approximately 150.5 kJ mol<sup>-1</sup> and an O-C-O bond distortion of 5.4° for both ammonium and imidazolium salts.

This indicated that physisorption was the primary process as O-C-O bond angles approaching 120° (60° distortion) are expected for processes undergoing chemisorption. Therefore, it was decided to investigate tetraalkylammonium acetates as the primary target as they would be good candidates for physisorption



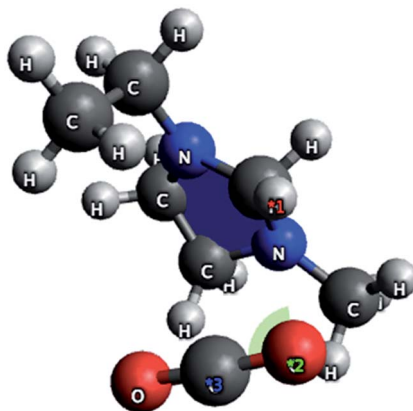


Fig. 4 CO<sub>2</sub>-cation interaction for [Emim]<sup>+</sup> cation from Avogadro molecular simulation.

studies and considerably cheaper than other anion-cation combinations. Some bromide derivatives were also prepared for comparison. These have weaker binding energies than the chlorides but also suffer from moisture instability.

### CO<sub>2</sub> adsorption by SoILs

As expected, the SoILs show somewhat lower CO<sub>2</sub> uptake capacity than found with corresponding RTILs at similar pressures (Fig. 5 and 6).<sup>24</sup> However, trends in uptake performance continued to follow previously-established trends in CO<sub>2</sub>

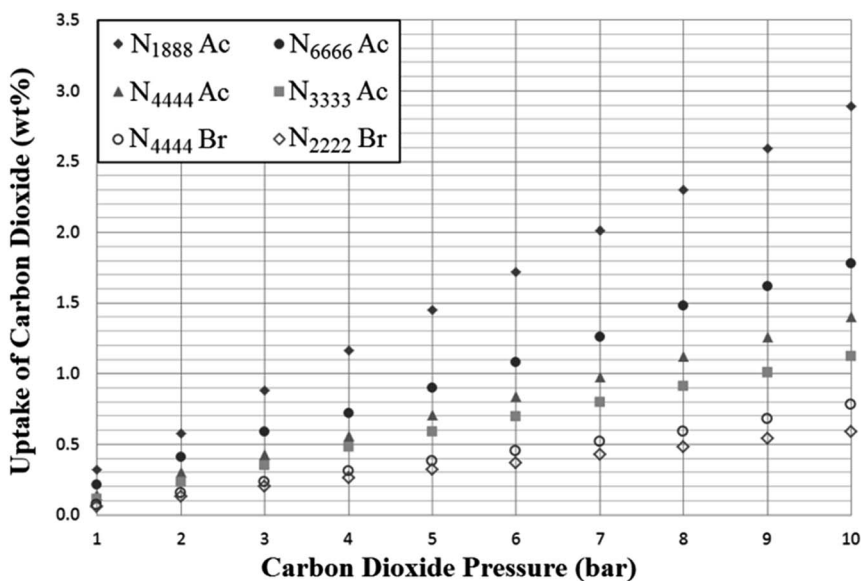


Fig. 5 Adsorption of carbon dioxide by selected tetraalkylammonium solid ionic liquids (SoILs) at a pressure range of 1–10 bar, 298 K. Uptake is given as mass CO<sub>2</sub> adsorbed per gram of sorbent.



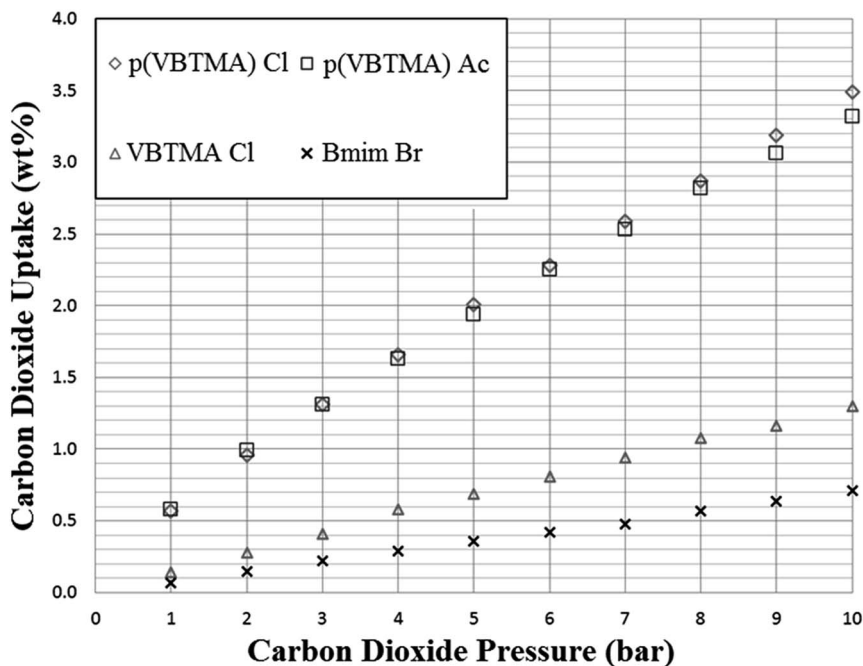


Fig. 6 Adsorption of carbon dioxide by selected polymer and solid ionic liquids at a pressure range of 1–10 bar, 298 K. Uptake is given as mass CO<sub>2</sub> adsorbed per gram of sorbent.

uptake shown by room temperature ionic liquids, such as the typically poorer performance of halide anion salts. This trend was reversed in the case of p(VBTMA) Cl, however, this can likely be attributed to differences in performance between PILs and monomeric SoILs, evidenced further by the differences in the uptake rate shown in later uptake experiments. Overall, it was shown that cations with longer chain lengths tended to show improved CO<sub>2</sub> adsorption. However, the difference in uptake capacity between N<sub>1888</sub> Ac and N<sub>6666</sub> Ac could also indicate that while long alkyl chain lengths are beneficial for CO<sub>2</sub> uptake, access to the quaternised nitrogen centre may also have a strong effect. Unfortunately, further exploration of any trends in tetraalkylammonium acetate SoILs with one short chain and three long chains was hindered by many other examples including N<sub>1666</sub> Ac, N<sub>1444</sub> Ac, N<sub>1333</sub> Ac and N<sub>2666</sub> Ac being found to be liquids at room temperature.

### Selectivity of SoILs for CO<sub>2</sub> and N<sub>2</sub> adsorption

As anticipated, adsorption of nitrogen was extremely low for all SoILs tested, with very small quantities adsorbed at higher pressures (see Fig. 7). Due to the near-zero uptake at low pressures and the low adsorption amounts, assumptions concerning the buoyancy correction had to be carried out. While, as mentioned in the experimental section, this is more likely to underestimate uptake than overestimate, with the buoyancy correction effect being 10 times larger than the measured uptake, it cannot be ruled out that the uptake observed is not an artifact



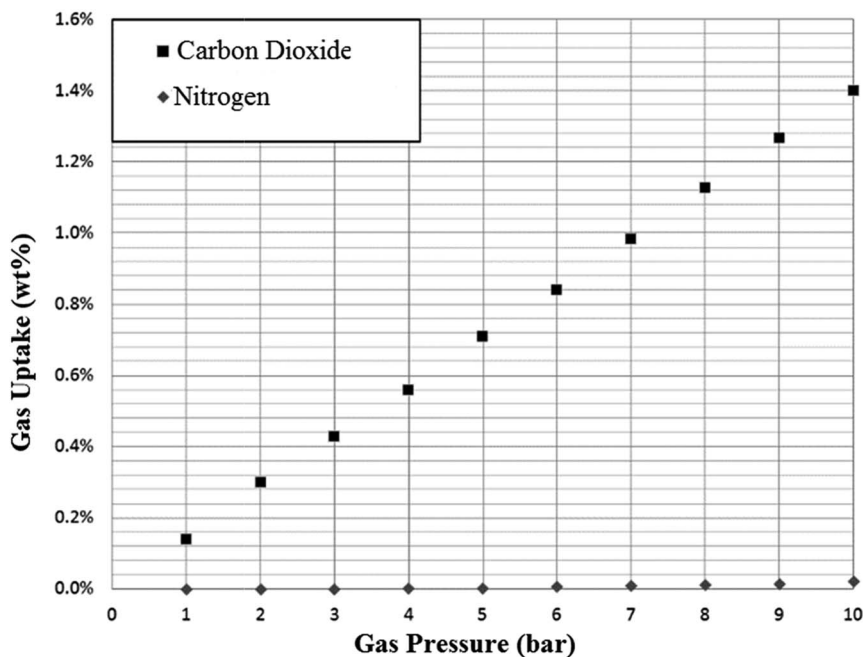


Fig. 7 Example adsorption of nitrogen on  $N_{4444}$  Ac at 298 K. Uptake is given as mass  $CO_2$  adsorbed per gram of sorbent.

of buoyancy correction, which might explain the quadratic shape of the uptake curves. In any event, as shown in Table 1,  $CO_2:N_2$  selectivity for all ILs is very high and approximately in line with RTIL behaviour.<sup>4</sup> It should be noted that for these measurements  $CO_2$  and nitrogen uptake were measured separately and not in competition.

### High pressure testing

A further selection of the SoILs were synthesised on a larger scale, to allow for testing at higher pressures and larger scales in the high pressure testing

Table 1  $CO_2$ ,  $N_2$  and selectivity results for each SoIL at 10 bar, 298 K. Uptake is given as mass  $CO_2$  adsorbed per gram of sorbent

SoIL	Uptake of $N_2$ at 10 bar, 298 K (wt%)	Uptake of $CO_2$ at 10 bar, 298 K (wt%)	Selectivity for $CO_2$
$N_{3333}$ Ac	0.019	1.12	59 : 1
$N_{4444}$ Ac	0.021	1.40	67 : 1
$N_{6666}$ Ac	0.023	1.78	77 : 1
$N_{1888}$ Ac	0.025	2.89	116 : 1
$N_{2222}$ Br	0.011	0.59	53 : 1
$N_{4444}$ Br	0.013	0.78	60 : 1
Bmim Br	0.013	0.71	54 : 1
VBTMA Cl	0.047	1.30	28 : 1
p(VBTMA) Cl	0.032	3.49	109 : 1
p(VBTMA) Ac	0.023	3.32	144 : 1



apparatus shown previously in Fig. 3. Sample sizes in each experiment were at least 2.5 g and the SoILs were chosen for availability and ease of synthesis and purification. Small discrepancies can be seen between the small-scale testing and those carried out in the larger adsorber when the same pressures are used. However, this is likely due to the slightly diminished gas–solid contact occurring within the solid-walled adsorber pipe compared to the stainless steel mesh container used within the IGA sample chamber. The results of these experiments showed that at elevated pressure, uptake results comparable with those previously reported using RTILs were achieved (see Fig. 8). For comparison, the maximum theoretical uptake of aqueous MEA in 30 wt% water is 10.8% when a stoichiometry of  $\text{CO}_2 : \text{MEA}$  of 1 : 2 is achieved. While this metric compares high pressure uptake using SoILs with atmospheric-pressure uptake of MEA, the possibility of MEA achieving higher uptakes at elevated pressures cannot be ruled out. However, in a working scenario, this approach would have to combine the high MEA temperature swing energy costs with further pressure swing energy costs.<sup>25–27</sup>

Other more direct comparisons may be made with solid sorbents such as activated carbon and zeolite 13X. Of these, activated carbon shows an uptake capacity of 48.6 wt% at 40 bar, and zeolite 13X shows 32.4 wt% at 32 bar. While compared to Fig. 8, both activated carbon and zeolite 13X have much higher  $\text{CO}_2$  uptake capacities at elevated pressures,  $\text{CO}_2/\text{N}_2$  uptake selectivity is lower (3.9 : 1 and 3.3 : 1 respectively) by the same measurement as shown in Table 1. Additionally, it should be noted that a significant amount of  $\text{CO}_2$  remains bound to



Fig. 8 Results of higher pressure testing of selected ionic liquids from this work (solid markers) compared with literature results for common RTILs used for  $\text{CO}_2$  adsorption at 298 K (hollow markers). <sup>(a)</sup>Zhu,<sup>25</sup> <sup>(b)</sup>Peters,<sup>26</sup> <sup>(c)</sup>Lee<sup>27</sup> Uptake is given as mass  $\text{CO}_2$  adsorbed per gram of sorbent.



these sorbents at atmospheric pressure (9.8% and 28.7% respectively), which will either reduce efficiency when using pressure swing only, or mandate vacuum swing approaches, which again would add costs.<sup>28,29</sup>

### Rate of CO<sub>2</sub> uptake

The nature of the high pressure testing apparatus allowed measurement of the rate of CO<sub>2</sub> adsorption. This was achieved by over-pressurising the inlet CO<sub>2</sub> pipeline (see Fig. 3) to a fixed pressure, which allowed it to act as a ballast vessel while the valve to the adsorber was closed. In this way, it was possible to pressurise the adsorber to a repeatable pressure and measure the isobaric rate of uptake in discrete, extremely short experiments. Desorption experiments were carried out by simple depressurisation to atmosphere during weighing.

Due to the limitations of manually opening and closing the adsorber valves and the response times of the pressure gauge and balance, sample times shorter than 2 or 3 seconds were not possible. Results shown in Fig. 9 show the extremely rapid uptake and desorption achieved for both the tetra-alkylammonium and imidazolium SoILs. It should be noted that for both A and B a significant portion of the adsorb time will be limited by the motion of the gas itself and as such these represent an overestimation of maximum uptake times. Fig. 9A shows N<sub>4444</sub> acetate reaching 94% capacity: no weight change is observed in experiments longer than 10 seconds, with maximum capacity reached after approximately 8 seconds. Following this, desorption back to the starting weight was completed within 4 seconds. In comparison, RTILs have been shown to take up to 5 hours to reach equilibrium, typically taking longer than 1 hour to reach 50% maximum capacity.<sup>30</sup> Other solid sorbents such as activated carbon and 13X are swifter than RTILs, but still significantly slower than the SoILs with uptake rates of 1 minute to reach 50% of maximum capacity and 30 minutes to reach 100% for activated carbon.<sup>31</sup> 13X has a similar uptake rate performance, taking 50 seconds to 1 minute to achieve approximately 50% uptake and up to 100 minutes to reach full capacity.<sup>32</sup>

By taking the mass of CO<sub>2</sub> adsorbed during the first 3 seconds of uptake and the desorb rate, it can then be calculated that the N<sub>4444</sub> acetate, if cycled for 3 seconds of uptake followed by 4 seconds of desorb, could theoretically process a total of 129.4 g of CO<sub>2</sub> per kilogram of sorbent per minute in pure CO<sub>2</sub> at a pressure of 15 bar. While this measure does not take into account a wide range of factors, not least that the working partial pressure of CO<sub>2</sub> of a real pressure swing capture system would be much lower, or any possible scaling effect, it usefully illustrates the potential benefits of fast sorbent cycling.

Fig. 9B shows Bmim bromide achieving even faster uptake, although at lower total capacity with the maximum capacity being reached in approximately 3.5 seconds. Once again desorption was complete in under 4 seconds. By applying the same calculation as that carried out for N<sub>4444</sub> acetate, the combination of the higher density and lower uptake capacity of the Bmim bromide gives a maximum CO<sub>2</sub> process rate of 98.5 g CO<sub>2</sub> per kilogram sorbent per minute under the same conditions. This shows the poorer performance of the halide-based SoILs in comparison with their acetate counterparts.

Significantly slower uptake was observed using the polymeric ionic liquid sorbent p(VBTMA) chloride (Fig. 9C), requiring approximately 3 minutes to reach





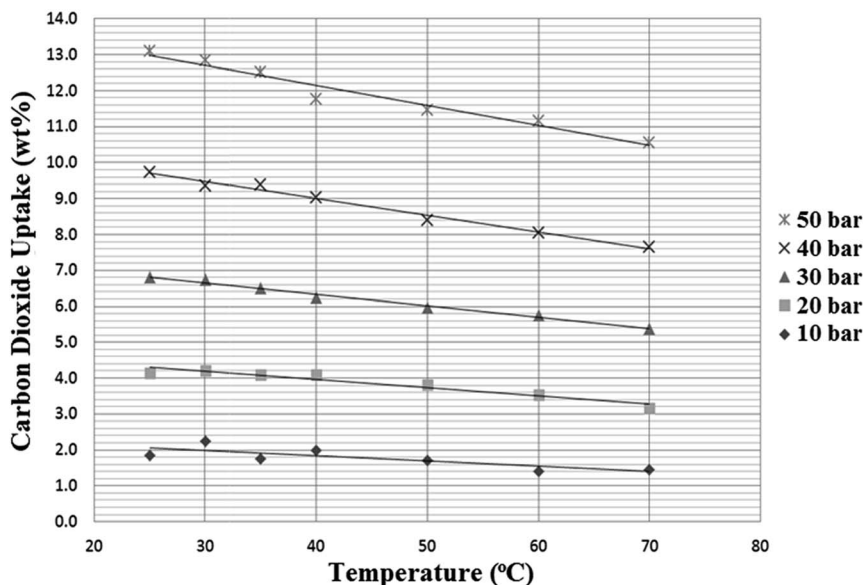


Fig. 10 The effect of temperature on the CO<sub>2</sub> uptake capacity of N<sub>4444</sub> acetate at different pressures.

which can easily be very high, even at only moderate pressures. Therefore, a final series of tests was carried out on the N<sub>4444</sub> acetate SoIL, chosen for its high melting point (95–98 °C), to determine the effect of temperature on CO<sub>2</sub> uptake at different pressures. While CO<sub>2</sub> solubility in RTILs is extremely sensitive to gas temperature, the sensitivity of the SoILs to temperature was much subtler, with more pronounced drops in uptake capacity only occurring at both high temperatures and high pressures as shown in Fig. 10. While we were unable to carry out these experiments when both nitrogen and carbon dioxide were present to probe how this may affect selectivity, it can be suggested that as long as the SoILs do not melt, temperature may be no great obstacle to uptake capacity. This feature, if common across other SoILs, further underlines their observed robust nature, as seen in the prolonged experiments carried out to provide the data shown in Fig. 10 on a single sample which showed no detectable degradation despite the prolonged heating.

## Conclusions

In summary, a series of experiments were carried out to determine if the high degree of CO<sub>2</sub> solubility and selectivity over N<sub>2</sub> in Room Temperature Ionic Liquids (RTILs) for pressure swing carbon capture was replicated in finely-ground solid ionic liquids. From the results shown here, it can be shown that despite slightly diminished maximum uptake capacity for CO<sub>2</sub>, these Solid Ionic Liquids (SoILs) have great potential benefit as capture agents in pressure swing adsorption due to their extremely rapid uptake and desorb speeds, thousands or tens of thousands of times faster than RTILs. As a consequence, far less solid ionic sorbent would be required in a given process than the corresponding liquid



sorbent system, helping to counteract the major perceived disadvantage to ionic liquids of high cost. Additional benefits would appear to include a high tolerance to elevated temperatures without significant loss of capture capacity and a very low rate of degradation under experimental conditions. We believe that this overlooked class of organic salt has great potential for further development, enabling low-cost carbon capture for climate change mitigation.

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## Notes and references

- 1 J. Gale, J. Bradshaw, Z. Chen, A. Garg, D. Gomez, H.-H. Rogner, D. Simbeck and R. Williams, *IPCC Special Report on Carbon Dioxide Capture and Storage, Working Group III of the Intergovernmental Panel on Climate Change*, Cambridge University Press, Cambridge, UK, 2005, ISBN-13 978-0-521-86643-9.
- 2 L. B. Gregory and W. G. Scharmann, *Ind. Eng. Chem.*, 1937, **29**, 514–519.
- 3 G. Gouedard, D. Picq, F. Launay and P.-L. Carrette, *Int. J. Greenhouse Gas Control*, 2012, **10**, 244–270.
- 4 J. L. Anthony, J. L. Anderson and E. J. Maginn, *J. Phys. Chem. B*, 2005, **109**, 6366–6374.
- 5 C. Maton, N. De Vos and C. V. Stevens, *Chem. Soc. Rev.*, 2013, **42**, 5963–5977.
- 6 Aqueous MEA diffusion coefficient: M. S. Jassim, G. Rochelle, D. Eimer and C. Ramshaw, *Ind. Eng. Chem. Res.*, 2007, **46**, 2823–2833 Example ionic liquid diffusion coefficients: C. Moya, J. Palomar, M. Gonzales-Miquel, J. Bedia and F. Rodriguez, *Ind. Eng. Chem. Res.*, 2014, **53**, 13782–13789.
- 7 Example of MEA-IL mixture for capture: J. Yang, X. Yu, J. Yan and S.-T. Tu, *Ind. Eng. Chem. Res.*, 2014, **53**, 2790–2799 Example of MeOH-IL mixture for capture: C. Dai, W. Wei, Z. Lei, C. Li and B. Chen, *Fluid Phase Equilib.*, 2015, **391**, 9–17.
- 8 N. Markusson and S. Haszeldine, *Energy Policy*, 2010, **38**, 6695–6702.
- 9 D. Cameron, Hansard, HC Deb, December 16 2015, vol. 603, col 1548.
- 10 J. S. Wilkes, P. Wasserscheid and T. Welton, *Ionic Liquids in Synthesis*, ed. P. Wasserscheid and T. Welton, Wiley-VCH, Weinheim, Germany, 2nd edn, 2002, ch. 1, pp. 1–6.
- 11 J. Tang, Y. Shen, M. Radosz and W. Sun, *Ind. Eng. Chem. Res.*, 2009, **48**, 9113–9118; J. Tang, W. Sun, H. Tang, M. Radosz and Y. Shen, *Macromolecules*, 2005, **38**, 2037–2039.
- 12 J. M. Plaza, D. Van Wagener and G. T. Rochelle, *Int. J. Greenhouse Gas Control*, 2010, **4**, 161–166.
- 13 R. Gross, P. Heptonstall, M. Leach, J. Skea, D. Anderson and T. Green, *Renewable Electricity and the Grid: The Challenge of Variability*, ed. G. Boyle, Cromwell Press, Trowbridge, UK, 2007, ch. 4, pp. 73–95.
- 14 T. Nittaya, P. L. Douglas, E. Croiset and L. A. Ricardez-Sandoval, *Fuel*, 2014, **116**, 672–691.



- 15 O. M. Moen and H. S. Stene, *Power Plant with CO<sub>2</sub> Capture Based on PSA Cycle*, Norwegian University of Science and Technology, Trondheim, Norway, 2014.
- 16 MEA capture energy figures taken from: T. Harkin, A. Hoadley and B. Hooper, *Energy Proc.*, 2009, **1**, 3817–3825; L. M. Romeo, I. Bolea and J. M. Escosa, *Appl. Therm. Eng.*, 2008, **28**, 1039–1046; Y. Yang and R. Zhai, *Paths to Sustainable Energy*, J. Nathwani and A. Ng, InTech, Rijeka, Croatia, 2010, ch. 24, pp. 499–510; U. Desideri and A. Paolucci, *Energy Convers. Manage.*, 1999, **40**, 1899–1915.
- 17 Advanced amine capture figures estimated from existing figures given by: S. Wong and R. Bioletti, *Carbon Dioxide Separation Technologies*, Carbon & Energy Management, Alberta, Canada, 2002; M. Rameshni, *Carbon Capture Overview*, Worley Parsons Resources & Energy, Monrovia, CA, USA, 2010, calculated as 30% reduction in energy usage with advanced amines compared to MEA.
- 18 Membrane CO<sub>2</sub> separation energy figures taken from: P. K. Kundu, A. Chakma and X. Feng, *Int. J. Greenhouse Gas Control*, 2014, **28**, 248–256; B. Belaissaoui, G. Cabot, M.-S. Cabot, D. Willson and E. Favre, *Chem. Eng. Sci.*, 2013, **97**, 256–263; B. Belaissaoui, D. Willson and E. Favre, *Chem. Eng. J.*, 2012, **211–212**, 122–132.
- 19 Vacuum pressure swing separation energy figures taken from: J. Zhang, P. A. Webley and P. Xiao, *Energy Convers. Manage.*, 2008, **49**, 346–356; S. Krishnamurth, V. R. Rao, S. Guntuka, P. Sharratt, R. Haghpanah, A. Rajendran, M. Amanullah, I. A. Karimi and S. Farooq, *AIChE J.*, 2014, **60**, 1830–1842; L. Liu, T. Du, X. Fang, S. Che and W. Tan, *The 26<sup>th</sup> Chinese Control and Decision Conference*, IEEE, USA, 2014, pp. 4038–4041.
- 20 High pressure swing energy costs calculated in hybrid thermal/high pressure and vacuum/high pressure systems in line with model predictions: Y. Xie, Y. Zhang, X. Lu and X. Ji, *Appl. Energy*, 2014, **136**, 325–335; O. M. Moen and H. S. Stene, *Power Plant with CO<sub>2</sub> Capture Based on PSA Cycle*, NTNU Trondheim, Norway, 2014.
- 21 J. Albo, T. Yoshioka and T. Tsuru, *Sep. Purif. Technol.*, 2014, **122**, 440–448.
- 22 K. Murata, M. El-Merraoui and K. Kaneko, *J. Chem. Phys.*, 2001, **114**, 4196–4205.
- 23 H. E. White and S. F. Walton, *J. Am. Ceram. Soc.*, 1937, **20**, 155–166.
- 24 Y. Xie, Y. Zhang, X. Lu and X. Ji, *Appl. Energy*, 2014, **136**, 325–335.
- 25 Z. Lei, J. Yuan and J. Zhu, *J. Chem. Eng. Data*, 2010, **55**, 4190–4194.
- 26 A. Shariati, K. Gutkowski and C. J. Peters, *AIChE J.*, 2005, **51**, 1532–1540.
- 27 D.-J. Oh and B.-C. Lee, *Korean J. Chem. Eng.*, 2006, **23**, 800–805.
- 28 F. Dreisbach, R. Staudt and J. U. Keller, *Adsorption*, 1999, **5**, 215–227.
- 29 S. Cavenati, C. A. Grande and A. E. Rodrigues, *J. Chem. Eng. Data*, 2004, **49**, 1095–1101.
- 30 J. Tang, H. Tang, W. Sun and M. Radosz, *Polymer*, 2005, **46**, 12460–12567.
- 31 E. S. Kikkinides and R. T. Yang, *Ind. Eng. Chem. Res.*, 1993, **32**, 2714–2720.
- 32 D. Ko, R. Siriwardane and L. T. Biegler, *Ind. Eng. Chem. Res.*, 2003, **42**, 339–348; Z. Zhang, W. Zhang, X. Chen, Q. Xia and Z. Li, *Separ. Sci. Technol.*, 2010, **45**, 710–719.

