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Reinforcement of ultrahigh thermoresistant polybenzimidazole films by hard craters†

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Porous structures were formed in polybenzimidazole derivative films by a silica template method, followed by HF etching. As expected, the resulting ultrahigh thermoresistant films showed better elongation properties than did the non-porous films, with renewed strength and hardness. Microscopic analyses revealed that the pores were clearly formed, and craters with swollen edges and hardened surfaces were also observed.

Production of bioplastics from renewable biological resources is imperative for developing a sustainable society and achieving low-carbon technology.¹ One of the major research topics in this regard is the synthesis of highly heat-resistant bioplastics because carbon dioxide in the atmosphere can be immobilized in durable materials for a considerable amount of time. For instance, 3-amino-4-hydroxybenzoic acid produced by genetically modified *Escherichia coli* can be converted to polybenzimidazole and its copolymers, both of which have extremely high heat resistance. Despite having the highest thermal decomposition temperature on record, polybenzimidazole-co-polyamide (poly(DABA-co-ABA)) films are found to be brittle in nature due to their rigid chain structure. Numerous studies have been conducted to improve the flexibility of polybenzimidazole through molecular design,² inorganic composites,³ and porous structure formation,⁴ among others. Porous structure formation can influence the merits of lightweight, physical stability, and high resiliency, which has attracted the attention of researchers in the last few decades.⁵ Luo and coworkers prepared porous PBI films using a phase separation process induced by water vapour. Chaudhari and coworkers prepared these films using the immersion precipitation method.⁶ The

effects of the porous structure on the mechanical properties of the films are rarely discussed in those reports, but the results reveal that the formation of porous structures improves the elongation rate of the material while degrading their mechanical properties. On the other hand, the silica (SiO₂) hard-template method, which is primarily used for water-absorbable materials such as hydrogels does not alter the components or chemical structure of the polymer, thus being a promising strategy for the processing of materials.⁷ In our study, we discovered that high-performance polymer films are also water-absorbable plastics due to their polar structures.⁸ Therefore, porous structures were cast in poly(DABA-co-ABA) films, and the hard-template method using SiO₂ nanoparticles was adopted to improve their stretchability and hardness (Fig. 1).

To form pores in poly(DABA-co-ABA), SiO₂ having a particle size of 300 nm was added to a mixed solution of poly(DABA-co-ABA) in trifluoroacetic acid (TFA)/methanesulfonic acid (MSA) and stirred until dissolution. Then, a PBI-SiO₂ composite film was produced by casting the mixed solution onto a glass substrate. The obtained film was etched with hydrofluoric acid (HF) to obtain a poly(DABA-co-ABA) porous film. The Fourier transform infrared (FT-IR) spectrum of SiO₂ showed a broad absorption band at 1000–1180 cm⁻¹, which was assigned to the Si–O–Si groups (Fig. S2†). As for the pristine poly(DABA-co-ABA), the characteristic bands at 1636, 1553, and 1284 cm⁻¹ were assigned to the stretching vibration of the C=N, C=C, and C–N groups, respectively, and the broad absorption band at 3250–3450 cm⁻¹ corresponded to N–H groups. A medium-strong peak was observed at 1000–1180 cm⁻¹ in the spectrum



Fig. 1 Preparation of porous poly(DABA-co-ABA) films.

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of the composite poly(DABA-co-ABA), confirming that the SiO₂ nanoparticles were templated. After HF etching, the Si–O–Si absorption peak disappeared from the spectrum of the porous poly(DABA-co-ABA), indicating that the SiO₂ nanoparticles were completely removed and no change in the chemical structure occurred since the observed characteristic peaks of pristine poly(DABA-co-ABA). Based on these results, visual confirmation through scanning electron microscopy (SEM) was carried out to establish that pores were actually formed in the poly(DABA-co-ABA) film (Fig. 2). The pristine poly(DABA-co-ABA) film, as seen in Fig. 2a, was dense and homogenous with no pores on both the surface and the edge. As for the porous poly(DABA-co-ABA) films, nanoporous structures with a diameter of about

300 nm were observed on the surface and the edges after HF etching, corresponding to the size of the used SiO₂ nanoparticles (Fig. 2b and c).

PBI has high elastic properties because of its rigid backbone, numerous hydrogen bonds and strong intermolecular interactions. Furthermore, it is well-known that when pores are introduced into polymer films, the elongation ratio is improved, but the strength and hardness are significantly reduced.⁹ On the other hand, after introducing pores into the poly(DABA-co-ABA) films, Young's modulus increased from 2.9 to 3.4 GPa for the film (including pore area for calculation) and from 2.9 to 8.4 GPa for matrix polymers (excluding pore area for calculation) (Table 1). Elongation at break increased from 2.6 to 12.7%, as expected. The strain energy density (toughness) increased from 0.7 MJ m⁻³ for pristine poly(DABA-co-ABA) film to 18.7 MJ m⁻³ for porous poly(DABA-co-ABA) film. In addition, an improved toughness was observed at the SiO₂ nanoparticles addition of 10 wt%, and the toughness improved as increasing the amount of SiO₂ nanoparticles (Fig. S3†). From these results, the introduction of porous structures by HF etching of SiO₂ nanoparticles forms a hard crater and shows higher strength than pristine poly(DABA-co-ABA) film. At the same manner, it also appears the effect of improving the elongation rate due to introducing the porous structures. These effects led to the synergistic improvement of the mechanical properties. As stated earlier, the pores usually compromise the mechanical properties, but the porous poly(DABA-co-ABA) film displayed an improvement in both toughness and stiffness (Young's modulus) as compared to those of the pristine poly(DABA-co-ABA) film. Regarding poly(DABA-co-ABA) without pores, there was no change in the mechanical properties before and after HF treatment (Fig. S4†). From this result, it was strongly suggested that the toughness improvement of porous poly(DABA-co-ABA) films was due to the introduction of the porous structures. Meanwhile, unlike the porous structures reported in other works, a rim of the white region was seen around each of the pores, circumscribing them (Fig. 2b and c). These unusual regions were investigated by a scanning probe microscope (SPM, SHIMADZU NANO6A). These white rims around each pore appear brighter than the area apart from the pores, indicating that these rims areas (around the pores) are higher or elevated than the rest of the



Fig. 2 SEM images of (a) pristine poly(DABA-co-ABA), (b) porous poly(DABA-co-ABA)-30%, and (c) porous poly(DABA-co-ABA)-50% film. SEM images of cross-section of films are inset.

Table 1 Mechanical properties of pristine poly(DABA-co-ABA) and porous poly(DABA-co-ABA)-50% films

Mechanical property	Pristine film	Porous film
Stress ^a (MPa)	47 ± 1	71 ± 3 (169 ± 6)
Strain ^a (%)	2.6 ± 0.1	12.7 ± 0.1 (12.7 ± 0.1)
Young's modulus ^a (GPa)	2.9 ± 0.1	3.4 ± 0.1 (8.4 ± 0.3)
Toughness ^a (MJ m ⁻³)	0.7 ± 0.1	7.9 ± 0.1 (18.7 ± 0.3)
Elastic modulus ^b (MPa)	72	672 ± 36

^a Properties of entire films including pore volume. The value in parentheses were the properties based on the polymer matrix which was calculated from excluding pore volume. ^b Calculated from the Johnson–Kendall–Roberts (JKR) model.



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