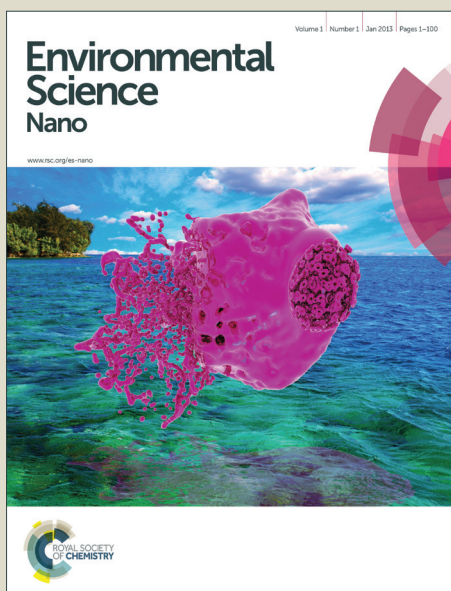


# Environmental Science Nano

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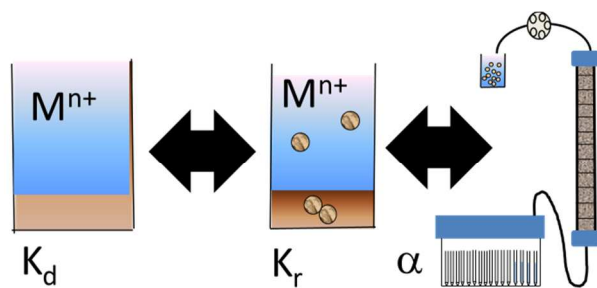


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Analyzing three existing fate descriptors for engineered nanoparticles highlights the need for a new mindset to calculate available concentrations.

**Fate descriptors for engineered nanoparticles: the good, the bad, the ugly**

Cornelis, Geert

**Nano impact statement**

Developments of risk assessment of engineered nanoparticles (ENP) have one-sidedly occurred on hazard assessments, whereas exposure assessments are lagging behind. Quite some discussion has therefore occurred in the regulatory arena, e.g. in OECD expert workshops, what proper fate descriptors should be used for environmental ENP risk assessment. The current perspective nurtures this discussion by comparing and evaluating three ENP fate descriptors that have been suggested in the literature and in workshops. While technical arguments favor column tests, practical ones favor batch test, because any successful fate descriptor should not require many new parameters to be determined. This perspective aims to balance these two perspectives, to further possible research efforts towards fate descriptors balanced in accuracy and practical use.

# 1 Fate descriptors for engineered nanoparticles: the good, the bad, the ugly

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## 5 Abstract

6 Developments in hazard identification of engineered nanoparticles (ENP) have not been met with proper  
7 fate descriptors to calculate travel distances and the bioavailable concentration of ENP. Three possible  
8 fate descriptors for ENP in soils are compared - batch partitioning coefficients ( $K_d$  values), batch  
9 retention coefficients ( $K_r$  values) and column attachment efficiency - in view of both technical and  
10 practical aspects of environmental risk assessments of ENP.  $K_d$  are deemed not appropriate fate  
11 descriptors for ENP because the equilibrium assumption is not valid. The kinetic interpretation of batch  
12 studies offered by  $K_r$  values bears a link to relevant ENP processes in the environment, but interpretation  
13 may be confounded by the conditions of high shear during batch tests complicating direct use in  
14 transport or bioavailability calculations. Column experiments are to some extent also operationally  
15 defined and require a more experimentally dedicated approach that does not necessarily leads to a  
16 widely carrying physical parameter. Future efforts should therefore be investigated in development of  
17 tests that strike a better balance between operational simplicity and technical accuracy.

## 18 Introduction

19 In the last decade, knowledge and insights in the environmental hazard of engineered nanoparticles  
20 (ENPs) have increased markedly and the field has moved well beyond the reconnaissance stage,  
21 warranting research in mechanisms that lie at the basis of ENP ecotoxicity. What has been investigated  
22 much less is how interactions between ENP and the specific environmental medium affect bioavailability,  
23 transport and thus the eventual risk<sup>1,2</sup>. One reason for this slower development may be the absence of  
24 generally agreed fate indicators for ENPs, being a preferably small set of parameter values that can be  
25 used to calculate travel distances within a particular environmental compartment and/or the  
26 bioavailable fraction of the total ENP concentration. It has become clear that the magnitude of different  
27 toxic endpoints<sup>3-8</sup>, the travel distances of ENP in different soil types<sup>1,9,10</sup> or sedimentation speed in  
28 different water types<sup>11,12</sup> vary greatly with the chemical and/or physical properties of the receiving  
29 environmental compartment. Currently available hazard data of ENP and mass flux calculations are,  
30 however, based on a total mass concentration basis across all water, soil or sediment types, because  
31 there are currently no agreed fate indicators or model approaches to calculate mobile and/or  
32 bioavailable ENP concentrations, a situation that may lead to very high uncertainty. For instance, metallic  
33 silver ENP are found both more hazardous or less hazardous based on total concentrations compared to  
34 dissolved counterparts in different works<sup>5,13</sup>. Using a fate descriptor to estimate the bioavailable ENP  
35 fraction from the total ENP concentration could lead to more consistent trends. Likewise, basing ENP  
36 travel distances in e.g. freshwater systems only on the concentration of ENP leads to serious  
37 overestimation of their travel distances and it is clear that interaction with the environmental matrix  
38 needs to be quantified for a more correct assessment.<sup>14</sup> Current model approaches for ENPs are,

39 however, very numerous and not always comparable, hampering the development of standardized tests  
40 or large datasets that could serve to discover trends in ENP behavior as a function of characteristics of  
41 the natural environment.

42 The current perspective compares three fate indicators of ENP that have been put forward in the  
43 literature:  $K_d$  values,  $K_r$  values, both obtained in batch tests, and attachment efficiency ( $\alpha_{att}$ ) obtained in  
44 column tests. Praetorius et al.<sup>15</sup> have undertaken a rigorous thermodynamic assessment in this issue and  
45 concluded that fate descriptors based on batch test are not to be used based on the inapplicability of the  
46 equilibrium concept to ENP, while column tests would provide a more accurate means to assess the fate  
47 of ENPs. To the author's view, their thorough thermodynamic analysis could be broadened to better take  
48 practical arguments into account as well as a more rigorous analysis of the environmental realism of  
49 both batch and column tests. Development of appropriate fate indicators should not only build on  
50 technical arguments. The most appropriate method is most likely a compromise between technical  
51 accuracy and operational simplicity as has been the case for methods to calculate bioavailability and  
52 transport of molecular chemicals (i.e. chemicals occurring as individual molecules in the environment,  
53 rather than as ENPs). Moreover, where mechanistic approaches potentially provide the most accurate  
54 results, the data requirements are also high and often intractable in highly heterogeneous systems such  
55 as natural soils or rivers so that no real increase in accuracy is effectively gained despite high costs and  
56 efforts.

#### 57 **Deposition and bioavailability of ENP**

58 In the case of soils, the mobile fraction is mostly the ENP concentration that is suspended in the soil pore  
59 water.<sup>1</sup> Deposition is in this respect a key process limiting the mobile fraction of ENP in soils given the  
60 large reactive immobile surface in soils to which ENP can attach in various ways<sup>1</sup>. The term "deposition"  
61 is often only used when particle attachment to immobile surfaces is irreversible<sup>16</sup>. The term is used more  
62 broadly here, involving also reversible attachment<sup>17</sup>.

63 In the case of aquatic systems, the mobile fraction may be related to the ENP concentration that does  
64 not or does only slowly settle gravimetrically, thus being able to be transported further<sup>14</sup>. The mobile  
65 ENP concentration in aquatic systems is thus, similarly to soils, the fraction that remains suspended.  
66 Recent research indicates that interactions between ENP and the much more numerous, naturally  
67 occurring particles such as clays is determining the settling and thus transport distances of ENP in aquatic  
68 systems.<sup>18</sup> These interactions are called heteroaggregation but are termed deposition here. Deposition is  
69 often reserved for interaction of particles with immobile pore walls, but it is in essence the same process  
70 than heterocoagulation<sup>19</sup>, often reserved for the interaction between mobile, unlike particles.

71 ENP bioavailability has yet to be defined, but it is argued here that the mobile ENP concentration may be  
72 assumed as a good estimate of the bioavailable concentration and that deposition is a key mechanism  
73 determining bioavailability. Soil pore water is the key exposure pathway to molecular contaminants for  
74 soil organisms, even for soil-ingesting invertebrates that are in direct contact with the soil matrix in the  
75 gut<sup>20</sup>. Soil pore water is at least also an important uptake route of ENP for many soil organisms<sup>3</sup>. Even in  
76 the case of soil-ingesting invertebrates where direct contact with the soil matrix occurs, ENP detachment

77 from the ingested soil is required prior to uptake. Bio-available ENPs therefore need to be suspended  
78 and mobile to be taken up, albeit in a different chemical environment in the case of invertebrate guts.  
79 Similarly, there are numerous accounts that homoaggregation of ENP reduces their toxicity in aquatic  
80 systems, probably because the rate of many biological particle uptake processes is size dependent<sup>1</sup>.  
81 Attachment of ENP to solid particles increases their size and thus reduces their bioavailability<sup>21</sup>.  
82 Deposition thus reduces both mobility and bioavailability. Many other processes (e.g. coatings<sup>1</sup>) are of  
83 course also relevant for bioavailability and the relation between mobility of ENP surely has not yet been  
84 fully elucidated, but the main argument here is that fate descriptors for deposition must be the first  
85 improvement in better predicting both travel distances and bioavailability of ENP relative to using total  
86 concentrations only.

### 87 **$K_d$ values of molecular chemicals**

88  $K_d$  values quantify the ratio between the concentrations of a chemical found on the solid and liquid  
89 phase (Table 1).  $K_d$  values are an equilibrium concept and are therefore termed “equilibrium partitioning  
90 coefficients” by Praetorius et al.<sup>15</sup>, but “partitioning coefficient” is preferred here, because  $K_d$  values are  
91 often used to describe processes that are in essence not in equilibrium.

92 A thorough analysis of the concept and applicability of  $K_d$  values in a soil perspective has been done by  
93 Degryse et al.<sup>22</sup>  $K_d$  values are operationally defined, i.e. the method by which they are obtained defines  
94 the values they represent and can only be seen as a way to model/estimate a real process or property, in  
95 this case the partitioning of chemicals between solid and liquid phase.  $K_d$  values are determined after  
96 shaking a suspension of soil in a liquid (usually 1 mM  $\text{KNO}_3$  or 0.1 M  $\text{CaCl}_2$ ) with a certain liquid-to-solid  
97 ratio (L/S) holding a certain concentration of chemical for a certain amount of time (usually 24 h)  
98 followed by a separation, usually 0.02  $\mu\text{m}$  or 0.45  $\mu\text{m}$  microfiltration, and measurement of the mass of  
99 the chemical in the filtrate. Variation in any of these method parameters will result in a different  $K_d$  value  
100 for the same chemical so the  $K_d$  value cannot be claimed to be equal to a real physical value such as an  
101 equilibrium constant or attachment rate constant.<sup>23</sup> An operational definition thus presents problems if  
102 the method is not fully standardized so that  $K_d$  values can in effect often not be compared to each  
103 other<sup>22</sup>.

104  $K_d$  values are seen as a mechanistic approach to predict transport and bioavailability of chemicals in the  
105 environment, because they contrast with e.g. empirical relations between total chemical relationships,  
106 soil properties and bioavailable concentration.<sup>24</sup> As argued by Praetorius et al.<sup>15</sup>,  $K_d$  values are most often  
107 regarded as an estimate of true equilibrium constants. This assumption can be valid for molecular  
108 chemicals, provided that equilibrium was attained in the subjectively set time limit of the  $K_d$   
109 determination<sup>22</sup>.  $K_d$  values can in this case be used in combination with the convection-dispersion  
110 equation to predict retardation during transport of molecular chemicals in soils through the so-called  
111 retardation factor (R), that expresses the ratio of the travel speed of a chemical relative to an inert  
112 tracer<sup>22</sup> as also schematically shown in Figure 1:

$$113 \quad R = 1 + (\rho_b/\theta_e)K_d. \quad (\text{eq. 1})$$

114  $\rho_b$  is the soil bulk density and  $\theta_e$ , the effective porosity.  $K_d$  are also often combined with other  
115 mechanistic approaches such as the biotic ligand model when accurately predicting bioavailability<sup>22</sup>.

116 The equilibrium assumption is, however, often violated for a range of possible chemicals in soils and  
117 sediments.<sup>22, 23</sup> Many reactions of e.g. metals in soils are slow and even irreversible, such as strong  
118 fixation of metals over time<sup>22</sup>. Deviations between experimental and predicted transport is most often  
119 found in the case of relatively high  $K_d$  values, an observation that is explained by association with  
120 naturally occurring colloids (particles < 1  $\mu\text{m}$ ) in soils<sup>25</sup>. The transport of colloids occurs with entirely  
121 different mechanisms that are all essentially non-equilibrium.

122 Notwithstanding the many limitations of  $K_d$  values, they have been successful in providing more realistic  
123 risk assessment of many chemicals that were otherwise based on total concentrations. Determining a  $K_d$   
124 value is in principle relatively straightforward and can therefore be easily standardized, resulting in  
125 precise values for a particular environmental system and a given protocol.  $K_d$  values are especially  
126 successful if the values are soil-specific, if the labile fraction of the contaminant is estimated accurately  
127 (e.g. using ageing correction<sup>26</sup> and/or using diffuse gradient thin film measurements) and if the  $K_d$  value  
128 has been calculated based on *in-situ* concentrations<sup>22</sup>. Because of their conceptual simplicity,  $K_d$  values  
129 know a wide applicability, resulting e.g. in relationships between  $K_d$  values and routinely measured soil  
130 properties such as texture, pH and organic matter content<sup>22, 27</sup>, relationships that allows distribution  
131 estimation in soils where a  $K_d$  measurement did not happen *per se*.

### 132 **$K_d$ values of ENPs**

133 Praetorius et al.<sup>15</sup> argue that  $K_d$  values, as equilibrium concepts, cannot be used for ENPs, because  
134 deposition cannot be described as an equilibrium process. This should imply that eq. (1) cannot be used  
135 to model ENP fate in soils. The most basic and most used theory for modelling particle transport in soils,  
136 colloid filtration theory, assumes that only irreversible attachment is relevant for particles. Figure 1  
137 schematically contrasts irreversible attachment, retardation and a combination of the two processes,  
138 following a step input relative to an inert (non-interacting) tracer molecule (e.g. tritiated water). If only  
139 retardation is relevant, the same concentration as the step-input feed concentration ( $C_0$ ) may appear at  
140 the column outflow. This behavior is often found for dissolved chemicals in soils and can be modelled  
141 purely on the basis of equation (1). It is usually observed, however, that the concentration of ENP, like all  
142 particles, rarely reaches  $C_0$  at the outflow and arrival at the column outlet is simultaneous or even earlier  
143 (because of preferential flow<sup>1</sup>) compared to the inert tracer (e.g.<sup>28</sup>). Such a behavior owes to  
144 irreversible attachment of ENPs and cannot be modelled only based on equation (1) that assumes that  
145  $C/C_0 = 1$  will eventually be reached.

146 The combination of two processes, i.e. retardation and irreversible attachment, however, occurs and is  
147 usually explained based on the existence of sites where detachment of ENPs is possible<sup>9, 29-32</sup>. Particle  
148 detachment has been studied much less compared to attachment<sup>33</sup>, but it is a common process that  
149 explains the often high colloid concentrations found in soil pore waters<sup>34</sup> and is necessary in the context  
150 of ENP risk assessment where the main route of exposure of soil to ENPs is through detachment from  
151 sludge applied to arable soils<sup>35, 36</sup>. The  $K_d$  value has in this context been seen as the approximation of the

152 ratio between the rate constants of attachment ( $k_{att}$ ) and detachment ( $k_{det}$ ) of ENP<sup>29</sup>, but this is a  
 153 fundamentally different definition than the conventional one for  $K_d$  values. The  $k_{att}/k_{det}$  ratio is not an  
 154 equilibrium constant because, as Praetorius et al.<sup>15</sup> point out, the processes of attachment and  
 155 detachment each rely on entirely different mechanisms. Moreover, a term accounting for irreversible  
 156 attachment always has to be added in addition to the retardation term to the convection-dispersion  
 157 equation, accounting for the loss of recovery<sup>9, 29-32</sup>. The term “pseudo-equilibrium” has been used  
 158 instead to designate the steady-state colloid concentration often found in natural systems.<sup>34</sup> Partitioning  
 159 of Ag ENPs in the same natural soils were determined using a batch method<sup>37</sup> or a column method<sup>9</sup>, at  
 160 least allowing to investigate whether the  $k_{att}/k_{det}$  ratio describing pseudo-equilibrium can be obtained in  
 161 a similar manner to  $K_d$  values from batch tests based on the aforementioned batch and column tests on  
 162 Ag ENP in the same set of natural soils.  $K_r$  values were calculated in the batch method study - values that  
 163 are, as will be explained further, essentially obtained in the same way as  $K_d$  values<sup>38</sup>. Figure 2a compares  
 164 these values to the ratio of  $k_{att}/k_{det}$  parameters that were fitted to breakthrough curves in the column  
 165 study. A poor relation can be observed and  $K_r$  values are generally higher than  $k_{att}/k_{det}$  ratios. Attachment  
 166 rates tend to be higher during batch tests compared to column tests, because of the high shear and  
 167 complex hydrodynamic conditions during batch tests<sup>39</sup>. It can thus be concluded that the batch tests  
 168 could not describe the pseudo-equilibrium that occurred in the column tests.

#### 169 **$K_r$ values**

170 The ratio between total and aqueous ENP concentration after 24 h shaking has also been called the  
 171 retention coefficient ( $K_r$  [L kg<sup>-1</sup>]) (Table 1)<sup>38</sup>. The major difference with  $K_d$  values is that no equilibrium is  
 172 assumed, i.e. it is not claimed that  $K_r$  values are estimators for some equilibrium constant. The kinetics of  
 173 deposition or aggregation in a batch test can be considered to discover to what physical entities  $K_r$  values  
 174 can alternatively be related. A soil suspension can be conceptualized as a suspension of uniform spheres  
 175 having a diameter equal to the average diameter of the soil grains ( $d_{50}$  [m]). Similarly, the stock ENP  
 176 suspension used for spiking can be assumed insoluble for convenience and also consisting of uniform  
 177 spheres having diameter  $d_{ENP}$ . Orthokinetic aggregation of ENP with soil grains will begin upon addition  
 178 of ENP to the soil suspension followed by shaking, which imposes shear on both soil grains and ENPs<sup>40</sup>. In  
 179 the case of a batch system with intense shear such as during a  $K_d$  or  $K_r$  determination, it can be shown  
 180 that orthokinetic ENP – soil grain aggregation dominates over perikinetic, i.e. diffusion-driven,  
 181 aggregation, especially if the particle size difference is large as is the case for ENPs and soil grains. The  
 182 initial orthokinetic aggregation rate of ENP with soil grains can be written as<sup>40</sup>

$$183 \left( \frac{dn_{ENP}}{dt} \right)_{t \rightarrow 0} = -\alpha_{ortho} k_{ortho} n_{ENP} n_{soil} = -\frac{\alpha_{ortho}}{6} G (d_{ENP} + d_{50})^3 n_{ENP} n_{soil} \quad [L^{-1} s^{-1}] \text{ (eq. 2)}$$

184  $k_{ortho}$  is the orthokinetic heteroaggregation rate constant [ $s^{-1}$ ],  $n_{ENP}$  and  $n_{soil}$  are the number  
 185 concentrations of ENP and soil grains respectively [ $L^{-1}$ ],  $G$  is the shear rate [ $s^{-1}$ ] and  $\alpha_{ortho}$  is the  
 186 orthokinetic collision efficiency. If  $\alpha = 1$ , there are no repulsive barriers to be overcome and no long  
 187 range attractive forces exist. Aggregation then only depends on the shear rate, sizes and concentration  
 188 of particles. The balance between repulsive barriers, e.g. similar surface charges, and attractive forces,  
 189 e.g. Van der Waals attraction, results in  $\alpha_{ortho} \neq 1$ .



Eq. 1 can only describe the very early stages of aggregation, because in conditions of high shear, large soil flocs are continuously formed and broken up. After a certain equilibration time, usually much less than 24 h<sup>41</sup>, an equilibrium average floc size  $d_{eq}$  [m] and number  $n_{eq}$  [L<sup>-1</sup>] are established, the magnitude of which depends on  $n_{soil}$ ,  $G$ ,  $k_{ortho}$ , and the particle break-up rate<sup>42</sup>. The  $d_{eq}$  of e.g. clay suspensions are usually of the order of several 100  $\mu\text{m}$ <sup>41</sup>. In a realistic fate assessment, the ENP number concentration is low enough so that deposition sites on soil flocs do not become saturated, i.e. ENP can continuously aggregate with the same floc of soil granules. Moreover, the large difference between  $d_{ENP}$  and  $d_{eq}$  means that any ENP-soil grain aggregation does not significantly increase the size of soil aggregates. This means that the floc size and number is not affected by aggregation with ENP. At the same time, ENP homoaggregation is assumed unlikely during a  $K_r$  determination<sup>37, 43</sup>. By assuming spherical soil granule aggregates,  $n_{eq}$  can be estimated.

$$n_{eq} = \frac{\rho \pi d_{eq}^3}{6L/S} \quad (\text{eq. 3})$$

Moreover,  $d_{ENP} + d_{eq} \approx d_{eq}$  in eq. 1 given that  $d_{ENP} \ll d_{eq}$ .  $K_r$  values are ratios of mass concentrations, but number concentrations can be estimated from these in a similar way as  $n_{eq}$  was estimated from the L/S ratio (eq. 3). Combining eqs. 2 and 3, the definition of  $K_r$  values and the approximations above results in eq. 4.

$$K_r = \frac{n_{ENP,t=0}}{n_{ENP,t=T}} \times L/S = \exp\left(\frac{G\alpha_{ortho}}{\pi(L/S)\rho} T\right) \times L/S \quad (\text{eq. 4})$$

$n_{ENP,t=0}$  and  $n_{ENP,t=T}$  [L<sup>-1</sup>] are the ENP number concentrations at the start and end (e.g.  $T = 24$  h) of the  $K_r$  experiment. Eq. 4 shows that  $K_r$  values are dependent on the shear rate  $G$  that is currently poorly defined during most batch tests. In addition, if  $n_{ENP,t=0}$  is increased, homoaggregation may become important, leading to higher  $K_r$  values that increase with ENP concentration<sup>38</sup>.  $K_r$  values thus suffer from a similar operational definition as do  $K_d$  values of molecular chemicals. However, if shear conditions and L/S ratio are kept constant and  $n_{ENP}$  sufficiently low,  $K_r$  values of different ENP/soil combinations will vary with  $\alpha_{ortho}$ , the orthokinetic collision efficiency.

Praetorius et al.<sup>15</sup> argue that ENP fate indicators obtained from batch tests are entirely irrelevant to realistic processes in the field if starting from an equilibrium assumption. Here, it was investigated whether batch tests could be interpreted in a kinetic context, arguing that  $K_r$  values are to some extent related to processes such as surface potentials that determine deposition (thus also heterocoagulation). This assessment may be especially applicable if conditions are modelled where high shear predominates, e.g. wastewater treatment plants or turbulent rivers. The likelihood of deposition can thus be compared between individual ENP – soil or ENP – natural colloid combinations to some extent. However, eq. 4 assumes  $\alpha_{ortho}$  is independent of  $G$  while  $\alpha_{ortho}$  is in fact heavily influenced by the hydrodynamic conditions during the shaking process<sup>39, 40</sup>. It is currently unclear to what extent these hydrodynamic effects may overshadow the  $K_r$  differences between soils or natural waters that can be related to deposition efficiency, but some indications exist that  $K_r$  values may reflect relevant physicochemical variations. The relationship between  $K_r$  values and granulometric clay found e.g. for Ag ENP<sup>37</sup> has also been shown to exist for bioavailability<sup>5</sup>. A similar relationship between natural colloids concentration

227 and ENP travel distances has been concluded from the increase of ENP sedimentation rates as a function  
228 of natural colloid concentration in freshwater systems<sup>18</sup>. Figure 2b combines  $\alpha_{ortho}$  values calculated from  
229  $K_r$  values for Ag ENP<sup>37</sup> using eq. 3 assuming a relatively high  $G = 100 \text{ s}^{-1}$  with fitted attachment  
230 efficiencies ( $\alpha_{att}$ ) that will be explained below and soil densities obtained during column tests with the  
231 same ENP in the same soils<sup>9</sup>. Two outliers were found, probably owing to a poor calculation of  $\alpha_{att}$  for  
232 clayey soils where breakthrough is often not detected. Omitting the two outliers from the dataset leads  
233 to a significant relationship between  $\alpha_{ortho}$  and  $\alpha_{att}$  values. It is thus argued that results from batch tests  
234 can potentially be related to real properties of ENP if analyzed in a kinetic context.

### 235 ENP column deposition

236 Modelling of particle dynamics in porous media has been to a large extent built on colloid filtration  
237 theory (CFT) (as described by<sup>40</sup>) and is also the theory of choice to model the fate of ENP in porous media  
238 <sup>16</sup>. There are many modifications of CFT to account for all the possible interactions of particles during  
239 transport. The most basic theory conceptualizes soils as stacked, uniform spheres having a diameter  $d_{50}$ ,  
240 the average diameter of soil grains. It also assumes that all successful collisions lead to irreversible  
241 attachment with a rate constant according to eq. 5.

$$242 \quad k_{att} = \alpha_{att} \frac{3(1-\theta)}{2d_{50}} \eta u \quad (\text{eq. 5})$$

243  $\alpha_{att}$  is the attachment efficiency,  $\theta$  is the porosity,  $\eta$  is the single-collector contact efficiency and  $u$  is the  
244 pore flow velocity.  $\eta$  accounts for all physicochemical parameters determining the deposition efficiency  
245 under favorable conditions, i.e. in the absence of repulsive barriers.  $\alpha_{att}$  quantifies the extent by which  
246 electrosteric barriers reduce the deposition rate relative to the favorable case<sup>33</sup>.

247 The environmental realism of column experiments should, however, not be overstated. Column tests can  
248 range from stacked glass beads, sand beds, and saturated stacked columns to unsaturated intact soil  
249 cores. Increases in environmental realism make the systems less well defined and thus more difficult to  
250 model, so most often relatively simple set-ups are chosen. Most column experiments study ENP  
251 transport using aqueous suspensions, of which several pore volumes are pumped through a saturated  
252 soil column. This often leads to unrealistically high ENP concentrations that deposition on soil grains,  
253 whereas in a realistic situation, low ENP concentrations first have to detach from e.g. wastewater  
254 treatment plant sludge to be transported<sup>35</sup>. Moreover, field soils are nearly always unsaturated, which  
255 leads to entirely different particle transport trends compared to e.g. saturated soil columns<sup>1</sup>.

256 Even within the limits of a relatively simple column set-up, it is difficult to deduce an unambiguous fate  
257 descriptor. Praetorius et al.<sup>15</sup> argue that  $\alpha_{att}$  is currently the most appropriate fate indicator, while also  
258 partly acknowledging the implementation difficulties. From a practical viewpoint, eq. 5 requires many  
259 parameters that are not routinely measured for soils or for which there are no robust pedotransfer  
260 functions available. Some efforts have been invested to predict  $\alpha_{att}$  based on first principles<sup>44</sup>, but many  
261 other simultaneously occurring processes such as straining, pore wall blockage, steric repulsion, and  
262 preferential flow complicate this assessment<sup>45-47</sup>.  $\alpha_{att}$  is therefore in essence an empirical parameter that  
263 is nearly always fitted to column outflow data using eq. 5.  $\eta$  can be calculated using empirical correlation

264 equations<sup>48,49</sup>, but these require Hamaker constants that are often available when studying  
265 homogeneous columns of e.g. quartz, but which are much more poorly defined for the case of more  
266 realistic, heterogeneous soils. Finally,  $\alpha_{att}$  values vary to some extent with physical parameters such as  
267 flow rate<sup>50</sup> and many other mechanisms that are not taken into account in clean-bed CFT such as  
268 straining are also dependent on flow rate<sup>51</sup>. Some of these effects can be taken into account by designing  
269 a more comprehensive model, but such a model would require many more parameters to be fitted or  
270 experimentally determined (e.g. blocking factors, straining coefficients, etc.) because they cannot be  
271 calculated based on first principles.  $\alpha_{att}$  values are therefore in essence also operationally defined,  
272 meaning that it is not clear, how an  $\alpha_{att}$  value can be used outside of the boundaries of the test system  
273 used, at least not with a strong claim of mechanistical accuracy.

#### 274 **Conclusions: The best fate indicator?**

275 Table 1 summarizes the comparison between the three fate descriptors discussed in this work.  
276 Evaluating fate indicators requires some reference point, which is ideally the situation in the field. ENP  
277 contamination has not been going on long enough to produce historically contaminated sites and  
278 analysis of ENP in the field currently presents such technical difficulties<sup>52</sup> that there is only one study on  
279 freshwater to the authors' knowledge<sup>53</sup>. Comparison may occur with mesocosms and microcosms where  
280 ENP fate processes are still close to the situation in field<sup>54,55</sup>, but the effect of the environmental matrix  
281 on any fate predictor is pronounced, making quantitative evaluation across studies using different  
282 environmental systems impossible. Column tests are intuitively seen as more environmentally realistic,  
283 but it has been argued that this realism may be overstated and column tests can thus not serve as  
284 reference points.

285 The current perspective investigates whether  $K_d$ -type batch methods could be used instead. One virtue  
286 of  $K_d$  values for molecular chemicals is that the concept is simple enough so that it can be widely applied.  
287 Similarly to Praetorius et al.<sup>15</sup>, technical objections were found that showed that batch type fate  
288 descriptors could not be related to column type descriptors. Where Praetorius et al.<sup>15</sup> focused on the  
289 lack of equilibrium, the effect of shear during batch tests was argued here to complicate comparability.  
290 However, considering previous counterarguments against the environmental realism of column tests, it  
291 is difficult to use the lack of comparability between these and batch tests to prefer the former.

292 Concurring with Praetorius et al.<sup>15</sup>, deposition cannot be considered an equilibrium process and any  
293 attempt to model this process as such, e.g. using equation (1), will lead to very large errors. Fate  
294 prediction of ENPs should be based on a kinetic assessment and fate descriptors should be developed on  
295 that basis. It remains to be investigated to what extent the results from batch tests can be used in this  
296 context to predict travel distances and bioavailability. Since it was argued that it would not be practical  
297 and not necessarily more accurate to widely apply column tests, there is still a need for a fate descriptor  
298 that is the best possible compromise between operational simplicity and technical accuracy. Alternatives  
299 to both batch and column tests could be investigated, such as, for the soil case, a centrifugal pore water  
300 extraction from soil incubated with ENP (e.g.<sup>56</sup>). Such a test could potentially eliminate effects of shear  
301 while being still operationally relatively simplistic.

302 **Tables**

303 Table 1. Comparison of three fate descriptors for ENP in soils

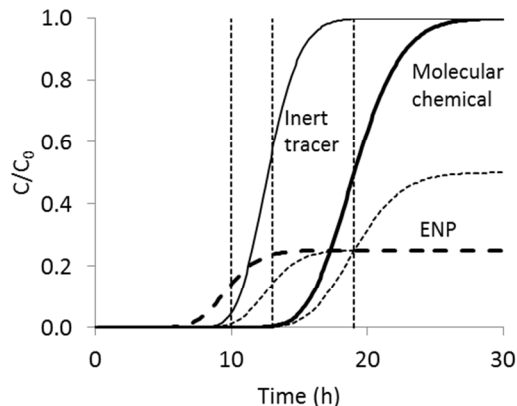
	$K_d$	$K_r$	$\alpha$
Units	$L\ kg^{-1}$	$L\ kg^{-1}$	-
Formulas	$K_d = \frac{M_{tot} - M_{MF} + M_{MF,geo}}{M_{MF}}$	$K_r = \frac{ENP_{add} - M_{MF} + M_{MF,geo}}{M_{MF} - M_{UF}}$	$\alpha_{att} = k_{att}/k_0$
Set-up	batch	batch	column
Targeted physical property	$K_{ads}$	$\alpha_{ortho}$	$\alpha_{att}$
Operationally defined nature of the setup	High	High	Lower
Environmental realism	Not useable	Poor	Medium

304 Symbols:

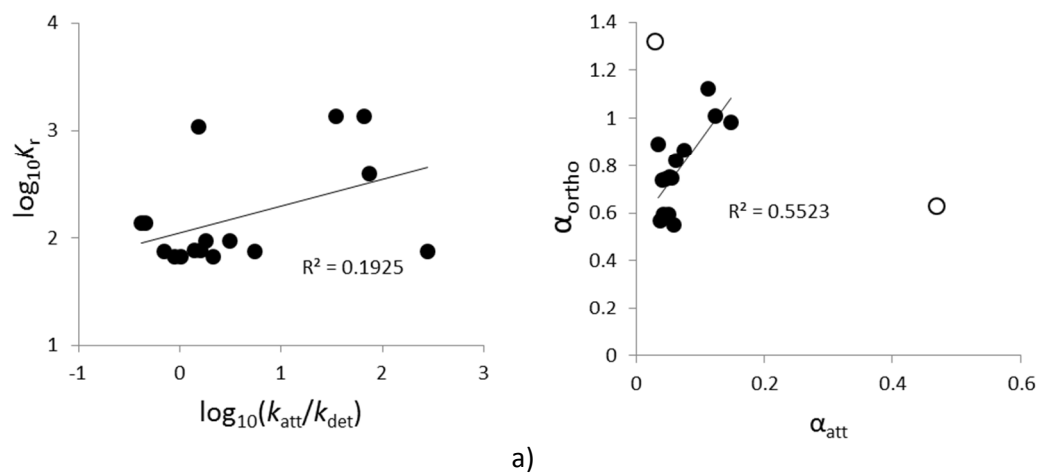
305  $M_{tot}$ : The mass concentration of aqueous contaminant initially present or added306  $M_{MF}$ : The mass concentration of aqueous contaminant measured after microfiltration307  $M_{MF,geo}$ : The mass concentration of aqueous contaminant measured in a zero addition control after microfiltration308  $ENP_{add}$ : The total added mass concentration of NPs309  $M_{UF}$ : The mass concentration of aqueous contaminant measured after ultrafiltration310  $\alpha_{att}$ : Attachment efficiency311  $k_{att}$ : The attachment rate constant under unfavourable conditions312  $k_{att}$ : The attachment rate constant under favourable conditions313  $K_{ads}$ : Adsorption equilibrium constant314  $\alpha_{ortho}$ : Orthokinetic collision efficiency

315

316

317 **Figures**

318  
 319 **Fig. 1.** Schematic representation of possible breakthrough curves of an inert (non-interacting) tracer, a  
 320 molecular chemical and ENP after a step input with mass concentration  $C_0$ . Vertical lines indicate the  
 321 retention times (at 50 % of the maximum concentration). Three breakthrough curves are shown for ENP  
 322 symbolizing behaviors that can be explained by early elution ( $t_r < t_{r,\text{inert tracer}}$ ), particle elution absent of  
 323 early elution or particle detachment ( $t_r = t_{r,\text{inert tracer}}$ ), particle detachment ( $t_r > t_{r,\text{inert tracer}}$ ).



324  
 325 **Fig. 2.** Relation between fate descriptors a)  $K_r$  values<sup>37</sup> compared to the ratio fitted attachment and  
 326 detachment rate constants<sup>9</sup>. b) The orthokinetic attachment efficiency calculated from  $K_r$  values based  
 327 on eq. 3 and assuming  $G = 100 \text{ s}^{-1}$ . Data points represented by open circles were not used to calculate  
 328 the linear fit and the Pearson correlation coefficients are shown.

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