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1 **Suspended Growth Kinetic Analysis on Biogas Generation from Newly Isolated**  
2 **Anaerobic Bacterial Communities for Palm Oil Mill Effluent at Mesophilic**  
3 **Temperature.**

4  
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13

14 **Abstract**

15 The anaerobic degradation of palm oil mill effluent (POME) was carried out under  
16 mesophilic temperature in anaerobic suspended growth closed bioreactor (ASGCB). Monod  
17 model was applied to describe the kinetic analysis of POME at different organic loading rates  
18 (OLR) in the range of 2.75 - 8.2 g TCOD/L day. The hydraulic retention time (HRT) was  
19 ranged between 8 and 24 days. The TCOD removal efficiency was achieved between 89.66%  
20 and 79.83%. The evaluated kinetic coefficients were: growth yield,  $Y_G$  (0.357 gVSS/ g  
21 TCOD), specific biomass decay rate,  $b$  (0.07/day), maximum specific biomass growth rate,  
22  $\mu_{max}$  (0.27/day), saturation constant for substrate,  $K_s$  (25.03 g TCOD/L), critical retention  
23 time,  $\Theta_c$  (3.72 day) and methane yield,  $Y_{CH_4}$  (0.34 L CH<sub>4</sub>/ TCOD<sub>removed</sub>), respectively.  
24 Besides, new fermentative anaerobic bacteria isolated from POME were identified as  
25 *Escherichia fergusonii*, *Enterobacter asburiae*, *Enterobacter cloacae*, *Desulfovibrio*

26 *aerotolerans*, *Desulfobulbus propionicus*, *Fusobacterium nucleatum*, *Paenibacillus pabuli*,  
27 *Bacillus subtilis*, *Methanobacterium sp.*, *Methanosaeta concilii*, *Methanofollis tationis*,  
28 *Methanosarcina mazei* and *Methanosarcina acetivorans* using 16S rDNA.

29 **Keywords:** Anaerobic Processes; Biodegradation; Biogas; Kinetics; DNA; Mesophilic.

30

### 31 **Nomenclature**

32	b	Specific biomass decay (1/day)
33	$r_x$	Specific substrate utilization rate (g TCOD/g VSS day)
34	$r_v$	Substrate utilization rate per volume (g TCOD/ day)
35	$r_{x,max}$	Maximum specific substrate utilization (g TCOD/g VSS day)
36	t	Time (day)
37	ASGCB	Anaerobic Suspended Growth Closed Bioreactor
38	Alk	Total Alkalinity
39	BOD	Biochemical Oxygen Demand (mg/L)
40	CO <sub>2</sub>	Carbon Dioxide Gas
41	CH <sub>4</sub>	Methane Gas
42	D	Dilution rate, 1/HRT (1/day)
43	DNA	Deoxyribonucleic Acid
44	HRT	Hydraulic Retention Time (day)
45	H <sub>2</sub>	Hydrogen Gas
46	H <sub>2</sub> S	Hydrogen Sulfide Gas
47	K <sub>s</sub>	Saturation constant for substrate (g TCOD/L)
48	L	Liter
49	NH <sub>3</sub> -N	Ammonia Nitrogen (mg/L)
50	O & G	Oil and Grease (mg/L)

51	OLR	Organic Loading Rate (g TCOD / L day)
52	PCR	Polymerase Chain Reaction
53	POME	Palm Oil Mill Effluent
54	Q	Volumetric Flow rate (L/day)
55	S	Substrate concentration in the reactor (mg/L)
56	S <sub>1</sub>	Influent substrate concentration (mg/L)
57	S <sub>2</sub>	Effluent substrate concentration, (mg/L)
58	SCOD	Soluble Chemical Oxygen Demand (mg/L)
59	SRT	Solid Retention Time
60	SS	Suspended Solid (mg/L)
61	TCOD	Total Chemical Oxygen Demand (mg/L)
62	TN	Total Nitrogen (mg/L)
63	TS	Total Solid (mg/L)
64	TVS	Total Volatile Solid (mg/L)
65	V	Reactor volume (L)
66	V <sub>CH<sub>4</sub></sub>	Methane Gas Volume (L)
67	VFA	Volatile Fatty Acid (mg/L)
68	VSS	Volatile Suspended Solid (mg/L)
69	X	Biomass concentration in the reactor, (mg/L)
70	Y <sub>G</sub>	Growth yield (g VSS/g TCOD <sub>removed</sub> )
71	Y <sub>CH<sub>4</sub></sub>	Methane yield (L CH <sub>4</sub> /TCOD <sub>removed</sub> )
72	<b>Greek letter</b>	
73	μ <sub>max</sub>	Maximum specific biomass growth rate (1/day)
74	Θ <sub>c</sub>	Critical retention time (day)
75	μ	Specific biomass growth rate (1/day)

## 76 1. Introduction

77 Palm oil industry produces high strength organic wastewater known as Palm Oil Mill  
78 Effluent (POME). POME is a viscous, brownish liquid containing about 95-96% water, 0.6-  
79 0.7% oil and 4-5% total solids (including 2-4% SS, mainly debris from fruit). It is acidic (pH  
80 4-5), hot (80-90°C) with average Chemical Oxygen Demand (COD) and Biochemical  
81 Oxygen Demand (BOD) values of 50,000 mg/L and 25,000 mg/L, respectively [1].

82 Anaerobic digestion has often been used for high strength organic wastewater, since it  
83 produces less sludge compared to conventional aerobic treatment. An advantage of anaerobic  
84 treatment is operational cost effectiveness with simultaneous production of methane or  
85 hydrogen gas as energy resource. Anaerobic treatment is a complex process which involves  
86 decomposition of organic compounds and production of methane, hydrogen and carbon  
87 dioxide gases in the absence of molecular oxygen. The degradation process takes place by  
88 different types of anaerobic bacteria. The degradation mechanisms involve hydrolysis,  
89 acidogenesis (including acetogenesis) and methanogenesis [2]. Hydrolysis is the conversion  
90 reaction in which complex molecules such as carbohydrate, lipids and protein are converted  
91 into sugar, organic acids and etc. Acidogenic bacteria are responsible for breaking down the  
92 sugar, fatty acids and amino acids in acidogenesis process. Methanogenesis process occurs in  
93 which hydrogenotropic methanogens utilize the hydrogen and carbon dioxide gases produced  
94 by acetoclastic methanogens from short chain fatty acids to produce beneficial end product of  
95 methane gas [3].

96 For better control of degradation process with high operational efficiency,  
97 identification of microbial community of anaerobic digestion process is an essential  
98 requirement [4]. Currently only few anaerobic bacteria such as *Clostridium* spp.,  
99 *Streptococcus cohnii* spp., *Lactobacillus* and *Thermoanaerobacterium* spp. have been  
100 reported with hydrogen producing ability from palm oil wastewater [5,6,7]. However,

101 hitherto no work regarding anaerobic bacteria with methane producing ability from palm oil  
102 wastewater has been reported. Kinetic study is required for a better understanding of the  
103 underlying phenomena in the anaerobic digestion process. Among many important  
104 applications, it can predict the compounds produced or consumed on their corresponding  
105 rates. The process kinetics for the anaerobic digestion are composed of several aspects.  
106 Firstly, there are the mass balance models involving input and output streams of the  
107 anaerobic system. Secondly, the selected model of flow or hydraulic must be formed for the  
108 anaerobic process. Finally, the selection of kinetic model for the reaction and stoichiometry  
109 can be conducted to determine the kinetic coefficients. Numerous kinetic models for  
110 anaerobic digestion such as Monod, First-order, Second-order, Modified Stover-Kinannon,  
111 Contois, Chen and Hashimoto have been proposed [8].

112 The literature study is abound with results of research on attached growth anaerobic  
113 treatment such as immobilised cell bioreactor [9], two stage up-flow anaerobic sludge blanket  
114 (UASB) [10], high rate up-flow anaerobic sludge fixed film [11], and combined high-rate  
115 anaerobic reactors [12] for the treatment of POME. Little research has been conducted on the  
116 application of anaerobic suspended growth process and also identification of anaerobe  
117 bacteria from POME for better control of the degradation process. Therefore, the aim of the  
118 present work was focused on the identification of anaerobic bacteria and kinetic coefficients  
119 for the anaerobic digestion of POME using suspended growth closed bioreactor.

120

## 121 **2. Materials and Methods**

### 122 *2.1 Wastewater preparation*

123 The raw POME was collected by onsite sampling from MALPOM Industries Bhd, in  
124 Nibong Tebal, Penang, Malaysia. The seeding required to acclimatize the Anaerobic  
125 Suspended Growth Closed Bioreactor (ASGCB) was taken from the anaerobic pond of

126 MALPOM Industries Bhd wastewater treatment plant. The composition and properties of the  
127 collected POME used in the present study are summarized in Table 1. The POME was stored  
128 in the refrigerator at 4°C until further experimental work was conducted. This storage  
129 observed no change of composition.

130

### 131 *2.2 ASGCB set-up*

132 The schematic configuration of the ASGCB set-up is shown in Figure 1. The ASGCB  
133 is 0.25 m in diameter and 0.36 m in height. The reactor consists of a cylindrical-shape flexi  
134 glass vessel with total and working volumes of 17.7 L and 14 L, respectively. It comprises an  
135 integrated on-line pH data recording system connected to a pH probe and an overhead stirrer.  
136 The operating temperature of ASGCB was maintained constant at 35 °C using thermal  
137 jacket. The ASGCB has a gas sampling valve (or clamp) which allows gas samples to be  
138 collected without interference with head space composition and is connected to a 50 L gas  
139 collection bag.

140

### 141 *2.3 Bacteria Cultivation and Isolation*

142 Cultivation of bacteria was conducted according to isolation techniques of  
143 microbiology [13]. The culture medium contained (in g/L): Heart Extract and Peptone 20;  
144 Yeast Extract 5.0; Sodium Chloride 5.0; Bacteriological Agar 15; Sodium Thioglycollate 2.0  
145 and Sodium Formaldehyde Sulfoxylate 1.0. The pH of the medium was adjusted to pH 7.0  
146  $\pm 0.1$  with 1 N Sodium Hydroxide (NaOH) or 0.1 N of Hydrochloric Acid (HCl) by using pH  
147 meter (Metrohm, 826 pH Mobile). The medium was sterilized at 121°C for 15 minutes.  
148 Isolation of bacteria in the sample was done with serial dilution where one mL of the sample  
149 was diluted with 9 mL of sterile saline water. The dilution was repeated until the colonies on  
150 the agar plate was countable. Pure isolates were then stored on culture medium at 4 °C until

151 further analysis. The cultivation and isolation were done in the Anaerobic Chamber (Fisher  
152 Scientific, Forma Anaerobic System) at 35 °C.

153

## 154 2.4 Molecular identification of isolates

### 155 2.4.1 DNA extraction and PCR amplification

156 The bacteria genomic DNA was extracted by using I-genomic DNA extraction kit (QIAGEN)  
157 according to the manufacturer's instruction from the cultivated medium. Then, PCR  
158 amplification of 16S rDNA was conducted using the amplification kit (PROMEGA)  
159 according to the manufacturer's operation procedure. The amplification reaction was done in  
160 a 50 µL tube with mixtures of 10 µL of 5X colorless GoTaq buffer, 1mM of MgCl<sub>2</sub>, 0.1 mM  
161 of dNTP, 0.5 µM forward primer, 0.5 µM reverse primer, 0.02 units of Taq DNA polymerase  
162 and nuclease-free water. Two types of primer pair were applied by using universal primer of  
163 27F and 1492R (27F: AGA GTT TGA TCM TGG CTC AG ; 1492R: CGG TTA CCT TGT  
164 TAC GAC TT) and archaea primer of ARC344F and ARC915R (ARC344F: ACG GGG  
165 YGC AGC AGG GGC GA; ARC915R: GTG CTC CCC CGC CAA TTC CT). The PCR  
166 amplification was 2 min at 95 °C followed by 34 cycles of denaturation at 95 °C for 50s,  
167 annealing at 58 °C for 45s, elongation at 72 °C at 45s and the final elongation at 72 °C for 8  
168 minutes. The PCR amplification procedures for archaea were set similar to that of bacteria  
169 with only difference in the annealing temperature at 54 °C for 1 min. The PCR products were  
170 then analyzed with 1% agarose gel electrophoresis (AGE).

171

### 172 2.4.2 Bacteria Identification based on 16S rDNA sequences

173 The PCR products were sent to the Genomics BioScience and Technology Co., Ltd. in  
174 Malaysia for 16S rDNA sequence analysis. The clone libraries were finally built based on the  
175 obtained sequences. The obtained sequences were analyzed through the gene bank database

176 of National Center for Biotechnology Information (NCBI) for highest similarity identification  
177 of bacteria. The maximum bacteria identity was determined through the Basic Local  
178 Alignment Search Tool (BLAST) between the similarity identification of aligned sequence  
179 nucleotides and nucleotides stored in the gene bank database.

180

### 181 *2.5 ASGCB experimental procedure*

182 The seeding required for starting the ASGCB was taken from the anaerobic pond of  
183 MALPOM Industries Bhd Penang, Malaysia wastewater treatment plant. About 14 liters of  
184 the anaerobic digested POME were used to acclimatize the laboratory ASGCB. The start-up  
185 of the ASGCB involved step increases of the influent organic volumetric loading rates from  
186 2.72 g COD/L/day to 6.55 g COD/L/day. This acclimatization phase was important to allow  
187 the microorganisms present in the mixed liquor perfectly acclimatize to the new environment  
188 and reach a steady state condition before proceeding to the next phase of research studies.  
189 The pH in the ASGCB was adjusted to  $7.50 \pm 0.05$  using 1 N Sodium Hydroxide (NaOH).

190 Once the start-up phase has been completed, a series of continuous experiments using  
191 feed flow-rates of 0.58, 0.7, 0.88, 1.17 and 1.75 liters of raw POME per day, corresponding  
192 to Hydraulic Retention Time (HRT) of 24, 20, 16, 12 and 8 days was followed. The rate of  
193 influent substrate concentration of TCOD was controlled in the range of 62500-65500 mg/L.  
194 Biogas and samples from ASGCB were collected for analysis after 24 hours of input raw  
195 POME. For each batch of HRT, the ASGCB was continuously operated until steady state  
196 condition was achieved. The steady-state condition was reached once the values of TCOD  
197 removal efficiency, VFA, biogas production rate and biogas composition remained  
198 unchanged for five consecutive days. The variation of the actual results from the mean values  
199 was  $<3\%$ .

200

## 201 2.6 Analytical method

202 The TCOD of a sample was measured using reactor digestion method (HACH, range:  
203 20 - 1500 mg/L) for two hours at 150 °C. The MLSS, MLVSS, O & G, NH<sub>3</sub>-N, VFA and Alk  
204 were determined according to the Standard Methods for the Examination of Water and  
205 Wastewater (APHA, 2005). Daily biogas production was recorded using Binder  
206 COMBIMASS gas analyzer consisted of five gas channels: CO<sub>2</sub>, CH<sub>4</sub>, O<sub>2</sub>, H<sub>2</sub>S and H<sub>2</sub>. The  
207 volatile fatty acids such as acetic, propanoic, butanoic and iso-butanoic were extracted from  
208 the sample using 10% phosphoric acid (H<sub>3</sub>PO<sub>4</sub>) and methanol. The extracted samples were  
209 analyzed by Shimadzu GCMS QP 2010 Plus equipped with SGE BP21 capillary column (25  
210 m length, 0.22 mm internal diameter and 0.25 µm thickness). Helium was used as the carrier  
211 gas. The injection temperature was 220 °C and the column temperature was initially held at  
212 120 °C for 6 minutes then was raised progressively at 15 °C/minute until 220 °C. The carbon,  
213 hydrogen, nitrogen, sulfur and oxygen contents of POME wastewater were measured by  
214 elemental analyzer (PerkinElmer 2400 Series II CHNS/O).

215

## 216 2.7 Kinetic model development

### 217 2.7.1 Substrate balance model

218 Determination of kinetic coefficients can be done on the specific parameters of the  
219 system performance. Different kinetic models were used for different biological systems to  
220 evaluate kinetic coefficients. For this purpose, various kinetic models such as Monod, Stover-  
221 Kincannon, Michaelis-Menten, first order and second order have been applied. In the present  
222 study, the mass balance, reaction rate equation and Monod models were used. The equations  
223 describing the performance of the system are the mass balance equations of both the substrate  
224 and biomass.

225

## 226 2.7.2 Mass balance equation

227 The substrate balance can be expressed as (1):

228 
$$\frac{dS}{dt} = \frac{Q(S_1 - S_2)}{V} - r_v \quad (1)$$

229 where, S = substrate concentration in the reactor, Q = volumetric flow rate, S<sub>1</sub> = influent  
 230 substrate concentration, S<sub>2</sub> = effluent substrate concentration (S<sub>2</sub> = S), V = working volume,  
 231 r<sub>v</sub> = substrate utilization rate per volume, and t = time.

232

233 Once the reactor was completely mixed and continuously fed without recycle,  $\frac{dS}{dt} = 0$ .

234 Equation (1) then becomes:

235 
$$r_v = (S_1 - S_2) D \quad (2)$$

236 where, D = dilution rate =  $\frac{Q}{V} = \frac{1}{HRT}$ 

237 The specific substrate utilization rate, r<sub>X</sub> is defined as  $r_X = \frac{r_v}{X}$ , where X = biomass  
 238 concentration in the reactor:

239 
$$r_X = \frac{(S_1 - S_2) D}{X} \quad (3)$$

240 On the other hand, the biomass balance gives:

241 
$$\frac{dX}{dt} = \frac{-QX}{V} + \mu X \quad (4)$$

242 where, μ = specific biomass growth rate. At steady state,  $\frac{dX}{dt} = 0$ . Hence, Equation (4) yields

243 
$$\mu = D = \frac{1}{HRT} \quad (5)$$

244 The growth of microorganism is proportional to the substrate utilization. Biomass  
 245 decay or endogenous metabolism should also be taken into account to describe the specific  
 246 growth rate [11]:

$$247 \quad \mu = Y_G r_X - b \quad (6)$$

248 where,  $Y_G$  = growth yield coefficient and

249  $b$  = specific biomass decay coefficient.

250

251 Combining Equations (5) and (6) gives:

$$252 \quad D = Y_G r_X - b \quad (7)$$

253 or

$$254 \quad r_X = \frac{D}{Y_G} + \frac{b}{Y_G} \quad (8)$$

### 255 2.7.3 Reaction Rate equation

256 Several types of reaction rate equations have been proposed to describe the  
 257 relationship between the growth rate and the substrate utilization. Monod equation is the  
 258 simplest and well known in biological treatment system [10]. The Monod equation is:

$$259 \quad r_X = \frac{S}{K_S + S} r_{X,\max} \quad (9)$$

260 where,  $r_{X,\max}$  = maximum specific substrate utilization rate,  $K_S$  = saturation constant for  
 261 substrate, and  $S$  = substrate concentration in the reactor.  $r_X$  is half of  $r_{X,\max}$  when the substrate  
 262 concentration is  $K_S$ . Equation (9) can be rearranged to the following three types of linear  
 263 equation to obtain  $r_{X,\max}$  and  $K_S$  from experimental data of  $r_X$  and  $S$ .

$$264 \quad \frac{1}{r_X} = \left( \frac{K_S}{r_{X,\max}} \right) \left( \frac{1}{S} \right) + \frac{1}{r_{X,\max}} \quad \text{Lineweaver-Burk plot} \quad (10)$$

$$265 \quad r_X = r_{X,\max} - K_S \left( \frac{r_X}{S} \right) \quad \text{Eadie plot} \quad (11)$$

$$266 \quad \frac{S}{r_X} = \frac{S}{r_{X,\max}} + \frac{K_S}{r_{X,\max}} \quad \text{Hofstee plot} \quad (12)$$

267 The maximum specific biomass growth rate,  $\mu_{\max}$ , is obtained by substituting  $r_{X,\max}$  for  $r_X$  in  
 268 Equation (6):

$$269 \quad \mu_{\max} = Y_G r_{X,\max} - b \quad (13)$$

270 Critical retention time  $\Theta_C$  is a safety factor for anaerobic degradation process where substrate  
 271 utilization does not happen but bacteria washout could happen if the reactor is loaded below  
 272 the critical retention time [10].  $\Theta_C$  can be expressed as:

$$273 \quad \Theta_C = \frac{1}{\mu_{\max}} \quad (14)$$

274

#### 275 *2.7.4 Methane yield*

276 Methane yield is a vital economic factor for the anaerobic digestion process. In most  
 277 cases, the methane yield coefficient,  $Y_{CH_4}$  is determined from experimental data. If the  
 278 volume of methane gas produced,  $V_{CH_4}$  is assumed to be proportional to the amount of  
 279 substrate consumed, then Equation (15) is formed:

$$280 \quad V_{CH_4} = Y_{CH_4} Q(S_1 - S_2) \quad (15)$$

281 A plot of  $V_{CH_4}$  versus  $Q(S_1 - S_2)$  should yield a straight line passing through the origin with a  
 282 slope equal to  $Y_{CH_4}$ .

283

### 284 **3. RESULTS AND DISCUSSION**

#### 285 *3.1 Bacteria Identification*

286 Bacteria cultivation and isolation processes were conducted from the ASGCB mix  
 287 sludge samples at the end of each batch operating HRT. Table 2 summarizes the microbial  
 288 identification of ASGCB mix sludge sample by using 16S rDNA. Eight types of bacteria and  
 289 five types of archaea were obtained. The 16S rDNA data of ASGCB sample illustrates that

290 the microorganisms consisted of *Phylum Proteobacteria* (38.5%), *Firmicutes* (15.4%),  
291 *Fusobacteria* (7.6%) and *Euryarchaeota* (38.5%).

292 *Escherichia fergusonii*, *Enterobacter asburiae* and *Enterobacter cloacae* which  
293 belong to the family of *Enterobacteriaceae* were identified in the ASGCB. These types of  
294 bacteria are known to produce hydrogen gas from carbohydrates and fatty acids [14,15].  
295 Sulfur-reducing anaerobe bacteria such as *Desulfovibrio aerotolerans*, *Desulfobulbus*  
296 *propionicus*, *Fusobacterium nucleatum*, *Paenibacillus pabuli* and *Bacillus subtilis* were also  
297 obtained. These types of bacteria survived with sulfur content in POME wastewater in the  
298 ASGCB (Table 1). To our knowledge this is the first report that *Fusobacterium nucleatum*,  
299 *Paenibacillus pabuli* and *Bacillus subtilis* as sulfur-reducing bacteria are present in the  
300 anaerobic process of POME wastewater. The sulfur-reducing bacteria consumed of sulfur as  
301 the electron acceptor to form hydrogen sulfide gas (H<sub>2</sub>S) from the hydrogen gas (H<sub>2</sub>) as the  
302 electron donor [16,17,18,19]. Therefore, high concentration of H<sub>2</sub>S gas was obtained from the  
303 anaerobic degradation process (Table 3). Low H<sub>2</sub> gas production was detected as most of the  
304 hydrogen ion had been used to form H<sub>2</sub>S gas (Table 3).

305 High contents of fatty acids were characterized from POME wastewater (Table 1).  
306 Therefore, five species of methane producing bacteria such as *Methanofollis ationis*,  
307 *Methanobacterium sp.*, *Methanosaeta concilii*, *Methanosarcina mazei*, and *Methanosarcina*  
308 *acetivorans* have been obtained in ASGCB. The methanogenic archaea bacteria converted  
309 acetates into methane gas (CH<sub>4</sub>) and carbon dioxide gas (CO<sub>2</sub>) [20,21]. Perhaps, the presence  
310 of the identified microbial community in the ASGCB played an important role in degrading  
311 POME in the complex anaerobic degradation processes.

312

313

314

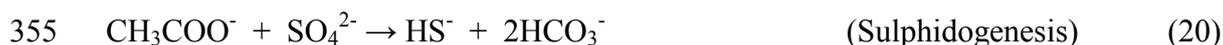
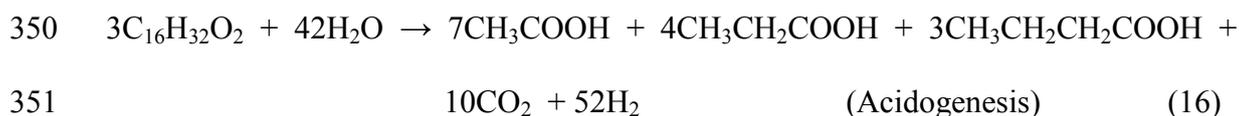
315 *3.2 Operational parameters and biodegradability of POME wastewater in ASGCB*

316 Table 3 summarizes the results obtained under various HRT. An analysis of variance  
317 (ANOVA) was conducted to test the significance of experimental data at different HRT in  
318 Table 3. Table 4 states the outcome of ANOVA test as F-value and p-value for each  
319 operational variables under various HRT. High F-value with low p-value ( $< 0.05$ ) was  
320 obtained through ANOVA significant test. Therefore, the operational results are statistically  
321 proven to be significant in the present study [22,23].

322 Throughout the study, the organic loading rates were varied from 2.75 g TCOD/L/d to  
323 8.2 g TCOD/L/d. At each HRT, the operational parameters were operated until steady state  
324 was reached as indicated by a constant effluent TCOD, biogas production, total VFA,  
325 alkalinity, and MLVSS level. The effluent TCOD of the reactor increased as the HRT  
326 reduced. This is due to the increase of input organic loading rates as the volumetric flow rate  
327 of POME was increased. On the other hand, the anaerobic degradation process of POME is  
328 operated without acidification risk in the ASGCB with the level of VFA/Alk between 0.05  
329 and 0.50. The VFA/Alk levels fall between the recommended condition of 0.3 - 0.5 whereby  
330 this process is considered to be operating favorably in anaerobic condition [24,25]. The level  
331 of alkalinity reduced from 11400 mg  $\text{CaCO}_3/\text{L}$  to 7650 mg  $\text{CaCO}_3/\text{L}$  as the HRT reduced.  
332 The high level of bicarbonate alkalinity was reached in the reactor due to the reaction of  
333 ammonia with carbon dioxide and water in forming ammonium bicarbonate [26]. The mixed  
334 liquor volatile suspended solid (MLVSS) inside the ASGCB was analyzed as the microbial  
335 growth or biomass concentration. The MLVSS varied from 7610 mg MLVSS/L to 11570 mg  
336 MLVSS/L. This result proves that the anaerobic degradation of POME could be well  
337 performed as the increase of microbial growth with increasing organic loading rate (OLR).

338 The daily biogas production increased from 12.90 L/d to 30.81 L/d with increasing  
339 OLR. This is because the POME was characterized with high concentration of palmitic fatty

340 acids as stated in Table 1. Palmitic acids containing 16 carbons long-chain fatty acid  
 341 decomposed faster to shorter chain fatty acids such as acetic; propanoic; butanoic; iso-  
 342 butanoic and etc. The identified anaerobic bacteria *Escherichia fergusonii*, *Enterobacter*  
 343 *asburiae*, *Enterobacter cloacae*, *Desulfovibrio aerotolerans*, *Desulfobulbus propionicus*,  
 344 *Fusobacterium nucleatum*, *Paenibacillus pabuli*, *Bacillus subtilis*, *Methanobacterium sp.*,  
 345 *Methanosaeta concilii*, *Methanofollis tationis*, *Methanosarcina mazei* and *Methanosarcina*  
 346 *acetivorans* further decomposed the fatty acids to produce methane (CH<sub>4</sub>), carbon dioxide  
 347 (CO<sub>2</sub>), hydrogen (H<sub>2</sub>) and hydrogen sulfide (H<sub>2</sub>S) gases through acidogenesis, acetogenesis  
 348 and methanogenesis of anaerobic degradation pathway. The anaerobic degradation reactions  
 349 are:



357

358 The contents of the CH<sub>4</sub>, CO<sub>2</sub>, H<sub>2</sub> and H<sub>2</sub>S produced during the steady-state period at  
 359 different HRTs are shown in Table 3. The CH<sub>4</sub> content decreased from 72.5 % to 65.9 % with  
 360 decrease of HRT. A decrease in CH<sub>4</sub> content is caused by an increase of the VFA level and  
 361 poor performance of effluent TCOD. This is because high OLR was characterized by high  
 362 concentration of VFA at the low HRT. These results are in agreement with the finding by  
 363 Hikmet [27] who reported that the CH<sub>4</sub> content decreased with TCOD removal efficiency  
 364 and decrease in HRT.

### 365 3.3 Evaluation of kinetic coefficients

#### 366 3.3.1 Kinetic coefficients $Y_G$ and $b$

367 The experimental data under steady state condition (Table 3) were analyzed and  
368 biological kinetic models were tested. The growth yield ( $Y_G$ ) and specific biomass decay ( $b$ )  
369 were obtained using Equation (8) by plotting  $r_x$  versus  $D$ . As illustrated in Figure 2, the  
370 points fitted well on a straight line with a regression coefficient of 0.99. The values of  $Y_G$  and  
371  $b$  were calculated to be 0.357 gVSS/g TCOD<sub>removed</sub> and 0.07/ day, respectively from the slope  
372 and intercept. The evaluated growth yield,  $Y_G$  was in the range of 0.181 gVSS/g TCOD<sub>removed</sub>  
373 and 0.99 gVSS/g TCOD<sub>removed</sub> as reported in the literature: 0.69 gVSS/g TCOD<sub>removed</sub> [28];  
374 0.174 gVSS/g TCOD<sub>removed</sub> [11]; 0.99 gVSS/g TCOD<sub>removed</sub> [29] and 0.181 gVSS/g  
375 TCOD<sub>removed</sub> [30]. Hitherto, this is due to the similar substrate of POME wastewater was  
376 treated in the anaerobic degradation process.

377

#### 378 3.3.2 $r_{x,max}$ ; $k_s$ ; $\mu_{max}$ and $\Theta_C$ biokinetic coefficients

379 The maximum specific substrate utilization rate ( $r_{x,max}$ ) and saturation constant for  
380 substrate ( $k_s$ ) were obtained through Equation (10) by Lineweaver-Burk plot. By plotting  $1/r_x$   
381 and  $1/S$  data pairs, a straight line with regression coefficient of 0.98 is obtained (Figure 3).  
382 The values of  $r_{x,max}$  and  $k_s$  are 0.957 g TCOD/g VSS day and 25.03 g TCOD/ L, respectively,  
383 from the intercept and slope. The maximum specific biomass growth rate ( $\mu_{max}$ ) and the  
384 critical retention time ( $\Theta_C$ ) are 0.27 day<sup>-1</sup> and 3.72 day, respectively, obtained from  
385 Equations (13) and (14). The value of  $\mu_{max}$  for the substrate of TCOD is close to that of the  
386 reported work of 0.207/day [11] and 0.304/day [31]. This is due to similar activity for  
387 microbial growth in the treatment of POME. The critical retention time,  $\Theta_C$  at which the  
388 washout of microorganisms was 3.72 days for the substrate of TCOD. Thus, the ASGCB was

389 operated without risk to avoid low performance of anaerobic degradation process as the  
390 kinetic analysis experiments were conducted between 24 days and 8 days of retention time.

391 The small values of  $r_{x,max}$ ,  $k_s$  and  $\mu_{max}$  were achieved as the anaerobe bacteria could  
392 easily degrade the organic matters in the input of palm oil wastewater. Therefore, the ASGCB  
393 significantly performed well between 79.83 % and 89.66 % reduction of TCOD with increase  
394 of OLR (Table 3). This significant finding is reflected by the newly isolated anaerobe  
395 bacteria: *Escherichia fergusonii*, *Enterobacter asburiae* , *Enterobacter cloacae*,  
396 *Desulfovibrio aerotolerans*, *Desulfobulbus propionicus* , *Fusobacterium nucleatum*,  
397 *Paenibacillus pabuli*, *Bacillus subtilis*, *Methanobacterium sp.*, *Methanosaeta concilii*,  
398 *Methanofollis tationis*, *Methanosarcina mazei* and *Methanosarcina acetivorans* that are able  
399 to degrade the fatty acid contents of POME wastewater.

400

### 401 3.3.3 Kinetics of methane production

402 The experiment data listed in Table 3 were used to determine the yield of methane,  
403  $Y_{CH_4}$ . By plotting  $V_{CH_4}$  against  $(S_1 - S_2)Q$  in Equation (15), a value of 0.34 L CH<sub>4</sub>/ g  
404 TCOD<sub>removed</sub> was obtained from the slope (Figure 4). In Figure 4, the straight line passing  
405 through the origin with a correlation coefficient of 0.99 suggests the validation of Equation  
406 (15). The value of  $Y_{CH_4}$  of 0.34 L CH<sub>4</sub>/ g TCOD<sub>removed</sub> is reported so far to be the highest  
407 methane yield for palm oil wastewater compared to the previously reported values of 0.325 L  
408 CH<sub>4</sub>/ g TCOD<sub>removed</sub> [9]; 0.325 L CH<sub>4</sub>/ g TCOD<sub>removed</sub> [11] and recently 0.32 L CH<sub>4</sub>/ g  
409 TCOD<sub>removed</sub> [30]. Therefore, the presence of *Methanobacterium sp.*, *Methanosaeta concilii*,  
410 *Methanofollis tationis*, *Methanosarcina mazei* and *Methanosarcina acetivorans* anaerobes  
411 performs well in suspended growth anaerobic process.

412

413

#### 414 4. CONCLUSION

415 New anaerobic bacteria such as *Escherichia fergusonii*, *Enterobacter asburiae* ,  
416 *Enterobacter cloacae*, *Desulfovibrio aerotolerans*, *Desulfobulbus propionicus* ,  
417 *Fusobacterium nucleatum*, *Paenibacillus pabuli*, *Bacillus subtilis*, *Methanobacterium sp.*,  
418 *Methanosaeta concilii*, *Methanofollis tationis*, *Methanosarcina mazei* and *Methanosarcina*  
419 *acetivorans* were isolated from ASGCB. Their presence in the ASGCB produced the highest  
420 ever methane yield at 0.34 L CH<sub>4</sub>/ TCOD<sub>removed</sub>. Monod model obtained for the suspended  
421 growth anaerobic process produces the following biological kinetic coefficients: Y<sub>G</sub> (0.357  
422 gVSS/ g TCOD), b (0.07/day), μ<sub>max</sub> (0.27/day), K<sub>s</sub> (25.03 g TCOD/L) , Θ<sub>c</sub> (3.72 day) and  
423 Y<sub>CH<sub>4</sub></sub> (0.34 L CH<sub>4</sub>/ TCOD<sub>removed</sub>), respectively.

424

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563 **Captions of Figures:**

564 Fig 1 Schematic configuration of the Anaerobic Suspended Growth Closed Bioreactor  
565 (ASGCB)

566 Fig 2 Plot of specific substrate utilization rate,  $r_x$  versus dilution rate,  $D$  (Equation 8)

567 Fig 3 Determination of maximum specific substrate utilization,  $r_{x,max}$  and saturation  
568 constant,  $k_s$  through Lineweaver-Burk plot (Equation 10)

569 Fig 4 Determination of methane yield,  $Y_{CH_4}$  by Equation (15)

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588 Table 1: Composition and properties of POME used

589	<b>Parameter *</b>	<b>Concentration range (mg/L)</b>	<b>Mean</b>
590	pH	4.3 – 4.75	4.5
591	COD	62500 – 65000	63750
592	SCOD	30500 – 34500	32500
593	BOD	31500 – 38500	35000
594	MLSS	35050 – 41090	38070
595	MLVSS	30230 - 34700	32465
596	O & G	15500 – 16600	16050
597	TN	725 – 835	780
598	NH <sub>3</sub> -N	65 - 70	67.5
599	Palmitic Acid	7420 - 7500	7460
600	Acetic Acid	1900 - 2110	2005
601	Propanoic Acid	53.2 - 56	54.6
602	Butanoic Acid	28.6 - 33.4	31
603	Iso- Butanoic Acid	2.8 - 5.8	4.3
604	Carbon (%)	35.8 - 59.5	47.7
605	Hydrogen (%)	5.3 - 9.1	7.2
606	Nitrogen (%)	0.9 - 2.7	1.8
607	Sulfur (%)	0.5 - 1.3	0.9
608	Oxygen (%)	21 - 55	38

609 \* Unit for all parameter is mg/L except pH, carbon, hydrogen, nitrogen, sulfur and oxygen.

Table 2: Microbial community identification in ASGCB.

Microbial Group	Sequence similarity (%)	Accession no.	Phylogenetic affiliation			
			Phylum	Class	Family	
Bacteria	<i>Escherichia fergusonii</i>	99	NR 074902	Proteobacteria	Gammaproteobacteria	Enterobacteriaceae
	<i>Enterobacter asburiae</i>	99	NR 024640	Proteobacteria	Gammaproteobacteria	Enterobacteriaceae
	<i>Enterobacter cloacae</i>	99	NR 044978	Proteobacteria	Gammaproteobacteria	Enterobacteriaceae
	<i>Desulfovibrio aerotolerans</i>	99	NR 043163	Proteobacteria	Deltaproteobacteria	Desulfobulbaceae
	<i>Desulfobulbus propionicus</i>	99	NR 074930	Proteobacteria	Deltaproteobacteria	Desulfovibrionaceae
	<i>Paenibacillus pabuli</i>	99	NR 040853	Firmicutes	Bacilli	Paenibacillaceae
	<i>Bacillus subtilis</i>	99	NR 102783	Firmicutes	Bacilli	Bacillaceae
	<i>Fusobacterium nucleatum</i>	99	NR 074412	Fusobacteria	Fusobacteria	Fusobacteriaceae
Archaea	<i>Methanobacterium sp.</i>	99	NR 102889	Euryarchaeota	Methanobacteria	Methanobacteriaceae
	<i>Methanofollis tationis</i>	99	NR 041717	Euryarchaeota	Methanomicrobia	Methanomicrobiaceae
	<i>Methanosarcina mazei</i>	99	NR 118787	Euryarchaeota	Methanomicrobia	Methanosarcinaceae
	<i>Methanosaeta concilii</i>	99	NR 104707	Euryarchaeota	Methanomicrobia	Methanosaetaceae
	<i>Methanosarcina acetivorans</i>	99	NR 044724	Euryarchaeota	Methanomicrobia	Methanosarcinaceae

Table 3: The stable operation results obtained under various HRT in ASGCB.

Composition	HRT (day)				
	24	20	16	12	8
OLR (g TCOD/ L day)	2.75± 0.01	3.3± 0.06	4.1± 0.05	5.45± 0.06	8.2± 0.05
Volumetric feed flow rate (L POME/ day)	0.583± 0.00	0.7± 0.00	0.875± 0.00	1.167± 0.00	1.75± 0.00
TCOD removal efficiency (%)	89.66± 0.03	86.06± 0.10	85.15± 0.03	84.56± 0.29	79.83± 0.03
Effluent TCOD (mg/ L)	6810± 4.65	9130± 2.90	9720± 2.90	10130± 10.00	13200± 5.85
Inside TCOD (mg/ L )	12650± 5.00	14250± 14.45	16860± 44.80	21270± 36.00	32150± 11.55
Total Alkalinity in ASGCB (mg CaCO <sub>3</sub> /L)	11400± 13.30	10400± 28.90	9160± 5.00	8400± 5.75	7650± 2.90
Total VFA in ASGCB (mg CH <sub>3</sub> COOH/ L)	514.29± 2.50	1017.14± 0.50	2028.57± 0.82	2497.14± 9.80	3860.57± 5.35
VFA:Alk	0.05± 0.01	0.10± 0.01	0.22± 0.01	0.30± 0.01	0.50± 0.01
MLVSS in ASGCB (mg/ L )	7610± 2.90	8220± 28.85	9290± 25.05	10780± 5.05	11570± 5.80
Total Volume Biogas Production (L /day)	17.79± 0.05	19.85± 0.03	23.82± 0.01	32± 0.06	46.76± 0.11
Daily Volume Methane Production, Q <sub>CH<sub>4</sub></sub> (L CH <sub>4</sub> /day)	12.90± 0.06	14.17± 0.06	16.41± 0.06	21.71± 0.05	30.81± 0.05

Methane Gas (CH <sub>4</sub> ) %	72.50± 0.03	71.40± 0.29	68.90± 0.15	67.90± 0.30	65.90± 0.26
Carbon Dioxide Gas (CO <sub>2</sub> ) %	27.30± 0.25	28.40± 0.11	31± 0.23	31.80± 0.06	33.90± 0.06
Hydrogen Sulfide Gas (H <sub>2</sub> S) (mg /L)	1825± 3.00	3245± 5.05	5820± 28.80	6975± 15.25	12370± 5.25
Hydrogen Gas (H <sub>2</sub> ) (mg/ L)	214± 0.50	488± 0.55	717± 0.50	1998± 0.55	3841± 0.55

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± Standard Deviation

Table 4: Analysis of variance (ANOVA) for the anaerobic degradation in ASGCB.

Factors	Statistics		
	F-value	p-value	Remark
TCOD removal efficiency	48.08	$6.15 \times 10^{-3}$	Significant
Effluent TCOD	49.22	$5.95 \times 10^{-3}$	Significant
Reactor TCOD	87.76	$2.58 \times 10^{-3}$	Significant
Total Alkalinity in ASGCB	284.76	$4.53 \times 10^{-4}$	Significant
Total VFA in ASGCB	97.22	$2.22 \times 10^{-3}$	Significant
VFA:Alk	230.09	$6.22 \times 10^{-4}$	Significant
MLVSS inside ASGCB	70.21	$3.57 \times 10^{-3}$	Significant
Total Biogas Production	54.94	$5.08 \times 10^{-3}$	Significant
Daily volume Methane Production	50.36	$5.76 \times 10^{-3}$	Significant
Methane Gas	96.43	$2.25 \times 10^{-3}$	Significant
Carbon dioxide Gas	27.37	$4.24 \times 10^{-2}$	Significant
Hydrogen Sulfide Gas	27.37	$1.36 \times 10^{-2}$	Significant
Hydrogen Gas	251.13	$5.46 \times 10^{-4}$	Significant

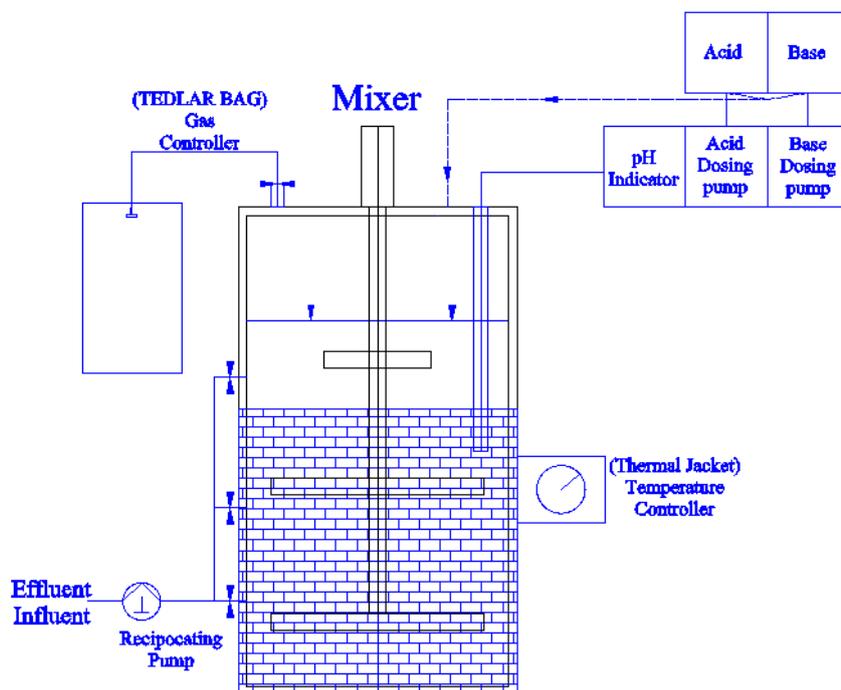


Figure 1: Schematic configuration of the Anaerobic Suspended Growth Closed Bioreactor (ASGCB)

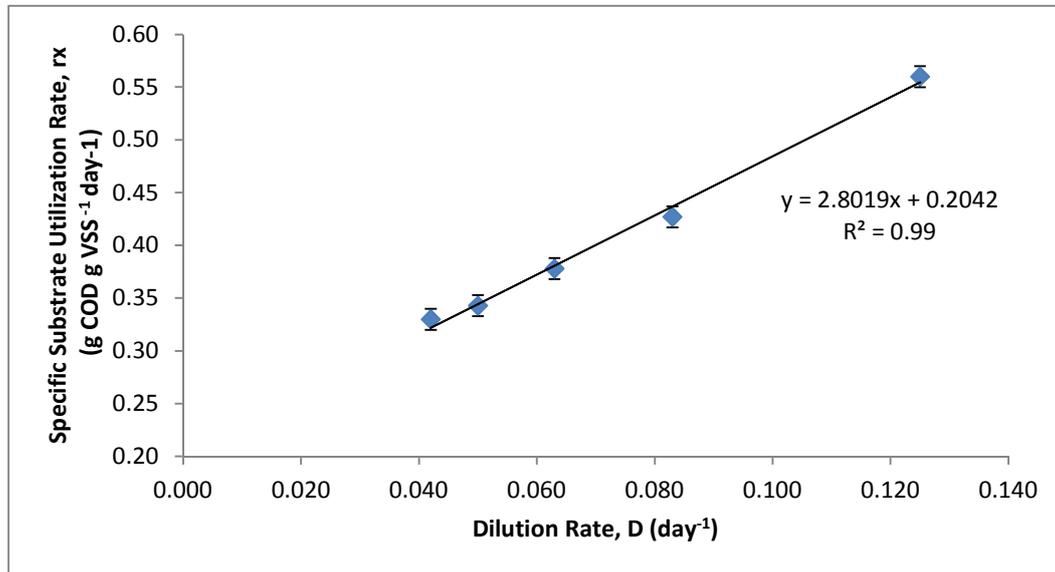


Figure 2: Plot of specific substrate utilization rate,  $r_x$  versus dilution rate,  $D$  (Equation 8).

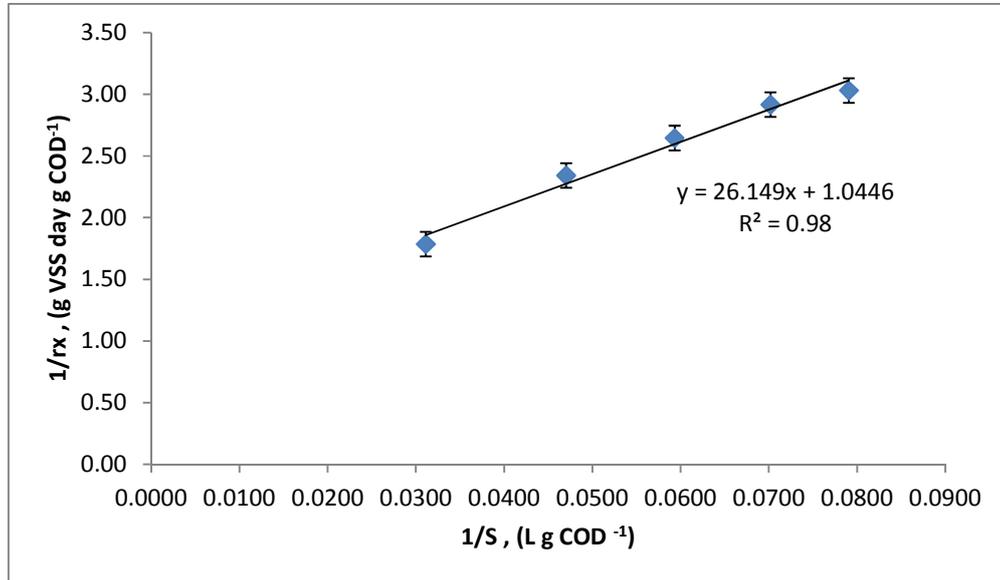


Figure 3: Determination of maximum specific substrate utilization,  $r_{x,\max}$  and saturation constant,  $k_s$  through Lineweaver-Burk plot (Equation 10)

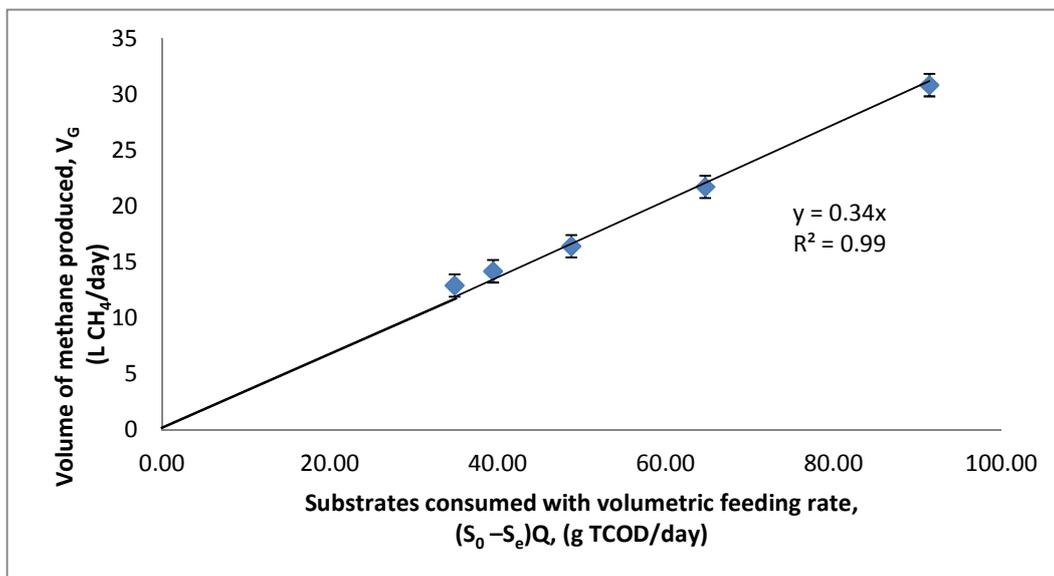


Figure 4: Determination of methane yield,  $Y_{CH_4}$  by Equation (15).