



phenomena.<sup>30–33</sup> In particular,  $\text{Tm}^{3+}$  is known for its transitions between energy levels that result in emissions in the infrared range, making it ideal for temperature sensors and optical communication applications.<sup>14,15,30,33</sup>

PA holds promising applications across various technological fields.<sup>34,35</sup> In optical sensors, the high detection sensitivity offered by PA enables the development of exact temperature measurements. These sensors can detect minute temperature variations based on changes in the luminescence of  $\text{Ln}^{3+}$ -doped materials.<sup>16–18,36</sup> Furthermore, PA is used in signal amplification for optical communication systems, enhancing the efficiency and range of data transmissions.<sup>36</sup> PA can improve imaging techniques in the medical field, providing higher resolution and contrast in visualizing biological structures.<sup>36–38</sup> Current research is also exploring the use of PA in developing solid-state lasers and advanced optoelectronic devices, leveraging its capacity to generate intense and controlled emissions.<sup>36,39</sup>

Recently, interesting optical devices have been developed employing additive manufacturing (AM) technology.<sup>40</sup> In this sense, Zheng *et al.*<sup>41</sup> reported 3D-printed units that exhibit intense mechanoluminescence in response to mechanical impact and friction. Runowski *et al.*<sup>42</sup> fabricated 3D-printed polymers for high-resolution anti-counterfeiting and latent fingerprint detection.<sup>43</sup> Concerning sensors' applications, in previous work, we reported a luminescent gear manufactured by 3D printing that incorporates optically active nanoparticles in resin.<sup>44</sup> Following these novelty researches, a new remote optical temperature sensor is fabricated in this work, combining AM with a photo-curable polymer.

This study focuses on characterizing the photon-avalanche process in  $\text{Tm}^{3+}$ -doped glasses and evaluating their potential as high-sensitivity temperature sensors. We used the glass ceramic to ensure high emission intensity. In contrast to nanoparticles or nanopowders, glasses, and bulk crystals are less prone to quenching processes due to defects in the structure or surface-related interactions with the surrounding environment.<sup>13</sup> Through a series of experiments, we investigated the luminescent emission dynamics under varying excitation and temperature conditions. Additionally, we developed a model to correlate the luminescence intensity ratios with temperature, providing precise calibration of the material for practical applications. We propose a 3D-printed resin-based sensor containing luminescent particles to determine the temperature of the selected environment. We aim to demonstrate these materials' viability as reliable optical sensors and explore their applicability in diverse environments such as air and isopropanol.

## 2. Experimental section

### 2.1. Materials and synthesis

The initial composition for preparing the sample, given in mol%, was  $(40-x)\text{LnF}_3$ ,  $20\text{ZnF}_2$ ,  $20\text{SrF}_2$ ,  $20\text{BaF}_2$ ,  $x\text{TmF}_3$ , where  $x$  was set to 2.5. All chemicals used had a minimum purity of

99.5%. The mixture corresponding to this composition was first heated at 673 K for one hour with  $\text{NH}_4\text{F}\cdot\text{HF}$  to ensure the conversion of any residual oxides into fluorides. Afterward, the mixture was melted at 1446 K. The molten material was then cast into an aluminum mold preheated to 796 K, producing glass plates with a thickness of 1–2 mm.<sup>30</sup>

A natural 3D850 SMARTFIL polylactic acid (PLA) filament of 1.75 mm in diameter from Smart Materials 3D was used to manufacture the temperature sensor. The prototype was designed with Tinkercad software, and the digital design was exported in surface tessellation language (STL) format. The STL file was imported to the Bambu Studio slicer to select the manufacturing parameters and generate the G-code file. Finally, the specimen was printed by fused deposition modeling (FDM) using a Bambu Lab X1 Carbon printer. During manufacturing, fixed parameters were layer width of 0.4 mm, layer height of 0.2 mm, 100% infill pattern density, bed temperature of 323 K, extruder temperature of 493 K, and deposition speed of  $30\text{ mm s}^{-1}$  for the base and  $25\text{ mm s}^{-1}$  for the sensor part.

The resin employed was a Simple Siraya Tech, which consists of a mixture composition of urethane acrylate (CAS no. 877072-28-1, wt% = 20–50%), acrylic monomer (CAS no. 64401-02-1, wt% = 30–60%), and photoinitiator (CAS no. 119-61-9, wt% = 0–5%). The resin was doped with the optically active material, which was initially ground using a mortar to reduce its size and then processed in a ball mill for 1 hour at 600 rpm in reversing mode to ensure homogeneous milling and obtain a powder. The doped resin was then coupled to the PLA specimen and cured under an UV lamp at 365 nm.

A small piece was fabricated and submerged in isopropanol for two weeks to control the stability in service of this temperature sensor. After this period, it was verified that the sample did not lose any mass and the geometric was perfectly preserved.



Fig. 1 Temperature sensor fabricated using fluorindate glass through 3D printing.



The experiment ensures the use of the prototype as a temperature sensor in this aqueous medium (see Fig. 1)

## 2.2. Characterization

A tunable CW Ti:sapphire laser system (Spectra Physics 3900S) pumped by a 532 nm laser (Spectra-Physics Millennia) and tuned to 1060 nm was used to excite the sample. The excitation intensity was varied by changing the laser power, and the Gaussian beam was focused on the sample with a 20 mm lens. The waist spot size on the sample (defined as the  $1/e^2$  radius of the intensity) was shown to be  $5.6 \times 5.6 \mu\text{m}^2$ . The temporal evolution measurements were obtained by modulating the beam with a mechanical chopper and using a LeCroy oscilloscope. The laser power was monitored using an Ophir StarLite power meter. The emission spectra within the visible range were captured using an Andor Shamrock 500 spectrometer coupled with the silicon and InGaAs Andor Newton CCD cameras. The sample was heated using a Linkam system (THMS600). For the temperature measurements with the printed sensor, a thermostatically controlled water bath was used to heat the liquid-containing cuvette.

## 3. Results and discussion

### 3.1. Photon-avalanche process

In the photon-avalanche process, the material absorbs energy in a weak absorption region with an excitation wavelength of 1060 nm, and through energy transfer mechanisms between its energy levels, an intense emission is produced. Emission peaks were observed at 475 nm ( ${}^1\text{G}_4 \rightarrow {}^3\text{H}_6$ ), 800 nm ( ${}^3\text{H}_4 \rightarrow {}^3\text{H}_6$ ), 1460 nm ( ${}^3\text{H}_4 \rightarrow {}^3\text{F}_4$ ), and 1625 nm ( ${}^3\text{F}_4 \rightarrow {}^3\text{H}_6$ ), with our study focusing on the latter two emissions (see Fig. 2a and b). It should be noted that the  ${}^3\text{F}_4$  level can be populated significantly through phonon decay and *via* 1460 nm radiative decay. Additionally, an electron in the ground state can be excited to this level by cross-relaxation, leading to a photon-avalanche process when conditions are right.

Fig. 3a illustrates how the emission band's rise time and luminescence intensity at 475 nm depend on the excitation power. It is observed that around 142 mW of excitation power, the response time shifts from increasing to decreasing. Additionally, the dependence of luminescence intensity on excitation power changes, with slopes of  $s = 2.90$  and  $s = 10.07$ , indicating a shift in the number of photons required for the emission of 475 nm, placing the sample in the PA region.<sup>14,15,18,36,39</sup> These are clear indicators of avalanche processes, suggesting a power threshold for photon-avalanche initiation.<sup>14,15,18,36,39</sup> Fig. 3b shows the temporal evolution curves at three different excitation powers (83 mW, 142.5 mW, and 279 mW), illustrating the changes in emission behavior as the excitation power varies. The inset in Fig. 3b presents a three-dimensional graph of the luminescence intensity increase, showing how the material's response varies with excitation power and time. This behavior is critical for understanding the relaxation and energy transfer processes within the  $\text{Tm}^{3+}$ -doped material.<sup>14,15,18,36,39</sup>

### 3.2. Temperature sensor

Once the photon-avalanche regime is reached, the emission spectrum in the infrared range can be obtained. Fig. 4a shows the characteristic emission peaks of the  $\text{Tm}^{3+}$  ion in the IR region.<sup>45,46</sup> These peaks correspond to transitions between different energy levels  ${}^3\text{H}_4 \rightarrow {}^3\text{F}_4$  (1460 nm) and  ${}^3\text{F}_4 \rightarrow {}^3\text{H}_6$  (1625 nm). It is observed that, as the temperature increases, the emission at 1460 nm decreases. This is due to the higher probability of the  ${}^3\text{H}_4$  level decaying non-radiatively to the  ${}^3\text{F}_4$  level through phonon interactions.

Additionally, the population of the  ${}^3\text{F}_4$  level increases because of the cross-relaxation process occurring during the avalanche process. This level then emits radiatively at 1625 nm (spectra normalized to the emission at 1625 nm). Parameters such as the luminescence intensity ratio (LIR) were used to characterize an optical sensor based on luminescence, representing the luminescence intensity ratio (1625 nm/1460 nm). As photon-avalanche processes are complex and involve multiple



Fig. 2 (a) Energy level diagram of  $\text{Tm}^{3+}$  illustrating the photon-avalanche process under 1060 nm excitation. (b) Near-infrared emission spectrum of studied material under 1060 nm excitation.



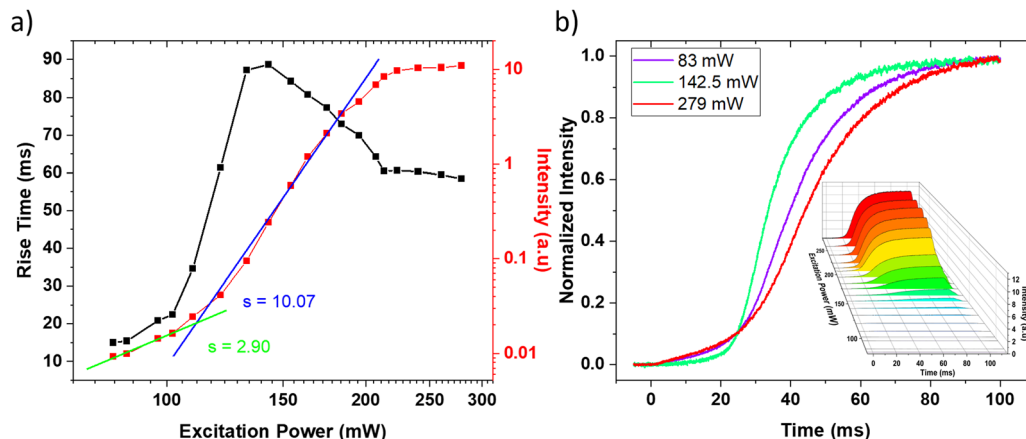


Fig. 3 (a) Rise time and fluorescence intensity as a function of excitation power. (b) Temporal evolution curves for three different excitation powers. Inset: Three-dimensional graph of fluorescence intensity increase from excitation at  $t = 0$  ms.

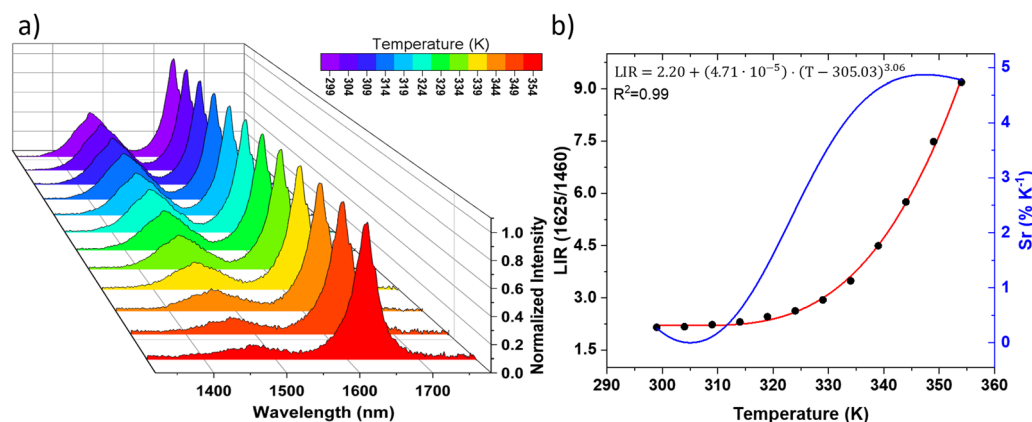


Fig. 4 (a) Emission spectrum in the IR range under 1060 nm excitation. (b) LIR and relative sensitivity as a function of temperature.

Table 1 Comparison of performance of different luminescent thermometers using the photon-avalanche

Host	Ln <sup>3+</sup>	Temperature range [K]	Maximum $S_r$ [% K <sup>-1</sup> ]	$\lambda$ [nm]	Ref.
Fluoroindate glass	Tm	299–354	4.9	1625/1460	This work
YAG	Nd	273–573	5.3	800	16
LiLaP <sub>4</sub> O <sub>12</sub>	Nd	300–573	5.6	800	16
Y <sub>2</sub> O <sub>3</sub>	Nd	300–573	7.1	800	16
GdO <sub>3</sub>	Nd	300–573	6.7	800	16
GdYO <sub>3</sub>	Nd	300–573	7.0	800	16
NaYF <sub>4</sub> :Ln <sup>3+</sup> @NaYF <sub>4</sub>	Yb, Pr	98–273	7	607	17
		98–448	7.5	482	
			4.3	607	
			4.3	482	
NdVO <sub>4</sub>	Yb, Er	298–618	3.5	750/853	18

parameters, the fitting equation  $f(T)$  was proposed empirically to correlate the LIR with temperature, thereby calibrating the material for future experiments.

$$LIR \equiv \frac{I_{1625}}{I_{1460}} = f(T) \quad (1)$$

In order to compare the sensitivity of the sample with other commonly used luminescent temperature sensors, the relative

sensitivity ( $S_r$ ) given by the following formula was calculated:

$$S_r(T) = 100\% \times \frac{1}{LIR} \frac{dLIR}{dT} \quad (2)$$

The values obtained change from 0.01 to 4.9% K<sup>-1</sup> in the range of temperatures studied, *i.e.*, from 299 to 354 K (Fig. 4b), cannot be compared with other results because no literature is



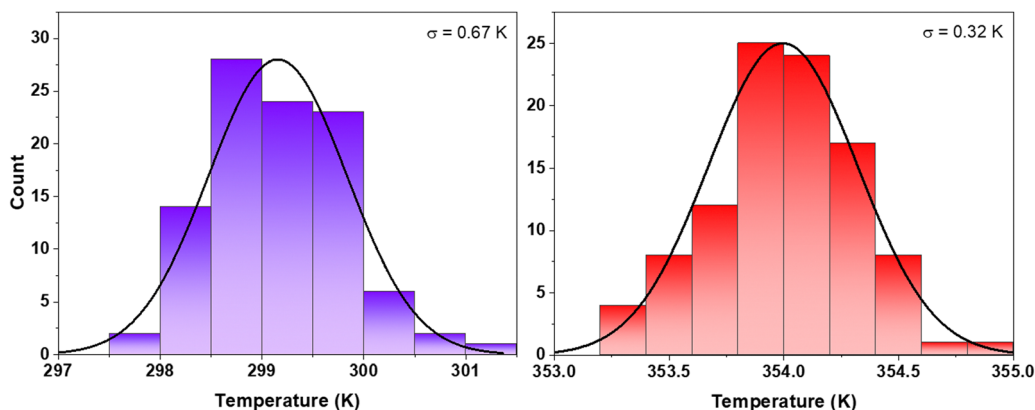


Fig. 5 Histograms of the measurement error for the lowest and highest temperatures.

available on temperature sensors using the photon-avalanche process in  $\text{Tm}^{3+}$ . To the best of our knowledge, this is the first reported temperature sensor based on the photon-avalanche

process in  $\text{Tm}^{3+}$ . On the other hand, Table 1 presents a compilation of different materials and their respective dopants, providing a general reference for the temperature ranges and



Fig. 6 (a) Diagram presenting the application of the photon-avalanche effect in liquid temperature measurement. (b) Infrared emission spectrum for the sample immersed in isopropanol (excited at 800 nm). (c) Corresponding LIR and relative sensitivity.



relative sensitivities associated with temperature sensors utilizing the photon-avalanche phenomenon.

The use of a sensor also depends on the uncertainty in estimating the temperature change. An experimental estimation of this error was performed by recording 100 spectra under the same conditions at different temperatures (299 K and 354 K), repeating the measurements 100 times at each temperature point (see Fig. 5). The resulting standard deviation ranged between 0.67 and 0.32 K.

### 3.3. Liquid temperature control

Achieving the photon-avalanche condition requires precise control of the working system, which can present specific challenges. These requirements might limit its direct implementation in practical applications, particularly in maintaining the necessary excitation power to induce the phenomenon. However, it can be achieved for suitable applications and systems without significant difficulty, depending on the environment and intended use. In the diagram shown in Fig. 6a, we propose using 3D printing to create a resin support embedded with luminescent particles. By exciting these particles (to induce photon-avalanche), the infrared emission spectrum of the sample immersed in isopropanol is obtained (see Fig. 6b). This approach provides insights into how the environment affects calibration, as the surrounding liquid may absorb the emission bands. In Fig. 6c, the variation of the LIR and  $S_r$  as a function of the solvent (isopropanol) temperature is shown, highlighting changes in LIR behavior (ranging from 5.86 to 9.17) and  $S_r$  (varying between 1.52 and 1.98%  $K^{-1}$ ) when the medium is altered. These values differ from those observed in Fig. 4b. This underscores the potential applications of this material as a temperature sensor in different media using the photon-avalanche effect, provided that a new calibration is performed for each specific medium.

## 4. Conclusions

In summary, we have characterized the photon-avalanche process in a fluorindate glass doped with  $Tm^{3+}$  and evaluated its potential as a temperature sensor receiving high sensitivity. The experiments demonstrated that the photon-avalanche phenomenon in these materials can be utilized to detect temperature variations with high precision, achieving a relative sensitivity of up to 4.9%  $K^{-1}$ , with a temperature measurement uncertainty ranging between 0.67 and 0.32 K. The practical application of the obtained sensor for temperature measurement in air and isopropanol was also explored, demonstrating the versatility of these materials in different environments. These results open new possibilities for using lanthanide-doped materials in optical sensor technologies and other advanced optoelectronic devices by applying the photon-avalanche effect.

## Data availability

Data are available upon request from the authors.

## Conflicts of interest

There are no conflicts of interest to declare.

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