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Investigation of the mechanical properties and local structural evolution of Ti₆₀Zr₁₀Ta₁₅Si₁₅ bulk metallic glass during tensile deformation: a molecular dynamics study

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Abstract

 $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ bulk metallic glass (BMG) has been proven to have potential for use in an orthopedic bone fixation device, and further studies on its structural properties and deformation mechanism under uniaxial tension have been conducted using molecular dynamics (MD) simulations. The Honeycutt-Andersen (HA) index analysis, Voronoi tessellation method and Warren-Cowley short-range order parameter are employed to investigate its structural properties. The results show a high content of icosahedral-like structures, which suggests an amorphous state and the trend of silicon to pair with a metal atom.

In its tensile test, the Ti₆₀Zr₁₀Ta₁₅Si₁₅ bulk metallic glass showed good ductility and an estimated Young's modulus of about 93 GPa, which is close to the experimental value. Local strain distribution was used to analyze the deformation mechanism, and results show that shear bands develop homogeneously, which enhances the plasticity. The Voronoi tessellation analysis and HA index were used to further investigate the plastic/elastic deformation mechanism. The results of the HA analysis show that icosahedral local structures (1551, 1541, 1431) transfer to less dense structures (1422 and 1311), which shows an increase of open volume and which can be attributed to the formation of the shear bands. In addition, the Voronoi tessellation analysis also shows the notable change from perfect icosahedra to distorted icosahedra. Further investigation shows the variations of Voronoi index are mostly the Ti and Si-centered clusters. This suggests that the structures around Ti and Si atoms undergo a severe evolution during the tension process.

Keywords: Bulk metallic glasses, molecular dynamic, DFT calculations, mechanical properties

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Introduction

Bulk metallic glasses (BMGs) have been proven to possess many material properties far superior to their crystalline counterparts, including higher tension and compression strength up to 6 GPa [1,2], larger elastic deformation strain limit up to 2% [3], and excellent corrosion resistivity [4]. In recent years, much more attention has been paid to BMG's biomedical applications for artificial implants such as bone substitute applications or as orthopedic bone fixation devices [5-7]. Previous studies have shown that Zr-based and Ti-based BMGs display high biocompatibilities with tests in NaCl and PBS (phosphate-buffered saline) solutions showing good corrosion resistance to chloride (Cl) and phosphorus (P) ions [5, 8, 9]. Because of these two characteristics, BMGs have been commonly applied to materials for biodegradable implants for bone [10].

In 2007, Oak produced a series of biocompatible Ti-based BMGs without using toxic elements such as Ni and Cu [11]. They have successfully prepared the fully amorphous ribbons in Ti–Zr–Ta–Si systems, and the results prove that these alloys possess high corrosion resistance *in vivo* and good ductility as measured by folding the specimen without observing any obvious cracks. Moreover, the Young's moduli of Ti-Zr-Ta-Si BMGs (~88 GPa) [11] are relatively close to that of human bone (~30 GPa) [12] when compared to 200 GPa and 106 GPa, respectively, for the 316 L stainless steel and Ti–6Al–4V alloy which are commonly used in the current biomedical industry[13]. With Young's moduli closer to that of human bone, BMGs could prevent the occurrence of stress concentration at the interface between the BMG and the bone after the implant. Thus, the Ti–Zr–Ta–Si alloys have great potential for biomedical implants.

In the fabrication of biocompatible BMGs, the advantages of adding the Si element have been reported by several experimental studies. Wang *et al.* reported that small metalloid elements carbon (C), silicon (Si), and boron (B) may tighten the alloy structures and stabilize the amorphous alloy against crystallization [14]. In Zhang's study, they stated that the benefits of additional Si would be the forming of efficiently packed local structures which are often associated with low energy and high viscosity of liquid [15]. Hu's study also demonstrated that the dense and randomly packed clusters are the reason why smaller atoms can enhance the glass forming ability because these clusters make the redistribution of atoms on large range scale during the cooling process more difficult [16].

Although the X-ray diffraction (XRD) profile can be used to evaluate the crystallinity of BMGs [17], it is very difficult to investigate the detailed local atomic arrangements around each compositional element and the variations of local atomic arrangements under external loading by the experimental approach directly. The

possible alternative to investigate the local atomic arrangement of BMGs is by using numerical simulation. Among different numerical methods, molecular dynamics (MD) simulation can overcome the limitations of traditional empirical approaches and enable detailed observations on local structural variations and the deformation mechanism of BMGs under external loading on the atomic scale. For example, Wang studied the tensile behavior of a $Cu_{46}Zr_{46}Al_8$ BMG at elevated temperatures by molecular dynamics simulation [18]. The results show that open volume increases notably after pure elastic deformation, indicating that sufficient open volume activates the plastic deformation. Albe used MD to observe the shear band formation process for CuZr BMG and CuZr BMG with nanoglass [19]. They found that plastic deformation is enhanced in the CuZr BMG with nanoglass due to the homogeneous shear band initiated around the BNG and nanoglass interfaces. In Zhang's study, the structure anisotropy is quantified through the information obtained by molecular dynamics [20]. Results show that the major atomic pairs causing the structure's anisotropy are different in Cu₅₀Zr₅₀ and Cu_{64.5}Zr_{35.5}, and influence their deformation mechanisms.

From the discussions above, it is clear that MD simulation provides a powerful tool for investigating the variation of local atomic arrangements of Ti–Zr–Ta–Si BMG during the deformation process at the atomic level. Since Oak and Inoue have stated the optimal element composition of Ti–Zr–Ta–Si to avoid Cl and P corrosion is $Ti_{60}Zr_{10}Ta_{15}Si_{15}$, the BMG model with the same Ti, Zr, Ta, and Si compositions were used to explore the local atomic arrangements and deformation mechanism under tensile loading. To the best of our knowledge, this study is the first to provide the interaction parameters between Si and three other metal elements for this multi-element system by the force-matching method [21]. By these potential parameters, the BMG model was constructed and the detailed local structural arrangements around each atom type were conducted.

Simulation model

In order to model the Ti-Zr-Ta-Si alloy system by molecular dynamics (MD) simulation, two potential functions, the tight-binding[22] and Tersoff [23] forms, were used to describe the interactions between different atomic pairs. The tight-binding potential is responsible for modeling the interaction between metallic element pairs and the Ta-Si pair, while the Si-Si, Zr-Si, and Ti-Si pairs are simulated by Tersoff potential.

The tight-binding potential form is shown as Eq. (1):

$$E_{i} = -\left\{\sum_{j}\xi^{2}\exp\left[-2q\left(\frac{r_{ij}}{r_{0}}-1\right)\right]\right\}^{1/2} + \sum_{j}A\exp\left[-p\left(\frac{r_{ij}}{r_{0}}-1\right)\right]$$
(1)

where ξ is an effective hopping integral, r_{ij} is the distance between atoms *i* and *j*, and r_0 is the first-neighbor distance.

The Tersoff potential involving both two- and three-body terms is shown as Eq.(2):

$$U_{total}^{Ter} = \sum_{i=1}^{N} E_{i} = \frac{1}{2} \sum_{i \neq j} V(r_{ij})$$
(2)

where E_i is the potential energy of atom *i* and $V(r_{ij})$ is the energy formed between two atoms. The term $V(r_{ij})$ is defined as:

$$V(r_{ij}) = \sum_{i} \sum_{j>i} f_c(r_{ij}) [f_R(r_{ij}) + b_{ij} f_A(r_{ij})]$$
(3)

$$f_A = -B_{ij} \exp(-u_{ij}r_{ij}) \tag{4}$$

$$f_R = A_{ij} \exp(-\lambda_{ij} r_{ij})$$
⁽⁵⁾

$$b_{ij} = (1 + \beta_i^{n_i} \zeta_{ij}^{n_i})^{-1/2n_i}$$
(6)

$$\zeta_{ij}^{n_i} = \sum_{k \neq i,j} f_c(r_{ik}) g(\theta_{ijk})$$
(7)

$$g(\theta_{ijk}) = 1 + \frac{c_i^2}{d_i^2} - \frac{c_i^2}{[d_i^2 + (h_i - \cos \theta_{ijk})^2]}$$
(8)

$$f_{c}(r_{ij}) = \begin{cases} 1, r_{ij} < R_{ij} \\ \frac{1}{2} + \frac{1}{2} \cos[\pi \frac{(r_{ij} - R_{ij})}{(S_{ij} - R_{ij})}], R_{ij} < r_{ij} < S_{ij} \\ 0, S_{ij} < r_{ij} \end{cases}$$
(9)

The coefficient b_{ij} corresponds to a many-body interaction and the function f_C is merely a smooth cutoff function which limits the range of the potential. The function $g(\theta_{ij}k)$ represents the influence of the bending angle.

The force-matching method (FMM) [24] was used to determine all parameters of tight-binding and Tersoff potentials on the basis of binding energies and elastic constants of pure elements (Ti, Zr, Ta, Si) and binary metal systems including structures reported in experiment (Zr₃Si₂[25], ZrSi[26], ZrSi₂[27], Ta₂Si[28], Ta₅Si₃[28], TaSi₂[29], TiSi[30], TiSi₂[31], Ti₃Si[32]) and those structures built by DFT calculation (ZrTi, TiTa, and ZrTa). These parameters can be seen in the supplemental file.

After the parameters are fitted, they are used to generate the stable $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ amorphous structure by the simulation anneal basin-hopping (SABH) method[33] along the search direction for the energy local-minimal structure at higher energy. The unit cell with a total of 5,000 atoms (3,000 Ti, 500 Zr, 750 Ta and 750 Si atoms) is shown in Fig. 1(a), and the model shown in Fig. 1(b) for the tension test by MD was constructed by replicating the unit cell to $6 \times 3 \times 6$ for the x, y and z axes.

Next, the MD simulation was performed by the large-scale atomic/molecular massively parallel simulator (LAMMPS) developed by Plimpton and co-workers[34]. By MD simulation, the model was quenched from 1000 K to 300 K for 10 ps to relax the system with an NPT ensemble at 0 GPa. During the tensile process, the periodic boundary conditions (PBC) were applied to the x-, and y-dimensions and the open boundary was used in the z-dimension. The strain rates of 5×10^9 , 1×10^9 , 5×10^8 , 4×10^8 and 2×10^8 m/s were examined for obtaining the appropriate strain rate for the current system. For 5×10^9 and 1×10^9 m/s, the predicted strengths and the fracture strains are considerably lower than those from the MD simulations with the slower strain rates. By using the strain rates of 5×10^8 , 4×10^8 and 2×10^8 m/s, the strengths and the fracture strains are strains are very close. For saving the simulation time, the strain rate of 5×10^8 m/s was used for the current study by increasing the z-dimensional length of the PBC box. During the tension process, the tensile stress at different strains was calculated by the following equation in LAMMPS code [35]:

$$\sigma_{mn} = \frac{\sum_{i} -1 \times \left[m v_i^m v_i^n + \frac{1}{2} \sum_{n=1}^{N_p} (r_{1m} F_{1n} + r_{2m} F_{2n}) + \frac{1}{3} \sum_{n=1}^{N_a} (r_{1m} F_{1n} + r_{2m} F_{2n} + r_{3m} F_{3n}) \right]}{\sum_{i} V_i}$$
(10)

where $\sum_{n=1}^{N_p} (r_{1m}F_{1n} + r_{2m}F_{2n})$ is the effect of the pairwise potential function and indexes 1 and 2 indicate two atoms interacting with each other. The term $\sum_{n=1}^{N_n} (r_{1m}F_{1n} + r_{2m}F_{2n} + r_{3m}F_{3n})$ is the effect of bond angle to consider the three atoms

involved in the interaction. Indexes of m and n represent the m plane and n-direction. The r is the interatomic distance between two atoms 1 and j, m is the weight of the atom, and V_i is a local volume defined by:

$$V_i = \frac{2\pi \sum r_{ij}^{-1}}{3\sum r_{ij}^{-2}}$$
(11)

Results and Discussion

The $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ unit cell of 5000 atoms obtained by SABH method was characterized by the X-ray diffraction (XRD) module REFLEX [36-38] in Accelrys Materials Studio 5.5 [39]. In REFLEX, Bragg's law is used to obtain the constructive interference intensity for X-rays scattered by materials, and its formula is listed as follows:

$$d = \frac{n\lambda}{2\sin\theta} \tag{1}$$

where θ is a certain angle of incidence when the cleavage faces of crystals appear to reflect X-ray beams. The term d is the distance between atomic layers in a crystal, and λ is the wavelength of the incident X-ray beam. When n is an integer, the diffraction is constructive with higher intensity. While n is a half integer, the diffraction is destructive and the intensity approaches zero.

The XRD and RDF profiles of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ are shown in Figs. 2(a) and 2(b). One can see no specific crystalline peak appearing in the 2 θ range between $10^{\circ} - 90^{\circ}$ for the XRD profile, and the range of the XRD peak is located between $35^{\circ} - 43^{\circ}$, which is consistent with the previous experimental XRD profile of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ [40]. For the RDF profile, the broad splitting second peak indicates the amorphous configuration of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$, which is consistent with the inference of the short range order by the XRD profile. According to the XRD and RDF profiles shown in Figs. 2(a) and 2(b), the $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ structure constructed by SABH is amorphous and corresponds to realistic $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG in experiment.

A further study into the local microstructural distribution for $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG was conducted by using the Honeycutt-Anderson (HA) pair analysis [40]. The detailed definition of the HA index can be found elsewhere [41,42] and is not presented here. The HA indexes of 1421 and 1422 represent f.c.c. and h.c.p. crystal structures, and 1431, 1541, and 1551—which occupy the largest fraction in the amorphous or liquid state—are used to search the icosahedral local structures. The 1551 pair is particularly characteristic of the icosahedral ordering; the 1541 and 1431 are indexes for the defect icosahedra and f.c.c. defect local (or distorted icosahedra) structures, respectively. HA indexes 1661 and 1441 are employed to identify the local b.c.c. structure. Finally, the indexes 1321 and 1311 are the packing related to rhombohedral pairs which tend to evolve when the 1551 packing forms, which can be viewed as the side product accompanying icosahedral atomic packing. The schematic diagrams for the HA indexes introduced above can be clearly seen in Fig. 3(a).

Figure 3(b) shows the HA index distribution of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG, and the fraction of icosahedra-like local structures (1551, 1541, and 1431) are over 70%. The fractions of these three icosahedra-like structures are very close and each of them

occupies about 23% of all HA fractions. For other HA indexes, the b.c.c local structures (1441 and 1661), h.c.p local structure (1422), rhombohedral local structures (1321 and 1311), and f.c.c. local structure (1421) are about 7.5, 9.1, 7.2, and 6.7%, respectively. The high HA fractions of icosahedra-like structures verify the amorphous $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ structure and are consistent with the HA analysis results reported previously for BMGs.

Since the atomic radii of Zr, Ti, Ta, and Si are 1.55, 1.47, 1.46, and 1.11 Å, with the atomic size of Si smaller than the other three by about 24.0%- 28.4%, the HA fraction distribution for different atom type pairs could be very different. Because the HA index profiles shown in Fig. 3(b) do not contain enough information about the HA fraction distributions for different atom pairs, they should be analyzed to better understand the local structural arrangements around different atom pairs with different pair lengths. The HA indexes of different the atomic pairs in $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG are shown in Fig. 4. Because Ti occupies the highest atomic fraction of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG, the Ti-related HA indexes (Zr-Ti, Ti-Ti, Ti-Ta, and Ti-Si) are relatively higher than those for other atom type pairs. The summations of the icosahedra-like HA indexes 1551, 1541, and 1431, referring to the liquid local structures, are about 23.02, 13.14, 7.81 and 8.06% for the atom pairs of Ti-Ti, Ti-Ta, Ti-Si and Ti-Zr, respectively.

HA index analysis can provide detailed fraction distribution of different local structural configurations around all two bonded-atom pairs of the system. However, the HA index lacks the information to describe the complete morphology surrounding an investigated atom. Thus, further classification of the polyhedral order is performed by using the Voronoi tessellation analysis [43,44]. The Voronoi polyhedra (VP) are constructed from all edges formed by the intersections of the planes halfway between the central atom and all of its first neighbor atoms. The Voronoi indexes (n_3, n_4, n_5, n_6) are classified based on the number of edges making up each polyhedral face. These indexes, n₃, n₄, n₅, and n₆, are the numbers of 3-, 4-, 5-, and 6-edged faces comprising the polyhedron. Consequently, the summation of n_3 , n_4 , n_5 , and n_6 is the coordination number of the referenced atom. For example, the Voronoi indexes of the perfect ICO, BCC, and FCC/HCP are (0,0,12,0), (0,6,0,8) and (0,12,0,0), respectively. However, the VPs will be distorted to many other VP forms when compared to their crystalline counterparts because of the thermal noise or atoms in the amorphous system. Therefore, only the most frequently observed VPs from previous studies [43-47] are discussed. These VPs include (0,2,8,1), (1,0,9,3), (0,1,10,2), (0,3,6,2), (0,4,4,3), (0,3,6,3), (0,2,8,2), and (0,4,4,4) for deformed icosahedrons; (0,3,6,5), (0,4,4,6), and(0,4,4,7) for deformed f.c.c.; and (0,2,8,4) for deformed b.c.c. These results are shown in Fig. 5, and the higher (0,0,12,0) fraction for Si indicates that the ideal icosahedral

structures are prone to construct around Si atoms, while the distorted icosahedral structures are mainly constructed around Ti and Si atoms. This VP analysis result indicates that the Si atom, having the smallest radius, enhances the formation of local icosahedral or deformed icosahedral clusters and therefore improves the glass forming ability by forming more dense and more viscous local Si icosahedra-like clusters.

Table I lists the average coordination numbers (CNs) of Ti, Zr, Ta, and Si atoms in $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG as well as the partial coordination numbers of different atomic pairs. The coordinate number was calculated by counting the amount of first neighbor atoms around the center atom. The first subscript for atomic pair indicates the type of the reference atom and the second subscript stands for the atom type of the first neighbor of the reference atom. Among the average CNs of these four elements, the Zr and Si atoms have the highest and lowest CNs of 13.63 and 11.04, respectively. Since in the $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG, the atomic size of Zr is the largest and Si is smallest, this suggests that the atom with the larger atomic size tends to be located at the center of a cluster with a higher CN. A closer investigation of the partial CNs of Zr-Si, Ti-Si, Ta-Si, and Si-Si shows that the partial CN of Zr-Si is the highest and that of Si-Si is the lowest. Thus, the larger atom provides more open volume for the placement of the first neighbor atom of a smaller size.

The Warren-Cowley chemical short-range-order (CSRO) analysis [48] for $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG was employed to quantify the attraction and repulsion between element pairs. With the CN information shown in Table 1, the chemical affinities of a referenced atom with its first neighbor atoms are evaluated by the CSRO parameter. The definition of this parameter is as the following equation:

$$\alpha_{ij} = 1 - \frac{N_{ij}}{c_j N_i} \tag{12}$$

where a_{ij} is the CSRO parameter of the *i*-type referenced atom related to *j*-type atom, N_{ij} is the partial CN for the *i*-type referenced atom related to *j*-type atom, and c_j and N_i are the fractions of *j*-type atom within the alloy and the average CN of *i*-type atoms, respectively. The value of c_j by N_i is an ideal partial CN for the referenced *i*-type atom related to the first neighbor *j*-type atom, and this value completely depends on the respective atomic composition fraction of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$. According to this analysis, it can be seen that if the alloys are in the ideal solution, the value of N_{ij} should be very close to c_jN_i and allows the value of α_{ij} to be 0. On the other hand, a value larger than 0 means the *j*-type atoms are less prone to gather around *i*-type atoms, causing the value of N_{ij} to be less than the number of ideal N_{ij} . For the same reason, a negative value means the *j*-type atoms are prone to gather around *i*-type atoms.

The CSRO parameters of all pairs of Ti₆₀Zr₁₀Ta₁₅Si₁₅ BMG are listed in Table II.

The results show that the CSRO parameters for Zr-Zr, Ta-Ta, and Si-Si are positive and that of Ti-Ti is relatively close to zero. This CSRO analysis result indicates the Ti atom has no preference to another Ti atom, and the three other elements display less affinity to themselves, indicating that this alloy easily forms the glassy structure and has higher thermal stability. Furthermore, most CSRO parameters of Si-related pairs are negative except for Ti-Si, and Ta-Si pairs with smaller CSRO values, indicating that the affinities between Si and the three other metal elements are relatively higher than Zr-Zr, Ta-Ta, and Ti-Ti. The Si-Si and Si-Zr CSRO values are the most positive and the negative among all atom pairs, and this reveals that the smallest atom, Si, tends to pair with a metal atom instead of itself. Because the Zr is the largest atom of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG, Si has the highest affinity to the Zr atom. With these results, one can realize that a diversity of atom sizes in the solution can advance the formation of the amorphous state. When this increases, it is relatively easy to form the amorphous structure because the higher fractions of denser icosahedra-like local structures decrease the atomic mobility and lead to a more viscous solution.

Figure 6 shows the stress-strain profile and $\Delta V/V$ value with strain for the $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG under tension. One can see the stress increases linearly with strain while strain increases from 0 to 0.05, indicating the elastic behavior of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG is located within this strain range. The Young's modulus derived from the slope of the stress-strain profile at the elastic region is about 93 GPa, while the corresponding experimental value is about 88 GPa [11]. The predicted Young's modulus is slightly larger than the experimental value by about 5.7%, indicating our simulation model by the TB and Tersoff potentials can realistically reflect the mechanical properties of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG. At strains from 0.05 to 0.33, the stress displays a parabolic increase with the increasing strain, and reaches its maximal value about 12.25 GPa. At strains from 0.33 to 0.36, the stress shows an abrupt drop from its maximal value, indicating the occurrence of fracture.

The $\Delta V/V$ value, the ratio of open volume (ΔV) to the system volume at strain 0 (V), was used to indicate the volume variation during the tension process. It is a general view that more open volume allows for more plastic deformation [18]. The system volume is defined as the summation of the atomic volume calculated by Eq. (13), and the ΔV value is calculated by the following equation:

 $\Delta \mathbf{V} = \mathbf{V}_{\varepsilon} - \mathbf{V}_0 \tag{13}$

where V_{ε} and V_0 are the system volumes at strains of ε and 0, respectively. Consequently, the $\Delta V/V$ value indicates the percentage increase in system volume during the tension. In Fig. 6, it is apparent that $\Delta V/V$ is linearly proportional to the strain within the elastic region. At strains from 0.05 to 0.15, the open volume increases parabolically with the strain, and the increase of $\Delta V/V$ with the strain becomes more significant when the strain exceeds 0.15.

The atomic local shear strain η_i^{Mises} of an individual atom, introduced by Shimizu *et. al.* [49], was used to monitor the development of shear transition zones (STZ) and the formation of the shear band within Ti₆₀Zr₁₀Ta₁₅Si₁₅. The detailed definition of η_i^{Mises} can be found in reference [50] of this study and is therefore not introduced here. A large η_i^{Mises} value indicates atom *i* is under local plastic and shear deformation, whereas a small η_i^{Mises} value implies atom *i* undergoes a small amount of movement relative to all its first neighbor atoms or atom *i* is under local elastic deformation.

Figure 7(a)-(f) shows snapshots of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG with atomic η_i^{Mises} values at strains of 0, 0.05, 0.15, 0.25, 0.325 and 0.35, which are labelled as the letters a-f on the stress-strain curve of Fig. 6. For the reference structure at strain of 0, the n^{iMises} value of each atom is 0, and the initialization of STZs labeled by dashed circles in Fig. 7(b) occurs at strain of 0.05. These STZs distribute randomly within Ti₆₀Zr₁₀Ta₁₅Si₁₅ BMG. From Fig. 6, one can infer that the sufficient open volume increase significantly activates the initialization of shear banding and enhances the appearance of STZs when the strain exceeds the yielding strain. At strain of 0.15, the extension of STZs begins to form several shear bands, as shown in Fig. 7(c), and more shear bands can be seen in Fig. 7(d) for $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG at strain of 0.25. In Fig. 6, the $\Delta V/V$ value increases more significantly with the strain when the strain exceeds 0.15. From the the η_i^{Mises} distributions shown in Figs. 7(c) and 7(d), one can note that the increase in the shear band number results in the significant increase of the open volume and a local structure rearrangement. The shear bands propagate at a direction 45⁰ from the tensile direction and intersect with one another, resulting in the vein-like pattern. This vein-like pattern can be also seen in previous theoretical [51] and experimental studies [11,52]. These results show that good ductility of $T_{i_{60}}Zr_{10}Ta_{15}Si_{15}$ might be caused by the homogeneous development of shear bands which increase the deformed area. Fig. 7(e) and 7(f) show the fracture areas at strains of 0.325 and 0.35, where considerable atomic rearrangements occur.

To understand the local structural rearrangement during the tension process, the numbers of different HA pairs for $Ti_{60}Zr_{10}Ta_{15}Si_{15}BMG$ at different strains during the tension are illustrated in Fig. 8. The vertical axis represents the total number of one particular HA pair and the horizontal axis is the tensile strain. The reason that this study uses the number of pairs instead of pair fraction is that total bonding pairs at each strain will decrease due to increasing distance between atoms during the tensile process such that the fraction is not the best choice to represent the variation of local structure. It can be seen from Fig. 8 that at different strains, the icosahedral local structures 1431, 1541, and 1551 are predominant. Among all HA pairs, there are four

indexes with notable changes. The 1551 and 1541 HA indexes referring to the icosahedral and defected icosahedral structures show considerable decreases such that the pair numbers of 757,007 and 732,142 for 1551 and 1541 at the beginning of the tensile test become 548,512 and 601,358 at strain of 0.35. For 1422 and 1311, these two HA indexes increase with the strain from 85,203 and 146,013 to 156,471 and 240,939, respectively. Since the second index of the HA analysis is the number of common neighbor atoms between the investigated atomic pair, the decrease of HA indexes with the larger second indexes implies the local structures in $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG become less dense during the tensile process.

Because the atomic radii of Zr, Ti, Ta and Si are different, the variations of HA index numbers for different atom type pairs during the tension process could be very different. Figure 9(a)-(j) shows the HA index numbers for different atom pairs of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG at different strains during the tension process. The HA indexes of different atom pairs show two distribution patterns of the icosahedra-like structures. For Si-related HA atom pairs (Zr-Si, Ti-Si, Ta-Si, and Si-Si) at strain of 0, the icosahedral structures (1551) are the most populous among all indexes in Fig. 9(d), 9(g), 9(i), and 9(j). For other atom pairs, the defected icosahedra (1541) or distorted icosahedra (1431) structures have higher numbers than other HA indexes.

Although the 1431 HA fraction of all atom pairs remains constant during the tension process shown in Fig. 8, the 1431 HA fraction of the Ti-Si pair displays an increasing trend when the strain is larger than 0.15, whereas the 1431 fractions of Ta-Ta, Ta-Si, and Si-Si pairs decrease with the increasing strain. For other atom pairs in Fig. 9(a)-(f), the 1431 numbers remain almost the same at different strains. For the 1551 HA index, the numbers of all atom pairs decrease with increasing strain. For Si-related atom pairs, the 1551 numbers display a more significant decrease when strain is larger than the yielding strain of 0.05. For the Si-Si pair, the 1551 number remains almost constant until the strain of 0.15, at which the shear band begins to form and the shear band number increases. For the defected icosahedra HA index 1541, Ti-Si, Zr-Si, and Si-Si increase with the strain, even though the 1541 number of all atom pairs in Fig. 8 displays a significant decrease with the increasing strain. It should be noted that the HA index distribution of the Si-Si pair is very different from those of other atom pairs. The fraction of the defected icosahedra HA index (1541) is relatively much lower than those of other atom pairs, and the (1551) icosahedra HA fraction is much higher than those of other atom pairs. As the strain exceeds 0.15, the increase in the 1541 number of the Si-Si pair can be attributed to the decrease of 1551 and 1431 numbers.

The variations of local cluster structures during the tension were investigated by the Voronoi tessellation analysis. Figure 10 shows the Voronoi index variations during

the tensile process. At strain between 0 and 0.05, the fractions of all VP indexes display only slight variation, indicating that most cluster structures do not rearrange at strain within the elastic region. When the strain exceeds 0.05, however, the deformed icosahedra fractions of (0,1,10,2), (0,3,6,3), and (0,4,4,4) increase considerably with strain, whereas the fraction of the distorted b.c.c. (0,2,8,4) decreases. It should be noted that the icosahedra (0,0,12,0) VP fraction slightly increases when the strain increases from 0.05 to 0.08 and then undergoes a significant decrease when the strain is larger than 0.15. From these results and the η_i^{Mises} distributions shown in Fig. 7(b)-(d) for strains of 0.05, 0.15, and 0.25, it can be inferred that once the strain exceeds the yielding strain of 0.05, the deformed icosahedral clusters appear within the STZs, and the shear bands formed by the evolution of STZs at strain of 0.15 increase and result in the decrease of icosahedral clusters and the increase of open volume shown in Fig. 6.

Because the VP fractions of (0,0,12,0), (0,1,10,2), (0,3,6,3), and (0,2,8,4) indexes have significant changes during the tension process, the fractions of these four VP indexes with different center atoms are given in Fig. 11. It is apparent that the fraction of icosahedral clusters with the Si center atom significantly decreases and transforms into a deformed icosahedral and b.c.c. clusters.

As shown in the discussion above, icosahedral clusters play a crucial role in the tension process. Previous studies [53, 54] have reported that the perfect icosahedra, which refers to 1551 HA index and (0,0,12,0) in Voronoi tessellation analysis, has high corrosion resistivity and high density. Moreover, the work of Cao *et al.* [55] has suggested that the onset of local instability will be triggered by structural softening. Thus, it is proposed that the STZs tend to be initiated at the regions with higher fractions of icosahedral local structures for different atom type pairs, and icosahedral structures become more disordered and more loosely packed clusters due to tensile loading. These instabilities then nucleate and lead to the formation of STZs. With increasing strain, STZs extend along a direction 45° from the tensile direction to form multiple shear bands, as shown in Fig. 7, and finally cause the fracture.

Conclusion

Molecular dynamics simulation has been conducted to investigate the structural and mechanical properties of $Ti_{60}Zr_{10}Ta_{15}Si_{15}BMG$. The unit cell of $Ti_{60}Zr_{10}Ta_{15}Si_{15}BMG$ built by the SABH method is examined by XRD and no specific crystalline peak is found, indicating these two BMGs from our SABH prediction are totally amorphous. From HA index and Voronoi index analyses, the icosahedra-like structures that indicate liquid local structures appear to be the major local structures in the $Ti_{60}Zr_{10}Ta_{15}Si_{15}BMG$, with these icosahedra-like structures prone to form around

Ti and Si atoms. The considerable icosahedra-like structures improve the glass forming ability by forming denser and more stable local clusters. Furthermore, chemical affinities are investigated by CSRO parameters. The CSRO parameter of the Zr-Si pair has the most positive value, which indicates that the smaller Si atom tends to pair with a metal atom instead of itself and therefore demonstrates the fact that a high diversity of atom sizes in the solution will advance the formation of the amorphous state.

Based on the stress-strain profile obtained from the tensile test, the predicted Young's modulus is close to the available experimental results, indicating that the current simulation model using the TB and Tersoff potentials can accurately reflect the realistic atomic interaction among Ti, Zr, Ta and Si atoms. Besides the Honeycutt-Anderson (HA) pair analysis and Voronoi tessellation analysis, analysis of variation in the open volume is also employed to monitor the development of STZ [56] and the evolution of the shear band. The distributions of the stress-strain curve and open volume with strain show linear increases of stress-strain and open volume-strain curves which suggest an elastic region. Moreover, stress and open volume increase significantly at STZ initialization stages. This can be attributed to an increase in the number of shear bands, resulting in a significant increase of open volume and the activation of local structure rearrangement. In addition, shear bands measured by the local atomic strain develop along a direction 45⁰ from the tensile direction and indicate good ductility of the Ti₆₀Zr₁₀Ta₁₅Si₁₅ BMG. This ductility is due to the homogeneous development of shear bands that cause a larger area to undergo plastic deformation.

As shown by the HA index analysis during the tensile test, Si-related pairs have a relatively higher content of perfect icosahedral local structures (1551), while other pairs are dominated by defect (1541) and distorted (1431) icosahedra. Less dense indexes (1422 and 1311) are found to increase for all pairs with increasing strain, consistent with the results of a parabolic increase of open volume with increasing strain. Further, Voronoi tessellation analysis shows that (0,0,12,0), (0,1,10,2), (0,3,6,3) and (0,2,8,4) forms undergo the most notable changes during the tensile process. With strain increase, local structures surrounding Si transform from perfect icosahedra (0,0,12,0) to distorted icosahedra (0,1,10,2) and (0,3,6,3), while local structures surrounding Ti transform from (0,2,8,4) b.c.c.-like structures in liquid state to distorted icosahedral ones (0,3,6,3). The HA and Voronoi index results show the change from denser local structures to loose local structures that lead to the increase in open volume. Furthermore, these loose and unstable clusters will gather to form the shear band and the fracture occurs after the extension of STZs.

Reference

- [1] Jianfeng Wang, Ran Li, Nengbin Hua, and Tao Zhang, "Co-based ternary bulk metallic glasses with ultrahigh strength and plasticity," *Journal of Materials Research, vol 26, Res. 26 (2011) 2072.*
- [2] Z. Q. Liu and Z. F. Zhang, "Strengthening and toughening metallic glasses: The elastic perspectives and opportunities," *Journal of Applied Physics*, 115, 163505 (2014)
- [3] W. L. Johnson, *MRS Bull.*, vol. 24, pp. 42-56, 1999.
- [4] A. Inoue, Acta Mater., vol. 48, pp. 279-306, 2000.
- [5] J. J. Oak, D. V. Louzguine-Luzgin, and A. Inoue, "Fabrication of Ni-free Ti-based bulk-metallic glassy alloy having potential for application as biomaterial, and investigation of its mechanical properties, corrosion, and crystallization behavior," *Journal of Materials Research*, vol. 22, pp. 1346-1353, May 2007.
- [6] J. F. Wang, Y. Y. Wei, S. F. Guo, S. Huang, X. E. Zhou, and F. S. Pan, "The Y-doped MgZnCa alloys with ultrahigh specific strength and good corrosion resistance in simulated body fluid," *Materials Letters*, vol. 81, pp. 112-114, Aug 2012.
- [7] S. Zhu, G. Xie, F. Qin, X. Wang, and A. Inoue, "Ni- and Be-free Zr-based bulk metallic glasses with high glass-forming ability and unusual plasticity," *Journal of the Mechanical Behavior of Biomedical Materials*, vol. 13, pp. 166-173, 2012.
- [8] H. F. Li, Y. F. Zheng, F. Xu, and J. Z. Jiang, "In vitro investigation of novel Ni free Zr-based bulk metallic glasses as potential biomaterials," *Materials Letters*, vol. 75, pp. 74-76, May 15 2012.
- [9] X. N. Gu, N. Li, Y. F. Zheng, and L. Q. Ruan, "In vitro degradation performance and biological response of a Mg-Zn-Zr alloy," *Materials Science and Engineering B-Advanced Functional Solid-State Materials*, vol. 176, pp. 1778-1784, Dec 15 2011.
- [10] B. Zberg, P. J. Uggowitzer, and J. F. Loffler, "MgZnCa glasses without clinically observable hydrogen evolution for biodegradable implants," *Nature Materials*, vol. 8, pp. 887-891, Nov 2009.
- J.-J. Oak and A. Inoue, "Attempt to develop Ti-based amorphous alloys for biomaterials," *Materials Science and Engineering: A*, vol. 449, pp. 220-224, 2007.
- [12] J.-Y. Rho, T. Y. Tsui, and G. M. Pharr, "Elastic properties of human cortical and trabecular lamellar bone measured by nanoindentation," *Biomaterials*, vol.

18, pp. 1325-1330, 1997.

- [13] S. F. Guo, Z. Liu, K. C. Chan, W. Chen, H. J. Zhang, J. F. Wang, and P. Yu, "A plastic Ni-free Zr-based bulk metallic glass with high specific strength and good corrosion properties in simulated body fluid," *Materials Letters*, vol. 84, pp. 81-84, 2012.
- [14] W. H. Wang, P. W. Z. Bian, Y. Zhang, M. X. Pan, and D. Q. Zhao, "Role of addition in formation and properties of Zr-based bulk metallic glasses," *Intermetallics*, vol. 10, pp. 1249-1257, 2002.
- B. Zhang, Y. Jia, S. Wang, G. Li, S. Shan, Z. Zhan, R. Liu, and W. Wang,
 "Effect of silicon addition on the glass-forming ability of a Zr–Cu-based alloy," *Journal of Alloys and Compounds*, vol. 468, pp. 187-190, 2009.
- [16] Y. Hu, M. X. Pan, L. Liu, Y. H. Zhao, D. Q. Zhao, and W. H. Wang, "Synthesis of Fe-based bulk metallic glasses with low purity materials by multi-metalloids addition," *Materials Letters*, vol. 57, pp. 2698-2701, 2003.
- [17] G. Duan, D. Xu, Q. Zhang, G. Zhang, T. Cagin, W. L. Johnson, and W. A. Goddard, "Molecular dynamics study of the binary metallic glass motivated by experiments: Glass formation and atomic-level structure," *Physical Review B*, vol. 71, p. 224208, 2005.
- X. D. Wang, H. B. Lou, J. Bednarcik, H. Franz, H. W. Sheng, Q. P. Cao, and J. Z. Jiang, "Structural evolution in bulk metallic glass under high-temperature tension," *Applied Physics Letters*, vol. 102, Feb 4 2013.
- [19] D. Sopu, Y. Ritter, H. Gleiter, and K. Albe, "Deformation behavior of bulk and nanostructured metallic glasses studied via molecular dynamics simulations," *Physical Review B*, vol. 83, Mar 23 2011.
- [20] Y. Zhang, N. Mattern, and J. Eckert, "Molecular dynamic simulation study of the structural anisotropy in Cu50Zr50 and Cu64.5Zr35.5 metallic glasses induced by static uniaxial loading within the elastic regime," *Journal of Alloys* and Compounds, vol. 509, Supplement 1, pp. S74-S77, 2011.
- [21] G. Grochola, S. P. Russo, and I. K. Snook, "On fitting a gold embedded atom method potential using the force matching method," *The Journal of Chemical Physics*, vol. 123, p. 204719, 2005.
- [22] F. Cleri and V. Rosato, "Tight-Binding Potentials for Transition-Metals and Alloys," *Physical Review B*, vol. 48, pp. 22-33, Jul 1 1993.
- [23] J. Tersoff, "Modeling Solid-State Chemistry Interatomic Potentials for Multicomponent Systems," *Physical Review B*, vol. 39, pp. 5566-5568, Mar 15 1989.
- [24] F. Ercolessi and J. B. Adams, "Interatomic Potentials from 1st-Principles Calculations - the Force-Matching Method," *Europhysics Letters*, vol. 26, pp.

583-588, Jun 10 1994.

- [25] O. Schob, F. Benesovsky, and H. Nowotny, "Strukturbestimmung an Einigen Phasen in Den Systemen - Zr-Al-Si Und Hf-Al-Si[Zral3(Si) - Zrsi(Al), Hf(Si,Al) - Zr3si2 - Hf3si2]," *Monatshefte Fur Chemie*, vol. 92, pp. 1218-&, 1961.
- [26] A. Raman and K. Schubert, Z Metallkd, vol. 56, pp. 44-52, 1965.
- [27] M. Setton and J. Vanderspiegel, "STRUCTURAL AND ELECTRICAL-PROPERTIES OF ZRSI2 AND ZR2CUSI4 FORMED BY RAPID THERMAL-PROCESSING," *Journal of Applied Physics*, vol. 70, pp. 193-197, Jul 1991.
- [28] O. G. K. Y. A. Kocherzhinskii, Shishkin E.A., Doklady Chemistry, vol. 261, pp. 464-465, 1981.
- [29] I. Engström and B. Lönnberg, "Thermal expansion studies of the group IV-VII transition-metal disilicides," *Journal of Applied Physics*, vol. 63, pp. 4476-4484, 1988.
- [30] N. F. P. G. V. Samsonov, L.A. Dvorina, *Inorg. Mater.*, vol. 13, pp. 1429-1431, 1977.
- [31] J. Jongste, O. Loopstra, G. Janssen, and S. Radelaar, "Elastic constants and thermal expansion coefficient of metastable C49 TiSi2," *Journal of Applied Physics*, vol. 73, pp. 2816-2820, 1993.
- [32] Y. A. K. V.N. Svechnikov, L.M. Yupko, O.G. Kulik, E.A. Shishkin, *Dokl. Chem. Technol.*, vol. 192, pp. 82-85, 1970.
- [33] D. J. Wales and J. P. K. Doye, "Global optimization by basin-hopping and the lowest energy structures of Lennard-Jones clusters containing up to 110 atoms," *Journal of Physical Chemistry A*, vol. 101, pp. 5111-5116, Jul 10 1997.
- [34] S. Plimpton, "Fast parallel algorithms for short-range molecular dynamics," *Journal of computational physics,* vol. 117, pp. 1-19, 1995.
- [35] N. Miyazaki and Y. Shiozaki, "Calculation of mechanical properties of solids using molecular dynamics method," *Jsme International Journal Series a-Mechanics and Material Engineering*, vol. 39, pp. 606-612, Oct 1996.
- [36] G. S. Pawley, "Unit-Cell Refinement from Powder Diffraction Scans," *Journal* of *Applied Crystallography*, vol. 14, pp. 357-361, 1981.
- [37] H. M. Rietveld, "A Profile Refinement Method for Nuclear and Magnetic Structures," *Journal of Applied Crystallography*, vol. 2, pp. 65-&, 1969.
- [38] J. E. Post and D. L. Bish, "Rietveld Refinement of Crystal-Structures Using Powder X-Ray-Diffraction Data," *Reviews in Mineralogy*, vol. 20, pp. 277-308, 1989.

- [39] I. Accelrys Software, "Materials Studio, Release 5.5," ed: Accelrys Software, Inc. San Diego, CA, 2009.
- [40] X. Q. Wu, H. L. Wang, and J. G. Lin, "Effects of Sn content on thermal stability and mechanical properties of the Ti60Zr10Ta15Si15 amorphous alloy for biomedical use," *Materials & Design*, vol. 63, pp. 345-348, 2014.
- [41] J. D. Honeycutt and H. C. Andersen, "Molecular-Dynamics Study of Melting and Freezing of Small Lennard-Jones Clusters," *Journal of Physical Chemistry*, vol. 91, pp. 4950-4963, Sep 10 1987.
- [42] Y. C. Lo, J. C. Huang, S. P. Ju, and X. H. Du, "Atomic structure evolution of Zr-Ni during severe deformation by HA pair analysis," *Physical Review B*, vol. 76, Jul 2007.
- [43] T. Debela, X. Wang, Q. Cao, D. Zhang, S. Wang, C. Wang, and J. Jiang,
 "Atomic structure evolution during solidification of liquid niobium from ab initio molecular dynamics simulations," *Journal of Physics: Condensed Matter*, vol. 26, p. 055004, 2014.
- [44] H. L. Peng, M. Z. Li, W. H. Wang, C.-Z. Wang, and K. M. Ho," Effect of local structures and atomic packing on glass forming ability in Cu_xZr₁₀₀
 _{-x} metallic glasses," *Applied Physics Letters*, 96, 021901, 2010.
- [45] S. Wu, M. Kramer, X. Fang, S. Wang, C. Wang, K. Ho, Z. Ding, and L. Chen, "Structural and dynamical properties of liquid Cu 80 Si 20 alloy studied experimentally and by ab initio molecular dynamics simulations," *Physical Review B*, vol. 84, p. 134208, 2011.
- [46] B. Shen, C. Y. Liu, Y. Jia, G. Q. Yue, F. S. Ke, H. B. Zhao, L. Y. Chen, S. Y. Wang, C. Z. Wang, and K. M. Ho, "Molecular dynamics simulation studies of structural and dynamical properties of rapidly quenched Al," *Journal of Non-Crystalline Solids*, vol. 383, pp. 13-20, 2014.
- [47] M. Aykol, A. O. Mekhrabov, and M. V. Akdeniz, "Nano-scale phase separation in amorphous Fe–B alloys: Atomic and cluster ordering," *Acta Materialia*, vol. 57, pp. 171-181, 2009.
- [48] R. N. Singh and F. Sommer, "Segregation and immiscibility in liquid binary alloys," *Reports on Progress in Physics*, vol. 60, pp. 57-150, Jan 1997.
- [49] F. Shimizu, S. Ogata, and J. Li, "Theory of shear banding in metallic glasses and molecular dynamics calculations," *Materials Transactions*, vol. 48, pp. 2923-2927, Nov 2007.
- [50] J. T. Wang, P. D. Hodgson, J. D. Zhang, W. Y. Yan, and C. H. Yang, "Effects of pores on shear bands in metallic glasses: A molecular dynamics study," *Computational Materials Science*, vol. 50, pp. 211-217, Nov 2010.
- [51] K. Albe, Y. Ritter, and D. Şopu, "Enhancing the plasticity of metallic glasses:

Shear band formation, nanocomposites and nanoglasses investigated by molecular dynamics simulations," *Mechanics of Materials,* vol. 67, pp. 94-103, 2013.

- [52] J. S. C. Jang, S. R. Jian, C. F. Chang, L. J. Chang, Y. C. Huang, T. H. Li, J. C. Huang, and C. T. Liu, "Thermal and mechanical properties of the Zr53Cu30Ni9Al8 based bulk metallic glass microalloyed with silicon," *Journal of Alloys and Compounds*, vol. 478, pp. 215-219, 2009.
- [53] K.-W. Park, E. Fleury, H.-K. Seok, and Y.-C. Kim, "Deformation behaviors under tension and compression: Atomic simulation of Cu65Zr35 metallic glass," *Intermetallics*, vol. 19, pp. 1168-1173, 2011.
- [54] C. C. Wang and C. Wong, "Different icosahedra in metallic glasses: stability and response to shear transformation," *Scripta Materialia*, vol. 66, pp. 610-613, 2012.
- [55] A. Cao, Y. Cheng, and E. Ma, "Structural processes that initiate shear localization in metallic glass," *Acta Materialia*, vol. 57, pp. 5146-5155, 2009.
- [56] H. L. Peng, M. Z. Li, and W. H. Wang, "Structural Signature of Plastic Deformation in Metallic Glasses," *Phys. Rev. Lett.*, 106, 135503, 2011.

$Ti_{60}Zr_{10}Ta_{15}Si_{15}BMGs$							
Туре	Zr-Zr	Zr-Ti	Zr-Ta	Zr-Si	Zr_Total		
N _{ij}	1.13± 1.09	8.11± 1.97	2.11± 1.28	2.28± 1.24	13.63± 1.65		
Туре	Ti-Zr	Ti-Ti	Ti-Ta	Ti-Si	Ti_Total		
N _{ij}	1.39± 1.11	7.31± 1.85	2.12± 1.11	1.73± 1.15	12.55± 1.51		
Туре	Ta-Zr	Ta-Ti	Ta-Ta	Ta-Si	Ta_Total		
N _{ij}	1.40± 1.06	8.11± 1.94	1.51± 1.09	1.83± 1.07	12.84± 1.57		
Туре	Si-Zr	Si-Ti	Si-Ta	Si-Si	Si_Total		
N _{ij}	1.44± 1.14	7.05± 1.70	1.87± 0.90	0.69± 0.83	11.04± 1.76		

Table I. Average coordination numbers (CNs) for Zr, Ti, Ta and Si atoms and each pair in $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG.

Ti ₆₀ Zr ₁₀ Ta ₁₅ Si ₁₅ BMG							
Туре	Zr-Zr	Zr-Ti	Zr-Ta	Zr-Si			
α_{ij}	0.171	0.008	-0.032	-0.115			
Туре	Ti-Zr	Ti-Ti	Ti-Ta	Ti-Si			
α_{ij}	-0.108	0.029	-0.126	0.081			
Туре	Ta-Zr	Ta-Ti	Ta-Ta	Ta-Si			
α_{ij}	-0.090	-0.053	0.216	0.050			
Туре	Si-Zr	Si-Ti	Si-Ta	Si-Si			
α_{ij}	-0.304	-0.064	-0.129	0.583			

Table II. CSRO parameters (α_{ij}) for all atomic pairs of Ti₆₀Zr₁₀Ta₁₅Si₁₅ BMG.



Fig. 1. Structures of (a) unit cell and (b) tensile test model for $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG.



Fig. 2. (a) Simulated XRD pattern and (b) RDF profile for the $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG.

Fig. 3. (a) Schematic diagrams corresponding to several characteristic HA indexes; (b) HA index numbers for $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG.



Fig. 4. The HA indexes for different pairs of the $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG.



Fig. 5. The Voronoi index and the center atom composition for different pairs in the $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG.



Fig. 6. The stress – strain curve and $\Delta V/V$ for Ti₆₀Zr₁₀Ta₁₅Si₁₅ BMG.



Fig. 7. The distribution of atomic local shear strain.



Fig. 8. The HA indexes at different strains for $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG.







Fig. 9. The HA indexes at different strains for different pairs of $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG.



Fig. 10. The Voronoi indexes at different strains for $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG.



Fig. 11. Notable changes in center atoms for four Voronoi indexes at different strain for $Ti_{60}Zr_{10}Ta_{15}Si_{15}$ BMG.