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Regulating the preparation of antibacterial poly(amidoxime)  
for efficient uranium extraction from seawater

Polyacrylonitrile (PAN) contain around  $-C\equiv N$  groups,  
and is one of hot materials in uranium extraction. However,  
intermolecular polymerization seriously hindered its  
application. In this work, a nano-scale antibacterial adsorbent  
was developed by inhibiting PAN agglutination with  $K_2FeO_4$ ,  
and it presents excellent anti-biofouling property and  
adsorption capability for  $U(VI)$  in uranium extraction from  
seawater.

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# Regulating the preparation of antibacterial poly (amidoxime) for efficient uranium extraction from seawater†

Xue Zhang and Dadong Shao \*

Seawater is a huge store of uranium, and the related uranium retraction technology has become a critical step in the sustainable development of nuclear power. For obtaining uranium U(VI) from seawater cheaply and environmentally, we introduced K<sub>2</sub>FeO<sub>4</sub> during the polyamidoxime (PAO) preparation process in water to endow PAO with high antibacterial and low agglomeration properties. In this reaction, only water was used as the solvent with the goal of extracting U(VI) from seawater in a low-cost, pollution-free manner. Studies showed that the adsorption of U(VI) on K<sub>2</sub>FeO<sub>4</sub>@PAO conformed to a pseudo-second-order model, and the maximum adsorption capacity calculated by the Langmuir model was 137 mg g<sup>-1</sup> at 298 K and pH 8.2. Moreover, K<sub>2</sub>FeO<sub>4</sub>@PAO showed high selectivity for U(VI) compared with a range of metal ions. K<sub>2</sub>FeO<sub>4</sub>@PAO also showed good recyclability, and the recovery rate only decreased by 3% after six cycles. In addition, antibacterial experiments indicated that K<sub>2</sub>FeO<sub>4</sub>@PAO could effectively inhibit the growth of *Escherichia coli* (*E. coli*) and *Vibrio alginolyticus* (*V. alginolyticus*) that are commonly found in seawater.

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## Introduction

As a low-carbon and efficient energy, the sound development of nuclear power is crucial for a future low-carbon society.<sup>1,2</sup> As the most important nuclear fuel for nuclear power operations, the safe supply of uranium is key to guaranteeing the sustainable development of nuclear power. Traditional terrestrial uranium resources are limited and would be exhausted in few decades. It is thus a worldwide task to explore new uranium resources. As a typical uranium resource, seawater has attracted worldwide attention because an estimated ~4.5 billion tons of U(VI) in seawater can solve the global shortage of uranium.<sup>3,4</sup> There is thus an urgent need to develop appropriate methods and materials for seawater U(VI) extraction.<sup>5-7</sup> Thus far, several technologies have been reported to recover U(VI) from seawater, such as ionic exchange, electrochemical process, co-precipitation, and adsorption method.<sup>8-11</sup> Among them, adsorption has been widely adopted due to its low cost and practicability. However, the complexity of the marine environment, such as very low U(VI) concentration (~3 ppb), presence of many coexisting competing ions, high salinity, and easy biofouling, makes the U(VI) extraction process extre-

mely challenging.<sup>12-14</sup> Other factors, such as the technical economy of the extraction process, also need to be seriously considered. Therefore, it is necessary to develop high-performance materials to improve comprehensive properties of the used adsorbents to enable the economical extraction of U(VI) from seawater.<sup>15</sup>

Polyamidoxime (PAO)-based materials can adsorb U(VI) due to the O and N atoms of PAO having the same distance and lone pair of electrons, and these are thus among the hot materials in U(VI) extraction research. Resulting from polyacrylonitrile's (PAN) low cost, good chemical stability, and easy industrial production, numerous adsorbents select it to prepare PAO-based materials for U(VI) recovery.<sup>16-18</sup> There are many methods for synthesizing PAO in the laboratory. The classic synthesis method is -C≡N amidoximation, which can be divided into homogeneous and heterogeneous processes according to the solvent. The homogeneous method mainly involves the reaction of PAN and NH<sub>2</sub>OH in an organic solvent with dimethyl sulfoxide and *N,N'*-dimethyl formamide generally chosen in the laboratory. The heterogeneous method mainly involves the reaction of PAN with NH<sub>2</sub>OH in water and methanol/water solutions. Organic solvents are often required in this method, which makes it not only harmful to the environment but also increases the cost of U(VI) recovery, dramatically reducing the competitiveness of PAO in U(VI) extraction. Thus, we considered selecting water as a solvent during the amidoximation process. PAN, as a macromolecule

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material, is prone to agglomerate in water, leading to intramolecular bond accumulation without the reaction of its groups.<sup>19,20</sup> In this work,  $K_2FeO_4$  was adopted to inhibit the aggregation of PAN in water with an aim to obtain a higher conversion rate.

In the  $U(VI)$  extraction process, the interaction between  $U(VI)$  extraction materials and marine microorganisms should be considered in addition to improving the  $U(VI)$  recovery rate and cost.<sup>21,22</sup> Seawater is a very harsh corrosive environment, which is typically characterized by high biological activity, with  $10^6$  colony-forming units (CFU) per mL level microbes (including bacteria and microalgae) found to exist in seawater. The microbes and their metabolisms affect material surface properties, which can eventually affect the  $U(VI)$  extraction performance. Thus, there is a necessity to design a novel adsorbent to achieve an antifouling goal.<sup>15,23,24</sup> The corresponding standard electrode potentials of  $FeO_4^{2-}$  both in acid (2.20 V) and alkali (0.72 V) media are higher than the well-known strong oxidant  $KMnO_4$  under the same conditions. This strong oxidation ensures the strong bactericidal ability of  $FeO_4^{2-}$ .  $K_2FeO_4$  can kill both Gram-positive and Gram-negative bacteria, fungi, viruses, and spores.<sup>25,26</sup> The introduced  $K_2FeO_4$  in PAN can inhibit the corrosion from marine microorganisms.

The structure of a material determines its properties, and ultimately affects its application optimizing the structure of a material is an effective way to enhance its properties and expand its application fields. Herein, we constructed the antibiofouling nanoscale adsorbent  $K_2FeO_4@PAO$  for  $U(VI)$  recovery by introducing  $K_2FeO_4$  during the amidoximation method with only water as a solvent (Fig. 1). The added  $K_2FeO_4$  could overcome PAN agglomeration in water, so that PAN could well contact with  $NH_2OH$ , which could help realize the economic and environmental recovering of uranium. Meanwhile, the high oxidation ability of  $K_2FeO_4$  could exterminate bacterial. The obtained antibacterial  $K_2FeO_4@PAO$  particles exhibited a higher adsorption capacity and better antibiofouling properties than PAO under the experimental conditions.



Fig. 1 Scheme for the fabrication and application of  $K_2FeO_4@PAO$  in the extraction of  $U(VI)$  from seawater.

## Results and discussion

### Characterization

As shown in Fig. S1A and B,† PAN tends to aggregate into large particles and is extremely unstable in aqueous solution, which is detrimental to the conversion of PAN into PAO, and ultimately affects the adsorption capability of PAO. Therefore,  $K_2FeO_4$  was introduced to inhibit the agglomeration of PAN during the amidoximation process in this work. This is a simple way to obtain a high conversion of PAN, which would accelerate the practical application of PAO as a candidate for  $U(VI)$  extraction from seawater. As shown in Fig. S1C,† after introducing  $K_2FeO_4$ , the obtained PAO-based material could uniformly disperse in aqueous solution and the PAO appearance was improved overall. Given the effect of  $K_2FeO_4$  on the inhibition of PAN particle agglomeration, the obtained PAO morphology may be regulated by  $K_2FeO_4$ .

To study the effect of  $K_2FeO_4$  on the PAO surface topologies, the microstructures of PAN and PAO prepared at different conditions were analyzed by SEM (Fig. 2A), with varying the addition amounts of  $K_2FeO_4$  and PAN in the preparation process, as shown in Table 1. The SEM images indicated that the addition of 0.20 g  $K_2FeO_4$  had no significant effect on PAO surface topologies, and the obtained  $K_2FeO_4@PAO$  was uniformly dispersed. As the mass of  $K_2FeO_4$  increased, PAN agglomeration became more evident, and eventually, a PAN block was formed. The three reactions include the formation of  $-C\equiv N$  from unsaturated amine, the redox reaction between  $NH_2OH$  and  $K_2FeO_4$ , and the conversion of  $-C\equiv N$  to  $-C(NH_2)=N-OH$ , which restrict and promote each other in water. When the amounts of PAN and  $NH_2OH$  were much more than  $K_2FeO_4$ , the amidoximation reaction was the primary reaction in solution, and finally, uniform dispersed PAO particles were obtained. When the  $K_2FeO_4$  amount was higher than PAN and

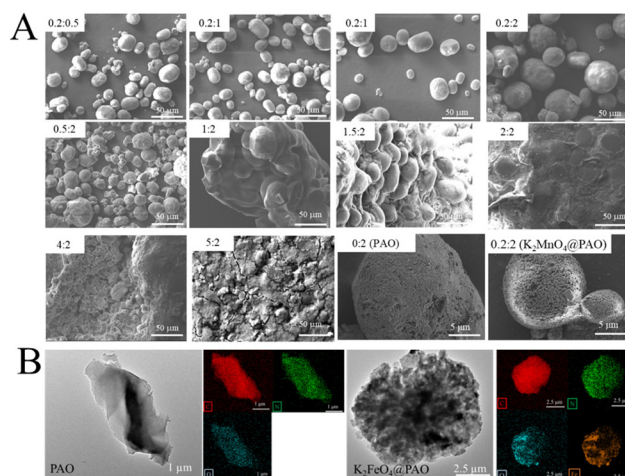


Fig. 2 SEM images of  $K_2FeO_4@PAO$  with different  $K_2FeO_4$  and PAO contents (A) and TEM image and EDS mappings of PAO and  $K_2FeO_4@PAO$  (B). The preparation conditions for  $K_2FeO_4@PAO$  are shown in Table 1.

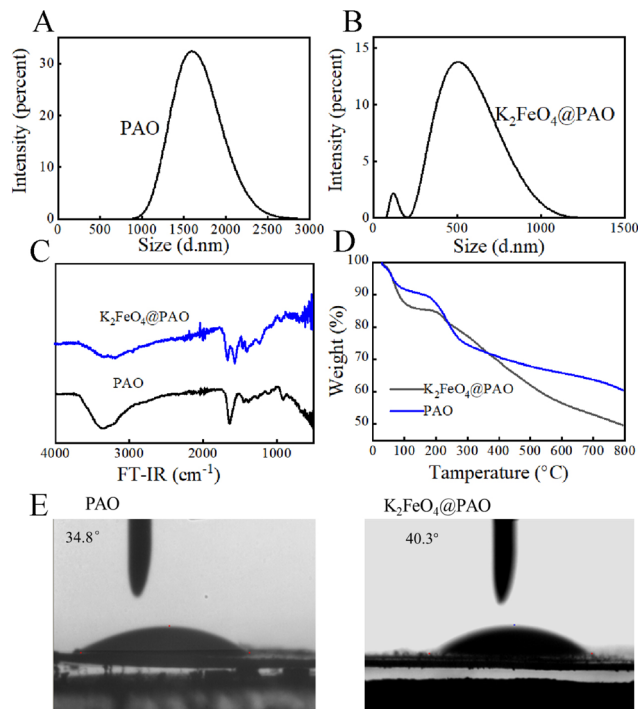


**Table 1** Preparation conditions for K<sub>2</sub>FeO<sub>4</sub>@PAO

	K <sub>2</sub> FeO <sub>4</sub> (g)	PAN (g)	Name
Fixed K <sub>2</sub> FeO <sub>4</sub> series	0.20	0.50	0.2 : 0.5
		1.00	0.2 : 1
		1.50	0.2 : 1.5
		2.00	0.2 : 2
Fixed PAN series	0	2.00	0 : 2
		0.50	0.5 : 2
		1.00	1 : 2
		1.50	1.5 : 2
		2.00	2 : 2
		4.00	4 : 2
5.00	5 : 2		

NH<sub>2</sub>OH, the solution reaction was dominated by the redox reaction of K<sub>2</sub>FeO<sub>4</sub> and NH<sub>2</sub>OH, which consumed most of the NH<sub>2</sub>OH and made it impossible to complete the conversion of -C≡N, instead forming -C≡N rings on the PAN macromolecular chains and thus creating bulk materials. Besides SEM, TEM was also applied to study the morphologies of PAO and K<sub>2</sub>FeO<sub>4</sub>@PAO. As shown in Fig. 2B, the single PAO presents a block form, but transformed into nanoscale particles (K<sub>2</sub>FeO<sub>4</sub>@PAO) after K<sub>2</sub>FeO<sub>4</sub> was introduced. It was found that C, N, and O elements were uniformly distributed on PAO and K<sub>2</sub>FeO<sub>4</sub>@PAO surfaces by the TEM element mapping. Moreover, Fe was evenly distributed on the K<sub>2</sub>FeO<sub>4</sub>@PAO surface, proving that K<sub>2</sub>FeO<sub>4</sub> recombined with PAO successfully. It is considered that the -C(NH<sub>2</sub>)=N-OH unit in K<sub>2</sub>FeO<sub>4</sub>@PAO is the core of its application in U(vi) extraction. The adsorption capacity of K<sub>2</sub>FeO<sub>4</sub>@PAO for U(vi) gradually increased with increasing the PAN amount when the K<sub>2</sub>FeO<sub>4</sub> amount was fixed at 0.20 g (Fig. S2A†) and decreased with increasing the K<sub>2</sub>FeO<sub>4</sub> amount when the PAN amount was set at 2.00 g (Fig. S2B†). Therefore, the K<sub>2</sub>FeO<sub>4</sub> amount should be well controlled during the K<sub>2</sub>FeO<sub>4</sub>@PAO preparation process. The aggregation of PAN could be significantly inhibited, and PAO particles with smaller particle sizes and better adsorption capability could be obtained at the composition of 0.20 g K<sub>2</sub>FeO<sub>4</sub> and 2.00 g PAN. This reactant amount was selected in the following experiment.

The effect of K<sub>2</sub>FeO<sub>4</sub> on the PAO particle-size distribution was also studied. Dynamic light scattering (DLS) measurements showed that the PAO particle sizes were concentrated around 1600 nm (Fig. 3A). The particle diameter of K<sub>2</sub>FeO<sub>4</sub>@PAO was reduced ~31% at 500 nm (Fig. 3B) compared with PAO. The introduced K<sub>2</sub>FeO<sub>4</sub> could thus inhibit the agglomeration of PAN in water and promote the formation of nano-sized K<sub>2</sub>FeO<sub>4</sub>@PAO particles. The smaller K<sub>2</sub>FeO<sub>4</sub>@PAO particle size will help the adsorbent application in the target solution. The Tyndall phenomenon was used to further verify the size of the two particles. Here, if the particle is smaller than the wavelength of incident light, light scattering occurs. In this case, a light wave around the particle is observed and radiates around it, which is called scattered light and the Tyndall phenomenon is the scattering phenomenon of light.

**Fig. 3** Size distributions (A and B), FT-IR spectra (C), TGA curves (D), and water contact angles (E) of PAO and K<sub>2</sub>FeO<sub>4</sub>@PAO.

In terms of the macroscopic performance for the same incident light, if the particles are small, have a larger scattering angle, the scattered light has a weak flood angle, and its brightness is high, then the Tyndall phenomenon is obvious. If the particles are large, have a small scattering angle, the scattered light has a large flood angle, and a low centre brightness, then the Tyndall phenomenon is poor. As shown in Fig. S3,† the light-scattering angle of the particles of K<sub>2</sub>FeO<sub>4</sub>@PAO was large, the centre brightness was high, the flooding was small, and the Tyndall phenomenon was obvious. However, PAO had a poor particle size uniformity, and the light tended to be scattered by large particles. The light-scattering angle of the particles was small, the flooding area was large, the centre brightness was low, and the Tyndall path was dark.

FT-IR and TGA were used to analyze the effects of K<sub>2</sub>FeO<sub>4</sub> on the surface functional groups and thermal stability of PAO. As shown in Fig. 3C, The FT-IR spectra of K<sub>2</sub>FeO<sub>4</sub>@PAO and PAO were similar. In the K<sub>2</sub>FeO<sub>4</sub>@PAO spectrum, the peaks of N-H and O-H were at 3500–3000 cm<sup>-1</sup>, the peak of -C≡N was at ~1668 cm<sup>-1</sup>, and the characteristic peak of N-O was at ~932 cm<sup>-1</sup>, which were all consistent with the PAO infrared spectrum. Fig. 3D shows the TGA curves of PAO and K<sub>2</sub>FeO<sub>4</sub>@PAO. The first ~4% weight losses of PAO and K<sub>2</sub>FeO<sub>4</sub>@PAO could be assigned to moisture loss. PAO and K<sub>2</sub>FeO<sub>4</sub>@PAO showed good thermal stability at 100–200 °C. The second weight loss at 200–500 °C was related to the cyclization dehydrogenation of PAO. PAO and K<sub>2</sub>FeO<sub>4</sub>@PAO then underwent severe oxidative cleavage at 500–700 °C.<sup>19</sup>



Static contact-angle experiments were used to quantify the surface hydrophilic property of PAO and  $\text{K}_2\text{FeO}_4\text{@PAO}$ . Before the test, each powder material was pressed into a tablet with a tablet press and the pressure of 20 MPa was maintained for 40 s. During the contact-angle measurement, 2  $\mu\text{L}$  ultrapure water was injected for each test. Each sample was tested three times, and every test used a new sample to exclude residual effects. The results of the three tests are shown in Fig. 3E, whereby the average contact angles of PAO and  $\text{K}_2\text{FeO}_4\text{@PAO}$  were  $34.8^\circ$  and  $40.3^\circ$ , respectively. The lower water contact angles of PAO and  $\text{K}_2\text{FeO}_4\text{@PAO}$  indicated they both have good hydrophilicity, which would benefit their application in aqueous solution.

XPS was used to infer the binding states of the atoms and the electron distribution in  $\text{K}_2\text{FeO}_4\text{@PAO}$  and PAO by measuring the chemical shift of electrons in their layers (Fig. 4A). The high resolution of Fe 2p in the  $\text{K}_2\text{FeO}_4\text{@PAO}$  spectrum revealed the characteristic Fe 2p<sub>3/2</sub> and Fe 2p<sub>1/2</sub><sup>27–29</sup> of Fe signals located at 711.8 and 724.7 eV, respectively (Fig. S4†). A new peak appeared at  $\sim 390$  eV (Fig. S5†) related to XPS U 4f<sup>4</sup> after U(vi) adsorption, revealing the high enrichment of U(vi) on PAO and  $\text{K}_2\text{FeO}_4\text{@PAO}$  surfaces. The XPS peaks of O 1s, N 1s, and C 1s were located at  $\sim 532$ ,  $\sim 400$ , and  $\sim 285$  eV, respectively. The C 1s spectra (Table S1† and Fig. 4B) could be divided into five components at  $284.6 \pm 0.1$ ,  $285.3 \pm 0.1$ ,  $286.4 \pm 0.1$ ,  $287.4 \pm 0.1$ , and  $288.6 \pm 0.1$  eV corresponding to  $-\text{C}\equiv\text{N}$ , C–C, C–OH and  $-\text{C}(\text{NH}_2)=\text{NOH}$ ,  $-\text{C}=\text{O}$ , and  $-\text{COO}^-$  groups of PAO and  $\text{K}_2\text{FeO}_4\text{@PAO}$  surfaces, respectively.<sup>30,31</sup> As indicated in the N 1s spectra (Fig. 4C and Table S2†), the characteristic peaks with binding energies at  $398.7 \pm 0.1$ ,  $399.3 \pm 0.1$ , and  $400.5 \pm 0.1$  eV were attributed to the  $-\text{C}\equiv\text{N}$ , N–H, and  $-\text{C}(\text{NH}_2)=\text{NOH}$  bonds, respectively.<sup>31,32</sup> The three fitting peaks in the O 1s spectra (Fig. 4D and Table S3†) belonged to  $-\text{COO}^-$  ( $531.2 \pm 0.1$  eV), C=O ( $532.3 \pm 0.1$  eV), and  $-\text{OH}$  ( $533.4 \pm 0.1$  eV), respectively.<sup>33,34</sup> The XPS results showed that the chemical environments of PAO and  $\text{K}_2\text{FeO}_4\text{@PAO}$  were

similar to each other, revealing that  $\text{K}_2\text{FeO}_4$  did not affect PAO's chemical properties.

### Adsorption performance of $\text{K}_2\text{FeO}_4\text{@PAO}$

The solution pH can affect the forms of U(vi) existing in solution and on the adsorbent surface, therefore affecting the U(vi) adsorption behaviours.<sup>35</sup> Fig. 5A shows that the U(vi) extraction capacity of  $\text{K}_2\text{FeO}_4\text{@PAO}$  displayed an increasing trend at pH 2–5.  $\text{UO}_2^{2+}$  was the dominant form of U(vi) at pH < 4, and  $\text{K}_2\text{FeO}_4\text{@PAO}$  was positive due to protonation. Electrostatic repulsion would lead to a poor recovery effect for  $\text{K}_2\text{FeO}_4\text{@PAO}$  to U(vi). At pH 4.0–6.0,  $\text{K}_2\text{FeO}_4\text{@PAO}$  surface was gradually deprotonated and the electrostatic attraction of the solution-dominant positively charged U(vi) species was enhanced, resulting in increased U(vi) adsorption on  $\text{K}_2\text{FeO}_4\text{@PAO}$ . The U(vi) uptake decreased when the pH value increased from 6.0 to 9.0. The main reason for this phenomenon was that the negatively charged U(vi) species was the dominant substance, and so the adsorption capacity of  $\text{K}_2\text{FeO}_4\text{@PAO}$  for U(vi) was inhibited by electrostatic repulsion with the pH increasing. The maximum adsorption capacity of  $\text{K}_2\text{FeO}_4\text{@PAO}$  ( $17.1 \text{ mg g}^{-1}$ ) was obtained at pH  $\sim 5.0$ . The higher maximum adsorption capacity of  $\text{K}_2\text{FeO}_4\text{@PAO}$  over PAO illustrated that nano-sized  $\text{K}_2\text{FeO}_4\text{@PAO}$  favours U(vi) extraction.

The adsorption performances of  $\text{K}_2\text{FeO}_4\text{@PAO}$  at different contact times were also studied. U(vi) adsorption on PAO and  $\text{K}_2\text{FeO}_4\text{@PAO}$  rose sharply in the first 2 h, and then increased slowly with further increasing the reaction time (Fig. 5B), reaching equilibrium within 8 h. The adsorption kinetics were analyzed by pseudo-first-order ( $q_t = q_e \times (1 - \exp(-k_1 t))$ ), where  $q_e$  and  $q_t$  ( $\text{mg g}^{-1}$ ) are the adsorbed amounts of U(vi) at equilibrium time and time  $t$  (h), respectively, and  $k_1 t$  ( $1 \text{ h}^{-1}$ ) is the pseudo-first-order kinetic constant) and pseudo-second-order

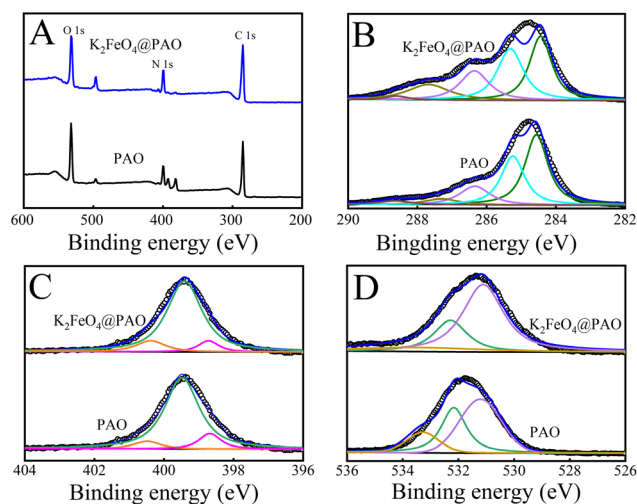


Fig. 4 XPS survey (A), C 1s (B), N 1s (C), and O 1s (D) spectra of  $\text{K}_2\text{FeO}_4\text{@PAO}$  and PAO.

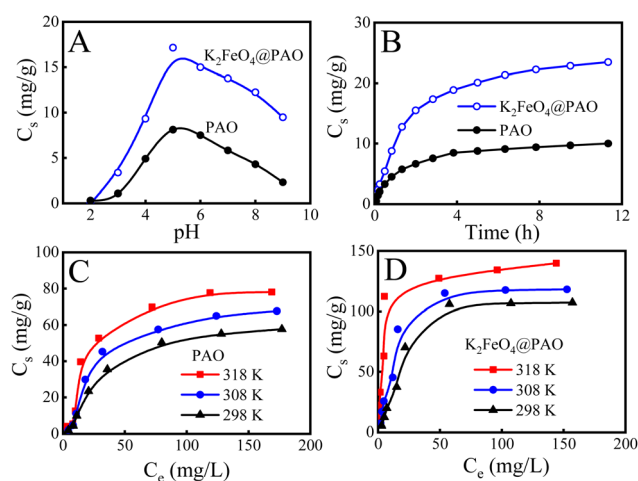


Fig. 5 Effects of pH (A), contact time (B), adsorption isotherms, and reaction temperature on the adsorption of U(vi) on PAO (C) and  $\text{K}_2\text{FeO}_4\text{@PAO}$  (D) from solution.  $m = 0.02 \text{ g}$ ,  $V = 50 \text{ mL}$ ,  $I = 0.1 \text{ mol L}^{-1}$  NaCl. (A)  $T = 298 \pm 1 \text{ K}$ , pH =  $8.2 \pm 0.1$ ,  $C[\text{U(vi)}]_{\text{initial}} = 10.0 \text{ mg L}^{-1}$ . (B)  $T = 298 \pm 1 \text{ K}$ , pH =  $8.2 \pm 0.1$ ,  $C[\text{U(vi)}]_{\text{initial}} = 20.0 \text{ mg L}^{-1}$ . (C and D) pH =  $8.2 \pm 0.1$ , contact time: 24 h.



( $q_t = q_e \times t / (K' \times q_e + t)$ , where  $K'$  ( $\text{g} (\text{mg h})^{-1}$ ) is the pseudo-second-order kinetic constant) models.<sup>36,37</sup> The relevant these parameters coefficients are generalized in Table S4.† The adsorption process of  $\text{U}(\text{VI})$  by  $\text{K}_2\text{FeO}_4@\text{PAO}$  and PAO conformed to the pseudo-second-order model and chemisorption was the primary adsorption mode for  $\text{U}(\text{VI})$  adsorption on  $\text{K}_2\text{FeO}_4@\text{PAO}$  and on PAO. According to the relevant results of the pseudo-second-order model, the maximum adsorption capacities of  $\text{U}(\text{VI})$  on  $\text{K}_2\text{FeO}_4@\text{PAO}$  and PAO were 26.9 and 10.9  $\text{mg g}^{-1}$  at pH 8.2 and 298 K, respectively.

Given the above excellent  $\text{U}(\text{VI})$  recovery performance of  $\text{K}_2\text{FeO}_4@\text{PAO}$ , its effect for  $\text{U}(\text{VI})$  recovery in various environmental solutions was also studied. As shown in Table 2,  $\text{K}_2\text{FeO}_4@\text{PAO}$  could effectively extract most  $\text{U}(\text{VI})$  from this complex system. Therefore, the real application of  $\text{K}_2\text{FeO}_4@\text{PAO}$  in extraction  $\text{U}(\text{VI})$  from seawater was performed, and seawater was prepared with sea salt. We found that  $\text{K}_2\text{FeO}_4@\text{PAO}$  could effective uptake  $\sim 57\%$  of 5  $\text{mg L}^{-1}$   $\text{U}(\text{VI})$  from seawater. Experimental results further confirmed the high efficiency of  $\text{K}_2\text{FeO}_4@\text{PAO}$  in the extraction of  $\text{U}(\text{VI})$  from seawater.

Adsorption isotherms was used to depict the adsorption capacities of  $\text{K}_2\text{FeO}_4@\text{PAO}$  and PAO at three different temperatures (*i.e.* 298, 308, and 318 K). As shown in Fig. 5C and D, with increasing the  $\text{U}(\text{VI})$  initial concentration and temperature, the adsorption capacities of  $\text{K}_2\text{FeO}_4@\text{PAO}$  and PAO for  $\text{U}(\text{VI})$  increased. Langmuir ( $C_s = b \times C_{s,\text{max}} \times C_{\text{eq}} / (1 + b \times C_{\text{eq}})$ , where  $C_{\text{eq}}$  is the equilibrium concentration of  $\text{U}(\text{VI})$  after adsorption,  $C_{s,\text{max}}$  ( $\text{mg g}^{-1}$ ) and  $b$  ( $\text{L mg}^{-1}$ ) are the maximum adsorption capability of the adsorbent and the Langmuir constant, respectively) and Freundlich ( $C_s = K \times C_e^{1/n}$ ,  $K$  ( $\text{mg g}^{-1}$ ) and  $1/n$  are the constants indicative of the adsorption capability and intensity, respectively) models were used to fit the experimental data, and the mechanism of the adsorption process is discussed.<sup>36,37</sup> According to the  $R^2$  values in Table S5,† the Langmuir isotherm model could better describe the experimental data, suggesting there was no interaction

between the adsorption sites, and the  $\text{U}(\text{VI})$  adsorption process on  $\text{K}_2\text{FeO}_4@\text{PAO}$  was a monolayer adsorption. The  $C_{s,\text{max}}$  value  $\text{K}_2\text{FeO}_4@\text{PAO}$  for  $\text{U}(\text{VI})$  at pH 8.2 and 298 K was calculated to be 137  $\text{mg g}^{-1}$ .

According to the adsorption results, the adsorption capacity of PAO prepared in water was lower than that reported when prepared in organic reagents.<sup>38–40</sup> From the perspective of economic cost and environmental protection, obtaining PAO in water is more conducive to the long-term development of PAN as a material for extracting  $\text{U}(\text{VI})$  from seawater. More importantly, the PAO's preparation in water has not been reported yet. PAN is widely used in  $\text{U}(\text{VI})$  recovery, mainly because its surface contains a large number of  $-\text{C}\equiv\text{N}$  groups, which can be converted into  $-\text{C}(\text{NH}_2)\text{N}=\text{OH}$  by chemical reaction with  $\text{NH}_2\text{OH}$  in solution and  $-\text{C}(\text{NH}_2)\text{N}=\text{OH}$  can coordinate with  $\text{U}(\text{VI})$  to recover uranium. However, one cannot ignore that PAN is easy to agglomerate and most  $-\text{C}\equiv\text{N}$  is not reacted with  $\text{NH}_2\text{OH}$  in water, resulting in PAO having a low adsorption capacity for  $\text{U}(\text{VI})$ . Here,  $\text{K}_2\text{FeO}_4@\text{PAO}$  nanoparticles were obtained after  $\text{K}_2\text{FeO}_4$  was introduced into the PAN transformation process. Compared with PAO, the adsorption capacity of  $\text{K}_2\text{FeO}_4@\text{PAO}$  was significantly increased, indicating that PAN reacted more fully with  $\text{NH}_2\text{OH}$  and the amount of  $-\text{C}(\text{NH}_2)\text{N}=\text{OH}$  on its surface increased.

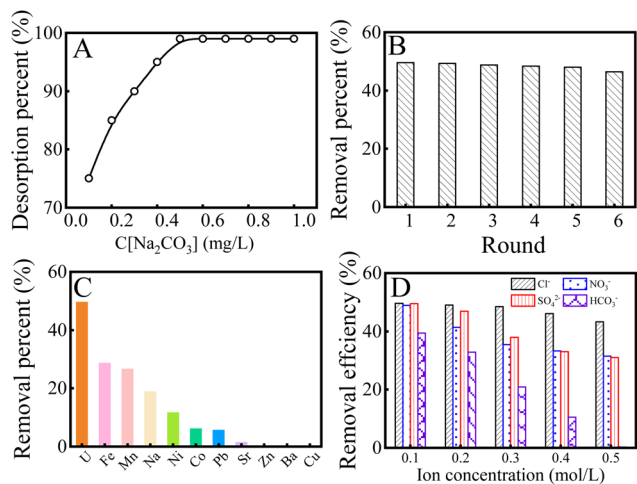
The relevant thermodynamic parameters,<sup>41</sup> standard enthalpy change ( $\Delta H^\circ$ ), standard Gibbs free energy change ( $\Delta G^\circ$ ), and entropy change ( $\Delta S^\circ$ ) of  $\text{K}_2\text{FeO}_4@\text{PAO}$  and PAO for  $\text{U}(\text{VI})$  adsorption at three different temperatures (*i.e.* 298, 308, and 318 K) were investigated and are discussed, and the results are shown in Table S6.† The energy released or adsorbed in the chemical reaction process can be expressed by heat, called the heat of reaction, also known as the “enthalpy change” ( $\Delta H^\circ$ ).  $\Delta H^\circ > 0$  means that the adsorption of  $\text{U}(\text{VI})$  on  $\text{K}_2\text{FeO}_4@\text{PAO}$  and PAO surfaces is an endothermic process, which is consistent with the improved  $\text{U}(\text{VI})$  adsorption at higher reaction temperature. For a chemical reaction, the  $\Delta G^\circ$  value determines the reaction direction. The negative  $\Delta G^\circ$  value indicated that the adsorption of  $\text{U}(\text{VI})$  on  $\text{K}_2\text{FeO}_4@\text{PAO}$  and PAO is a spontaneous process, which also confirmed the strong affinity between  $-\text{C}(\text{NH}_2)\text{N}=\text{OH}$  and  $\text{U}(\text{VI})$ .

To evaluate the stability of  $\text{K}_2\text{FeO}_4@\text{PAO}$ , the desorption-regeneration properties of  $\text{K}_2\text{FeO}_4@\text{PAO}$  were studied. Different concentrations and solvents were used to eluate  $\text{K}_2\text{FeO}_4@\text{PAO}$ . First, 0.5  $\text{mol L}^{-1}$  HCl,  $\text{HNO}_3$ , NaOH, and  $\text{Na}_2\text{CO}_3$  were selected as eluting agents for the desorption of  $\text{U}(\text{VI})$  from the  $\text{K}_2\text{FeO}_4@\text{PAO}$  surface. As shown in Fig. S6,†  $\text{Na}_2\text{CO}_3$  showed the best resolution rate at 99%. Different concentrations (0.1–1  $\text{mol L}^{-1}$ ) of  $\text{Na}_2\text{CO}_3$  solution were used to eluate the  $\text{K}_2\text{FeO}_4@\text{PAO}$ . The elution results are shown in Fig. 6A, where it can be seen that the elution rate gradually increased with the increase in  $\text{Na}_2\text{CO}_3$  concentration. When the  $\text{Na}_2\text{CO}_3$  concentration reached 0.5  $\text{mol L}^{-1}$ , the solution elution rate could reach almost 100%, so 0.5  $\text{mol L}^{-1}$   $\text{Na}_2\text{CO}_3$  solution could achieve effectively regenerate  $\text{K}_2\text{FeO}_4@\text{PAO}$ . The adsorption capability of the regenerated  $\text{K}_2\text{FeO}_4@\text{PAO}$  for  $\text{U}(\text{VI})$  is shown in Fig. 6B. The adsorption capacity of  $\text{K}_2\text{FeO}_4@\text{PAO}$

**Table 2** Selected results of  $\text{U}(\text{VI})$  adsorption on  $\text{K}_2\text{FeO}_4@\text{PAO}$ .  $m/V = 0.40 \text{ g L}^{-1}$ ,  $T = 298 \pm 1 \text{ K}$ , contact time: 24 h, pH 8.2  $\pm 0.1$

Sample	$C[\text{U}(\text{VI})]$ ( $\text{mg L}^{-1}$ )		
	Initial	Final	Adsorption (%)
Diluted $\text{U}(\text{VI})$ slolution	20	10.62	46.90
	15	7.07	52.87
	10	5.04	49.60
	5	2.85	43.00
Running water	20	13.39	33.05
	15	8.65	42.33
	10	6.40	36.00
	5	2.87	42.60
Seawater	20	14.51	27.45
	15	8.78	41.47
	10	5.78	42.20
	5	2.17	56.60





**Fig. 6** Effect of Na<sub>2</sub>CO<sub>3</sub> concentration on the desorption of U(vi) from K<sub>2</sub>FeO<sub>4</sub>@PAO (A); recycling of K<sub>2</sub>FeO<sub>4</sub>@PAO in the extraction of U(vi) from solution (B); comparison of K<sub>2</sub>FeO<sub>4</sub>@PAO enrichment performance for 10 mg L<sup>-1</sup> U(vi) and heavy metal ions (C); U(vi) removal efficiency for K<sub>2</sub>FeO<sub>4</sub>@PAO with the coexistence of different anions (D).  $l = 0.1 \text{ mol L}^{-1} \text{ NaCl}$ ,  $T = 298 \pm 1 \text{ K}$ , contact time: 24 h.  $C[\text{U(vi)}]_{\text{initial}} = 10.0 \text{ mg L}^{-1}$ ,  $m = 0.02 \text{ g}$ ,  $V = 50 \text{ mL}$ ,  $\text{pH} = 8.2 \pm 0.1$ .

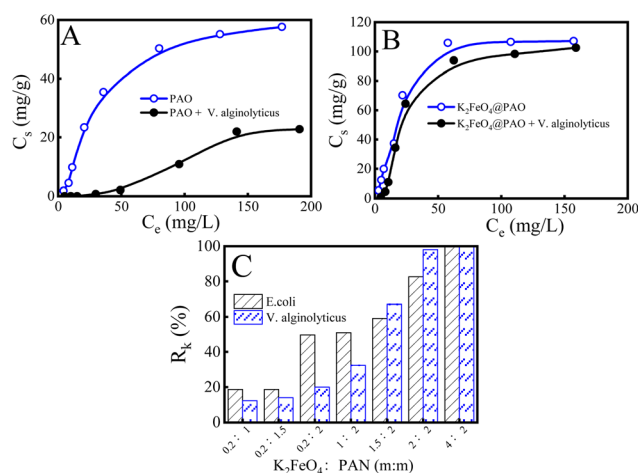
only decreased by 3% after its regeneration and reuse six times.

Based on the complex compositions of seawater, the coexistence of ions in seawater can affect the U(vi) adsorption. With various metal ions coexisting in seawater (such as Na(i), Ba(ii), Sr(ii), Ni(ii), Co(ii), Zn(ii), Cu(ii), Mn(ii), Pb(ii), and Fe(iii)), ICP-MS was used to detect the concentration of each ion and then to evaluate the selectivity of K<sub>2</sub>FeO<sub>4</sub>@PAO for U(vi). As depicted in Fig. 6C, the adsorption capacity of K<sub>2</sub>FeO<sub>4</sub>@PAO for U(vi) was higher than that of the other ions, indicating that K<sub>2</sub>FeO<sub>4</sub>@PAO had excellent selective adsorption capacity for U(vi) in the coexistence ion system. The recovery of U(vi) from anionic solutions was also investigated for K<sub>2</sub>FeO<sub>4</sub>@PAO. As shown in Fig. 6D, with the increase in ion concentration, the influence of HCO<sub>3</sub><sup>-</sup> on U(vi) recovery was undeniable due to the formation of new U(vi) species. In natural seawater, the concentration of various anions is far lower than 0.1 mol L<sup>-1</sup>, which means that anions have little effect on recycling U(vi).<sup>42</sup> K<sub>2</sub>FeO<sub>4</sub>@PAO was obtained by introducing K<sub>2</sub>FeO<sub>4</sub> into PAN to inhibit PAN agglomeration in water. The overall structure and morphology of the adsorbent were optimized. The particle size of K<sub>2</sub>FeO<sub>4</sub>@PAO can reach the nanometre scale, and it can be evenly dispersed in solution, so that the adsorbent can better contact with U(vi) and promote the occurrence of chemical reactions. The introduced K<sub>2</sub>FeO<sub>4</sub> did not damage the stability and selectivity of PAO. As we expected, the adsorption capability of K<sub>2</sub>FeO<sub>4</sub>@PAO was much higher than PAO in various U(vi) solutions. In K<sub>2</sub>FeO<sub>4</sub>@PAO, PAO ensures the excellent selectivity of K<sub>2</sub>FeO<sub>4</sub>@PAO for U(vi), and the nanoscale particle size enables K<sub>2</sub>FeO<sub>4</sub>@PAO to fully react with U(vi) in solution, ultimately ensuring that K<sub>2</sub>FeO<sub>4</sub>@PAO has better adsorption effect on U(vi) than other ions in complex systems.

Furthermore, K<sub>2</sub>FeO<sub>4</sub>@PAO also showed good cycling and selectivity for U(vi). In summary, K<sub>2</sub>FeO<sub>4</sub>@PAO can not only reduce the cost of the PAO preparation process and make the process greener, but can also further optimize the surface structure of the PAO and improve its adsorption properties in a variety of environments.

### Antibacterial activity of K<sub>2</sub>FeO<sub>4</sub>@PAO

Many marine microorganisms in seawater will accumulate on the surface of materials, resulting in the biological contamination of materials, which will lead to materials corrosion and finally affect the U(vi) adsorption performance. Conventionally obtained PAO powders have no ability to resist biological fouling and often need to work synergistically with other antibacterial materials in the field of anti-biological fouling U(vi) extraction from seawater. As is well known, K<sub>2</sub>FeO<sub>4</sub> presents excellent properties in decontamination, off-colour, and flocculation applications *etc.* Researchers have also found that the strong oxidation of K<sub>2</sub>FeO<sub>4</sub> can destroy bacterial structures (such as cell walls and cell membranes) and suppress the reproduction of bacteria.<sup>24,25</sup> Combining K<sub>2</sub>FeO<sub>4</sub> with PAO can be expected to break through the inhibition of PAO adsorption by marine bacteria and maintain good U(vi) recovery performance in bacteria-containing solutions. *Vibrio marine* is a kind of bacteria commonly living in the ocean. Here, we took *V. alginolyticus* as an example to investigate the effects of marine microorganisms on the U(vi) recovery performance by PAO and K<sub>2</sub>FeO<sub>4</sub>@PAO. We adjusted the *V. alginolyticus* concentration to  $1.0 \times 10^6 \text{ CFU mL}^{-1}$  (close to its concentration in offshore areas) and balanced this with PAO and K<sub>2</sub>FeO<sub>4</sub>@PAO for 24 h. As shown in Fig. 7A, *V. alginolyticus* resulted in severe biological contamination and significantly decreased the adsorption capacity compared with the samples without bac-



**Fig. 7** Adsorption of U(vi) by PAO (A) and K<sub>2</sub>FeO<sub>4</sub>@PAO (B) in solutions of different concentrations.  $m = 0.02 \text{ g}$ ,  $V = 50 \text{ mL}$ ,  $l = 0.1 \text{ mol L}^{-1} \text{ NaCl}$ .  $T = 298 \pm 1 \text{ K}$ ,  $\text{pH} = 8.2 \pm 0.1$ , contact time: 24 h; bactericidal rates against *E. coli* and *V. alginolyticus* of different particles (C). The K<sub>2</sub>FeO<sub>4</sub>@PAO materials were named according to the used amounts of K<sub>2</sub>FeO<sub>4</sub> and PAN (Table 1).



teria. These results indicated that biofouling has a significant effect on PAO-based materials. Unlike PAO, the recovery capability of  $K_2FeO_4@PAO$  for  $U(VI)$  did not significantly decrease compared with the data results for tests performed under sterile conditions, indicating that the  $K_2FeO_4$  ensured  $K_2FeO_4@PAO$  presented excellent anti-biofouling properties (Fig. 7B). Therefore, we studied the effect of the  $K_2FeO_4$  and PAO contents on the anti-biofouling properties of  $K_2FeO_4@PAO$ , using two Gram-negative bacteria (*E. coli* and *V. alginolyticus*). Fig. S7† shows the change in colonies of *E. coli* and *V. alginolyticus* on agar plates at different conditions. Fig. 7C exhibits the bactericidal rates calculated by the Petri dish counting method to quantitatively analyze different materials antibacterial properties. The results showed that  $K_2FeO_4$  is critical for the anti-biofouling properties of  $K_2FeO_4@PAO$  for *E. coli* and *V. alginolyticus*, and the anti-biofouling performance increased with increasing the  $K_2FeO_4$  content in  $K_2FeO_4@PAO$ .  $K_2FeO_4@PAO$  could kill almost all *E. coli* and *V. alginolyticus* when the  $K_2FeO_4$  dosage was increased to 4.0 g. The introduced  $K_2FeO_4$  not only promoted formatting PAO with good recovery performance for  $U(VI)$ , but also directly endowed the PAO with antibacterial properties to maintain good recovery for  $U(VI)$  in bacterial-containing solutions.

## Conclusions

Considering the limitation of PAO as a single material for  $U(VI)$  extraction from seawater, we further optimized the structure of PAN during the conversion of PAN into PAO to further enable the application of PAO to be used for multiple relationships. The results showed that fine control of  $K_2FeO_4$  dosage during the preparation process can effectively enhance the anti-biofouling property and adsorption capability of the PAO-based material ( $K_2FeO_4@PAO$ ) for extracting  $U(VI)$  from seawater.  $K_2FeO_4@PAO$  displayed good adsorption and circulatory capacities under laboratory conditions.  $K_2FeO_4@PAO$  also showed remarkable selectivity for  $U(VI)$  against multiple coexisting metal ions. Due to the  $K_2FeO_4$  effect,  $K_2FeO_4@PAO$  exhibited excellent anti-biofouling property, and could kill almost all *E. coli* and *V. alginolyticus*. In summary, research attempts to convert PAN into PAO in water and inhibit PAN agglomeration, improve the conversion rate of surface functional groups, improve its  $U(VI)$  adsorption capacity, and confer antibacterial properties will promote the further development of low-cost, pollution-free, and biofouling resistant  $U(VI)$  extraction materials from seawater.

## Experimental section

### Synthesis of $K_2FeO_4@PAO$

Two series of  $K_2FeO_4@PAO$  materials with different mass ratios (Table 1) were prepared by regulating PAN and  $K_2FeO_4$ . Specific amounts of  $K_2FeO_4$  and PAN powder, 3.20 g

$NH_2OH\cdot HCl$ , and 1.75 g NaOH were added into 20 mL de-gassed water. The solution was reacted at 75 °C for 6 h. After washing with de-gassed water, the  $K_2FeO_4@PAO$  materials were vacuum dried at 75 °C. To evaluate the effect of  $K_2FeO_4$ , PAO was also prepared by the same method.

### Synthesis of PAO in methanol/water solution

$NH_2OH$  solution was prepared by dissolving 4.0 g  $NH_2OH\cdot HCl$  in 50 mL methanol/water (4 : 1, V/V) solution, and the pH was adjusted to ~7.0 with NaOH under stirring condition. Then, 2.0 g PAN powder was added to the solution. Amidoximation reactions were performed at 75 °C for 6 h in a 100 mL glass flask under nitrogen and electromagnetic stirring condition. The resulting material was repeatedly washed with methanol/water (4 : 1, V/V) to remove the residual  $NH_2OH$ , and then vacuum dried at 50 °C.

### Synthesis of PAO in $H_2O$

After 3.2 g  $NH_2OH\cdot HCl$  was dissolved in 20 mL de-gassed water, NaOH was slowly added to pH ~ 7.0 under stirring condition. Then, 2.0 g PAN powder was added and reacted at 75 °C for 6 h. The resulting material was washed with de-gassed water, and vacuum dried at 50 °C.

### Characterization

Scanning electron microscopy was adopted to analyze the morphology of the particles (SEM, FEI Quanta 250 FEG) and transmission electron microscopy (TEM, FEI Tecnai G2 F20) was used to obtain the morphology of the particles. FT-IR spectroscopy was mounted on a Bruker Tensor II system with a platinum ATR instrument at room temperature. Thermogravimetric analysis (TGA, TGA 5500) was performed from room temperature to 800 °C under  $N_2$  atmosphere at a uniform heating rate of 10 °C  $min^{-1}$ . X-Ray photoelectron spectroscopy (XPS) measurements were obtained with an ESCALab220i-XL surface microanalysis system (VG Scientific) equipped with an Al  $K\alpha$  ( $h\nu = 1486.6$  eV) source at a chamber pressure of  $3 \times 10^{-9}$  mbar. The surface charging effects were corrected with the C 1s peak at 284.4 eV as a reference. Dynamic light scattering (DLS) measurements were used to measure the distribution of particles. DLS was operated on a Malvern Instruments Zetasizer operated in the backscatter (173°) mode. The PAO and  $K_2FeO_4@PAO$  were dispersed in methanol to prepare 250  $mg L^{-1}$  and 500  $mg L^{-1}$  sample slurries. A 10 mm sample pool was used for the measurements. The hydrophilicity of the adsorbents was determined by the dynamic contact angle of pure water droplets on a solid surface with a contact angle meter (JC200d Zhongchen Digital Technology, China).

### Batch adsorption experiments

The adsorption capabilities of  $K_2FeO_4@PAO$  for  $U(VI)$  were studied by batch adsorption technique, with  $UO_2(NO_3)_2\cdot 6H_2O$  (>99% purity) used as the  $U(VI)$  source.  $U(VI)$  stock solution was prepared from  $UO_2(NO_3)_2\cdot 6H_2O$  (>99% purity). Different concentrations of  $U(VI)$  sample solutions were prepared from the





stock solution. Briefly, after  $\text{K}_2\text{FeO}_4@\text{PAO}$  and PAO were pre-equilibrated with NaCl for 24 h, a solution containing  $\text{U}(\text{VI})$  diluted to a certain concentration with ultrapure water was added. The salinity of seawater is  $\sim 3.5\%$ , and most of it is NaCl. Because of the considerable amount of water used, the adsorbent must be competent for normal seawater values and salinity conditions. The equilibrium of the adsorbent in NaCl solution lays the foundation for  $\text{K}_2\text{FeO}_4@\text{PAO}$  for  $\text{U}(\text{VI})$  extraction from seawater. The solution pH values were adjusted by adding  $0.1 \text{ mol L}^{-1}$  NaOH or HCl. After shaking for the desired time in a thermostatic oscillation incubator, the suspension was filtered with a  $0.22 \mu\text{m}$  needle filter. The final  $\text{U}(\text{VI})$  concentration in the supernatant was measured by inductively coupled plasma mass spectrometry (ICP-MS, Thermo Scientific X-Series II,  $\lambda = 358.8 \text{ nm}$ ). The adsorption capacity of  $\text{U}(\text{VI})$  was calculated as follows:

$$C_s = (C_0 - C_e) \times \frac{v}{m} \quad (1)$$

$$R = \frac{C_0 - C_e}{C_0} \times 100\% \quad (2)$$

where  $V$  (L) is the volume of solution;  $C_0$  ( $\text{mg L}^{-1}$ ) refers to the original  $\text{U}(\text{VI})$  concentration;  $C_s$  stands for the adsorption capacity,  $m$  (g) represents the mass of adsorbent;  $R$  stands for the removal percentage; and  $C_e$  ( $\text{mg L}^{-1}$ ) is expressed as the equilibrium  $\text{U}(\text{VI})$  concentration.

#### Desorption of $\text{U}(\text{VI})$ from $\text{K}_2\text{FeO}_4@\text{PAO}$

Here,  $0.5 \text{ mol L}^{-1}$   $\text{Na}_2\text{CO}_3$  was used as the eluting agent to study the desorption of  $\text{U}(\text{VI})$  from the  $\text{K}_2\text{FeO}_4@\text{PAO}$  surface. Briefly,  $0.02 \text{ g}$   $\text{U}(\text{VI})$ -laden  $\text{K}_2\text{FeO}_4@\text{PAO}$  was immersed in  $50 \text{ mL}$   $0.5 \text{ mol L}^{-1}$   $\text{Na}_2\text{CO}_3$  and shaken at  $200 \text{ rpm}$  for  $24 \text{ h}$ . The regenerated  $\text{K}_2\text{FeO}_4@\text{PAO}$  was washed with de-gassed water and vacuum dried at  $50 \text{ }^\circ\text{C}$ .

#### Antibacterial property

The two kinds of Gram-negative bacteria *E. coli* and *V. alginolyticus* were chosen to verify the antibacterial properties of  $\text{K}_2\text{FeO}_4@\text{PAO}$ . The bacteria were severally cultured in Luria–Bertani (LB) medium and shaken at  $37 \text{ }^\circ\text{C}$  for  $12 \text{ h}$ . The resulting bacterial suspension was subsequently centrifuged at  $10\,000 \text{ rpm}$  for  $10 \text{ min}$ . The obtained bacterial precipitate was diluted by sterile physiological saline and the cell density was adjusted to  $\sim 1.0 \times 10^6 \text{ CFU mL}^{-1}$ . Next,  $0.02 \text{ g}$   $\text{K}_2\text{FeO}_4@\text{PAO}$  and  $50 \text{ mL}$  diluted bacterial solution at  $37 \text{ }^\circ\text{C}$  were incubated for  $24 \text{ h}$  to determine the antibacterial activity. The cultured bacterial solution ( $0.1 \text{ mL}$ ) was taken out and diluted and spread on an LB nutrient agar plate, followed by cultivation at  $37 \text{ }^\circ\text{C}$  for  $24 \text{ h}$ .

#### Effect of biofouling on $\text{U}(\text{VI})$ adsorption

To obtain the target compositions, the adsorbents ( $\text{K}_2\text{FeO}_4@\text{PAO}$ ) and NaCl were pre-reacted for  $24 \text{ h}$  at first; and then deionized water,  $\text{U}(\text{VI})$ , and exponential growth phase *V. alginolyticus* were injected, finally adjusting the suspension

pH. After reacting for  $24 \text{ h}$ , the suspensions were centrifuged at  $9000 \text{ rpm}$  for  $30 \text{ min}$  at  $25 \text{ }^\circ\text{C}$ , and then filtered. Except for specific evaluations, the reaction temperature, time,  $m/V$ , pH, and ionic strength were  $298 \pm 1 \text{ K}$ ,  $24 \text{ h}$ ,  $0.04 \text{ g L}^{-1}$ ,  $8.2 \pm 0.1$ , and  $0.10 \text{ mol L}^{-1}$  NaCl, respectively. The final  $\text{U}(\text{VI})$  concentrations were analyzed by inductively coupled plasma mass spectrometry (ICP-MS, Thermo Scientific X-Series II,  $\lambda = 358.8 \text{ nm}$ ).

## Conflicts of interest

There are no conflicts to declare.

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