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Asymmetric Toughening in the Lap Shear of Metamaterial Structural Adhesives

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Abstract

Metamaterial structural adhesives (MSAs), whose properties primarily rely on structural designs, offer promising advantages over traditional adhesives, including asymmetric, switchable, and programmable adhesion. However, the effects of thick backing structures on the adhesion properties remain largely underexplored. Herein, we investigate a series of MSAs featuring a thin adhesive layer and an asymmetric thick beam structure terminated with a film. We conduct lap shear tests on the MSAs with varied terminated film thickness (t) and beam tilting angle (θ) while maintaining an identical adhesive layer. For MSAs with a thick terminated film ($t = 2$ mm), the effective adhesion energy is double that of solid samples without compromising shear strength, consistent with the theoretical predictions based on the crack trapping mechanism. Conversely, for MSAs with a thin terminated film ($t = 0.5$ mm), the maximum shear strength and effective adhesion energy are ~2.8 times and ~18.6 times that of solid samples, respectively, deviating significantly from the theoretical predictions due to new crack initiations. We further explore adhesion asymmetry by tuning the beam tilting angle (θ). For MSAs with highly tilted beams ($\theta = 70.3^{\circ}$), we achieve a maximum adhesion strength asymmetry factor of $\tau_2/\tau_1 \sim 2.2$ for a thick terminated film ($t = 2$ mm), and a maximum adhesion energy asymmetry factor of $\Gamma_1/\Gamma_2 \sim 5.3$ for a thin terminated film ($t = 0.5$ mm). Our work provides useful insights for designing metamaterial structural adhesives suitable for robotic grippers, wall-climbing robots, and wearable devices, particularly those requiring asymmetric, switchable, and stimuli-responsive adhesion, and adhesives on rough surfaces or in underwater conditions.

Key words: Metamaterial structural adhesives; Crack trapping; Lap shear; Toughening of adhesion; Asymmetric adhesion.

1. Introduction

Adhesives and tapes play crucial roles in various fields in modern society. Traditional adhesives and tapes largely rely on semi-empirical modification of bulk rheological properties and interfacial chemistry of polymers to achieve strong, tunable, or stimuli-responsive adhesion[1-8]. Achieving asymmetric adhesion is generally challenging through chemical modifications of bulk materials, which is strongly desired for emerging applications requiring switchable adhesion[6, 7]. For example, for wearable devices, tissue adhesives, robotic grippers, and wall-climbing robotics, asymmetric adhesives can enable strong attachment in one direction during service while easy detachment in the other direction after service with reversibility[9, 10]. Notably, metamaterial adhesives (MAs) have recently been explored, which have shown significantly enhanced adhesion, reversibility and reusability, directional and spatial programmability, universal adhesion to diverse substrates without chemical modifications, and directionally asymmetric adhesion[9-21]. Representative examples of MAs include adhesive thin films with stiffness variations[11, 20-23], asymmetric adhesive thin films with nonuniform thickness profiles[17, 24], and kirigami-based adhesives with asymmetric cuts[9, 10, 14, 25]. Previous MAs typically resemble thin pressure sensitive adhesives utilizing two-dimensional planar patterns, comprising a thin adhesive layer and a thin, mostly non-stretchable backing layer.

On the contrary, thick structural adhesives, e.g., commercial foam tapes for insulating, protecting, and sound dampening[26-28], are typically composed of a thin adhesive layer and a relatively thick and compliant backing structure. In recent years, new structural adhesives have been developed, exhibiting some unique benefits for engineering applications in robotic grippers[15, 16, 29] and wall-climbing robots[30, 31]. For example, a recent study presented a structural adhesive utilizing bistable beams within an enclosed frame as the backing, together with an adhesive tape for pick-and-release purposes[16]. Another study proposed a structural adhesive for robotic grippers employing a thick backing structure composed of periodic tilted beams and a gecko-inspired adhesive layer for enhanced grasping[15]. Notably, an earlier study demonstrated that a hollow backing with symmetric vertical beams could significantly enhance the adhesion energy of gecko-inspired structural adhesives through crack trapping-induced adhesion toughening[13]. Another study measured asymmetric adhesion using indentation tests and frictional properties using sliding tests of gecko-inspired structural adhesives with an asymmetric hollow backing structure consisting of periodic tilted beams[32]. However, the mechanistic understanding and quantitative influence of asymmetric backing structures on adhesion toughening and asymmetry of thick structural adhesives under shear loading remains unexplored in fracture-dominated conditions.

In this study, we develop a series of metamaterial structural adhesives (MSAs) comprising two components: a thin adhesive layer, and a thick and asymmetric hollow backing consisting of tilted beams terminated with a film (Fig. 1a, top). The hollow structure is originally designed as the backing of the structural adhesive for robotic grippers, as reported in a previous study[15]. Subjected to an external shear force, the hollow backing undergoes beam buckling, allowing different structural adhesives, i.e., adhesive pads of the robotic grippers, to equally share the load. In our study, we aim to combine experimental, numerical, and theoretical methods to study how the geometry of the backing structure affects the adhesion properties of MSAs under lap shear tests in fracture-dominated conditions. We conduct lap shear tests using one rigid PMMA plate and one flexible PET film (Fig. 1a).

Our results have shown that for MSAs with a relatively thick terminated film ($t = 2$ mm), the effective adhesion energy is approximately twice that of solid samples, without compromising its shear strength. Our theoretical and numerical analyses identify crack trapping as the toughening mechanism if the crack propagates unidirectionally following a predefined path. For hollow MSAs, with a fixed shear displacement, the energy release rate varies periodically with the crack length, causing unstable crack propagation in practical loadings and thus adhesion toughening. For MSAs with a relatively thin terminated film ($t = 0.5$ mm), the maximum shear strength is ~2.8 times and ~2.4 times that of solid samples for two opposite pulling directions, and the effective adhesion energy is ~18.6 times and 9.8 times that of solid samples for two opposite pulling directions. However, new crack initiation at the interface may lead to a substantial deviation between experimental results and theoretical predictions based on the crack trapping mechanism. Furthermore, we explore the adhesion asymmetry by varying the beam tilting angle θ. For MSAs with a thick terminated film ($t = 2$ mm), a shear strength asymmetry factor of $\tau_2/\tau_1 \sim 2.2$ is achieved for highly tilted beams ($\theta = 70.3^{\circ}$), while the adhesion energy asymmetry factor Γ_2/Γ_1 is less dependent of θ due to the crack trapping mechanism for both pulling directions. For MSAs with a thin terminated film ($t = 0.5$ mm), a strength asymmetry factor of $\tau_1/\tau_2 \sim 1.4$ and an adhesion energy asymmetry factor of $\Gamma_1/\Gamma_2 \sim 5.3$ are attained for highly tilted beams ($\theta = 70.3^{\circ}$). Our research may provide useful insights to develop metamaterial structural adhesives with enhanced, asymmetric, and switchable properties through simple structural designs.

2. Experimental methods

2.1 Fabrication of the MSAs

To fabricate the thick backing structures with a relatively thick terminated film ($t = 1$, 1.5 and 2 mm) (Fig. S1a), we first printed a rigid mold with the fused filament fabrication printer (FlashForge Guider 2) or the high-resolution polyjet printer (Connex 3 Objet 500, Stratasys). Then, we mixed parts A and B of

Dragon Skin 00-30 (Smooth-on) in a 1:1 weight ratio. The precursor underwent mixing using the ARM-310 mixer (THINKY) at 2000 RPM for 1 min, followed by refrigeration for 5 min, and a final mixing step at 2000 RPM for 1 min. The resulting precursor was poured into the mold and left at room temperature for 4 h for curing.

To fabricate the thick backing structures with a relatively thin terminated film ($t = 0.5$ or 0.75 mm) (Fig. S1b), we first followed the above procedures to fabricate one part of the hollow structure. We then injected the Dragon Skin precursor into a sandwiched mold with a silicone spacer ($t = 0.5$ or 0.75 mm) to fabricate the thin terminated film. Next, we mixed the base and curing agent of PDMS (Sylgard 184, Dow Corning) at a 20:1 weight ratio, and then added a Pt-catalyst (Gelest SIP6831.2) at 0.5 uL/g. The PDMS precursor was mixed for 2 min and degassed for 5 min in a vacuum pump, which was then used to bond the thin terminated film with the molded partial hollow structure. We stored the assembled sample in a 60 ℃ oven overnight for curing.

We listed the dimensions of hollow structures in Fig. S1c and Supplementary Table 1. The length, height, and width of the hollow backing structure are denoted as L, H, and w, respectively. The beam tilting angle is denoted as θ. The width of a beam and the spacing between two neighboring beams are denoted as b and s, respectively. The spatial period of the hollow structure is thus $\lambda = b + s$. The number of periods/beams is denoted as N. The thickness of the terminated film is denoted as t. For each backing design, we fabricated the solid sample with the same dimensions of $L \times H \times w$ to measure the intrinsic adhesion properties.

We next bonded a polyethylene terephthalate (PET) thin film (75um, McMaster Carr) to the top of the backing structure using silicone adhesive (Loctite 908570). Then, we mixed the base and curing agent of PDMS at a 15:1 weight ratio and added the Pt-catalyst (Gelest SIP6831.2) at 0.5 uL/g. We used the PDMS precursor to bond the backing structure to a rigid polymethyl methacrylate (PMMA) plate (3 mm). We stored the assembled sample at room temperature overnight and then in a 50 °C oven for curing. The fabricated MSAs had an ultra-thin PDMS adhesive layer (t~0.08 mm) with the shear modulus (μ) of 0.3 MPa[33] (Fig. 1a). Notably, both PET film and PMMA plate matched the width of the hollow backing. We prepared the solid samples using identical procedures (Fig. 1a).

2.2 Lap shear tests of MSAs

As shown in Fig. 1a, we introduced an initial crack with the length of C_0 (Supplementary Table 1) at the interface between the PDMS adhesive layer and the PMMA plate. Then, we tested all samples using a tensile machine (5965 Dual Column Testing Systems; Instron) equipped with a 1 kN load cell. We fixed the ends of the PET film and PMMA plate to the bottom and top grippers, respectively. Then, we applied

monotonic loading to all the samples at a rate of 0.05 mm/s until the MSAs completely debonded from the PMMA plate. Simultaneously, we recorded force-displacement curves and filmed all tests with a digital camera (Canon 60D). In all the tests, adhesive failure was consistently observed between the PDMS adhesive layer and the PMMA plate, rather than debonding between the PDMS adhesive layer and the hollow backing structure (Fig. 2b).

We measured the intrinsic adhesion properties from solid samples. The intrinsic shear strength (τ_0) is defined as the maximum force (F_{max}) divided by the effective adhesion area (A_{eff}), i.e., $\tau_0 = F_{max}/A_{eff}$, where $A_{eff} = (L - C_0) \times w$. The intrinsic work of adhesion (W_{ad}) is defined as the input work to rupture the entire interface divided by A_{eff}, i.e., $W_{ad} = \frac{1}{A_{eff}}\int_{u=0}^{u=u_{debond}} Fdu$, where u_{debond} is the displacement at which the force drops to zero.

Similarly, for MSAs, we define the shear strength (τ_i) and the effective adhesion energy (Γ_i) as $\tau_i = F_{i\_max}/A_{eff}$ and $\Gamma_i = \frac{1}{A_{eff}}\int_{u=0}^{u=u_{debond}} Fdu$, respectively, where $i = 1$ or 2 represents the two opposite pulling directions. The normalized shear strength and normalized adhesion energy of MSAs relative to solid samples are defined as τ_i/τ_0 and Γ_i/W_{ad}, respectively.

2.3 Finite element simulation

We simulated the lap shear tests of MSAs in Abaqus using a static, general method. We adopted linear elastic models for both PMMA and PET, with PET characterized by a Young's modulus (E) of 2950 MPa and Poisson's ratio (ν) of 0.43, and PMMA with E of 2900 MPa and ν of 0.4. We modeled the hollow backing structure as a Neo-Hookean material with a shear modulus (μ) of $= 0.28$ MPa. We set the bulk modulus at least 1000 times of shear modulus to account for incompressibility. As mentioned above, the PDMS adhesive layer (t~0.08 mm) is much thinner than the thinnest terminated film ($t = 0.5$ mm) in this study. Additionally, PDMS and the hollow backing structure have similar shear moduli. Therefore, when computing the energy release rate, it is appropriate to ignore the ultra-thin PDMS adhesive layer in the geometry of the model. We introduced a seam crack with the length of C_0 at the MSA-PMMA interface. We assumed plane strain conditions using CPE4RH elements. In the FEM modeling, we applied displacement control to the end of the PMMA plate while fixing the end of the PET film (Fig. 1a). We then obtained force-displacement curves from the simulation and calculated *J*-integral around the crack tip. We gradually increased the crack length by a finite value dC, and repeated the above process. We varied the crack length within a range more than the spatial period λ. Finally, with energy release rate-displacement curves at different crack lengths, we processed the data to get energy release rate-crack length curves at

different applied shear displacements. Mesh refinement, especially near the crack tip, was conducted through iterative refinement until simulation results converged.

3. Results

3.1 The adhesion toughening arising from the crack trapping mechanism

In engineering applications like robotic grippers[15, 16, 29] and wall climbing robotics[30, 31], structural adhesives usually experience shear load. In this study, we focus on lap shear experiments of MSAs in fracture-dominated conditions with no normal force applied to MSAs. As shown in Fig. 1a, we attached the MSA with a flexible PET backing layer to a rigid PMMA plate. We maintained the adhesive layer, a thin PDMS film cured from its precursor, unchanged throughout this study. We introduced an initial crack of C_0 at the PDMS-PMMA interface, exceeding the sample height (H) but much shorter than the sample length (L) (Supplementary Table 1). We monotonically pulled the end of PMMA plate while fixing the end of PET film until the crack propagated through the entire interface. During the pulling, we recorded force-displacement curves (Fig. 1b). As expected, the MSA displays a smaller stiffness than the solid sample.

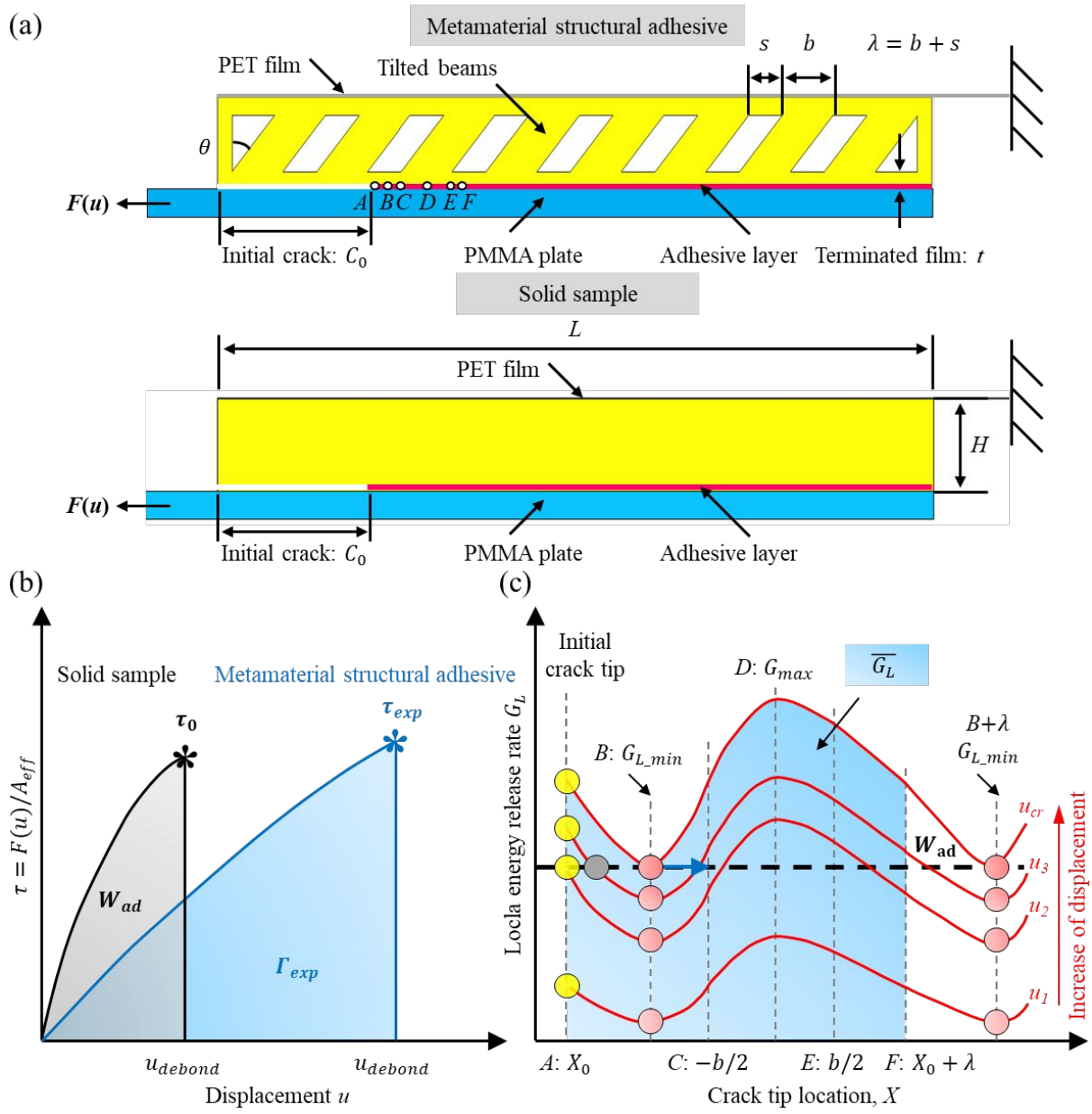


Fig. 1. Adhesion toughening arising from the crack trapping mechanism in the lap shear of metamaterial structural adhesives. (a) Schematics depict lap shear tests for both the hollow MSA (top) and solid sample (bottom), with labeled geometric dimensions and horizontal positions. (b) Representative shear stress-displacement curves for the MSA (blue) and solid sample (black), respectively. For the solid sample, the black star symbol indicates the intrinsic shear strength τ_0 and the shaded area represents the intrinsic work of adhesion W_{ad}. For the MSA, the blue star symbol indicates the shear strength τ_{exp} and the shaded area indicates the effective adhesion energy Γ_{exp}. (c) Local energy release rate G_L around the crack tip versus the crack tip location X for the MSA (red lines). The black dash line represents W_{ad}. Yellow circles denote G_L at the initial crack tip ($X = X_0$). Red circles denote the minimum of G_L at $X = X_{min}$ and

$X = X_{min} + \lambda$, respectively. With the increase of the applied shear displacement u, $G_{L\_min} = W_{ad}$ is satisfied at the critical displacement ($u = u_{cr}$), leading to unstable crack propagation (blue arrow). The blue shaded area, divided by the period λ, represents the averaged energy release rate $\overline{G_L}$. Note that the relationship between the local energy release rate and the crack length depends on the geometric parameters of the hollow backing structures, as reported in a previous theoretical study[34].

The adhesion enhancement of MSAs is achieved through the crack trapping mechanism as previously proposed[11, 13, 34-36], which is briefly reformulated as follows. We establish a horizontal X-axis, with the origin ($X = 0$) located at the center of the beam ahead of the crack (mark *D* in Fig. 1a). We assume the initial crack length is C_0 with the tip located at $X = X_0$ (mark *A* in Fig. 1a). When the crack propagates by a distance of λ, the crack tip reaches at $X = X_0 + \lambda$ (mark *F* in Fig. 1a). To maintain stable equilibrium crack propagation, it is required that

$$G_L = W_{ad}, \text{ and } \frac{dG_L}{dc} < 0, \quad (1)$$

where c is the crack length, G_L is the energy release rate around the crack tip, and W_{ad} is the intrinsic work of adhesion. For stable crack propagation, the averaged energy release rate is the same as W_{ad}.

However, for the MSA, at a fixed displacement u, due to its periodic beam structures, the local energy release rate G_L varies periodically in space (Fig. 1c):

$$G_L(c = C_0) = G_L(c = C_0 + \lambda). \quad (2)$$

To satisfy eqn (1), the applied displacement u needs to be varied with the crack length c non-monotonically during the crack propagation. However, in practice, the applied displacement u is usually monotonically increased, leading to unstable crack propagation.

As shown in Fig. 1c, at a small displacement ($u = u_1$), $G_L < W_{ad}$ at the initial crack tip prevents crack propagation. At a larger displacement ($u = u_2$), $G_L = W_{ad}$ is satisfied at the initial crack tip, yet crack propagation is hindered because $\frac{dG_L}{dc} < 0$. At an even larger displacement ($u = u_3$), the crack front propagates unstably from the initial position (yellow circle) to the position indicated by the gray circle because $G_L \geq W_{ad}$. Afterwards, crack propagation stops because $G_L < W_{ad}$ and $\frac{dG_L}{dc} < 0$. To overcome the crack trapping, a critical displacement ($u = u_{cr}$) is required to achieve $G_{L\_min} = W_{ad}$ at both $X = X_{min}$ and $X = X_{min} + \lambda$. When the crack propagates by a period from $X = X_{min}$ to $X = X_{min} + \lambda$, $G_L > W_{ad}$ always holds true, resulting in unstable crack propagation. The total elastic energy stored in the MSAs before the

critical displacement ($u = u_{cr}$) is calculated as $\int_{c=X_{min}}^{c=X_{min}+\lambda} G_L dc$. Under practical monotonic loadings in experiments, all the stored elastic energy is dissipated through unstable crack propagation. In addition to the energy required to separate the interface, the excess elastic energy compared to W_{ad} is fully dissipated through inelastic processes such as damping, damage, and viscoelasticity[11, 13, 34-36].

Therefore, for our MSAs, we defined the effective adhesion energy ($\overline{G_L}$) by averaging the reduction of elastic energy within one period (λ) at $u = u_{cr}$ (the blue shaded area in Fig. 1c), which is calculated as

$$\overline{G_L} = \frac{1}{\lambda}\int_{c=C_0}^{c=C_0+\lambda} G_L dc\,. \quad (3)$$

Similar definitions have been widely used to assess the toughening effect of periodically heterogeneous materials in previous studies[13, 34, 37, 38].

Based on the argument of the energy balance in fracture mechanics, we assume the work done by the external force is all dissipated by the formation of the new crack surface:

$$\int_{u=0}^{u=u_{debond}} F du = A_{eff}\Gamma_{exp}, \quad (4)$$

where A_{eff} is the effective adhesion area between the MSA and PMMA plate and Γ_{exp} is defined as the effective adhesion energy as shown in Fig. 1b.

Recall the definition of energy release rate $G_L = -\frac{\partial U(u,c)}{\partial c}$, where U is the elastic energy of the MSA per unit width and c is the crack length. When the crack propagates through the entire interface, with the periodic assumption in eqn (3), we have

$$\Delta U = \int_{c=C_0}^{c=L} G_L dc = N\lambda\overline{G_L}, \quad (5)$$

where N is the number of periods and is defined as $N = \frac{L-C_0}{\lambda}$. Thus, we have

$$\Delta U = (L - C_0)\overline{G_L}, \quad (6)$$

which can be obtained using the integration of the blue shaded area in Fig. 1c.

Before the onset of crack propagation, the work done by the external force is stored as elastic energy in the MSA:

$$\int_{u=0}^{u=u_{debond}} F du = w\Delta U. \quad (7)$$

Thus, with eqn (4), (6), and (7), we can obtain

$$\frac{1}{A_{eff}}\int_{u=0}^{u=u_{debond}} Fdu = \Gamma_{exp} = \overline{G_L}, \quad (8)$$

which indicates the toughening effect of MSAs compared to solid samples that $\Gamma_{exp} > W_{ad}$ for unstable crack propagation.

3.2 Experimental results and theoretical predictions

To confirm the crack trapping mechanism, we employ a hollow design featuring slender tilted beams and a thick terminating film (the cases with "$b = 2.4$ mm" and "$t = 2$ mm" in the first group of Supplementary Table 1) (Fig. 2a). As shown in Fig. S2a and Movie S1, the solid sample shows an initial crack opening upon the shear loading, followed by stable and fast propagation as the load increases. Eventually, adhesive failure occurs between the solid sample and PMMA plate. As shown in Fig. 2b and Movie S2, for the MSA, an initial crack opening is observed upon the shear loading. However, subsequent crack propagation stops on the left side of the beam. To enable further crack propagation, the loading needs to be further increased to advance the crack through the beam in an unstable manner. We observe periodic crack trapping and unstable crack propagation in experiments till the entire interface fails. Unless otherwise specified, adhesive failure was consistently observed between the PDMS adhesive layer and the PMMA plate in all the tests.

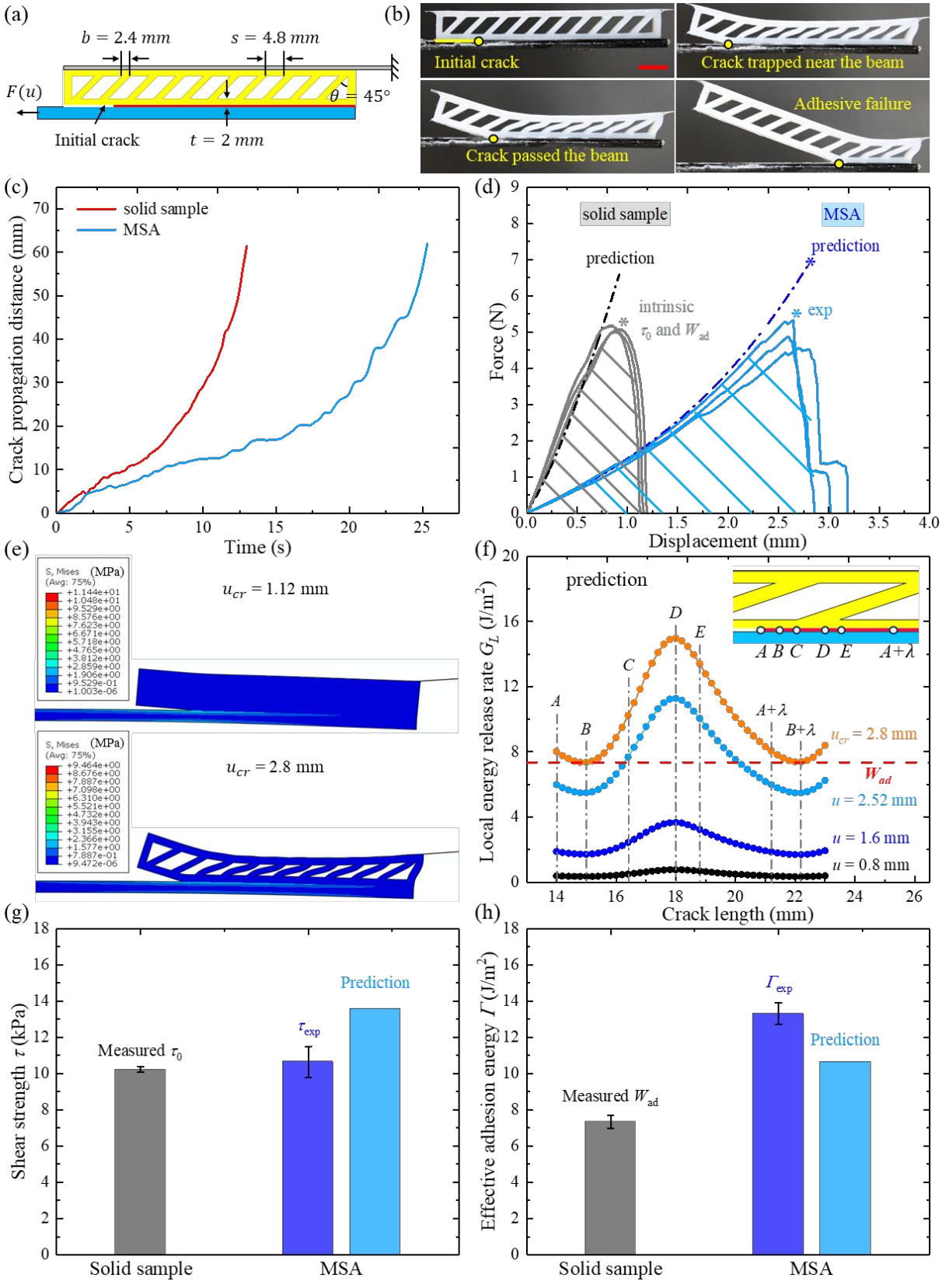

(a)
b = 2.4 mm
s = 4.8 mm
F(u)
θ = 45°
Initial crack
t = 2 mm
(b)
Initial crack
Crack trapped near the beam
Crack passed the beam
Adhesive failure
(c)
solid sample
MSA
Crack propagation distance (mm)
Time (s)
(d)
solid sample
MSA
prediction
prediction
intrinsic
τ0 and Wad
exp
Force (N)
Displacement (mm)
(e)
S, Mises (MPa)
(Avg: 75%)
ucr = 1.12 mm
ucr = 2.8 mm
(f)
prediction
A B C D E A+λ
Local energy release rate GL (J/m2)
ucr = 2.8 mm
Wad
u = 2.52 mm
u = 1.6 mm
u = 0.8 mm
Crack length (mm)
(g)
Prediction
τexp
Measured τ0
Shear strength τ (kPa)
Solid sample
MSA
(h)
Γexp
Prediction
Measured Wad
Effective adhesion energy Γ (J/m2)
Solid sample
MSA

Fig. 2. Agreements between experimental measurements and theoretical predictions in the lap shear of MSAs with slender beams and a thick terminated film when the crack propagates unidirectionally along the predefined path. (a) Schematic showing the lap shear test and geometric parameters of the MSA. (b) Images capturing the crack propagation dynamics, with the crack tip highlighted by a yellow circle. Scale bar, 1cm. (c) Crack propagation distance versus time for both the solid sample and MSA. (d) Comparison between experimental and predicted force-displacement curves for the solid sample and MSA, respectively. Predicted curves are truncated at $u = u_{cr}$ where $G_{L\_min} = W_{ad}$ is satisfied. (e) Simulation of deformation for the solid sample (top) and MSA (bottom) at $u = u_{cr}$ (stress unit: MPa). (f) Theoretical predictions of G_L versus crack length at various displacements for the MSA, with the red dash line denoting W_{ad}. Positions marked by gray dash dot lines correspond to locations labeled in the top right insert: *A* (the initial crack tip, $X = X_0$), *B* ($X = X_{min}$ where $G_L = G_{L\_min}$), *C* (beam left), *D* ($X = X_{max}$ where $G_L = G_{L\_max}$), and *E* (beam right). Comparative analysis between experimental and predicted shear strength τ (g) and effective adhesion energy Γ (h) of MSAs relative to solid samples.

We plot the crack propagation distance with time and find that crack propagation of the solid sample is much faster than that of the MSA (Fig. 2c). Additionally, the MSA displays stepwise increment of crack size, indicating crack trapping and unstable crack propagation as shown in Fig. 2b and Movie S2.

Both solid samples and MSAs exhibit reproducible force-displacement curves, with negligible dispersion across multiple samples (solid lines in Fig. 2d). We measure the intrinsic shear strength τ_0 (gray star) and work of adhesion W_{ad} (gray shaded area) from solid samples, which exhibits weak dependence on sample dimensions (Fig. S2b and c). Similarly, we measure the shear strength τ_{exp} (blue star) and effective adhesion energy Γ_{exp} (blue shaded area) for MSAs.

We further conduct finite element analysis to quantitatively elucidate the adhesion toughening of MSAs. We truncate the predicted force-displacement curves at the critical displacement $u = u_{cr}$ when $G_{L\_min} = W_{ad}$ is satisfied, which agrees well with experimental results (dash dot lines in Fig. 2d). Deformation profiles from finite element simulation also agree with experimental results (Fig. 2e). Next, we compute the G_L-crack length relationship from the simulations. For the solid sample, G_L remains nearly constant as a function of crack length provided that the initial crack is long enough (Fig. S2d). At a critical displacement ($u_{cr} = 1.12$ mm), $G_L = W_{ad}$ and $\frac{dG_L}{dc} = 0$ are satisfied, indicating the onset of stable crack propagation (Fig. S2d). In contrast, for the MSA, the energy release rate $G_L$varies periodically with the crack length (Fig. 2f), reaching $G_{L\_min} = W_{ad}$ at the critical displacement ($u_{cr} = 2.8$ mm). As explained in

Fig. 1, unstable crack propagation occurs once $G_{L\_min} = W_{ad}$ is satisfied, which leads to adhesion toughening.

Experimental results reveal a shear strength of $\tau_{exp} = 10.7$ kPa for MSAs, close to that of solid samples ($\tau_0 = 10.2$ kPa) (Fig. 2g). The predicted shear strength of MSAs is $\tau_{pre} = 13.6$ kPa, deviating by ~27% from numerical predictions. We attribute such discrepancy to several factors: first, $W_{ad} = 7.3\ \mathrm{J/m^2}$, measured from solid samples, represents an averaged work of adhesion for rupturing the entire interface rather than work of adhesion corresponding to crack initiation; second, our simulations assume a stable equilibrium state, neglecting all the inelastic processes; third, by claiming $\Gamma_{exp} = \overline{G_L}$, we neglect the edge effects of the finite MSAs and viscoelastic dissipation; lastly, in the simulations, the initial crack doesn't propagate until $G_{L\_min} = W_{ad}$ is satisfied ($u = u_{\mathrm{cr}}$ in Fig. 1c), whereas in experiments, the crack propagates a little bit with the increase of displacement from $u = u_2$ to $u = u_{\mathrm{cr}}$ (Fig. 1c).

Furthermore, the experimental effective adhesion energy of MSAs is $\Gamma_{exp} = 13.3\ \mathrm{J/m^2}$, nearly doubling that of solid samples ($W_{ad} = 7.3\ \mathrm{J/m^2}$) (Fig. 2h), showing the toughening effect. The predicted adhesion energy is $\overline{G_L} = 10.6\ \mathrm{J/m^2}$ calculated with eqn (3) using the simulation results in Fig. 2f, close to our experimental results. The minor deviation from experimental results can be attributed to similar reasons as discussed above.

3.3 Effects of the beam tilting angle θ on asymmetric adhesion

We next investigate the effects of beam tilting angle θ on adhesion asymmetry while maintaining constant beam thickness $b\cos(\theta)$ (group 1 listed in Supplementary Table 1). We pull the samples in two opposite directions (D1 and D2, as illustrated in Fig. 3a). With the pulling direction D1, tilted beams undergo buckling followed by stretching upon shear loading and simultaneously exhibit crack trapping behaviors (Fig. S3 and Movie S3). Conversely, with the pulling direction D2, tilted beams immediately get stretched upon shear loading (Fig. 2b and Movie S2). Consequently, MSAs exhibit greater stiffness for the pulling direction D2 compared to D1 but are softer than solid samples (Fig. 3b). With the increase of θ, the asymmetry in force-displacement curves for D1 and D2 pulling directions becomes more pronounced. In the experiments, the crack always propagates unidirectionally following the predefined path.

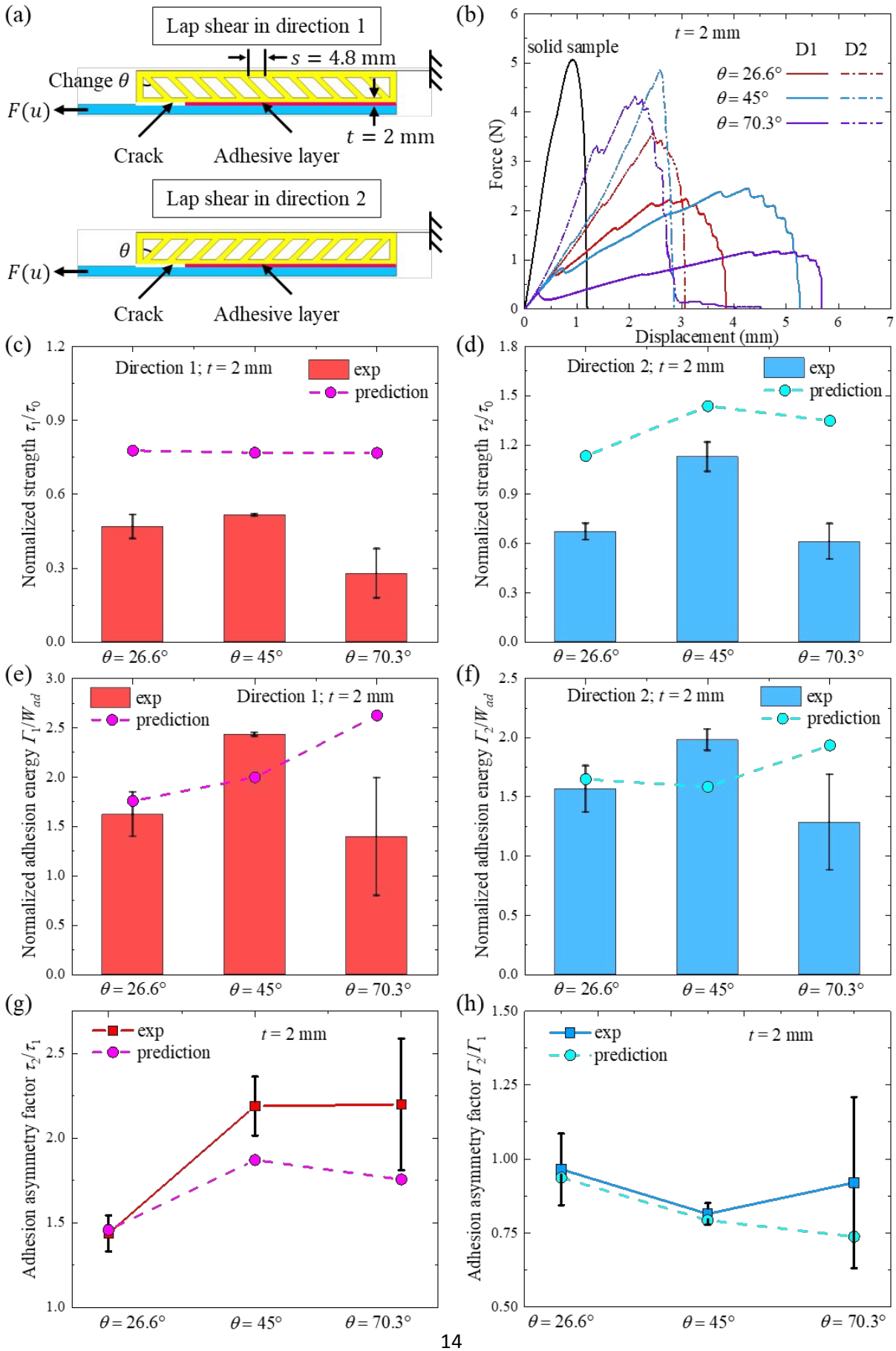

(a)
Lap shear in direction 1
s = 4.8 mm
Change θ
$F(u)$
t = 2 mm
Crack
Adhesive layer
Lap shear in direction 2
θ
$F(u)$
Crack
Adhesive layer
(b)
solid sample
t = 2 mm
D1
D2
θ = 26.6°
θ = 45°
θ = 70.3°
Force (N)
Displacement (mm)
(c)
Direction 1; t = 2 mm
exp
prediction
Normalized strength τ_1/τ_0
θ = 26.6°
θ = 45°
θ = 70.3°
(d)
Direction 2; t = 2 mm
exp
prediction
Normalized strength τ_2/τ_0
θ = 26.6°
θ = 45°
θ = 70.3°
(e)
exp
prediction
Direction 1; t = 2 mm
Normalized adhesion energy Γ_1/W_{ad}
θ = 26.6°
θ = 45°
θ = 70.3°
(f)
Direction 2; t = 2 mm
exp
prediction
Normalized adhesion energy Γ_2/W_{ad}
θ = 26.6°
θ = 45°
θ = 70.3°
(g)
exp
prediction
t = 2 mm
Adhesion asymmetry factor τ_2/τ_1
θ = 26.6°
θ = 45°
θ = 70.3°
(h)
exp
prediction
t = 2 mm
Adhesion asymmetry factor Γ_2/Γ_1
θ = 26.6°
θ = 45°
θ = 70.3°

Fig. 3. Effects of the beam tilting angle (θ) on asymmetric adhesion properties of MSAs with slender beams and a thick terminated film when the crack propagates unidirectionally along the predefined path. (a) Schematics showing the lap shear tests of MSAs with labeled geometric parameters for two opposite pulling directions (D1 and D2). (b) Effects of the beam tilting angle θ on asymmetric force-displacement curves for two opposite pulling directions compared to the solid sample. Effects of the beam tilting angle θ on the normalized shear strength (c) τ_1/τ_0 and (d) τ_2/τ_0 from experiments and theoretical predictions, respectively. Effects of the beam tilting angle θ on the normalized effective adhesion energy (e) Γ_1/W_{ad} and (f) Γ_2/W_{ad} from experiments and theoretical predictions, respectively. Effects of the beam tilting angle θ on the adhesion asymmetry factors (g) τ_2/τ_1 and (h) Γ_2/Γ_1 from experiments and theoretical predictions, respectively.

For the normalized shear strength τ_i/τ_0 (i=1 or 2), our results show that τ_1/τ_0 first remains nearly constant slightly increasing from $\sim$0.47 at $\theta = 26.6°$ to $\sim$0.51 at $\theta = 45°$, and finally decreases significantly to $\sim$0.28 at $\theta = 70.3°$ (Fig. 3c). Meanwhile, τ_2/τ_0 first increases from $\sim$0.67 at $\theta = 26.6°$ to $\sim$1.1 at $\theta = 45°$, and then significantly decreases to $\sim$0.61 at $\theta = 70.3°$ (Fig. 3d). Our numerical predictions generally agree with experimental trends but are obviously larger (colored circles in Fig. 3c and d).

For the normalized effective adhesion energy Γ_i/W_{ad} (i=1 or 2), our results show that Γ_1/W_{ad} first significantly increases from $\sim$1.6 at $\theta = 26.6°$ to $\sim$2.4 at $\theta = 45°$, and then significantly decreases to $\sim$1.4 at $\theta = 70.3°$ (Fig. 3e); Γ_2/W_{ad} first increases from $\sim$1.6 at $\theta = 26.6°$ to $\sim$2.0 at $\theta = 45°$, and then decreases to $\sim$1.3 at $\theta = 70.3°$ (Fig. 3f). Our theoretical predictions generally agree with experimental results, with the exception for $\theta = 70.3°$ (colored circles in Fig. 3e and f).

Lastly, we define the adhesion asymmetry factors for strength (τ_2/τ_1) and effective adhesion energy (Γ_2/Γ_1), respectively. τ_2/τ_1 first significantly increases from $\sim$1.4 at $\theta = 26.6°$ to $\sim$2.2 at $\theta = 45°$, and then stays almost constant at $\sim$2.2 at $\theta = 70.3°$ (Fig. 3g). Meanwhile, Γ_2/Γ_1 first slightly decreases from $\sim$0.96 at $\theta = 26.6°$ to $\sim$0.81 at $\theta = 45°$, and then slightly increases to $\sim$0.92 at $\theta = 70.3°$ (Fig. 3h). Our numerical predictions mostly agree with our experimental findings, as indicated by the colored circles in Fig. 3g and h.

3.4 Effects of the terminated film thickness *t* on adhesion properties

We next conduct a parametric study examining the influence of terminated film thickness (t) on adhesion properties. We design the second group of MSAs with identical stubby beams but varied film

thickness t (see Fig. 4a and Supplementary Table 1) and test all the samples using identical experimental conditions. Our experimental results show that while the thickness t has minimal impact on the initial section of force-displacement curves, it significantly affects the later portion (Fig. 4b). Such behavior stems from the dominance of tilted beams in carrying loads during elastic deformation, whereas the terminated film governs the energy release rate (G_L) transferred to the crack tip during crack propagation, thus affecting the rupturing point[13, 34-36]. Notably, when the terminated film thickness is decreased from $t = 2$ mm to $t = 0.75$ mm, the later section of force-displacement curves varies appreciably. However, further decreasing the thickness to $t = 0.5$ mm leads to a dramatic increase in the maximum shear force, accompanied by a pronounced dispersion of experimental measurements (shown in the next section; Fig. 5c).

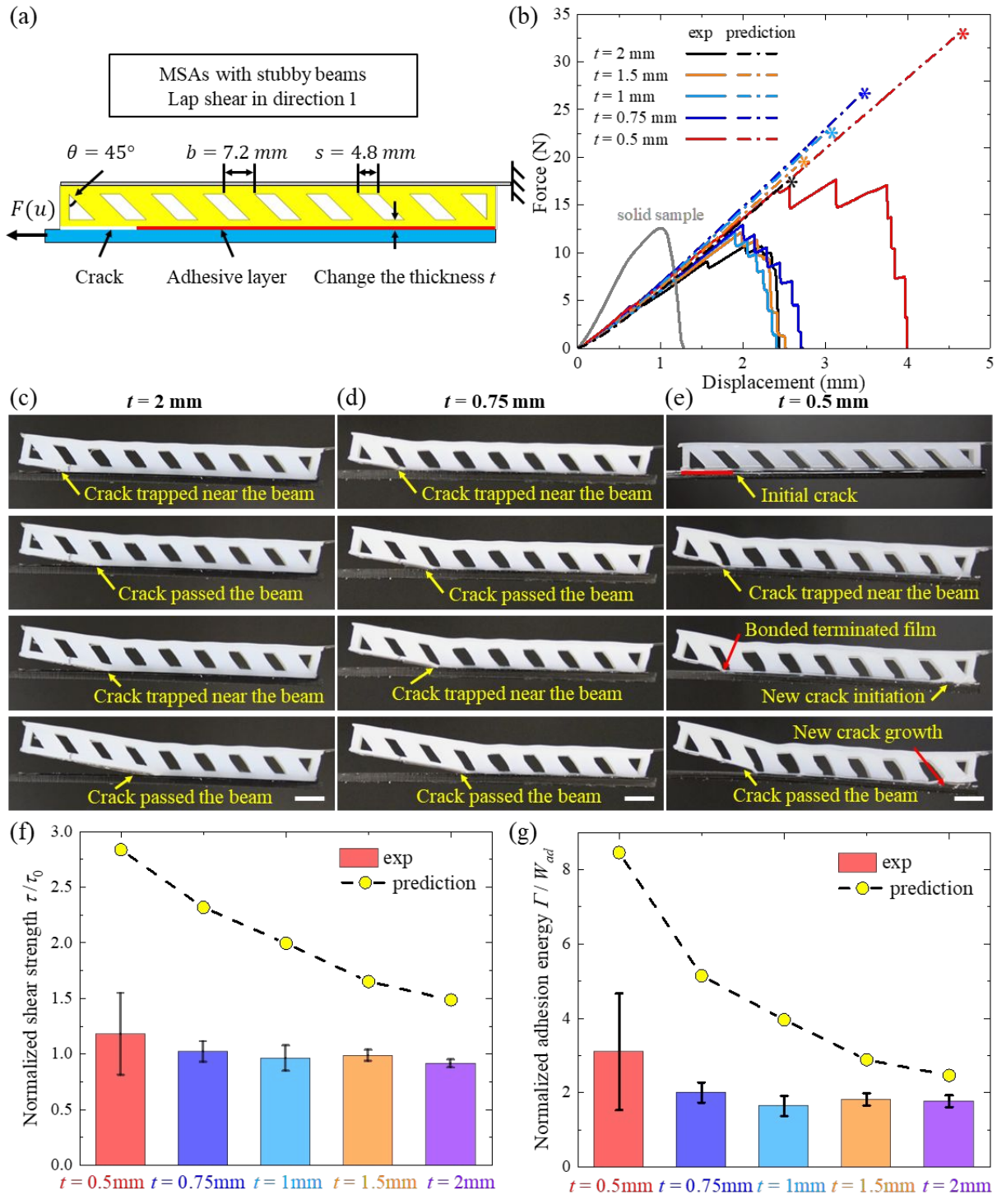


Figure 4. Effects of the terminated film thickness (*t*) on crack propagation dynamics and adhesion properties of MSAs with stubby beams from both experimental measurements and theoretical predictions. (a) Schematic showing the lap shear test and geometric parameters of MSAs with identical stubby beams but varied terminated film thickness (*t*). (b) Effects of the terminated film thickness *t* on the

force-displacement curves of MSAs compared to the solid sample. Representative images showing crack propagation dynamics of MSAs with a terminated film thickness of (c) $t = 2$ mm, (d) $t = 0.75$ mm, and (e) $0.5 = 2$ mm, respectively. All scale bars are 1cm. Effects of the terminated film thickness t on (f) the normalized shear strength τ/τ_0 and (g) the normalized adhesion energy Γ/W_{ad} of MSAs, respectively.

Fig. 4c-e illustrates crack propagation dynamics of the MSAs with varied terminated film thickness. For a thick terminated film ($t = 2$ mm), the crack propagates unidirectionally following the predefined path, exhibiting evident crack trapping behaviors (Fig. 4c). Conversely, for a thin terminated film ($t = 0.5$ mm), we usually observe new crack initiations with a finite distance from the initial crack tip. Despite the presence of crack trapping behaviors, the crack propagation deviates from the predefined path (Fig. 4e). For an intermediate terminated film thickness ($t = 0.75$ mm), the crack consistently propagates along the predefined path, displaying clear crack trapping behaviors (Fig. 4d). While random new crack initiations may still occur, they are not discernible in our recorded videos. See Movie S4 for details.

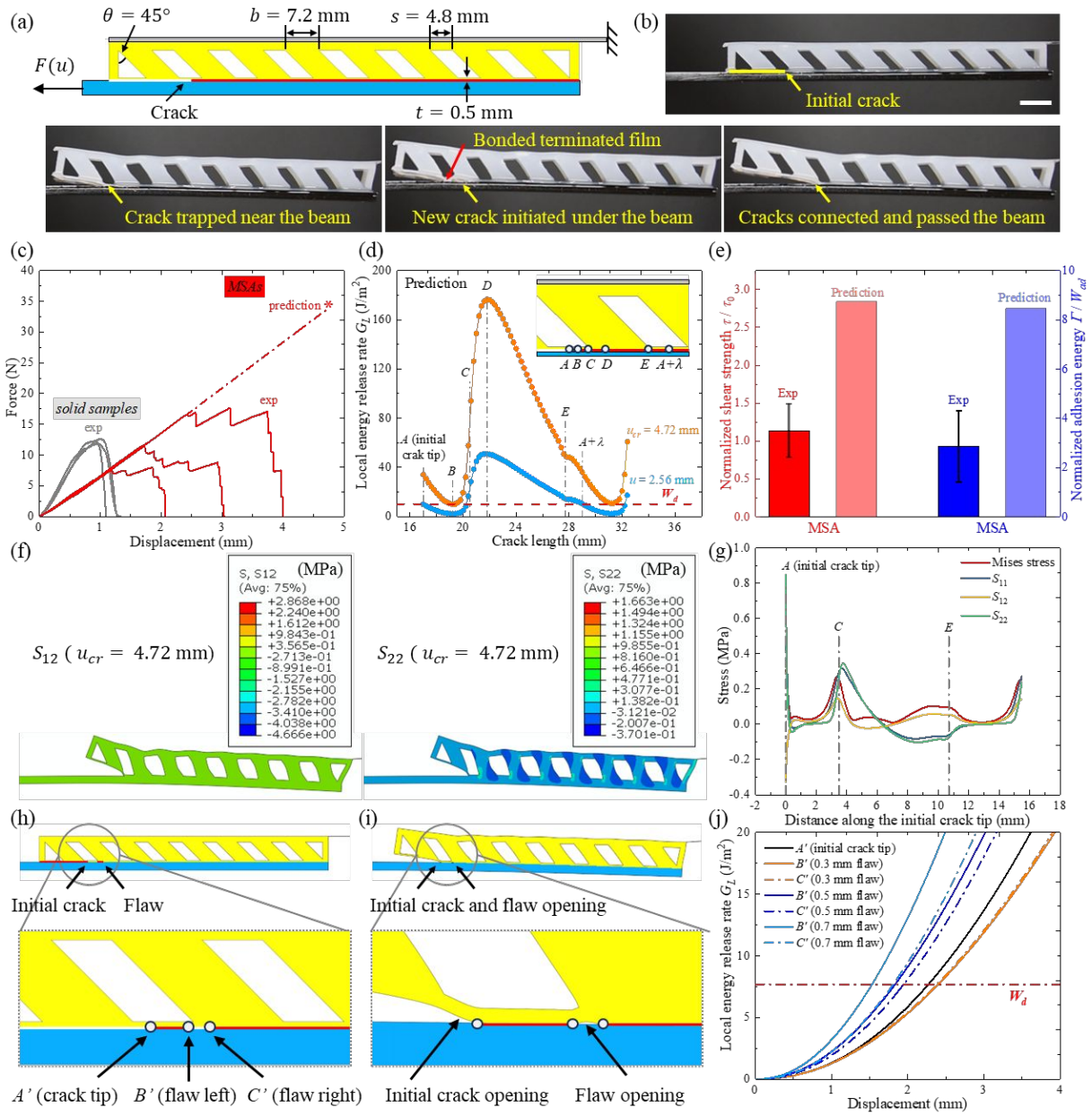
Consequently, as shown in Fig. 4f, the normalized shear strength τ/τ_0 slightly increases with the decrease of t, ranging from $\sim 0.91 \pm 0.04$ at $t = 2$ mm to $\sim 1.18 \pm 0.37$ at $t = 0.5$ mm. Notably, for a thin terminated film ($t = 0.5$ mm), τ/τ_0 scatters greatly due to the randomly initiated new cracks. As shown in Fig. 4g, the normalized adhesion energy Γ/W_{ad} generally demonstrates a nonmonotonic increase with the decrease of t, ranging from $\sim 1.77 \pm 0.16$ for $t = 2$ mm to $\sim 3.1 \pm 1.57$ for $t = 0.5$ mm. Similarly, for a thin terminated film ($t = 0.5$ mm), Γ/W_{ad} scatters greatly due to the randomly initiated new cracks.

For a relatively large thickness ($t = 2$ mm), the crack propagation follows the predefined path, and τ/τ_0 and Γ/W_{ad} are close to the theoretical predictions based on the crack trapping mechanism (yellow circles in Fig. 4f and g). In contrast, for a relatively small thickness ($t = 0.5$ mm), the propagation of the initial crack coexists with noticeable random new crack initiations, and τ/τ_0 and Γ/W_{ad} are significantly smaller than the theoretical predictions (yellow circles in Fig. 4f and g). For the intermediate thickness ranging from $t = 1.5$ mm to $t = 0.75$ mm, the theoretically predicted τ/τ_0 and Γ/W_{ad} (Fig. 4f and g) deviate more and more from experimental results. This deviation coincides with a gradual transition between the two distinct crack propagation modes as mentioned above (Movie S4). Clear experimental observation of this transition is challenging, attributed to sample opacity and the difficulty in discerning micro-scale crack initiations.

Similarly, for the third group of MSAs with identical slender beams (Supplementary Table 1), with the decrease of terminated film thickness (t), the experimental results of adhesion properties deviate more and more significantly from theoretical predictions (Supplementary Text 1 and Fig. S4).

3.5 New crack initiation reduces the enhancement of adhesion toughening

As discussed above, new crack initiation may be responsible for the difference between experiment results and theoretical predictions. While similar phenomena have been observed in the hollow structural adhesives with symmetric beams[13, 34-36], they have not been carefully studied. Herein, we systematically investigate the influence of new crack initiations on adhesion toughening, using MSAs featuring stubby beams and a thin terminating film as an example ("$t = 0.5$ mm" cases in the second group of Supplementary Table 1; Fig. 5a). In experiments, the stochastic nature of new crack initiation results in varied crack propagation dynamics among different samples, and thus, we present another representative case in Fig. 5b and Movie S5, as a comparison with the results shown in Fig. 4e and Movie S4.



395

396 **Fig. 5. New crack initiations along the interface lead to the discrepancy between experimental**
397 **measurements and theoretical predictions for MSAs with a relatively thin terminated film.** (a)
398 Schematic showing the lap shear test and geometric parameters of the MSA. (b) Representative images
399 showing crack propagation dynamics, including new crack initiating alongside the propagation of the initial
400 crack. Scale bar, 1cm. (c) Experimental and numerically predicted force-displacement curves of MSAs
401 compared to solid samples. (d) Numerically predicted variation of energy release rate G_L versus crack length,
402 with the red dash line representing W_{ad}. Various positions along the interface are marked in the top right
403 insert and on the curves. (e) Comparison between experimental and numerically predicted τ/τ_0 (left) and $\Gamma/$
404 W_{ad} (right), respectively. (f) Numerical calculations of the stress field of the MSA at the critical

displacement of $u_{cr} = 4.72$ mm. Left: S_{12} (unit: MPa). Right: S_{22} (unit: MPa). (g) Stress distribution along the interface near the initial crack. Marked positions are the same as those in (d). (h) Schematic showing the artificially introduced flaw (e.g., 0.7 mm) underneath the beam. (i) Deformed state of the initial crack and flaw at a displacement of $u = 1.6$ mm. (j) Effects of the flaw size on the relationship between the energy release rate G_L and the applied displacement u at different positions. Marked positions are the same as those in (h).

In experiments, we find significant scattering in the force-displacement curves of MSAs (Fig. 5c), and consequently significantly dispersed values of τ/τ_0 (Fig. 5e, left) and Γ/W_{ad} (Fig. 5e, right), both of which are much smaller than the theoretically predicted values. Meanwhile, our simulations show that the energy release rate G_L changes more rapidly with the crack length (Fig. 5d) compared to that in Fig. 2f.

To investigate the possibility of new crack initiation, we first examine the stress field on the interface between the MSA and PMMA plate (Fig. 5f). We observe pronounced stress concentration near the left and right edges of the beam (marks *C* and *E* in the insert of Fig. 5d) by plotting the stress distribution against the distance from the initial crack tip along the interface (Fig. 5g), which is likely the cause of new crack initiation.

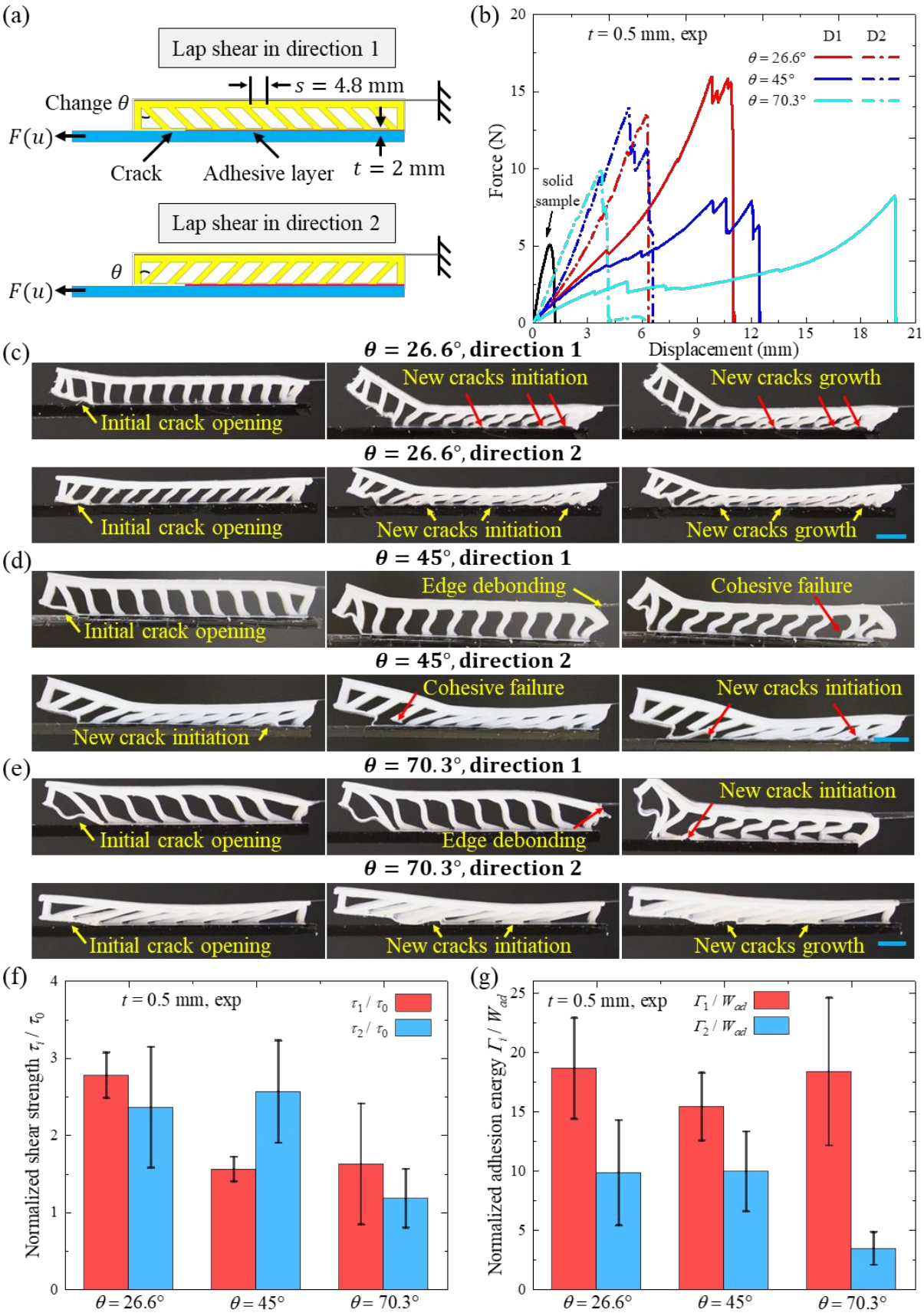
To quantitatively assess the impacts of inevitable flaws on the interface, we introduce a flaw along the interface beneath the left side of the beam (Fig. 5h). We repeat the simulation and compute the energy release rate at the initial crack tip (*A'*), on the left of the flaw (*B'*), and right of the flaw (*C'*), respectively (Fig. 5h). Fig. 5i shows the deformation near the initial crack and the flaw (0.7 mm) with an applied displacement of $u = 1.6$ mm. As shown in Fig. 5j, for a relatively small flaw (0.3 mm), the energy release rate G_L at the tips of the flaw is smaller than that at the initial crack tip. However, for a larger flaw size (0.5 mm or 0.7 mm), G_L at the tips of the flaw exceeds that at the initial crack tip, enabling new crack propagation before the propagation of the initial crack and thus decreasing the measured adhesion energy. As the flaw size increases, the critical displacement u_{cr}, where $G_L = W_{ad}$ is satisfied at the flaw tips, decreases.

Though our simulations have suggested the possibility of new crack initiation, our objective in the current study does not involve the theoretical prediction of adhesion toughening for those scenarios where new cracks initiate during the propagation of the initial crack, which can be extremely challenging.

3.6 Maximizing the adhesion toughening using MSAs with a thin terminated film

In this section, we experimentally explore the possibility of maximizing the adhesion toughening using MSAs with slender beams and a thin terminated film ($t = 0.5$ mm) (group 4 listed in Supplementary

436 Table 1; Fig. 6a). We vary the beam tilting angle θ while maintaining constant beam thickness $b\cos(\theta)$,
437 and perform lap shear tests in two opposite pulling directions, respectively.


(a)
Lap shear in direction 1
Change θ
s = 4.8 mm
F(u)
Crack
Adhesive layer
t = 2 mm
Lap shear in direction 2
θ
F(u)
(b)
t = 0.5 mm, exp
D1 D2
θ = 26.6°
θ = 45°
θ = 70.3°
solid sample
Force (N)
Displacement (mm)
(c)
θ = 26.6°, direction 1
Initial crack opening
New cracks initiation
New cracks growth
θ = 26.6°, direction 2
Initial crack opening
New cracks initiation
New cracks growth
(d)
θ = 45°, direction 1
Initial crack opening
Edge debonding
Cohesive failure
θ = 45°, direction 2
New crack initiation
Cohesive failure
New cracks initiation
(e)
θ = 70.3°, direction 1
Initial crack opening
Edge debonding
New crack initiation
θ = 70.3°, direction 2
Initial crack opening
New cracks initiation
New cracks growth
(f)
t = 0.5 mm, exp
τ1 / τ0
τ2 / τ0
Normalized shear strength τi / τ0
θ = 26.6°
θ = 45°
θ = 70.3°
(g)
t = 0.5 mm, exp
Γ1 / Wadi
Γ2 / Wadi
Normalized adhesion energy Γi / Wadi
θ = 26.6°
θ = 45°
θ = 70.3°

438

Fig. 6. Optimization of adhesion toughening by varying the beam tilting angle (θ) of MSAs with a thin terminated film and slender beams. (a) Schematics showing the lap shear tests and geometric parameters of MSAs with two opposite pulling directions. (b) Effects of the beam tilting angle θ on asymmetric force-displacement curves of MSAs for two opposite pulling directions. Representative images showing crack propagation dynamics for two opposite pulling directions with the beam tilting angle of (c) $\theta = 26.6°$, (d) $\theta = 45°$, and (e) $\theta = 70.3°$, respectively. All scale bars are 1 cm. (f) Effects of the beam tilting angle θ on τ_1/τ_0 and τ_2/τ_0, respectively. (g) Effects of the beam tilting angle θ on Γ_1/W_{ad} and Γ_2/W_{ad}, respectively.

Our experimental results show increased asymmetry in force-displacement curves for the two opposite pulling directions with the increase of θ (Fig. 6b). We present representative images and movies illustrating crack propagation dynamics for different designs of MSAs (Fig. 6c-e). At $\theta = 26.6°$, new crack initiations occur along the interface during the propagation of the initial crack for both pulling directions (Fig. 6c and Movie S6). At $\theta = 45°$, both edge debonding from the PET film and cohesive failure within the hollow backing occur during the propagation of the initial crack for the D1 pulling direction; for the D2 pulling direction, cohesive failure and new crack initiations occur along the interface during the propagation of the initial crack (Fig. 6d and Movie S7). At $\theta = 70.3°$, both edge debonding from PET film and new crack initiations occur during the propagation of the initial crack for the D1 pulling direction; for the D2 pulling direction, new cracks initiate during the propagation of the initial crack (Fig. 6e and Movie S8).

Consequently, τ_1/τ_0 first decreases significantly from ~2.8 at $\theta = 26.6°$ to ~1.6 at $\theta = 45°$, and then remains nearly constant at ~1.6 at $\theta = 70.3°$; but τ_2/τ_0 first remains almost unchanged from ~2.4 at $\theta = 26.6°$ to ~2.6 at $\theta = 45°$, and then decreases to ~1.2 at $\theta = 70.3°$ (Fig. 6f). Similarly, Γ_1/W_{ad} first decreases from ~18.6 at $\theta = 26.6°$ to ~15.4 at $\theta = 45°$, and then increases to ~18.4 at $\theta = 70.3°$; Γ_2/W_{ad} first remains almost constant from ~9.8 at $\theta = 26.6°$ to ~10.0 at $\theta = 45°$, and then decreases to ~3.5 at $\theta = 70.3°$ (Fig. 6g). Finally, the adhesion asymmetry factor τ_2/τ_1 significantly increases from ~0.85 at $\theta = 26.6°$ to ~1.6 at $\theta = 45°$, and then decreases to ~0.73 at $\theta = 70.3°$ (Fig. S5a). Similarly, Γ_2/Γ_1 slightly increases from ~0.53 at $\theta = 26.6°$ to ~0.65 at $\theta = 45°$, and then significantly decreases to ~0.19 at $\theta = 70.3°$ (Fig. S5b).

4. Discussion

In the following, we discuss several critical points that require further in-depth investigations.

Our theoretical predictions of adhesion toughening, based on the crack trapping mechanism[11, 13, 34-36], agree well with experimental results when the crack propagates unidirectionally following a predefined path for a relatively thick terminated film. However, with the decrease of the terminated film thickness, the measured adhesion energy of MSAs deviates significantly from theoretical predictions, which is attributed to new crack initiations based on experimental observations and numerical simulations. However, the transition between the two distinct crack propagation modes remains unclear and may indicate the involvement of the fracto-adhesive length scale, which characterizes the thickness-dependent adhesion properties, as systematically investigated in a previous study on lap shear of soft hydrogels[39]. Note that currently, the length scales governing the fracture and adhesion of discrete metamaterials are yet explored [9, 12, 40, 41], which calls for more comprehensive theoretical and experimental investigations.

Recently, stretchable and low-hysteresis composites comprising hard and soft phases have been developed to enhance both the fracture toughness and fatigue resistance[33, 42, 43]. While stress deconcentration mechanism has been widely used to elucidate the toughening effects, the periodically varied relationship between the energy release rate versus crack length based on the crack trapping mechanism provides an alternative way to predict the fracture and fatigue enhancement.

In this study, lap shear tests were conducted with no normal force applied to MSAs. We want to point out that lap shear tests under displacement control (using two rigid fixtures) is rare in practical applications but prevalent in lab tests[39, 44-46], which can lead to significant artifacts for thick structural adhesives (Fig. S6a and b). For both solid samples and MSAs, the maximum shear force is much higher in displacement-control mode than in zero normal force-control mode when the displacement along the thickness direction is fixed (Fig. S6c and d). Consequently, solid samples exhibit appreciable increases in shear strength and adhesion energy in displacement-control mode (Fig. S6e and f). For MSAs, both shear strength and effective adhesion energy show significant increases in displacement-control testing mode (Fig. S6e and f). The reason is as follows: with displacement-control mode, the stress normal to the applied shear force increase significantly for MSAs due to beam bending, compared to solid samples. This significantly increased the friction between MSAs and PMMA substrate, resulting in mixed-mode fracture. These findings highlight the importance of carefully selecting the lap shear conditions for testing thick structural adhesives[44].

Finally, we envision that there are ample opportunities for the further exploration of MSAs. For example, stimuli-responsive materials can be used to fabricate either the thick backing or the adhesive layer for stimuli-responsive MSAs targeted for responsive and switchable applications[5]. Besides, designing the backing structures of MSAs to be better conformal to rough or curved surfaces may enable strong and reversible adhesion, addressing the well-known challenge for conventional pressure sensitive adhesives[47,

[48]. Furthermore, exploring MSAs for achieving strong and reversible adhesion in wet and underwater conditions is also important for biomedical applications and ocean explorations[49, 50].

5. Conclusions

In summary, we have achieved adhesion toughening and asymmetry in the lap shear of MSAs using asymmetric and thick hollow backings. By combining theoretical, numerical and experimental investigations, we identity the crack trapping as one toughening mechanism, which leads to unstable crack propagation in practical monotonic loadings and thus dissipates more energy. For MSAs with a relatively thick terminated film, the experimental results agree well with theoretical predictions based on the crack trapping mechanism when the crack propagates unidirectionally along the predefined path. However, for MSAs with a relatively thin terminated film, the experimental results deviate significantly from theoretical predictions based on the crack trapping mechanism. We attribute such discrepancy to new crack initiations, which are observed experimentally and elaborated through numerical simulations. Additionally, we explore the adhesion asymmetry by varying the beam tilting angle (θ). Notably, for MSAs with $t = 0.5$ mm and $\theta = 26.6^{\circ}$, we achieve a maximum effective adhesion energy being ~18.6 times that of solid samples. For MSAs with $t = 0.5$ mm and $\theta = 70.3^{\circ}$, we achieve a maximum adhesion energy asymmetry factor of Γ_1/Γ_2~5.3. Our study provides useful insights for designing metamaterial structural adhesives for engineering applications in robotic grippers, wall-climbing robotics, and wearable devices that require reversible and switchable adhesion.

Author contributions: C.L. and S.C. conceived the study and designed the overall experiments. Q.G. provided suggestions on the interpretation of experimental results and numerical simulations. R.C. helped with 3D-printing the molds. C.L. and S.C. wrote the manuscript with input from all authors. All authors read and approved the final article.

Conflicts of interest: The authors declare they have no competing interests.

Data availability

The authors confirm that the data supporting the findings of this study are available within the article and its ESI.

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Data availability

The authors confirm that the data supporting the findings of this study are available within the article and its ESI.

Best regards,

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