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# Role of ion-selective membranes in the carbon balance for CO<sub>2</sub> electroreduction *via* gas diffusion electrode reactor designs†

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In this work, the effect of ion-selective membranes on the detailed carbon balance was systematically analyzed for high-rate CO<sub>2</sub> reduction in GDE-type flow electrolyzers. By using different ion-selective membranes, we show nearly identical catalytic selectivity for CO<sub>2</sub> reduction, which is primarily due to a similar local reaction environment created at the cathode/electrolyte interface *via* the introduction of a catholyte layer. In addition, based on a systematic exploration of gases released from electrolytes and the dynamic change of electrolyte speciation, we demonstrate the explicit discrepancy in carbon balance paths for the captured CO<sub>2</sub> at the cathode/catholyte interface *via* reaction with OH<sup>−</sup> when using different ion-selective membranes: (i) the captured CO<sub>2</sub> could be transported through an anion exchange membrane in the form of CO<sub>3</sub><sup>2−</sup>, subsequently releasing CO<sub>2</sub> along with O<sub>2</sub> in the anolyte, and (ii) with a cation exchange membrane, the captured CO<sub>2</sub> would be accumulated in the catholyte in the form of CO<sub>3</sub><sup>2−</sup>, while (iii) with the use of a bipolar membrane, the captured CO<sub>2</sub> could be released at the catholyte/membrane interface in the form of gaseous CO<sub>2</sub>. The unique carbon balance path for each type of membrane is linked to ion species transported through the membranes.

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## Introduction

The electrochemical reduction of CO<sub>2</sub> to valuable chemicals and fuels powered by renewable electricity provides an attractive strategy to close the anthropogenic carbon cycle and store intermittent renewable energy.<sup>1–8</sup> In the past, great efforts have been devoted to the development of selective, efficient and stable electrocatalysts in CO<sub>2</sub>-saturated aqueous solutions using H-type cells.<sup>9–16</sup> Striking progress has been made in exploring catalysts for CO<sub>2</sub> reduction in H-type cells. However, CO<sub>2</sub> reduction in H-type cells only allows for relatively low current densities due to mass transport limitations in aqueous solutions.<sup>17–19</sup> Large-scale utilization of electrochemical conversion of CO<sub>2</sub> requires high reaction rates (*i.e.* high current densities). In this context, flow electrolyzers with gas-diffusion electrodes (GDEs) have gained considerable attention for CO<sub>2</sub> reduction, owing to the fact that GDEs allow for a very thin mass-transfer boundary layer (~50 nm).<sup>18,19</sup> By using GDE-type flow electrolyzers, the mass-transport of CO<sub>2</sub> and gaseous products on the surface of the catalysts can be accelerated, achieving

commercially relevant current densities (>100 mA cm<sup>−2</sup>) along with high selectivity toward a desired product.<sup>20–29</sup>

To date, most of the high-rate CO<sub>2</sub> reduction studies based on GDE-type flow electrolyzers have been performed using anion exchange membranes (AEMs).<sup>20–29</sup> However, our recent work demonstrated a substantial crossover of anionic CO<sub>2</sub> reduction products such as acetate and formate through AEMs in GDE-type flow electrolyzers.<sup>29</sup> More importantly, after the electrolytes reach a steady state, it was found that about 70% of the consumed CO<sub>2</sub> is captured at the cathode/electrolyte interface *via* reaction with OH<sup>−</sup>, forming CO<sub>3</sub><sup>2−</sup>, which is transported to the anolyte *via* an AEM as a charge-carrier.<sup>29</sup> Subsequently, CO<sub>3</sub><sup>2−</sup> coming from the catholyte reacts with H<sup>+</sup> in the vicinity of the anode, releasing gaseous CO<sub>2</sub> from the anolyte with the O<sub>2</sub> stream, which means that most of the consumed CO<sub>2</sub> (70%) is captured in the catholyte and emitted from the anolyte. In other words, only 30% of the CO<sub>2</sub> consumed is involved in CO<sub>2</sub> conversion into products. This finding indicates that many of the current techno-economic analyses for high-rate electroreduction of CO<sub>2</sub> must be reconsidered if significant CO<sub>2</sub> crossover occurs.<sup>29,30</sup>

One approach to reduce the CO<sub>2</sub> crossover would be to use a two-step cascade process, which consists of an initial CO<sub>2</sub> reduction to CO and a subsequent CO conversion into highly valuable multi-carbon products that have no carbon source crossover.<sup>31,32</sup> However, even in this two-step procedure with 100% CO faradaic efficiency for the first step, 50% of all consumed CO<sub>2</sub> could still be emitted out of the anolyte using an

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AEM.<sup>29</sup> Theoretically, utilization of a cation exchange membrane (CEM) or a bipolar membrane (BPM) can prevent the CO<sub>2</sub> crossover in GDE-type flow electrolyzers. However, only a few studies on high-rate CO<sub>2</sub> reduction (>100 mA cm<sup>-2</sup>) have been carried out in GDE-type electrolyzers using CEMs<sup>33–35</sup> or BPMs<sup>36–38</sup> to date.

This study describes a systematic exploration of the effect of ion-selective membranes on the detailed carbon balance including CO<sub>2</sub> consumption, products and CO<sub>2</sub> crossover, as well as CO<sub>2</sub> emission in GDE-type flow electrolyzers. Herein, we demonstrate the comparison of catalytic selectivity, CO<sub>2</sub> consumption rate (*via* the reaction with OH<sup>-</sup>), and the dynamic change of electrolyte speciation among three different types of ion-selective membranes. By a systematic exploration of the gases released from the catholyte or anolyte, ion species change in the electrolyte and ion species transport *via* membranes, and this work provides mechanistic insights into the role of ion-selective membranes in carbon balancing for high-rate CO<sub>2</sub> reduction.

## Results and discussion

### Electrocatalytic CO<sub>2</sub> reduction performance

In this work, Cu electrocatalyst layers (~70 nm) were prepared on top of microporous carbon layers of GDEs by magnetron sputtering at an argon pressure of 2 mTorr (Fig. S1†). The detailed materials characterization of the Cu catalyst layers on GDEs has been reported in our previous work.<sup>29</sup> We conducted CO<sub>2</sub> reduction electrolysis experiments in a three-compartment flow electrolyzer where a Cu catalyst coated on a GDE was positioned between the gas and catholyte chambers, as shown in Fig. 1a. An ion-selective membrane was used to separate the catholyte and anolyte flow chambers in which electrolytes continuously flow, and it should be noted that AEM, CEM and BPM were all tested in this work. During CO<sub>2</sub> reduction, gaseous CO<sub>2</sub> at a constant flow rate (45 ml min<sup>-1</sup>) was continuously fed into the gas chamber (Fig. 1a), and a fraction of the CO<sub>2</sub> diffused to the surface of the catalysts in an electrolyte and then converted into gas products such as C<sub>2</sub>H<sub>4</sub> and liquid products such as ethanol (Fig. 1b). Gas products mixed with the unreacted CO<sub>2</sub> were directly vented into the gas-sampling loop of a gas chromatograph (GC) for periodic quantification. The liquid products were diluted and circulated in the given catholyte and anolyte reservoirs, and were detected *via* high-performance liquid chromatography (HPLC) after completion of the CO<sub>2</sub> reduction electrolysis experiments.

In order to get reliable catalytic selectivity for gas products in high-rate CO<sub>2</sub> reduction, gas flow out of the reactor was monitored *via* a volumetric flowmeter (Fig. S2†).<sup>29</sup> Fig. 1c shows that nearly identical gas flow rates were observed out of the electrolyzer when using an AEM, CEM and BPM in 1 M KHCO<sub>3</sub> at 200 mA cm<sup>-2</sup>, indicating a similar CO<sub>2</sub> consumption rate. This observation is primarily due to the same OH<sup>-</sup> generation rate *via* cathodic reactions (*i.e.* similar local pH created at the cathode/electrolyte interface). The faradaic efficiencies of gas products calculated using these corrected gas flow rates were

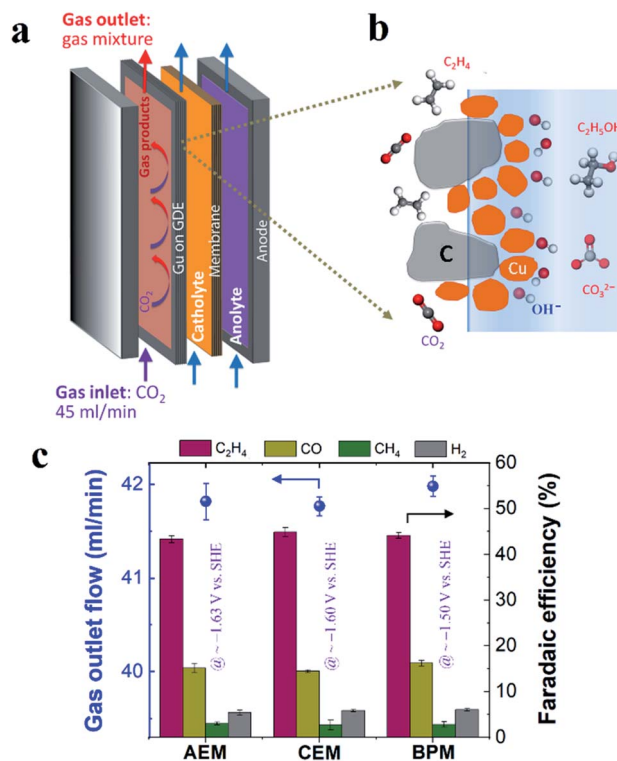


Fig. 1 (a) Schematic illustration of three-compartment flow electrolyzers. (b) Schematic illustration of the cathode/electrolyte interface for CO<sub>2</sub> conversion. (c) Rates of gas flow out of the gas chamber after CO<sub>2</sub> reduction (left axis) and faradaic efficiencies for gas products (right axis) using different ion-selective membranes in 1 M KHCO<sub>3</sub> at 200 mA cm<sup>-2</sup>. The *iR*-corrected potentials are labeled with purple color in (c). 45 ml min<sup>-1</sup> CO<sub>2</sub> inlet flow was used in all the experiments.

plotted for different ion-selective membranes (Fig. 1c). As shown in Fig. 1c, C<sub>2</sub>H<sub>4</sub> is the primary gas product for all the different ion-selective membranes, along with small amounts of CO and H<sub>2</sub> and only trace amounts of CH<sub>4</sub>. Notably, the faradaic efficiencies for gaseous products had no obvious variation when different types of membranes were utilized (at nearly identical potentials, as shown in Fig. 1c). This result indicates that catalytic selectivity of gaseous products is independent of the type of ion-selective membrane for high-rate CO<sub>2</sub> reduction in the three-compartment electrolyzers.

In addition to the detected gas products, liquid-phase products in both catholyte and anolyte were all analyzed due to the potential crossover of liquid products from the catholyte to the anolyte *via* membranes.<sup>39,40</sup> As noted in Fig. 2a, substantial anionic CO<sub>2</sub> reduction products (such as formate and acetate) crossed over from the catholyte to the anolyte *via* the AEM by electromigration, with only minimal crossover for uncharged liquid products. In contrast, the CEM and BPM exhibited negligible crossover for both anionic liquid products and uncharged products (Fig. 2a). This observation indicates that both CEM and BPM are capable of inhibiting the crossover of anionic and neutral liquid products.

For determining the total amounts of liquid products, liquid products evaporated from GDEs into the gas chamber



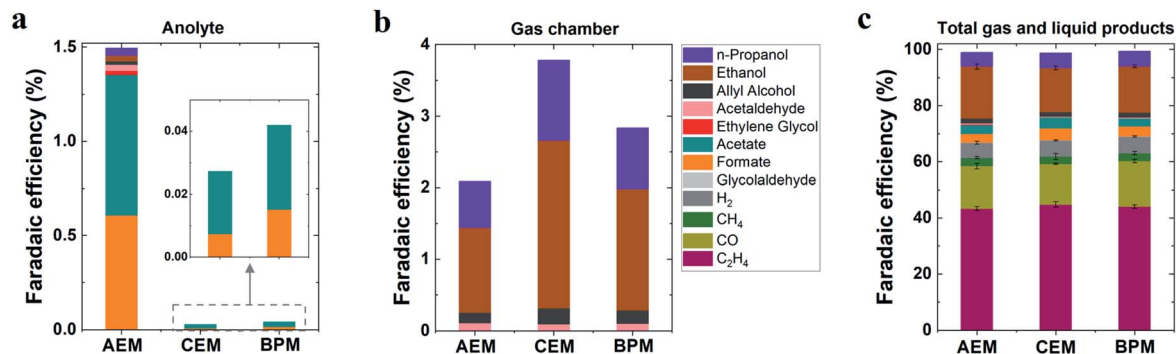


Fig. 2 (a) Faradaic efficiencies for detected liquid products in anolyte and (b) faradaic efficiencies for liquid products evaporated from GDEs into the gas chamber. (c) Faradaic efficiencies for all detected gas and liquid products in 1 M KHCO<sub>3</sub> at 200 mA cm<sup>-2</sup> for various membranes. Total liquid products were counted *via* analysis of both catholyte and anolyte as well as liquid products evaporated from GDEs into the gas chamber.

of the reactor were also collected for analysis (using a setup shown in Fig. S3†).<sup>41</sup> No matter which type of ion-selective membrane was used, alcohol products such as *n*-propanol and ethanol experienced considerable evaporation through the gas diffusion layer of the GDE (Fig. 2b), which is due to their high volatility. In addition, we found that acetaldehyde had the highest evaporation ratio among liquid products (Fig. S4†). This finding may be attributed to two reasons, (i) its relatively high vapor pressure and (ii) its further reduction to ethanol on the cathode where a substantial amount of acetaldehyde was produced initially and subsequently converted into ethanol.<sup>42</sup> Based on the quantification of liquid products in both catholyte and anolyte as well as liquid products evaporated from GDEs into the gas chamber (eqn (S12)†), faradaic efficiencies of all liquid products were evaluated for all the different types of membranes (Fig. 2c). As shown in Fig. 2c, ethanol was the dominant liquid product along with *n*-propanol, acetate and formate as minor products. There appears to be no significant variation in liquid product formation across all types of membranes. All the above results imply that the role of ion-selective membrane is almost negligible in affecting catalytic selectivity of high-rate CO<sub>2</sub> reduction in the three-compartment electrolyzers, owing to the similar local reaction environment created on the cathode *via* the introduction of a catholyte layer. It should be noted that zero-gap electrolyzers lacking a catholyte layer have clearly shown the change of CO<sub>2</sub> reduction selectivity by the different types of ion-selective membranes.<sup>43,44</sup>

### Capture and emission of CO<sub>2</sub> throughout the electrolyte

In accordance with our recent carbon balance study,<sup>29</sup> the gases released from the anolyte were systematically explored for CO<sub>2</sub> reduction *via* an AEM with 1 M KHCO<sub>3</sub>, elucidating a two-step procedure of CO<sub>2</sub> capture at the cathode/electrolyte interface *via* reaction with OH<sup>-</sup> and subsequent CO<sub>2</sub> degassing from the anolyte due to H<sup>+</sup> in the vicinity of the anode (Scheme 1a). With the nearly identical catalytic selectivity (Fig. 2c) and similar total CO<sub>2</sub> consumption rate (similar gas outlet shown in Fig. 1c), the same OH<sup>-</sup> generation rate *via* cathodic reactions means that the capability of capturing CO<sub>2</sub> for carbonate formation at the

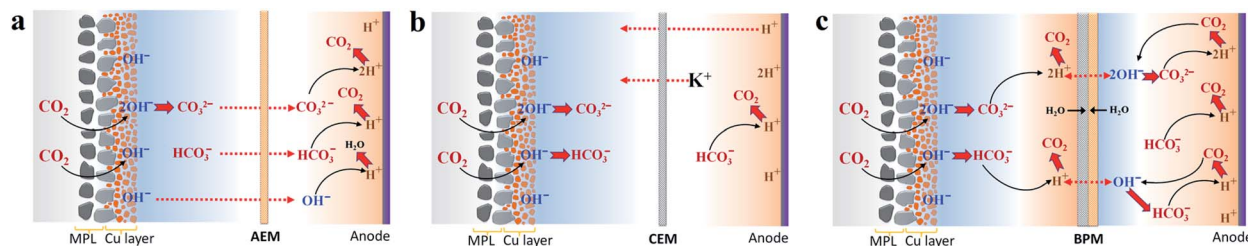
cathode/electrolyte interface using a CEM and BPM should be similar to that of an AEM. Thus, for a CEM and BPM, substantial additional carbonate anions produced in the reaction of CO<sub>2</sub> and OH<sup>-</sup> generated *via* the cathodic reactions must be either balanced with extra cation species (the total anion charge equals the total cation charge) or emitted from the electrolyte as gaseous CO<sub>2</sub>. To uncover the role of different membrane types in the carbon balance for flow electrolyzers, gases released from the electrolyte were detected for the CEM and BPM, respectively (using a closed-cycle anolyte with a vent for gases shown in Fig. S5†).

Theoretically, the composition ratio of CO<sub>2</sub>/O<sub>2</sub> in the gas stream from the anolyte will be 4, 2 or 0 if the only anion species for neutralizing H<sup>+</sup> generated on the anode is HCO<sub>3</sub><sup>-</sup>, CO<sub>3</sub><sup>2-</sup> or OH<sup>-</sup>.<sup>28,29</sup> In addition, under the consideration that HCO<sub>3</sub><sup>-</sup>, CO<sub>3</sub><sup>2-</sup> or OH<sup>-</sup> is the only anion species of neutralization reaction with H<sup>+</sup>, the theoretically calculated CO<sub>2</sub> flow rate will be 6.0, 3.0 or 0 ml min<sup>-1</sup> at 200 mA cm<sup>-2</sup> with a geometric active area of 2 cm<sup>2</sup> (Table S2†).

Fig. 3a–c show the comparison of gases released in the anolyte over the course of electrolysis for all the different ion-selective membranes. When an AEM was used, the CO<sub>2</sub>/O<sub>2</sub> ratio decreased from ~3 to ~2 in the first 4 h and then remained at ~2 over the remaining course of electrolysis. This observation is due to the fact that the CO<sub>2</sub> evolution *via* the H<sup>+</sup> neutralization reaction changed rapidly from a mixture of HCO<sub>3</sub><sup>-</sup> and CO<sub>3</sub><sup>2-</sup> to nearly pure CO<sub>3</sub><sup>2-</sup> using the AEM (Fig. 3a). In contrast, as noted in Fig. 3b, the CEM experienced a consistent CO<sub>2</sub>/O<sub>2</sub> ratio of ~4 and a constant CO<sub>2</sub> flow rate of 6 ml min<sup>-1</sup> for the duration of electrolysis at 200 mA cm<sup>-2</sup>, which implies that the CO<sub>2</sub> formation was always derived from HCO<sub>3</sub><sup>-</sup> in the anolyte. This finding is ascribed to the fact that the CO<sub>3</sub><sup>2-</sup> formed *via* CO<sub>2</sub> capture in the catholyte cannot be transported to the anolyte *via* the CEM since the functional groups (typically SO<sub>3</sub><sup>-</sup> groups) only allow cation species (such as K<sup>+</sup>) to pass through (Scheme 1b). It should be noted that the CO<sub>2</sub> reduction electrolysis *via* the CEM was tested for just ~3 h, since the anolyte conductivity rapidly decreased from ~70 mS cm<sup>-1</sup> to ~3 mS cm<sup>-1</sup> after ~3 h (Fig. S8b†), which is consistent with previous work.<sup>45</sup> All the above results with the CEM indicate that almost no anionic species were





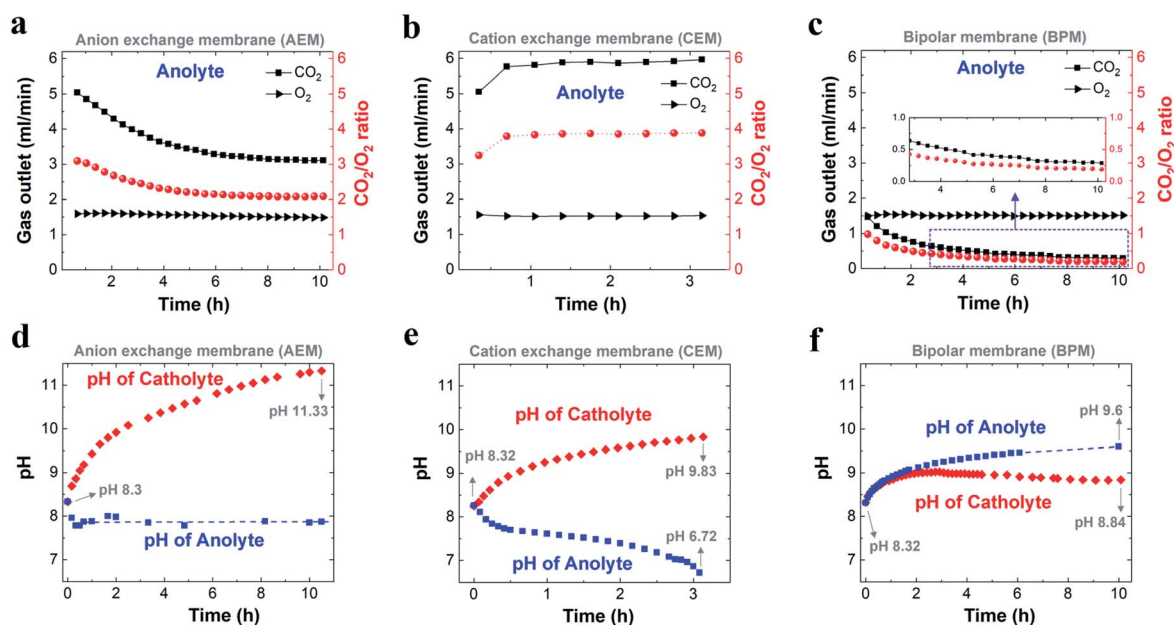


**Scheme 1** Proposed carbon balance paths *via*  $\text{CO}_2$  capture at the cathode/catholyte interface and  $\text{CO}_2$  evolution from the anolyte or catholyte in flow electrolyzers combined with an AEM (a), CEM (b) and BPM (c), respectively, while using  $\text{KHCO}_3$  as the initial catholyte and anolyte. Red dashed lines with arrows indicate the probable charge-carrying ionic species for membranes. Carbon balance paths for the AEM were adapted from ref. 29.

transported to the anolyte *via* the membrane, but cation species such as  $\text{K}^+$  served as the main charge carrier *via* the CEM. Thus, the concentration of  $\text{KHCO}_3$  in the anolyte was significantly reduced over time as  $\text{K}^+$  was constantly transported to the catholyte and the remaining  $\text{HCO}_3^-$  in the anolyte was consumed for  $\text{CO}_2$  evolution (Scheme 1b).

A bipolar membrane is composed of a cation exchange layer (CEL) and an anion exchange layer (AEL) as well as a catalyst layer that is sandwiched between the CEL and AEL. The catalyst layer in a BPM dissociates water (fed from both the catholyte and anolyte) into  $\text{H}^+$  and  $\text{OH}^-$ , which is subsequently transported to the catholyte and anolyte *via* the CEL and AEL, respectively (Scheme 1c).<sup>46</sup> With the use of a BPM (Fig. 3c), the flow rate of  $\text{CO}_2$  released from the anolyte rapidly decreased from  $1.4 \text{ ml min}^{-1}$  to  $0.5 \text{ ml min}^{-1}$  in the first 4 h, corresponding to a decline in the  $\text{CO}_2/\text{O}_2$  ratio from  $\sim 1$  to  $\sim 0.3$ . This observation may be linked to the fact that an alkaline boundary

layer near the AEL of the BPM created *via* the constant supply of  $\text{OH}^-$  from the BPM was unfavorable for releasing  $\text{CO}_2$  (the distance between the anode and the membrane was  $\sim 3 \text{ mm}$ ). In addition, the almost constant conductivity in both catholyte and anolyte over the 10 h electrolysis (Fig. S8c†) may imply that neither anionic species ( $\text{CO}_3^{2-}$  or  $\text{HCO}_3^-$ ) nor cationic species ( $\text{K}^+$ ) had any apparent crossover. This result reveals that the additional anion species ( $\text{CO}_3^{2-}$  or  $\text{HCO}_3^-$ ) generated by  $\text{CO}_2$  capture could not be accumulated in the catholyte during  $\text{CO}_2$  reduction electrolysis due to the charge balance issue (the total anion charge must equal the total cation charge). Thus, the additional  $\text{CO}_3^{2-}$  or  $\text{HCO}_3^-$  should be emitted from the catholyte as gaseous  $\text{CO}_2$ . As expected, gas bubbles released from the catholyte were observed when a BPM was used (no gas evolution was observed in the catholyte using an AEM or CEM), and this gas evolution immediately disappeared after stopping the electrolysis.



**Fig. 3** Comparison of flow of  $\text{CO}_2$  and  $\text{O}_2$  released from the anolyte (left axis), and corresponding ratio of  $\text{CO}_2$  to  $\text{O}_2$  (right axis) when using an AEM (a), CEM (b) and BPM (c) over the course of  $\text{CO}_2$  reduction electrolysis at  $200 \text{ mA cm}^{-2}$ . Variation in related electrolyte pH during  $\text{CO}_2$  reduction electrolysis for an AEM (d), CEM (e) and BPM (f), respectively. In all the experiments, 1 M  $\text{KHCO}_3$  was used as the initial catholyte (50 ml) and anolyte (50 ml). (a) and (d) for AEM were adapted based on ref. 29.

To verify the  $\text{CO}_2$  degassing in the catholyte, the gases released from the catholyte during the  $\text{CO}_2$  reduction electrolysis were analyzed using a setup shown in Fig. 4a. Fig. 4b shows  $\text{CO}_2$  degassing from the catholyte when using a BPM, owing to the neutralization reaction of  $\text{CO}_3^{2-}$  or  $\text{HCO}_3^-$  with  $\text{H}^+$  near the CEL of the BPM (Scheme 1c), which is in line with previous BPM work.<sup>37</sup> In addition, the related flow rate of  $\text{CO}_2$  released from the catholyte slightly decreased from  $\sim 3.5 \text{ ml min}^{-1}$  to  $\sim 2.6 \text{ ml min}^{-1}$ , and was maintained at  $\sim 2.6 \text{ ml min}^{-1}$  over the electrolysis experiment (Fig. 4b). This observation can be attributed to the fact that the carbon source (anion species) for  $\text{CO}_2$  evolution abruptly transformed from a mixture of  $\text{HCO}_3^-$  and  $\text{CO}_3^{2-}$  to almost pure  $\text{CO}_3^{2-}$ . In addition, a fraction of  $\text{CO}_2$  released from the catholyte chamber can transport to the cathode surface to be reused for both  $\text{CO}_2$  reduction<sup>37</sup> and the buffering reaction with  $\text{OH}^-$  at the cathode/electrolyte interface. This back-diffusion effect leads to a slightly lower  $\text{CO}_2$  flow ( $\sim 2.6 \text{ ml min}^{-1}$ ) compared to the theoretical value ( $3.0 \text{ ml min}^{-1}$ ). Furthermore, with nearly identical catalytic selectivity (Fig. 2c) and the same  $\text{OH}^-$  generation rate on the cathode (due to the same current density) among all the different membranes, the utilization of a fraction of  $\text{CO}_2$  released from a catholyte with a BPM results in a slightly lower  $\text{CO}_2$  consumption rate in the gas chamber. This result is in line with the slightly higher gas outlet flow rate for the BPM in comparison with those of the AEM and CEM (Fig. 1c).

While each type of ion-selective membrane had a different flow rate of  $\text{CO}_2$  released from the anolyte,  $\text{O}_2$  was detected with a constant flow rate of  $\sim 1.5 \text{ ml min}^{-1}$  during the electrolysis irrespective of membrane type (Fig. 3a–c). This finding is consistent with the theoretical value of the  $\text{O}_2$  flow rate ( $1.5 \text{ ml min}^{-1}$  shown in Table S2†) at  $200 \text{ mA cm}^{-2}$  for a geometric active area of  $2 \text{ cm}^2$ .

To further understand the transformation of anionic species in the electrolyte, the pH of the electrolyte was also monitored over the course of the electrolysis for all the membranes. Fig. 3e shows that for a CEM the catholyte pH was enhanced from 8.3 to nearly 9.8 after  $\sim 3 \text{ h}$ . The catholyte pH with the AEM increased to 10.2 after  $\sim 3 \text{ h}$  under identical conditions. Thus, the similar increasing trend in catholyte pH between the AEM and CEM over  $3 \text{ h}$

indicates that the captured  $\text{CO}_2$  at the cathode/electrolyte interface (*via* reaction with  $\text{OH}^-$ ) mainly formed  $\text{CO}_3^{2-}$  using the CEM,<sup>29</sup> leading to  $\text{CO}_3^{2-}$  acting as the dominant anion species in the catholyte after  $3 \text{ h}$ . The catholyte pH with the BPM was maintained below 9 over the entire electrolysis experiment (Fig. 3f) due to the fact that a constant supply rate of  $\text{H}^+$  from water dissociation in the BPM enables carbonate and bicarbonate concentrations in the catholyte to reach a steady state. In addition, this  $\text{pH} < 9$  also indicates that most of the existing anion species in the catholyte was bicarbonate over the entire electrolysis (Table S4†). However, the observed  $\text{CO}_2$  flow rate ( $2.6 \text{ ml min}^{-1}$ ) from the catholyte (after reaching a steady state) also reveals that  $\text{CO}_2$  was captured and converted to  $\text{CO}_3^{2-}$  at the cathode/electrolyte interface, and then combined with the aforementioned  $\text{H}^+$  at the BPM/catholyte interface to release  $\text{CO}_2$ . In addition, it should be noted that the theoretical calculations have shown that the pH near the cathode is  $\sim 13$  in  $1 \text{ M KHCO}_3$  at  $200 \text{ mA cm}^{-2}$ ,<sup>18</sup> which means that the reaction of  $\text{CO}_2$  with  $\text{OH}^-$  at the cathode/electrolyte interface forms  $\text{CO}_3^{2-}$  instead of  $\text{HCO}_3^-$  (eqn (S8) and (S9)†). Thus, all these results reveal that the  $\text{CO}_2$  captured by the electrolyte near the cathode formed  $\text{CO}_3^{2-}$  irrespective of membrane type.

We found that the anolyte quickly reached a near neutral pH for both the AEM and the CEM during the electrolysis (Fig. 3d and e), which allows for  $\text{CO}_2$  degassing in the anolyte. Specifically, the anolyte pH with the AEM was maintained at  $\sim 7.9$  after  $20 \text{ min}$  (Fig. 3d), owing to the fact that the constant  $\text{H}^+$  generation rate near the anode and continuous carbonate supply derived from the catholyte created a steady state for all the anion species in the anolyte *via* the neutralization reactions (Scheme 1a). In contrast, with the CEM, the anolyte pH rapidly decreased from 8.3 to 6.7 over  $3 \text{ h}$  (Fig. 3e). This finding is due to the fact that the  $\text{CO}_2$  degassing with the continuous consumption of  $\text{KHCO}_3$  in the anolyte created a  $\text{CO}_2$ -saturated  $\text{KHCO}_3$  anolyte and its concentration gradually reduced over time (pH of  $\text{CO}_2$ -saturated  $0.1 \text{ M KHCO}_3$  is  $\sim 6.8$ ). Interestingly, a slow increase in the anolyte pH from 8.3 to 9.6 was observed over  $10 \text{ h}$  electrolysis when using the BPM, as shown in Fig. 3f. This observation may be linked to a slow variation in the anionic species concentrations (here, an increase in the  $\text{CO}_3^{2-}/\text{HCO}_3^-$  ratio was likely created) in the anolyte during the electrolysis. This slow alteration is ascribed to the fact that the anolyte species did not completely reach a steady-state within  $10 \text{ h}$  electrolysis *via* the two major reactions, (i) the reaction of  $\text{CO}_2$  with  $\text{OH}^-$  at the BPM/anolyte interface forming  $\text{CO}_3^{2-}/\text{HCO}_3^-$ , and (ii) simultaneously,  $\text{CO}_3^{2-}/\text{HCO}_3^-$  converting into  $\text{CO}_2$  near the anode (Scheme 1c).

### Carbon balance *via* different types of membranes and implications

For high-rate  $\text{CO}_2$  reduction in flow electrolyzers, the carbon source for  $\text{CO}_2$  fed from the inlet of the reactor must be balanced with that of all  $\text{CO}_2$  reduction products,  $\text{CO}_2$  captured by electrolyte (carbonate formation) and residual  $\text{CO}_2$  out of the reactor (*i.e.* unreacted  $\text{CO}_2$ ). As noted in Fig. 5a, (i) the flow rate of residual unreacted  $\text{CO}_2$  out of the reactor, (ii) the flow rate of  $\text{CO}_2$  consumed for carbonate formation *via* the reaction with

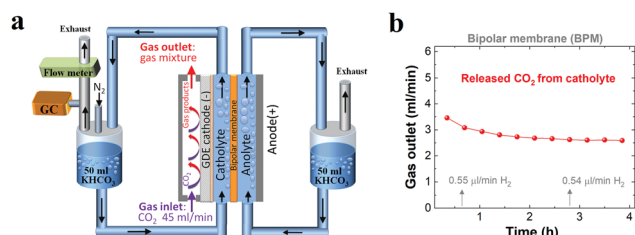


Fig. 4 (a) Schematic illustration of the flow cell setup for detecting gases released from the catholyte over the course of  $\text{CO}_2$  reduction when using a BPM ( $\text{N}_2$  with a constant flow rate was used as a carrier gas). (b) Flow rate of  $\text{CO}_2$  released from the catholyte when using a BPM for  $\text{CO}_2$  reduction at  $200 \text{ mA cm}^{-2}$  with a negligible amount of  $\text{H}_2$ .  $1 \text{ M KHCO}_3$  was used as the initial catholyte ( $50 \text{ ml}$ ) and anolyte ( $50 \text{ ml}$ ).



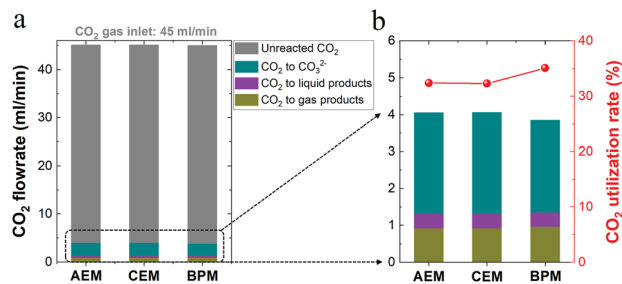


Fig. 5 (a) Carbon balance for high-rate CO<sub>2</sub> reduction in 1 M KHCO<sub>3</sub> using different membranes. The unreacted (*i.e.* residual) CO<sub>2</sub> flow rate as well as the total consumed CO<sub>2</sub> flow rate for carbonate formation and CO<sub>2</sub> reduction to all liquid and gas products were considered. (b) Ratio of CO<sub>2</sub> converted into products to total CO<sub>2</sub> consumption (right axis).

OH<sup>-</sup> (*i.e.* captured CO<sub>2</sub> throughout the electrolyte) and (iii) the flow rate of consumed CO<sub>2</sub> that was converted into all the gaseous and liquid products add up to a total CO<sub>2</sub> flow rate of ~45 ml min<sup>-1</sup> for each type of ion-selective membrane. Thus, the carbon element during the electrolysis is balanced with that of the CO<sub>2</sub> inlet flow rate (45 ml min<sup>-1</sup>) in this work. In addition, Fig. 5b shows the nearly identical CO<sub>2</sub> consumption rate for the formation of gaseous and liquid products using different ion-selective membranes, which is in line with the roughly same catalytic selectivity shown in Fig. 2c.

It should be noted that there should be nearly the same carbonate formation rate (*via* CO<sub>2</sub> reaction with OH<sup>-</sup>) near the cathode among all the different membranes due to the identical OH<sup>-</sup> generation rate *via* cathodic reactions at identical current densities. While membrane types should have a minimal effect on the total carbonate formation rate near the cathode, the BPM had a slightly lower consumption rate of CO<sub>2</sub> from the gas chamber for carbonate formation compared to those of the AEM and CEM, as shown in Fig. 5b. This finding correlates with the discrepancy in carbon balance paths among the three different types of membranes. In other words, while the unavoidable CO<sub>2</sub> capture near the cathode forms carbonate in the catholyte, the end result of where the carbonate goes is different in each type of membrane. For the CEM, the captured CO<sub>2</sub> was accumulated in the form of carbonate in the catholyte without emission. In contrast, when the AEM was used, the captured CO<sub>2</sub> in the form of carbonate crossed over to the anolyte and was emitted as gaseous CO<sub>2</sub> with the O<sub>2</sub> stream in the anolyte. Notably, with the BPM, the captured CO<sub>2</sub> could be released from the catholyte as gaseous CO<sub>2</sub>. Thus, a fraction of the generated CO<sub>2</sub> in the catholyte may be involved in the reaction with OH<sup>-</sup> for carbonate formation, which corresponds to a relatively low consumption rate of CO<sub>2</sub> in the gas chamber for carbonate formation (~65% of the total CO<sub>2</sub> consumption), as shown in Fig. 5b. In addition, the reuse of a fraction of the released CO<sub>2</sub> in the catholyte, derived from the captured CO<sub>2</sub> in the form of carbonate, also results in a slightly higher CO<sub>2</sub> utilization rate of the BPM (ratio of CO<sub>2</sub> converted into products *versus* total CO<sub>2</sub> consumption) in Fig. 5b.

From an economic and environmental perspective, the released CO<sub>2</sub> from the electrolyte in flow electrolyzers would

need to be captured and recycled. When the AEM is used, the released CO<sub>2</sub> in the anolyte can only be recycled for CO<sub>2</sub> reduction after removing O<sub>2</sub> in the gas mixture (mole ratio of CO<sub>2</sub>/O<sub>2</sub> is 2 : 1). Interestingly, the BPM could degas CO<sub>2</sub> from the catholyte, which can be directly fed into the gas compartment for CO<sub>2</sub> conversion due to its high purity (~100% CO<sub>2</sub> by mole). Thus, compared to the necessary CO<sub>2</sub> and O<sub>2</sub> separation process for CO<sub>2</sub> recycling with the AEM, the BPM has the potential to reduce the total cost of the carbon source. However, it should be noted that using a BPM for high-rate CO<sub>2</sub> reduction (current densities > 100 mA cm<sup>-2</sup>) currently requires an additional potential (>~1.5 V) for membranes that may reduce the energy efficiency of CO<sub>2</sub> conversion reactors.<sup>47</sup> In this work, an additional potential of ~2 V was observed when using the BPM at 200 mA cm<sup>-2</sup> (Fig. S9†). Thereby, how to balance the energy efficiency along with the easy recyclability of the produced CO<sub>2</sub> in the catholyte (from inevitably captured CO<sub>2</sub>) with the use of BPMs will need a full techno-economic analysis in the future.

## Conclusions

In conclusion, our results show that the role of ion-selective membranes is minimal in affecting the catalytic selectivity of high-rate CO<sub>2</sub> reduction, owing to the nearly same local reaction environment created near the catalysts through having a catholyte layer. By rigorously analyzing gases released from electrolytes as well as monitoring electrolyte pH, we found that most of the consumed CO<sub>2</sub> source (≥~65%) was captured *via* reaction with OH<sup>-</sup> near the cathode to form CO<sub>3</sub><sup>2-</sup>, which is almost independent of membrane type.

Importantly, each type of ion-selective membrane produces a unique carbon balance path for the captured CO<sub>2</sub> source. Specifically, the captured CO<sub>2</sub> in the form of CO<sub>3</sub><sup>2-</sup> could cross an AEM from the catholyte to the anolyte and then be emitted as gaseous CO<sub>2</sub> mixed with the O<sub>2</sub> stream. In contrast, the captured CO<sub>2</sub> could not be transported to the anolyte when using a CEM or BPM. With a CEM, captured CO<sub>2</sub> in the form of carbonate continuously accumulated in the catholyte, since there was no concomitant H<sup>+</sup> supply for CO<sub>2</sub> evolution (mainly K<sup>+</sup> crossed the membrane). With the bipolar membrane, the captured CO<sub>2</sub> was released from the catholyte as gaseous CO<sub>2</sub>, owing to the reaction of carbonate with H<sup>+</sup> transported from its cation exchange layer. In addition, while for an AEM CO<sub>2</sub> was emitted together with O<sub>2</sub>, for a BPM the pure CO<sub>2</sub> was released, which can be directly recycled back to the gas compartment for CO<sub>2</sub> conversion, correspondingly decreasing the cost of the CO<sub>2</sub> source. This study shows that while the catalytic selectivity is independent of the type of ion-selective membrane, membrane type plays an important role in the corresponding carbon balance path for high-rate CO<sub>2</sub> reduction. Thus, future work should focus on membrane exploration for achieving the practical utilization of high-rate CO<sub>2</sub> reduction.

## Author contributions

M. M. and B. S. developed the conceptual idea, designed the experiments and wrote the original manuscript. S. K. carried out





a part of the electrolyte pH and conductivity measurements. All authors contributed to discussing the results and editing the manuscript.

## Conflicts of interest

There are no conflicts to declare.

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