



Cite this: *Energy Adv.*, 2023,
2, 1309

Received 13th June 2023,
Accepted 14th July 2023

DOI: 10.1039/d3ya00274h

rsc.li/energy-advances

Reviewing thermal conductivity aspects of solar salt energy storage

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In recent years, nanoparticles have gained significant attention as additives in thermal energy storage materials for concentrated solar power plants. Depletion of fossil fuels and environmental concerns have prompted a shift towards clean renewable energy sources, like solar energy that is available in abundance. To harvest solar energy using thermal energy storage (TES) materials and enhancing such a materials thermal conductivity using nanoparticle additives, has emerged as a key research area. Hence, this review provides a comprehensive consideration of the thermal conductivity of solar salts with different nanoparticle additives; and the measurement techniques and various models that are used to study them experimentally and theoretically. Furthermore, the various factors that can influence the thermal conductivity are also analyzed and some issues – like high concentrations leading to high viscosity and agglomeration of nanoparticles in TES materials – are discussed. The different results show that thermal conductivity exhibits a linear relationship with the concentration of nanoparticles in TES materials at a certain level.

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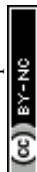
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1 Introduction

Recently the human population growth rate has been very high, with the global population reaching 7.9 billion in 2020,¹ resulting in increased demand for basic necessities such as food, water and transportation. Transportation is necessary for many daily requirements and pleasures. However, the vehicles we rely on are predominantly oil-based engines, which contribute to significant pollution, global warming, and various health hazards. The excessive usage of fossil fuels has depleted non-renewable resources to a critically low level, and their replenishment takes millions of years; the escalating consumption of fossil fuel globally is illustrated in Fig. 1.

A growing population means more vehicles causing higher fossil fuel emissions that result in numerous deaths worldwide. One potential solution to mitigate these issues is to reduce the use of oil based engines and transit towards electric vehicles (EVs). EVs are designed to minimize the use of fossil fuels and becoming a hot topic of research due to its pollution-free nature, low maintenance requirements and numerous other advantages. However, it should be noted that powering EVs with fossil fuels still contributes to pollution:³

- 65% emission of carbon dioxide (CO₂), one of the main greenhouse gases.
- 16% emission of methane that causes cardiovascular, respiratory problems, memory loss, depression.
- 2% emission of F-gases (fluorinated gases), the most powerful greenhouse gases.
- 6% emission of nitrogen oxides (NO_x), which results the production of ozone and smog when react with sunlight.
- Particulate matter is the major cause of lung cancer and acute respiratory distress.

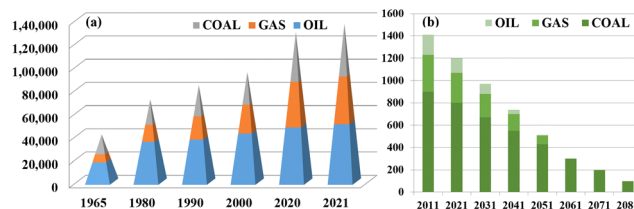


Fig. 1 (a) Global consumption rate of fossil fuel has increased and (b) fossil fuel levels are degrading day by day and are currently low (energy consumption in Terawatt-hours on the y-axis).² Adapted from Open Access data under the Creative Commons BY license. Copyright 2022 Global Change Data Lab.

As mentioned, our increasing population and their demands have led to a continuous rise in energy consumption from 1980 to 2013, increasing from 7300 TW h to 22 100 TW h, and the trend has continued.⁴ According to a report by the International Energy Agency,⁵ energy consumption almost doubled between 2010 and 2018. Various industries are actively working towards increasing the production of electric vehicles in the market, recognizing its potential as the next generation of vehicles. In 2017, there was a significant increase in EV sales, reaching nearly 200 000 units, which is impressive compared to traditional oil-based engine sales.

Efforts are being made worldwide to ban the sale of gasoline-powered cars, mainly due to environmental concerns and the declining availability of fossil fuels. Many countries, including India, are planning to completely phase out gas and diesel vehicles in the coming decade but its success will depend on the affordability of electric vehicles. The complex components involved in their production and the range of electric vehicles on a single charge can make them expensive, making it difficult for all to afford,⁶ however, as production increases and



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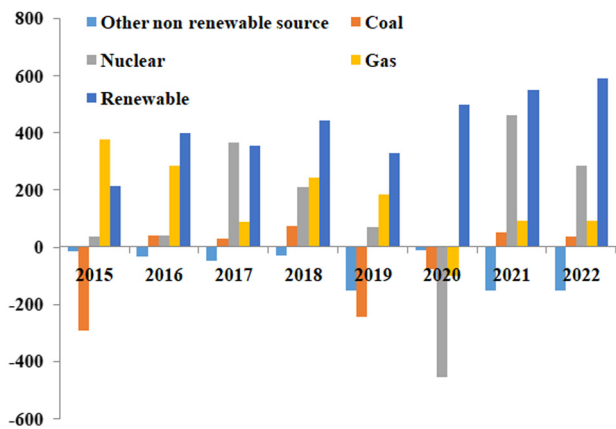


Fig. 2 Global electricity generation from different energy sources, including renewable energy sources, from 2015 to 2022.⁷ Adapted from Open Access data under the Creative Commons BY license. Copyright 2021 International Energy Agency.

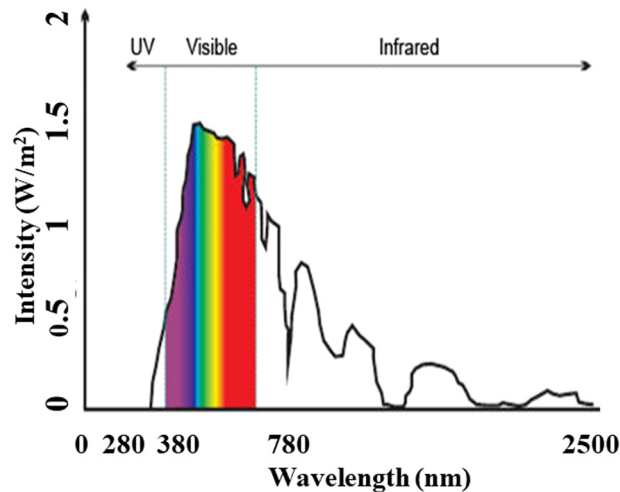


Fig. 3 Solar radiation spectrum, similar to blackbody spectrum illustrating the span of electromagnetic radiation.

competition grows, there is the possibility of cost reduction in the future.

Currently, available electric vehicles in the market are still charged using electricity produced from non-renewable sources, contributing to pollution. Fig. 2 displays global electricity generation from 2015 to 2022 using different sources such as coal, natural gas, nuclear energy, and more.⁷ Although the usage of non-renewable energy sources has declined in recent years, but are still in use.

With fossil fuel availability diminishing, electric vehicles powered by renewable energy sources like solar energy can be considered as an alternative to conventional gasoline engine vehicles. Solar energy is the most abundant renewable energy source globally, and harnessing it effectively can significantly reduce greenhouse gas emissions and reduce dependence on fossil fuels.

1.1 Solar energy

Relying solely on fossil fuels, will not meet our needs, switching towards renewable energy sources can address the electricity shortage problem, with a clean, pollution-free and abundant source. Among the various renewable energy sources, “solar energy” stands out the most readily available source that can be harnessed to generate electricity for multiple purposes, including charging stations for electric vehicles (EVs).

The solar energy spectrum⁸ encompasses the entire range of electromagnetic radiation, including infrared, visible, and ultraviolet light, as shown in Fig. 3. While it resembles a blackbody spectrum, it can be specifically divided into five regions:

- Ultraviolet C (UVC): ranging from 100 to 280 nm, this high-frequency radiation is mostly absorbed by the Earth’s atmosphere, resulting in a minimal percentage of UV rays reaching the surface.
- Ultraviolet B (UVB): ranging from 280 to 315 nm, most of this radiation is also absorbed by the Earth’s atmosphere.
- Ultraviolet A (UVA): ranging from 315 to 400 nm, this region of the spectrum reaches the Earth’s surface in significant amounts.

- Visible (VIS): ranging from 380 to 700 nm, all parts of the visible spectrum are received by the Earth.
- Infrared (IR): ranging from 700 nm to 1 000 000 nm (1 mm), this infrared region is divided into three parts:
 - (a) Infrared-A: ranging from 700 nm to 1400 nm
 - (b) Infrared-B: ranging from 1400 nm to 3000 nm
 - (c) Infrared-C: ranging from 3000 nm to 1 mm

Solar energy can be converted into electrical energy through two main processes: photovoltaic cells and concentrated power plants. Solar panels primarily convert visible light and a portion of infrared light into electricity, while the remaining energy from the spectrum goes to waste. When comparing various factors such as efficiency, electrical output, capacity utilization factor, net present value (NPV), net capital cost (NCC), levelized cost of energy (LCOE), and payback period for a plant with a capacity of 100 MW, concentrated solar power (CSP) systems exhibit higher efficiency compared to photovoltaic (PV) systems. In terms of electrical energy generation, CSP in its best case scenario outperforms PV as CSP can generate up to 33% more electricity than the best-case scenario of PV.⁹

1.2 Concentrated solar power plant

CSP plants operate on the basis of the thermal energy storage (TES) principle, which involves conversion of high-temperature thermal energy into power generation which provides a solution to the mismatch timing of solar energy availability and electricity demand.¹⁰ Solar energy has the potential to generate a significant amount of electricity if harnessed effectively. Two main methods exist for harnessing solar energy: active solar energy, which involves devices that convert solar energy into other usable forms; and passive solar energy, which focuses on the design, placement, and optimization of materials to maximize the utilization of sunlight, such as in greenhouse structures.¹¹

The first CSP plant was established in Italy by Sant’Ilario in 1968,¹² since then, there have been continuous advancements



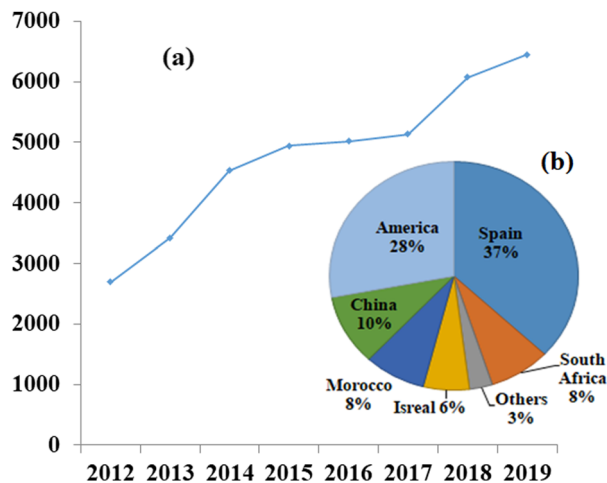


Fig. 4 (a) Globally installed capacity of concentrated solar power plants in Megawatts, increasing over the years,¹³ and (b) contribution of different countries to the overall installation of concentrated solar power plants, with Spain and America leading the way.¹³ Adapted from Open Access data under the Creative Commons BY license. Copyright 2015 International Energy Agency.

taking place in the field. However, CSP technology is not yet widely used due to its relatively low development compared to other renewable energy technologies. Nevertheless, significant efforts are being made to reduce the dependency on fossil fuels, and many countries, such as Spain and the US, are striving to unlock the full potential of CSP, as illustrated in Fig. 4.¹³ The global installed capacity of concentrated solar power plants from 2012 to 2019 and the capacity of CSP installations across different countries, highlighting the competition and growth of large-scale commercial CSP projects.^{14,15}

In India, during the first phase of the Jawaharlal Nehru National Solar Mission (JNNSM) from 2010 to 2013, CSP projects with a planned capacity of 470 MW were initiated.¹⁶ However, by 2018, only 228.5 MW had been achieved, but efforts are underway in India to generate clean energy and make the country self-reliant in this regard, by setting up a target to achieve 10 000 MW of CSP capacity in the coming years.¹⁷

1.3 Components of CSP

Considering the value of CSP, many countries are now investing in this technology for electricity generation regardless of the challenges related to reproducibility, sustainability, and efficiency. CSP is a form of passive solar energy that relies on storing thermal energy using heat-storing materials that should possess specific characteristics, such as high thermal conductivity, low density, large heat capacity, a wide range of working temperatures, stability under radiation, and cost-effectiveness.¹⁸ Designing an efficient CSP system remains a significant challenge, as it requires considerations of factors such as the levelized cost of electricity (LCOE),¹⁹ sustainability, durability, and cost-effectiveness.

A CSP system comprises various components, including a solar energy receiver, solar energy storage, a heat exchanger,

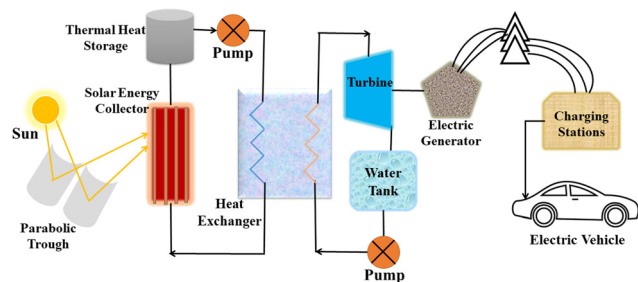


Fig. 5 Basic components of a concentrated solar power plant for the storage of thermal energy.

a turbine, charging stations, and more,^{20,21} as shown in Fig. 5. Currently, operational CSP plants are expensive and suffer from lower efficiency but could be improved by optimizing various parameters and components within the system.

First step for efficiency enhancement is the collection of solar energy with technologies like troughs, linear Fresnel mirrors, or concentrators, as the development level of these technologies directly impacts the system's efficiency.²² Another crucial aspect is the TES material, which allows for the storage of thermal energy and its utilization during periods when the sun is not available, such as rainy days, cloudy days, or at night.

1.4 Thermal energy storage (TES)

TES plays a crucial role in storing solar thermal energy for later use, and different materials can be used, including synthetic oil, molten salt, nanofluids, saturated steam, and ethylene glycol.^{23,24} Some of these materials are used at an industrial level, while others are still in the research phase.

For TES in a CSP, it is essential to use materials that can withstand high temperatures and effectively function within a wide temperature range. Molten salts are phase changing materials at specific temperature, with characteristics such as a low boiling point, a suitable working temperature difference, thermal stability, high thermal conductivity, and low density.²⁵

The low boiling point of molten salts ensures their changing state which can transfer heat at relatively low temperatures.²⁶ A good temperature difference implies a high heat capacity, enabling the capture of significant amounts of thermal energy from the sun. Thermal stability is important to maintain the efficiency and reproducibility of molten salts, preventing evaporation. Therefore, utilizing molten salts in CSP systems can reduce the LCOE,^{27–29} examples include liquid nitrate and carbonate salts, Hitec and Hitec XL doped with different nanoparticles at varying concentrations. The selection of an appropriate salt for TES depends on its working temperature, density (to avoid issues with viscosity), thermal conductivity, thermal stability, specific heat capacity, *etc.*, and should be sustainable, reproducible and cost-effective.

1.5 Thermophysical properties – thermal conductivity and its importance

To consider such solar salts for thermal energy storage, several thermophysical properties need to be taken into account:



thermal conductivity, specific heat capacity,²⁹ viscosity, stability, working temperature and corrosion resistance. Among these factors, thermal conductivity is of utmost importance in solar thermal energy storage systems as it is the cause of low efficiency in current CSP systems, and is caused by different factors, including density, moisture content, temperature and fluidity.

The thermal conductivity of solar salts is not particularly high, but by incorporating nanoparticles into solar salts, their conductivity can be enhanced, as shown in Fig. 6. When materials are reduced to the nanoscale, they exhibit fascinating properties such as photothermal and photoconductive behavior, as well as other attractive characteristics related to light: electricity, magnetism and catalysis. Nanoparticles of different metal oxides – such as Al₂O₃, TiO₂, ZnO, CuO, MgO – have been used to enhance the thermal conductivity of solar salts in different domains.

Al₂O₃ nanoparticles, with their spherical morphology and hexagonal structure, have been added to solar salts, resulting in an 8.3% increase in thermal conductivity at a temperature of 400 °C, depending on the shape, size, and concentration of the nanoparticles.³⁰ TiO₂ nanoparticles, which can exist in different structures (anatase, rutile, and brookite) depending on temperature, can enhance thermal conductivity by 8.1% when added to solar salts at particular concentrations.³⁰ The addition of ZnO nanoparticles to solar salts has not been extensively studied, but it has been observed that their incorporation with water increases thermal conductivity.³¹ CuO nanoparticles, with their monoclinic structure,³² exhibits the excellent heat and electricity conductivity and act as a p-type semiconductor with a band gap of 1.2 eV.³³ When nanoparticles of CuO are added to the base fluid, thermal conductivity of the mixture increases by approximately 30% at a volume concentration of 2%.³⁴ Adding MgO nanoparticles to solar salt shows an enhancement of 62.1% at 5.0% concentration,³⁵ but slightly

increases the density of the nanofluid. Besides metal oxide nanoparticles, carbon nanotubes (CNTs)³⁶ are gaining more attention due to their high thermal conductivity between 1100 W m⁻¹ K⁻¹ to 7000 W m⁻¹ K⁻¹.³⁷ Therefore, adding CNTs to solar salt could improve its thermal conductivity extensively.^{38,39}

As mentioned earlier, the thermal conductivity of solar salts is crucial for efficient heat transfer. However, their thermal conductivity falls between 0–1 W m⁻¹ K⁻¹ in liquid and in the solid state, which limits their heat transfer efficiency. Therefore, by incorporating nanoparticles the thermal conductivity of solar salts can be enhanced, resulting in increased efficiency and cost reduction.

2 Historical development

The historical understanding of thermal conductivity can be traced back to the 18th century when scientists began the study of heat. In 1686, Daniel Fahrenheit invented the mercury thermometer, which sparked interest in the study of heat.⁴¹ Prior to that, Guillaume Amontons proposed a theory about the flow of heat in the direction of decreasing temperature in a linear manner, although without any proof or experimental results. In 1761, Joseph Black introduced the concept of latent heat (the heat required to change the state of a substance) and specific heat (the quantity of heat required by a unit mass to raise its temperature by 1 °C), which laid the foundation for the concept of heat storage. Antoine Lavoisier and Pierre Simon Laplace demonstrated constancy of the latent heat of melting ice through the invention of the calorimeter.⁴² In 1776, Johann Heinrich Lambert advanced the study of heat movement by conducting experiments using a metal rod to study the linear temperature profile.⁴³ However, the results showed that the temperature decreases logarithmically along the rod, which may have been due to the specific shape and material of the rod not being taken into account.

Benjamin Franklin (1706–1790)⁴⁴ carried out experiments to determine the relative heat conducting abilities of different metals using wax. He coated the metals with wax and uniformly heated them to observe at what distance the wax would melt for each case. Further experiments by Igen Housz (1730–1794)⁴⁵ involved seven different metals of the same length and diameter, leading to the conclusion that different materials have different tendencies to conduct heat. His experiments also revealed that thermal conductivity in crystals is direction-dependent.

Count Rumford studied the relative insulating properties of various materials such as cotton, silk, wood, fur and down.⁴⁶ He used a thermometer placed in a glass bulb filled with the material of interest (*e.g.*, air, water, mercury) and immersed the apparatus in hot and cold water to establish temperature–time correlations, which allowed for the measurement of thermal conductivity.

By the end of the 18th century, a complete explanation of thermal conductivity had not yet been established. In 1802,

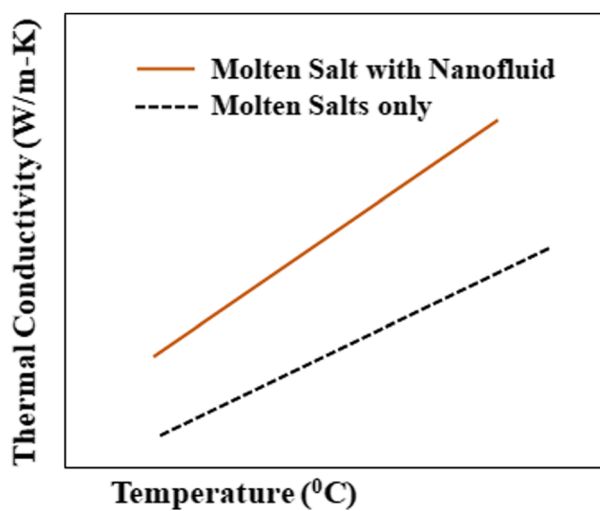


Fig. 6 Elevation in thermal conductivity after addition of nanoparticles to a molten salt. Adapted from ref. 40, with permission from AIP Publishing, Copyright 2017.



Fourier studied heat diffusion and built upon the research of Jean-Baptiste Biot,⁴⁷ who had focused on the heat conduction differential equation. Biot's work was based on Newton's law of cooling, which was derived for the case of radiative heat loss rather than conductive loss. So the idea of directly continuing Biot's work was dropped by Fourier who further formulated thermal conductivity using a boundary condition at the radiative surface, as given in eqn (1),

$$hT = -\kappa/dT/dx. \quad (1)$$

Here, h represents the relative heat transfer coefficient, T denotes temperature, κ represents thermal conductivity, and $\frac{dT}{dx}$ represents the temperature gradient. However, no devices or experiments were available at the time to directly measure heat flow, Fourier had to devise experiments to calculate thermal conductivity based on whether temperature is a function of heat or not. Subsequently, various experiments were conducted to determine the relative thermal conductivity of different materials and the absolute thermal conductivity after a specific stage was set by Fourier.⁴⁸

3 Thermal conductivity analytics

Thermal conductivity is a material property that determines how well a material conducts heat, commonly represented by the symbol ' k ', but in some books and literature, it is also denoted by ' λ ' or ' κ '; the inverse of thermal conductivity gives thermal resistivity. Materials with high thermal conductivity are often used in heat sinks as they can efficiently absorb and transfer heat energy to the environment. Many experiments have been conducted to develop devices that can precisely measure the thermal conductivity of materials. In 1807 to 1811, Joseph Fourier designed a device and formulated a mathematical expression that provides a good estimate of thermal conductivity. Fourier's law of thermal conduction (also known as the law of heat conduction),⁴⁷ as described by eqn (2), states that the rate of heat transfer through a material is proportional to the negative gradient of temperature and the area of heat flow.

$$q = -\kappa \cdot \nabla T \quad (2)$$

where ∇T refers to the temperature gradient, q denotes the thermal flux or heat flux, and κ refers to the thermal conductivity of the material.

Mathematics:

Consider a material in which the flow rate of heat is $\frac{dT}{dx}$ through a cross-sectional area represented by A . Initially, at a distance x , the temperature is denoted as T , and after some time, at a distance $x + \nabla x$ and temperature $T + \nabla T$. Heat flows in the positive direction, the temperature gradient must be negative, as heat flows from higher to lower temperatures, as shown in Fig. 7.

Now, the thermal conductivity κ can be defined as the ratio of heat flow rate per unit area to the negative of the temperature gradient. It can be written as in eqn (3):

$$dQ/dt = \kappa \cdot A \cdot (dT/dx) \quad (3)$$

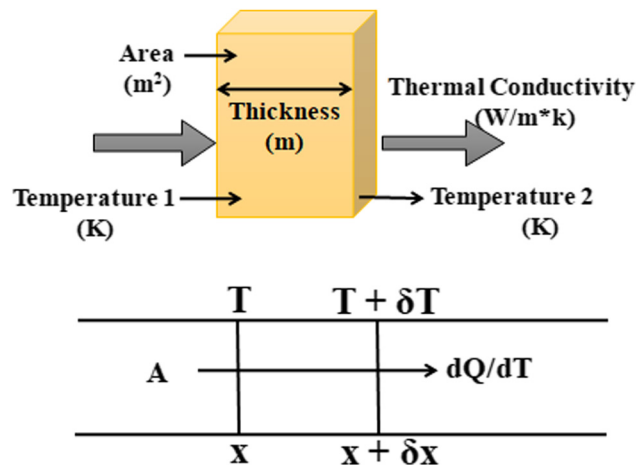


Fig. 7 A typical heat flow mechanism inside the conductor.

Units:

- Fundamental units of thermal conductivity can be: temperature, length, mass and time.
- It can also be written as power/(length \times temperature).
- Watts per meter-Kelvin ($\text{W m}^{-1} \text{K}^{-1}$) is the standard unit of thermal conductivity.
- These units relate heat conduction rate for a unit thickness of a material, for each Kelvin of temperature difference.

Discussion so far considers a one-dimensional situation in an isotropic medium, where all properties are uniform and independent of direction. In such a scenario, heat flow is opposite to the temperature gradient. However, in an anisotropic medium, where properties vary with direction, the heat flow rate and the temperature gradient can differ along different axes of the crystal. In that case, the heat flow may not strictly be antiparallel to the temperature gradient, and thermal conductivity becomes a tensor quantity.

3.1 Thermal conductivity in different states

Matter is composed of extremely small particles that cannot be seen with the naked eye, and is classified into four states – solid, liquid, gas, and plasma – but for the purpose of discussion here only three states (excluding plasma) are considered. The thermal conductivity of a material⁴⁹ varies depending on its state whether it is solid, liquid, or gas state. This variation is due to the differences in intermolecular spacing: the molecules in a liquid are further apart from each other than in a solid, and move in a random manner due to the larger intermolecular spacings. This random movement hinders the efficient conduction of heat, resulting in a decrease in thermal conductivity in liquids.

Thermal conductivity is directly proportional to the mean molecular speed and mean free path.⁵⁰ The mean free path depends on the diameter of the molecule, where larger molecules have a higher probability of collisions compared to smaller molecules. Light gases like hydrogen and helium have high thermal conductivity, whereas denser gases like xenon and dichlorodifluoromethane have low thermal conductivity due to



hindered molecular movement. Additionally, the thermal conductivity of gases generally increases with temperature.

When comparing liquids to gases, liquids tend to have better thermal conductivity and with their fluidity properties, they are suitable to use as heat sinks. Liquids can absorb heat and effectively transfer it through the heat sink, acting as heat transfer agents but for non-metallic liquids, the thermal conductivity tends to decrease with increasing temperature. It is important to note that thermal conductivity cannot be generalized for all liquids, as it depends on the specific properties of each liquid.

3.2 Thermal conductivity of solar salts with nanoparticles

Molten salts undergo a phase change from solid to liquid when their temperature is increased, making them suitable for use as thermal energy storage media. However, the thermal conductivity of molten salt is not sufficiently high, an important characteristic for an applicable thermal energy storage material, addition of selected nanoparticles to molten salt could resolve this, as illustrated in Fig. 8. Among the molten salts, solar salt stands out due to its favorable thermophysical properties, affordability and availability in the market, as seen in Table 1, having significant potential for incorporation in CSP systems.⁵¹

Extensive research has been conducted to investigate how the addition of nanoparticles and other parameters can enhance thermal conductivity. Several models have been proposed to explain the behavior of nanofluids, which are a weighted average of nanoparticles and base fluids, and their contribution to thermal conductivity.⁵⁴ These models incorporate various factors such as the diameter of the base fluid, sphericity of nanoparticles, viscosity, temperature, volume fraction, nano-layer thickness, and so on. Maxwell was the first to propose a model predicting the thermal conductivity of nanofluids,⁵⁵ which considered spherical bodies in low concentrations. In this context of nanofluids, the thermal conductivity is typically denoted as κ , but for ease of understanding, we will

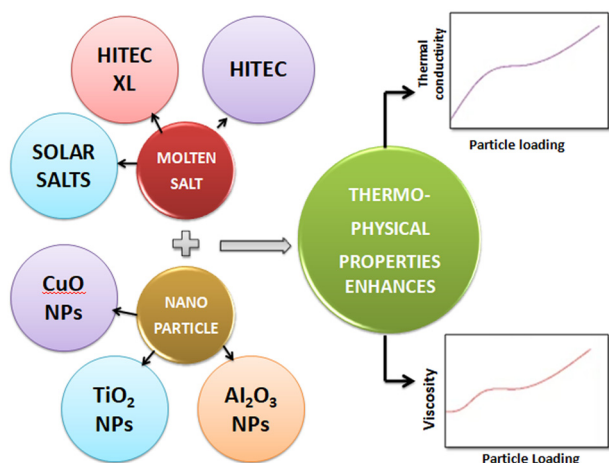


Fig. 8 Addition of nanoparticles to molten salt, elevating their thermo-physical properties for use as thermal energy storage materials.

Table 1 List of molten salts^{52,53}

No.	Salt	Composition (wt%)	T. C. (W m ⁻¹ K ⁻¹)	Cost (Rupees per kg)
1	Solar salt	NaNO ₃ -KNO ₃	0.52	37.30
2	Hitec	NaNO ₃ -KNO ₃ -NaNO ₂	0.33	70.78
3	Hitec XI	NaNO ₃ -KNO ₃ -Ca(NO ₃) ₂	0.52	108.82
4	Therminol VP-1	Biphenyl-diphenyl oxide	0.090	301.36

use K in this discussion. Different suffixes and prefixes are employed to represent the thermal conductivity of different fluids.

$$K_{nf \max} = K_f \left(\frac{K_{np} - 2K_{bf} - 2\phi(K_{np} - K_{bf})}{K_{np} - 2K_{bf} - 2\phi(K_{np} - K_{bf})} \right) \quad (4)$$

Symbols in the above equation as well as in following ones are: K_{bf} is the thermal conductivity of the basefluid, K_{np} is the nanoparticle thermal conductivity, ϕ is the concentration of nanoparticles. K_{nf} is the thermal conductivity of nanofluid and can be predicted using eqn (4). Maxwell included thermal conductivity of the basefluid and nanoparticles only. Thermal conductivity was further studied by Hamilton and Crosser⁵⁶ who developed another model (eqn (5)), that includes factors like particle shape and composition as well as the thermal conductivity of the basefluid and nanoparticle.

$$K_{nf \text{ H\&C}} = K_{bf} \left(\frac{K_{np} - (n-1)K_{bf} - \phi(n-1)(K_{bf} - K_{np})}{K_{np} - (n-1)K_{bf} - \phi(K_{np} - K_{bf})} \right) \quad (5)$$

where n denotes the shape factor and can be determined from the sphericity of particles, w , for instance the sphericity is considered to be 3.0 for a sphere and 0.5 for a cylindrical shape, related as in eqn (6),

$$n = 3/w. \quad (6)$$

The next model was provided by Wasp,⁵⁷ which includes the convection heat transfer problems, and eqn (7) can be considered as a special case of the Hamilton and Crosser model,⁵⁶ in which particles are exactly spherical in shape and this model can act as a good practical approach whenever there is uncertainty about a particles' shape,

$$K_{nf \text{ wasp}} = K_{bf} \left[\frac{K_{np} + 2K_{bf} - 2\phi(K_{bf} - K_{np})}{K_{np} + 2K_{bf} + \phi(K_{bf} - K_{np})} \right] \quad (7)$$

Another model as seen in eqn (8) was given by Xue,⁵⁴ which includes factors like composition, shape, logarithmic progression and again thermal conductivity of the nanoparticle and basefluid,

$$K_{nf \text{ Xue}} = K_{bf} \left(\frac{(1-\phi) + 2\phi \frac{K_{np}}{K_{np} - K_{bf}} \ln \frac{K_{np} + K_{bf}}{2K_f}}{(1-\phi) + 2\phi \frac{K_f}{K_{np} - K_{bf}} \ln \left(\frac{K_{np} + K_{bf}}{2K_{bf}} \right)} \right) \quad (8)$$

None of these models consider the random movements of particles in the fluid due to Brownian motion, and are hence considered to be static models. Dynamic models have also been



developed that include the viscosity, temperature, size and distribution, layer thickness, cluster formation *etc.*, by which the thermal conductivity of nanofluids is affected. A dynamic model (eqn (9)) was given by Xuan *et al.*⁵⁸ using the Maxwell model⁵⁵ as a baseline and adding the other factors also.

$$K_{\text{nfXuan}} = K_{\text{nfmax}} + 1/2\rho_{\text{np}}c_{\text{np}}\phi(2D_{\text{B}})^{1/2} \quad (9)$$

where D_{B} is the Brownian diffusion that includes the temperature, viscosity of basefluid and of the cluster, that impact the thermal conductivity and can be calculated as,

$$D_{\text{B}} = k_{\text{B}}T/6\pi\mu_{\text{bf}}r_{\text{c}} \quad (10)$$

where T corresponds to the temperature of fluid, r_{c} represent the radius of nanoparticle, k_{B} is denoted as the Boltzmann constant and μ_{bf} is the basefluid viscosity.

The Kleinstreuer model⁵⁹ again uses the Maxwell model⁵⁵ as a base model and adds other dynamic factors that affect the thermal conductivity. These include volume fraction, types of particle, temperature and also the properties of the basefluid. It considers function f , that depends on these various factors, as given in eqn (11),

$$K_{\text{nfKlein}} = K_{\text{nfmax}} + \frac{(5 \times 10^4)}{K_{\text{bf}}} \beta(\phi) \rho_{\text{bf}} c_{\text{np}} f(T, \phi) \sqrt{\left(\frac{k_{\text{B}}T}{\rho_{\text{np}}d_{\text{np}}} \right)} \quad (11)$$

Next model is given by Xie *et al.*⁶⁰ that include the volume fraction, radius of nanoparticles and basefluid, nanolayer thickness, ratio between nanoparticle and basefluid. Using eqn (12), thermal conductivity can be measured.

$$K_{\text{nfXie}} = 1 + 3\Theta\phi_{\text{T}} + \left(\frac{3\Theta^2\phi_{\text{T}}^2}{1 - \Theta\phi_{\text{T}}} \right) \quad (12)$$

where Θ depends on volume fraction, radius of nanoparticle, nanolayer thickness, and ϕ_{T} is the total volume fraction. Avsec⁶¹ presented a model, in which thermal conductivity of the base fluid and nanoparticle, and liquid layer thickness have been included, ignoring the particle size and the interface between the particles. Another empirical model is given by Jang and Choi⁶² eqn (13) including all the factors like the diameter of molecules of the basefluid, Reynolds number, Prandtl number, nanoparticle thermal conductivity and it's the surface resistance, particle fraction, *etc.*

$$K_{\text{nfJang\&Choi}} = K_{\text{bf}}(1 - \phi) + 0.01K_{\text{nano}}\phi + 18 \times 10^6 \left(\frac{d_{\text{bf}}}{d_{\text{np}}} \right) K_{\text{bf}} \text{Re}_d^2 \text{Pr}_{\text{bf}}\phi \quad (13)$$

where K_{nano} is the thermal conductivity of nanoparticles with Kapitza resistance, Re_d and Pr are the Nusselt number, d_{bf} and d_{np} are the characteristic lengths of the basefluid and nanoparticle, respectively. Another model given by Pak and Cho⁶³ (eqn (14)) is very compact, taking into consideration geometry, diameter and also the surface resistance of nanoparticles,

$$K_{\text{nfP\&C}} = 1 + 7.47\phi. \quad (14)$$

The next model was given by Timofeeva *et al.*⁶⁴ and also includes agglomeration factors. The thermal conductivity model predicted is given by eqn (15),

$$K_{\text{nfTim}} = K_{\text{f}}(1 + 3\phi). \quad (15)$$

Yu and Choi's⁶⁵ model predicts the thermal conductivity by modifying the Maxwell equation. This model includes the nanolayer thickness, original nanoparticle radius and all above discussed factors. Using eqn (16), thermal conductivity can be measured,

$$K_{\text{nfY\&C}} = K_{\text{bf}} \left[\frac{K_{\text{pe}} + 2K_{\text{bf}} + 2(K_{\text{pe}} - K_{\text{bf}})(1 + \beta)^3\phi}{K_{\text{pe}} + 2K_{\text{bf}} - (K_{\text{pe}} - K_{\text{bf}})(1 + \beta)^3\phi} \right] \quad (16)$$

where K_{pe} represents the thermal conductivity of the equivalent particle, β is the ratio of nanolayer thickness to the radius of the original particle, ϕ denotes the particle volume concentration. Another model (eqn (17)) was given by Wang *et al.*⁶⁶ and includes factors of nanolayer thickness, particle size, temperature, volume fraction and also considers the interaction between particles,

$$K_{\text{nfWang}} = K_{\text{bf}} \left(1 + \frac{\frac{3fq\langle p \rangle}{p_0}}{1 - \frac{fq\langle p \rangle}{p_0}} \right) \quad (17)$$

where f is the graded nanolayer and depends on the original volume fraction, $\langle p \rangle$ is the average dipole moment of a sphere, p_0 is the thermal dipole due to temperature distribution among the spherical particles, q is the dipole factor. Under the assumption by Chandrasekar *et al.*⁶⁷ gave two models M1 and M2, believing that nanoparticles are uniformly dispersed in the basefluid, thermal conductivity which can be calculated using M1 given in eqn (18). The second model predicted, M2, depends on particle shape, Brownian motion, contribution layer thickness, *etc.* and is given by eqn (19), and can be reduced to the models predicted by Maxwell, Hamilton and Crosser, Yu and Choi, if sufficient conditions are applied.

$$K_{\text{nfCh,M1}} = K_{\text{bf}} \left[\left(\frac{c_{\text{np,nf}}}{c_{\text{p}}} \right) \left(\frac{\rho_{\text{nf}}}{\rho} \right)^{1.33} \left(\frac{M}{M_{\text{nf}}} \right)^{0.33} \right] \quad (18)$$

$$K_{\text{nfCh,M2}} = K_{\text{bf}} \left[\frac{K_{\text{np}} + (n-1)K_{\text{bf}} + (n-1)(K_{\text{nf}} - K_{\text{bf}})(1 + \beta)^3\phi}{K_{\text{np}} + (n-1)K_{\text{bf}} - (K_{\text{np}} - K_{\text{bf}})(1 + \beta)^3\phi} \right] \quad (19)$$

where $c_{\text{np,nf}}$ denotes specific heat of the nanofluid, c_{p} represents the specific heat, ρ_{nf} is the density of the nanofluid, ρ is density, M is the molecular weight, M_{nf} is the molecular weight of the nanofluid and other symbols have the same meaning as mentioned above.

Another empirical model⁶⁸ predicted by Corcione *et al.* (eqn (20)) includes factors of dynamic viscosity of the nanofluids, volume fraction, temperature but only for the range 294–324 K, and diameter of nanoparticles in the range 10–150 nm. This type of specified model is very beneficial from an



engineering point of view for thermal design tasks:

$$K_{\text{nfC}} = 1 + 4.4\text{Re}^{0.4} \text{Pr}^{0.66} \left(\frac{T}{T_{\text{fre}}}\right)^{10} \left(\frac{K_{\text{np}}}{K_{\text{bf}}}\right)^{0.03} (\phi)^{0.66} \quad (20)$$

As discussed, the various models⁶⁹ developed consider all the factors that can affect the thermal conductivity of the nanoparticles, basefluid and nanofluid. All the models started with the basic Maxwell predicted model and were modified depending on the factors considered.

4 Factors affecting thermal conductivity

Various factors affect the thermal conductivity of a material, including its structure, density, phase, composition and temperature, and can be intensive or extensive in nature. The thermal conductivity also differs between metals and non-metals due to their distinct characteristics, which are also influenced by various factors.

4.1 Effect of temperature

The behavior of thermal conductivity with temperature depends on whether the material is a metal or a non-metal, as each behaves differently in response to temperature changes.

4.1.1 Metals.

• According to the Wiedemann–Franz law, thermal conductivity is directly proportional to temperature and electrical conductivity.

• When the temperature increases, the electrical conductivity of a pure metal decreases due to electron collisions.

• This implies that the thermal conductivity of a pure metal varies slightly with increasing temperature and abruptly decreases when the temperature reaches 0 K.

• Alloys, on the other hand, exhibit less change in electrical conductivity, resulting in an increase in thermal conductivity with temperature.⁷⁰

4.1.2 Non-metals.

• In non-metals, thermal conductivity is mainly attributed to lattice vibrations that carry energy in the form of phonons due to scarcity of free electrons.

• As phonons travel and collide with each other they experience a mean free path that does not significantly change with temperature. This indicates that the thermal conductivity of non-metals remains largely unaffected by higher temperatures.

• Below the Debye's temperature,⁷⁰ both the thermal conductivity and heat capacity of non-metals decrease.

4.2 Other factors that affect thermal conductivity

Variations in thermal conductivity can be attributed to several factors, including thermal anisotropy, electrical conductivity, magnetic fields, and more. The influencing factors of thermal conductivity in substances are illustrated below.

• Phase change of material: changing the phase of a material results in abrupt changes in thermal conductivity. For example, water exhibits this dependency, where the thermal conductivity

of ice⁷¹ is $2.18 \text{ W m}^{-1} \text{ K}^{-1}$ and changes to $0.56 \text{ W m}^{-1} \text{ K}^{-1}$ in the liquid phase.

• Thermal anisotropy: crystals have different planes, and as a result, the physical properties of crystals vary across these planes. It is possible that phonons along a specific plane are coupled differently to phonons in other planes of the same crystal. Thus, the thermal conductivity varies due to thermal anisotropy, which means that the direction of the temperature gradient may not align with the direction of heat flow.

• Influence of magnetic fields: the Maggi–Righi–Leduc effect⁷² describes the change in thermal conductivity of a conductor when subjected to an applied magnetic field, which causes formation of an orthogonal temperature gradient, that can be responsible for alterations in thermal conductivity.

• Isotopic purity of the crystal: while thermal conductivity is an intensive property, the addition of impurities decreases its value. For instance, in type IIa diamond, a 98.9% concentration of carbon-12 results in a thermal conductivity of $10\,000 \text{ W m}^{-1} \text{ K}^{-1}$, whereas a 99.9% enriched diamond exhibits a thermal conductivity of $41\,000 \text{ W m}^{-1} \text{ K}^{-1}$.⁷³

4.3 Factors affecting the thermal conductivity of nanoparticles

It has been established that the thermophysical properties of bulk matter differ from nanoparticles. Various factors that affect the thermal conductivity of nanoparticles⁶⁹ are listed below.

• Numerous experiments have demonstrated how different nanoparticles of different shapes and size affect the thermal conductivity. Ambreen and Kim *et al.*⁷⁴ showed that reducing nanoparticle size increases the effective surface area, enhancing Brownian motion and leading to an increase in thermal conductivity. Subsequently, Xu *et al.*⁷⁵ and Anoop *et al.*⁷⁶ conducted different experiments and showed that different shapes of nanoparticles, such as spherical, cylindrical, rod, banana-shaped, nearly-rectangular, brick, platelet, and blade shapes, have an impact on thermal conductivity.

• Thermal conductivity also depends on the base fluids and the concentration of nanoparticles. Increasing the concentration amplifies the interfacial area between the base fluid and the nanoparticles, resulting in an increase in thermal conductivity.⁷⁷

• Thermal conductivity also depends on agglomeration of NPs, as it provides an extra conduction path to the nanofluids, but excessive agglomeration can lead to sedimentation, creating difficulties for fluid to flow.^{78,79}

• Different experiments have been done to confirm if the thermal conductivity of nanoparticles depends on temperature. Chon *et al.*⁸⁰ and Mintsa *et al.*⁸¹ showed that it is independent of temperature, but some experiments showed an inverse relation with temperature, like the experiment carried out by Duangthongsuk and Wongwises⁸² for water-based TiO₂ nanofluids.

• The pH of nanofluids is a crucial factor that directly or indirectly affects thermal conductivity by influencing the degree of nanoparticle aggregation, zeta potential, particle size distribution, rheology, viscosity, and stability, all of which impact the thermal conductivity of nanofluids.⁸³



• When a strong magnetic field is applied, small-dimensional particles form chains that tend to align with the direction of the magnetic field observed in experiments.⁸⁴ The alignment of particles promotes heat transfer capability and lead to an increment in thermal conductivity.⁸⁵

• Sonication also plays an important role. Decreasing sonication time reduces the probability of sedimentation and enhances Brownian motion, ultimately increasing the thermal conductivity of nanofluids. However, excessive sonication time can have a reverse effect on thermal conductivity.^{86,87}

5 Experimental techniques

Thermal conductivity is enhanced by the addition of nanoparticles to solar salts, making it an important factor in the operation of CSP systems. Solar salts typically have low thermal conductivity, but inclusion of nanoparticles can improve. Different methods are available for the synthesis and mixing of nanoparticles with solar salts, as well as various techniques for measuring the thermal conductivity of nanofluids.

The current methods for measuring thermal conductivity can be categorized based on their temperature dependence. Fig. 9 illustrates the various methods used to approximate thermal conductivity, primarily falling into three types: transient methods (where temperature changes with time), steady-state methods (where temperature remains constant and heat transfer is characterized by a constant, specific heat transfer), and the thermal comparator method (a relative method that uses a calibration curve to determine the value of the unknown parameters).⁸⁸

5.1 Transient hot wire method

Stalhane and Pyk proposed the transient hot wire method in 1932 as discussed by Horrocks *et al.*⁸⁹ which is used to measure the thermal conductivity of nanomaterials where solar salts are used as the base fluid and nanomaterials are additives with temperature-dependent thermal conductivity. This method involves a thin wire, typically made of platinum or tantalum, which serves as both a sensor and a heat sink submerged in a sample cell filled with the test fluid, as shown in Fig. 10. Applying a specific voltage across the thin wire, heat is

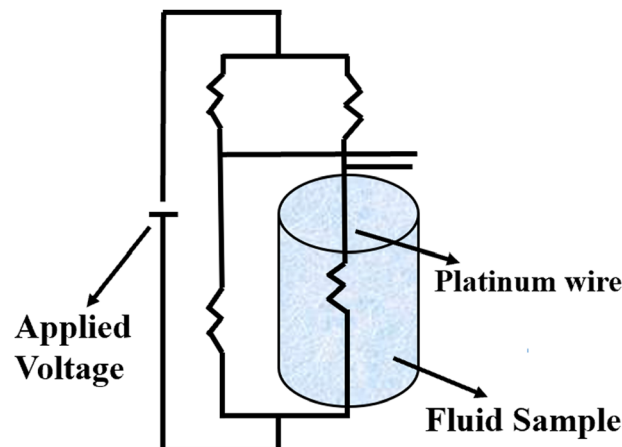


Fig. 10 Schematic diagram of the transient hot wire method. Adapted from ref. 69, with permission from MDPI, Copyright 2021; and ref. 91 with permission from Elsevier, Copyright 2020.

generated and transferred to the surrounding fluid at a rate dependent on the thermal conductivity of the liquid.

As the heat is transferred, the changes in resistance can be correlated with the variations in temperature, allowing for the calculation of thermal conductivity. According to Carslaw and Jaeger,⁹⁰ the relationship between change in temperature with time can be described by eqn (21),

$$\Delta T = \frac{-q}{4\pi K_{\text{nf}}} E_i \frac{-r^2}{4Dt} \quad (21)$$

where K represents the thermal conductivity, r denotes the distance at which the temperature is measured, q is the constant heat applied, and E_i is the integral term upon expanding it, as shown by eqn (22),

$$-E_i(\alpha) = \int 1/u \exp(-u) du = -\beta - \ln \alpha - \alpha^2/4 + \dots \quad (22)$$

Higher order terms of α are neglected for long wires as it is very small. So eqn (21) changes to eqn (23),

$$\Delta T \approx \frac{-q}{4\pi K_{\text{nf}}} \left[-\beta - \ln \left(\frac{r^2}{4Dt} \right) \right] \quad (23)$$

and thermal conductivity can be calculated using eqn (24)

$$K_{\text{nf}} = \left[\frac{q}{4\pi(\Delta T_2 - \Delta T_1)} \right] \ln \frac{t_2}{t_1} \quad (24)$$

5.2 Thermal constants analyzer

The thermal constants analyzer technique is utilized to determine the thermal conductivity of nanofluids by employing a transient plane source based on Fourier's law of heat conduction. The setup consists of a thermal constants analyzer, a vessel, a constant temperature bath, and a thermometer, as depicted in Fig. 11. The probe is immersed in the vessel containing the nanofluid, which is then placed in the constant temperature bath. The thermometer is used to measure the temperature of the nanofluid.

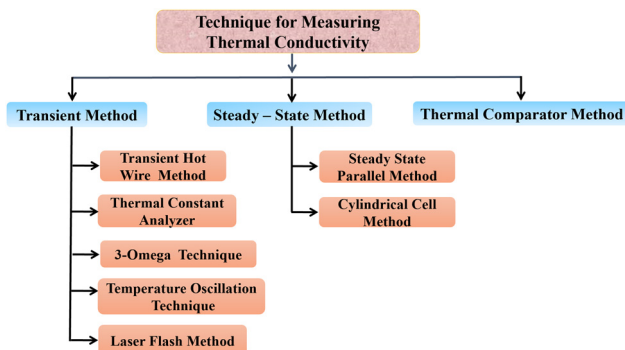


Fig. 9 The different techniques for measuring the thermal conductivity of nanofluids.



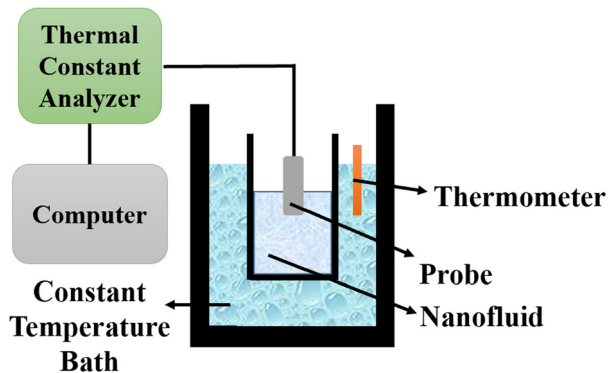


Fig. 11 Schematic diagram of a thermal constants analyzer. Adapted from ref. 69, with permission from MDPI, Copyright 2021; and ref. 91 with permission from Elsevier, Copyright 2020.

The probe utilized in this technique should comprise a thin foil made of an electrical conducting material, which is responsible for generating the heat. By applying Fourier's law of thermal conductivity and utilizing the relationship between resistance and temperature, described by eqn (25),⁹² the thermal conductivity of the nanofluid can be determined,

$$\Delta T(\tau) = \frac{1}{\alpha} \left[\frac{R_p(\tau)}{R_0} - 1 \right] \quad (25)$$

where $\Delta T(\tau)$ is the rise in temperature of the probe, $R_p(\tau)$ is the resistance function of time, α is the temperature coefficient of the electric resistance, R_0 is the electrical resistance. The dimensionless time, τ , is given by eqn (26), where R is the thermal diffusivity of the fluid and r_p is the radius of the probe, at $\tau = 0$, and t is the real time.

$$\tau = \sqrt{\frac{tR}{r_p^2}} \quad (26)$$

If there is no natural convection of the fluid taking place then thermal conductivity can be calculated using eqn (27),⁹³

$$\Delta T = \frac{W}{\pi^{1.5} r_p K_{nf}} D(\tau) \quad (27)$$

where $D(\tau)$ is described as a geometric function, and W is the electric power supplied to the probe.

5.3 3-Omega method

This method was initially developed for measuring the thermal conductivity of bulk materials and has been subsequently adapted for nanofluids and thin films.⁹⁴ It involves the application of sinusoidal current with a frequency ω across the sample using a metal wire heater which is similar to the hot wire method, where the sample element serves as both the heater and the thermometer. The applied current at frequency ω generates heat at a frequency of $2 - \omega$, and the corresponding voltage is measured at $3 - \omega$. The thermal conductivity can be determined using eqn (28),

$$\Delta T(r) = \frac{P}{l\pi K_{nf}} \left(\frac{1}{2} \ln \frac{D}{r^2} + \ln 2 - 0.5772 - \frac{1}{2} \ln 2\omega - \frac{i\pi}{4} \right) \quad (28)$$

where, $\frac{P}{l}$ represents the amplitude of the power per unit length generated at a frequency $2 - \omega$, D is the thermal diffusivity, and r is the distance. Hence thermal conductivity (K_{nf}) can be measured using the real or imaginary part of the given equation. For more detail, one can look into the paper by Cahill *et al.*⁹⁵

5.4 Temperature oscillation technique

The temperature oscillation technique is employed initially to measure the thermal diffusivity, then it is used for the calculation of thermal conductivity. A nanofluid is used to fill the cylindrical volume, and temperature oscillations are applied where amplitude and phase of the temperature oscillations are determined by selecting reference and end points, as shown in Fig. 12.⁹⁶ It has been demonstrated that thermal diffusivity can be accurately measured using the amplitude attenuation of thermal oscillations. Therefore, by calculating the density and specific heat using eqn (29), the thermal conductivity can be determined using a principle first utilized by Das *et al.*⁹⁷ for nanofluid comprising nanoparticles of Al_2O_3 and CuO in water,

$$C_{p,nf} = \frac{m_s C_{p,s} + m_w C_{p,w}}{m_s + m_w} \quad (29)$$

The thermal conductivity can be calculated using eqn (30),

$$K_{nf} = \alpha_{nf} \rho_{nf} C_{p,nf} \quad (30)$$

5.5 Laser flash method

The laser flash method was developed to determine the thermal diffusivity, which is subsequently used to calculate thermal conductivity. In this method, a short laser pulse is applied to heat up a specific region of the specimen, either at the lower or upper part, while the change in temperature is recorded using an infrared detector.⁹⁸ The laser pulse is directed towards a disc-shaped sample containing nanoparticles, as illustrated in Fig. 13. The thermal diffusivity (α) can be calculated using eqn (31),

$$\alpha = 0.13879 \times \frac{L^2}{t_{0.5}} \quad (31)$$

where L is the thickness of the sample, $t_{0.5}$ is the time at which temperature rises to half of its maximum value. Then using

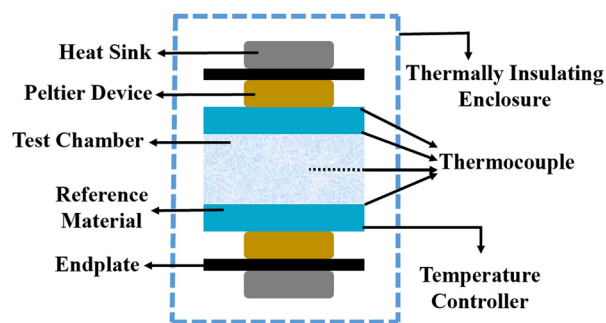


Fig. 12 Schematic diagram of the temperature oscillation technique. Adapted from ref. 96, with permission from Elsevier, Copyright 2021.



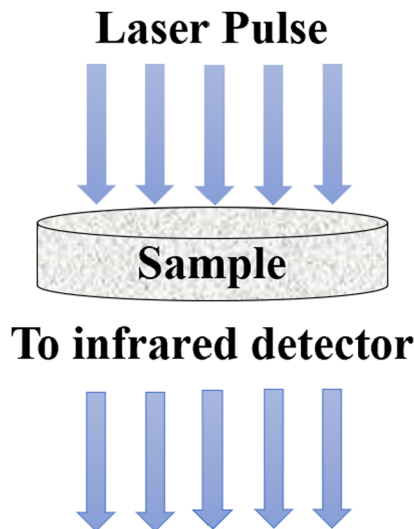


Fig. 13 Schematic diagram of the laser flash method. Adapted from Open Access data under the Creative Commons BY license from ref. 69, Copyright 2021 MDPI.

eqn (31) thermal conductivity K can be calculated using eqn (32).

$$K = \alpha \times \rho \times C_p \quad (32)$$

where ρ is the density and C_p is the specific heat capacity.

5.6 Steady-state parallel plate method

Different structures can be utilized to estimate the thermal conductivity of nanofluids based on steady-state heat conduction, where the temperature difference is constant. Two preferred structures for heat transfer measurement are the parallel plate and concentric cylindrical cells, employing the concept of heat conduction in a single direction and thermal resistance.

In the parallel plate experimental setup, a sample is inserted between copper plates, and a main heater supplies heat. After a certain time, a steady temperature is achieved by the upper and lower copper plates, allowing the calculation of the sample's thermal conductivity given a detailed description by Wang *et al.*⁹⁹ The schematic diagram of the technique is shown in

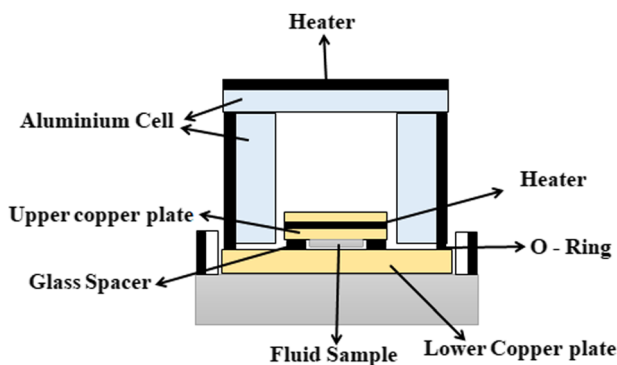


Fig. 14 Schematic diagram of the steady-state parallel plate method. Adapted from ref. 100, with permission from IOP Science, Copyright 2017.

Fig. 14 where another heater had been used to maintain the inner environment for the prevention from heat loss. This method was used to calculate the thermal conductivity of alumina and copper oxide-based nanofluids and the heat conduction in a single direction can be calculated using eqn (33),

$$K = \frac{qL_g}{S\Delta T} \quad (33)$$

where L_g denote the thickness of the glass spacer between the two copper plates and S is cross-sectional area of the upper copper plate, q represents the power of the heater and ΔT is the temperature difference between the two plates. The thermal conductivity of the nanofluid can be calculated using eqn (34).

$$K_c = \frac{KS - K_g S_g}{S - S_g} \quad (34)$$

where K_g , S , and S_g are the thermal conductivity, cross-sectional area of the upper copper plate, and the total cross-sectional area of the glass spacers, respectively.

5.7 Cylindrical cell method

The cylindrical cell method uses two concentric cylinders, similar to the parallel plates in the steady-state parallel method. A detailed description of this method can be found in the work by Kurt and Kayfeci,¹⁰¹ and the schematic diagram is shown in Fig. 15.

In this setup, a sample fluid is inserted inside the coaxial cylinder, and an electrical heater is positioned inside the cylinder to heat it up. As the temperature of the inner cylinder increases, heat flows radially outwards through the sample, which fills the annular gap between the cylinders. Two calibrated thermocouples are used to measure the outer surface temperature T_i of the glass tube and the inner cylinder temperature T_o . The thermal conductivity can then be calculated using eqn (35),

$$K_{nf} = \frac{\ln \frac{r_2}{r_1}}{2\pi L} \left[\frac{1}{\Delta T/Q_c - \ln(r_3/r_2)/2\pi L K_c} \right] \quad (35)$$

where Q_c is the heat input, and can be calculated from the current and voltage through the heater, ΔT denotes the

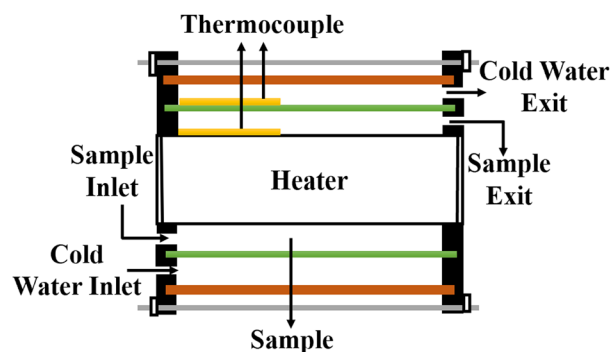


Fig. 15 Cross-section of the cylindrical cell method. Adapted from ref. 101, with permission from Elsevier, Copyright 2009.



temperature difference between T_1 and T_0 in °C, L is the length of the cylinders, r_1 is the outer glass cell, and r_2, r_3 are the inner and outer radius of the inner cylinder, respectively.

5.8 Thermal comparator method

The indirect technique, proposed by Powell *et al.*,¹⁰² is based on the principle of heat transfer from a hotter material to a colder one when they are brought into contact over a small area. The setup for this technique is shown in Fig. 16. The establishment of thermal equilibrium depends on the thermal conductivity of both materials involved. In this method, one material with a known thermal conductivity is chosen, while the other material has an unknown thermal conductivity where heat transfer occurs under steady-state conditions. Considering the flow of heat in semi-infinite bodies with the boundary conditions $0 < z < \infty$ and $-\infty < z < 0$, having an initial temperature T_0 for the material with a known thermal conductivity K_1 , and an unknown temperature T_1 for the material with thermal conductivity K_2 . By considering the boundary conditions, the relationship can be expressed as eqn (36),

$$T_1 = T_0 - \frac{2K_2T_0}{\Pi(K_1 + K_2)} \int \exp(-\lambda z) (\sin \lambda r_1) J_0(\lambda r) d\lambda / \lambda \quad (36)$$

where $J_0(\lambda r)$ is the zero order Bessel function. For $z = 0$, and $r < r_1$ the equation becomes eqn (37) for the calculation of thermal conductivity,

$$T_1(0) = \frac{T_0K_1}{K_1 + K_2} \quad (37)$$

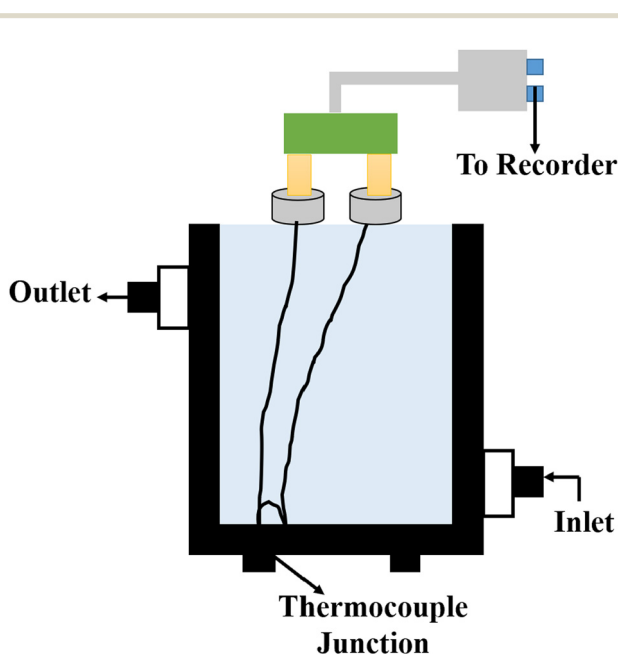


Fig. 16 Schematic diagram of the thermal comparator method. Adapted from ref. 103, with permission from the American Chemical Society, Copyright 1983.

6 Discussions and experimental results

Various approaches have been employed over the years for measuring the thermal conductivity of nanofluids, with some methods considered more sophisticated and widely accepted as standard. However, all of these methods share a common challenge: the measurements are highly sensitive to initial conditions, where minor changes can significantly impact the results. Measuring the thermal conductivity of nanomaterials is not an easy task, primarily due to the requirement for sample stability, which is influenced by factors such as material composition, temperature, and the concentration of the BF and NPs. Research has revealed that achieving sample stability can take up to a month, and ongoing maintenance is necessary to prevent sedimentation of nanoparticles.¹⁰⁴ Among the various measurement techniques reviewed, the transient hot wire method (Section 5.1) stands out as the most commonly used approach which offers good accuracy, requires no calibration, and is a simple experiment with low cost.^{105,106} Here, we provide an overview of experimental results using the laser flash method.

SEM of CuO in solar salt is shown in Fig. 17. The small and dark spots are the CuO particles spread in the salt where agglomeration of CuO particles happens in the order 100–300 nm, which is the result of natural convection taking place in the liquid phase of the salt. These particles are distributed very well in the salt and can be seen by visual inspection.

The thermal conductivity can be calculated using thermal diffusivity measured using the laser flash method (Section 5.5). The thermal conductivity results of CuO nanoparticles in solar salt are shown in Fig. 18, where incremental changes in thermal conductivity occur after mixing 2% by volume of CuO in pure NaNO₃–KNO₃ at different temperatures. Different concentrations of CuO nanoparticles enhance the thermal conductivity, although this is not significant at higher concentration due to the large error measurements.³⁴

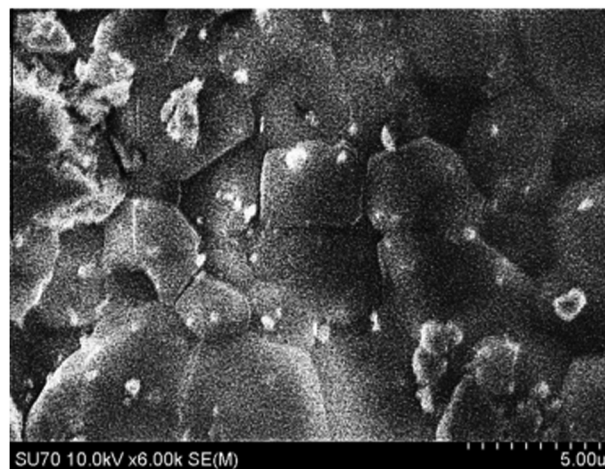


Fig. 17 SEM of CuO in solar salt. Adapted from ref. 34, with permission from Elsevier, Copyright 2016.



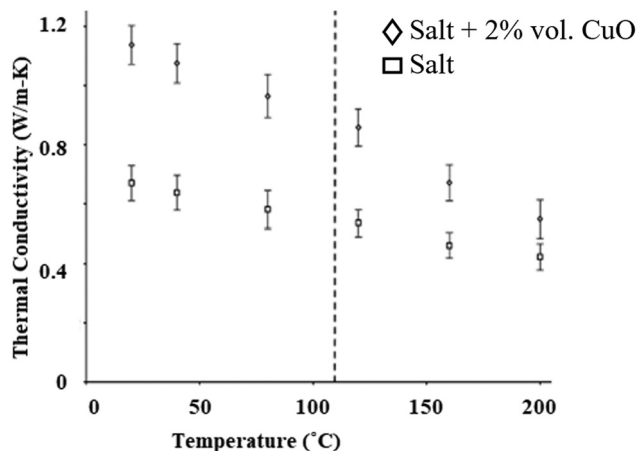


Fig. 18 Experimental data showing elevation in thermal conductivity before and after addition of CuO nanoparticles to $\text{NaNO}_3\text{-KNO}_3$. Adapted from ref. 34, with permission from Elsevier, Copyright 2016.

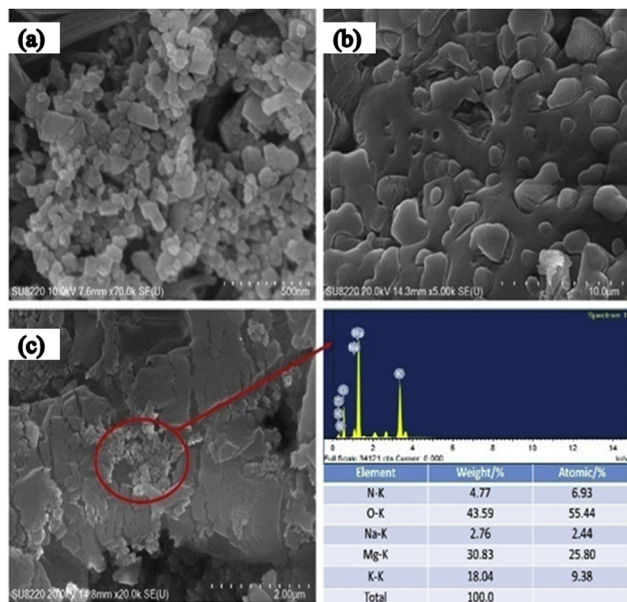


Fig. 19 SEM of MgO with solar salt: (a) shows MgO nanoparticles, (b) solar salt, and (c) MgO with solar salt at 5% concentration. Adapted from ref. 35, with permission from Elsevier, Copyright 2020.

The thermal conductivity of Al_2O_3 and TiO_2 nanoparticles have also been calculated using the laser flash method; resulting in an elevation in thermal conductivity of 8.3% and 8.1%, respectively, when adding different concentrations by mass at room temperature, which results in an increased heat transfer rate and lower melting point.³⁰

The SEM image of another metal oxide, MgO, reveals size variation from 30–60 nm, as illustrated in Fig. 19(a) and again shows the good dispersion of nanoparticles in the solar salt (Fig. 19(b) and (c)) where nano-MgO particles are surrounded by the melted solar salt forming a solid-liquid interface. MgO in solar salt enhances the thermal conductivity from 5.4% to 62.1% with mass increments of 2.5% to 5.0%, as seen in

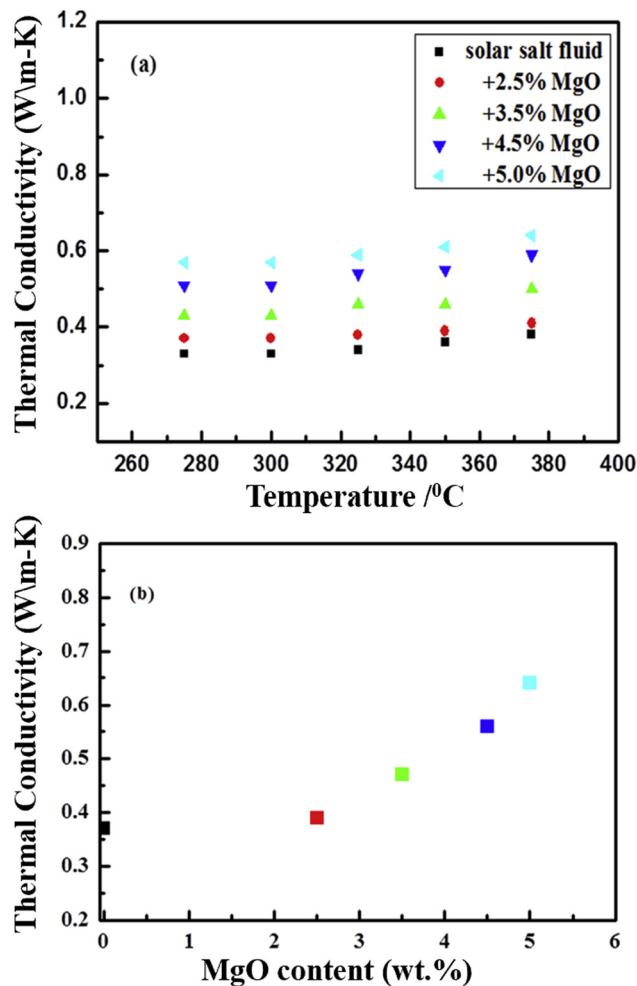


Fig. 20 Experimental data showing the thermal conductivity of $\text{NaNO}_3\text{-KNO}_3$ (a) improves with the addition of MgO at different mass concentrations (2.5%, 3.5%, 4.5% and 5%) with temperature, and (b) the increasing thermal conductivity at different concentrations. Adapted from ref. 35, with permission from Elsevier, Copyright 2020.

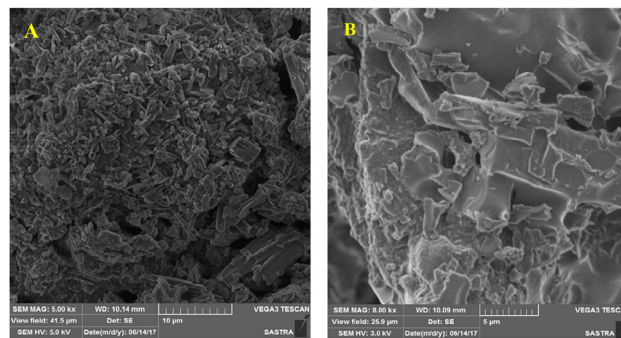


Fig. 21 SEM images of pure (A) and CNT-enhanced solar salt, and (B). Adapted from ref. 39, with permission from the American Chemical Society, Copyright 2023.

Fig. 20(b), the measurements were done using the laser flash method at 375 °C for different concentrations in pure solar salt.



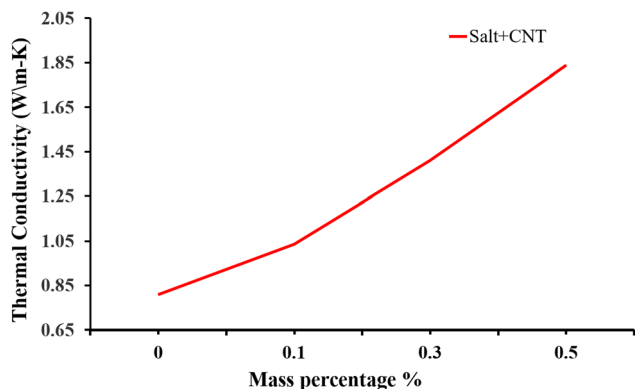


Fig. 22 Experimental data showing how the thermal conductivity of $\text{NaNO}_3\text{-KNO}_3$ improves with addition of CNT at different mass concentrations of 0.1%, 0.3% and 0.5%. Adapted from ref. 39, with permission from the American Chemical Society, Copyright 2023.

Besides metal oxides, results using CNTs as an additive in solar salt have been reported. An SEM image is shown in Fig. 21, which shows consistent CNT dispersion in $\text{NaNO}_3\text{-KNO}_3$.³⁹ The authors reported that the solar salt appeared white at room temperature, and after addition of CNTs it became darker. Addition of nanocomposite CNTs³⁹ in solar salt provides good elevation in thermal conductivity, as calculated using the laser flash method with varying mass percentage from 0.1% to 1.5% (Fig. 22). Although some calculations using theoretical models have been done, as discussed, the experimental results are very different due to different BFs, with a large difference in thermal conductivity results.¹⁰⁷ However, it is clear that the addition of nanoparticles elevates thermal conductivity and this elevation depends on the quantity of nanoparticles added.

7 Conclusions and future aspects

An improvement in the thermal conductivity of a solar salt can be observed after the addition of nanoparticles in small amounts, like 2% of CuO by volume increases the thermal conductivity by approximately 30% over the range of temperature, which is a more significant increase than when adding a higher concentration. When using Al_2O_3 and TiO_2 nanoparticles, the elevation in thermal conductivity seen is around 8.3% and 8.1%, respectively.³⁰ However as the mass concentration increases, the changes in thermal conductivity are again not that significance, as also seen in the case of CuO.³⁴ MgO nanoparticles with solar salts show good elevation even at higher concentrations of 5.4% to 62.1%, at 375 °C, but elevate the density of the nanofluid making flow difficult. In the case of CNTs, enhancement in thermal conductivity is around 27% which elevates with mass percentage. CNTs are thermally stable at 600 °C but at higher temperature mass loss rapidly occurs.³⁹

Research into latent heat increments in materials for thermal heat storage have included various experimental and theoretical models showing different outcomes and discrepancies.^{30,107,108} Issues like lack of theoretical understanding

and instrumentation errors,⁹¹ may be causing the inaccuracy in nanofluid thermal conductivity measurements. Although study results are not always consistent, some conclusions can be drawn, as follows.

- Study of thermal conductivity and the heat transfer capability of the molten salts shows that it can be increased with NP additives.
- Better characterization techniques provide insight into NP additive effects.
- Techniques for the measurement of a nanofluids' thermo-physical properties are still under development.
- Theoretical models and experimental results do not match, which may be due to negligence of various factors.
- Increments in concentration of NPs in the BF leads to agglomeration, which causes uncertainty in the measurements.
- For long durability usage of nanofluids for TES, stability is mandatory for better efficiency and repeatability.

We provide insights into thermal conductivity with respect to theoretical discussion, experimental techniques and mathematics. This will be beneficial in terms of a complete review of variation with temperature or with concentration at a particular temperature, providing the complete results on thermal conductivity enhancement of TES using nanoparticles.

Author contributions

Sanjeev Gautam: conceptualization, investigation, formal analysis, writing – review & editing, resources, funding acquisition, project administration and supervision; Monika Verma: methodology, discussions and original draft preparation; Rashi Chauhan: investigation, formal analysis and revision; Sukesh Aghara: critic discussions and supervision; Navdeep Goyal: critic discussions and supervision.

Conflicts of interest

There are no conflicts to declare.

Acknowledgements

SG acknowledges the financial support from the CSR-Industrial Research Project from Electrowaves Electronics Pvt. Ltd, Parwanoo, Himachal Pradesh-173 220, India.

Notes and references

- 1 J. Bongaarts, *Philos. Trans. R. Soc. London, Ser. B*, 2009, **364**, 2985–2990.
- 2 H. Ritchie, M. Roser and P. Rosado, *Energy*, 2022, <https://ourworldindata.org/energy>.
- 3 T. Stocker, *Climate change 2013: the physical science basis: Working Group I contribution to the Fifth assessment report of the Intergovernmental Panel on Climate Change*, Cambridge University Press, 2014.
- 4 Z. Liu, *Glob. Energy Interconnect.*, 2015, **1**, 1–64.



- 5 G. E. Iea, *CO₂ Status Report 2018*, IEA, Paris Technical Report, 2019.
- 6 A. Guizani, M. Hammadi, J.-Y. Choley, T. Soriano, M. S. Abbes and M. Haddar, *Mech. Ind.*, 2016, **17**, 405.
- 7 IEA, *Electricity Market Report*, IEA Technical Report, 2021.
- 8 A. Stepanovich, Doctoral thesis, Ruhr-Universität Bochum, Universitätsbibliothek, 2014.
- 9 A. B. Awan, M. Zubair, R. Praveen and A. R. Bhatti, *Sol. Energy*, 2019, **183**, 551–565.
- 10 U. Herrmann and D. W. Kearney, *J. Sol. Energy Eng.*, 2002, **124**, 145–152.
- 11 J. F. Kreider, *Solar heating design process: active and passive systems*, OSTI, 1982.
- 12 E. B. Kapstein, *A Golden Thread: 2500 Years of Solar Architecture and Technology*, 1980.
- 13 L. R. Cirocco, M. Belusko, F. Bruno, J. Boland and P. Pudney, *IET Renew. Power Gen.*, 2015, **9**, 379–388.
- 14 S. Manju and N. Sagar, *Renewable Sustainable Energy Rev.*, 2017, **70**, 298–313.
- 15 W. Fuqiang, C. Ziming, T. Jianyu, Y. Yuan, S. Yong and L. Linhua, *Renewable Sustainable Energy Rev.*, 2017, **79**, 1314–1328.
- 16 A. Ummadisingu and M. Soni, *Renewable Sustainable Energy Rev.*, 2011, **15**, 5169–5175.
- 17 A. Kumar, O. Prakash and A. Dube, *Renewable Sustainable Energy Rev.*, 2017, **79**, 304–307.
- 18 S. Hasnain, *Energy Convers. Manage.*, 1998, **39**, 1127–1138.
- 19 X. Xu, K. Vignarooban, B. Xu, K. Hsu and A. M. Kannan, *Renewable Sustainable Energy Rev.*, 2016, **53**, 1106–1131.
- 20 W. Ruidong and M. Jun, *IOP Conf. Ser.: Earth Environ. Sci.*, 2021, **vol. 687**, p. 012088.
- 21 J. Len, J. Fernandez and M. Berenguel, *et al.*, *J. Process Control*, 2019, **85**, 76–90.
- 22 EASAC, *Concentrating solar power plant: its potential contribution to a sustainable energy future*, European Academics Science Advisory Council Technical Report, 2011.
- 23 G. Paul, M. Chopkar, I. Manna and P. Das, *Renewable Sustainable Energy Rev.*, 2010, **14**, 1913–1924.
- 24 E. González-Roubaud, D. Pérez-Osorio and C. Prieto, *Renewable Sustainable Energy Rev.*, 2017, **80**, 133–148.
- 25 K. Vignarooban, X. Xu, A. Arvay, K. Hsu and A. M. Kannan, *Appl. Energy*, 2015, **146**, 383–396.
- 26 A. Gautam and R. Saini, *J. Energy Storage*, 2022, **48**, 103993.
- 27 J. E. Pacheco and R. Gilbert, *Overview of recent results of the solar two test and evaluations program*, Sandia National Labs., Albuquerque, NM (US) Technical Report, 1999.
- 28 H. Reilly and G. Kolb, *SAND: Sandia National Laboratories*, 2001, p. 3674.
- 29 U. Nithyanantham, L. González-Fernández, Y. Grosu, A. Zaki, J. M. Igartua and A. Faik, *Appl. Therm. Eng.*, 2020, **169**, 114942.
- 30 T. Raja Jeyaseelan, N. Azhagesan and V. Pethurajan, *J. Therm. Anal. Calorim.*, 2019, **136**, 235–242.
- 31 S. Ferrouillat, A. Bontemps, O. Poncet, O. Soriano and J.-A. Gruss, *Appl. Therm. Eng.*, 2013, **51**, 839–851.
- 32 J. Singh, G. Kaur and M. Rawat, *J. Bioelectron. Nanotechnol.*, 2016, **1**, 1–9.
- 33 Ç. Oruç and A. Altndal, *Ceram. Int.*, 2017, **43**, 10708–10714.
- 34 P. D. Myers Jr, T. E. Alam, R. Kamal, D. Goswami and E. Stefanakos, *Appl. Energy*, 2016, **165**, 225–233.
- 35 X. Wei, Y. Yin, B. Qin, W. Wang, J. Ding and J. Lu, *Renewable Energy*, 2020, **145**, 2435–2444.
- 36 Q. Wang, C. Wu, X. Wang, S. Sun, D. Cui, S. Pan and H. Sheng, *Int. J. Heat Mass Transfer*, 2023, **205**, 123904.
- 37 H. Badenhorst, *Sol. Energy*, 2019, **192**, 35–68.
- 38 B. Jo and D. Banerjee, *Int. J. Therm. Sci.*, 2015, **98**, 219–227.
- 39 P. Vigneshwaran, S. Shaik, S. Suresh, M. Abbas, C. A. Saleel and E. Cuce, *ACS Omega*, 2023, **8**(20), 17563–17572.
- 40 B. Ma and D. Banerjee, *AIP Adv.*, 2017, **7**, 115124.
- 41 J. Pearce, *Int. J. Med.*, 2002, **95**, 251–252.
- 42 A.-L. Lavoisier and P. DeLaplace, *Obes. Res.*, 1994, **2**, 189–202.
- 43 J. H. Lambert, *Pyrometrie oder vom Maaße des Feuers und der Wärme*, bey Haude und Spener, 1779.
- 44 B. Franklin, *Science*, 1956, **123**, 47–50.
- 45 J. Ingen-Housz, *Nouvelles expériences et observations sur divers objets de physique*, Th. Barrois, 1785, vol. 1.
- 46 C. Rumford, *The Collected Works of Count Rumford*, Harvard University Press, 1968, vol. 5.
- 47 J. B. J. Baron Fourier, *The analytical theory of heat*, The University Press, 1878.
- 48 T. Narasimhan, arXiv, 2010, preprint, arXiv:1005.2119.
- 49 G.-H. Kim, D. Lee, A. Shanker, L. Shao, M. S. Kwon, D. Gidley, J. Kim and K. P. Pipe, *Nat. Mater.*, 2015, **14**, 295–300.
- 50 K. Wark and D. E. Richards, *et al.*, *Termodinámica*, McGraw-Hill Madrid, Spain, 2001.
- 51 R. Serrano-López, J. Fradera and S. Cuesta-López, *Chem. Eng. Process.*, 2013, **73**, 87–102.
- 52 D. C. P. Grogan, *Development of Molten-Salt Heat Transfer Fluid Technology for Parabolic Trough Solar Power Plants – Public Final Technical Report*, Abengoa solar, llc technical report, US Department of Energy, 2013.
- 53 D. Kearney, U. Herrmann, P. Nava, B. Kelly, R. Mahoney, J. Pacheco, R. Cable, N. Potrovitza, D. Blake and H. Price, *et al.*, *J. Sol. Energy. Eng.*, 2003, **125**, 170–176.
- 54 P. K. Das, *J. Mol. Liq.*, 2017, **240**, 420–446.
- 55 J. C. Maxwell, *Treatise on electricity and magnetism*, Hanserbooks, 2016.
- 56 B. Lamas, B. Abreu, A. Fonseca, N. Martins and M. Oliveira, *Int. J. Therm. Sci.*, 2014, **78**, 65–76.
- 57 E. J. Wasp, *Solid-liquid flow slurry pipeline transportation*, Trans. Tech. Publ., 1977.
- 58 Y. Xuan, Q. Li and W. Hu, *AIChE J.*, 2003, **49**, 1038–1043.
- 59 J. Koo and C. Kleinstreuer, *J. Nanopart. Res.*, 2004, **6**, 577–588.
- 60 H. Xie, M. Fujii and X. Zhang, *Int. J. Heat Mass Transfer*, 2005, **48**, 2926–2932.
- 61 J. Avsec and M. Oblak, *Int. J. Heat Mass Transfer*, 2007, **50**, 4331–4341.
- 62 S. Pil Jang and S. U. S. Choi, *J. Heat Transfer*, 2007, **129**, 617–623.



- 63 B. C. Pak and Y. I. Cho, *Exp. Heat Transfer*, 1998, **11**, 151–170.
- 64 E. V. Timofeeva, D. S. Smith, W. Yu, D. M. France, D. Singh and J. L. Routbort, *Nanotechnology*, 2010, **21**, 215703.
- 65 W. Yu and S. Choi, *J. Nanopart. Res.*, 2003, **5**, 167–171.
- 66 W. Wei, *et al.*, *J. Adv. Res. Phys.*, 2017, **3**(2), 021209.
- 67 M. Chandrasekar, S. Suresh, R. Srinivasan and A. C. Bose, *J. Nanopart. Nanotechnol.*, 2009, **9**, 533–538.
- 68 M. Corcione, *Energy Convers. Manage.*, 2011, **52**, 789–793.
- 69 I. Gonçalves, R. Souza, G. Coutinho, J. Miranda, A. Moita, J. E. Pereira, A. Moreira and R. Lima, *Appl. Sci.*, 2021, **11**, 2525.
- 70 D. W. Hahn and M. N. Özisik, *Heat conduction*, John Wiley & Sons, 2012.
- 71 M. L. Ramires, C. A. Nieto de Castro, Y. Nagasaka, A. Nagashima, M. J. Assael and W. A. Wakeham, *J. Phys. Chem. Ref. Data*, 1995, **24**, 1377–1381.
- 72 D. W. G. Ballentyne and D. R. Lovett, *A dictionary of Named effects and laws of Chemistry, physics and mathematics*, Springer Netherlands, Dordrecht, 1980, pp. 200–217.
- 73 L. Wei, P. Kuo, R. Thomas, T. Anthony and W. Banholzer, *Phys. Rev. Lett.*, 1993, **70**, 3764.
- 74 T. Ambreen and M.-H. Kim, *Appl. Energy*, 2020, **264**, 114684.
- 75 J. Xu, B. Yu, M. Zou and P. Xu, *J. Phys. D: Appl. Phys.*, 2006, **39**, 4486.
- 76 K. Anoop, T. Sundararajan and S. K. Das, *Int. J. Heat Mass Transfer*, 2009, **52**, 2189–2195.
- 77 M. H. Esfe, S. Esfandeh, M. Afrand, M. Rejvani and S. H. Rostamian, *Appl. Therm. Eng.*, 2018, **133**, 452–463.
- 78 S. Jana, A. Salehi-Khojin and W.-H. Zhong, *Thermochim. Acta*, 2007, **462**, 45–55.
- 79 S. H. Rostamian, M. Biglari, S. Saedodin and M. H. Esfe, *J. Mol. Liq.*, 2017, **231**, 364–369.
- 80 C. H. Chon, K. D. Kihm, S. P. Lee and S. U. Choi, *Appl. Phys. Lett.*, 2005, **87**, 153107.
- 81 H. A. Mintsu, G. Roy, C. T. Nguyen and D. Doucet, *Int. J. Therm. Sci.*, 2009, **48**, 363–371.
- 82 W. Duangthongsuk and S. Wongwises, *Exp. Therm. Fluid Sci.*, 2009, **33**, 706–714.
- 83 C. T. Wamkam, M. K. Opoku, H. Hong and P. Smith, *J. Appl. Phys.*, 2011, **109**, 024305.
- 84 B. Wright, D. Thomas, H. Hong, L. Groven, J. Puszynski, E. Duke, X. Ye and S. Jin, *Appl. Phys. Lett.*, 2007, **91**, 173116.
- 85 D. Elcock, *Potential impacts of nanotechnology on energy transmission applications and needs*, Argonne national lab.(anl), argonne, il (united states) technical report, 2007.
- 86 J. Philip and P. D. Shima, *Adv. Colloid Interface Sci.*, 2012, **183**, 30–45.
- 87 A. Asadi, M. Asadi, M. Siahmargoi, T. Asadi and M. G. Andarati, *Int. J. Heat Mass Transfer*, 2017, **108**, 191–198.
- 88 G. Xu, J. Fu, B. Dong, Y. Quan and G. Song, *Int. J. Heat Mass Transfer*, 2019, **130**, 978–988.
- 89 J. Horrocks and E. McLaughlin, *Proc. R. Soc. London, Ser. A*, 1963, **273**, 259–274.
- 90 H. S. Carslaw and J. C. Jaeger, *Conduction of heat in solids*, Clarendon Press, Technical Report, 1959.
- 91 L. Qiu, N. Zhu, Y. Feng, E. E. Michaelides, G. Żyła, D. Jing, X. Zhang, P. M. Norris, C. N. Markides and O. Mahian, *Phys. Rep.*, 2020, **843**, 1–81.
- 92 Y. Xuan and Q. Li, *Int. J. Heat Fluid Flow*, 2000, **21**, 58–64.
- 93 J. G. Bleazard and A. S. Teja, *J. Chem. Eng. Data*, 1995, **40**, 732–737.
- 94 A. A. Guermoudi, P. Y. Cresson, A. Ouldabbes, G. Boussatour and T. Lasri, *J. Therm. Anal. Calorim.*, 2021, **145**, 1–12.
- 95 D. G. Cahill, *Rev. Sci. Instrum.*, 1990, **61**, 802–808.
- 96 P. Bhattacharya, S. Nara, P. Vijayan, T. Tang, W. Lai, P. Phelan, R. Prasher, D. Song and J. Wang, *Int. J. Heat Mass Transfer*, 2006, **49**, 2950–2956.
- 97 S. K. Das, N. Putra, P. Thiesen and W. Roetzel, *J. Heat Transfer*, 2003, **125**, 567–574.
- 98 B. Lin, H. Ban, C. Li, R. N. Scripa, C.-H. Su and S. L. Lehoczky, *ASME International Mechanical Engineering Congress and Exposition*, 2005, pp. 725–730.
- 99 X. Wang, X. Xu and S. U. Choi, *J. Thermophys. Heat Transfer*, 1999, **13**, 474–480.
- 100 T. T. Loong and H. Salleh, *IOP Conf. Ser.: Mater. Sci. Eng.*, 2017, **vol. 226**, p. 012146.
- 101 H. Kurt and M. Kayfeci, *Appl. Energy*, 2009, **86**, 2244–2248.
- 102 R. Powell, *J. Sci. Instrum.*, 1957, **34**, 485.
- 103 A. A. Rousan and D. M. Roy, *Ind. Eng. Chem. Prod. Res. Dev.*, 1983, **22**, 349–351.
- 104 S. Ganguly and S. Chakraborty, *Phys. Lett. A*, 2011, **375**, 2394–2399.
- 105 S. Lee, S.-S. Choi, S. Li and J. Eastman, *J. Heat Transfer*, 1999, **121**(2), 280–289.
- 106 J. Magnusson, M. Memmott and T. Munro, *Ann. Nucl. Energy*, 2020, **146**, 107608.
- 107 S. M. Mamand, *Appl. Sci.*, 2021, **11**, 1459.
- 108 D. Ceotto and V. Y. Rudyak, *Colloid J.*, 2016, **78**, 509–514.

