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# Enabling high performance n-type metal oxide semiconductors at low temperatures for thin film transistors

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Amorphous oxide semiconductors have drawn considerable attention as a replacement for ubiquitous silicon based technologies. By virtue of their flexible substrate compatibility and transparency, amorphous metal oxide semiconductor (AOS) thin film transistors (TFTs) are being explored in emerging flexible/ transparent technologies. However, rapid advances in such technologies require the development of high-performance thin film transistors, which can be fabricated at low processing temperatures. In this review paper, we discuss the recent progress made in n-type semiconductor TFTs activated at low temperatures both on rigid and flexible substrates with a focus on the replacement of conventional high temperature annealing. Several low temperature processing approaches that have been reported in both vacuum deposited and solution processed n-type metal oxide semiconductor based thin film transistors are evaluated, with an emphasis on some novel techniques which can effectively modulate the electronic properties of the n-type metal oxide semiconductor systems at low temperatures. The final part of this review draws conclusions and discusses the outlook for future research efforts in achieving low temperature activated high performance n-type TFTs.

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## 1. Introduction

Thin-film transistors (TFTs) have been the focus of intense worldwide research during the past decade, and have emerged as fundamental building blocks for optoelectronic devices such as flat-panel displays, liquid crystal displays (LCDs) and active matrix organic light emitting diodes (AMOLEDs),



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and dielectrics and 2D composites for thin film transistor applications.

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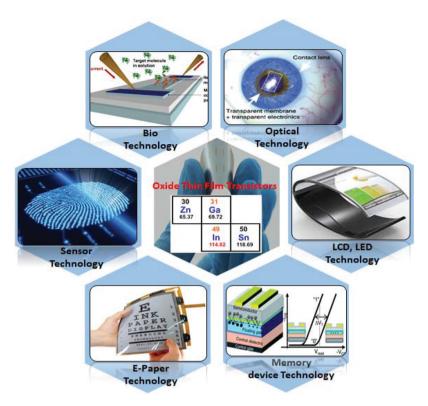


Fig. 1 Metal oxides for thin film transistors and their applications in flexible electronics.

wherein they perform a critical function in display operation. 1-5 With the display technology's insatiable demand for higher resolution, larger screen size, lower power consumption and reduced costs, a-Si thin-film transistors have been challenged by low-temperature polycrystalline silicon and metal-oxide TFTs. In comparison with low-temperature poly-Si (LTPS) TFTs, metal oxide TFTs present inherent advantages such as improved large-area uniformity and considerably lower manufacturing cost, while maintaining high carrier mobility,

good transparency and reasonable electrical reliability/ stability.<sup>6,7</sup> By virtue of their flexible substrate compatibility and transparency, amorphous metal oxide semiconductor (AOS) TFTs are of interest in emergent technologies such as flexible displays, flexible transparent circuitry, electronic skin, smart contact lenses and flexible neuromorphic devices (Fig. 1).8,9 Metal oxide (MO) semiconductors contain heavy post-transition metal cations with (n-1) d<sup>10</sup>ns<sup>0</sup>  $(n \ge 5)$  electronic configurations, where the large radii of the metal ns



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temperature sensors, mechanical energy harvesting, and neuromorphic electronic devices.



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orbitals lead to adjacent orbital overlap and consequently result in a high degree of wave-function overlap, electron delocalization, and relatively high electron mobility, independent of the microstructure. As a result, they retain relatively high electron mobility even in the amorphous state, thus making them an ideal material for high throughput and low cost manufacturing processes.10 Deposition of these thin films is achieved by using either vacuum techniques such as sputtering, atomic layer deposition (ALD) etc. or ambient pressure solution-processed TFTs requiring relatively higher processing temperatures (temperature >350 °C) for optimum film formation, densification, and impurity removal. Oxide semiconductor thin films formed at low temperatures exhibit poor electrical characteristics due to the presence of numerous defects and impurities and the high temperature post-deposition annealing aids in modulating their electronic properties for the fabrication of high performance thin film transistors.<sup>3,6</sup> Recently significant effort has been expended to explore new materials compositions and novel processing methodologies to improve the electronic transport in metal oxides, and to lower the processing temperature for compatibility with lowcost and flexible polymer substrate materials.8 New alternatives for activation/improvement of the properties of oxide thin film transistors are also being concurrently explored, with the research focus currently leaning towards oxygen vacancy modulation of MO semiconductors.3,8 Metal oxide semiconductors for thin film transistors have been reviewed previously. 3,8,11,12 Among these, majority of the reviews that focus on low temperature processing dealt with solution processed metal oxide systems. In this review, we discuss low temperature fabrication of metal oxide TFTs (≤300 °C) using both solution and vacuum processing. In addition to reviewing the prevalent low temperature methods such as photoactivation, microwave and combustion synthesis etc. which have



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been reviewed previously, 3,8,11,12 we also explore and analyze more unconventional athermal methods such as capping layer and electric field driven approaches which have been recently reported to result in high performance devices.

Electronic structure modulation: In 1996, Hosono et al. proposed a multicomponent combination of cations for the design of an amorphous metal oxide semiconductor. The selected cations possess conduction bands derived from large ionic-radius, spherically symmetric 4s, 5s, or 6s electron orbitals from the portion of the periodic table shown in the inset of Fig. 1. Since then, there have been many metal oxide semiconductor trials with the most prevalent ones involving indium (In), tin (Sn), zinc (Zn), and gallium (Ga) as AOS design starting points. This is because their binary oxides such as indium oxide (In<sub>2</sub>O<sub>3</sub>), tin-oxide (SnO<sub>2</sub>), and zinc oxide (ZnO) are the three most commonly used transparent conducting oxides (TCOs). These materials have wide band gaps ( $E_{g} > 3$ eV), high transparency (>80%) and high electrical conductivity. Additionally, they retain relatively high electron mobility even in the amorphous state and are hence widely considered as the base materials for amorphous MO semiconductors. The small effective masses and corresponding relatively high mobility of these oxides are valued for both TCO and AOS applications. However, these materials suffer from very high carrier concentrations, non-uniformity and high leakage currents. These issues were addressed by mixing two or more metal cations to form ternary or quaternary systems, to boost the formation of amorphous films, thereby reducing the carrier concentration and decreasing the grain boundaries present in polycrystalline samples. 10 For MO TFTs to exhibit a low  $I_{\text{off}}$ , high  $I_{\text{on}}$  and stable performance, it is imperative to limit the semiconductor carrier concentration to a low level, preferably <10<sup>17</sup> cm<sup>-3</sup>. 10,14 In the case of binary or ternary MO systems, moderate n-type doping can be controlled by the cation/anion non-stoichiometry or process optimization. An alternative approach is to introduce an extra component, such as a carrier suppressor (a dopant). The primary requirements for dopants are the following: (i) M-O bond strength should be higher than that of the matrix metal ion; (ii) dopant size should be smaller than the matrix host metal ion size; else the dopant will act as a defect site;15 (iii) high Lewis acid strength, since it results in higher mobility via suppression of scattering by oxygen interstitials;<sup>16</sup> and (iv) an appropriate concentration of the dopant to ensure accurate control of the oxygen vacancies without a significant decrease in the mobility. Various elements such as gallium (Ga), tungsten (W), silicon (Si), hafnium (Hf), zirconium (Zr), titanium (Ti), aluminum (Al) and tantalum (Ta) have been studied and shown to exhibit carrier suppressor behavior. 16 Therefore, the cation composition can be modified to improve the stability of transparent metal oxide (TMO) TFTs under bias and illumination stress. In addition, incorporation of nitrogen into the binary systems also appears to suppress the growth of indium oxide and zinc oxide resulting in a nanostructured phase.<sup>14</sup> The substitution of an oxygen anion with a nitrogen anion effectively passivates the Vo sites in ZnO and In2O3 by eliminating the oxygen deficiency related deep levels near the

valence band maximum, thereby improving the photo-bias stability. 14,17

Processing methods: Electronic and optoelectronic devices based on metal oxides usually comprise thin films deposited on appropriate substrates. High-quality metal oxide networks can be obtained by using extremely controlled deposition processes such as pulsed laser deposition (PLD) and atomic layer deposition (ALD) and even by using less sophisticated methods such as radiofrequency (RF) magnetron sputtering as depicted in Fig. 2a-c. These techniques permit the growth of high-quality uniform thin films with atomic layer precision.<sup>18</sup> Solution processing is another widely adopted method for fabricating MO films for TFT applications and is appealing in terms of its low cost, scalability and compatibility with high throughput manufacturing. Fig. 2d illustrates the stages involved in solution processing, namely, the synthesis of the

solution, deposition of the solution on substrates and pyrolysis or condensation for MO formation. The evolution of the film as it proceeds through these stages is also illustrated. The various deposition techniques employed, such as spin-coating, inkjet printing and spray coating, are presented in Fig. 2e. The nanoparticle route and precursor route are two widely adopted approaches for the synthesis of the solution for metal oxide film formation. The nanoparticle route is a straightforward approach wherein a metal oxide nanoparticle dispersion in appropriate solvent is deposited on the substrate. The evolution of metal oxide films deposited through the precursor route is depicted in Fig. 2f, where the metal cation complexes formed by the solvation of metal precursors undergo hydrolysis and condensation reactions to form a metal-oxide (M-O) network. Although the nanoparticle approach seems advantageous in terms of low temperature processing, the inherent

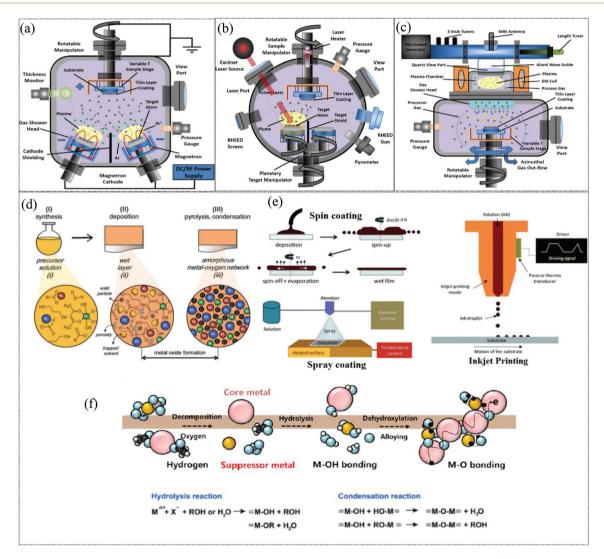


Fig. 2 Low-cost deposition techniques used to produce electronic devices based on semiconducting metal oxides. (a) RF magnetron sputtering, (b) pulsed laser deposition (PLD), (c) atomic layer deposition (ALD) (reproduced from ref. 18), (d) stages of solution processing of metal oxide films (reproduced from ref. 168), (e) deposition techniques (reproduced from ref. 168), and (f) a schematic of the evolution of metal oxide films through precursor route film deposition and subsequent annealing (reproduced from ref. 21).

porous nature affects the film quality and the particle boundaries limit charge transport which severely impair the device characteristics of the fabricated TFTs. 19-21 In comparison, the precursor route aids in the formation of denser, grain boundary-free MO films with lower surface roughness. However, it needs to be noted that high temperature annealing is generally a prerequisite for the formation of high-quality metal oxide films for effective and complete hydrolysis, condensation and densification reactions which are imperative for the formation of M-O-M networks and for the removal of organic residues.

Table 1 summarizes the recent progress made on n-type metal oxide TFTs processed at temperatures below 300 °C. The table lists a selection of MO TFTs fabricated on rigid substrates, which is further divided into TFTs that use a SiO2 dielectric and those employing high-k dielectrics. The table also lists a selection of MO TFTs fabricated on flexible substrates. The technique used for MO film formation and the processing and post-processing annealing temperatures (where applicable) are listed for each, together with the important figures of merit of TFT performance (the mobility and on/off ratio). The materials are listed in the order of binary, ternary and quaternary metal oxide systems with the TFT reports. In general, the following observations can be made: (i) mobilities above 10 can be achieved in metal oxide TFTs even at low processing temperatures, (ii) TFT performance is more robust on rigid substrates when compared to those on flexible substrates, (ii) vacuum processed metal oxide films are superior in quality and hence lead to overall enhanced device characteristics and (iv) high-k dielectrics with their higher gate capacitance and interface quality result in devices with high mobility at low operation voltages.

# Low-temperature route for n-type metal oxide semiconductors

Previous studies have proven that MO films annealed at high temperature (>400 °C) exhibited good TFT device characteristics. However, low-temperature processing (≤350 °C) is indispensable for realizing AOS TFTs for flexible electronic applications and a low thermal budget post-deposition annealing (PDA) process is required to minimize the production cost. In this context, conventional thermal annealing (CTA), which has been generally adopted for the PDA process, is disadvantageous in terms of the duration and high thermal budget required. Herein we discuss the various approaches reported, broadly divided into physical and chemical routes to reduce the processing temperature for the fabrication of metal oxide based TFTs.

## 2.1 Physical routes for the reduction of process temperature

2.1.1 High pressure annealing. High pressure annealing (HPA), has been recently reported as a promising alternative to CTA for the formation of high-quality metal oxide films. HPA is effective in the activation of sputtered films, as in the case of IGZO reported by Kim et al. 110 The mechanism of activation

by employing N2 and O2 high pressure activation is illustrated in Fig. 3a. Here, the temperature necessary for activation was reduced from 300 to 100 °C with the incorporation of HPA in N<sub>2</sub> and O<sub>2</sub> gases, where the kinetic energy of the gas molecules provides the activation energy required, while the incorporation of O<sub>2</sub> gas provides the additional benefit of elevating the metal oxide construction by ensuring sufficient ns metal orbital overlap for efficient charge transport while simultaneously reducing the electron trap density at lower pressure as is evident in Fig. 3b. This results in TFTs with higher bias stress stability and higher mobility (~11 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>) at a low temperature of 100 °C compared to TFTs annealed at 300 °C. In the case of solution processed metal oxide films, HPA requires lower fabrication temperature compared to CTA methods as it reduces the Gibbs free energy and decomposition temperature for the formation of the metal oxide network, with minimal organic residues. 111 In addition, employing HPA also produces denser MO films due to the drastic reduction of porosity, a bane, especially for low temperature solution processed MO films (Fig. 3). Definitive work on HPA annealing has been done by Kim et al. and in 2012 they demonstrated a solution processed IZO TFT on a polyimide (PI) substrate subjected to 1 MPa HPA under an O2 atmosphere at 220 °C. 112 The reduced bulk defects and charge traps provided by HPA also resulted in more stable devices as indicated by the positive bias stress with the lowest  $V_{\rm th}$  shift obtained for 1 MPa O2 HPA. In addition to activation, HPA can also be utilized as a post-treatment for activated films, as the process can assist in improving the electrical stability of TFTs through defect passivation and enhanced densification of metal oxide films. However, HPA requires a long duration of treatment (~1 h) and a specialized O2/N2 environment under high pressure conditions which could hamper widespread industrial applications. Though promising as a CTA replacement, the scalability issues of utilizing HPA for metal oxide layer activation for TFT applications need to be addressed as a facile integration of this activation method into a roll-to-roll production process flow will be challenging.

2.1.2 Microwave annealing approach. The microwave assisted annealing (MWA) technique has attracted significant attention due to the volumetric heating involved, which directly and uniformly delivers thermal energy to the MO film, while enabling a low thermal budget and fast processing, primarily due to the short exposure duration. 70,113-117 In principle, microwaves compromise with rapid changes in electric and magnetic fields as well (Fig. 4a). The microwave will heat any material with mobile electric charges such as ions in dielectrics. For example, polar solvents are heated due to the interaction of the time varying fields with the polar molecules. As a result, the polar molecules tend to vibrate with the fields and lose energy in collisions. Charges such as ions or electrons within the semiconducting and conducting materials constitute the electric current in response to the field and the resulting loss in energy through resistive heating and dielectric relaxation of the materials. In particular, the resistive heating/ ohmic loss dominates at lower frequencies (<10 GHz). Thus

Table 1 n-Type TFTs processed at low temperature

Material   Technique   C <sub>10p</sub> /T <sub>prov</sub>   PC    Substrate   Delectric   Mobility (m² V-¹ s² )   Oxforf art		s on rigid substrates						
1720	Material	Technique	$(T_{\text{dep.}}/T_{\text{post.}})/(^{\circ}\text{C})$		Dielectric	Mobility (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	On/off ratio	
WOO   Sputtering   150   Silicon   SiO <sub>2</sub>   39   10 <sup>10</sup>   WO   Sputtering   100   Silicon   SiO <sub>2</sub>   27.55   10 <sup>2</sup>   WO   Sputtering   100   Silicon   SiO <sub>2</sub>   27.55   10 <sup>2</sup>   WO   Sputtering   100   Silicon   SiO <sub>2</sub>   27.72   10 <sup>2</sup>   WO   Sputtering   300   Silicon   SiO <sub>2</sub>   27.22   10 <sup>2</sup>   WO   Sputtering   300   Silicon   SiO <sub>2</sub>   27.23   10 <sup>2</sup>   WO   Sputtering   300   Silicon   SiO <sub>2</sub>   27.24   10 <sup>2</sup>   WO   Sputtering   150/new   Silicon   SiO <sub>2</sub>   27.38   10 <sup>2</sup>   10 <sup>2</sup>   WO   Sputtering   150/new   Silicon   SiO <sub>2</sub>   11.22   10 <sup>2</sup>   GEO   Sputtering   R7/350   Silicon   SiO <sub>2</sub>   11.2   10 <sup>2</sup>   GEO   Sputtering   R7/350   Silicon   SiO <sub>2</sub>   11.2   10 <sup>2</sup>   GEO   Sputtering   R7/350   Silicon   SiO <sub>2</sub>   9.21   WO   WO   Sputtering   22.5   Silicon   SiO <sub>2</sub>   20.65   10 <sup>2</sup>   WO   WO   Sputtering   22.5   Silicon   SiO <sub>2</sub>   20.65   10 <sup>2</sup>   WO   WO   Sputtering   -1 Glass   SiO <sub>2</sub>   20.65   10 <sup>2</sup>   Glass   SiO <sub>2</sub>   24.6   10 <sup>4</sup>   WO   Sputtering   -1 Glass   SiO <sub>2</sub>   24.6   10 <sup>4</sup>   WO   Sputtering   -1 Glass   SiO <sub>2</sub>   48.4   10 <sup>2</sup>   WO   Sputtering   300   Silicon   SiO <sub>2</sub>   9.55   10 <sup>2</sup>   WO   SiO <sub>2</sub>   ALD   Sputtering   300   Silicon   SiO <sub>2</sub>   9.55   10 <sup>2</sup>   WO   SiO <sub>2</sub>   ALD   WO   SiO <sub>2</sub>   MICO   48.4   10 <sup>2</sup>   WO   SiO <sub>2</sub>   ALD   WO   SiO <sub>2</sub>   MICO   48.4   10 <sup>2</sup>   WO   SiO <sub>2</sub>   ALD   WO   SiO <sub>2</sub>   MICO   48.4   10 <sup>2</sup>   WO   SiO <sub>2</sub>   MICO   MICO   48.4   10 <sup>2</sup>   WO   SiO <sub>2</sub>   MICO   MI							$10^4$	2
WOO   Sputtering   100   Silicon   SiO <sub>2</sub>   36.7   107							1010	2
WOWNOWNON   Sputtering   100   Silicon   SiO_2   27.55   10 <sup>8</sup>							1010	2
								2
NEXPO   Sputtering   300   Silicon   SiO <sub>2</sub>   22.30   10 <sup>8</sup>	WO		100	Silicon		27.55		2
WZO   Sputtering   300   Silicon   Silo_2   22.30   10 <sup>8</sup>	WO/IWO:N	Sputtering	100	Silicon	$SiO_2$	27.2	$10^{7}$	2
IZIO	WZO		300	Silicon	SiO <sub>2</sub>	22.30	$10^{8}$	2
GZO	ZTO		180/350	Silicon		27.8	$10^{11}$	2
GZO	GZO	ALD	-/250	Silicon		22.1	10 <sup>8</sup>	3
1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500   1500							10 <sup>9</sup>	3
100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100								3
March   Marc								3
MZO   Sputtering   225   Silicon   SiO <sub>2</sub>   20.65   107							10	3
AIZO   Sputtering   FT   Glass   SiO <sub>2</sub>   5.67   10 <sup>6</sup>     TIO/AIZO   Sputtering   Light irradiation   Silicon   SiO <sub>2</sub>   48.4   10 <sup>6</sup>     TIO/AIZO   Sputtering   Light irradiation   Silicon   SiO <sub>2</sub>   48.4   10 <sup>6</sup>     TIO/AIZO   Sputtering   180   Silicon   SiO <sub>2</sub>   48.4   10 <sup>6</sup>     SiO <sub>2</sub>   Sputtering   180   Silicon   HfO <sub>2</sub>   92   10 <sup>6</sup>     SiO <sub>2</sub>   Sputtering   180   Silicon   HfO <sub>2</sub>   92   10 <sup>6</sup>     Mi,O <sub>2</sub>   ALD   160/300   Silicon   Al,O <sub>2</sub>   7.8   10 <sup>7</sup>     Mi,O <sub>3</sub>   ALD   -1/200   Silicon   Al,O <sub>2</sub>   7.8   10 <sup>7</sup>     TIO   ALD   -1/200   Silicon   Al,O <sub>2</sub>   7.8   10 <sup>7</sup>     TIO   Sputtering   300   Glass   SiN,/PiSiO <sub>2</sub>   50.4   10 <sup>10</sup>     TIO   Sputtering   300   Glass   SiN,/SiO <sub>2</sub>   41.8   10 <sup>7</sup>     TIO   Sputtering   300   Silicon   SiO <sub>2</sub>   14.0   10 <sup>10</sup>     TIO   Sputtering   300   Silicon   SiO <sub>2</sub>   14.0   10 <sup>10</sup>     TIO   Sputtering   250   Glass   Al,O <sub>2</sub>   55.9   10 <sup>10</sup>     TIO   Sputtering   250   Glass   Al,O <sub>2</sub>   25.9   10 <sup>10</sup>     GO   Sputtering   TIO   Spin-coating   -1/300   Si   SiO <sub>2</sub>   17.71   10 <sup>7</sup>   TIO   TIO   Spin-coating   -1/300   Si   SiO <sub>2</sub>   17.71   10 <sup>7</sup>   TIO   TIO   Spin-coating   -1/300   FI   SiO <sub>2</sub>   TIO   TIO   TIO   TIO   TIO   TIO   TIO   TIO							4.07	
TIOMATZO   Sputtering   Light irradiation   Silicon   SiO <sub>2</sub>   446   10 <sup>8</sup>								3
EXON   Sputtering   Light irradiation   Silicon   SiO <sub>2</sub>   48.4   10°								3
Incolor   Sputtering   300   Silicon   SiO <sub>2</sub>   9.55   10 <sup>7</sup>     ShoO <sub>2</sub>   Sputtering   180   Silicon   HPO <sub>2</sub>   9.56     In <sub>2</sub> O <sub>3</sub>   ALD   300   Glass   Al <sub>2</sub> O <sub>3</sub>   41.8   10 <sup>7</sup>     ALD   160/300   Silicon   Al <sub>2</sub> O <sub>3</sub>   7.8   10 <sup>7</sup>     AlD   -/200   Silicon   Al <sub>2</sub> O <sub>3</sub>   27.8   10 <sup>8</sup>     AlO   ALD   -/200   Silicon   Al <sub>2</sub> O <sub>3</sub>   27.8   10 <sup>9</sup>     AlO   ALD   -/200   Silicon   Al <sub>2</sub> O <sub>3</sub>   27.8   10 <sup>9</sup>     AlO   ALD   -/200   Silicon   Al <sub>2</sub> O <sub>3</sub>   27.8   10 <sup>9</sup>     AlO   Sputtering   300   Glass   SiN <sub>4</sub> PSiO <sub>2</sub>   48.28   10 <sup>7</sup>     AlO   Sputtering   300   Glass   SiN <sub>4</sub> PSiO <sub>2</sub>   48.28   10 <sup>7</sup>     AlO   Sputtering   300   Silicon   SiO <sub>2</sub>   15.30   10 <sup>8</sup>     TO   Sputtering   300   Silicon   SiO <sub>2</sub>   15.30   10 <sup>8</sup>     TO   Sputtering   250   Glass   Al <sub>2</sub> O <sub>3</sub>   25.1   10 <sup>9</sup>     TO   Sputtering   250   Glass   Al <sub>2</sub> O <sub>3</sub>   25.1   10 <sup>9</sup>     TO   Sputtering   250   Glass   Al <sub>2</sub> O <sub>3</sub>   25.9   10 <sup>9</sup>     GO   ALD   200/300   Glass   Al <sub>2</sub> O <sub>3</sub>   25.1   10 <sup>9</sup>     GO   ALD   200/300   Glass   Al <sub>2</sub> O <sub>3</sub>   25.1   10 <sup>9</sup>     GO   Sputtering   RT   Glass   Al <sub>2</sub> O <sub>3</sub>   25.9   10 <sup>9</sup>     GO   Sputtering   RT/200   Silicon   HO <sub>2</sub>   38.29   10 <sup>9</sup>     GO   Sputtering   RT/100   Silicon   Al <sub>2</sub> O <sub>3</sub>   4.0   4.3   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   TO   TO   TO   TO   TO   TO   TO	TO/ATZO	Sputtering	_	Glass	$SiO_2$	246		3
Incolor   Sputtering   300   Silicon   SiO <sub>2</sub>   9.55   10 <sup>7</sup>     ShoO <sub>2</sub>   Sputtering   180   Silicon   HPO <sub>2</sub>   9.56     In <sub>2</sub> O <sub>3</sub>   ALD   300   Glass   Al <sub>2</sub> O <sub>3</sub>   41.8   10 <sup>7</sup>     ALD   160/300   Silicon   Al <sub>2</sub> O <sub>3</sub>   7.8   10 <sup>7</sup>     AlD   -/200   Silicon   Al <sub>2</sub> O <sub>3</sub>   27.8   10 <sup>8</sup>     AlO   ALD   -/200   Silicon   Al <sub>2</sub> O <sub>3</sub>   27.8   10 <sup>9</sup>     AlO   ALD   -/200   Silicon   Al <sub>2</sub> O <sub>3</sub>   27.8   10 <sup>9</sup>     AlO   ALD   -/200   Silicon   Al <sub>2</sub> O <sub>3</sub>   27.8   10 <sup>9</sup>     AlO   Sputtering   300   Glass   SiN <sub>4</sub> PSiO <sub>2</sub>   48.28   10 <sup>7</sup>     AlO   Sputtering   300   Glass   SiN <sub>4</sub> PSiO <sub>2</sub>   48.28   10 <sup>7</sup>     AlO   Sputtering   300   Silicon   SiO <sub>2</sub>   15.30   10 <sup>8</sup>     TO   Sputtering   300   Silicon   SiO <sub>2</sub>   15.30   10 <sup>8</sup>     TO   Sputtering   250   Glass   Al <sub>2</sub> O <sub>3</sub>   25.1   10 <sup>9</sup>     TO   Sputtering   250   Glass   Al <sub>2</sub> O <sub>3</sub>   25.1   10 <sup>9</sup>     TO   Sputtering   250   Glass   Al <sub>2</sub> O <sub>3</sub>   25.9   10 <sup>9</sup>     GO   ALD   200/300   Glass   Al <sub>2</sub> O <sub>3</sub>   25.1   10 <sup>9</sup>     GO   ALD   200/300   Glass   Al <sub>2</sub> O <sub>3</sub>   25.1   10 <sup>9</sup>     GO   Sputtering   RT   Glass   Al <sub>2</sub> O <sub>3</sub>   25.9   10 <sup>9</sup>     GO   Sputtering   RT/200   Silicon   HO <sub>2</sub>   38.29   10 <sup>9</sup>     GO   Sputtering   RT/100   Silicon   Al <sub>2</sub> O <sub>3</sub>   4.0   4.3   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   Al <sub>2</sub> O <sub>3</sub>   4.0   4.0   4.0     GO   Sputtering   TO   Glass   TO   TO   TO   TO   TO   TO   TO	ZNON		Light irradiation	Silicon		48.4		3
Single   Sputtering   180   Silicon   HiO <sub>5</sub>   92   10 <sup>6</sup>	nON					9.55		1
1.0, 0								3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-							4
Tro								4
ZO							10 10 <sup>9</sup>	
ZZOHIZO   Sputtering   250							10	4
Part								4
International Content   Inte	ZO/HIZO		250	Glass		48.28		4
ZOZADO/IGZO   Sputtering   300   silicon   SiO <sub>2</sub>   14.0   10 <sup>8</sup>   TO   Sputtering   200   Glass   Al <sub>2</sub> O <sub>3</sub>   56.1   10 <sup>9</sup>   TO   Sputtering   250   Glass   Al <sub>2</sub> O <sub>3</sub>   25.9   10 <sup>9</sup>   GO   ALD   200/300   Glass   Al <sub>2</sub> O <sub>3</sub>   9.45   10 <sup>8</sup>   GO   Sputtering   RT   Glass   Al <sub>2</sub> O <sub>3</sub>   9.45   10 <sup>8</sup>   GZO   Sputtering   RT/200   Silicon   HfO <sub>2</sub>   38.29   10 <sup>6</sup>   GZO   Sputtering   RT/100   Silicon   HfO <sub>2</sub>   38.29   10 <sup>6</sup>   GZO   Sputtering   RT/100   Silicon   SiN <sub>1</sub>   26.63   10 <sup>7</sup>   GZO   Sputtering   RT/100   Silicon   Al <sub>2</sub> O <sub>3</sub>   6.3   10 <sup>7</sup>   GZO   Sputtering   RT   Glass   Al <sub>2</sub> O <sub>3</sub>   6.3   10 <sup>7</sup>   GZO   Sputtering   RT   Glass   Al <sub>2</sub> O <sub>3</sub>   6.3   10 <sup>7</sup>   GZO   Sputtering   Sputtering   Sputtering   Sputtering   Sputtering   Sputtering   Sputtering   300   Glass   SiN <sub>2</sub> SiO <sub>2</sub>   13.73   10 <sup>12</sup>   10 <sup>2</sup>   12/20   Sputtering   300   Glass   SiN <sub>2</sub> SiO <sub>2</sub>   13.73   10 <sup>12</sup>   10 <sup>2</sup>   10 <sup>2</sup>	PrIZO	Sputtering	300	Glass	SiO <sub>2</sub> /Si <sub>3</sub> N <sub>4</sub>	26.3		4
ZOZADO/IGZO   Sputtering   300   silicon   SiO <sub>2</sub>   14.0   10 <sup>8</sup>   TO   Sputtering   200   Glass   Al <sub>2</sub> O <sub>3</sub>   56.1   10 <sup>9</sup>   TO   Sputtering   250   Glass   Al <sub>2</sub> O <sub>3</sub>   25.9   10 <sup>9</sup>   GO   ALD   200/300   Glass   Al <sub>2</sub> O <sub>3</sub>   9.45   10 <sup>8</sup>   GO   Sputtering   RT   Glass   Al <sub>2</sub> O <sub>3</sub>   9.45   10 <sup>8</sup>   GZO   Sputtering   RT/200   Silicon   HfO <sub>2</sub>   38.29   10 <sup>6</sup>   GZO   Sputtering   RT/100   Silicon   HfO <sub>2</sub>   38.29   10 <sup>6</sup>   GZO   Sputtering   RT/100   Silicon   SiN <sub>1</sub>   26.63   10 <sup>7</sup>   GZO   Sputtering   RT/100   Silicon   Al <sub>2</sub> O <sub>3</sub>   6.3   10 <sup>7</sup>   GZO   Sputtering   RT   Glass   Al <sub>2</sub> O <sub>3</sub>   6.3   10 <sup>7</sup>   GZO   Sputtering   RT   Glass   Al <sub>2</sub> O <sub>3</sub>   6.3   10 <sup>7</sup>   GZO   Sputtering   Sputtering   Sputtering   Sputtering   Sputtering   Sputtering   Sputtering   300   Glass   SiN <sub>2</sub> SiO <sub>2</sub>   13.73   10 <sup>12</sup>   10 <sup>2</sup>   12/20   Sputtering   300   Glass   SiN <sub>2</sub> SiO <sub>2</sub>   13.73   10 <sup>12</sup>   10 <sup>2</sup>   10 <sup>2</sup>	ZO/IZO:Si		300	silicon	SiO <sub>2</sub>	15.30	$10^{8}$	4
TO Sputtering 200 Glass $A_1O_3$ 56.1 $10^9$ TO Sputtering 250 Glass $A_1O_3$ 25.9 $10^9$ GO ALD 200/300 Glass $A_1O_3$ 25.9 $10^9$ GO ALD 200/300 Glass $A_1O_3$ 2.66 $10^9$ GO Sputtering RT Glass $A_1O_3$ 2.66 $10^9$ GO Sputtering RT/200 Silicon HfO <sub>2</sub> 38.29 $10^6$ GZO Sputtering RT/100 Silicon HfO <sub>2</sub> 38.29 $10^6$ GZO Sputtering RT/100 Silicon $A_1O_3$ 6.3 $10^7$ GZO Sputtering RT Glass $A_1O_3$ 6.3 $10^7$ GZO Sputtering RT Glass $A_1O_3$ 6.3 $10^7$ GZO Sputtering RT Glass $A_1O_3$ 6.3 $10^7$ GZO Sputtering 150 Glass PVP-co-PMMA, PMF, HfO <sub>2</sub> 5.4 $10^6$ GTO Sputtering 150 Glass PVP-co-PMMA, PMF, HfO <sub>3</sub> 5.4 $10^6$ GTO Sputtering 300 Glass SiN, SiO <sub>2</sub> 13.73 $10^7$ ZO/IGZO Spin-coating $-/300$ Si $A_1O_3$ 2.5 $10^7$ $10^7$ Nilicon Spin-coating $-/350$ Si SiO <sub>2</sub> 25.5 $10^7$ Ni-LIO Spin-coating $-/350$ Si SiO <sub>2</sub> 27.71 $10^6$ Metal oxide TFTs on flexible substrates and the spin substrates are spin substrained by the spin substrained				silicon	$SiO_2$	14.0		4
TO Sputtering 250 Glass $Al_2O_3$ 25.9 $10^9$ GO ALD 200/300 Glass $Al_2O_3$ 9.45 $10^8$ GO Sputtering RT Glass $Al_2O_3$ 2.66 $10^6$ GCO Sputtering RT/200 Silicon $HO_2$ 38.29 $10^6$ GCO Sputtering RT/100 Silicon $SiN_x$ 26.03 $10^7$ GCO Sputtering RT/100 Silicon $SiN_x$ 26.03 $10^7$ GCO Sputtering RT/100 Silicon $SiN_x$ 26.03 $10^7$ GCO Sputtering RT Glass $Al_2O_3$ 6.3 $10^7$ GCO Sputtering 300 Glass $Al_2O_3$ 6.3 $Al_2O_3$ 7.1 $Al_2O_3$ 7.1 $Al_2O_3$ 8.1 $Al_2O_3$ 8.1 $Al_2O_3$ 8.2 $Al_2O_3$ 8.2 $Al_2O_3$ 8.3 $Al_2O_3$ 8.4 $Al_2O_3$ 8.4 $Al_2O_3$ 8.4 $Al_2O_3$ 8.5 $Al_2O_3$ 8.5 $Al_2O_3$ 8.5 $Al_2O_3$ 8.7 $A$								4
GO ALD 200/300 Glass Al <sub>2</sub> O <sub>3</sub> 9.45 10 <sup>8</sup> GO Sputtering RT Glass Al <sub>2</sub> O <sub>3</sub> 2.66 10 <sup>6</sup> GZO Sputtering RT/200 Silicon HfO <sub>2</sub> 38.29 10 <sup>6</sup> GZO Sputtering RT/100 Silicon HfO <sub>2</sub> 38.29 10 <sup>6</sup> GZO Sputtering RT/100 Silicon HfO <sub>2</sub> 38.29 10 <sup>6</sup> GZO Sputtering RT Glass Al <sub>2</sub> O <sub>3</sub> 6.3 10 <sup>7</sup> GZO Sputtering RT Glass Al <sub>2</sub> O <sub>3</sub> 6.3 10 <sup>7</sup> GZO Sputtering RT Glass Al <sub>2</sub> O <sub>3</sub> 6.3 10 <sup>7</sup> GZO Sputtering RT Glass PtPt-0-PtMMA, PMF, HfO <sub>2</sub> 5.4 10 <sup>6</sup> GITO Sputtering 150 Glass PtPt-0-PtMMA, PMF, HfO <sub>2</sub> 5.59 10 <sup>7</sup> HZO Sputtering 300 Glass SiN <sub>2</sub> /SiO <sub>2</sub> 13.73 10 <sup>12</sup> ZO/IGZO Spin-coating −/300 Si Al <sub>2</sub> O <sub>3</sub> 25 10 <sup>7</sup> Ni-InO Spin-coating −/350 Si SiO <sub>2</sub> 23.53 10 <sup>6</sup> Mi-InO Spin-coating −/350 Si SiO <sub>2</sub> 17.71 10 <sup>6</sup> Metal oxide TFTs on flexible substrates and the spin spin spin spin spin spin spin spin		Sputtering						4
GO Sputtering RT Glass Al <sub>2</sub> O <sub>3</sub> 2.66 10 <sup>6</sup> GZO Sputtering RT/200 Silicon HfO <sub>2</sub> 38.29 10 <sup>6</sup> GZO Sputtering RT/100 Silicon SiN <sub>x</sub> 26.03 10 <sup>7</sup> GZO Sputtering RT/100 Silicon SiN <sub>x</sub> 26.03 10 <sup>7</sup> GZO Sputtering 70 Silicon Al <sub>2</sub> O <sub>3</sub> 6.3 10 <sup>7</sup> GZO Sputtering RT Glass Al <sub>2</sub> O <sub>2</sub> 5.4 10 <sup>6</sup> GZO Sputtering 150 Glass PVP-co-PMMA, PMF, HfO <sub>2</sub> 25.9 10 <sup>7</sup> HZO Sputtering 300 Glass PVP-co-PMMA, PMF, HfO <sub>2</sub> 25.9 10 <sup>7</sup> HZO Sputtering 300 Glass SiN <sub>x</sub> /SiO <sub>2</sub> 25.5 10 <sup>7</sup> n <sub>2</sub> O <sub>3</sub> Spin-coating —/250 Si Si SiO <sub>2</sub> 23.53 10 <sup>6</sup> HZO Spin-coating —/250 Si Si SiO <sub>2</sub> 23.53 10 <sup>6</sup> HZO Spin-coating —/250 Si Si SiO <sub>2</sub> 23.53 10 <sup>6</sup> HZO Spin-coating —/250 Si Si SiO <sub>2</sub> 17.71 10 <sup>6</sup> HZO Spitering NFX FKT PF Al <sub>2</sub> O <sub>3</sub> 12 10 <sup>7</sup> HZO Spitering NFX FKT PF Al <sub>2</sub> O <sub>3</sub> 12 10 <sup>8</sup> HZO Spitering HZ/KT PF HfO <sub>2</sub> 11.56 10 <sup>8</sup> HZO Sputtering HZ/KT PFN Al <sub>2</sub> O <sub>3</sub> 12 10 <sup>8</sup> HZO Spitering HZ/KT PFN Al <sub>2</sub> O <sub>3</sub> 12 10 <sup>8</sup> HZO Spitering HZ/KT PFN Al <sub>2</sub> O <sub>3</sub> 11.56 10 <sup>8</sup> HZO Spitering HZ/KT PFN Al <sub>2</sub> O <sub>3</sub> 3.07 10 <sup>8</sup> HZO Spitering HZ/KT PFN Al <sub>2</sub> O <sub>3</sub> 3.07 10 <sup>8</sup> HZO Spitering —/250 PF HfO <sub>2</sub> 7.95 10 <sup>8</sup> HZO Spitering —/250 PF HfO <sub>2</sub> 1.66 10 <sup>6</sup> HZO Spitering —/250 PF HGO Spitering HZ/KT PFN Al <sub>2</sub> O <sub>3</sub> 3.07 10 <sup>2</sup> HZO Spitering —/250 PF HGO Spitering HZ/KT PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering —/250 PF HGO Spitering —/250 PF HGO Spitering HZ/KO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.5 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.6 6.6 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.6 6.6 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.6 6.6 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.6 6.6 10 <sup>6</sup> HZO Spitering HZ/KO PFN Al <sub>2</sub> O <sub>3</sub> 1.6 6.6 10								
GZO Sputtering RT/200 Silicon Hr  GZO Sputtering RT/100 Silicon SiN₂ 26.03 10²  GZO Sputtering RT Glass Al₂O₃ 6.3 10²  GZO Sputtering RT Glass PVP-Co-PMMA, PMF, HfO₂ 25.9 10²  HZO Sputtering 300 Glass SiN₂/SiO₂ 13.73 10¹  ZO/IGZO Spin-coating −/300 Si Si SiO₂ 23.53 10²  N-100 Spin-coating −/250 Si Si SiO₂ 23.53 10²  N-100 Spin-coating −/350 Si SiO₂ 23.53 10²  Metal oxide TFFs on flexible substrates  ALD 100/− PET Al₂O₃ 37.1 10²  ALD 200/− PI Al₂O₃ 12.2 10²  ALD 200/− PI Al₂O₃ 11.56 10²  ALO Sputtering RT/RT PEN Al₂O₃ 11.56 10²  ALO Sputtering N-160 PET PMMA 7.53 10²  ALO Spin-coating −/160 PET PMMA 7.53 10²  ALO Spin-coating −/160 PEN Al₂O₃-2.7.95 10²  ALO Spin-coating −/150 PEN Al₂O₃-3 3.07 10²  ALO Spin-coating −/250 PI Ion-gel 1.67 10²  ALO Sputtering RT/200 PES Al₂O₃-1.5 10²  ALO Sputtering RT/200 PI SiO₂-1.5 10²  ALO Spin-coating −/150 PES Al₂O₃-1.5 10²  ALO Spin-coating −/150 PES Al₂O₃-1.5 10²  ALO Spin-coating RT/200 PI SiO₂-1.5 10²  ALO Spin-coating RT/200 PI SiO₂-1.3 10²  ALO Spin-coating RT/200 PEN RSiO1.5 0.07 10²  ALO Spin-coating RT/200 PI SiO₂-1.3 10²  ALO Spin-coating RT/200 PI ZrO₂-1.4 10²  ALO Spin-coating RT/200 PI ZrO₂-1.4 10²  ALO Spin-coating RT/280 P								5
GZO   Sputtering   RT/100   Silicon   SiN_   26.03   10^7								5
GZO   Sputtering   70   Silicon   Al $_2$ O $_3$   6.3   10 $^7$   GZO   Sputtering   RT   Glass   Al $_2$ O $_3$   5.4   10 $^6$   GZO   Sputtering   RT   Glass   Al $_2$ O $_3$   5.4   10 $^6$   GZO   Sputtering   150   Glass   Al $_2$ O $_3$   5.4   10 $^6$   GZO   Sputtering   300   Glass   SiN $_2$ SiO $_3$   13.73   10 $^{12}$   10 $^7$   141ZO   Sputtering   -/250   Si   SiO $_2$   23.53   10 $^6$   10 $^6$   Ni-InO   Spin-coating   -/250   Si   SiO $_2$   23.53   10 $^6$   Ni-InO   Spin-coating   -/350   Si   SiO $_2$   23.53   10 $^6$   Ni-InO   Spin-coating   -/350   Si   SiO $_2$   17.71   10 $^6$   Metal oxide TFTs on flexible substrates   Table 100/	GZO	Sputtering	RT/200	Silicon		38.29		5
GZO   Sputtering   RT   Glass   Al_O'   5.4   106   GTO   Sputtering   150   Glass   PVP-co-PMMA, PMF, HfO <sub>x</sub>   25.9   107   MIZO   Sputtering   300   Glass   SiN <sub>x</sub> /SiO <sub>2</sub>   25.9   107   MIZO   Sputtering   -/300   Si   Al <sub>2</sub> O <sub>3</sub>   25   107   MIZO   Spin-coating   -/250   Si   SiO <sub>2</sub>   23.53   106   MIZO	GZO	Sputtering	RT/100	Silicon	$SiN_x$	26.03		5
GZO	GZO	Sputtering	70	Silicon	$Al_2O_3$	6.3	$10^{7}$	5
GTO   Sputtering   150   Glass   PVP-co-PMMA, PMF, HfO <sub>x</sub>   25.9   107   HIZO   Sputtering   300   Glass   SiN <sub>x</sub> /SiO <sub>2</sub>   13.73   10 <sup>12</sup>   12.7300   Si   Al <sub>2</sub> O <sub>3</sub>   25   107   10.90 <sub>3</sub>   Spin-coating   -/250   Si   SiO <sub>2</sub>   23.53   10 <sup>6</sup>   Sil-InO   Spin-coating   -/350   Si   SiO <sub>2</sub>   23.53   10 <sup>6</sup>   Sil-InO   Spin-coating   -/350   Si   SiO <sub>2</sub>   23.53   10 <sup>6</sup>   Sil-InO   Spin-coating   -/350   Si   SiO <sub>2</sub>   23.53   10 <sup>6</sup>   Sil-InO   Spin-coating   -/350   Si   SiO <sub>2</sub>   23.53   10 <sup>6</sup>   Sil-InO   Spin-coating   -/350   PET   Al <sub>2</sub> O <sub>3</sub>   37.1   10 <sup>7</sup>   Al <sub>2</sub> O <sub>3</sub>   37.1   10 <sup>7</sup>   Al <sub>2</sub> O <sub>3</sub>   25.00   PEALD   200/	GZO		RT	Glass		5.4	$10^{6}$	5
HIZO Sputtering 300 Glass SiN_SiO <sub>2</sub> 13.73 $10^{12}$ IZO/IGZO Spin-coating — $J$ 250 Si Al <sub>2</sub> O <sub>3</sub> 25 $10^7$ InnO <sub>3</sub> Spin-coating — $J$ 250 Si SiO <sub>2</sub> 23.53 $10^6$ Ni-InO Spin-coating — $J$ 250 Si SiO <sub>2</sub> 17.71 $10^6$ Metal oxide TTs on flexible substrates ZnO ALD $I$ 100/— PET Al <sub>2</sub> O <sub>3</sub> 37.1 $I$ 10 $^7$ ZnO PEALD $I$ 200/— PI Al <sub>2</sub> O <sub>3</sub> 12 $I$ 10 $^8$ ZnO Sputtering RT/RT PEN Al <sub>2</sub> O <sub>3</sub> 11.56 $I$ 10 $^8$ ZnO Sputtering RT/RT PEN Al <sub>2</sub> O <sub>3</sub> 11.56 $I$ 10 $^8$ ZnO Sputtering PO/100 PET HfO <sub>2</sub> 7.95 $I$ 10 $^8$ ZnO Hydrothermal 90/100 PET PMMA 7.53 $I$ 10 $^4$ ZnO Spin-coating — $I$ 160 PEN Al <sub>2</sub> O <sub>3</sub> 3.0.7 $I$ 10 $^7$ ZnO Printing Printing — $I$ 250 PI Ion-gel 1.67 $I$ 10 $^5$ ZnO Sputtering $I$ 27.00 PI Al <sub>2</sub> O <sub>3</sub> 3.0.7 $I$ 10 $^5$ ZnO Sputtering $I$ 27.00 PI SiO <sub>2</sub> 1.66 $I$ 10 $^5$ ZnO Sputtering $I$ 27.00 PI SiO <sub>2</sub> 1.6 $I$ 10 $^5$ ZnO Sputtering $I$ 27.00 PI SiO <sub>2</sub> 1.6 $I$ 10 $^5$ ZnO Sputtering $I$ 27.00 PI SiO <sub>2</sub> 1.6 $I$ 10 $^5$ ZnO Sputtering $I$ 27.00 PI SiO <sub>2</sub> 1.6 $I$ 10 $^5$ ZnO Sputtering $I$ 27.00 PI SiO <sub>2</sub> 1.6 $I$ 10 $^5$ ZnO Sputtering $I$ 27.00 PI SiO <sub>2</sub> 1.6 $I$ 10 $^5$ ZnO Sputtering $I$ 27.100 PI SiO <sub>2</sub> 1.6 $I$ 10 $^5$ ZnO Sputtering $I$ 27.100 PI SiO <sub>2</sub> 1.6 $I$ 10 $^5$ ZnO Spin-coating $I$ 27.100 PI SiO <sub>2</sub> 1.6 $I$ 10 $^5$ ZnO Spin-coating $I$ 27.100 PI SiO <sub>2</sub> 1.3 $I$ 10 $^6$ ZnO Spin-coating $I$ 27.100 PES Hybrid 1.42 $I$ 10 $^4$ ZnO Spin-coating $I$ 27.100 PES $I$ 30.300 PI ZrO <sub>2</sub> 1.6 $I$ 31.00 $I$ 31.00 PET $I$ 27.00 Spin-coating $I$ 27.00 PI $I$ 32.00 Spin-coating $I$ 30.00 PI $I$ 30.00 PI $I$ 30.00 Spin-coating $I$ 30.00 PI $I$								5
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Metal oxide TFTs on flexible substrates								5
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	ZnO	Spin-coating	<del>/160</del>	PEN	$Al_2O_3$ - $ZrO_2$	5		6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	ZnO	ALD	150/—	PI	$Al_2O_3$	3.07		6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	ZnO	Printing	<del>/250</del>	PI	Ion-gel	1.67	$10^{5}$	6
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TTO Inkjet-print 30/300 PI $ZrO_2$ 0.04 $10^3$ ZO Sputtering RT/RT PET $SiO_2$ 65.8 $10^6$ ZO Spin-coating RT/280 PI $Zr-Al_2O_3$ 51 $10^4$ ZO Sputtering $-/300$ PI $Al_2O_3$ 6.64 $10^7$ ZO SCS $275/-$ Polyester $Al_2O_3/ZrO_2$ 3.9/6.2 $10^4$ ZO Spin-coating RT/350 PI $Zr-Bl$ 4.1	ZnO	Spin-coating	<b>/135</b>	PEN		0.07		7
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ZO       Spin-coating       RT/350       PI       K-PIB       4.1 $10^5$ ZO:F       Spin-coating       RT/200       PEN $Al_2O_3$ 4.1 $10^8$ WO       Sputtering       270       PI $Al_2O_3$ 25.86 $10^5$ ZITO       PLD       RT/—       PET       v-SAND       110 $10^4$ ZITO       Sputtering       300/200       PI       SiO2       32.9 $10^9$								
ZO:F       Spin-coating       RT/200       PEN $Al_2O_3$ 4.1 $10^8$ WO       Sputtering       270       PI $Al_2O_3$ 25.86 $10^5$ ZITO       PLD       RT/—       PET       v-SAND       110 $10^4$ ZITO       Sputtering       300/200       PI       SiO <sub>2</sub> 32.9 $10^9$								8
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WO       Sputtering $270$ PI $A_2^1O_3$ $25.86$ $10^5$ CITO       PLD       RT/—       PET       v-SAND $110$ $10^4$ CITO       Sputtering $300/200$ PI $SiO_2$ $32.9$ $10^9$	ZO:F	Spin-coating	RT/200	PEN	$Al_2O_3$	4.1		-
RT/- PET v-SAND 110 10 <sup>4</sup> LTO Sputtering 300/200 PI SiO <sub>2</sub> 32.9 10 <sup>9</sup>	WO	Sputtering		PI		25.86	$10^{5}$	8
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GZO Spin-coating RT/350 PI $Al_2O_3$ 84.4 $10^5$								8

Table 1 (Contd.)

Metal oxide TFTs on rigid substrates											
Material	Technique	$(T_{\rm dep.}/T_{\rm post.})/({\rm ^{\circ}C})$	Substrate	Dielectric	Mobility (cm $^2$ V $^{-1}$ s $^{-1}$ )	On/off ratio					
IGZO	Sputtering	RT/RT	PC	SiO <sub>2</sub> /TiO <sub>2</sub> /SiO <sub>2</sub>	76	$10^{5}$	87				
IGZO	Sputtering	RT/200	PI	HfLaO	22.1	$10^{5}$	88				
IGZO	Sputtering	RT/200	PDMS	P(VDF-TrFE)	21	$10^{7}$	89				
IGZO	Sputtering	200/220	PI	$\widetilde{\mathrm{SiO}_2}$	19.6	$10^{9}$	90				
IGZO	Sputtering	RT/—	PI	$Al_2O_3$	17	$10^{5}$	91				
IGZO	Sputtering	RT/180	PEN	$Al_2O_3$	15.5	$10^{9}$	92				
IGZO	Sputtering	<b>-</b> /180	PEN	$Si_3N_4$	13	$10^{8}$	93				
IGZO	Sputtering	150/150	PEN	$Al_2O_3$	12.87	$10^{9}$	94				
IGZO	Sputtering	<b>—</b> /160	PEN	$Al_2O_3$	11.2	$10^{9}$	95				
IGZO	Spin-coating	—/PN254 nm	PI	ZAO	11	$10^{9}$	96				
IGZO	Sputtering	RT/110	PET	c-PVP	10.2	$10^{6}$	97				
IGZO	Sputtering	RT/150	PVA	SiO <sub>2</sub> /Si <sub>3</sub> N <sub>4</sub>	10	$10^{6}$	98				
IGZO	Sputtering	<b>—</b> /300	Thin glass	$Si_3N_4$	9.1	$10^{8}$	99				
IGZO	Sputtering	RT/190	PEN	$SiO_2$	8	$10^{7}$	100				
IGZO	Sputtering	—/PN254 nm	PAR	$Al_2O_3$	7	$10^{8}$	101				
IGZO	Spin-coating	—/PN254 nm	PI	$Al_2O_3$	5.41	$10^{8}$	102				
IGZO	Sputtering	RT/—	PI	Al <sub>2</sub> O <sub>3</sub> /SiO <sub>2</sub>	4.93	5	103				
IGZO	Sputtering	RT/—	PI	PVP	3.6	$10^{4}$	104				
IGZO	Sputtering	RT/—	PEN	PVP	0.43	$10^{5}$	105				
IGZO	Sputtering	RT/200	PDMS	P(VDF-TrFE)	0.35	$10^{4}$	106				
IGZO/IZO	Sputtering	40/200	PEN	$\dot{SiO}_2$	18	$10^{9}$	107				
IGZO	Spin-coating	-/140 200	PI	$Al_2O_3$	1.5	$10^{4}$	108				
$In_2O_3$	Flexographic printing	/200	PI	$Al_2O_3$	2.83	$10^{6}$	109				

the MWA process has been shown to provide a lower temperature process that results in good activation. 118 In 2010, T. Jun et al. demonstrated a comparison between hot plate annealing and microwave annealing effects on the performance of a solution processed ZnO TFT. Microwave-annealing of ZnO TFTs on a rigid substrate for 30 min at 140 °C showed a better field effect mobility of 1.7 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> compared to hot plate annealing (0.32 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>). Additionally, transistors on flexible substrates exhibited device characteristics of 0.57 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>. Microwave annealing reduces the grain boundaries due to an increase in the size of the ZnO nanoparticles and leads to improved transport properties of the charge carriers, resulting in better performance of the TFT. 113 In 2014, S. Park et al. also investigated the effect of microwave annealing on a sputtered ZnO TFT (Fig. 4b). The microwave irradiation of 2.45 GHz at 700 W for 15 min increased the field effect mobility from 0.2 to 1.5 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> and the on/off current ratio from 36.5 to 6.9 × 10<sup>6</sup>. The microwave irradiation induces a large number of oxygen vacancies as confirmed by photoluminescence, resulting in enhanced mobilities.<sup>70</sup> H.-C. Cheng also demonstrated a microwave annealed solution processed flexible a-IZO TFT<sup>119</sup> with a mobility of 6.9 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>, and an  $I_{ON}/I_{OFF}$  ratio greater than 10<sup>6</sup> (Fig. 4d). In 2014, Lee et al. demonstrated highly reliable microwave assisted annealed a-IGZO thin-film transistors to be used as biosensors. Microwave irradiation of 2.45 GHz at 1000 W for 10 min improved the TFT performance ( $\mu_{\rm FE}$ = 9.51 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>,  $V_{\text{th}}$  = 0.99 V,  $I_{\text{ON}}/I_{\text{OFF}}$  = 1.18 × 10<sup>8</sup>), compared to that of furnace-annealed a-IGZO TFTs at 400  $^{\circ}\text{C}$  for 30 min ( $\mu_{\rm FE}$  = 4.51 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>,  $V_{\rm th}$  = 4.85 V,  $I_{\rm ON}/I_{\rm OFF}$  = 3.38 × 10<sup>7</sup>). The microwave annealing eliminated the defect density inside the a-IGZO film and improved the device performance. In addition, the microwave-assisted annealed TFT displayed

excellent sensing properties in terms of pH sensitivity, reliability, and chemical stability when employed as a transducer in an extended-gate ion-sensitive field-effect transistor biosensor. 114 In 2015, K.-W. Jo and his co-workers developed ultra-thin (5 nm) SnO<sub>2</sub> TFTs. The performance of the TFTs was significantly improved with a field effect mobility of 35.4 cm<sup>2</sup>  $V^{-1}$  s<sup>-1</sup> and  $I_{ON}/I_{OFF} = 4.48 \times 10^7$  under microwave irradiation of 2.45 GHz at 1000 W for 15 min assisted annealing as compared to that of CTA (400 °C, 30 min) TFTs ( $\mu_{FE} = 20.3 \text{ cm}^2 \text{ V}^{-1}$  $s^{-1}$ ,  $I_{ON}/I_{OFF} = 2.76 \times 10^7$ ) as depicted in Fig. 4e. This result is due to the enhancement of crystallinity and elimination of defects in SnO<sub>2</sub> TFTs by the microwave irradiation. 115 In 2019, Shin reported the microwave-assisted annealing of various compositional ratios of sputtered IGZO films under O2 ambient atmosphere (Fig. 4c). The temperature of the a-IGZO TFT samples was measured using an infrared thermometer during the MW-PDA process and observed to be 399.6 °C on average. However, CTA at 400 °C showed poorer performance since MWA results in lowered defect densities  $(D_{it}, N_t)$  and subgap density of states (DOS). 116 Compared to conventional annealing techniques, the novel microwave annealing techniques facilitate low temperature activation of devices on flexible substrates and may be promising for roll to roll processing of flexible electronics. 117 In addition, microwave annealing is also more efficient at improving the electrical performance of IGZO TFTs than the other low temperature annealing processes such as electron beam (e-beam) radiation and low-temperature hot-plate annealing. It is shown that, the IGZO TFTs subjected to microwave annealing exhibit a typical field effect mobility of 11.3 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> and a threshold voltage of -1.54 V, while the TFTs subjected to e-beam annealing exhibit a slightly lower mobility of 7.40 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> and a more negative

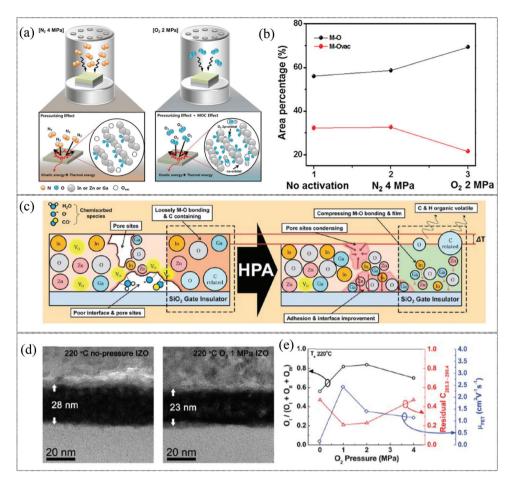


Fig. 3 (a) Schematic of the effect of  $N_2$  and  $O_2$  HPA on sputtered IGZO films (reproduced from ref. 110), (b) area ratio of M-O and M-O<sub>vac</sub> for various conditions (reproduced from ref. 110), (c) illustration of the effect of high pressure on low temperature solution-processed metal oxide thin films (reproduced from ref. 112), (d) cross-sectional HRTEM image of the IZO thin film annealed at 220 °C (right) and at 220 °C in 1 MPa O<sub>2</sub> (reproduced from ref. 112), and (e) the  $O_1/O_1 + O_{11} + O_{11}$  ratio, residual carbon ratio (286.1 + 287.1 + 288.1 + 288.9 eV/284.6 eV), and field-effect mobilities as functions of O<sub>2</sub> pressure (reproduced from ref. 112).

threshold voltage of -1.95 V. The poor performance is attributed to structural damage during e-beam radiation, which generates electrical defect levels within the forbidden band gap of IGZO. 120 However, the low-temperature hot-plate annealing resulted in comparable device performance with microwave annealing and both microwave annealing and low-temperature hot-plate annealing increased the mobility from 12.3 cm<sup>2</sup> V<sup>-1</sup>  $s^{-1}$  (as-deposited) to ~19 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> in microwave and hot plate annealing states. However, the negative shift in the threshold voltage with microwave annealing (from 0.23 V to -2.86 V) is smaller than that with low-temperature hotplate annealing (to -9 V) due to the suppression of oxygen vacancy formation. 121 Microwave annealing offers various advantages such as rapid and effective heating, low temperature processing, and suppression of unnecessary diffusion to the adjacent material. However, there may be challenges in terms of safety and variations associated with the specific sample size and the shape may also need to be managed.

2.1.3 Photoactivation. Photoactivation is the most prevalent substitute for thermal annealing of MO films, especially

for solution processed MO films, where the light source provides photothermal energy sufficient to initiate the chemical conversion for the formation of metal oxide networks. Photoactivation has been demonstrated with deep UV irradiation as a viable annealing technique for the formation of MO films such as IZO, IGZO and IO. Recently, there have been reports on the use of other sources including infrared and intense pulsed light for the activation of metal oxide films for TFT applications. 122-124 Deep UV (DUV) irradiation provides sufficient energy for the decomposition, condensation and densification reactions and results in MO films with properties comparable to high temperature CTA MO films (mechanism of activation is illustrated in Fig. 5a). In 2012, Park et al. demonstrated the use of DUV irradiation, specifically suitable for nitrate precursors (compared to acetate or chloride precursors) by virtue of their stronger absorption of UV irradiation. 125 Though there is inherent heating to around 150 °C during photoactivation, which may aid in the removal of organic residues, this is insufficient as an independent thermal energy source for the formation of M-O-M networks, as is evident in

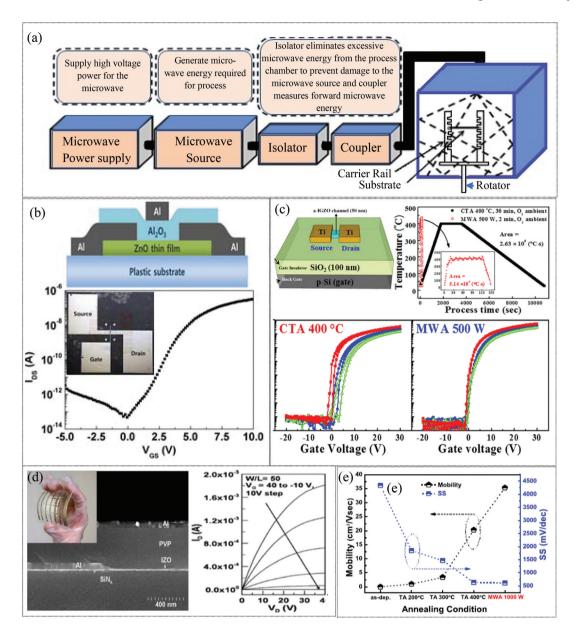


Fig. 4 (a) A schematic of the microwave annealing system (reproduced from ref. 169). (b) A schematic of the flexible ZnO TFT and transfer characteristics of the microwave processed flexible device (reproduced from ref. 70). (c) Schematic diagram of back-gate top-contact structure a-IGZO TFTs, temperature profile of the annealing process using CTA at 400 °C for 30 min in O<sub>2</sub> and MWA at 500 W for 2 min in O<sub>2</sub>, respectively, and transfer characteristics of microwave and CTA processed devices (reproduced from ref. 116). (d) SEM local cross-sectional image of the flexible a-IZO TFT device on the PI substrate; the inset shows a flexed 5 cm × 5 cm PI substrate with 27 a-IZO TFT devices and output characteristics (reproduced from ref. 119). (e) Field-effect mobility ( $\mu_{EF}$ ) and subthreshold swing (SS) of 5 nm thick UTB SnO<sub>2</sub> TFTs annealed under different conditions (reproduced from ref. 115).

Fig. 5b. Though initially demonstrated under an inert atmosphere, UV photochemical activation was shown to be equally effective under ambient conditions as reported by Mathews et al. 126 Here, a mid-UV range source with emission spectra of 200 to 300 nm, corresponding to 398.48 to 598.2 kJ mol<sup>-1</sup>, was used to ensure decomposition of precursors and initiate condensation and densification for the formation of high quality InO and IZO films with TFT mobilities of  $\sim 30 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ . On the other hand, infrared irradiation activation relies on the

rapid photothermal effect provided by IR irradiation (Fig. 5c). IR irradiation increases the free energy of the precursor system, elevating it to a metastable state, which reduces the activation energy necessary for the formation of the oxide network. Thus, in comparison with conventional thermal annealing, with adequate duration of IR irradiation, lower temperature is sufficient for complete precursor decomposition and metal oxide network formation. This results in metal oxide films with higher carrier concentration and lower

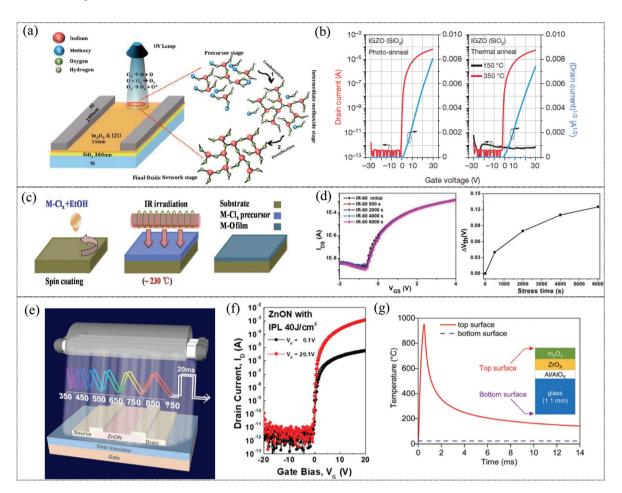


Fig. 5 (a) Proposed mechanism for photochemical activation via UV irradiation (reproduced from ref. 126). (b) Transfer and output characteristics of photo-annealed and thermally annealed (150 and 350 °C) IGZO TFTs (reproduced from ref. 125). (c) Process flow of IR irradiation activation for formation of a metal oxide film (reproduced from ref. 123). (d) Transfer characteristics and V<sub>th</sub> shift results of positive bias stress on IGZO TFTs activated by IR irradiation (reproduced from ref. 122). (e) Illustration of sub-second exposure of IPL (xenon flash lamp) for activation (reproduced from ref. 128). (f) Transfer characteristics of IPL activated ZnON TFTs at different drain voltages (reproduced from ref. 128). (g) Simulation results obtained using the SimPulse software of the temperature at the top and at the bottom of the In<sub>2</sub>O<sub>3</sub> TFT fabricated on a 1.1 mm-thick glass substrate after exposure to a xenon light pulse (reproduced from ref. 127).

defect density due to improved interface quality and higher oxygen vacancy generation. Wang et al. reported that an IGZO TFT fabricated by IR irradiation (induced temperature of 230 °C) in ambient environments could achieve a mobility of 60 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>, and an  $I_{\rm ON}/I_{\rm OFF}$  ratio of 10<sup>6</sup>. This was a marked improvement in mobility compared to those of conventional high temperature (450 °C) annealed IGZO TFTs. The higher M-O bond content and oxygen vacancies and lower M-OH content and trap density demonstrated by the IR irradiated MO layers in comparison with thermally annealed counterparts are indicative of a high quality, low defect content metal oxide layer with good interface quality which manifests in the high stability exhibited during a positive bias stress test (Fig. 5d). Unlike UV annealing, IR irradiation is also effective with chloride precursors (which typically require >400 °C annealing). Xia et al. have reported the use of IR irradiation to form both an AlO<sub>x</sub> solution processed dielectric and an IO film employing chloride precursors. 123 The resultant AlO<sub>x</sub> dielectric

demonstrated properties comparable to vacuum processed counterparts with a capacitance of 158 nF cm<sup>-2</sup> and a small leakage current (5.4 Å-10<sup>-8</sup> A cm<sup>-2</sup>) by virtue of the low defect density of IR irradiated films. The IO TFTs exhibited a mobility of around 33 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>. However, the incidental temperature on the substrate during IR radiation is higher than that generated during UV irradiation, which may make it unsuitable for certain flexible substrates. The primary advantage of other novel photoactivation sources such as intense pulse light is the sub-second exposure duration necessary for the activation of the metal oxide films which ensures selective heating of the precursor film. Intense pulsed light (IPL) using a xenon light source was used for the photoactivation of solution processed MO films such as IGZO and In2O3 TFTs and In2O3/ZnO heterojunctions for TFT applications. 124,127 It was also used for the activation of sputtered ZnON films, where a 20 ms pulse of 40 J cm<sup>-2</sup> resulted in TFT devices with high stress stability and a mobility of around 48 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>. <sup>128</sup> Even though the inci-

dental heating can be as high at 1000 °C during exposure in the case of a xenon flash lamp, the sub-second (500 µs-20 ms) exposure duration ensures negligible heating of the substrate (Fig. 5g). 127 In<sub>2</sub>O<sub>3</sub> TFTs were fabricated on polyimide (PI) and heat-stabilized polyethylene naphthalate (PEN) substrates using xenon lamp photonic activation, demonstrating their compatibility with flexible substrates. 129 Thus, photoactivation seems to be a prime candidate for the replacement of CTA, providing a low temperature alternative to form high performance metal oxide films with condensation and densification comparable to those of their high temperature annealed counterparts. 130 In addition, photochemically activated films have been reported to result in improved surface roughness (<0.7 nm or below) compared to CTA samples, which can aid in enhancing device performance. 129 Studies on bias illumination stress behaviors have shown that the photoactivated samples show enhanced stability and faster recovery when compared to CTA samples.<sup>20</sup> In addition, the durations of these photoactivation techniques range from a few ms (in the case of IPL) to a few min to less than an hour (in the case of deep UV and IR), which is beneficial from a high throughput R2R manufacturing point of view. However, it has to be noted that the materials properties of the metal oxide films or precursors such as their absorption range, thermal conductivity etc., have a profound effect on the successful photoactivation of the films. 129 In the case of deep UV photoactivation of solution processed films, the nitrate precursors are preferred due to its favorable UV absorption may be harmful due to the NO<sub>x</sub> decomposition byproduct. DUV is also known to be incompatible to various flexible substrates and has been shown to reduce the optical transmission of certain flexible substrates. 123 Due to the limitations of the photoactivated area using IPL, the feasibility of scaling up of the activation process for large area or R2R production has to be investigated.

Sections 2.1.1-2.1.3 discussed the widely reported alternatives to CTA. However, there are always unavoidable thermal components in many of these processes and other limitations that make them incompatible with flexible substrates. Recently, there have been studies on other novel physical techniques which effectively modulate the oxygen vacancies/electronic structures of MO films athermally, with an additional advantage of being substrate independent. Among these, the use of capping layers and ionic liquid activation are two promising techniques, which will be covered in the following sections.

2.1.4 Capping layers. In AOS TFTs, electron mobility is sensitive to defect states and therefore the mobility is expected to increase significantly by reducing the defect density. Metallic capping layers overlaid between S/D contacts reduce drain current-crowding and the carrier scattering effect due to their lower value of sheet resistance. 131 Additionally, the proposed devices effectively prevent the adsorption/desorption reaction of ambient oxygen and hydrogen molecules on the surface. This structure showed high  $\mu_{\rm FE}$  and enhanced stability simply by adopting a metal capping layer. 132 In 2012, H.-W. Zan et al. demonstrated an amorphous indium-gallium-zinc oxide

(a-IGZO) TFT with a double capping layer of metal calcium/aluminium at its back channel (Fig. 6a). The mobility of the TFT increased from 12 to 160 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> after deposition of the capping layer of Ca/Al. The Ca layer (150 µm long, 35 nm thick) deposited on the back channel of these devices served as the mobility enhancement capping layer, while the Al layer deterred the formation of CaO, Ca(OH)2 and CaCO3 by absorption of oxygen, water and carbon dioxide, respectively, from the atmosphere. The Ca atoms close to the IGZO layer react with weakly bonded oxygen atoms of Zn-O, In-O, and Ga-O to form Ca-O bonds and enhance the field effect mobility of the device due to the reduction of defect density. 132 In 2015, Z. Wang et al. successfully demonstrated facile fabrication of a CMOS inverter at low temperature by using single-step deposition of a tin mono-oxide channel layer (Fig. 6b). Selective deposition of a copper oxide capping layer on top of the tin mono-oxide provided additional oxygen to form an n-type SnO<sub>2</sub> phase at temperature as low as 190 °C in air. The phase transition from SnO to SnO<sub>2</sub> typically occurs at temperatures above 300 °C. However, in the case of a bilayer system this can occur at temperatures as low as 190 °C. 133 In 2017, Y. Shin et al. showed low-temperature crystallization of IGZO using a tantalum (Ta) catalytic layer. The field-effect mobility was significantly boosted to 54.0 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> for the IGZO device with a metal induced polycrystalline channel formed at 300 °C as compared to 18.1 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> for the non-catalysed IGZO TFT. A 20 nm thick Ta thin film, serving as the crystallization catalytic layer, was sputtered selectively through a shadow mask on top of the active layer between the source and drain electrodes. Improvement in the device mobility occurred because Ta acted as a catalyst to break weak IGZO bonds, and these broken bonds within IGZO rearranged to form crystallized regions during thermal annealing. 134 In 2019, T. Kim and co-workers also investigated novel TaO<sub>r</sub> encapsulation to enhance the performance of ZnO:N thin-film transistors (Fig. 6c). A 10 nm thick Ta film was selectively deposited and annealed at 200 °C for 1 h under  $O_2$  ambient atmosphere. Ta capped TFTs ( $\mu_{\rm FE}$  = 89.4 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>,  $V_{\text{th}} = -0.45$  V,  $I_{\text{ON/OFF}} = 8.6 \times 10^8$ ) showed improved performance when compared to uncapped TFTs ( $\mu_{ ext{FE}}$ = 36.2 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>,  $V_{\text{th}}$  = 1.28 V,  $I_{\text{ON/OFF}}$  = 2.9 × 10<sup>8</sup>) owing to scavenging and passivation effects of the TaO<sub>x</sub> film which occurred due to facile elevation of the quasi-Fermi level as a result of a lower acceptor-like trap state distribution and a large carrier concentration value. A smaller number of sub-gap states near the conduction band (CB) minimum and a higher net carrier density for the TaOx-capped devices increased the Fermi energy level toward the CB edge under thermal equilibrium conditions, thus leading to efficient band conduction and fast carrier transport under the on-state conditions. 135 Various metal capping layers have been shown to improve device performance and stability; however, the additional patterning steps required for the capping layer increases the manufacturing cost. It also lowers the optical transparency of transparent electronics due to a reduced aperture ratio. 136

2.1.5 Ionic liquid approach or electric field driven approaches. Owing to the capability to generate an extremely

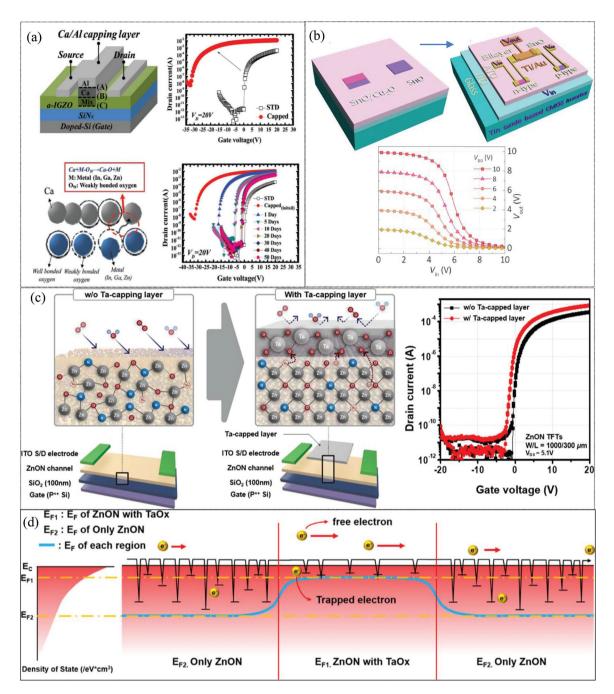


Fig. 6 (a) Bottom-gate top-contact a-IGZO TFT (STD device) is capped with a Ca/Al dual layer and transfer characteristics of STD and of Ca/Alcapped a-IGZO TFTs with a 50 days storage test in air (reproduced from ref. 132). (b) Schematic diagram of CMOS inverter fabrication and transfer curves of an optimized CMOS inverter (reproduced from ref. 133). (c) Schematic diagram of Ta-capped ZnON TFT P++ silicon wafer, transfer characteristics (d) schematic energy-band diagram dictated by trap-limited conduction (TLC) modulation for the Ta-capped ZnON TFTs (reproduced from ref. 135).

high electrostatic field (~50 MV mm<sup>-1</sup>), ionic liquid (IL) gating has been extensively used to investigate electrostatic effects on fundamental physics problems in strongly correlated systems. These extremely high electric fields can extract or intercalate ionic species out of or into solids. Thus manipulation of the oxygen vacancy concentration via IL gating is a promising approach to tune the electrical properties, mitigating the need

for high temperature annealing. 137,138 In 2019, Kulkarni et al. demonstrated athermal activation in an IWO channel TFT via an electrolyte-gating approach. Room temperature, RF sputtered IWO thin films (thickness ~7 nm) on SiO<sub>2</sub>/Si wafers and on flexible substrates were activated by EMIM TFSI (1-ethyl-3methylimidazolium bis(trifluoromethylsulfonyl)imide) ionic liquids. This technique facilitated the activation of non-func-

tioning TFTs to working transistors with a mobility of  $\mu_{\rm FE}$  = 7.1 cm $^2$  V $^{-1}$  s $^{-1}$  and  $I_{\rm ON/OFF}$  = 10 $^6$  (back gate) and ionic-gated transistors with  $\mu_{\text{FE}} = 105.4 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$  on flexible substrates at room temperature. Modulation of the local electronic structure of the channel by migrating oxygen species across the semiconductor-dielectric interface generated sufficient carriers for charge transport and for activation of oxygen-compensated thin films. 137 In 2016, Pudasaini et al. demonstrated IL gating of a-IGZO with a 1-hexyl-3-methylimidazolium bis (trifluoromethylsulfonyl) imide ([Hmim][TFSI]) ionic liquid to modulate the oxygen concentration in the channel layer and tune the threshold voltage  $(V_{th})$ . The ionic liquid was dispensed to cover the a-IGZO active area and auxiliary gate electrode as shown in Fig. 7b. The strong electric field induced by the electrical-double layer (EDL) formed at the interface between the IL and a-IGZO surface was responsible for the extraction of oxygen in the IGZO layer. A relatively large ON current ( $\approx$ 50  $\mu$ A) with an  $I_{\text{ON/OFF}} = 10^5$  and  $\mu_{\text{FE}} = 23.2 \text{ cm}^2 \text{ V}^{-1}$ s<sup>-1</sup> was obtained for the athermal activated IL side gated a-IGZO TFT. 138 In 2013, J. Jeong et al. showed an electrolyte gating approach which suppresses the metal-to-insulator transition and stabilizes the metallic phase to temperatures below 5 kelvin for epitaxial thin films of VO2, even after the ionic liquid is completely removed. These large electrostatic fields have been shown to be capable of moving ions in/out of other oxides as well (VO2 and SrTiO3).139 In 2011, K. Ueno et al.

demonstrated an unexpected superconducting phase in KTaO<sub>3</sub> by an ionic gating approach. EDL transistor devices were fabricated on KTaO3 single crystals with an ionic liquid (as shown in Fig. 7a) with high  $I_{ON}/I_{OFF} > 1 \times 10^5$ . After biasing the ionic gate, electrostatic carrier doping could induce superconductivity in KTaO3. 140 These novel oxygen vacancy modulation techniques facilitate low temperature activation of devices on flexible substrates. However, the modulation of oxygen vacancies is still debated as some researchers continue to suspect the changes to be related to movements of other ions (H<sup>+</sup> and OH<sup>-</sup>) present in the ionic liquid. 141 For electronic gating on flexible substrates, having a liquid on top of the device may not be feasible; thus researchers are trying to form ionic gels which are mainly ABA type tri-block copolymers which consist of ionic liquid-phobic A blocks and ionic liquidphilic B blocks. Ionic liquids can absorb water and could also induce chemical reaction on prolonged exposure; hence care should be taken to minimize contact with water/humidity and other reactive elements.

#### Chemical routes for reduction of process temperature

For solution-processed metal oxide films deposited from precursor solutions, the as-deposited thin films consist of metal cation complexes, hydroxides, oxides etc. During the subsequent high temperature annealing, the M-O-M network is formed through a condensation process and complete anion

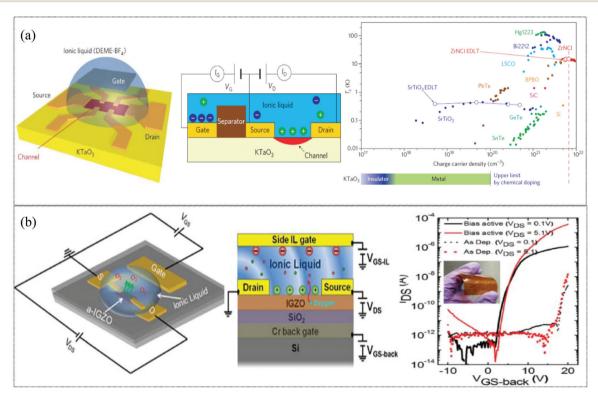


Fig. 7 (a) Electric double-layer (EDL) KTaO $_3$  transistor and superconducting critical temperature  $T_c$  as a function of three-dimensional charge carrier density for chemical doping induced superconductivity in 11 different materials systems (filled symbols), and electrostatically induced superconductivity in two of these (open symbols) (reproduced from ref. 140). (b) Dual-side gated a-IGZO TFT on a silicon substrate used for field induced activation testing and transfer characteristics of an IL gate activated flexible IGZO TFT (reproduced from ref. 138).

decomposition and organic residue removal. If insufficient thermal energy is available for the consumption of hydroxides and the decomposition of anions, the M-O-M structure formation and oxygen vacancy formation are affected and excess trap sites are generated, leading to degraded TFT device characteristics.

2.2.1 Precursor and solvent selection. For the precursor route of metal oxide film formation for MO thin film transistors, the choice of the precursor and solvent plays a vital role in the structural and electrical properties of the resultant metal oxide film. The figures of merit of a TFT such as the mobility, subthreshold swing and threshold voltage are predominantly influenced by the physical properties of the films such as M-O, M-OH and oxygen vacancy content, density, defect concentration, the presence of impurities etc. and these are in-turn dependent on the precursors and solvent utilized. Of the various metal precursors available, chlorides, acetates and nitrates have been widely adopted for the formation of metal oxide films. 142 A comprehensive study has been conducted by Kim et al. to investigate and analyze the effect of precursors and solvent on MO TFTs. 143 The mobility and threshold voltage of the fabricated MO TFTs are influenced by the type of precursor and type of solvent, respectively, (Fig. 8a). Analytical studies proved that the precursor type affected the trap density and also the band mobility, which is an indication of s orbital overlap, while the solvent, which determines the metal-ion complex formed in the precursor solution, affected the deep level traps, dependent on the number of metal interstitials. Of the various precursors, nitrate-based MO-films demonstrated the highest field-effect mobility and lowest trap density, while the use of acetonitrile as the solvent leads to the highest threshold voltage. XPS investigations corroborated the findings and illustrated that the nitrate-based films display the lowest M-OH content, resulting in reduced trap density and the largest M-O to M-OH bond area ratio, resulting in the highest s orbital overlap. The precursor type was also found to affect the density of the film formed and hence the mobility, by virtue of the volume of the decomposed ions and atoms in the precursors. Nitrates also yielded MO films with the highest density while chlorides by virtue of their inherent defects yielded MO films with the lowest density. Among the various metal precursors used such as chlorides, acetates and nitrates, the latter also shows the weakest anion complexation, which ensures complete anion decomposition at lower temperatures.144 The use of nitrate precursors thus provides an approach to reduce the thermal energy required for the formation of high-quality MO films with reduced hydrates and other M-O-M network disrupting impurities by virtue of anions capable of lower temperature decomposition, as is evident from the thermogravimetric studies (Fig. 8b). Metal alkoxides are a class of precursors, which afford the formation of metal oxide films at low temperatures in the presence of an aqueous catalyst or in an aqueous environment. H. Sirringhaus et al. have demonstrated a sol-gel on chip process using an indium alkoxide cluster and zinc-bis-methoxyethoxide in which an in situ process involved the use of a controlled

amount of water vapor to facilitate hydrolysis on the surface of a spin coated film, resulting in metal-oxide film formation at a low temperature of 230 °C with a low M-OH content. The fabricated TFT exhibited a mobility of 10 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>,  $V_{on} = 0$ V, high  $I_{\rm on}/I_{\rm off}^{108}$  and low hysteresis with stable, repeatable performance and high operational stability. 145 Solution processed MO TFTs typically employ 2-methoxy ethanol or similar alcohol-based solvents for precursor solutions. Recently, water has emerged as a contender by virtue of its ability to carbon residue-free films at low processing temperature. 66,146,147 Ionic species dissociation is promoted by the high polarity and high dielectric constant (~80) of the aqueous solvent and by acting as a sigma donor, resulting in the formation of hexaaqua complexes as shown in Fig. 8d. Water, when used for the fabrication of both Al<sub>2</sub>O<sub>3</sub> dielectric and In<sub>2</sub>O<sub>3</sub> films, resulted in TFTs with a mobility of ~38 cm<sup>2</sup>  $V^{-1}$  s<sup>-1</sup> and an  $I_{on}/I_{off}$  of 10<sup>7</sup> at a processing temperature of 250 °C. 148 The duration and temperature at which aqueous precursors are processed before spin-coating also exhibit significant impact on the MO film formed. According to Park et al., precursors retained at 70 °C for longer durations (12-72 h) have a higher concentration of dissociated cations which results in a higher concentration of hexaaqua metal ion complexes, critical for the low temperature metal oxide formation using the aqueous route.<sup>59</sup>

2.2.2 Combustion synthesis. As discussed, in the case of solution-processed metal oxides, low temperature annealing results in incomplete metal oxide formation and hydroxyl group rich films. A universal and facile method to reduce the processing temperature of solution-processed metal oxide films viz., combustion synthesis, was demonstrated by Kim et al., in 2011. 149 In the combustion synthesis approach, a fuel additive triggers a localized exothermic reaction with metal nitrate precursors (oxidisers), thereby providing sufficient energy to eliminate the need for a subsequent high temperature annealing for M-O-M network formation and residue removal (Fig. 8e). Acetyl acetone and urea are the commonly used fuels for combustion synthesis of metal oxide films. 150-153 Facchetti et al. reported that the addition of an oxidizing NO2 group to an acetylacetone fuel results in an enthalpy of combustion of 988.6 compared to 784.4 J g<sup>-1</sup> of acetyl acetone and an ignition temperature of 107.8 °C compared to 166.5 °C of acetylacetone (Fig. 8f). 154 This results in a lowering of the processing temperature for the formation of metal oxide films while simultaneously resulting in denser films with a higher M-O-M content. Non-toxic and environmentally safe carbohydrates such as sorbitol, sucrose and glucose as co-fuels have been shown to be effective at increasing the enthalpy of the overall reaction. 155 Their optimized incorporation into the fuel system results in a dense, smooth, high-quality metal oxide content as is clear from XPS and thickness measurements, where the M-O-M to total O 1s peak ratio and film densification are the highest at a 10% sugar content, as shown in Fig. 8g, with the higher sugar content adversely affecting the film formation due to exploitation of oxidizers for excess sugar decomposition and the generation of

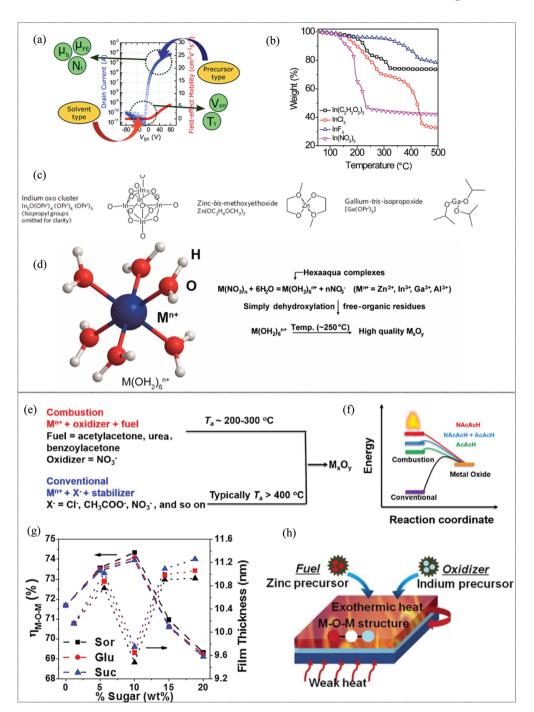


Fig. 8 (a) Illustration of the effect of the solvent and precursor type on the TFT device characteristics (reproduced from ref. 143), (b) thermogravimetric analyses of the various aqueous metal precursors of In(C<sub>2</sub>H<sub>3</sub>O<sub>2</sub>)<sub>3</sub>, InCl<sub>3</sub>, InF<sub>3</sub>, and In(NO<sub>3</sub>)<sub>3</sub> (reproduced from ref. 148), (c) various alkoxide derivatives used for metal oxide formation (reproduced from ref. 145), (d) structure of the hexaaqua complexes formed in aqueous solvent and the progress of reactions resulting in the formation of metal oxide films (reproduced from ref. 148), (e) combustion vs. conventional synthetic approaches (reproduced from ref. 149), (f) energetics of combustion synthesis for various fuels (reproduced from ref. 154), (g) XPS O 1s M-O-M peak area to total peak area ratio and film thickness vs. sugar concentration (reproduced from ref. 155), and (h) schematic diagram of combustion synthesis via the use of metal precursors bearing the fuel and oxidizer ligands (reproduced from ref. 156).

impurities. With a prudent choice of metal precursors which can act as the source of both the oxidizer and fuel (Fig. 8h), Cho et al. have demonstrated that a self-combustion synthesis can also be activated in a two-component precursor system without the need for further fuels or additives. 156 Combustion synthesis is a viable method for reducing the processing temperature as it is independent of any additional post-processing steps and is readily scalable. However, though combustion can

proceed at temperatures as low as 100 °C, a higher temperature of around 200-300 °C is required to ensure adequate decomposition of the precursors to ignite the combustion, especially since nitrates are generally oxidizers for the combustion synthesis. Due to the thermal ignition required, combustion synthesis is often used in conjunction with CTA, thus requiring a long duration for activation. In addition, the oxygen vacancy generation during the combustion synthesis is determined by the reaction environment, oxygen generated during the combustion reaction and post-treatment. For high performance metal oxide films, a precise control of the reaction environment during processing is thus imperative. 157

## 3. Other low temperature processing approaches

Plasma treatment using hydrogen, argon etc. has also been used for sputtered MO films to improve the device performance under low temperature processing conditions and has also been extended to solution processed MO TFTs. 158,159 Plasma treatment using hydrogen has been used for the decomposition of residual organic species subsequent to the formation of metal oxide layers. This treatment followed by an oxidation step has been shown to increase the stability of the device while improving the TFT device performance. 160 There have recently been reports on the use of NH3 and N2O plasma treatments resulting in improved device performance. 161,162 Other novel techniques include water vapour annealing, 163 where the presence of water vapor leads to efficient hydrolysis reaction for solution processed MO films, resulting in higher M-O and lower M-OH concentrations and photocatalytic reactions using TiO2 under UV irradiation for decomposition of organic residues and defect site reduction. 164 In addition to these novel methods, a combination of various annealing conditions and techniques has been shown to result in improved performance of MO TFTs. Combining plasma treatment with (a) thermal annealing, 165 (b) atmospheric pressure treatment<sup>166</sup> or (c) microwave irradiation<sup>167</sup> has been shown to drastically improve TFT performance.

#### 4. Conclusions and outlook

Significant research effort is being dedicated to achieving low temperature processing for MO TFTs, thus enabling their widespread application in flexible electronics. Conventional annealing techniques such as high-temperature thermal annealing, rapid thermal annealing, laser annealing etc. require high temperature to tune the oxygen vacancy in the metal oxide semiconductor which results in adverse effects on flexible substrates. Replacing the high thermal budget required for such conventional annealing with photochemical, plasma-assisted and microwave annealing techniques is applicable to both vacuum deposited and solution processed MO TFTs. In the case of solution processed MO films, additional avenues are

available such as appropriate selection of precursors, solvents and fuel additives for aiding in combustion synthesis, and reducing the process temperature for the formation of highquality metal oxide films. However, all these techniques except for laser annealing are nonselective, i.e., all the TFTs on the substrates are affected by the process. If selective annealing is required, a complex number of steps will be required, such as photolithography, to tune the attributes of the thin film semiconductor selectively. As discussed in this review, another promising alternative is the athermal oxygen vacancy modulation and defect passivation of the metal oxide film for tailoring the electronic structure, which makes high temperature treatments, typically critical for achieving high performance TFTs, dispensable. Athermal activation using a capping layer or an ionic liquid paves the way for flexible and transparent electronics. In the ionic liquid gating approach, which is limited to charge modulation and accumulation for an ionic liquid TFT, the high electric field of the order of 50 MV mm<sup>-1</sup> present at the interface due to Helmholtz layers can be used to vary the oxygen ions present in the film. The controlled manipulation of oxygen vacancies changes the conductance of the film in a precise manner which is of interest for novel applications such as neuromorphic electronics. Such techniques also allow for selective treatments on individual TFTs within a large substrate. The metal capping layer approach facilitates the decrease of weakly bonded oxygen density or reduction in the defect density by partial crystallization of the underlying AOS layer at low temperature. This structure has shown high  $\mu_{FE}$  and enhanced stability simply by adopting a selective metal capping layer while ensuring reduction in the process temperature as discussed in the above sections. Apart from the options discussed in the review, manipulation of the active layer structure is another viable alternative for achieving high performance metal oxide TFTs. Hybrid metal oxide-2D TFTs have been investigated, where the addition of high conductivity 2D materials, such as graphene/CNT, in the active layer stack leads to enhanced TFT mobility. Hybrid metal oxide-2D heterostructure and quasi-superlattice metal oxide stacks are another class of active layers employed for realizing high mobility TFTs at low processing temperature. According to reports, the ultrathin metal oxide layers that form these active layers enable the manifestation of a 2D charge transport phenomenon, while the incorporation of a deep Fermi level metal oxide in the stack results in a higher  $I_{on}/I_{off}$  ratio. Compared to initial research studies, effort is now being made to ensure that the methods used for enhanced device performance at lower processing temperatures do not adversely affect the device stability. Metal oxide semiconductors are also highly sensitive to their atmosphere, and exposure to moisture and oxygen can affect device stability, an issue which needs to be addressed. As discussed, researchers have reported that using capping layers, such as Al2O3, SiO2, Y2O3, HfO2, ZrO2, TiO<sub>2</sub>, AHO (Al<sub>2</sub>O<sub>3</sub>-HfO<sub>2</sub> stack) and ATO (Al<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub> stack) can improve the stability of oxide semiconductors in air and at higher temperatures. In addition, the scalability and production-line compatibility of the various techniques for reducing the processing temperature of metal oxide semiconductors should also be thoroughly examined. With continued research efforts being made to realize stability, scalability and low temperature processing, metal oxide thin films are the most promising material system for propelling flexible and transparent electronics into a ubiquitous technology.

## Conflicts of interest

There are no conflicts to declare.

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