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Synergistic effects of zeolite imidazole framework@graphene oxide composites in humidified mixed matrix membranes on CO₂ separation

Dandan Huang,^a Qingping Xin,^{ID} *^a Yazhou Ni,^a Yingqian Shuai,^a Shaofei Wang,^{ID} ^a Yifan Li,^{ID} ^b Hui Ye,^{ID} ^a Ligang Lin,^a Xiaoli Ding^a and Yuzhong Zhang^{*a}

In this study, composite nanosheets (ZIF-8@GO) were prepared *via* an *in situ* growth method and then incorporated into a polyimide (PI) matrix to fabricate mixed matrix membranes (MMMs) for CO₂ separation. The as-prepared MMMs were characterized by Fourier transform infrared (FT-IR) spectroscopy, scanning electron microscopy (SEM), X-ray diffraction (XRD), differential scanning calorimetry (DSC), thermogravimetric analyses (TGA) and water uptake measurements. Water uptake measurements establish the relationship between the gas permeability and water uptake of membranes and an increase in the water uptake contributes to the CO₂ permeability owing to an increase in the CO₂ transport channels. The MMMs exhibit excellent CO₂ permeability in when compared with an unfilled PI membrane in a humidified state. The ZIF-8@GO filled membranes can separate CO₂ efficiently due to the ZIF-8@GO nanocomposite materials combining the favorable attributes of GO and ZIF-8. First, the high-aspect ratio of the GO nanosheets enhances the diffusivity selectivity. Second, ZIF-8 with a high surface area and microporous structure is beneficial to the improvement of the CO₂ permeability. Third, ZIF-8@GO possesses synergistic effects for efficient CO₂ separation. The MMM with 20 wt% ZIF-8@GO exhibits the optimum gas separation performance with a CO₂ permeability of 238 barrer, CO₂/N₂ selectivity of 65, thus surpassing the 2008 Robeson upper bound line.

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1 Introduction

CO₂, as the main greenhouse gas, has received extensive attention in order to reduce its emission all over the world. Membrane separation, as an attractive alternative of conventional techniques, has developed rapidly due to its high efficiency, low cost, and energy saving and environment-friendly characteristics and has become one of the promising CO₂ separation technologies in the field of carbon capture technology.^{1–4} Polymer membrane materials have good processing performance; however, their gas separation performance suffers from trade-off properties. Inorganic membranes have excellent separation performance, but they are difficult to process. Mixed matrix membranes (MMMs) with organic and inorganic materials embedded into polymeric membranes overcome this trade-off limit and realize the simultaneous improvement of selectivity and permeability.^{5,6,7} Different from the pure polymer, the MMM has multiple functions, multi-level structure, multiple phases and multiple functions, which

provide a wealth of possibilities for the design and preparation of MMMs, thus becoming a hot spot in recent years. However, due to the differences in the physical and chemical characteristics of the polymer and inorganic filler, poor interface morphologies such as interface defects and interface cavities could be easily produced. Therefore, to create a good interface morphology between the polymer and filler is key to preparing high-performance MMMs. Such filler-materials include zeolites,⁸ carbon molecular sieves (CMS),⁹ metal-based oxides,^{10–13} silica,^{14,15} carbon nanotubes,^{16,17} graphene oxide,^{18,19} metal organic frameworks,^{20,21} and covalent organic frameworks.^{22,23}

Due to their high surface area and porous properties, metal organic frameworks (MOFs) are widely used as membranes in gas separation processes.^{24,25} MOF membranes have been researched for their gas separation performances; these membranes often show high gas separation performances because of their rigid pores and uniformity. However, ultra-thin MOF membrane fabrication has a significant challenge that MOF membranes usually need to be supported because they do not have enough mechanical strength to support themselves. Moreover, their high cost and complex manufacturing and processing have limited their widespread industrial applications.

^aState Key Laboratory of Separation Membranes and Membrane Processes, School of Materials Science and Engineering, Tianjin Polytechnic University, Tianjin 300387, P. R. China. E-mail: xinqingping@tjpu.edu.cn; zhangyz2004cn@vip.163.com

^bSchool of Chemical Engineering and Energy, Zhengzhou University, Zhengzhou 450001, P. R. China



An alternative approach is to embed the porous MOF materials into a polymer matrix to fabricate MMMs. MMMs may combine the advantages of both the filler phase with uniform pores and the polymer phase with superior mechanical strength and easy fabrication.²⁶ The favorable properties of the two phases are endowed in the MMMs and overcome the defects of a single material, generating additional synergy. The functional filler plays a key role in the membrane structure because its pore size distribution determines the separation performance.²⁷ In other words, fillers with a well-defined pore size and shape increase the porosity of the MMMs and provide more gas permeation and diffusion channels. Vankelecom *et al.* fabricated MMMs by incorporating $\text{Cu}_3(\text{BTC})_2$ into the polymer matrix and found that the CO_2 permeability of the PI/30 wt% [$\text{Cu}_3(\text{BTC})_2$] membrane was 80% higher than that of the unfilled membrane.²⁸ Kaliaguine *et al.* fabricated CO_2/CH_4 gas separation MMMs and investigated the effect of modifying the MOF structure with $-\text{NH}_2$ functional groups in CO_2/CH_4 gas separation.²⁹ It was found that the MMMs loaded with MOF-199 increased both the CO_2 permeability and ideal selectivity by 49% and 16%, respectively, while the MMMs loaded with NH_2 -MOF-199 increased by 82% and 35% both in CO_2 permeability and ideal selectivity when compared with the unfilled membrane. MOF-5 containing MMMs were prepared by Musselman *et al.*³⁰ and the permeability of gases was enhanced by 120%, while the CO_2/CH_4 selectivity increased by 6% at 30% MOF-5 loading. Gascon *et al.* incorporated 1,4-benzenedicarboxylate (CuBDC) MOF nanosheets into Matrimid® 5218 polymer to fabricate a MOF-polymer thin membrane.²⁰ The ultrathin membrane shows outstanding CO_2 separation performance from CO_2/CH_4 gas mixtures. Liu *et al.*³¹ reported the permeability of H_2 and the H_2/CO_2 selectivity of 6 wt% $\text{Cu}_3(\text{BTC})_2$ MMM increased by 45% and a factor of 2.78 when compared with pure PI. Subsequently, Hu *et al.*³² compared the effect of three types of fillers (MOF-5, $\text{Cu}_3(\text{BTC})_2$, and MIL-53(Al)) on the gas separation performance and proved that the $\text{Cu}_3(\text{BTC})_2$ loaded membrane had the best separation performance.

Graphene oxide (GO) as a well-known two-dimensional material possesses a unique one-atom-thick structure.³³ These properties endowed GO to become a promising material for use in separation membranes. GO nanosheets can assemble a graphene laminate membrane and GO can be used as the filler embedded in a polymer matrix to obtain MMMs.^{34,35} GO-based membranes are predicted to be highly selective owing to their inherent 2D channels. The composites of MOF and GO, such as ZIF-8@GO³⁶ and MOF-505@GO,³⁷ have attracted great attention owing to their advantageous gas separation performances. The MOF@GO may develop new pores at the interface of the MOF and GO surfaces and the CO_2 separation will be enhanced due to the new porosity. Recently, MOF@GO materials used as fillers to prepare MMMs have been reported. Dong *et al.* fabricated MMMs by incorporating ZIF-8@GO into a Pebax® matrix and investigated their CO_2 separation performance.³⁸ The membrane showed the CO_2 permeability and CO_2/N_2 selectivity of MMMs was 249 barrer and 47.6, respectively at 6 wt% ZIF-8@GO loading. The MOF@GO loaded membranes have good

compatibility at the filler/polymer interface owing to the presence of GO.³⁷ Moreover, this type of membrane can combine the advantages of the two materials.

In this study, MOF@GO was prepared as a filler to fabricate MMMs to enhance the CO_2 separation performance. ZIF-8 was selected as a multifunctional filler because of its uniform pore and high thermal and chemical stability. GO was selected as the support for ZIF-8 due to its high surface area and abundant surface functional groups. Matrimid® 5218 was used as the polymer matrix due to its superior chemical and thermal properties. The ZIF-8@GO composite nanosheets were used as fillers embedded into the polymer matrix to fabricate a series of MMMs and the CO_2 separation performance of the MMMs was investigated. Moreover, the influence of the water uptake and pressure on the gas separation performance was studied. In addition, the microstructure and thermal properties of the MMMs were revealed.

2 Experimental

2.1 Materials

Polyimide (PI, Matrimid® 5218) was supplied by Huntsman Advanced Materials Americas Inc. $\text{Zn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ and 2-methylimidazole were purchased from Aladdin. Potassium permanganate (KMnO_4), sodium nitrate (NaNO_3), hydrochloric acid (HCl), and concentrated sulfuric acid (H_2SO_4 , 98 wt%) were obtained from Tianjin Jiangtian Ltd. (Tianjin, China). Methanol and hydrogen peroxide aqueous solution (H_2O_2 , 30 wt%) and *N,N*-dimethyl acetamide (DMAc) were obtained from Kemiou Chemical Reagent Co., Ltd. (Tianjin, China). Deionized water was used throughout the experiments.

2.2 Preparation of ZIF@GO

ZIF-8 particles were synthesized according to a literature procedure.³⁴ $\text{Zn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ (98.0 wt%, 1.464 g) and 2-methylimidazole (Hmim, 99.0 wt%, 3.244 g) were dissolved in 48 mL and 80 mL of methanol under stirring, respectively, and then mixed. The mixed solution was stirred for 3 h at 30 °C. The products were collected by centrifugation and washed three times with methanol. Finally, the as-obtained ZIF-8 was dried under vacuum.

GO was prepared using the modified Hummers method.⁴⁰ Natural graphite powder (2.0 g) and NaNO_3 (1.0 g) were dissolved in concentrated H_2SO_4 (150 mL) under stirring in an ice bath. Then, KMnO_4 (7.0 g) was added slowly to the mixture with stirring over 1 h, while the temperature was maintained at ~ 5 °C. The mixture was stirred at 55 °C for 4 h. Then, 150 mL of ice-cold deionized water was added into the mixture and then, the mixture was heated to 97 °C and kept at this temperature for 30 min. Finally, 50 mL of deionized water and 30 mL of H_2O_2 were added to the mixture, in sequence, with stirring. The mixture was centrifuged at 6000 rpm for 15 min and washed three times with 300 mL of HCl aqueous solution. Then, the mixture was washed with water until the filtrate was neutral. The product was dispersed in a certain amount of water. An aqueous suspension of GO at a concentration of 5 mg mL^{-1} was



obtained. Then, the GO suspension was further diluted to 1 mg mL⁻¹ using methanol and sonicated for 8 h prior to use.

The ZIF-8@GO nanosheets were prepared *via* the same process used for the preparation of ZIF-8 along with the addition of 8 mL of the as-prepared GO suspension. To prepare the ZIF-8@GO sample, Zn(NO₃)₂·6H₂O (0.366 g) and 2-methylimidazole (0.811 g) were dissolved in 12 mL and 20 mL of methanol, respectively, and then mixed to obtain a mixed solution under stirring. Immediately, 8 mL of the as-prepared GO suspension was added to the above mixed solution and stirred for 3 h. Then, the mixture was washed and centrifuged at least three times and the products were dried in a vacuum oven.

2.3 Preparation of MMMs

The PI-ZIF-8@GO loaded MMMs and unfilled PI membrane were fabricated using a solution casting method. The PI powder (0.6 g) was dissolved in DMAc (6 mL) under stirring for 1 h and a desired amount of ZIF-8 or ZIF-8@GO was homogeneously dispersed into another vial containing 6 mL of DMAc *via* ultrasonication for 2 h. Then, the suspension was mixed with the PI solution and stirred for 12 h. The mixed suspension was cast onto a glass slide, dried at 50 °C for 12 h and then at 80 °C for 12 h. The MMMs were designated as PI-ZIF-8@GO-*x*, where *x* is the weight percentage of the fillers relative to the PI matrix.

2.4 Characterization of filler and membranes

Size and morphology of the GO and ZIF-8@GO were observed by transmission electron microscopy (TEM Hitachi H7650). The FT-IR spectra of GO, ZIF-8, ZIF-8@GO and the MMMs were recorded on a BRUKER Vertex 70 FT-IR spectrometer over the range of 4000–400 cm⁻¹. The morphology of ZIF-8 and the cross-sectional structure of the membranes were obtained by scanning electron microscopy (SEM, S-4800). The TGA of the membranes were conducted using a STA449F3 apparatus. The measurements were tested from 40 °C to 800 °C under N₂ atmosphere. The glass transition temperature of the membranes was studied using a DSC200F3 apparatus over the temperature range of 200–400 °C under N₂ atmosphere. The crystalline structure of the fillers and membranes were recorded on a D8 DISCOVER X-ray diffractometer (XRD) over the range of 5–40°.

The water uptake and water state of the membranes have an important influence on the gas transport mechanism and were studied using a literature procedure.³⁹ The membranes were weighed (*m*₁, mg) after the gas permeation test under humidified conditions. Then, the membranes were dried at 100 °C for 6 h to remove any free water and weighed again (*m*₂, mg). Finally, the membranes were dried at 150 °C for 6 h to remove any bound water and their absolute dry weight (*m*₀, mg) was measured. The content of total water (*W*_t, %), free water (*W*_f, %) and bound water (*W*_b, %) were acquired using eqn (1)–(3), respectively.

$$W_t = (m_1 - m_0)/m_0 \times 100\% \quad (1)$$

$$W_f = (m_1 - m_2)/m_0 \times 100\% \quad (2)$$

$$W_b = (m_2 - m_0)/m_0 \times 100\% \quad (3)$$

2.5 Gas permeation experiment

A single gas (CO₂, N₂) permeation test of the humidified membranes was conducted using the constant pressure/variable volume method at 35 °C. Before the gas separation test, all the membranes were soaked in water for over two weeks to absorb adequate amount of water. In the measurement process, both the feed gas and sweep gas were saturated with water vapor by a bubbling method at 35 °C and then passing through an empty bottle at room temperature to remove the condensed water. N₂ was used as the sweep gas for CO₂, otherwise CO₂ was used as the sweep gas for N₂. The gas permeability (*P*_{*i*}, barrer, 1 barrer = 10⁻¹⁰ cm³ (STP) cm (cm² s⁻¹ cmHg)) was obtained from the average value of more than three experiments using the following equation:

$$P_i = \frac{Q_i l}{\Delta P_i A} \quad (4)$$

Where *Q*_{*i*}, *l*, Δ*P*_{*i*} and *A* are the gas volumetric flow rate of the gas (cm³ s⁻¹) (STP), membrane thickness (cm), transmembrane pressure difference (cmHg) and effective membrane area (cm²), respectively. The pure gas ideal selectivity (α_{*ij*}) was obtained using eqn (5):

$$\alpha_{ij} = \frac{P_i}{P_j} \quad (5)$$

The permeability of the dry membrane is given by eqn (6):

$$P_i = D_i \times S_i \quad (6)$$

where *D*_{*i*} and *S*_{*i*} are the diffusion (cm² s⁻¹) and solubility coefficients (cm³ (STP) cm⁻³ cmHg⁻¹) of gas '*i*' in the polymer membrane, respectively. The diffusion coefficients *D*_{*i*} were measured by the time lag method^{14,41,42} using eqn (7):

$$D_i = \frac{l^2}{6\theta} \quad (7)$$

Where θ is the diffusivity time lag and *l* is the thickness of the membrane. The solubility coefficient *S*_{*i*} was obtained using eqn (6).

The membrane samples were dried under a vacuum for 24 h prior to testing. In this study, N₂/CO₂ was used as the feed gas. The pressure and temperature of the high-pressure side were maintained at 1 bar and 30 °C, respectively. For each membrane, the gas permeation was tested three times to ensure that the error range of the gas permeability was within 5% and that for the gas selectivity was within 8%. The errors of the gas diffusivity coefficient and solubility coefficient of dry membranes were all less than 10%.

3 Results and discussion

3.1 Characterization of nanofillers

The size and morphology of GO, ZIF-8, and ZIF-8@GO were observed using SEM and TEM. The ZIF-8 nanoparticles are a rhombic dodecahedron shape with sizes in the range of 50–60 nm as shown by SEM (Fig. 1a). GO is fully exfoliated into



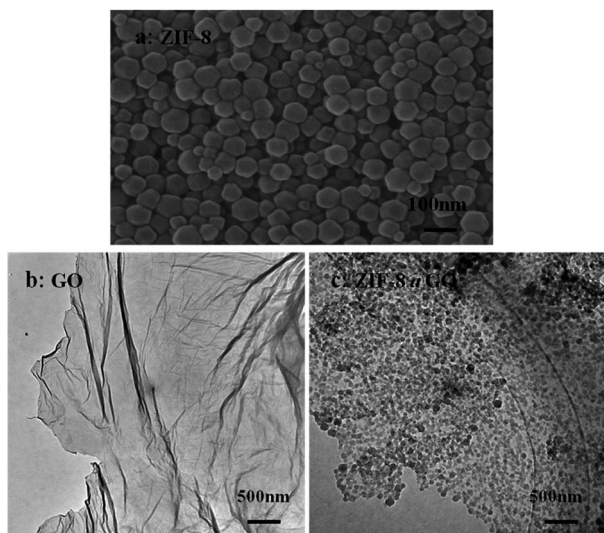


Fig. 1 SEM image of (a) ZIF-8 and TEM image of (b) GO and (c) ZIF-8@GO.

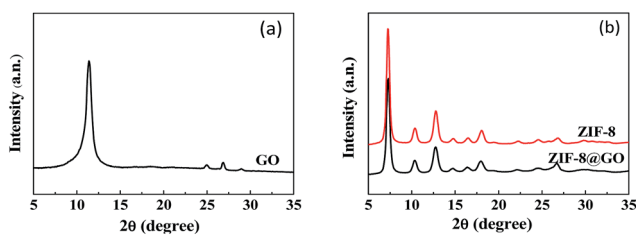


Fig. 2 XRD patterns recorded for (a) GO and (b) ZIF-8, ZIF-8@GO.

ultrathin nanosheets as shown by TEM (Fig. 1b). The size and morphology of ZIF-8@GO are similar to pristine GO; the difference is that ZIF-8 was grown *in situ* on the surface of GO. The TEM image (Fig. 1c) demonstrates a homogeneous distribution of ZIF-8 on GO. In addition, the ZIF-8 does not show any visible aggregation.

The XRD patterns of GO, ZIF-8 and ZIF-8@GO are shown in Fig. 2. The XRD pattern of the GO nanosheets has a strong peak at $2\theta = 11.6^\circ$. The distance between the corresponding chain (d -spacing) is 0.765 nm, indicating that GO was successfully exfoliated into single layer ultrathin nanosheets.⁴³ However, the strong diffraction peak of GO in ZIF-8@GO disappears; the reason is that the content of GO in ZIF-8@GO was too low to be examined. The pattern of ZIF-8@GO is similar to pristine ZIF-8 with another diffraction peak exhibited at about 8° .³⁶

Fig. 3(a) shows the N_2 adsorption–desorption isotherms at 77 K observed for ZIF-8, ZIF-8@GO and GO. The specific surface area decreases from $1964 \text{ m}^2 \text{ g}^{-1}$ for ZIF-8 to $1413 \text{ m}^2 \text{ g}^{-1}$ for ZIF-8@GO. This indicates that GO occupies a certain amount of the pores in ZIF-8. The pore size distribution of ZIF-8, ZIF-8@GO and GO is shown in Fig. 3(b). The pore size distribution of ZIF-8@GO is similar to ZIF-8 at 2–4 nm.

When compared with the GO nanosheets, the FT-IR spectra of ZIF-8@GO does not have a peak at 1724 cm^{-1} , corresponding

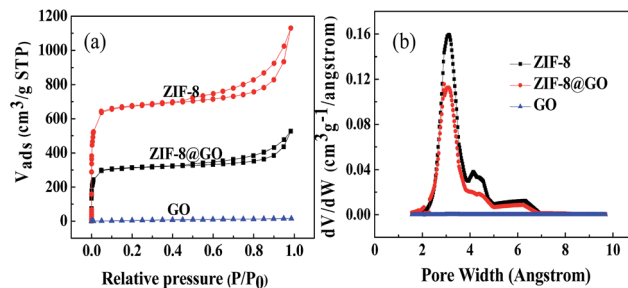


Fig. 3 (a) Nitrogen adsorption–desorption isotherms and (b) pore size distribution curves observed for ZIF-8, ZIF-8@GO and GO.

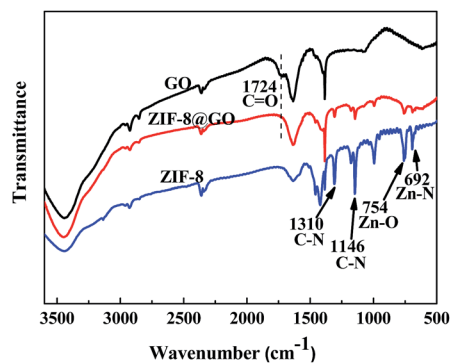


Fig. 4 FT-IR spectra recorded for GO, ZIF-8 and ZIF-8@GO.

to $\text{C}=\text{O}$, as shown in Fig. 4.⁴⁴ Other bands at 1146 cm^{-1} and 1310 cm^{-1} , corresponding to the $\text{C}-\text{N}$ bonds in the imidazole group, 754 cm^{-1} , corresponding to the $\text{Zn}-\text{O}$ bonds, and 692 cm^{-1} , corresponding to $\text{Zn}-\text{N}$ bonds, were ascribed to the ZIF-8 structure.^{38,45}

TGA was performed to analyze the thermal stability of the fillers and the ratio of GO and ZIF-8 in ZIF-8@GO was estimated (Fig. 5). The weight loss of ZIF-8@GO at $150\text{--}200^\circ\text{C}$ is attributed to the thermal decomposition of GO and the weight loss starting from 200°C is attributed to the thermal decomposition of ZIF-8. Based on the obtained data, the content of GO and ZIF-8 in ZIF-8@GO was about 5% and 95%, respectively.

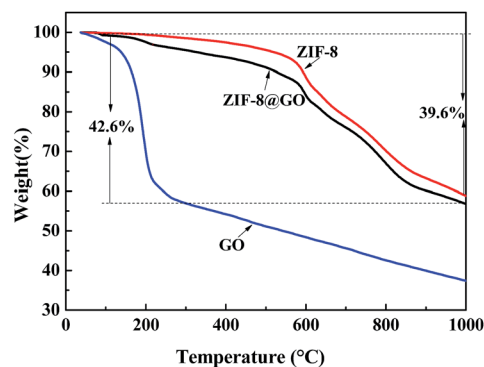


Fig. 5 TGA curves observed for GO, ZIF-8 and ZIF-8@GO.



3.2 Characterization of membranes

The cross-sectional morphologies of the membranes were characterized by FESEM as shown in Fig. 6. The membrane structures were strongly influenced by the incorporation of the fillers. When compared to the unfilled PI membrane (Fig. 6a) with a smooth and dense morphology, the MMMs show a rougher cross-section. Fig. 6b–i reveals that at low ZIF-8@GO loadings, the fillers are dispersed homogeneously in the PI matrix, resulting in a relatively uniform cross-sectional structure. The cross-sectional image of PI-ZIF-8@GO-20 shows that ZIF-8@GO was well-dispersed in the PI matrix, implying the good compatibility between ZIF-8@GO and the PI matrix. As the

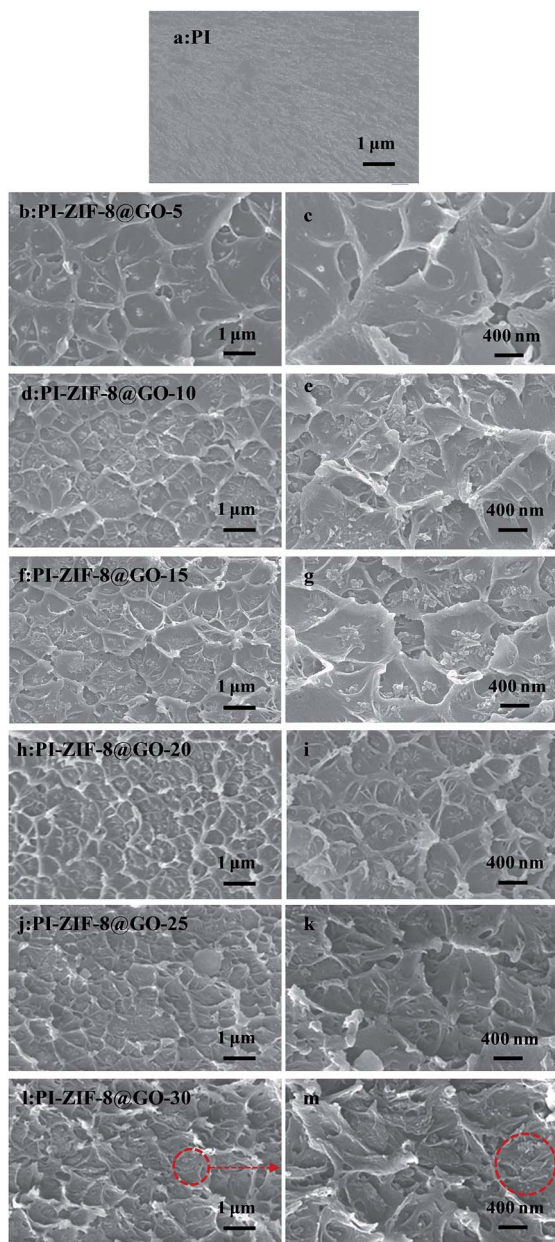


Fig. 6 Cross-section FESEM images of (a) unfilled PI, (b, c) PI-ZIF-8@GO-5, (d, e) PI-ZIF-8@GO-10, (f, g) PI-ZIF-8@GO-15, (h, i) PI-ZIF-8@GO-20, (j, k) PI-ZIF-8@GO-25 and (l, m) PI-ZIF-8@GO-30.

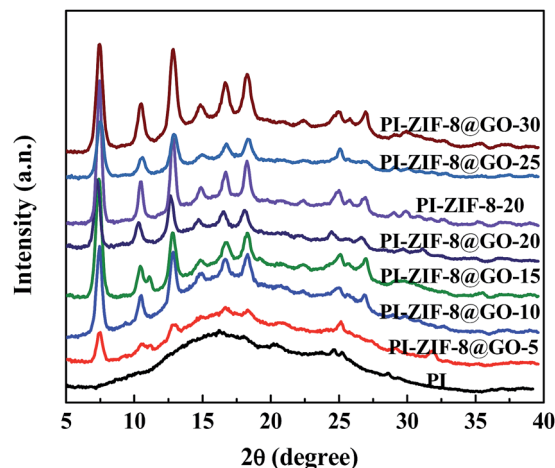


Fig. 7 XRD patterns recorded for the membranes.

ZIF-8@GO content increases, *e.g.*, PI-ZIF-8@GO-25 and PI-ZIF-8@GO-30 membranes (Fig. 6j–m), ZIF-8@GO tends to slightly aggregate in the membrane.

The XRD spectra of the unfilled PI and the MMMs with different filler content are presented in Fig. 7. The unfilled PI membrane shows broad and strong peaks at 10–30°, which result from the crystalline region of the polyamide segment.^{46,47} However, the MMMs have both the broad and characteristic peaks of the fillers, which imply that the crystallinity of the fillers was not affected by the PI matrix.

The FT-IR spectra of the unfilled PI membrane and ZIF-8@GO loaded MMMs are presented in Fig. 8. The characteristic peaks at 1781 cm^{-1} and 1720 cm^{-1} correspond to the C=O bond stretching vibrations of the imide groups and 1375 cm^{-1} was attributed to the C–N stretching vibrations of the imide group for the unfilled PI membrane.⁴⁸ The peak at 1298 cm^{-1} was attributed to the bending vibrations of the C–CO–C groups.⁴⁹ The FT-IR spectra observed for the MMMs are similar to the unfilled PI membrane with no significant change. However, upon the incorporation of ZIF-8 or ZIF-8@GO, the two new peaks at 1146 cm^{-1} and 1310 cm^{-1} were attributed to the C–N stretching vibrations in the imidazole groups, which proves that the ZIF-8 or ZIF-8@GO are well incorporated into the polymer matrix and retains the original chemical structure.

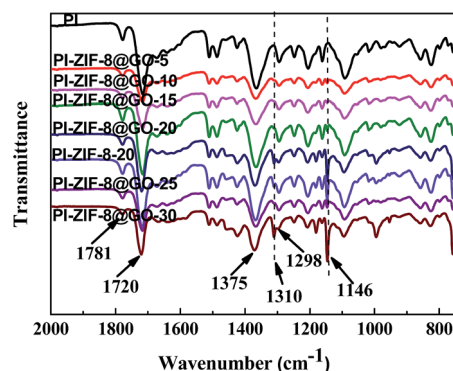


Fig. 8 FT-IR spectra recorded for the membranes.



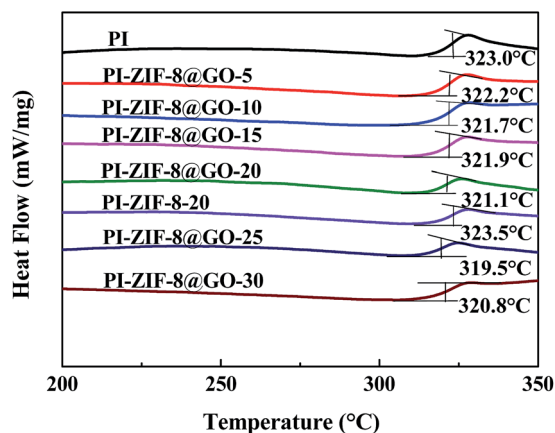


Fig. 9 DSC curves obtained for the membranes.

The glass transition temperature (T_g) of the membranes were detected using DSC. The unfilled PI membrane exhibits a T_g at 323.0 °C as shown in Fig. 9. The T_g of all the MMMs, except for the ZIF-8 filled membrane, shows a slight decrease when compared with the unfilled PI membrane. The T_g of the ZIF-8@GO filled membranes (from 323.0 to 320.8 °C) gradually decreases as the ZIF-8@GO content increases. The decline in T_g indicates that the incorporation of the fillers increases the chain mobility of PI. In general, the incorporation of GO leads to the rigidity of the polymer chain.¹⁹ In this study, the membranes do not show evident rigidity because the growth of ZIF-8 on the GO interferes with the interaction between GO and PI. Furthermore, the T_g of the PI-ZIF-8-20 filled membrane (323.5 °C) is higher than all the ZIF-8@GO filled membranes and unfilled PI membrane because the high surface area of the ZIF-8 nanoparticles increases the contact area between the polymer and fillers, thus increasing the interactions that inhibit the chain mobility of PI.

The thermal stability of the membranes was analyzed using TGA as shown in Fig. 10. The three typical membranes, which are unfilled PI, PI-ZIF-8@GO-20 and PI-ZIF-8-20 were tested. The TGA curves of the membranes have two main degradation

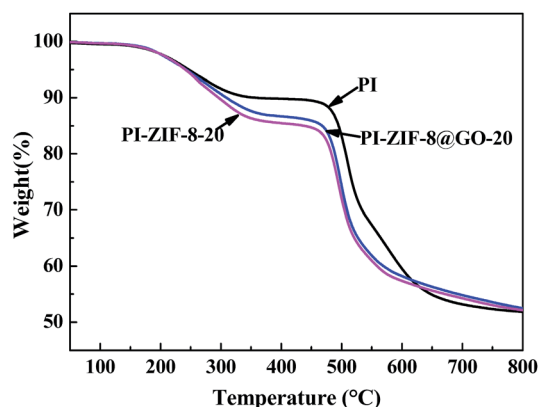


Fig. 10 TGA curves obtained for the unfilled PI, PI-ZIF-8@GO-20 and PI-ZIF-8-20 membranes.

processes: the first phase of weight loss at 240–350 °C resulted from the decomposition of the organic ligands in ZIF-8; the second stage of weight loss at ~450 °C is primarily ascribed to the PI chain decomposition. Before 625 °C, the thermal stability was as follows: PI > PI-ZIF-8@GO-20 > PI-ZIF-8-20. Above 625 °C, the thermal stability was in the order: PI-ZIF-8@GO-20 > PI-ZIF-8-20 > PI. Moreover, the decomposition rate of PI-ZIF-8@GO-20 is slightly slower than that of PI-ZIF-8-20 throughout the TGA analysis.

3.3 Water uptake and water state

The content of free water in the MMMs is higher than that of the unfilled PI membrane and exhibits a maximum value with 43.52% at a ZIF@GO loading of 30 wt% as shown in Table 1. Moreover, the content of bound water in the MMMs is higher than that of unfilled PI membrane, but reaches a maximum value when the ZIF@GO loading is 20 wt%.

3.4 Gas separation performance of the membranes

The pure gas permeability and ideal selectivity of the dry and humidified membranes were investigated (Table 2). To further investigate the gas transport mechanism, the diffusion coefficient (D) and the solubility coefficient (S) of CO₂ and N₂ for the dry membranes and their corresponding diffusion selectivity and solubility selectivity are determined and listed in Table 3.

Table 1 Water uptake and water state of unfilled Matrimid® 5218 membrane and MMMs

| Sample | Total water (W _t , %) | Free water (W _f , %) | Bound water (W _b , %) |
|----------------|----------------------------------|---------------------------------|----------------------------------|
| PI | 3.30 | 2.79 | 0.51 |
| PI-ZIF-8@GO-5 | 8.66 | 7.46 | 1.20 |
| PI-ZIF-8@GO-10 | 12.90 | 12.02 | 0.88 |
| PI-ZIF-8@GO-15 | 18.72 | 17.81 | 0.91 |
| PI-ZIF-8@GO-20 | 32.00 | 30.25 | 1.75 |
| PI-ZIF-8@GO-25 | 29.30 | 27.79 | 1.51 |
| PI-ZIF-8@GO-30 | 43.52 | 42.61 | 0.92 |
| PI-ZIF-8-20 | 21.35 | 18.94 | 2.41 |
| PI-GO-20 | 4.21 | 3.33 | 0.88 |

Table 2 Pure gas permeability and ideal CO₂/N₂ selectivity of the dry membranes and humidified membranes

| Sample | Dry membranes | | | Humidified membranes | | |
|----------------|---------------|-----------|---------------------|----------------------|-----------|---------------------|
| | P_{CO_2} | P_{N_2} | α_{CO_2/N_2} | P_{CO_2} | P_{N_2} | α_{CO_2/N_2} |
| PI | 6.62 | 0.20 | 33.10 | 52 | 1.44 | 36 |
| PI-ZIF-8@GO-5 | 9.28 | 0.28 | 33.14 | — | — | — |
| PI-ZIF-8@GO-10 | 7.32 | 0.18 | 40.67 | 84 | 1.82 | 46 |
| PI-ZIF-8@GO-15 | 14.50 | 0.31 | 46.77 | 124 | 2.51 | 49 |
| PI-ZIF-8@GO-20 | 11.14 | 0.21 | 53.05 | 238 | 3.65 | 65 |
| PI-ZIF-8@GO-25 | 14.32 | 0.29 | 49.40 | — | — | — |
| PI-ZIF-8@GO-30 | 21.80 | 0.64 | 34.06 | 259 | 6.59 | 39 |
| PI-ZIF-8-20 | 12.31 | 0.30 | 41.03 | 178 | 4.23 | 42 |
| PI-GO-20 | 8.23 | 0.23 | 35.78 | 134 | 3.70 | 36 |



Table 3 Gas diffusivity coefficient and solubility coefficient of the dry membranes loaded with GO, ZIF-8 and ZIF@GO, respectively (1 bar, 30 °C)

| Membrane | $D (\times 10^{-8} \text{ cm}^2 \text{ s}^{-1})$ | | $S (\times 10^{-2} \text{ cm}^3 (\text{STP}) / (\text{cm}^3 \text{ cmHg}))$ | | $D_{\text{CO}_2}/D_{\text{N}_2}$ | $S_{\text{CO}_2}/S_{\text{N}_2}$ |
|----------------|--|----------------|---|----------------|----------------------------------|----------------------------------|
| | CO ₂ | N ₂ | CO ₂ | N ₂ | | |
| PI | 2.75 | 1.46 | 2.41 | 0.14 | 1.88 | 17.57 |
| PI-ZIF-8@GO-5 | 3.18 | 1.69 | 2.92 | 0.17 | 1.88 | 17.61 |
| PI-ZIF-8@GO-10 | 2.93 | 1.51 | 2.50 | 0.12 | 1.94 | 20.96 |
| PI-ZIF-8@GO-15 | 4.07 | 2.08 | 3.56 | 0.15 | 1.96 | 23.90 |
| PI-ZIF-8@GO-20 | 3.51 | 1.67 | 3.17 | 0.13 | 2.10 | 25.24 |
| PI-ZIF-8@GO-25 | 4.02 | 2.03 | 3.56 | 0.14 | 1.98 | 23.94 |
| PI-ZIF-8@GO-30 | 5.41 | 2.96 | 4.03 | 0.22 | 1.83 | 18.64 |
| PI-ZIF-8-20 | 3.71 | 1.83 | 3.32 | 0.16 | 2.03 | 20.24 |
| PI-GO-20 | 3.01 | 1.57 | 2.73 | 0.15 | 1.92 | 18.66 |

As expected, the diffusion coefficient of gas increases for the MMMs when compared with the unfilled PI membrane (Table 3). The CO₂ diffusion coefficient increases from $2.75 \times 10^{-8} \text{ cm}^2 \text{ s}^{-1}$ for the unfilled PI membrane to $5.41 \times 10^{-8} \text{ cm}^2 \text{ s}^{-1}$ for the PI-ZIF-8@GO-20 membrane. This increase in the diffusion coefficient is primarily attributed to the synergistic effect of the modestly improved chain mobility, as shown by DSC results, and the increased transport pathways with sizes of 0.34 nm in ZIF-8. Similar to the diffusion coefficient, the MMMs show an enhanced CO₂ solubility coefficient when compared with the unfilled PI membrane. The MMMs contain ZIF-8, which shows CO₂ affinity, and provide ether-oxygen groups from GO for the CO₂ molecules. Moreover, the PI-ZIF-8@GO-20 membrane shows a higher diffusion selectivity and solubility selectivity than the other MMMs for CO₂/N₂ gas. The membrane loaded with ZIF-8@GO at a loading of 20 wt% shows an increased CO₂/N₂ diffusion selectivity and solubility selectivity by 12% and 44%, respectively, when compared with the unfilled PI membrane.

Both the CO₂ permeability and the selectivity of all the humidified membranes were significantly improved when compared with the CO₂ permeability and selectivity of all the dry membranes (Table 2). For the unfilled PI membrane in its dry state, the CO₂ permeability was 6.6 barrer, which increased to 52 barrer in its humidified state, thus increasing by 685%. Water plays an important role in gas transport for the humidified PI membrane. Water may swell and plasticize the PI polymer matrix, strengthening the intersegmental mobility of the polymer chains and enhance the gas diffusivity. Moreover, water may produce additional transport channels for gas transport. Consequently, the positive influence of water leads to the enhanced gas permeability. For the humidified MMMs, the CO₂ permeability increases upon increasing the ZIF-8@GO content. When compared with the unfilled PI membrane, the CO₂ permeability and CO₂/N₂ selectivity of the PI-ZIF-8@GO-20 membrane increase by 358% and 81%, respectively. The introduction of ZIF-8@GO improves the water content in the MMMs, which increases the dissolved CO₂ amount and simultaneously constructs interconnected CO₂ transport pathways in the MMMs, thus enhancing the CO₂ permeability and selectivity.

The FT-IR spectra obtained for CO₂ adsorption and desorption are shown in Fig. 11. All the membranes do not show any significant change in the FT-IR spectra after humidification, adsorption and desorption, while the CO₂-adsorbed PI-ZIF-8@GO-20 membrane in its humidified state shows a new infrared absorption peak at 2336 cm^{-1} , which was assigned to the adsorption band of water-CO₂, indicating the CO₂ adsorption in the membranes. The peak at 2336 cm^{-1} disappears in the CO₂-desorbed PI-ZIF-8@GO-20 membrane, indicating that the reversible interaction disappears, while only physical adsorption still exists in the membrane. However, there is no corresponding peak in the unfilled membrane. There is probably less water in the unfilled membrane, resulting in less CO₂ adsorption. In short, water effectively facilitates the transport of CO₂ in the humidified MMMs.

In the humidified state, for the PI-ZIF-8@GO MMMs, the CO₂ permeability and CO₂/N₂ selectivity increase as the loading of ZIF-8@GO increases up to 20 wt%, indicating the absence of non-selective defects. However, when the loading of ZIF-8@GO was 30 wt%, the significantly increased permeability and reduced selectivity were ascribed to the visible aggregation of ZIF-8@GO in the MMMs as shown by SEM. The CO₂ permeability increases from 52 barrer for the unfilled PI to 259 barrer for the PI-ZIF-8@GO loaded MMMs at 30 wt% loading. The ideal CO₂/N₂ selectivity increases from 36 for the unfilled PI

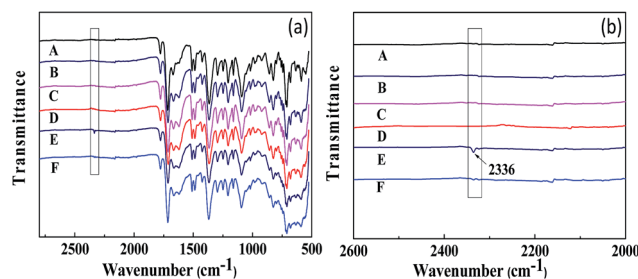


Fig. 11 FT-IR spectra of CO₂ adsorption and desorption within the humidified membranes. (A) PI membrane; (B) CO₂-adsorbed PI membrane; (C) CO₂-desorbed PI membrane; (D) PI-ZIF-8@GO-20 membrane; (E) CO₂-adsorbed PI-ZIF-8@GO-20 membrane; (F) CO₂-desorbed PI-ZIF-8@GO-20.



Table 4 Comparison of the gas permeability and selectivity of previously reported Matrimid-based MMMs with that of the MMMs determined in this study

| Filler | Loading (wt%) | Polymer | Operating conditions | | | | | | Ref. |
|---|---------------|----------------|----------------------|------------|----------|------------------|----------------------------|----------------------------------|------------|
| | | | Test state | Analysis | T (°C) | ΔP (bar) | P_{CO_2} [barrer] | $P_{\text{CO}_2}/P_{\text{N}_2}$ | |
| MIL-101 | 10 | Matrimid@5218 | dry state | Single gas | 35 | 10 | 6.95 | 52.92 | 50 |
| ZIF-90 | 15 | 6FDA-DAM | dry state | Single gas | 25 | 2 | 720 | 22 | 51 |
| MIL-53 | 37.5 | Matrimid@5218 | dry state | Single gas | 35 | 2 | 51.0 | 28.3 | 52 |
| CU-BPY-HFS | 30 | Matrimid@5218 | dry state | Single gas | 35 | 2.0 | 10.4 | 33.5 | 53 |
| MOF-5 | 30 | Matrimid@5218 | dry state | Single gas | 35 | 2 | 20.2 | 39 | 30 |
| ZIF-8 | 10 | Matrimid@5218 | dry state | Single gas | 22 | 4 | 13.67 | 21.6 | 54 |
| Mesoporous silica | 8 | Matrimid@5218 | dry state | Mixture | 25 | 1.75 | 15.3 | 40.3 | 55 |
| UiO-66-NH ₂ | 23 | Matrimid@5218 | dry state | Single gas | 25 | 1.36 | 23.7 | 36.5 | 56 |
| PA ^a -UiO-66-NH ₂ | 23 | Matrimid@5218 | dry state | Single gas | 25 | 1.38 | 29 | 37 | 56 |
| SO ₃ H-MCM-41 | 30 | Matrimid@9725 | dry state | Mixture | 25 | 10 | 9.4 | 31.5 | 57 |
| SO ₃ H-MCM-41 | 30 | Matrimid@9725 | dry state | Single gas | 25 | 10 | 10.4 | 37.4 | 57 |
| PEGSS | 20 | Matrimid@5218 | dry state | Single gas | 30 | 1 | 8.21 | 61.24 | 58 |
| CSM-23.3 | 30 | Matrimid@9725 | dry state | Mixture | 35 | 9 | 52.6 | 37.6 | 59 |
| POP-2 | 20 | Matrimid@5218 | dry state | Single gas | 35 | 2 | 25 | 25 | 60 |
| Cu-BTC | 30 | Matrimid@5218 | dry state | Single gas | 35 | 2 | 54 | 28.5 | 60 |
| ZIF-8 | 30 | Matrimid@5218 | dry state | Single gas | 35 | 2 | 40.1 | 24.5 | 60 |
| MIL-125 | 15 | Matrimid@9725 | dry state | Mixture | 35 | 9 | 9.4 | 34 | 61 |
| NH ₂ -MIL-125 | 15 | Matrimid@9725 | dry state | Mixture | 35 | 9 | 9.1 | 38 | 61 |
| Mg ₂ (dobdc) | 10 | 6FDA/TMPDA | dry state | Single gas | 25 | 2 | 850 | 23 | 62 |
| Cd-6F | 10 | 6FDA-ODA | dry state | Single gas | 25 | 2 | 37.8 | 35.1 | 63 |
| [Cu ₃ (BTC) ₂] | 30 | Matrimid@9725 | dry state | Mixture | 35 | 10 | 18.8 ^b | 24.1 | 64 |
| ZIF-8 | 30 | Matrimid@9725 | dry state | Mixture | 35 | 10 | 19.7 ^b | 19.5 | 64 |
| MIL-53(Al) | 30 | Matrimid@9725 | dry state | Mixture | 35 | 10 | 19.3 ^b | 23.6 | 64 |
| ZIF-8 | 20 | Matrimid@ 5218 | dry state | Single gas | 30 | 1 | 12.31 | 41.03 | This study |
| GO | 20 | Matrimid@ 5218 | dry state | Single gas | 30 | 1 | 8.23 | 35.78 | This study |
| ZIF-8@GO | 20 | Matrimid@ 5218 | dry state | Single gas | 30 | 1 | 11.14 | 53.05 | This study |
| ZIF-8 | 20 | Matrimid@ 5218 | Humidified state | Single gas | 30 | 1 | 178 | 42.12 | This study |
| GO | 20 | Matrimid@ 5218 | Humidified state | Single gas | 30 | 1 | 134 | 36.18 | This study |
| ZIF-8@GO | 20 | Matrimid@ 5218 | Humidified state | Single gas | 30 | 1 | 238 | 65.23 | This study |

^a PA = phenyl acetyl group. ^b PCO₂ units GPU.

membrane to 65 for the PI-ZIF-8@GO loaded MMMs at 20 wt% loading. The increased CO₂ permeability results from the following reasons. First, the content of free water in the membranes increases when compared with the unfilled PI membrane as listed in Table 1. The water swells the PI matrix and produces more CO₂ transport passageways in the MMMs, resulting in the increased CO₂ permeability. Second, the

increased CO₂ transport channels in ZIF-8 with sizes of 0.34 nm and additional CO₂ transport channels at the ZIF-8-GO interface lead to an increase in the CO₂ permeability. The MMM with 20 wt% ZIF-8@GO exhibits the optimum gas separation performance with a CO₂ permeability of 238 barrer and CO₂/N₂ selectivity of 65, which is 458% and 180% higher than the pure membrane, respectively, thus surpassing the 2008 Robeson

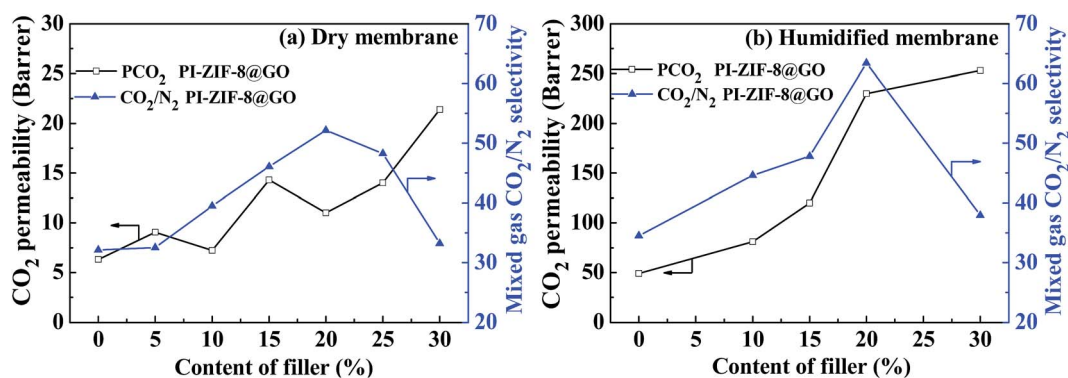


Fig. 12 Comparison of the mixed gas separation performance observed for the dry and humidified membranes: (a) CO₂ permeability and CO₂/N₂ selectivity observed for the dry membranes; (b) CO₂ permeability and CO₂/N₂ selectivity observed for the dry membranes with the ZIF-8@GO based MMMs (1.0 bar, 30 °C).



upper boundary line. The gas separation performance of PI-ZIF-8@GO-20 surpasses or is close to the gas separation as reported (Table 4).³⁸

When compared to the unfilled PI membrane, PI-ZIF-8@GO MMMs show a higher CO₂/N₂ selectivity. The ZIF-8 with high surface area in the PI-ZIF-8@GO MMMs may effectively enhance the adsorption capacity towards CO₂, resulting in the increased solubility selectivity. Moreover, when compared to the unfilled PI membrane, more free water exists in the PI-ZIF-8@GO loaded MMMs, which leads to the relatively lower transport resistance of CO₂ than that of N₂ with high CO₂/N₂ selectivity. In addition, the increased CO₂/N₂ diffusion selectivity causes the enhanced CO₂/N₂ selectivity. In comparison, the ZIF-8@GO are more effective in facilitating CO₂ transport than that of single ZIF-8 or GO in the MMMs. The underlying reason is that the ZIF-8@GO with uniform pore sizes of 0.34 nm, additional CO₂ transport channels at the interface of ZIF-8 and GO, and oxygen-containing functional groups on GO as well as the good interface compatibility between PI matrix and ZIF-8@GO constructs high-performance CO₂ transport pathways in the MMMs.

3.5 Mixed gas separation performance

Fig. 12 shows the separation performance of the unfilled PI membrane and the MMMs in a mixed gas. For the unfilled PI membrane, the mixed gas-real selectivity was lower than the corresponding ideal selectivity value of pure gas. However, the PI-ZIF-8@GO loaded MMMs exhibit real selectivity similar to their ideal value, suggesting the negligible competitive adsorption between CO₂ and N₂ in the MMMs. Since in water the solubility of CO₂ is remarkably higher than that of N₂ and PI-ZIF-8@GO loaded MMMs hold more water, the CO₂ transport pathways are multiplied with no evident competitive adsorption caused by N₂.

3.6 The effect of operating pressure

The effect of operating pressure was investigated in the range of 2–14 bar as shown in Fig. 13. The CO₂ permeability exhibits minor dependence on the gas pressure. The CO₂/N₂ selectivity

reduces as the feed pressure increases. When the pressure is lower than 8 bar, the CO₂ permeability decreases with an increase in the pressure, resulting from the saturation of the Langmuir absorption sites. At pressures up to 14 bar, the high concentration of CO₂ swells the PI chains and strengthens the mobility of the chain, leading to the increased CO₂ permeability. Moreover, N₂ transport is enhanced due to the enhanced mobility of the polymer chains and increased free volume in the membranes, leading to a reduced selectivity. Consequently, the plasticization phenomenon is not severe, which is primarily ascribed to the presence of water as a plasticizer in the PI matrix.

3.7 Long-term operation stability

As shown in Fig. 14, the long-term gas separation performance of the MMM containing 20 wt% ZIF-8@GO was investigated for up to 120 h. The CO₂ permeability and CO₂/N₂ selectivity fluctuate within a narrow range during this test. The MMM containing 20 wt% ZIF-8@GO exhibits favorable operation stability, indicating the structural stability of the MMM for potential application in gas separation.

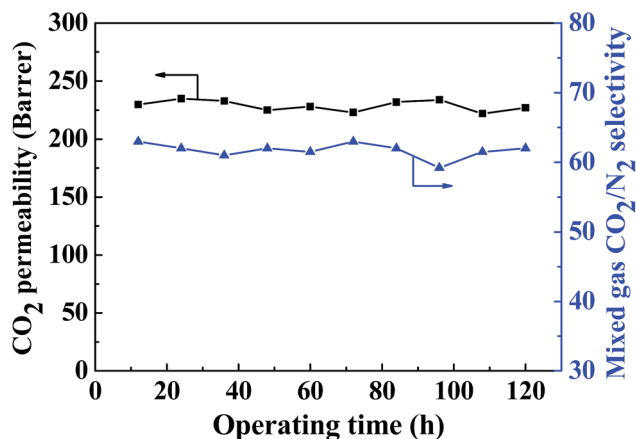


Fig. 14 Long-term operation stability of the gas separation performance observed for the MMM containing 20 wt% ZIF-8@GO.

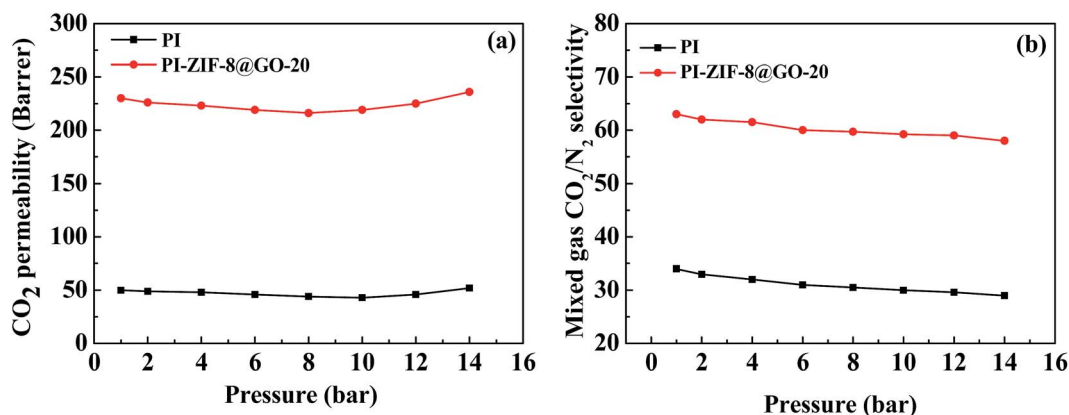


Fig. 13 Effect of feed pressure on (a) CO₂ permeability and (b) CO₂/N₂ selectivity of humidified membranes.



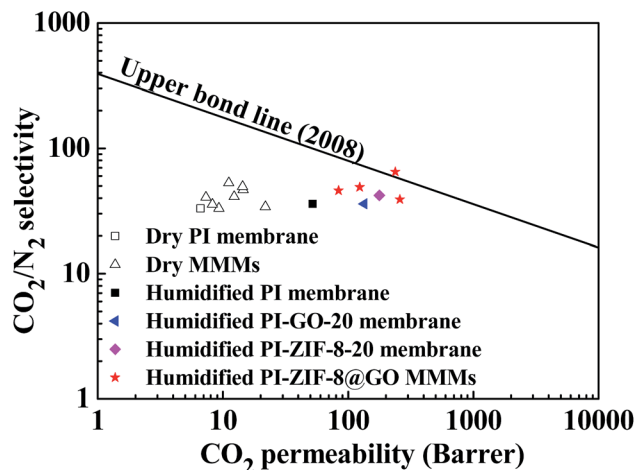


Fig. 15 Robeson's plots for CO₂/N₂ separation.

3.8 Comparison of the CO₂/N₂ separation performance with Robeson's upper boundary

Fig. 15 shows a comparison of the CO₂/N₂ separation performance with Robeson's upper boundary. In the humidified MMMs, the gas separation performance is close to or surpasses the Robeson's upper boundary reported in 2008, while in the dry MMMs, the gas separation performance falls far below the upper boundary. Both the CO₂ permeability and the CO₂/N₂ selectivity are remarkably improved in the PI-ZIF-8@GO MMMs, confirming the benefits of the synergistic effect of ZIF-8 and GO in the MMMs towards enhancing the CO₂ separation performance.

4 Conclusions

ZIF-8@GO was prepared using a facile *in situ* growth method and MMMs comprising PI and ZIF@GO were fabricated. The gas separation performance of the membranes was investigated and the CO₂ permeability and CO₂/N₂ selectivity of the ZIF-8@GO loaded MMMs increased when compared with that of the unfilled PI membrane. In particular, the membrane containing ZIF-8@GO exhibits the highest selectivity of up to 65 for the CO₂/N₂ system with a CO₂ permeability of 238 barrer, which surpasses the Robeson's upper boundary reported in 2008. The MMMs containing ZIF-8@GO show remarkable increments in the CO₂/N₂ selectivity when compared with the MMMs containing single ZIF-8 or GO fillers at the same content. The ZIF-8@GO loaded MMMs with high CO₂ separation performance are attributed to the ZIF-8@GO nanocomposite materials combining the favorable advantages of GO and ZIF-8. First, the high-aspect ratio of the GO nanosheets enhanced the diffusivity selectivity and ZIF-8 with high porosity is beneficial to the improvement of the CO₂ permeability. Second, ZIF-8 with high porosity is beneficial to the improvement of the CO₂ permeability. Third, ZIF-8@GO may construct extra CO₂ transport channels at the interface of ZIF-8 and GO. In their humidified state, the improved permeability is primarily ascribed to the incremental amount of free water, which produces more CO₂ transport passageways in the MMMs and

the elevated content of bound water as well as the good interface compatibility between ZIF-8@GO and the PI matrix.

Conflicts of interest

There are no conflicts to declare.

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