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1 Bulk Solvent Extraction of Biomass Slurries Using a Lipid Trap

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3 Nathan G. Schoepp^{1,2}, Wilson Wong¹, Stephen P. Mayfield^{2,3}, Michael D. Burkart^{1,2*}

4
5 ¹Department of Chemistry & Biochemistry, University of California San Diego, 9500 Gilman
6 Drive, Pacific Hall 6100D, La Jolla, CA 92093, United States

7 ²The California Center for Algae Biotechnology, University of California San Diego, 9500
8 Gilman Drive MC 0368, La Jolla, CA 92093, United States

9 ³Division of Biological Sciences, University of California San Diego, 9500 Gilman Drive,
10 Bonner Hall 2150C, La Jolla, CA 92093, United States

11
12 *Corresponding author Michael D. Burkart. E-mail: mburkart@ucsd.edu. Phone: 858-534-5673.
13 Address: University of California, San Diego, 9500 Gilman Drive, Pacific Hall 6100D, La Jolla,
14 CA 92093.

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18
19 Author emails:

20 NGS: nschoepp@pacbell.net

21 WW: wwong1035@gmail.com

22 SPM: smayfield@ucsd.edu

23 MDB: mburkart@ucsd.edu

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25

26 Abstract

27

28

29 Extraction of lipids and hydrophobic metabolites from microbial sources remains an
30 obstacle in the production of these compounds at the laboratory and industrial scale. Analytical
31 techniques for the total extraction of non-polar metabolites from biological material are well
32 established, but rely on expensive and time consuming processes. This makes these techniques
33 unsuitable for direct translation to continuous or large volume systems, unable to move beyond
34 proof-of-concept studies, and leaves a major gap in the translation of new bio-products requiring
35 a purified extract. Here we attempt to bridge that gap by demonstrating the use of a semi-
36 continuous liquid-liquid extraction system capable of bulk lipid extraction from wet, untreated
37 biomass, and simultaneous concentration of the unmodified extract in a lipid trap. A 1.8 L model
38 was used to evaluate system dynamics with bacterial, fungal, algal, and plant feedstock, prior to
39 scaling the system by an order of magnitude to demonstrate large-scale viability. Extraction
40 efficiency was above 90% for each feedstock compared to standard Bligh and Dyer extraction.
41 Following scale-up, extraction was performed on upwards of 4 kg of slurry (660 g dry weight),
42 yielding an average efficiency of 96%, and allowing generation of a crude extract at a scale not
43 previously possible in a laboratory setting. The resulting system allows for direct and high-
44 throughput extraction of biomass sources without pretreatment, specialized instrumentation, or
45 intensive user input.

46

47 Introduction

48
49 Intensive efforts in biotechnology have yielded organisms capable of producing a vast
50 array of lipid-derived bio-products, whose major end-uses include plastics ¹, surfactants ², fuel
51 replacements ^{3,4}, and pigments ⁵. As the microbial and plant product profile has grown, so has
52 the desire to investigate industrial production potential. In many cases, such as production of
53 pharmacologically-active natural products like phytosterols ⁶, feeding studies with microbial-
54 derived essential fatty acids ⁷, or the much-discussed general displacement of petrochemicals ⁸,
55 extraction must be performed at a scale larger than analytical techniques are capable of, in order
56 to generate sufficient material for downstream testing. This extraction step remains an obstacle
57 limiting many studies to the laboratory scale, and is insufficient for successful translation of
58 biotechnologies using microbial or plant derived lipid. The system described here overcomes the
59 obstacle of bulk extraction, and enables process testing (i.e. bulk lipid isolation, characterization,
60 and functionalization) at a scale informative of, and relevant to industrial production.

61 Lipid is an ambiguous term often used to describe biological fats and oils, but more
62 broadly encompassing an array of hydrophobic metabolites including sterols, long chain
63 alcohols, terpenes, essential oils, pigments, and carotenoids, among others ^{9,10}. Current analytical
64 techniques for solvent-based extraction of lipids and hydrophobic compounds from biomass
65 typically rely on a mixture of a non-polar organic solvent and an alcohol. The widely used
66 method of Bligh and Dyer ¹¹ remains the standard for analytical-scale total lipid extraction from
67 a wide variety of biomass sources, due to its simplicity, effectiveness, and widespread adoption.
68 Other solvent-based lipid extraction techniques utilize variations on a similar theme, such as
69 ethanol/hexane and isopropanol/hexane extractions ^{12,13}. The fundamental difficulty in total lipid
70 extraction is the effective removal of generally hydrophobic compounds with a broad range of
71 polarities into a single phase. In the case of solvent-based extraction techniques, including the
72 method of Bligh and Dyer, this separation is accomplished using centrifugation, an energy
73 intensive, batch-wise, and time-consuming technique. As with most processes, direct scale-up is
74 not feasible. Even when energy input is not an issue, centrifugation can still be prohibitive due to
75 the lack of large instruments, the cost of continuous flow centrifuges for handling large volumes,
76 and the difficulty of working with two phases in such instruments. In addition to challenges
77 involving separation, the lipid constituent of a cell is often bound in an overall hydrophilic
78 matrix of proteins, carbohydrates, and other cellular components, making single-pass total
79 extraction with a non-polar organic solvent difficult since the solvent cannot access the shielded
80 lipids ¹⁴.

81 Alternative extraction methods have been investigated in attempts to improve process
82 efficiency, such as supercritical CO₂ ¹⁴, soxhlet ¹⁵, and accelerated solvent extraction ¹⁶, but like
83 traditional solvent extraction, these systems can be difficult to scale up. Mechanical expression
84 of oil is a common and high-throughput technique, but is inefficient when oil content is low
85 (<20%), or water content high, as is typically the case with microbial feedstock. Methods for
86 direct conversion of biomass to hydrocarbons or biofuels have also been developed, such as
87 thermal treatment ¹⁷ and direct transesterification ¹⁸, but do not preserve the crude extract.
88 Critical drying and grinding steps comprise another major challenge for soxhlet extraction,
89 supercritical CO₂ extraction, thermal treatment, and mechanical pressing. These issues alone can
90 rule out the use of these techniques when volumes exceed workable quantities. Despite this
91 variety of techniques for analytical-scale extraction, few technologies have been scaled up due to
92 challenges associated with process enlargement (Table 1). Industrial processes for the production

93 of edible oils from select plant feedstock (i.e. soybean) exist¹⁹, as well as a variety of
94 technologies for large-scale extraction of aromatic and medicinal compounds from plant
95 material, including percolation, counter-current extraction, and distillation techniques²⁰.
96 However, these techniques also require a dry feedstock and in the latter case are less selective in
97 the compounds they extract than techniques aimed specifically at the lipid fraction, making them
98 impractical for use with aqueous slurries.

99 The ideal biomass extraction system must be able to handle a wet feedstock, be amenable
100 to process enlargement and automation, require minimal pretreatment of the biomass, and
101 produce a crude extract that has not been significantly affected by the extraction process.
102 Continuous solvent extraction can meet all of these requirements. Devices for continuous liquid-
103 liquid extraction have been constructed previously for a variety of purposes^{21,22}, as well as
104 automated²³, demonstrating feasible continuous operation. Recent studies have also focused on
105 optimizing solvent choice and efficiency^{24,25}, but a scalable system has yet to be developed. We
106 have designed a straightforward, scalable, semi-continuous liquid-liquid extraction system, and
107 demonstrated its effectiveness in generating an unmodified crude hydrophobic extract from a
108 range of biomass slurries with no pretreatment, with the hope that this system will serve as a unit
109 for processing a variety of natural metabolites regardless of the host organism. The described
110 system utilizes readily available materials, equipment, and solvents, and can be scaled by orders
111 of magnitude without changing the fundamentals or efficacy of the system.

113 Experimental methods

114 Biomass sources

115 The bacteria *Rhodococcus opacus* PD630 (*Ro*) was obtained courtesy of the Greenspan
116 lab, University of California, San Diego, and cultured in 2 L flasks in LB media on a rotary
117 shaker at 100 rpm at 30 °C. Conventional baker's yeast, *Saccharomyces cerevisiae* (*Sc*) was
118 purchased dry from Red Star® and re-suspended in water. The yeast *Rhodosporidium toruloides*
119 (*Rt*) was obtained from the Agricultural Research Service (NRRL) culture collection and
120 cultured in 2 L flasks of YPD media on a rotary shaker at 100 rpm at 30 °C. Cultures of *Ro* and
121 *Rt* grown in the laboratory were harvested via centrifugation. The microalgae *Scenedesmus*
122 *dimorphus* UTEX 1237 (*Sd*) was obtained from the University of Texas at Austin culture
123 collection and cultivated as described previously in outdoor ponds²⁶. Biomass was harvested via
124 settling and continuous flow centrifugation. Frozen, shelled soybeans, *Glycine max* (*Gm*) were
125 purchased locally, thawed, and blended until homogenous (in order to obtain consistent dry
126 weight measurements). All slurries were stored at -20 °C.

129 Analytical methods

130 Dry weight, lipid content, and lipid trap quantifications for each extraction experiment
131 were measured gravimetrically, in quadruplicate, using an analytical balance readable to 0.1 mg.
132 Extraction experiments were performed in triplicate. All solvents were reagent grade.

133 Dry weight percentage (g solids / g slurry) for each trial was determined by drying pre-
134 weighed amounts of the slurry in aluminum dishes in an oven at 80 °C for twelve hours. Total
135 mass of the solids in each extraction was determined by weighing the beaker containing the

138 slurry before and after addition to the extraction vessel, and multiplying by the solids percentage
139 obtained via dry weight measurements.

140 Total lipid content of the slurry was determined by the method of Bligh and Dyer ¹¹.
141 Total lipid content of the extract obtained using the lipid trap system was determined by
142 evaporating the organic solvent from pre-weighed amounts of the crude extract in a bead bath at
143 80 °C. Total mass of the lipid extracted was determined by weighing the round-bottom flask
144 containing the extract before and after removal of the extract, and multiplying by the lipid
145 percentage obtained from dried sample measurements.

146 Thin layer chromatography (TLC) was performed using glass-backed silica gel 60 plates
147 to visualize the lipid profile of the Bligh and Dyer and lipid trap extracts. 70:30:1 hexane -
148 diethyl ether - acetic acid by volume was used as the solvent system ¹⁰. Plates were visualized by
149 immersion in a solution of 10% (w/v) CuSO₄, 4% (v/v) H₂SO₄, 4% (v/v) H₃PO₄ in MeOH
150 followed by charring at 160 °C. Gas chromatography mass spectrometry (GC/MS) was run on an
151 Agilent 7890A GC system connected to a 5975C VL MSD quadrupole MS (EI) following
152 transesterification of the lipids to their methyl esters ²⁷. For transesterification, crude extracts
153 were dissolved in 1 M HCl in methanol, incubated at 60 °C for 1 hour, then extracted twice with
154 hexane. Samples were separated on a 60 m DB23 Agilent GCMS column using helium as carrier
155 gas and a gradient of 110 °C to 200 °C at 15 °C/min, followed by 20 minutes at 200 °C.

156
157 Lipid trap system

158
159 The lipid trap system used for assessment of the method consisted of a 2 L glass reagent
160 bottle used as an extraction vessel with a 1 L two-neck round-bottom flask serving as the “lipid
161 trap” (Figure 1). The reagent bottle was fitted with a male 24/40 joint at the top of the straight
162 wall, allowing connection to the round-bottom flask via a glass elbow. A Friedrich’s condenser
163 was fitted to the top of the vessel. A generic magnetic stirrer hot plate with temperature control
164 was used to heat and stir the vessel, and a heating mantle used to heat the lipid trap. A detailed
165 schematic of the system is provided (Figure S1).

166 During each extraction, the extraction vessel was charged with the biomass slurry (550
167 mL) and isopropanol (650 mL). In the case of *Rt*, the slightly acidic slurry was neutralized using
168 6 M NaOH. After stirring had begun, hexanes (550 mL) were added to the vessel along with the
169 condenser. The extraction vessel was then heated to 45 °C. If necessary, small additional
170 amounts of isopropanol were added to the extraction vessel such that the organic phase remained
171 sufficiently large to allow overflow without contamination of the aqueous emulsion phase.
172 Hexanes (700 mL) were then added to the round-bottom flask serving as the lipid trap, along
173 with boiling chips, and the flask heated to reflux at 68 °C. Temperature of the lipid trap was
174 monitored during the entirety of each run using a standard thermometer readable to 1.0 °C. Each
175 trial was run for 22 hours.

176 The scaled up 11 L system used for large extractions was identical in design, except a 13
177 L glass carboy was used as the extraction vessel, mechanically stirred using a 24 x 160 mm
178 PTFE stirrer blade, and heated using a three inch wide flexible silicone band heater. A 2 L, two-
179 neck round-bottom was used as the lipid trap. Temperature of both the extraction vessel and lipid
180 trap was monitored during the entirety of each run using a standard thermometer readable to 1.0
181 °C.

182
183 Results and Discussion

184
185 Feedstock choice, extraction efficiency, and composition
186

187 Five sources of biomass were tested in the system to demonstrate its effectiveness in
188 extracting the lipid fraction of both laboratory model and oleaginous production organisms.
189 *Rhodococcus opacus* PD630, *Rhodospiridium toruloides* and *Glycine max* were chosen as model
190 oleaginous bacterial, fungal, and plant feedstock, respectively. *Saccharomyces cerevisiae* was
191 chosen as a readily available laboratory model organism. *Scenedesmus dimorphus* was picked
192 specifically as a photosynthetic commercial-production organism, and because of its tough cell
193 wall. *Sd* is highly resistant to complete dissolution, which can create problems for certain
194 methods of extraction and digestion²⁸, but makes it an excellent test case for microalgae.

195 Despite major differences in size, cell membrane and wall composition, and total lipid
196 content, a crude lipid extract was generated for each feedstock as efficiently as standard
197 analytical techniques, but at a much larger scale. Following growth and harvesting, crude
198 extracts of *Ro*, *Sc*, *Rt*, *Sd*, and *Gm* were generated at efficiency ratios of 0.93, 2.45, 1.09, 0.97,
199 and 1.12 respectively, relative to Bligh and Dyer extraction (Figure 2). Overall, the relative
200 degree of extraction compared to Bligh and Dyer varied little across all five organisms, with the
201 exception of *Sc*. Total lipid content of *Sc* and *Gm* agreed well with values expected from
202 literature²⁹, but was slightly lower than previous reports in the case of *Ro* and *Rt*^{30,31}. Literature
203 values varied widely for *Sd*³². The large uncertainty in the measurements of *Ro* is most likely
204 due to variable losses during a filtration step that was carried out on the crude lipid trap extract.
205 This wash was performed only with the extract from *Ro* and was necessary due to the presence
206 of insoluble non-lipid material. Similarly, the increased lipid/mass ratio of *Sc* is likely due to
207 small amounts of insoluble material being extracted, since no filtration step was carried out, and
208 the starting material was fully dried. Neither *Ro* or *Sc* showed variations in the profile of the
209 extract. Lastly, it should also be noted that dry weights were determined as percent solids and
210 include any residual salts and ash from the growth medium and processing of the biomass, so
211 lipid percentages should not be taken as absolutes for each organism.

212 Timecourse experiments (Figure 2) using *Sd* and *Gm* revealed that the rate of extraction
213 in the 1.8 L system varied on the order of hours between feedstock. Timecourse experiments
214 were carried out with *Sd* and *Gm* specifically, since *Sd* contains a rigid cell wall and *Gm* has
215 exceptionally high lipid content relative to the other feedstock tested. It was assumed differences
216 in rate of extraction might be observed between the two organisms due to differences in
217 cellulosic components, cell walls, and lignin content³³. However, in both cases, the experiments
218 revealed the bulk of extraction was completed after five hours. In this time, extraction was over
219 90% and 77% complete for *Sd* and *Gm* respectively. The rate of extraction is a combination of
220 the rate of exchange of lipid from the aqueous to the organic phase and the rate of overflow
221 (same as rate of reflux of the trap) of the organic phase in the extraction vessel. The fact that
222 lipid accumulation in the organic phase of the extraction vessel was not observed with either
223 organism, but the initial rate of lipid accumulation in the trap were nearly identical indicates that
224 differences in composition had little affect on the rate of extraction, and the rate of extraction
225 was proportional to the total amount of lipid present. Steady accumulation of lipid was observed
226 in the trap, with the fatty acid profile of the extract remaining constant throughout extraction
227 (Figure S2).

228 Lipid composition of the crude extracts was compared to Bligh and Dyer extracts using
229 TLC and GC/MS. In all cases, both extracts showed identical composition (Figure 3).

230 Additionally, the fatty acid profiles highlight known and industrially relevant differences in
231 triacylglyceride and fatty acid composition between the organisms. As expected, TLC and
232 GC/MS profiling of extracts during the timecourse experiments revealed that no particular
233 component of the lipid fraction was extracted more rapidly than another (Figure S2).

234
235

236 Mechanism of extraction, feedstock flexibility, and scale-up

237

238 The most important advantage of the semi-continuous solvent extraction system
239 described here is the ability to generate an unmodified lipid extract from wet slurries, at a large
240 scale, without pretreatment or the use of expensive instrumentation. The formation of a fine,
241 stable emulsion phase at the isopropanol/water - hexane interface allows extraction and transport
242 of the lipid fraction into the separated hexane phase, where it eventually overflows and is
243 trapped. The degree of disintegration varied between the feedstock tested, and was observed via
244 microscopy (Figure S3). In the case of *Rt*, *Sd*, and *Gm* intact cells and biomass clumps were
245 visible following both Bligh and Dyer and lipid trap extraction, demonstrating that dissolution of
246 the cell wall is not requisite (Figure S3). Regardless of complete or incomplete dissolution
247 during the extraction process, all five biomass sources yielded crude extracts comparable to
248 standard methods. None of the biomass sources required pretreatment or concentration following
249 harvesting, and were used directly as obtained. Freezing was required to prevent lipid
250 degradation during storage due to the quantities of biomass used. Solids content of the various
251 feedstock used in the evaluation experiments varied from 1 – 16%. Minimum necessary water
252 content was tested using lyophilized soybean slurry, and revealed that acceptable solids content
253 of the incoming slurry can range from 1-70%, with the upper limit being set by the minimal
254 water content necessary to obtain two phases. The fact that water with very low solids content
255 functions fine in the system means the lipid fraction of dilute environmental samples with low
256 solids content could also be extracted and concentrated.

257 Following scale-up of the system, triplicate experiments were carried out with *Sd*,
258 resulting in an average efficiency of 96% compared to Bligh and Dyer extraction. Maximum
259 solids content in a single extraction was over 650 g yielding over 140 g of crude extract.

260

261 Process considerations

262

263 Ease of construction, total capacity, and amenability to scale-up were important factors in
264 design of the system. Both the small and large systems tested were constructed from readily
265 available glassware and equipment, with minimal customization, making replication
266 straightforward (Figure S1). The 1.8 L system used for evaluation can accept upwards of 50 g
267 solid material in slurry form, with the limiting factor being the ability to stir the slurry
268 magnetically. The 11 L system easily accepts many hundreds of grams, far exceeding the
269 capacity of currently available extraction systems.

270 In both systems, temperature of the extraction vessel was maintained at 45 °C over the
271 course of all extractions. Additionally, reflux was maintained in the lipid trap at 68 – 71 °C, and
272 no major increase in temperature of reflux was observed during extraction. This was expected, as
273 the overall concentration of lipid in the trap remained relatively low. If this concentration were to
274 increase due either to extraction of a more oleaginous feedstock, or an increase in total feedstock

275 mass without exchange of the lipid trap solvent, it is expected that the temperature of reflux
276 would increase.

277 We have tested the system in glass primarily for ease of construction. However, the
278 system is fundamentally two vessels with a single connection, meaning scale-up beyond volumes
279 workable with glass, as well as automation, and adaptation to a fully continuous system, would
280 be straightforward. One advantage of glass is its amenability to teaching and demonstration.

281 Solvents chosen were inexpensive and commonly available. However, a safer
282 replacement for hexane such as cyclohexane, toluene, or a terpene mixture could be used without
283 issue. Isopropanol was chosen as the transfer solvent based on preliminary studies, but ethanol
284 and acetone were tested as alternative transfer solvents (Figure S4), and showed nearly identical
285 efficiency, demonstrating that the identity of the transfer solvent is less important than its ability
286 to form a stable emulsion with the organic phase. This is likely due to the predominantly-hexane
287 organic phase allowing only hexane-soluble molecules to overflow into the trap. Once extraction
288 is complete, solvents can be recycled, since no solvent is lost during the extraction process.
289 Sustainable options also exist for utilizing the delipidated biomass, with valuable options being
290 aquaculture or animal feed³⁴. Removal and disposal of residual solvent presents little challenge
291 since no chlorinated hydrocarbon solvents or acids are used during the process, allowing
292 straightforward recovery of the biomass after fractionation.

293 Precise engineering of the system was not carried out but could yield major
294 improvements in energy efficiency at scales larger than discussed here. Improvements in heat
295 transfer, extraction time, trap volume, and mixing would be critical, and the authors hope this
296 work will be done.

297 298 Conclusion

299
300 Using a single, simple, and scalable system, crude lipid extracts have been generated
301 from five distinct biomass sources without specialized pretreatment. In a scaled-up construction
302 of the system, microbial biomass was extracted at a larger scale than ever previously reported in
303 a laboratory setting. As the product profile of microbes and plant continues to grow, efficient
304 systems like the one described here will serve a critical role in overcoming the obstacles of large-
305 scale production and isolation of microbial-derived products, and advance the viability of
306 sustainable production of bio-products.

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314

315 Notes and References

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- 382
383
384

385 Table 1 (full page width)

386

387 Brief literature survey of extraction trials in the last 15 years using microbial or plant slurries
 388 with total solids content greater than 100 g.

389

Method	Organism	Scale (g)	Pretreatment	Preservation of Lipids	Possible in Lab Setting	Demonstrated Scalability	Reference
Solvent	<i>M. oleifera</i> (plant)	150	Drying and enzyme treatment	+	+	-	15
Thermal	<i>C. protothecoides</i> (algae)	160	Hydrolysis	-	+	+	35
SC - CO ₂	<i>N. sp.</i> (algae)	180	Drying and grinding	+	+	-	36
SC - CO ₂	<i>J. regia</i> (plant)	370	Pressing	-	-	-	37
Thermal	<i>S. cerevisiae</i> (yeast)	540	None	-	-	-	38
Lipid Trap	<i>S. dimorphus</i> (algae)	660	None	+	+	+	This manuscript

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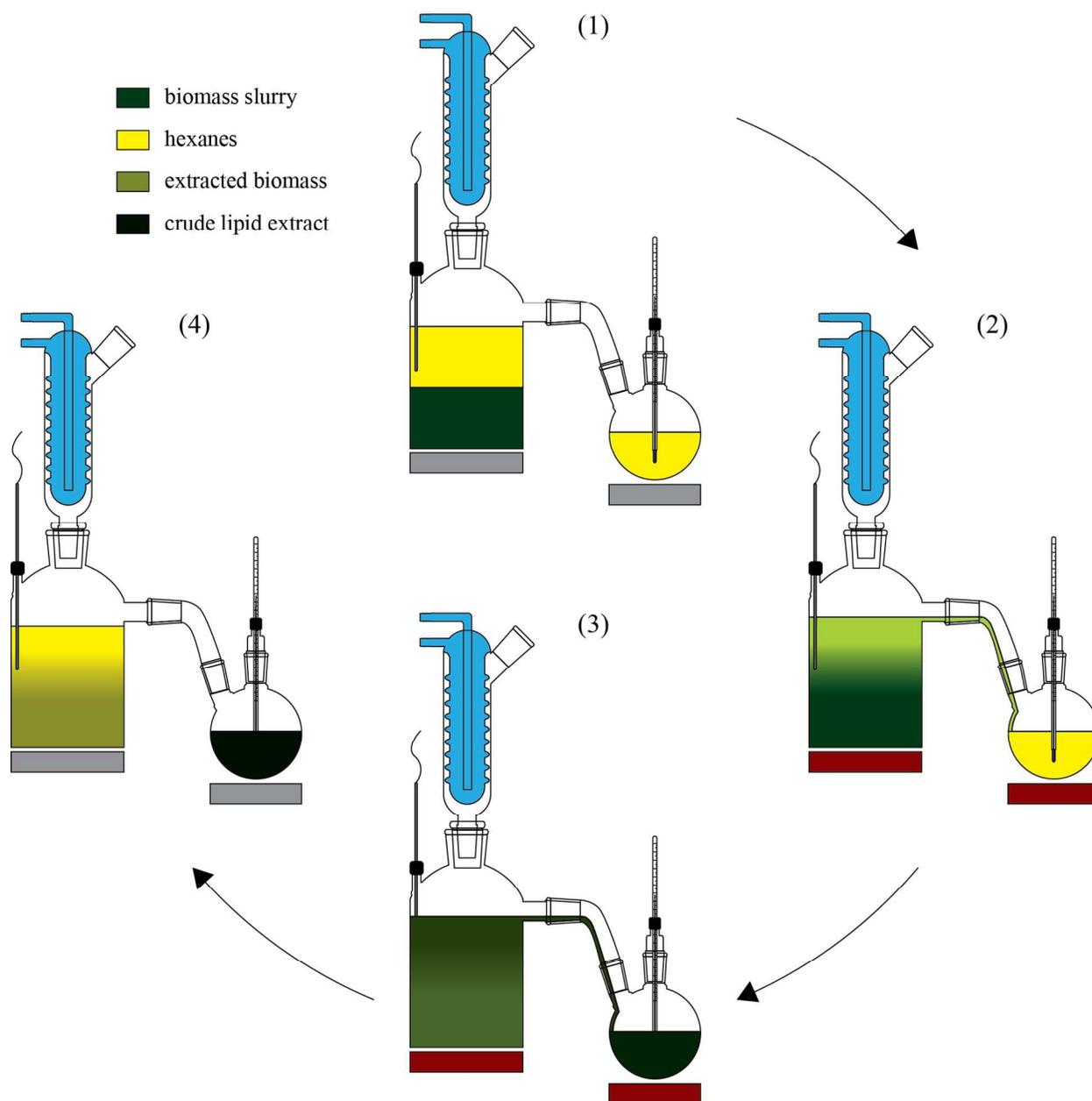
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393 Figure 1 (full page width)

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395 Operational diagram of the lipid trap system as observed with microalgae as the feedstock. The
396 extraction vessel (left) is initially charged with 550 mL of biomass slurry, 550 mL of hexane, and
397 650 mL of isopropanol as the transfer solvent, while the lipid trap is charged with 700 mL
398 hexane (right) (1). The extraction vessel is heated to 45°C to increase the rate of extraction, while
399 the lipid trap is heated to reflux. Upon heating, extraction begins, and the condensed solvent
400 from the trap causes the organic phase of the extraction vessel to overflow, carrying with it
401 extracted lipid (2). As extraction continues, lipids become concentrated in the trap while
402 extraction continues (3). Upon completion, the delipidated slurry remains in the extraction
403 vessel, with concentration of the lipid fraction in the trap (4).

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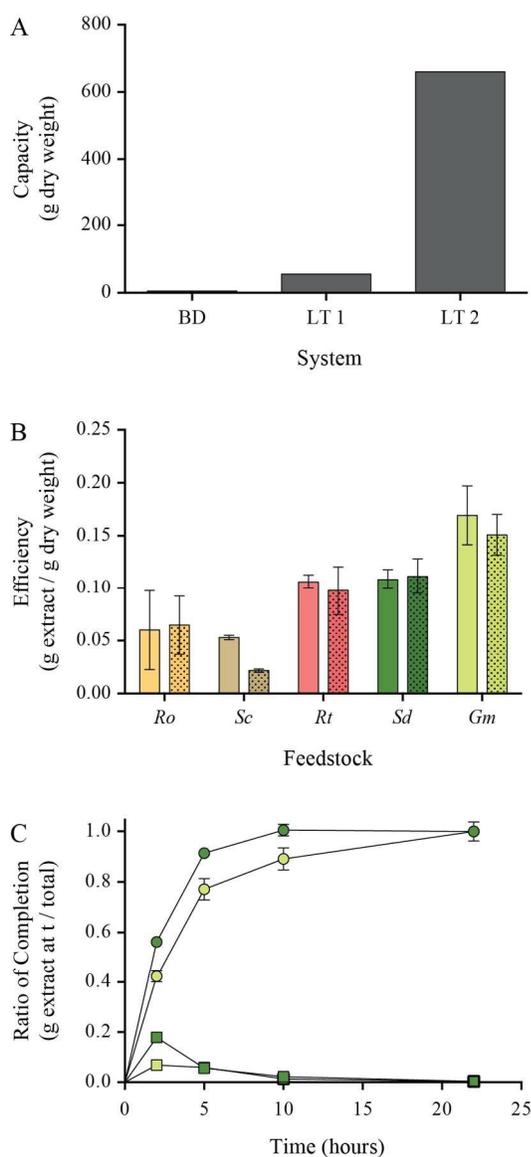


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407 Figure 2 (full page width)

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409 System dynamics. System capacity (A) was over an order of magnitude larger in the scaled-up
410 lipid trap system, with the smaller 1.8 L system still providing a 10-fold increase in capacity over
411 the analytical Bligh and Dyer method. Extraction efficiency (B) was comparable for each
412 biomass source. Solid bars represent extraction efficiency using the lipid trap, hashed bars
413 represent standard Bligh and Dyer extraction efficiency. Error bars represent the standard
414 deviation of triplicate experiments. Timecourse experiments (C) revealed that extraction of *Gm*,
415 the feedstock with the highest concentration of lipid, was over 80% complete after 10 hours, and
416 extraction of less oleaginous feedstock (*Sd*) neared completion after 5 hours.

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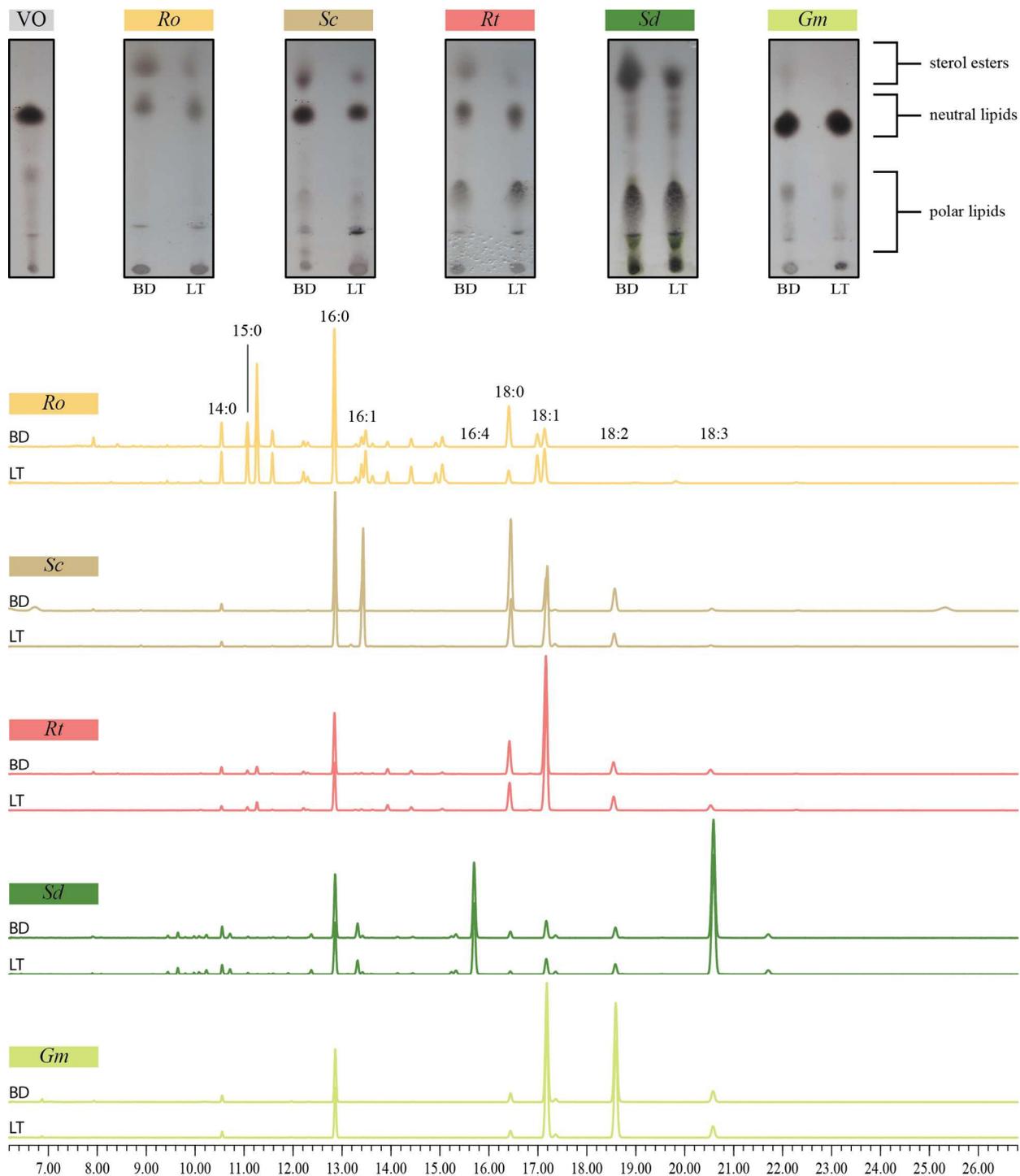
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419 Figure 3 (full page width)

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421 Compositional comparison using TLC and GC/MS of lipid trap (LT) extracts to Bligh and Dyer
422 (BD) extracts. TLC of vegetable oil (VO) is shown for reference.

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