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## Salient space detection algorithm for signal extraction from contaminated and distorted spectrum

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An algorithm for signal extraction from a contaminated and distorted spectrum is proposed. First, this algorithm combines the salient space of the spectrum and the statistical characteristics of the noise to detect signal regions at different scales. Second, it extracts signals by subtracting the baseline from the spectrum in the signal regions. The baseline is fitted by segmented polynomial functions. This algorithm has been applied to simulated and experimental data, and the results show that this algorithm can accurately and automatically extract signals with varying widths from a contaminated spectrum. This method minimizes the influence of baseline distortion and exhibits good anti-noise capability and high real-time performance.

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### 1 Introduction

A spectrum can be used to extract information from a sample such as the chemical and physical structure of a material,<sup>1,2</sup> or the concentration of a solution.<sup>3,4</sup> Spectrum is widely used in many fields such as mass spectrometry and chromatography. However, random noises and irregular baseline distortions, which can arise from several hardware and processing sources, inevitably exist in the spectrum.<sup>5</sup> These interferences in a spectrum result in incorrect detection of signal regions (representing the structural information of the sample) and inaccurate calculation of signal intensity<sup>6,7</sup> (denoting the concentration of the sample). Thus, it is important to avoid the influence of these interferences to correctly and accurately extract signals from the spectrum.<sup>8</sup>

Many methods have been used to extract signals such as the zero-crossing technique<sup>9</sup> (searching for zeros in the first derivative and treating these positions as signal regions), thresholding algorithm<sup>6,7</sup> (where only points three times larger than the standard deviation of the spectrum noise are treated as signal points) or wavelet decomposition and integration.<sup>10–13</sup> All these methods have significantly contributed to signal extraction. The zero-crossing technique is the simplest method to extract signals, but it is invalid when noises exist.<sup>9</sup> Thresholding algorithm is one of the mainstream approaches in signal extraction because of its simplicity and anti-noise capability. However,

two issues must be addressed. First, weak signals, having peaks three times smaller than the standard deviation of the spectrum noise, are lost in the spectrum. Second, the accuracy of this approach is adversely affected by the baseline, and this approach may fail because baseline distortions can be significantly larger than peak intensities.<sup>6</sup> Wavelet decomposition is widely used to eliminate baseline rolling before the thresholding algorithm or even to directly extract signals.<sup>14</sup> However, its accuracy is often influenced by the wavelet base and the number of decompositions, which are often chosen by experience, thereby restricting its applicability.<sup>15,16</sup>

In several literatures, the baseline is corrected before signal extraction to reduce baseline influence.<sup>17</sup> However, baseline correction of the whole spectrum is difficult, and it increases the computational problem. Furthermore, many methods must remove signal regions before baseline correction to acquire a better baseline.<sup>6</sup> Thus, baseline correction and signal extraction are typically restricted by each other.<sup>18</sup>

Algorithms that do not use a model of the baseline or signal shape and that have anti-noise capability are preferred. Many iterative algorithms<sup>19–21</sup> and Difference-of-Gaussian (DoG) functions can meet this requirement. Adaptive iteratively reweighted penalized least squares (airPLS) is a well-known iterative algorithm, because it is flexible and valid; however, it needs further optimization. Lowe<sup>22,23</sup> proposed DoG for image processing, and it has also been used for signal extraction.<sup>24</sup> Furthermore, DoG can automatically extract signals of different widths in the same spectrum, and its accuracy is seldom influenced by baseline and noise. However, applying DoG is time consuming.

Herein, we propose Salient-Space-Detection algorithm (SSD) for signal extraction. SSD has been developed with reference to

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DoG and noise statistics. SSD has all of the advantages of DoG, and it gives more real-time and accurate results than other algorithms.

We have evaluated our method using simulated spectra, and we have applied it to real measured spectra. The results show that the algorithm is robust, real-time and accurate for signal extractions of different kinds of spectra.

## 2 Methods

### 2.1 Signal region detection

Signal region detection based on SSD can be represented as follows:

First, the background space of a spectrum is defined as a function,  $B(x, r)$ , obtained by averaging the offset spectrum,  $I(x - r)$  and  $I(x + r)$ , of the original input spectrum,  $I(x)$ .

$$B(x, r) = [I(x - r) + I(x + r)]/2 \quad (1)$$

Here,  $r$  is the offset value of the original spectrum, which also represents the scale of the background spectrum. Different values of  $r$  produce various background spectra. All background spectra constitute the background space.

Second, the salient space,  $H(x, r)$ , can be obtained from the difference of the original spectrum and background space.

$$H(x, r) = \begin{cases} I(x) - B(x, r), & \text{spectrum is positive} \\ B(x, r) - I(x), & \text{spectrum is negative} \end{cases} \quad (2)$$

Here, a positive spectrum is a spectrum, such as a Raman spectrum, having peaks larger than the baseline. A negative spectrum is a spectrum, such as an absorption spectrum, having peaks smaller than the baseline.

As shown in Fig. 1a, the half-breadths of the square signal and the sharp Gaussian signal are 8 and 4 points, respectively (the width of a signal was defined as the total number of points having amplitude that is 1% larger than the maximum amplitude of this signal). Salient space, which can be obtained by eqn (2), is shown in Fig. 1b–f. When the scale of the salient space conforms to the half-breadth of the signal, the result of  $H(x, r)$  reaches its maximum at the centre of the signal region.

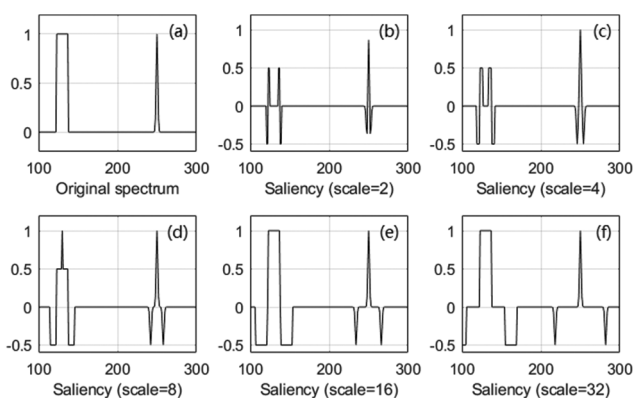


Fig. 1 Saliency of typical salient space. The horizontal and vertical axes of (b)–(f) represent position and saliency, respectively.

Thus, detecting the maximum of  $H(x, r)$  can help derive signals with different widths.

Next, the central coordinates of signal regions,  $X_{sc}$ , and the half-breadth of signal regions,  $R_s$ , are obtained by detecting the maximum of  $H$ .

$$(X_{sc}, R_s) = \left\{ (x, r) \begin{cases} H(x, r) > H(x, r - \Delta r) \text{ and} \\ H(x, r) = \max(H(x)) \text{ and} \\ H(x, r) = \max(H(x - 1, r), H(x, r), H(x + 1, r)) \end{cases} \right\} \quad (3)$$

Here,  $\Delta r$  is the difference of two nearby scales.

Noises are neglected in eqn (3). When noises are existed, as shown in Fig. 2, the maximum of  $H(x, r)$  is not guaranteed to be at the centre of the signal region even if the scale of salient space conforms to the half-breadth of the signal.

The most common method to decrease the influence of noise is denoising. However, most denoising methods inevitably weaken the signal intensity and induce spectrum distortion. Thus, we choose to revise eqn (3) instead of denoising the original spectrum before SSD.

First, the absolute mean of the noises,  $\mu_r$ , of each scale of the salient space is calculated. All points larger than  $k\mu_r$  and the mean value of the  $d$  neighbourhoods larger than  $\mu_r$  are then treated as candidate points of signal regions.

$$\mu_r = \frac{1}{N_h - 1} \sum_{x=2}^{N_h} \text{abs}(H(x, r) - H(x - 1, r)) \quad (4)$$

$$X_{ts} = \left\{ x \left| \frac{H(x, r) > k\mu_r}{\frac{1}{2d + 1} \sum_{i=x-d}^{x+d} H(i, r) > \mu_r} \right. \right\} \quad (5)$$

Here,  $N_h$  is the total number of points in  $H(x, r)$ , and  $k$  and  $d$  are constants; their values can be set as 2 and 4, respectively (these values correspond to the confidence level of 99% under normal distribution).

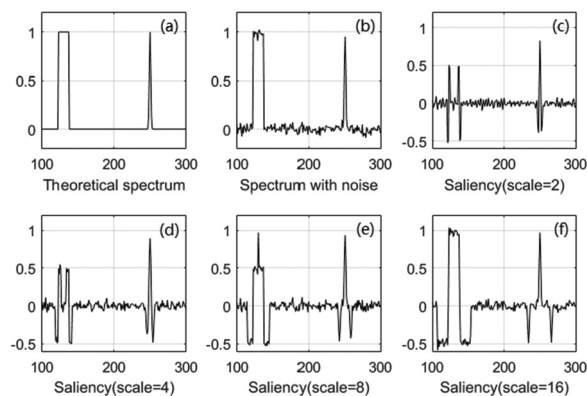


Fig. 2 Noise influence. The maximum saliency of the square signal is not at the centre of the signal and is not obtained when the scale equals half-breadth.



If only signal regions with peaks clearly larger than the noise can be detected, then  $k$  can be set at a value larger than 3, and eqn (5) can be simplified as eqn (6).

$$X_{ts} = \{x | H(x, r) > k\mu_r\} \quad (6)$$

Next, the start and end coordinates,  $X_s$  and  $X_e$ , of the signal regions are obtained by eqn (7) and (8), respectively.

$$X_s = \{(x_1 - r_T) \cup (x_j - r_T) | x_j - x_{j-1} > r_T \quad j \in (2, N_s)\}, \quad (7)$$

$$X_e = \{(x_j + r_T) \cup (x_{N_s} + r_T) | x_{j+1} - x_j > r_T \quad j \in (1, N_s - 1)\}. \quad (8)$$

Here,  $x_j$  represents the candidate signal points,  $N_s$  is the total number of these points, and  $x_1$  and  $x_{N_s}$  are the first and the last candidate signal points, respectively.  $r_T$  is a threshold, and it should be set at  $3\Delta r$  to get good results.

## 2.2 Signal extraction

Once the signal regions are detected, only the baseline of the signal regions is necessary to extract the signals. Thus, we cut the baseline into many segments, and we fitted each segment separately. Despite many baseline fitting algorithms, such as linear interpolation,<sup>6</sup> iterative moving averaging,<sup>25</sup> and Whittaker Smoother,<sup>26</sup> we choose a lower-order polynomial function<sup>27</sup> to fit the baseline. This choice is attributed to the smooth, real-time polynomial fitting while showing fidelity to the original data when the spectrum is divided into many segments.

First, a certain number of neighbour points of a signal region are chosen. Second, the baseline of this signal region is fitted by a lower-order polynomial function using the chosen points. Finally, signals can be extracted by subtracting the baseline from the spectrum at signal regions.

## 3 Experimental

We applied the algorithm to various spectra, including simple simulated spectra with constructed data, complex simulated spectra with absorption data, Nuclear Magnetic Resonance (NMR) data, real absorption spectra obtained by experiments and real Raman spectra from the Handbook of Minerals Raman Spectra database,<sup>28</sup> to evaluate its performance.

Simulated spectra were used because their theoretical signal regions and intensities were known; thus, evaluating the accuracy of the algorithm was easy. Real spectra were utilised because they can indicate the effect of an algorithm in real applications.

### 3.1 Simple simulated data

Simple simulated data were employed because they can show the process and results clearly.

All simulated spectra can be expressed as follows:

$$s(x) = a(x) + n(x) + b(x). \quad (9)$$

Here,  $a(x)$  is the theoretical signal,  $n(x)$  is the Gaussian noise,  $b(x)$  is the theoretical baseline and  $s(x)$  is the simulated spectrum.

More than 20 000 spectra were simulated with various SNRs (signal-to-noise ratios) and SBRs (signal-to-baseline ratios) to evaluate SSD performance. A Gaussian curve was used as the theoretical baseline in these spectra. The Gaussian curve used was typical; it had abundant curvatures in a single line. Four typical signals were constructed to enhance the simulation: one square signal, one sharp Gaussian signal, one broad Gaussian signal and one substantially overlapped signal. Fig. 3 shows the entire process; SNR and SBR used in this example were 30 and 0.2, respectively.

### 3.2 Complex simulated data

Spectra, such as real absorption and real NMR spectra, containing large amounts of data were simulated.

From the HITRAN spectroscopic database,<sup>29</sup> we can obtain the absorption intensity coefficient,  $a(\nu)$ , of  $C_2H_2$ . We chose the coefficient larger than  $0.0059 \times 10^{-19}$  as pure absorption peak, multiplied it by  $5 \times 10^{19}$  and designed each peak as Gaussian distribution. Thus, we derived the pure absorption spectrum,  $a(x)$ . The spectrum length was designed as 7200 sample points, mimicking that of the  $C_2H_2$  experimental spectra. Noise was then added to the pure absorption spectrum. Finally, the spectrum with noise was added to the theoretical baseline. The theoretical baseline,  $b(x)$ , was set as a slash connected with a Gaussian curve. This kind of baseline has abundant curvature, and it is more typical than a Gaussian curve.

The simulated NMR spectrum was extracted from the real NMR spectrum offered by Qingjia Bao.<sup>7</sup> First, we used DoG to detect the signal regions of real spectrum. Second, we fitted the baseline based on segmented lower-order polynomial fitting and segmented kernel smoothing.<sup>22</sup> Third, we extracted the signals as theoretical spectrum by subtracting the baseline from the real spectrum at signal regions. Finally, we added the noise and theoretical spectrum to the theoretical baseline, with its theoretical baseline,  $b(x)$ , set as a slash connected with a Gaussian curve.

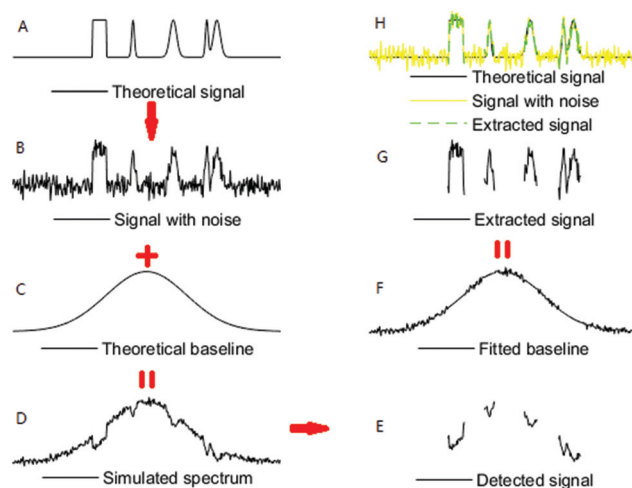


Fig. 3 Illustration of the whole process of simulated signal extraction.



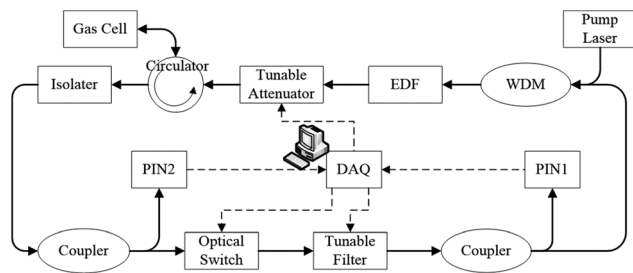


Fig. 4 Schematic of the  $C_2H_2$  experiment system.

### 3.3 Real absorption data

The efficiency of the SSD algorithm was also evaluated by  $C_2H_2$  absorption spectrum. The gas sensing system we used was an intra-cavity fibre ring laser gas sensing system (Fig. 4). The system consisted of an EDFA pumped by a 980 nm diode laser, a variable attenuator, a circulator, a gas cell with reflector, an isolator, a fibre coupler, and a Fabry–Perot tunable filter (TF), and its transmission wavelength was controlled by the controlling voltage from data acquisition equipment (DAQ); the system also consisted of two InGaAs PIN photodetectors with an operating wavelength of 1000–1650 nm and a DAQ of NI-USB-6251. The EDFA wavelength region was 1525–1565 nm. The bandwidth and the free spectral range of TF were 0.0353 and 200 nm, respectively. The length of the gas cell was 20 cm, and the gas concentration was 1%.

We utilised the amplified absorption intensity coefficient,  $a(\nu)$ , as the theoretical intensity in the experiments.

### 3.4 Real Raman data

Real Raman spectral data were obtained from the Handbook of Minerals Raman Spectra database. These real spectra have different SNRs and baselines. We chose three typical spectra, *i.e.*, spectra of adamite, fluorliddicoatite and abelsonite. The baseline of adamite is similar to a Gaussian curve connected with a slash. The baselines of fluorliddicoatite and abelsonite are more complex. These three spectra simultaneously have sharp, broad, strong and weak signals. Additionally, these spectra have signals that overlap with each other. The corresponding processed spectra were also given in the database. We used the processed spectra as the criteria for our comparison of SSD, DoG and airPLS.

## 4 Results and discussion

### 4.1 Influences of SNR and SBR

The influences of SNR and SBR were studied using simple simulated data. Table 1 shows that the accuracy of SSD was influenced by SNR and SBR in the following ways. (1) When SNR and SBR were smaller than 20 and 0.5, respectively, signal extraction may fail; otherwise, signals can be extracted all the time. (2) As SNR and SBR increased, the standard derivation of power error always decreased, whereas the mean error some-

Table 1 Extracted signal power error (%) with various SNRs and SBRs. P1, P2, P3 and P4 represent square, sharp Gaussian, broad Gaussian and overlapped signals, respectively. Mean and std represent the mean value and the unbiased estimation of standard derivation of the power error, respectively. "Non" means signals under these parameters could not always be extracted; thus, no statistical results are available

SNR \ SBR	P1			P2			P3			P4		
	0.2	0.3	0.5	0.2	0.3	0.5	0.2	0.3	0.5	0.2	0.3	0.5
20	mean	Non	Non	Non	Non	Non	Non	Non	Non	Non	Non	Non
	Std	Non	Non	Non	Non	Non	Non	Non	Non	Non	Non	Non
30	mean	-0.6	0.2	-1.0	0.2	0.4	-0.6	-0.2	-1.0	0.6	0.6	-0.4
	Std	15.0	9.3	6.4	4.1	3.3	13.7	10.3	6.7	4.1	3.2	14.8
50	mean	1.0	0.7	0.4	0.1	0.0	1.1	0.1	1.1	0.6	0.3	0.1
	Std	3.3	2.2	1.4	1.0	0.0	3.3	2.2	1.4	1.0	0.0	3.3
75	mean	1.1	0.6	0.3	0.1	0.0	1.1	0.1	1.1	0.6	0.3	0.1
	Std	3.0	2.0	1.0	0.0	0.0	3.0	2.0	1.0	0.0	0.0	3.0
100	mean	1.1	0.6	0.3	0.1	0.1	1.1	0.1	1.1	0.6	0.3	0.1
	Std	3.0	2.0	1.0	0.0	0.0	3.0	2.0	1.0	0.0	0.0	3.0
20	mean	Non	Non	Non	Non	Non	Non	Non	Non	Non	Non	Non
	Std	Non	Non	Non	Non	Non	Non	Non	Non	Non	Non	Non
30	mean	-2.1	12.1	12.1	-0.1	9.0	9.5	-0.6	-1.3	12.2	12.2	-1.3
	Std	9.3	-0.9	0.1	0.2	-1.0	0.2	0.4	-0.6	-0.6	-0.6	-0.6
50	mean	1.0	0.7	0.4	0.1	0.0	1.1	0.1	1.1	0.6	0.3	0.1
	Std	3.3	2.2	1.4	1.0	0.0	3.3	2.2	1.4	1.0	0.0	3.3
75	mean	1.1	0.6	0.3	0.1	0.0	1.1	0.1	1.1	0.6	0.3	0.1
	Std	3.0	2.0	1.0	0.0	0.0	3.0	2.0	1.0	0.0	0.0	3.0
100	mean	1.1	0.6	0.3	0.1	0.1	1.1	0.1	1.1	0.6	0.3	0.1
	Std	3.0	2.0	1.0	0.0	0.0	3.0	2.0	1.0	0.0	0.0	3.0
20	mean	-2.1	12.8	12.8	-0.7	8.9	8.9	-0.7	-1.1	11.0	11.0	-1.1
	Std	9.3	0.0	0.0	0.4	-0.3	-0.3	0.4	-0.3	-0.3	-0.3	-0.3
30	mean	1.0	0.7	0.4	0.1	0.0	1.1	0.1	1.1	0.6	0.3	0.1
	Std	3.3	2.2	1.4	1.0	0.0	3.3	2.2	1.4	1.0	0.0	3.3
50	mean	1.1	0.6	0.3	0.1	0.0	1.1	0.1	1.1	0.6	0.3	0.1
	Std	3.0	2.0	1.0	0.0	0.0	3.0	2.0	1.0	0.0	0.0	3.0
75	mean	1.1	0.6	0.3	0.1	0.0	1.1	0.1	1.1	0.6	0.3	0.1
	Std	3.0	2.0	1.0	0.0	0.0	3.0	2.0	1.0	0.0	0.0	3.0
100	mean	1.1	0.6	0.3	0.1	0.1	1.1	0.1	1.1	0.6	0.3	0.1
	Std	3.0	2.0	1.0	0.0	0.0	3.0	2.0	1.0	0.0	0.0	3.0



times oscillated if SNR was smaller than 50. (3) When SNR was smaller than 50, the mean and standard derivation of power error worsened rapidly as the SNR decreased; otherwise, they were almost stable and had high accuracies. The largest mean and standard derivation values were 1.1% and 3.3%, respectively. (4) The change in the accuracy with SNR was larger than that with SBR.

The statements (1), (2) and (3) indicate that SSD has strong anti-noise and anti-baseline-distortion capability; however, its accuracy and stability are still influenced by noise and baseline distortion. Thus, SSD cannot be used only when both SNR and SBR are too small. The statements (2), (3) and (4) indicate that the influence of SNR is larger than that of SBR and thus, improving the denoising performance may be important for future studies.

SBR and power error are defined as follows:

$$\text{SBR} = \frac{\max(a(x))}{\max(b(x))} \quad (10)$$

$$\text{Error} = \frac{\sum_{i=1}^n a_E^2(x_i) - \sum_{i=1}^n a^2(x_i)}{\sum_{i=1}^n a^2(x_i)} \quad (11)$$

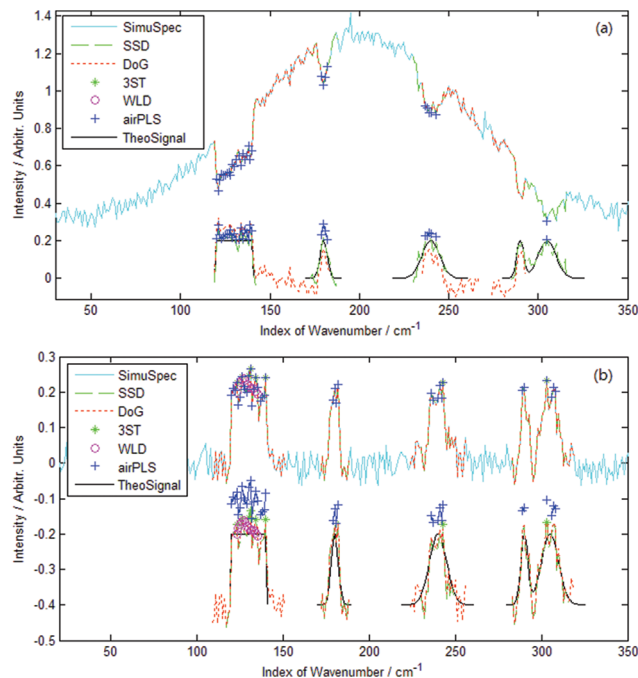
Here,  $n$  is the number of extracted signal points,  $a_E(x_i)$  is the intensity of the extracted signal and  $a(x_i)$  is the intensity of the theoretical signal.

## 4.2 Comparison with other algorithms

Fig. 5 shows the signal region detection results of two simple simulated spectra. SimuSpec and TheoSignal represent the simulated spectrum and theoretical signals, respectively, SSD represents the proposed algorithm, DoG denotes the DoG algorithm, 3ST represents the thresholding algorithm, WLD denotes wavelet decomposition combined with the thresholding algorithm and airPLS denotes airPLS combined with the thresholding algorithm. Of all the detected signal regions, the one detected by SSD is the most accurate, regardless of whether the theoretical baseline is chosen as a Gaussian curve or a horizontal line and regardless of whether the signal is negative or positive. Please note that in Fig. 5a, no signal points were detected by 3ST or WLD. However, the above-mentioned comparison is only based on a contaminated spectrum. A good result can also be obtained by 3ST when the baseline is a horizontal line and SNR is high.

DoG and airPLS were used to compare with SSD in the next experiments because they are more accurate than 3ST and WLD.

**Accuracy.** Fig. 6 presents the results of a simulated  $\text{C}_2\text{H}_2$  absorption spectrum. The signal regions detected by SSD are more accurate than those detected by DoG. Additionally, the overlapped signal regions near 1527 nm, and the weak signal region, which is drowned out by the noise near 1540 nm, are accurately detected. All signal regions are detected without any false-positive or false-negative considerations. Even while evaluating the accuracy in points, the false-positive (ratio of mis-



**Fig. 5** Comparison of different methods: (a) Gaussian and (b) horizontal baselines. SimuSpec and TheoSignal represent the simulated spectrum and theoretical signals, respectively; SSD represents the proposed algorithm, DoG denotes the DoG algorithm, 3ST represents the thresholding algorithm, WLD and airPLS denote the wavelet decomposition and airPLS combined with the thresholding algorithm, respectively. The lower part of (a) and (b) are the extracted signals and extracted signals with  $-0.4$  offset in  $y$  coordination, respectively.

taken signal points to total signal points) and false-negative (ratio of missed signal points to total signal points) values are found to be below 6.5%. The total false value (ratio of both mistaken points and missed points to total points) is only 1.06%. Fig. 6c shows that at 1535.4 nm, even SSD and DoG extract signals; however, the signal intensity extracted by SSD is often more accurate than that extracted by the DoG algorithm. The reason may be the difference between their denoising capabilities.

DoG has denoising capability because it obtains its scale space by convolution, as shown in eqn (12). Convolution, like a smooth filter, is influenced by the convolution radius. When the radius is too small, it cannot eliminate the noise, and some noise points, such as those at about 1526.1 and 1533.6 nm, may be treated as signal points, as shown in Fig. 6b. If the radius is too large, some signal points, such as that at about 1526.7 nm, are reduced and treated as baseline points, as shown in Fig. 6b.

$$D(x, \sigma) = (G(x, k\sigma) - G(x, \sigma)) * I(x) \quad (12)$$

Here,  $G(x, k\sigma)$  and  $G(x, \sigma)$  are the variable-scale Gaussian functions,  $\sigma$  is in proportion to the convolution radius,  $I(x)$  is the original input spectrum and  $D(x, \sigma)$  is the Difference-of-Gaussian. By detecting the maximum or minimum of  $D(x, \sigma)$



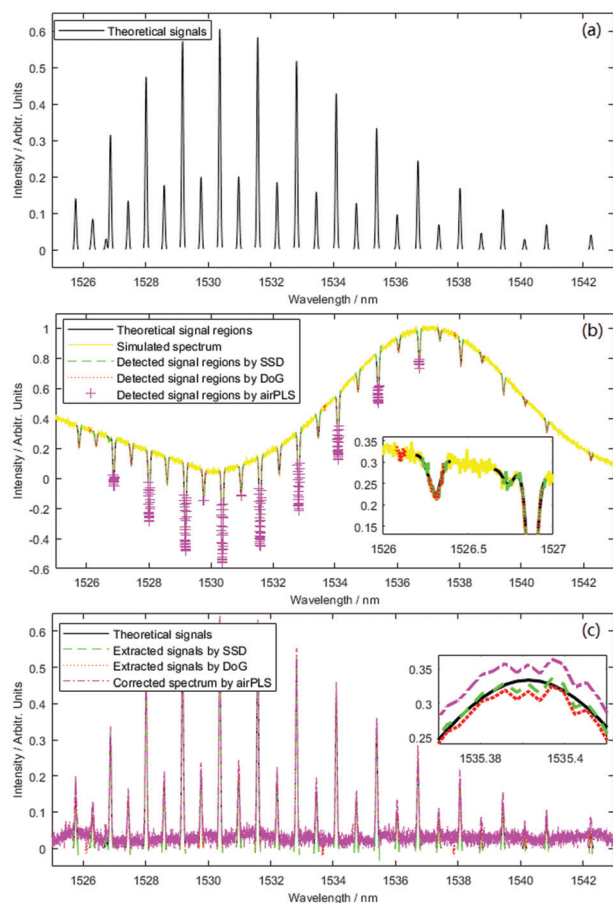


Fig. 6 Simulated data of  $C_2H_2$  absorption spectrum: (a) theoretical spectrum, (b) signal region detection and (c) signal extraction.

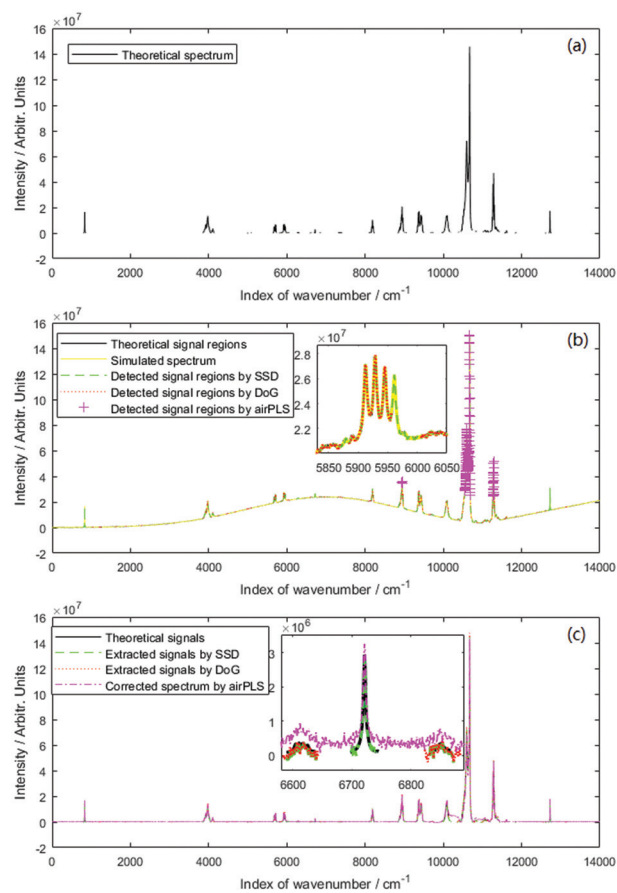


Fig. 7 Simulated data of NMR spectrum: (a) theoretical spectrum, (b) signal region detection and (c) signal extraction.

in various scale spaces, we can detect signals with various widths.

SSD uses noise statistics, as shown in eqn (4) and (5), to decrease the influence of noise. Additionally, SSD is not affected by the baseline or scale of salient space, and its confidence level is larger than 99%. Thus, SSD is more accurate than DoG.

AirPLS can correct the spectrum, but neither its signal region detection nor intensity accuracy is as good as those of SSD or DoG, as shown in Fig. 6b and c; this is because airPLS does not have strong anti-noise capacity, and the anti-baseline-distortion capability is not as good as is supposed.

Fig. 7 presents the results of a simulated NMR spectrum. The analysis is omitted here for brevity because the phenomena of Fig. 7 are the same as those of Fig. 6. Thus, we can conclude that SSD is more accurate than DoG, and DoG is more accurate than airPLS.

**Real-time performance.** Signal extraction by SSD is real-time, because it does not use time-consuming algorithms such as convolution or iteration. However, some parameters can still influence real-time performance. One is the difference of two nearby scales,  $\Delta r$ . The other is the range of  $r$ . A constant  $\Delta r = 2$  is used in this paper to guarantee the accuracy and real-time

performance of SSD. If more accuracy is necessary, then  $\Delta r$  should be set to a smaller value. If higher real-time performance is desired, then  $r$  can be set as a geometric series. The variance range of  $r$  is set to 3–19, including the possible half-breadths of the master signal regions. In this paper, the time for signal region detection is 0.011 s, which is only 1/40 of that of DoG.

### 4.3 Real absorption data

An example of a  $C_2H_2$  absorption spectrum showing a poor baseline and broad, contaminating peaks is depicted in Fig. 8a. SSD accurately extracts the signal regions even when the original spectrum is distorted sharply near 1526 nm. As Fig. 8b shows, all signal regions are extracted accurately by SSD, and no false-positive or false-negative observations are observed. The results are in accordance with the simulation results of Fig. 6, with the exception of intensity.

Many factors, such as existing noise and inaccurately extracted baseline, can induce the intensity difference between the theoretical and extracted spectra. However, the most important reason is that the spectrum is obtained by the intra-cavity fibre ring laser gas sensing system. In this system, the absorption length,  $L$ , is not absolutely identical because of the



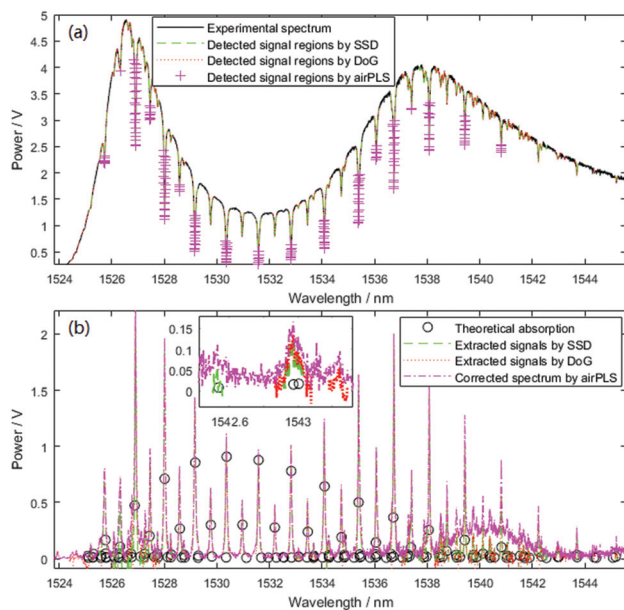


Fig. 8 Experimental data of  $C_2H_2$  absorption spectrum: (a) signal region detection and (b) signal extraction.

difference in the laser's settling time at various wavelengths (the larger the settling time, the longer the absorption length). Although the concentration,  $c$ , is a constant, the product of  $c \times L$  differs at various wavelengths. Thus, the proportions of the real absorption intensity,  $K$ , and absorption intensity coefficient,  $a(\nu)$ , are not the same by Lambert–Beer law as follows:

$$c = K/(a(\nu) \times L) \Rightarrow c \times L = K/a(\nu). \quad (13)$$

Using the same intracavity fibre ring laser gas sensing system, the settling time,  $t_s$ , of large absorption peaks is found to be shorter than that of the small absorption peaks of both sides. The settling time of large absorption peaks near 1530 nm is the shortest and then, it increases slightly as the wavelength increases. Considering  $L = \nu \times t_s$ , we can say that the proportion,  $K/a(\nu)$ , of large absorption peaks should be smaller than that of the small absorption peaks of both sides. The proportion,  $K/a(\nu)$ , of large absorption peaks near 1530 nm should be the smallest, and it should increase slightly with the increase in the distance between the wavelength of the peak and 1530 nm. Fig. 8 shows this deduction.

From Fig. 8 and the analysis mentioned above, we can see that SSD can extract signals from real absorption data, and the result of SSD is better than that of DoG or airPLS.

#### 4.4 Real Raman data

Fig. 9 presents the results of adamite spectrum. The extracted signals obtained by SSD concur with the processed results of the dataset, especially for the signals between 800 and 950  $cm^{-1}$ . Near 200  $cm^{-1}$ , the extracted signal is slightly larger than the database result, but it is still more accurate than the results obtained by DoG and airPLS.

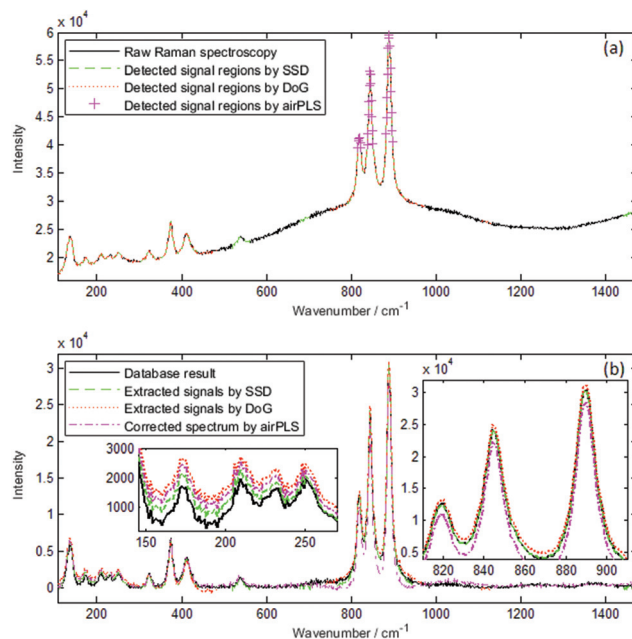


Fig. 9 Real adamite spectrum: (a) signal region detection and (b) signal extraction.

The raw spectra of fluorliddicoatite and abelsonite are even more complex than the adamite spectrum, and identifying where baseline and signals are located, even manually, is difficult. The fluorliddicoatite result obtained by SSD almost concurs with the database result, and it is more accurate than the results obtained by DoG and airPLS. The abelsonite result is not as good as the adamite or fluorliddicoatite result; however, it is better than the result obtained by DoG or airPLS. Fig. 11b shows that the intensity data near 750 and 1210  $cm^{-1}$  obtained by SSD are less accurate than the results obtained by airPLS; however, the results of SSD are better than those of airPLS or similar with those of airPLS at other wavenumber  $s$ . The results obtained by DoG are the least accurate for the abelsonite spectrum. Thus, SSD is the most effective method for the signal extraction of Raman spectra.

SSD is more accurate than DoG and airPLS due to the same reasons mentioned in section 4.2. AirPLS does not have strong anti-noise capability, and the anti-baseline-distortion capability is not as good as is supposed. DoG has strong anti-noise and anti-baseline-distortion capability; however, its convolution radius may influence the signal region detection.

Fig. 9–11 also illustrate that the overlapping of the signals may influence the accuracy of the intensity of the extracted signals, but Table 1 does not show this phenomena. When many signals overlap with each other and combine to form a signal that is too broad, such as the signal near 200  $cm^{-1}$  of Fig. 9 and the signal near 750  $cm^{-1}$  of Fig. 11, some signal points may be treated as baseline points. Thus, the accuracy of the fitted baseline declines and ultimately influences the accuracy of the intensity of these signals. Apart from that, the



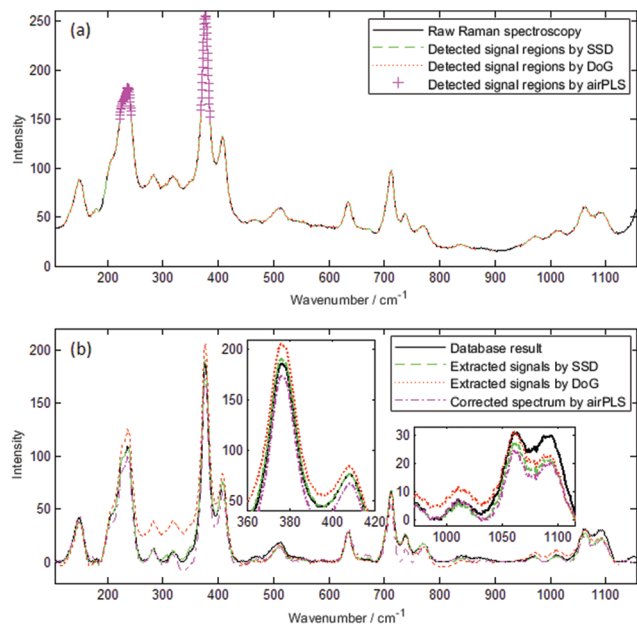


Fig. 10 Real fluoriddicoate spectrum: (a) signal region detection and (b) signal extraction.

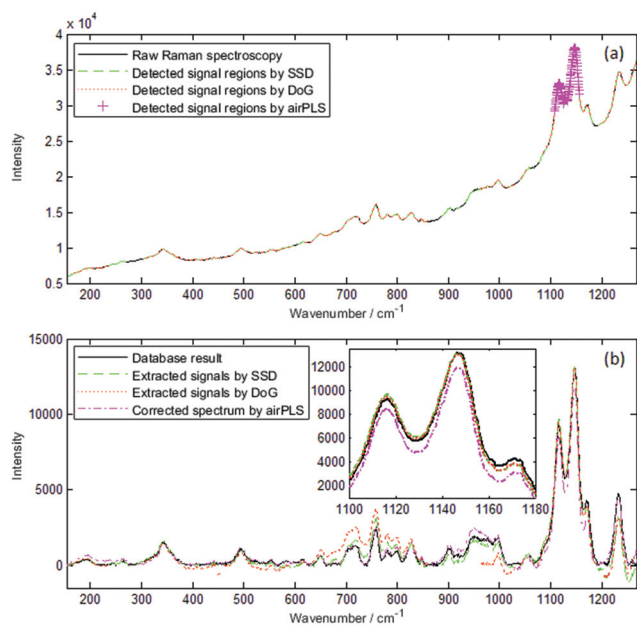


Fig. 11 Real abelsonite spectrum: (a) signal region detection and (b) signal extraction.

intensity of the extracted signals is accurate and is not influenced by the signal and baseline shapes.

## 5 Conclusions

We proposed an SSD algorithm for signal extraction. Experimental results showed that the new algorithm is

effective for most kinds of spectra such as absorption, NMR and Raman spectra. Three main improvements were obtained by using this algorithm. First, SSD could automatically and accurately extract signals even if the spectrum contained broad and sharp peaks synchronously with noise. Second, SSD could minimize the influence of the baseline distortion. Lastly, the proposed algorithm exhibited high real-time performance because it did not require iteration or convolution. The time for signal region detection was only 0.011 s. The total time for signal extraction was only about 0.031 s. We showed that SSD is an enhanced signal extraction method in which the results were not influenced by the baseline or signal shape, and it exhibited anti-noise capability and better real-time performance. Since the SNR value still influenced the accuracy of the extraction result when SNR was smaller than 50, the improvement of the denoising performance is considered in our following studies.

## Conflicts of interest

There are no conflicts to declare.

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