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Complete List of Authors:	McDonald, Matthew; Georgia Institute of Technology, School of Chemical + Biomolecular Engineering Salami, Hossein; Georgia Institute of Technology, School of Chemical + Biomolecular Engineering Harris, Patrick; Georgia Institute of Technology, School of Chemical + Biomolecular Engineering Lagerman, Colton; Georgia Institute of Technology, School of Chemical + Biomolecular Engineering Yang, Ben; US Food and Drug Administration, Center for Drug Evaluation and Research Bommarius, Andreas; Georgia Tech, School of Chemical and Biomolecular Engineering Grover, Martha; Georgia Institute of Technology, School of Chemical & Biomolecular Engineering Rousseau, Ronald; Georgia Institute of Technology, School of Chemical + Biomolecular Engineering

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# Reactive Crystallization: A Review

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- 3 Matthew A. McDonald,<sup>a</sup> Hossein Salami,<sup>a</sup> Patrick R. Harris,<sup>a</sup> Colton E. Lagerman,<sup>a</sup> Xiaochuan
- 4 Yang,<sup>b</sup> Andreas S. Bommarius,<sup>a</sup> Martha A. Grover,<sup>a</sup> and Ronald W. Rousseau <sup>a\*</sup>
- 5

<sup>6</sup> <sup>a</sup> School of Chemical and Biomolecular Engineering, Georgia Institute of Technology, Atlanta,

7 Georgia, 30332

8 <sup>b</sup> Office of Pharmaceutical Quality, Center for Drug Evaluation and Research, U.S. Food and

9 Drug Administration, Silver Spring, Maryland 20993-0002

10

## 11 Abstract

12 Reactive crystallization is not new, but there has been recent growth in its use as a means 13 of improving performance and sustainability of industrial processes. This review examines 14 phenomena and processes in which reaction and crystallization are coupled in the production of a 15 desired chemical species. Coverage includes fundamental phenomena, such as solubility, 16 supersaturation, crystal nucleation and growth, and chemical kinetics. Systems examined are 17 divided into two groups, those best described as undergoing ionic reactions (including 18 neutralizations), which have near instantaneous rates and result in the formation of ionic bonds, 19 and those undergoing covalent reactions in which the key step occurs at measurable rates and 20 results in the formation of covalent bonds, Discussion of the latter category also includes the 21 impact of catalysis. Examples of a variety of reactions and applications are enumerated, and 22 special attention is given to the utility of reactive crystallization in chiral resolution. Integration 23 of reactive crystallization into process design, including both batch and continuous operations, 24 and the development and efficacy of modeling, monitoring and control are reviewed. Finally, a 25 perspective addressing needs to advance the usefulness and applications of reactive 26 crystallization is included.

## 27 Introduction

28 Crystallization is used in the production of a wide variety and quantity of products and 29 intermediates, perhaps more than any other separation technique. In different applications, 30 crystallization can separate, concentrate, or purify a specific species or it may be part of 31 diagnostic or analytical procedures. In most applications the most important function of 32 crystallization is to generate a product in a specific solid form. Many medicines, synthetic 33 materials, food ingredients, and specialty and commodity chemicals require crystallization 34 during the transformation from raw materials to product. The process by which chemical species 35 are crystallized often impacts their properties, such as purity, morphology, mean size, and size 36 distribution. Such properties can affect therapeutic capabilities and dissolution profiles of 37 pharmaceuticals, the efficacy of agricultural chemicals, and a variety of material properties. 38 While the use of crystallization is older than the chemical industry, there are aspects of

39 the process that remain poorly understood. Furthermore, the diversity of processes utilizing 40 crystallization and the chemical and physical variations of species crystallized has led to many 41 different methodologies for conducting this operation. The present review focuses on reactive 42 crystallization from solution: that is, those processes in which a chemical reaction produces 43 a specific crystallizable species in solution and, thereby, generates a driving force for the 44 formation of a crystalline product. Clearly, the chemical reaction must produce sufficient 45 amounts of the crystallizing species to exceed solubility. While reactive crystallization may 46 fulfill the same functions of crystallization cited earlier, there also are two other important roles 47 that can be played by reactive crystallization: (1) If a reaction is controlled by equilibrium, 48 removal of the reaction product from solution by crystallization pulls the reaction towards the 49 product as dictated by Le Chatelier's principle. (2) Suppose the desired product is an 50 intermediate in a larger reaction network and the yield of that product is reduced by its 51 subsequent reaction. Then the yield can be increased by operating under conditions causing 52 crystallization of the product. As solids, species are stabilized and less likely to undergo 53 subsequent solution-phase reactions.

Besides being generated by reaction, the driving force for crystallization can be created or enhanced by solvent removal (for example, by evaporation or transport through a membrane), adjustment of pH, change in temperature, or addition of a nonsolvent. The presence of multiple species in solution complicates the system but is frequently encountered in industrial processes. In a reactive crystallization process, there are necessarily multiple species present—that is, the reactants and products of the reaction—that may impact the solubility of each species, the pH and temperature of the solution, and the kinetics of the reactions and the crystallization. Page 3 of 76

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61 As the chemical industry continues to strive towards ambitious goals of process 62 intensification, efficiency enhancements and sustainability, reactive crystallization can be a 63 helpful tool in achieving such goals. Thermal separations dominate the chemical industry and 64 have a huge energy cost; on the other hand, reactive crystallizations can be operated without 65 expenditure of the thermal energy that is required for cooling crystallization, evaporative crystallization, or many other separation processes.<sup>1</sup> The combination of reaction and 66 67 crystallization can also reduce production time and hold-up of intermediates, thereby reducing 68 the number of operations and eliminating the need to transfer materials between vessels. Use of 69 the same solvent for reaction and crystallization can additionally reduce waste production and 70 the need for wastewater treatment, and it may even eliminate the need to use additional solvents. 71 Reactive crystallization encompasses several fundamental phenomena. Reactant mixing 72 is limited by convection and diffusion, as are the reaction products as they are transported 73 through the bulk liquid to the surface of a growing crystal. New crystals are formed by either 74 primary or secondary nucleation, thereby generating fresh surfaces for growth. The rates at 75 which these kinetic phenomena occur are influenced by mixing, catalyst design, and other 76 engineering decisions, and they determine the size distribution, yield, and other aspects of crystal 77 quality. Moreover, such fundamental considerations work their way into the design, 78 implementation, and control of processes in which reactive crystallization plays the key role. 79 The aims of this review are to (1) describe fundamental thermodynamic and kinetic 80 phenomena important in reactive crystallization, (2) examine reaction types and provide 81 tabulations of references for specific reaction systems, (3) examine the design and control of 82 systems using reactive crystallization, and (4) identify areas for future research. Only 83 crystallization from solution is considered and there is an emphasis on processes involving high-84 value products such as pharmaceuticals and specialty chemicals. A condensed summary of 85 fundamentals of crystallization and reactive processes is followed by a compilation, with 86 commentary, of recent studies of processes utilizing reactive crystallization. Processes are 87 categorized based on reaction type and relative rates of reaction and crystallization. Finally, the 88 future of reactive crystallization processes is discussed, including what needs to be accomplished 89 for more widespread adoption of this intensified process. 90

## 91 Fundamentals

3

92 *Solubility.* Solid-liquid equilibrium thermodynamics determine solute solubility: that is, 93 the maximum mole fraction (or other measure) of the solute in a solution at a specific set of 94 conditions, including temperature, pressure, pH, and solution composition. The governing 95 requirement for solid-liquid equilibrium is that the chemical potential of each component 96 distributed between the two phases is the same in the solid and liquid phases; that is  $\mu_i^{\rm S} = \mu_i^{\rm L}$ . 97 Proceeding from this fundamental expression, a thermodynamic framework for cases involving 98 complex liquid mixtures, multi-component solids, and polymorphs can be developed.<sup>2</sup> 99 Thermodynamics also may determine the state of the solid, which may be anhydrous, a hydrate 100 or solvate, a salt, or one of a family of polymorphs.\* When the system involves a chemical 101 reaction, the thermodynamics must include interactions of reactants, products, and by-products, 102 all of which greatly complicate the system behavior and make it difficult to formulate working 103 expressions for solute solubility.

104 In reactive crystallization, system conditions usually are selected so that reactants and 105 byproducts<sup>‡</sup> remain in solution, and the driving force for crystallization of the reaction product is 106 created by its synthesis. This was the goal outlined by Encarnacion-Gomez et al.<sup>3</sup> and McDonald et al.<sup>4</sup> who compared the effect of pH value on solubilities of a product, ampicillin, to those of 107 108 the reactant, 6-aminopenicillanic acid, and byproduct, phenylglycine, to guide selection of the 109 pH value at which to run the reaction and crystallization. The approach was extended to include 110 systems in which primary products included amoxicillin and cephalexin and corresponding reactants and byproducts.<sup>5</sup> 111

In many instances, empirical relationships, which often are based on simplifying assumptions regarding the fundamental thermodynamics, are used to relate solubility as a function of temperature and composition. Such approaches require experimental measurements of solubilities, and the resulting correlations provide a means of interpreting and interpolating the

<sup>\*</sup> Hydrates and solvates are sometimes referred to a pseudopolymorphs, but strictly speaking they are distinct chemical entities. Polymorphs, on the other hand, are all the same species, but have different packing structures. <sup>‡</sup> Reactants are chemical species that are consumed by a reaction; byproducts are produced by a reaction but are not the desired species. Products are generated by a chemical reaction, but the term may also be used to indicate the output from the overall process.

124

- 116 data. As an illustration, consider the findings of Hu *et al.*<sup>6</sup> on the solubility of an important
- 117 intermediate compound, methyl D-(-)-4-hydroxy-phenyl glycinate, C<sub>9</sub>H<sub>11</sub>NO<sub>3</sub>, in the production
- 118 of certain  $\beta$ -lactam antibiotics. Over a pH range of 1-13 they showed that the solubility was
- 119 lowest at the isoelectric point,\* which is discussed below. Solubilities increased with solvent
- 120 polarity, except when water was the solvent, and it was asserted that water was an outlier
- 121 because of the dominance of the hydrophobic groups in the solute molecule. Temperature had
- 122 the most significant effect on solubility in both pure and mixed solvents, which was correlated by
- 123 the Apelblat equation

$$\ln x_1 = A + \frac{B}{T} + C \ln T \tag{1}$$

where  $x_1$  is the mole fraction of solute 1 and *A*, *B* and *C* are constants fit to data for each solvent reaction of solute 1 and *A*, *B* and *C* are constants fit to data for each solvent reaction of solvent mixture (*T* in Kelvin).

127 The rationale for the Apelblat equation was developed by Cuevas-Valenzuela *et al.*<sup>7</sup> and 128 it has since been cited in over 400 publications, with each describing its use for a variety of 129 solutes and solvents. In some instances, the third term in the equation can be omitted to obtain 130 the classic van't Hoff relationship

131 
$$\ln x_1 = A' + \frac{B'}{T}$$
(2)

where A' and B' are fitted parameters, and B' is often referred to as the apparent heat of solution(*T* in Kelvin).

<sup>\*</sup> The isoelectric point  $(pK_I)$  is the pH at which the species carries no net charge. For a molecule with two protonlabile moieties, like many amino acids, the isoelectric point commonly is taken to be the average of the acid dissociation constant  $(pK_A)$  of each moiety.

134 Solubilities of amphoteric species, 135 such as amino acids, are lowest at their 136 isoelectric point. At this condition, the solid 137 in equilibrium with the solution is a neutral 138 zwitterion. Addition of acid or base to move 139 the pH value away from the isoelectric point 140 initially causes modest increases in solubility, 141 but then much greater increases occur as pH 142 moves further from the isoelectric point. The 143 distribution of acidic, neutral, and basic forms



Figure 1. Distribution of acidic, neutral, and basic forms of L-serine as a function of pH value.

144 of serine are shown in Figure 1 and illustrate the general behavior of amino acids.<sup>8</sup>

145 The composition of the solid in equilibrium with a coexisting solution of an amphoteric 146 species can vary with pH. Over the pH range that includes the isoelectric point (see Figure 1), the 147 coexisting crystal is the zwitterion (neutral species), but as pH moves towards the lower  $pK_{A1}$  the 148 solid species may change from the zwitterion to an acid salt (for example, leucine hydrochloride when HCl is used to reduce pH). Kempkes and van Enckevort<sup>9</sup> presented *in situ* micrographs 149 150 showing both glutamic acid hydrochloride and glutamic acid crystals coexisting in a 1:1 solution 151 of glutamic acid and HCl in water. Alternatively, addition of a base to a solution near the 152 isoelectric point moves pH towards the higher  $pK_{A2}$  and the coexisting solid formed may be a 153 basic salt: for example, sodium leucinate (or leucine sodium) when sodium hydroxide is added to 154 a leucine solution near its upper pK<sub>A</sub>. At pH extremes, solubilities of acid or basic salts may be 155 lower than those of the zwitterion and used to enhance recovery of the species of interest. For example, Sano<sup>10</sup> describes the early production of L-glutamic acid hydrochloride by contacting 156 157 vegetable proteins with HCl, and then processing the recovered acid salt to become monosodium 158 glutamate.

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159 Tseng *et al.*<sup>11</sup> measured solubilities of five amino acids over a pH range from 2 to 10 and 160 used an NRTL model\* to describe activity coefficients of the non-ideal solutions. Figueiredo *et* 161  $al.^{12}$  developed a methodology for estimating activity coefficients using UNIFAC methods and 162 the Debye-Hückel equation that they tested successfully against literature data. Additional data 163 on the effect of pH on the aqueous solubility of a number of amino acids can be found in various 164 sources.<sup>13-16</sup>

The presence of co-solutes and/or impurities can impact the solubility of a species of 165 interest. McDonald et al.<sup>17</sup> showed that during crystallization of cephalexin, the reactants used 166 167 to make cephalexin inhibited complete consumption of supersaturation relative to the pure cephalexin system, by effectively increasing the drug solubility. Hu et al.<sup>6</sup> showed that 168 169 increasing concentrations of ammonium chloride or D-4-hydroxyphenylglycine methyl ester 170 hydrochloride increased the solubility of methyl D-(-)-4-hydroxy-phenyl glycinate. This is 171 particularly important because the ester is a reactant in the synthesis of the glycinate product. Cosolutes can also decrease solubility; Isakov et al.<sup>22</sup> showed that a compound with a valine-to-172 isoleucine ratio of 2:1 was formed from solutions containing the two amino acids and the 173 174 compound formed a third separate solid phase with lower solubility that contaminated the pure-175 component solid phases. The presence of electrolytes in solutions of amphoteric species such as 176 amino acids also affect the species' solubility. For example, the addition of sodium chloride to 177 neutral solutions decreased glycine solubility at low sodium chloride concentrations, but then increased solubility as concentration was increased.<sup>23</sup> The researchers hypothesized that such 178 179 behavior is based on ions of the electrolyte shielding the hydrophobic characteristics of the amino acid. Steendam et al.<sup>24</sup> examined how the difference in solubilities of two structurally 180 similar impurities in solutions of paracetamol (acetaminophen) impacted the properties of 181 182 paracetamol crystallized from those solutions. Further work with these species demonstrated that 183 despite their significant impact on paracetamol crystal properties, the impurities had little influence on paracetamol solubility at the prescribed impurity concentrations.<sup>25</sup> 184

<sup>\*</sup> The NRTL model (non-random two-liquid model) is an expression used to correlate activity coefficients of species in solution with the composition (expressed as mole fractions) of the solution. Activity coefficients are used to account for solution nonidealities, which usually represent deviations from Raoult's law. UNIQUAC and UNIFAC are group-contribution techniques for predicting activity coefficients.

185 Solubility is a function of solvent composition. For example, Granberg and Rasmuson<sup>26</sup> 186 measured solubilities of paracetamol in 26 solvents and determined ideal solubilities and activity 187 coefficients in the saturated solutions. Also, Jiang and Ni<sup>27</sup> considered how compositions of 188 water-acetic acid mixtures influenced paracetamol solubilities and crystal morphology. Solvent 189 effects on the solubilities of amino acids also have been investigated; the effects of ethanol on 190 aqueous solubilities of twenty amino acids were determined and found to be related to the side 191 chain on the amino acid.<sup>28</sup>

192 The relationship of solubility to the form of a co-existing solid at equilibrium has been observed in the work of Zhang et al.<sup>29</sup> who found that hydrogen-bonding ability was a key factor 193 194 in determining solubility and polymorph formation of clopidogrel hydrogen sulfate (CHS). They 195 used two different experimental procedures to determine solubilities of CHS Forms I and II in 196 five alcohols, two ketones and two acetates. The van't Hoff relationship was used to correlate 197 solubilities in the nine solvents for the two different polymorphic forms. Solubilities in ethyl 198 acetate of Forms I and II, along with that of an amorphous form, were also determined by Lu et al.<sup>30</sup> Additionally, temperature may determine which of two polymorphs is more soluble in a 199 200 given solvent, with the one having lower solubility being more stable. In enantiotropic systems 201 the form that has the lowest solubility changes with temperature. While there do not appear to be 202 any studies on reactive crystallization of enantiotropic species, several well-known enantiotropes 203 can be crystallized by reactive crystallization (e.g. *p*-aminobenzoic acid<sup>31, 32</sup>).

204 *Supersaturation.* The difference between a system at a given state and at equilibrium 205 represents a driving force for change, which in crystallization is referred to as supersaturation. 206 The formal definition of supersaturation is the difference in chemical potential of a solute at the existing conditions  $(\mu_i)$  and at equilibrium  $(\mu_i^*)$ : that is,  $\mu_i - \mu_i^* = RT \ln(a_i/a_i^*)$ , where  $a_i$  and  $a_i^*$ 207 208 are activities of solute *i* in the solution at the existing state and at equilibrium, *T* is absolute 209 temperature and R is the gas constant. Activity can be expressed as the product of an activity 210 coefficient ( $\gamma_i$ ), mole fraction<sup>\*</sup> and reference-state fugacity; choosing the same reference state for 211 the existing and saturated solutions (for example, pure supercooled liquid at the system 212 conditions) gives

<sup>\*</sup> Activities based on other expressions of composition such as concentration (mol/L) can be used.

213 
$$\Delta \mu_i = RT \ln \frac{\gamma_i x_i}{\gamma_i^* x_i^*}$$
(3)

214 Unless system conditions produce a significant difference between  $\gamma_i$  and  $\gamma_i^*$ , this

215 equation reduces to the simple dimensionless expression

216 
$$\frac{\Delta \mu_i}{RT} = \ln \frac{x_i}{x_i^*}$$
(4)

217 If the ratio of mole fractions is less than about 1.2, there is less than 10% error in substituting 218  $\left[ (x_i/x_i^*) - 1 \right]$  for  $\ln(x_i/x_i^*)$ . The dimensionless relative supersaturation  $\sigma_i$  then becomes

219 
$$\sigma_{i} = \frac{x_{i} - x_{i}^{*}}{x_{i}^{*}} = S_{i} - 1$$
(5)

where  $S_i$  is the ratio of mole fractions and is referred to as the supersaturation ratio. Expressions for systems involving hydrates, partially dissociated electrolytes and mixtures of electrolytes have been developed by Sohnel and Mullin.<sup>33</sup>

223 Mass balances and other operations in crystallization are often more convenient when 224 compositions are expressed in terms of ratios of mass of solute ( $w_i$ ) per unit mass of solvent ( $w_s$ ): 225  $X_i = w_i/w_s$ . The relative supersaturation and supersaturation ratio can be expressed as

226 
$$\sigma_{i} = \frac{X_{i} - X_{i}^{*}}{X_{i}^{*}} = S_{i} - 1$$
(6)

227 provided  $\sum (w_i/M_i) \ll$  where  $w_i$  is the mass of solute *i* in solution and  $M_i$  is the 228 molecular weight of *i*;  $w_s$  and  $M_s$  are, respectively, the mass of solvent and the solvent molecular 229 weight.

230 Another important way of expressing supersaturation is in terms of concentrations,  $c_i$ 231 (mol/L):

 $\sigma_i = \frac{c_i - c_i^*}{c_i^*} \tag{7}$ 

which is valid if the solution molar densities at system conditions and at saturation are
approximately the same. Mullin<sup>34</sup> provides an example illustrating a violation of this assumption
with mixtures of sucrose, where differences between system conditions and saturation are
substantial.

237 It may be useful at this point to contrast how supersaturation is generated in reactive 238 crystallization with how it is developed in other settings: here a chemical reaction creates the 239 desired solute. If the system is isothermal and solvent has constant composition and is not being 240 removed,  $\sigma$  can be created only as a species is formed by a chemical reaction. If the system is 241 operating as a batch unit, with reactants added at the start of the process, the concentration of the 242 product, ci would typically increase from an initial value of zero. Upon exceeding the solubility, 243  $c_i^*$ , the supersaturation ratio,  $S_i$ , becomes greater than one, and crystallization can begin to occur 244 and proceed as long as the reaction maintains supersaturation in the system  $(S_i > 1)$ .

245 Reactive crystallization necessarily occurs in the presence of multiple components, in 246 addition to the product. Accordingly, while the product solubility in pure solvent may provide a 247 first approximation to behavior in the reaction solution, such an assumption may be incorrect in 248 describing complicated interactions in the system with multiple species. As described earlier, the effects of other solutes may alter (increase or decrease) product solubility,  $c_i^*$ , and therefore 249 250 supersaturation, and if solubility is increased, there may no longer be a driving force for 251 crystallization. As the objective is to recover pure product, the supersaturation ratio of other 252 species formed in the reaction system must remain below their metastable limits (described in the 253 next section). Otherwise, subsequent separation of species simultaneously crystallized will be 254 required and detract from the efficiency of the process.

Nucleation and Growth Kinetics. The kinetics of crystallization are defined by
nucleation and growth phenomena and play a central role in determining the characteristics of a
crystalline product, such as crystal size distribution.<sup>\*</sup> In this section, nucleation is discussed from
the perspective of mechanisms leading to formation of crystals, and growth is recognized as how
crystals increase in mass (and size). Kinetics of nucleation and growth are given for several
crystallization systems to give context for crystallization kinetics in reactive systems.

*Nucleation*, in the context of this manuscript, is formation of a solid crystalline phase
 from a liquid solution, which often sets the character of the process and is a critical factor in
 determining product crystal size distributions. Classical nucleation theory (CNT) is based on

<sup>\*</sup> Agglomeration and breakage, two additional kinetic phenomena that can affect crystal size distribution, are covered by Randolph and Larson,<sup>35</sup> Lewis *et al.*,<sup>36</sup> Ochsenbein *et al.*,<sup>37</sup> and Salvatori and Mazzotti.<sup>38</sup>

homogeneous and heterogeneous mechanisms, both of which describe formation of crystals through a process of sequentially combining constituent units to form larger and larger entities until a stable nucleus is produced.<sup>39, 40</sup> Both heterogeneous and homogeneous mechanisms are referred to as primary nucleation because existing crystals play no direct role in the nucleation mechanism. Supersaturation has a highly nonlinear relationship to primary nucleation rate as illustrated by the following equation from classical nucleation theory:<sup>36</sup>

270 
$$J = AS \exp\left(-\frac{\phi 16\pi \gamma_{sl}^3 v^2}{3(kT)^3 (\ln S)^2}\right)$$
(8)

271 where J is the primary nucleation rate, A is a preexponential term,  $\gamma_{sl}$  is interfacial energy 272 between solid and liquid, v is molecular volume, k is the Boltzmann constant, T is absolute 273 temperature, and S is the supersaturation ratio as defined earlier. The term  $\phi$  is an empirical 274 parameter whose value is 1 for homogeneous nucleation (heterogeneous surfaces play no role in 275 the nucleation event) and between 0 and 1 for heterogeneous nucleation (the presence of heterogeneous surfaces lowers the energy barrier to nucleation). Paxton et al.<sup>41</sup> showed the effect 276 277 of  $\phi$  in distinguishing between homogeneous and heterogeneous nucleation of chicken egg-white 278 lysozyme. Because the effect of supersaturation in the exponential term is much greater than in the preexponential, the equation is often written as:<sup>34</sup> 279

280 
$$J = A' \exp\left(-\frac{\phi 16\pi \gamma_{sl}^3 v^2}{3(kT)^3 (\ln S)^2}\right)$$
(9)

Alternative mechanisms for primary nucleation have been proposed, including a two-step process in which a metastable liquid phase is formed prior to formation of solid. These are reviewed in various sources but are beyond the scope of this review.<sup>36, 42</sup>

It is generally recognized that solutions can maintain supersaturation without primary nucleation taking place over modest observation timescales. Classical nucleation theory shows that formation of a stable nucleus at low supersaturations is rare, but then substantial nucleation occurs beyond a threshold referred to as a metastable limit. The region of a phase diagram between solubility and nucleation is referred to as a metastable zone; at a given solute concentration, the difference between the saturation temperature and the temperature at which nucleation occurs is known as the metastable zone width (MSZW). Figure 2 illustrates behavior of mixtures of DL-glutamic acid in water by showing solubility and metastable limits obtained
when initially undersaturated solutions were cooled at different rates. Clearly, metastable limits
are not thermodynamic quantities.



295 296

294

Figure 2. Solubility and metastable limits for glutamic acid. Adapted from the work of Svang-Ariyaskul.<sup>43</sup>

297 Primary nucleation in the metastable zone is unlikely but not impossible. More than 550 298 references emerged from a recent search using key words nucleation and metastable zone, 299 demonstrating the effort that has gone into measuring how the metastable limit varies according 300 to the system in which it is measured. The width of the metastable zone has been measured to be as wide as 55 °C for citric acid ( $\sigma \approx 1.4$ ) with a cooling rate of 0.05 K/min.<sup>44</sup> Kashchiev *et al.*<sup>45</sup> 301 and Kashchiev and van Rosmalen<sup>46</sup> provide a formula for estimating the width of metastable 302 303 zones. In cooling crystallization, the MSZW increases with increased cooling rate (see Figure 2). 304 Ma *et al.* found the same result for reactant addition rate; they showed that in the reactive crystallization of lithium carbonate, increasing the addition rate led to a larger MSZW.<sup>47</sup> 305 Generally, the MSZW increases as the rate of supersaturation generation increases. Boukerche et 306 al.<sup>48</sup> found that adding heterogenous solids reduced metastable zone widths and facilitated 307 308 primary nucleation of different polymorphs. Sparging of inert gases was found to shrink the MSZW for several systems<sup>49</sup> and lessen the induction time.<sup>50</sup> 309

310 Primary nucleation rates are often linked to induction time, which is defined as the 311 elapsed time between a solution becoming supersaturated and observation of nuclei formation. 312 An estimate of this quantity frequently assumes that the time to form a nucleus is much greater 313 than the time required for that nucleus to grow to observable size. The stochastic nature of 314 primary nucleation contributes to variability in induction-time measurements, which have been correlated to probability distribution functions.<sup>51-55</sup> Interestingly, most, if not all, of the studies 315 observing stochastic outcomes are in small volumes (frequently 1 mL). Noting this, other 316 317 researchers have pointed out that as system volume increases, the observed stochasticity in both induction time and MSZW is diminished.<sup>56, 57</sup> Kadam et al.<sup>56</sup> described experiments on 318 319 paracetamol nucleated from clear 1-mL and 1-L solutions. In the former, MSZWs in many 320 experiments ranged from 7.2 °C to 33.8 °C. Variations in the 1-L experiments were low, having MSZWs between 7.0 °C and 7.5 °C: in other words, near the lower end of the range for 1-mL 321 measurements. Evolving from such observations, Kadam et al.<sup>56</sup> proposed what they called the 322 323 Single Nucleus Mechanism, which postulates that at a given supersaturation a single nucleus 324 forms and ultimately leads to secondary nucleation. Kadam et al.<sup>52</sup> extended this analysis by 325 suggesting that MSZW is a volume-dependent stochastic property in which the stochastic nature 326 of primary nucleation is dominant in systems of small volume; however, increasing system 327 volume enhances the probability of primary nucleation, making it deterministic at sufficiently 328 large volumes.

329 Uncertainties associated with primary nucleation lead to the common practice of seeding, 330 which is intentionally adding pre-existing crystals of the desired species into the system expected 331 to produce product crystals. This shift in the controlling phenomenon from primary to secondary 332 nucleation is especially useful in industrial settings where reproducibility of outcomes is a 333 paramount consideration. Moreover, after startup, continuous crystallizers maintain a slurry of 334 crystals which serves to repopulate itself through secondary nucleation. By this mechanism, a 335 metastable polymorph may be produced continuously. Kollges and Vetter predicted by modeling 336 and demonstrated with metastable  $\beta$ -L-glutamic acid that by tuning the residence time of the 337 reactor to the secondary nucleation kinetics (or adjusting the secondary nucleation kinetics by milling) a population of the metastable form could be sustained indefinitely.<sup>58, 59</sup> Similar results 338 were found by Agnew *et al.*<sup>60</sup> for Form II of paracetamol. 339

340 Any mechanism involving existing crystals in the formation of new crystals is referred to 341 as secondary nucleation. In the late 1960s and early 1970s, considerable research identified this form of nucleation as an important aspect of crystal formation, especially in industrial settings. 342 This early work was summarized in a foundational review by Garside and Davey<sup>61</sup> and a later 343 review provided by Agrawal and Paterson.<sup>62</sup> Among several mechanisms of secondary 344 nucleation, contacts or collisions of existing crystals with other crystals, crystallizer internals, 345 346 circulation pumps and impellers, which is known as contact nucleation or collision breeding, is 347 considered most important. Contact nucleation is characterized by a low-order dependence on 348 supersaturation (compared to primary nucleation) and absence of a metastable region. The latter 349 factor means that substantial secondary nucleation can occur at low supersaturation. Although 350 secondary nucleation is often considered to be a form of attrition,\* it need not produce macroscopic damage to parent crystals (those from which secondary nuclei are produced).<sup>63-70</sup> 351 352 Secondary nucleation kinetics have been examined extensively for stirred-tank 353 crystallizers, with some of the early proposed correlations provided by Grootscholten et al.,<sup>71</sup> Ploss and Mersmann,<sup>72</sup> and others. Lewis *et al.*<sup>36</sup> summarize such relationships in two related 354 355 power-law equations that link nucleation rate to variables such as impeller speed, power input, 356 and mass of crystals per unit volume:

357  
$$B_{sec} = k_{N}G^{i}N^{k}M_{T}^{j}$$
$$B_{sec} = k_{N}'S^{a}P^{b}M_{T}^{j}$$
(10)

where  $B_{sec}$  is the secondary nucleation rate [number/volume·time], *G* is crystal growth rate, *N* is rotational speed,  $M_{T}$  is a measure of the crystal concentration in the stirred-tank system (usually mass of crystals/volume of either slurry or solvent), *S* is supersaturation ratio, *P* is specific power input, and the other quantities are fitted parameters. Such correlations overlook some important process variables, such as type of impeller and existence of baffles or a draft tube and are likely to be most useful in scaling up between similar crystallizer geometries.

The roles of primary and secondary nucleation in a batch operation depend on whether seeding is used. Beginning with a clear solution (unseeded) means primary nucleation is an

<sup>\*</sup> In this context, attrition is taken to mean removal of small parts of a crystal by abrasion, collision, or friction.

366 essential step in crystal formation. Even so, it is likely that crystals resulting from primary 367 nucleation grow and then serve as stimuli for secondary nucleation, analogous to the Single Nucleus Mechanism.<sup>52</sup> Li et al.<sup>73</sup> used experiments in which paracetamol was crystallized from 368 clear solutions in ethanol to evaluate models, and then used these models to demonstrate that 369 370 only a small fraction of the final crystals per batch originated from primary nucleation. The 371 modeling results indicate that the foremost role of primary nucleation is to produce a small 372 number of crystals, which then serve to stimulate secondary nucleation. The overall rate of 373 crystallization in seeded batch and continuous operations is generally dominated by secondary 374 nucleation.

375 *Crystal growth* rates depend on how they are measured, and they may be expressed in 376 terms of those measurements. For example, both the linear advance rate of a specific crystal face 377 and the rate of change in a characteristic dimension (which, again, can be determined in a variety 378 of ways) are measures of growth kinetics. The rates of change in the mass of a crystal or a 379 population of crystals also provide growth rates. These seemingly different measures are related 380 through crystal shape and density:

$$\frac{dm_{\rm crys}}{dt} = 3\rho \frac{k_{\rm v}}{k_{\rm a}} a_{\rm crys} G \tag{11}$$

where  $m_{\text{crys}}$  and  $a_{\text{crys}}$  are the mass and interfacial area of a crystal,  $\rho$  is its density,  $k_{\text{a}}$  and  $k_{\text{v}}$  are area and volume shape factors (quantities that relate crystal surface area and volume to a selected characteristic dimension), and *G* is rate of change in the characteristic crystal dimension.

At least two resistances in series must be overcome for growth to occur: (1) transport (by diffusion or convection) of a solute species though solution to the crystal face and (2) incorporation of solute into a crystal lattice. The rates at which the two processes occur must be equal at steady state, and the growth rate may be expressed in terms of transport coefficients and driving forces associated with each:

390

$$G = k_d \left( c - c_{\text{int}} \right) \tag{12}$$

391

 $G = k_r (c_{\rm int} - c)^r$ (13)

392 where r,  $k_d$ , and  $k_r$  are fitted parameters, c is solute concentration and  $c_{int}$  is solute concentration 393 at the crystal-solution interface. Should the dominant resistance to growth lie in surface incorporation,  $c \to c_{int}$  and  $G = k_r (c - c^*)^r$ ; alternatively, if the dominant resistance is transport to the crystal surface,  $c_{int} \to c^*$  and  $G = k_d (c - c^*)$ .

Concepts of how molecules or ions incorporate into a growth face generally are based on either birth-and-spread or screw-dislocation theories. Mechanistic descriptions of these approaches, along with primary sources, are provided in several references.<sup>34, 36</sup> An empirical power-law expression can be used to relate growth kinetics to supersaturation by fitting growthrate data:

401

$$G = k_{G} A_{G} \sigma^{g} \tag{14}$$

402 where  $k_G$  is a rate coefficient and  $A_G$  is the surface area of the crystals. The exponent *g* is a fitted 403 parameter with typical values between 1 and 2. This range of values for *g* encompasses those 404 resulting from the cited theories, but, as demonstrated by Soto and Rasmuson,<sup>74</sup> distinguishing 405 among the birth-and-spread and spiral growth theories is difficult; the empirical power-law is 406 often sufficient.

407 Empirical expressions used to correlate nucleation and growth kinetics should be 408 developed in systems similar to those for which the expressions are to be used. Reactive 409 crystallizations present challenges in that regard because of the inherent presence of species 410 other than a primary crystalline product; in other words, reactants, byproducts, and other species 411 can impact crystallization kinetics of product crystals. The effect can result from changing either 412 the solubility (as discussed previously) or nucleation and/or growth kinetics. Illustrations of the effect on growth kinetics are provided by Capellades et al.<sup>75</sup> who found that impurities from 413 414 upstream operations impacted the growth rate of the antibiotic ciprofloxacin in a continuous crystallizer, while having little effect on nucleation kinetics. McDonald et al.<sup>17</sup> found that during 415 416 the reactive crystallization of cephalexin (which is from an antibiotic family that is different from 417 ciprofloxacin) the presence of reactants inhibited crystal growth in a mechanism dependent on 418 both the reactant concentration and cephalexin supersaturation. Neither of these two studies found an effect of co-solutes on nucleation kinetics. Kubota<sup>76</sup> presents a broad review of the 419 420 impact of co-solute species on crystal growth.

421 *Chemical Reactions*. Two broad categories of reactions are considered in this review:
 422 ionic reactions and covalent reactions. Both will be covered in sections that provide specific
 423 examples of such systems.

16

## **Reaction Chemistry & Engineering**

424 Ionic reactions are defined by bonds formed from electrostatic attractions between 425 oppositely charged ions; for example, a positive sodium ion and negative chloride ion in sodium 426 chloride (NaCl). Ionic reactions tend to be very fast; formation of the bond requires only 427 displacement of solvent molecules from the solvation shell and the interaction is governed 428 principally by coulombic forces. Computational work on aqueous NaCl crystallization suggests 429 that the rate limiting step in this reaction between Na<sup>+</sup> and Cl<sup>-</sup> is the removal of water from the chloride attachment site on the NaCl crystals.<sup>77</sup> One caveat to these results is the low 430 431 supersaturations studied. The ability of water to transport protons at a rate faster than expected 432 by diffusion suggests that in neutralizations (see below) the solvent may not pose the same barrier as in inorganic ionic systems like the NaCl system.<sup>78</sup> 433

434 Neutralizations are a subset of ionic reactions that involve the addition or removal of a proton from a proton-labile functional group such as an acid, amine, or alcohol. Neutralization 435 reaction rates are often considered instantaneous in the reactive crystallization literature.<sup>3, 79-81</sup> 436 437 The rates are governed by the collision frequency of the reactants; every collision between 438 reactants results in the product being formed, regardless of collision energy or orientation. 439 Therefore, these reactions are often treated as mixing-limited or diffusion-limited. Many studies investigate means of mixing reactants to ensure a uniform reaction,<sup>81-85</sup> with a minireview by 440 Tevchene et al.<sup>86</sup> The equilibrium composition of these reactions is highly pH-dependent in 441 442 aqueous systems; in organic solvents equilibrium composition depends on the species as well as 443 the proton capacity of the solvent.

444 Covalent reactions involve forming bonds requiring the sharing of electrons between 445 atoms. These reactions range from very slow to fast and often require a catalyst; both the flow 446 timescale of the reactor and diffusion in and out of the catalyst (if a heterogeneous catalyst is 447 used) may impact the effective reaction rates and overall conversion. While many covalent 448 reactions require a catalyst to proceed at appreciable rates, the presence of the catalyst does not 449 change the reaction equilibrium, which may favor reactants or products, depending on the 450 specific system. Many covalent reactions involve networks or series of reactions, which further 451 complicate reaction equilibria since the products of one reaction are reactants in another. 452 Covalent reactions may also be most amenable to reactive crystallization, as they may benefit 453 from shifts in equilibrium, enhancements in rate and selectivity, isolation of intermediates, and 454 many of the other motivators for implementing a reactive crystallization process.

455 The rate of reaction is described by an equation that expresses the rate of reactant 456 consumption as a function of reactant concentration and reaction conditions (such as 457 temperature, pressure, etc.). The function can be derived empirically, from insight into the 458 reaction mechanism, or through first-principle approaches in computational chemistry. For the simple reaction A  $\rightarrow$  B, the elementary rate equation could be  $r = -dc_A/dt = k_1 c_A^n$  where the rate 459 constant  $k_1$  is typically a function of reactor conditions (e.g. temperature),  $c_A$  is the concentration 460 of A (mol/L), and the exponent n is the reaction order. If the reverse reaction  $B \rightarrow A$  also occurs 461 then the overall rate equation for A (assuming a first order reaction so that n = 1) would be 462  $r = k_1 c_A - k_{-1} c_B$  where the subscript -1 indicates the reverse of the forward reaction.<sup>87</sup> 463

Reaction equilibrium occurs when the rates of the forward and reverse reactions are equal 464 and therefore the overall rate is zero; that is,  $dc_A/dt = 0.^*$  Such conditions are reached when 465 466 sufficient product has accumulated for the forward (desired) and reverse reactions to have equal 467 rates. The ratio of the forward and reverse rate constants,  $k_1$  and  $k_{-1}$ , is the equilibrium constant,  $K_{eq} = c_{B}/c_{A}$ . Equilibrium for a reaction system involving multiple reactions (for example, 468  $A \rightleftharpoons B \rightleftharpoons C$ ) means that the concentrations of all species are constant and the reaction 469 470 equilibrium constant for the overall system is the product of the individual equilibrium constants: 471  $K_{\text{overall}} = K_1 K_2$ . If the concentration of a compound, such as species B in the above system, is 472 elevated above its solubility, then crystallization removes the species from solution and pulls the 473 reaction further towards its production. Overall equilibrium of the system is reached when there 474 is no driving force for reactions, crystal nucleation, growth, or dissolution (i.e. the chemical 475 potential of each species is the same in all phases, and temperature and pressure are uniform).

In reactive crystallization, elementary kinetic expressions may be unknown, in which case empirical relations can be derived. Take for example the reactive crystallization of a cropprotection agent, Z, considered by Bhamidi *et al.*<sup>88</sup> The agent is synthesized in the reaction 2A +  $M \rightarrow Z$  with Z crystallizing from the water/methanol reaction solvent. It was empirically determined that consumption of M followed the rate equation  $-dc_M/dt = k_1c_Ac_M$  where  $k_1$  is the rate constant, and  $c_A$  and  $c_M$  are the concentrations of A and M respectively. An Arrhenius

<sup>\*</sup> This situation is analogous to solid-liquid equilibrium where the rates of crystallization and dissolution are equal.

relationship accounted for the dependence of  $k_1$  on temperature,  $k_1 = k_0 \exp(-E_A/RT)$  where  $k_0$ is the frequency factor,  $E_A$  is the activation energy, R is the universal gas constant, and T is the temperature. They were able to determine the heat of reaction as well as the activation energy and frequency factor using calorimetry. The relatively simple expression used here was sufficient for an economic analysis of the homogeneous uncatalyzed reaction to produce Z.

487 Complicated expressions are often required to describe complex reactions, especially 488 those requiring catalysts. Uncatalyzed reactions may only have one or two local energy minima 489 along their reaction pathway; catalyzed reactions, on the other hand, often have a more 490 complicated energy pathway with several transition states and energy minima corresponding to 491 different interactions between the catalyst and reacting species. Each of these steps has the 492 potential to be a rate-limiting transition state, leading to complex rate equations.

For example, enzymes, which represent an important class of catalysts, were used in a reactive crystallization leading to deracemization of amino acids.<sup>89</sup> The authors of that study confirmed that in the reactive crystallization the enzyme D-amino acid oxidase followed Michaelis-Menten kinetics:

497 
$$r = c_{\rm enz} \frac{k_{cat} c_{\rm A}}{K_{\rm M} + c_{\rm A}}$$
(15)

498 where  $c_{enz}$  is the concentration of the enzyme,  $c_A$  is the concentration of the reactant,  $k_{cat}$  is the 499 catalytic rate constant, and  $K_M$  is the Michaelis constant. When the reactant concentration is large 500 ( $c_A >> K_M$ ), as is often the case, the reaction rate varies only with the enzyme concentration, 501 rendering catalyst concentration an important design variable.<sup>87</sup> When  $c_A << K_M$  the rate is 502 sensitive only to the reactant concentration.

503 Catalyzed reactions involving two reactants require rate equations of even greater 504 complexity; at different concentration regimes the order of the reaction may appear to change as 505 the rate-limiting step shifts from one state to another. An example is palladium-catalyzed 506 hydrogenolysis, involving hydrogen and a second reactant, which is found in several reactive 507 crystallization systems.<sup>90-93</sup> Yap *et al.*<sup>94</sup> found that these reactions follow the mechanism

508  

$$A + S \rightleftharpoons AS$$

$$H_2 + 2 S \rightleftharpoons 2 HS$$

$$AS + HS \rightarrow B + 2 S$$
(16)

- 509 where A is the species undergoing hydrogenolysis, B is the product, and S denotes a catalytic
- 510 surface adsorption site; AS and HS indicate adsorbed reactant and hydrogen, respectively. They
- 511 formulated the rate equation using Langmuir-Hinshelwood kinetics as

512 
$$r = kc_{\rm s}^2 \frac{K_{\rm A}c_{\rm A}(K_{\rm H}c_{\rm H2})^{1/2}}{\left[1 + K_{\rm A}c_{\rm A} + \left(K_{\rm H}c_{\rm H2}\right)^{1/2}\right]^2}$$
(17)

where  $c_A$  and  $c_{H2}$  represent concentrations of reactants A and H<sub>2</sub>,  $c_S$  is the surface concentration of active sites S, and  $K_A$ ,  $K_H$ , and k represent the surface adsorption equilibrium constants for the first reaction, the second reaction, and the rate constant of the third reaction, respectively. The number of reactants is not limited to one (as in the above enzyme example) or two (as in the above palladium example) reactants; in general, increasing the number of species increases the complexity of the overall rate equation unless simplifying assumptions can be made.

519 Catalysts may be homogeneous (dissolved in solution) or they may be heterogeneous; in 520 the latter case, the active material often is bound to a porous, inert support. When a catalyst is a 521 solid, for example platinum supported on ceramic or an enzyme immobilized on a polymer, both 522 the rate of reactant consumption at the catalyst surface and the rate of reactant replenishment by 523 diffusion or convection (from the bulk fluid to the surface) may affect the overall reaction 524 kinetics. Solid catalysts are evaluated by their effectiveness factor  $\eta$ , which is defined as the ratio of the observed reaction rate  $r_{\rm obs}$  to the reaction rate with rapid mass transfer  $r.^{95}$  An 525 526 effectiveness factor close to unity indicates good utilization of the active catalytic material (i.e. 527 the palladium or enzyme on the solid support). An effectiveness factor << 1 indicates inefficient 528 use of the catalytic material; a re-engineering of the catalyst may increase the effectiveness 529 factor, possibly by changing the size or morphology of the catalyst surface, the catalyst loading, 530 the pore size of the inert support, or other aspects of the catalyst. A similar concept for crystal 531 growth involving resistances in series was described in the previous section, although usefulness of the effectiveness factor for crystal growth is limited.<sup>96</sup> 532

533 *Combined Crystallization and Reaction Kinetics*. Taken together, the kinetics of 534 nucleation, growth, and reaction, along with process configuration, determine the quality of the 535 crystal product. For illustrative purposes, four different kinetic scenarios are examined for the 536 first-order reversible reactive crystallization  $A \rightleftharpoons B \rightarrow B_{(s)}$  (with  $K_{eq} = 1$ ) taking place in a batch, 537 isothermal, unseeded system: scenario (1) slow reaction and slow crystallization kinetics (1×), 538 (2) fast reaction and fast crystallization kinetics (5×), (3) slow reaction and fast crystallization 539 kinetics, and (4) fast reaction and slow crystallization kinetics. For each of the four cases, three 540 different relative rates of nucleation and growth were examined, where the primary and 541 secondary nucleation rates (A' and  $k_N$  from Equations 9 and 10, respectively) were increased or 542 decreased by a factor of five. The growth rate was varied to match the concentration profile 543 while compensating for the change in nucleation rate, as is observed experimentally in many 544 well-mixed crystallizers.<sup>97</sup> Details of the simulation are available in the supplementary material.

For each case, the concentrations of reactant A and product  $B_{(S)}$  over time and endpoint normalized population densities (a representation of the more general crystal size distribution) are shown in Figure 3. Experimental observations of the concentration profile and end-point population density can be used to fit nucleation and growth kinetics.<sup>17</sup> As can be seen, depending on the relative rates of reaction, nucleation, and growth, a batch reactive crystallization can yield a variety of population densities, some of which may not meet product specifications. Bimodal or skewed population densities may be particularly problematic.



552

553 Figure 3. Quadrant plot showing solution concentrations (normalized by the saturation concentration) of 554 reactants (dashed blue curves) and products (solid red curves) during the first order reaction  $A \rightleftharpoons B \rightarrow B_{(s)}$  for 555 baseline reaction and crystallization kinetics (gray, lower left), fast reaction baseline crystallization kinetics (pink,

555 baseline reaction and crystallization kinetics (gray, lower left), jast reaction baseline crystallization kinetics (pink, 556 lower right), fast crystallization baseline reaction kinetics (orange, upper left) and fast reaction and crystallization

557 kinetics (white, upper right). The insets depict the population density calculated at baseline nucleation rate (gray),

558 fast nucleation (yellow), and slow nucleation (green); for the different nucleation rates the growth rate was varied

to match the concentration profile. In real systems the growth rate typically varies to match the rate of
 supersaturation generation. The size units and population density have been normalized such that the scale is the
 same in each inset.

562 The concentrations in Figure 3 have been normalized by the solubility of the product, 563 rendering the solid curve the product supersaturation. As expected, with slower crystallization 564 kinetics a larger supersaturation accumulates before crystal growth can match the rate of the 565 reaction. Crystallization is helping to pull the reaction towards the product, as illustrated by the 566 faster consumption of reactant in cases with faster crystallization kinetics. Sustained higher 567 supersaturations lead to large amounts of primary nucleation and bimodal crystal population 568 densities. If the product B were consumed by a second reaction the sustained higher 569 supersaturation would be expected to further decrease yield and productivity. When the rates of 570 reaction and crystallization are scaled together, comparable population density functions are 571 obtained, as can be seen in the similarity between the bottom left and top right insets in Figure 3. 572 In generalizing Figure 3 one realizes that in reactive crystallization systems the rate of 573 crystallization will always lag the reaction, a consequence of the sequential nature of the process. 574 Enhancing the rate of crystallization (and the benefits of reactive crystallization) can be 575 accomplished by increasing the rate of the reaction, as can be seen comparing the bottom two 576 panes of Figure 3; the faster reacting system spends less time at an elevated supersaturation and reaches a higher peak supersaturation. Alternatively, the kinetics of crystallization can be sped 577 578 up by techniques such as milling, which is discussed in a later section, to improve overall yield 579 and size distribution. A detailed understanding of the process kinetics is indispensable for 580 producing material with the desired properties in a process with the desired performance.

- 581 **Types of Reactions**
- 582 *Crystallization and Ionic Reactions.* Ionic compounds utilized in applications ranging 583 from pharmaceutical additives<sup>98, 99</sup> to polymer fillers,<sup>100, 101</sup> can be produced via reactive 584 crystallization. Processes involving reactive crystallization can be used for removing 585 contaminants, such as heavy metals, from water,<sup>102-104</sup> or for separating a product, such as 586 lithium carbonate, from solution.<sup>105, 106</sup> Ionic reactions include synthesis of inorganic 587 compounds, formation of salts, and neutralization of organic ions.

Reactive crystallization of ionic compounds is based on the reaction between an anion and a cation in solution. The solutions are typically aqueous, but other solvents, such as supercritical CO<sub>2</sub>, have been used.<sup>107</sup> The solubility of the target compound is often substantially

22

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591 lower than that of precursors supplying the reacting ions. For sparingly soluble ionic species,

solubility is usefully defined in terms of a solubility product. For example, for the species  $A_aC_c$ 

having an anion A with a negative charge c- and a cation C with a positive charge a+, the

594 solubility product  $K_{sp}$  is given by

595

$$K_{\rm sp} = \left[\mathbf{A}^{c-}\right]_{\rm eq}^{a} \left[\mathbf{C}^{a+}\right]_{\rm eq}^{c} \tag{18}$$

596 where the bracketed terms represent the concentrations of ions at equilibrium in mol/L. The 597 relative supersaturation  $\sigma$  for the compound  $A_aC_c$  may be defined as:

598 
$$\sigma = \frac{\left[A^{c-}\right]^a \left[C^{a+}\right]^c - K_{sp}}{K_{sp}}$$
(19)

 $[A^{c-}]$  and  $[C^{a+}]$  are the anion and cation concentrations at system conditions in the same units 599 600 used for  $K_{sp}$ . The time course of ion concentrations during a process can be measured using an ion-selective electrode,<sup>108</sup> a conductivity sensor,<sup>99</sup> or a spectrophotometric probe, such as a UV-601 vis probe,<sup>109</sup> an IR probe,<sup>110</sup> or a Raman probe.<sup>111</sup> In systems with high ionic strength, Equations 602 603 18 and 19 should be modified by replacing each concentration with an activity, which is defined 604 as the product of a concentration and an activity coefficient. In systems at low concentration, 605 ions do not interact with each other and the activity coefficient can be assumed to be unity, 606 otherwise, the activity coefficient for each species can be estimated using the Debye-Hückel theory.<sup>112</sup> Note that in some cases (for example, the production of calcium phosphate), the 607 608 compounds may have several dissociation states, depending on pH value, and the solubility product should be corrected to take that feature into account.<sup>105</sup> 609

610 A common theme in many ionic reactive crystallization studies is that the reaction between the anion and cation is considered instantaneous. The dynamic behavior of the system is governed 611 612 by crystal nucleation, growth, and mixing. Fast reaction kinetics contrast with those undergoing 613 covalent reactions such as enzymatic synthesis and crystallization of ampicillin, where the reaction step limits the overall timescale of the process.<sup>113</sup> Rapid reaction kinetics, in addition to the 614 615 formation of a practically insoluble compound, may lead to very high levels of supersaturation. In 616 such cases, the mixing strategy, especially in fed-batch systems, can have a significant impact on process attributes such as crystal size distribution and shape.<sup>114</sup> Mixing will be discussed further 617 618 in the process design sections.

619 Examples of inorganic compounds produced by reactive crystallization are hydroxides such as nickel<sup>85</sup> and aluminum hydroxide,<sup>115</sup> carbonates such as lithium<sup>98, 106</sup> and calcium 620 carbonate,<sup>116</sup> phosphates such as calcium phosphate,<sup>105</sup> and sulfates such as barium sulfate.<sup>79</sup> 621 Table 1 summarizes some of the representative inorganic ionic reactive crystallization studies 622 623 and precursor materials used in each. These systems have been examined from different viewpoints, including developing kinetic models for crystal nucleation and growth,<sup>98</sup> prediction 624 and control of particle size distribution,<sup>108</sup> the effect of process parameters such as stirring rate 625 on product size and morphology,<sup>116, 117</sup> and the effect of different additives on polymorph 626 formation.118 627

Gas-liquid reactive crystallizations result from contacting liquid and gas phases
containing reactants whose combination produces a crystalline product. Many of these systems
involve synthesis of carbonates through direct injection of CO<sub>2</sub> gas into the crystallizer.<sup>117, 119, 120</sup>
The gaseous CO<sub>2</sub> gets absorbed by the liquid phase to form the carbonate ion:<sup>120</sup>

632

$$CO_{2(g)} + H_2O \rightarrow CO_3^{2-} + 2H^+$$
(20)

633 The carbonate ions then react with cations to produce solid species. Several groups have studied 634 the effect of different gas-injection variables such as bubble size and CO<sub>2</sub> mole fraction on the 635 structural and chemical properties of the crystal product. For instance, Matsumoto et al.<sup>117</sup> 636 controlled the polymorphic form of calcium carbonate crystals by manipulating the CO<sub>2</sub>-to-N<sub>2</sub> ratio of the inlet gas. Varma et al.<sup>120</sup> used the same method with different dispersion agents, 637 including citrate ions and polyacrylic acid, for producing calcium carbonate nanocrystals. These 638 639 systems can be used both for the recovery of metals from solutions and potential removal of  $CO_2$ from industrial gas streams.<sup>120, 121</sup> 640

641 A similar approach was proposed and illustrated for production of hydroxides by 642 injecting ammonia gas into the crystallization solution to produce hydroxide ions:<sup>101</sup>

643

$$\mathrm{NH}_{\mathcal{A}(\alpha)} + \mathrm{H}_{2}\mathrm{O} \to \mathrm{NH}_{4}^{+} + \mathrm{OH}^{-}$$

$$\tag{21}$$

In these gas-liquid-solid cases, the absorption of gaseous reactant into the liquid phase can affect the supersaturation and kinetics of the process. Attempts have been made to model this transport limitation, such as proposing a double-film theory-based mass-transfer model.<sup>122-124</sup>

Table 1 highlights some of the studies of reactive crystallization in the types of inorganic
systems discussed above. The studies include continuous and batch processes with various

649reactor configurations. In inorganic systems the focus tends to be crystallization-centric, as seen650from the last column in the table. The listed works either give insight into a specific651crystallization phenomenon, such as growth mechanism, size control, or polymorph control, or652are case studies on process designs for recovery of a certain species, such as nickel from653wastewater or  $CO_2$  from flue gas. In the coming sections it will be shown that many desirable654features of reactive crystallization, such as equilibrium modification and intermediate isolation,655are more common in organic systems.

Table 1. A list of representative studies on the reactive crystallization of ionic compounds with the
precursors used and the focus of the work. MgDS<sub>2</sub> stands for dodecyl sulfate, FB for fluidized bed, and CSD for
crystal size distribution.

Product	Reference No.	Reactant 1	Reactant 2	Focus
Carbonate				
Li <sub>2</sub> CO <sub>3</sub>	106	LiOH	CO <sub>2</sub>	Li and CO <sub>2</sub> recovery
Li <sub>2</sub> CO <sub>3</sub>	98	Li <sub>2</sub> SO <sub>4</sub>	Na <sub>2</sub> CO <sub>3</sub>	Crystallization kinetics
Li <sub>2</sub> CO <sub>3</sub>	125	LiCl	Na <sub>2</sub> CO <sub>3</sub>	Growth morphology
Li <sub>2</sub> CO <sub>3</sub>	121	LiCl	$CO_2$	Growth mech./product characterization
Li <sub>2</sub> CO <sub>3</sub>	126	LiCl	Na <sub>2</sub> CO <sub>3</sub>	Effect of additives on shape/size
CaCO <sub>3</sub>	116	Ca(OH) <sub>2</sub>	Na <sub>2</sub> CO <sub>3</sub>	Crystal polymorph control
CaCO <sub>3</sub>	117	CaNO <sub>3</sub>	CO <sub>2</sub>	Crystal polymorph control
CaCO <sub>3</sub>	120	Ca(OH) <sub>2</sub>	CO <sub>2</sub>	Nanocrystal formation
CaCO <sub>3</sub>	127	CaCl <sub>2</sub>	Na <sub>2</sub> CO <sub>3</sub>	Crystal polymorph control
CaCO <sub>3</sub>	128	CaCl <sub>2</sub>	Na <sub>2</sub> CO <sub>3</sub>	Crystal polymorph control
CaCO <sub>3</sub>	118	CaCl <sub>2</sub>	NaHCO <sub>3</sub>	Effect of additives on size/morphology
CaCO <sub>3</sub>	129	Ca(OH) <sub>2</sub>	CO <sub>2</sub>	Effect of additives on size/morphology
CaCO <sub>3</sub>	119	Ca(OH) <sub>2</sub>	CO <sub>2</sub>	Crystallization kinetics
MgCO <sub>3</sub>	130	$Mg(OH)_2$	$CO_2$	Effect of gas flow/stirring on process
NiCO <sub>3</sub>	102	NiSO4	Na <sub>2</sub> CO <sub>3</sub>	Fluidized bed reactor design
NiCO <sub>3</sub>	131	NiSO <sub>4</sub>	Na <sub>2</sub> CO <sub>3</sub>	Metal recovery and effect of seeding
BaCO <sub>3</sub>	108	BaS	Na <sub>2</sub> CO <sub>3</sub>	Crystallization kinetics and CSD
BaCO <sub>3</sub>	132	BaCl <sub>2</sub>	Na <sub>2</sub> CO <sub>3</sub>	Crystallization kinetics
BaCO <sub>3</sub>	133	BaCl <sub>2</sub>	$(NH_4)_2CO_3$	Crystallization kinetics and morphology
Hydroxide				
Ni(OH)2	85	NiSO4	NaOH	Study of airlift-loop reactor
Ni(OH)2	134	NiSO4	NaOH	Ni recovery from wastewater
Al(OH) <sub>3</sub>	115	NaAl(OH) <sub>4</sub>	NaHCO <sub>3</sub>	Crystallization kinetics and morphology
Mg(OH) <sub>2</sub>	99	$Mg(NO_3)_2$	NaOH	Crystallization kinetics
$Mg(OH)_2$	101	MgCl/DS <sub>2</sub>	NH <sub>3</sub>	Impact of metal source on shape
Ca(OH) <sub>2</sub>	135, 136	CaCl <sub>2</sub>	NaOH	Crystallization kinetics
Phosphate				
CaClH <sub>2</sub> PO <sub>4</sub>	105	CaCl <sub>2</sub>	H <sub>3</sub> PO <sub>4</sub>	Process design for PO <sub>4</sub> recovery
CaHPO <sub>4</sub>	137	$Ca(NO_3)_2$	K <sub>3</sub> PO <sub>4</sub>	Effect of additives on size/shape
MgHPO <sub>4</sub>	138, 139	MgCl <sub>2</sub>	NaH <sub>2</sub> PO <sub>4</sub>	FB reactor for phosphate removal
MgHPO <sub>4</sub>	140	MgSO <sub>4</sub>	NH <sub>4</sub> H <sub>2</sub> PO <sub>4</sub>	Effect of pH on product solid phase
Sulfate		-		
BaSO <sub>4</sub>	79	BaCl <sub>2</sub>	Na <sub>2</sub> SO <sub>4</sub>	Process optimization
BaSO <sub>4</sub>	114	BaCl <sub>2</sub>	Na <sub>2</sub> SO <sub>4</sub>	Effect of mixing on CSD
BaSO <sub>4</sub>	83	BaCl <sub>2</sub>	Na <sub>2</sub> SO <sub>4</sub>	Effect of ultrasound on nucleation

659

Examples of organic ionic products from reactive crystallizations include calcium<sup>141</sup> and magnesium<sup>142</sup> carboxylates, amines with carboxylic acid anions,<sup>80</sup> and amphoteric molecules

such as amino acids.<sup>143</sup> Together these reactions are termed neutralizations because they remove 662 663 acids or bases from solution. They are highly pH-dependent as many species only possess the 664 required charge in a specific pH range. Some neutralizations are fermentation-based where the 665 primary reactant is glucose, although many other nutrients are needed by the fermenting 666 microbes. The motivation for each of the cited works on organic ionic reactions is different, and ranges from demonstration of continuous reactive crystallization in a chemical plant<sup>144</sup> to yield 667 enhancement by product sequestration<sup>145</sup> to crystal size optimization.<sup>146</sup> Applications of organic 668 669 ionic reactive crystallizations include pharmaceutical development, carbon capture, and 670 production of chemicals from renewable platforms.

671 Specially tailored amines are used to remove carboxylates or other anions selectively from solution. Custelcean et al.<sup>147</sup> engineered a m-benzene-(bis-iminoguanidine) (m-BBIG) 672 673 anion for crystallization of an amino-carbonate salt for direct air capture and sequestration of carbon dioxide. A much different application was described by Sturm et al.<sup>148</sup> who used 674 675 diphenylamine to crystallize the pharmaceutical compound cefdinir from a solution of impurities. 676 In addition to carboxylates, specialty amines can be used in reactively crystallizing other highly soluble anions. Custelcean et al.<sup>149</sup> synthesized urea functionalized amines to remove sulfate 677 678 from a nuclear-waste simulant and examined the competition between accelerated reaction 679 kinetics and increased solubility as the system temperature is increased. In these cases, 680 engineered amines were used to remove specific anions by reactive crystallization,

681 Amines can also be removed from solution through reactive crystallization. However, unlike the cases for carboxylic acids, simple ammonium salts tend to have high solubility,<sup>150</sup> 682 which means complex anions are needed to form salts with low solubility. Aakeroy et al.<sup>151</sup> 683 684 screened 105 potential reactive crystallizations of amines with carboxylates and found 30 685 combinations in which crystal products resulted, although the kinetics of these reactions and the possible role of solvent evaporation are unclear. Quon *et al.*<sup>80</sup> developed a continuous approach 686 to crystallize the amine drug aliskiren as the hemifumarate salt. Cole et al.<sup>152</sup> produced the amine 687 688 drug prexasertib as the lactate salt. While many amines are crystallizable as carboxylate salts, the 689 applications are mostly limited to specialty and pharmaceutical chemicals produced in low 690 volumes. General guidance for producing solid amines takes advantage of the reduced solubility of the free amine compared to their salts,<sup>150</sup> reacting the amine salt with a hydroxide to 691 692 crystallize the free amine.

693 Reactive crystallization may be used to control the pH in a fermenter, as in the synthesis 694 of carboxylic acids such as citric, lactic, gluconic, and itaconic acids. Synthesis of the acids 695 decreases the pH in the fermenter, and at high concentration can halt the fermentation. Addition 696 of a neutralizing base such as one of the calcium compounds Ca(OH)<sub>2</sub>, CaO, or CaCO<sub>3</sub> stabilizes pH and causes many carboxylic acids to crystallize as calcium salts,<sup>153</sup> which may further benefit 697 the fermentation by sequestering inhibitory products.<sup>154</sup> Magnesium compounds are also used, 698 but to a lesser extent.<sup>155</sup> Reactive crystallization with a calcium neutralizing agent is not always 699 the most economical approach to separating carboxylic acids<sup>153, 156</sup>. 700

Figure 4 illustrates several alternative operating procedures for reactive crystallization in the production of carboxylic acids. Line AB' represents neutralization with a calcium compound that produces a saturated solution at B' while Line AB represents neutralization with a soluble base such as sodium hydroxide. The need for neutralization can be avoided by engineering acidtolerant strains of the fermenting microorganism, in which case the operating line of the fermentations may be represented by Line AC.<sup>157</sup>



707

708Figure 4. Concentration of product species in the fermentation broth as a function of broth pH for709metastability, saturation, and process operating lines for the reactive crystallization of an organic acid produced by710fermentation. Black solid curves are solubilities; the black dashed curve is a metastable limit. Line AB represents711fermentation at constant pH with neutralization by NaOH. Line AB' represents fermentation with neutralization by712Ca(OH)<sub>2</sub>. Line BC represents acidification of solution with mineral acid. Curve CD follows the product solubility as713it is crystallized. Line AC follows fermentation using an acid-tolerant microorganism. Point C' represents conditions714at which unseeded crystallization is initiated.



acidification are illustrated in Figure 4, which represent a case in which either seed crystals are

added to initiate nucleation (curve BCD) or primary nucleation at the metastable limit is

followed (curve BC'D). Acidification after fermentation and continuous neutralization with  $Ca^{2+}$ 

are two competing methods to isolate the product acid from a fermentation broth. The same

process is used to isolate amino acids, although amino acids with multiple acid and base moieties

have more complex solubility curves than shown for the monoprotic acid in Figure 4.<sup>161</sup>

The inverse of acidification, deprotonation of an amine by a strong base, is also feasible. However, there are fewer studies of these systems as solid amines are typically limited to specialty chemicals and pharmaceuticals. For example, Diab *et al.*<sup>162</sup> optimized the continuous production of nevirapine with a final reactive crystallization step between sodium hydroxide and nevirapine hydrochloride.

Acidification of an organic acid by a strong mineral acid is at the boundary between ionic and covalent reactions; the product itself is covalent (e.g. RCOOH), but the reactants are ionic (e.g.  $RCOO^- + H^+$ ), and the reaction kinetics are fast (~10<sup>10</sup> mol/sec), which is why acidification is discussed in this section. The organic acid, after receiving a proton from the dissociated strong acid, crystallizes from solution, as exemplified by the chemical equation

734  $6-APA^{-} + HCl \rightarrow 6-APAH_{(s)} + Cl^{-}$  (22)

Typically, though not always, the neutral form of organic acids (or bases) tends to be less soluble than the negatively (or positively) charged deprotonated (or protonated) form in aqueous solution. Ferreira *et al.*<sup>163</sup> exploit this feature to produce the beta-lactam antibiotic precursor 6aminopenicillanic acid (6-APA). 6-APA is produced enzymatically from penicillin G at neutral pH where it exists primarily in a soluble, dissociated state. After complete conversion of penicillin G to 6-APA the solution is acidified to the isoelectric point, pH 3, and the zwitterionic 6-APA crystallizes.

McDonald *et al.*<sup>17</sup> used the extremely fast kinetics of acid/base reactions to study crystallization kinetics in the reactive crystallization of cephalexin. Cephalexin, which can be produced by a slow enzymatic reactive crystallization,<sup>164</sup> was instead crystallized by reacting HCl with a solution of cephalexin sodium. The reaction is mass-transfer controlled and, with sufficient agitation, can be considered instantaneous. By adding the reactants of the enzymatic system to the cephalexin sodium solution, cephalexin nucleation and growth could be studied in a manner representative of the enzymatic process without needing to deconvolute the enzyme

749 reaction kinetics and crystallization kinetics.

- 750 Table 2 lists reactive crystallizations involving organic acids and bases and their salts.
- 751 The diversity of listed compounds is much greater than was the case for inorganic reactive
- rystallizations. The cited studies are also more wide ranging as these species tend not to be the
- model compounds used to study phenomena but are industrial products or intermediates with
- 754 economic motivators for an intensified process.

Table 2. A list of representative studies on the reactive crystallization of acids and bases in which a species is crystallized as a salt or is crystallized as an acid (or base) by acidification with a stronger acid (or base).

Product	Reference No.	Reactant 1	Reactant 2	Focus
Organic Salts				
Aliskiren	80	Aliskiren free	Fumaric acid	Optimization of purity and yield
hemifumarate		base		
Aliskiren	144	Aliskiren free	Fumaric acid	Control of crystallization in an integrated
hemifumarate		base		continuous plant
Amino acid	143	K and Na salts of	$CO_2$	Found enhanced carbon capture using
bicarbonates		amino acids		precipitating CO2 absorbing solvents
<i>m</i> -BBIG carbonate	147	<i>m</i> -BBIG (see text	$CO_2$	Improved ligand for reversible
	146 165	for abbr.)		crystallization for CO2 direct air capture
Sodium	140, 105	Cefuroxime	Sodium	Control of mixing and particle size
cefuroxime	166		acetate	distribution, stability of product
Ca citrate	100	Citric acid	CaO	Large amount of gypsum byproduct, from <i>A. niger</i> fermentation
Ca gluconate	167	Glucose	Ca(OH)2,	Crystallization during fermentation in A.
			CaCO <sub>3</sub>	niger inhibits oxygen transfer
Mg 6-	168	Nicotinic acid	MgO	Hydroxylated by A. xylosoxidans.
hydroxynicotinate	147			Improved yield
Ca lactate	145	Glucose	Ca(OH) <sub>2</sub>	<i>B. coagulans</i> fermentation. 75% yield
	142	~		increase, 1.7x productivity increase
Mg lactate	142	Glucose	MgO	Reduction in water use by 40% and
0 1	160			nutrient use by 43%
Ca malate	107	Ca fumarate		Used overexpressed fumarase, better
Complements	141	Classes	C-(OII)	Enclose with solubilized Calumarate
	170			Concerning in angele from 100( to 010( here
I-PEA DPPA sait		IPA-DPPA	Acetophenone	shifting equilibrium (see text for abbreviations)
Pyridinium salts	151	2-aminopyridine	Carboxylic	Screening for new salts and cocrystals.
		derivative	acids	105 pyridine/carboxylate pairs tested
Ca succinate	171	Glucose	Ca(OH) <sub>2</sub>	Review of several fermentation technologies
NH4 succinate	155	Glucose	Ammonia	Future directions discussed, enhanced regeneration (succinate back to succinic acid) with ammonium salt.
TREN-tris-urea	149	1,1′,1″-	$Na_2SO_4$	Sulfate recovery from nuclear waste by
sulfate		(nitrilotris(ethane-		crystallization with engineered ligands,
		2,1-diyl))tris(3-		kinetic and equilibrium study
		(pyridin-3-yl)urea		
Acids/Bases				
6-amino-	163	6-APA NH4 salt	HCl	Growth and solubility in presence of
penicillanic acid				precursor and byproduct

Amoxicillin	172	Amoxicillin	NaOH	Nucleation and growth in the presence of
trihydrate		hydrochloride		impurities
Ampicillin	173	Ampicillin	HCl	Monitoring with online PAT
trihydrate		sodium		
BACE inhibitor	92	BACE inhibitor	NaOH	Purification, control of particle size,
		hydrochloride		control of fouling
Cefixime	174	Cefixime	HCl	Control of crystal morphology in a mixing
trihydrate		disodium		limited reaction
Cephalexin	17	Cephalexin	HCl	Nucleation and growth in the presence of
monohydrate		sodium		precursor molecules
Cinnamic acid	175	Sodium	HC1	Templating agents reduce induction time
		cinnamate		
Ciprofloxacin	176	Ciprofloxacin	HCl	Continuous process in flow
		sodium		
Fumaric acid	160	Glucose	Na <sub>2</sub> CO <sub>3</sub> ,	Optimize of fermenter neutralization to
			H <sub>2</sub> SO <sub>4</sub>	compete with benzene route
Fumaric acid	157	Glucose	КОН	Review with optimization of feedstocks
		Starch		and organism engineering
Furan dicarboxylic	159	Hydroxymethyl	O <sub>2</sub> , H <sub>2</sub> SO <sub>4</sub>	Recovery of terephthalic acid alternative
acid		furancarboxylate		from <i>P. putida</i> fermenter
Glutamic acid	79	Monosodium	HCl	Continuous manufacturing, control of size
		glutamate		and productivity
Glutamic acid	177, 178	Monosodium	H <sub>2</sub> SO <sub>4</sub>	Modeling, control, and parameter
		glutamate		estimation
Glutamic acid	179, 180	Monosodium	H <sub>2</sub> SO <sub>4</sub>	Control of reactive crystallization
		glutamate		2
p-Hydroxybenzoic	158	<i>p</i> -Hydroxy-	HCl	Electrochemically induced crystallization
acid		benzoate		by manipulation of local pH
Itaconic acid	181	Glucose	NaOH, HCl	Fermentation by A. terreus. Inhibition
				overcome by product removal
Malic acid	182	Fumaric acid	H <sub>2</sub> SO <sub>4</sub>	Fumarase in S. cerevisiae as catalyst.
				Continuous process with electro-dialysis.
				Yield up from 78% to 91%
Nevirapine	162	Nevirapine	NaOH	Continuous manufacturing, including
•		hydrochloride		reactive crystallization, of API
Riboflavin	183	Glucose	NaOH	Review of riboflavin fermentation
				processes

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758 Crystallization and Covalent Reactions. Covalent reactions are inherently more complex 759 than ionic reactions; the bonding moieties tend to be bulky with a variety of characteristics 760 (polarity, hydrophobicity, size, etc.) playing a role in the nature and strength of bonds formed. 761 This section addresses that complexity by dividing covalent systems into three broad categories: 762 non-catalytic, catalytic, and biocatalytic reactions. Lastly, reactive crystallization for chiral 763 resolution, an application with enormous industrial importance and unique operating 764 considerations, is discussed.

765 Dividing covalent reactive crystallization according to the use and nature of catalysts 766 assists in comparing the different process conditions each reaction type requires. Uncatalyzed 767 reactive crystallization is accomplished by controlling only the reactant concentrations and 768 crystallizer conditions (e.g. solvent composition, temperature, etc.). However, catalyzed

769 processes can be adjusted with variation of catalyst properties and loading. Reactive 770 crystallization utilizing traditional metal catalysts may have wider operating ranges than 771 uncatalyzed processes as the catalyst helps decouple reaction rates from important crystallization 772 conditions, such as temperature and solvent composition. Biocatalytic processes are constrained 773 by limited biocatalyst stability, but reactive crystallization is often applied to biocatalytic 774 processes as a means of overcoming other catalyst deficiencies, for example poor selectivity.<sup>184</sup> 775 Chiral resolution by reactive crystallization may be accomplished with any of the listed catalytic 776 strategies provided the reaction, which racemizes the enantiomers, is much faster than the 777 crystallization and prevents nucleation of the undesired form. Chiral resolution is given its own 778 section because of this unusual (in the context of the other examples) operating requirement and 779 industrial importance. Reactive crystallization enables chiral resolution by diastereomeric resolution,<sup>185</sup> preferential crystallization,<sup>186</sup> enantiomeric enrichment,<sup>89</sup> and attrition enhanced 780 deracemization.<sup>187</sup> 781

782 Uncatalvzed covalent reactive crystallization. The literature has relatively few examples 783 of covalent reactive crystallizations that do not use a catalyst. However, one prominent class involves synthesis of amides by coupling amines with acid chlorides.<sup>84, 122, 188</sup> The amines and 784 785 acid chlorides often have higher solubility than the resulting amides, making these products good candidates for reactive crystallization. Liu *et al.*<sup>122</sup> used a fed-batch system as the rate of reactant 786 787 addition provided adequate control over the rate of reaction and rate of generation of 788 supersaturation. As is typical of most crystallization processes, decreased supersaturation 789 suppressed nucleation and increased mean crystal size. Covalent reactions typically cannot be 790 considered instantaneous, and their rate is a strong function of temperature. In the system studied 791 by Liu et al.,<sup>122</sup> raising the temperature was shown to have a stronger effect on increasing 792 product solubility compared to the impact on reaction rate; the outcome was an overall lower 793 supersaturation at higher process temperatures and, concomitantly, larger mean crystal size. 794 While this result is important to note, the competition between increasing reaction rate and 795 solubility with temperature is system-specific and results from a single system cannot be used to 796 predict the outcome for other chemistries.

As another example of uncatalyzed covalent reactive crystallization, Jiang and Ni<sup>189</sup>
studied the synthesis of paracetamol from 4-aminophenol and acetic anhydride. The same
authors investigated several different types of reactors, including batch and continuous

oscillating-baffle reactors and concluded that combining reaction and crystallization improved
 yield by limiting the extent of further paracetamol reactions.<sup>190</sup> It was also found that the growth

802 mechanism for paracetamol was different in an aqueous solvent from that in a predominately

803 acetic acid solvent. Crystal shape also depended on the solvent composition, in qualitative

agreement with the observed change in growth kinetics.

805 Reactive crystallization can provide a framework to understand biological assembly, 806 supporting a means for chemical selection and evolution. For example, the assembly of peptide-807 like polymers into paracrystalline assemblies is driven by uncatalyzed polycondensation 808 reactions. Thioesters of racemic amino acids undergo polymerization and then beta-sheet assembly, providing a selection for isotactic peptides.<sup>191</sup> In a more recent study, peptide aldehyde 809 810 monomers first polymerize, driving a liquid-liquid phase separation from which beta-sheet 811 crystals nucleate and grow. The resulting peptides are highly monodisperse, supporting a secondary nucleation mechanism for templated polymerization.<sup>192</sup> 812

813 It is difficult to adjust the rate of reaction independent of the rate of crystal growth in 814 uncatalyzed reactive crystallizations; both are sensitive to temperature, composition, and 815 concentration. While the lack of a catalyst makes the process simpler, it may complicate 816 production of a specified size, shape, and form of crystal if the reaction rate cannot be adequately 817 controlled.

818 Inorganic catalyzed covalent reactive crystallization. Combining catalysis with reactive 819 crystallization results in complex but useful processes. For example, hydrogenolysis is a commonly encountered reaction that takes place on metal catalysts. Hansen et al.<sup>92</sup> published a 820 821 workup of a BACE (beta-site amyloid precursor protein cleaving enzyme) inhibitor, with 822 potential as an anti-Alzheimer's drug, involving hydrogenolysis of a precursor by hydrogen gas 823 in an aqueous environment with a palladium-on-carbon catalyst. The API (active pharmaceutical 824 ingredient) crystallized in the reaction environment, which made reclaiming the solid catalyst 825 difficult. Rather than pursue a solid-solid separation, acid was added to the reaction solvent to 826 increase the API solubility and allow the catalyst to be filtered off. After catalyst recovery the 827 API was deprotonated by reaction with sodium hydroxide and crystallized based on the 828 acidification mechanism described in the ionic reaction section.

Reactive crystallization to produce terephthalic acid (TPA), a precursor to the ubiquitous polymer polyethylene terephthalate, by oxidizing *p*-xylene can improve the impurity profile of

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839

the resulting product.<sup>193</sup> Species formed during the oxidation, which is catalyzed by soluble

832 cobalt/manganese catalysts with bromine promoter, are shown in Figure 5. Incomplete oxidation

- 833 leads to the formation of 4-carboxybenzaldehyde (4-CBA), which can incorporate into the
- 834 terephthalic acid crystals. Rejection of 4-CBA during crystallization of terephthalic acid is
- paramount as 4-CBA terminates polymerization. Wang *et al.*<sup>193</sup> found that 4-CBA was
- 836 incorporated to a greater extent when the TPA growth rate was faster and seed crystals were not
- 837 used. They developed a process with slow feed rate and higher temperature to minimize impurity
- 838 incorporation, while maintaining the same mean crystal size.



Figure 5. Successive oxidation in the conversion of p-xylene (left) to TPA (right). CBA (second from right)
can incorporate into TPA crystals at high concentration, requiring tuning reaction conditions to prevent buildup of
CBA while maintaining slow formation of TPA for crystal size control.

843 Biocatalytic covalent reactive crystallization. In this section, biocatalytic reactions are 844 described that crystallize products formed from specific reactants. There has already been some 845 discussion on reactive crystallization as it pertains to fermentation, which can be considered a 846 highly non-selective form of biocatalysis (glucose is converted into a myriad of products). In the 847 biocatalysis community reactive crystallization is sometimes referred to as *in situ* product crystallization, ISPC (a subset of *in situ* product removal, ISPR). Hulsewede et al.<sup>194</sup> provide a 848 849 minireview on ISPC; here ISPC is discussed in the general framework of reactive crystallization. 850 Biocatalytic processes are well-positioned to benefit from reactive crystallization. Many 851 biocatalysts, such as whole live cells, are poisoned by high concentrations of products, which can be reduced by reactive crystallization.<sup>195</sup> Other biocatalysts, such as resting or whole dead cells, 852 853 may catalyze undesired reactions with the desired product as reactant, but utilization of reactive crystallization can insulate that product from further reaction.<sup>196</sup> Purified enzymes, while highly 854 855 specific and more resistant to poisoning, often catalyze reactions with equilibrium coefficients on 856 the order of unity leading to low yields; reactive crystallization can shift equilibrium towards products.197 857 858 Synthesis of beta-lactam antibiotics is a well-studied example of a biocatalytic reactive

859 crystallization. Ferreira *et al.*<sup>198</sup> have demonstrated good recyclability of an immobilized

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860 penicillin G acylase (PGA) for production of ampicillin in saturating conditions. The three main

- 861 reactions catalyzed by PGA are shown in Figure 6 for ampicillin; they are synthesis (desired,
- top), reactant hydrolysis (undesired, left), and product hydrolysis (undesired, right). Using PGA
- 863 entrapped in agarose gel particles afforded only slight mass transfer resistance in the catalyst
- 864 particle.<sup>198</sup> After some time, the solution saturated and ampicillin crystallized because the
- 865 reactants, phenylglycine methyl ester (PGME) and 6-APA, are both more soluble than ampicillin
- 866 on a molar basis. Once again, the crystallization made reclaiming the catalyst difficult and so the
- 867 product was dissolved after filtration, leaving behind the immobilized enzyme for recycling.
- 868 Another study used a soluble version of the same enzyme to increase the selectivity towards
- ampicillin by >50% by sequestering the product from enzymatic hydrolysis by crystallization.<sup>4</sup>



- 870
- Figure 6. PGA-catalyzed synthesis of ampicillin (desired, top), hydrolysis of phenylglycine methyl ester,
   PGME (undesired, left), and hydrolysis of ampicillin (undesired, right).

873 The value of the biocatalyst (relative to the value of the product) often dictates whether 874 the catalyst is immobilized on a solid, which enables catalyst recovery and reuse, or is soluble, 875 enabling product recovery by filtration. In the case of ampicillin, the product is less valuable than 876 the enzyme, which must be recycled repeatedly for economic sustainability; since solid-solid 877 separations are difficult, the product crystals may be re-dissolved to enable recovery of the enzyme in solid form.<sup>198</sup> With the simplified recovery of a solid biocatalyst comes the challenge 878 879 of catalyst engineering: choosing a particle size and material to avoid mass-transfer limitations and efficiently utilize the active material, for example PGA in Figure 6.<sup>184</sup> When catalyst 880 881 recovery is a nonissue, and trace catalyst does not impact downstream quality, e.g. heavy metal 882 toxicity, a reactive crystallization with a dissolved catalyst may be preferable.

Recently, a biocatalytic process with reactive crystallization to produce the HIV drug
 islatravir has been described.<sup>199</sup> The reactive crystallization involves four dissolved enzymes.

885 The three final reactions to islatravir are reversible, so crystallization helps shift the equilibrium 886 towards the product, and the fourth enzyme catalyzes a reaction to consume a byproduct and 887 further improve the yield of islatravir (see Figure 7). The high value of the product favors its 888 recovery by filtration and use of fresh enzyme for each batch. Upstream of the reactions shown 889 in Figure 7 product recovery by filtration is not favorable, and five immobilized enzymes are 890 used. The starting solution for the reactive crystallization is the filtrate from the reactions 891 catalyzed with immobilized enzyme. The relative harmlessness of enzymes (compared to heavy 892 metals) and the value of the reaction products favor reactive crystallization processes. 893 Furthermore, the strong specificity of enzymes enables coupling many reactions to transform 894 soluble reactants to the desired insoluble product. A more recent study of the same system used 895 crystallization of the byproduct (previously consumed by the fourth enzyme) as a calcium salt to 896 drive the reaction further; the improvement in reaction yield (82% versus 76%) outweighed the 897 difficulty of recrystallization.<sup>200</sup>



898

Figure 7. Enzymatic synthesis of islatravir by three enzymes in a single vessel from an alkyne precursor
 (also produced enzymatically). Islatravir crystallization helps drive the reaction to the right; consumption of the
 phosphate byproduct by (top) reaction with calcium and crystallization of calcium phosphate or (bottom) enzymatic
 reaction with sucrose pulls the reaction further towards the product. Adapted from Huffman et al.<sup>199</sup>

903 Many chemistries that do not seem plausible with biocatalytic processes could be 904 implemented with biocatalytic reactive crystallization. For example, equilibrium favors removal 905 of CO<sub>2</sub> from carboxylic acids, not carboxylation by addition of CO<sub>2</sub>. However, Ren et al.<sup>201</sup> 906 overcame the unfavorable reaction equilibrium when they carboxylated phenols with a 907 decarboxylase enzyme (which, as the name suggests, typically catalyzes removal of  $CO_2$ ) by 908 crystallizing the products as quaternary ammonium salts, improving the yield from 40% to 97%. 909 Table 3 lists several examples of the three types of covalent reactive crystallizations 910 discussed, non-catalytic, catalytic, and biocatalytic. The product, reactants, and focus of the 911 study are listed for each entry in Table 3. The focuses are varied, reflecting the wide-ranging 912 applications of covalent reactive crystallization.
913 Table 3. A list of representative studies on covalent reactive crystallization processes, divided based on 914 catalyst usage and type.

Product	Reference No.	Reactant 1	Reactant 2	Focus
Uncatalyzed				
Paracetamol	189	4-aminophenol	Acetic anhydride	Impurity content, crystal shape, growth and nucleation kinetics
Paracetamol	190	4-aminophenol	Acetic anhydride	Continuous oscillating baffled reactor
2,4,6-triamino- 1,3,5-trinitro-	122	2,4,6-trichloro- 1,3,5-trinitro- benzene	Ammonia	Gas, liquid, solid phase. Effect of feed rate and temperature on particle size in hubble column reactor
Dithiocarbamate (DTC)	88	DTC-precursor	Formaldehyde	Narrow CSD, avoid oiling out and spherulites, optimize productivity
Amides	84	Acid chlorides	Amines	Plug flow reactor crystallizer, examined fouling
Inorganic catalys	it			
Terephthalic acid (TPA)	193	<i>p</i> -xylene	Oxygen	Intermediate impurity incorporation, Co/Mn catalyst, Br promoter
TPA	202	<i>p</i> -xylene	Oxygen	Evaporative cooling of exothermic reaction to avoid fouling
TPA	203	<i>p</i> -xylene	Oxygen	Two reactive crystallizers in series to eliminate intermediate impurity
BACE inhibitor	92	Isoxazidoline derivative	Hydrogen	Difficulty separating Pd/C catalyst from solid product, redissolved
Relebactam	204	Carboxybenzyl relebactam	Hydrogen, silylating agent	Pd/C, DABCO then HOAc. <i>In situ</i> protect/deprotect with crystallization
Akt kinase inhibitor	91	Amine precursor	Methyl phenylacetate	Cs <sub>2</sub> CO <sub>3</sub> catalyst, impurity rejection
		Boronate precursor	Chloropyridine derivative	Pd catalyzed Suzuki coupling, enhance yield and selectivity
Hedgehog pathway inhibitor	93	Carboxybenzyl protected API	Hydrogen	Solids formed on Pd/C catalyst, form HCl salt instead
Biocatalytic				
Ampicillin	4	6-amino penicillanic acid (6-APA)	Phenylglycine methyl ester (PGME)	Improved enzymatic yield with crystallization
Ampicillin	173	6-APA	PGME	Reactive crystallization of product and byproduct, phenylglycine
Ampicillin	198	6-APA	PGME	Taylor-Couette flow reactor to suspend slurry with low shear
Ampicillin, Amoxicillin, Cephalexin	205	6-APA, 7- amino- desacetoxy- cephalosporanic acid (7-ADCA)	Phenylglycine amide, 4-hydroxy- phenylglycine amide	Used supersaturated reactants for three different pen G acylase catalyzed reactions
Ampicillin	206	6-APA	Phenylglycine amide	Fed batch, solid reactants dissolving, solids purity versus conversion
Amoxicillin, Cephalexin	5, 113	6-APA, 7- ADCA	PGME	Continuous reactive crystallization modeling, size, purity, yield
Cephalexin	207	6-APA	Phenylglycine nitrile	Complex product with 1,5- dihydroxynaphthalene (reduced sol.)
Islatravir	199	2-Ethynyl- glyceraldehyde- 3- phosphate	2-F-adenine	Three reactions in series, crystallization pulls equilibrium right
Methyl trans-3-(4- methoxy-phenyl) glycidate	208	Racemate		Lipase immobilized on membrane to facilitate enzyme recovery from crystals. Deracemization
Levodione	154, 195	4-oxoisophorone		Reduction by live <i>S. cerevisiae</i> , crystallization reduce over-reduction

Nicotinamide	209	3-cyano	water	Avoid overhydration to nicotinic acid
		pyridine		by crystallization
Methionine,	210	Racemate	Ammonia borane,	Deracemization
phenylalanine			oxygen	
Alanine	196	Aspartic acid		Deracemization, whole cell (dead)
				Pseudomonas dacunhae catalyst
2,3- and 2,6-	201	Resorcinol	KHCO3	Use of quaternary ammonium salts to
dihydroxybenzoate		Catechol		increase yield from 40% to 97%
Allo-threonine	211	threonine		Isomerase reaction, solid reactant and
				product, constant liquid composition
Z-aspartame	212	Carboxybenzyl	Phenylalanine	Two enzymes tested, reaction kinetics
		aspartate	methyl ester	
L-Homo-	213	2-oxo-4-phenyl-	L-aspartate	Fed batch to overcome substrate
phenylalanine		butryic acid		inhibition
L-phenylglycine	214	Phenyl-	L-glutamate	Thermophilic enzyme, crystallization
		glyoxylate		shifted equilibrium to products
Peptides	215-219	Amino acid with	Unprotected amino	Improving yield, conversion
		protected amine	acid	

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In the carboxylation example by Ren et al.<sup>201</sup> the product formed is an organic salt, but it 916 917 is discussed in the covalent section of this review because the rate-limiting step is the formation 918 of covalent bonds (carboxylation). The kinetics of this process are more representative of those 919 found for other covalent and biocatalytic reactive crystallizations. The same behavior is observed 920 in fermentation with continuous neutralization by calcium hydroxide; the rate-limiting step is not 921 the reaction between carboxylate and neutralizing base, but rather production of the acid by the 922 microorganism. The product, a dissociated acid, is ionic, but the rate-limiting reaction that 923 produced the acid forms covalent bonds. Neutralization in batch at the end of the fermentation may also be practiced, in which case the ionic reaction between  $Ca^{2+}$  and the carboxylate is rate-924 limiting. The use of a second species, such as  $Ca^{2+}$  for carboxylates, to form a less-soluble 925 926 complex with the product is a common application of reactive crystallization.

927 Enzymatic peptide synthesis is thermodynamically unfavorable in aqueous solutions, but 928 reactive crystallization enables even thermodynamically-controlled reactions to achieve high 929 yields, especially when using a second species to promote crystallization. For example, the 930 thermolysin-catalyzed synthesis of the artificial sweetener aspartame (L-asp-L-phe-OMe) is used 931 in a 10,000 ton/year-scale process with 96% yield in the enzymatic step.<sup>220, 221</sup> Carboxybenzyl L-932 aspartate (Z-asp) is coupled with equimolar L-phenylalanine methyl ester (L-phe-OMe) at 933 neutral pH in purely aqueous solution. The anion generated at neutral pH values, Z-aspartame 934 (Z-asp-L-phe-OMe), forms an insoluble salt with cationic D-phe-OMe, Z-asp-L-phe-OMe·D-935 phe-OMe. Racemic DL-phe-OMe is employed in 2:1 molar ratio with Z-aspartate such that the 936 L-enantiomer is consumed in the reaction and the D-enantiomer promotes crystallization.

Eichhorn et al.<sup>217</sup> demonstrated that reactive crystallization of thermolysin-catalyzed dipeptide 937 938 couplings leads to high yields with a wide range of amino acids and their derivatives. In a high-939 solids medium (only about 10% aqueous solution), at the kilogram scale, mixing limits the reaction rate. In theoretical work on peptide synthesis, Erbeldinger et al.<sup>216</sup> and Ulijn et al.<sup>215</sup> 940 941 showed that high yield is the consequence of reactive crystallization and that above a threshold 942 of product solubility, yield switches from low values to values of almost 100%. The work of Hulsewede et al.<sup>170</sup> described a nearly 5-fold increase in the yield of 1-943 944 phenylethylamine (1-PEA), synthesized by a transaminase enzyme, by reactively crystallizing the 1-PEA. Starting with acetophenone and isopropylammonium-3,3-diphenylpropionate (iPA-945 946 DPPA), the enzyme transfers the amine group from *i*PA to acetophenone and the resulting 1-947 PEA crystallized as a salt with DPPA. The crystal product was a salt, but the rate-limiting step is 948 the enzyme-catalyzed covalent reaction. The DPPA was present in stoichiometric quantity 949 throughout the reaction since the *i*PA was fed as the DPPA salt. It was found that low reaction 950 equilibrium (19%) could be overcome by coupling to the favorable crystallization of 1-PEA-951 DPPA and 92% conversion could be reached. The general process, illustrated in Figure 8, is also applicable to similar chemistries.<sup>222</sup> 952



953

954Figure 8. Reaction scheme of the amine transaminase (ATA, cofactor pyridoxal phosphate, PLP) catalyzed955stereoselective amination of a ketone with iPA donor amine. The amine product forms a salt with the anion from the956amine donor. In the main text,  $R_1 = C_6H_5$ ,  $R_2 = CH_3$ , and  $R_3 = DPPA$ . Reprinted with permission from Hulsewede et957al.<sup>170</sup> copyright 2019, John Wiley and Sons.

Depending on the nature of the interactions between the product and the second species, the resulting crystals may be called salts (coulombic interactions) or cocrystals.<sup>223-225</sup> In the previous example, 1-PEA is crystallized as a salt of DPPA, but numerous examples can be found where the final solid is a cocrystal. As an illustration, the yield of cephalosporin antibiotics can

962 be increased by reactive crystallization with an aromatic species to isolate the antibiotic product, 963 which is an intermediate in an enzymatic cascade. The process has been demonstrated for cefaclor (yield increased from 57% to 80%),<sup>226</sup> cephalexin (42% to 67%),<sup>227</sup> and cephradine 964 (yield not evaluated).<sup>228</sup> Recent published work on cocrystallization has focused on discovery 965 and/or prediction of cocrystal-forming systems,<sup>229, 230</sup> which could make reactive crystallization 966 practical for a wider range of products if co-formers\* promoting crystallization can be identified 967 968 for more products. Other applications of cocrystallization include: improved solids handling,<sup>231</sup> solubility,<sup>232</sup> stability,<sup>233</sup> and pharmaceutical activity,<sup>234</sup> Karimi-Jafari et al. reviewed the entire 969 topic.235 970

971 Carbamazepine has been a favorite model compound for cocrystal research and is the 972 only compound for which cocrystallization kinetics have been published. Gagniere et al.<sup>236</sup> 973 qualitatively examined the rates of cocrystallization in the carbamazepine-nicotinamide system while Rodriguez-Hornedo et al.<sup>237</sup> used Raman spectroscopy to monitor the nucleation and 974 975 growth of carbamazepine-nicotinamide from a slurry of the individual solids. Kudo and Takivama<sup>238</sup> have worked out much of the thermodynamics of reactive cocrystallization in the 976 977 carbamazepine-saccharin system. Each of these studies highlights the difficulties designing 978 reactive crystallizations with multiple small molecules, namely complex phase diagrams with at 979 least three solids (more with chiral compounds and if cocrystals with several stoichiometries 980 exist) and uncertain driving forces for complexation.

981 *Chiral Resolution.* Enantiomers are prevalent in pharmaceutically active compounds, 982 with one enantiomer typically being responsible for clinical activity and, in some cases, the 983 mirror compound having deleterious effects. Both left and right enantiomers have the same 984 solubility, vapor pressure, partition coefficients, etc. (in achiral solvents), making their separation 985 by traditional methods very difficult. Many non-biological reactions are agnostic of chirality, the 986 products are racemic mixtures that, by definition, contain equal amounts of the two enantiomers. 987 Producing a compound with a single chirality often involves a deracemization step. Provided a 988 racemizing reaction (a reversible reaction interconverting the two enantiomers) occurs with

<sup>\*</sup> The FDA defines a co-former (or coformer) as one of the two different molecules in the same crystal lattice, forming a co-crystal. More information can be found at <u>https://www.fda.gov/media/81824/download</u>

appreciable speed, the left- and right-hand enantiomers (*S* and *R*) will exist in a 1:1 ratio insolution, irrespective of removal of one of the enantiomers from solution by crystallization.

991 Conglomerate-forming systems are ones in which each of the two enantiomers form 992 enantiomerically pure crystals that may be produced as a physical mixture if crystallized 993 together. Racemate-forming systems produce crystals in a single lattice structure with a 1:1 ratio 994 of the two enantiomers. Conglomerate-forming systems are more amenable to resolution by 995 reactive crystallization, and are estimated to comprise 5-20% of all enantiomeric systems with racemates making up the remainder.<sup>239, 240</sup> Reviews of several techniques for enhancing 996 997 enantiomeric purity, some involving reactive crystallization, are provided by Lorenz and Seidel-Morgenstern,<sup>241</sup> Palmans,<sup>242</sup> and Brands and Davies.<sup>185</sup> In the following discussion, special 998 999 emphasis is given to a class of covalent reactive crystallizations used to recover enantiomerically 1000 pure products.

1001 Crystallization can result in deracemization in four ways: (1) by formation of a 1002 diastereomeric salt with a chiral resolving agent, (2) by preferential crystallization, (3) by 1003 selectively subjecting the undesired enantiomer to racemization with an asymmetric reaction, 1004 thereby enriching the solution in the preferred enantiomer and facilitating its crystallization, and 1005 (4) by attrition-enhanced deracemization of conglomerate-forming enantiomers.

<u>Diastereomeric resolution</u>, or crystallization with a resolving agent, sometimes referred to as "classical resolution," takes advantage of differences in interactions between two chiral molecules. In this process, two enantiomers of a single species are reacted with a single enantiomer of another compound (resolving agent) to form two diastereomers that have different properties, including solubilities. The two diastereomers may then be separated by crystallizing the less soluble of the two. The desired free enantiomer is then recovered by reversing the reaction that formed the diastereomer.

1013 An illustration of diastereomeric resolution is the production of the unnatural amino acid 1014 R-(-)-2-phenylglycine, R-PG, mentioned previously in reference to certain beta-lactam 1015 antibiotics. In the commercial process, a racemic mixture of phenylglycine (RS-PG) is reacted 1016 with (1S)-(+)-camphor-10-sulfonic acid, S-CS, to produce two diastereomeric salts, RS-PG-CS 1017 and SS-PG-CS. The former has a lower aqueous solubility (5.75 g/100 g at 25 °C) than the latter 1018 (>150 g/100g, 25 °C), which facilitates separation.<sup>243</sup> Racemization of RS-PG in the presence of

- one equivalent of *S*-CS and half an equivalent of hydrochloric acid (to keep zwitterionic PG from
  crystallizing) leads to greater than 90% yield of *R*-PG from *RS*-PG.
- 1021 The simultaneous use of multiple resolving agents has been shown to enhance resolution, likely by inhibiting nucleation of the undesired diastereomeric salt.<sup>244</sup> Brands and Davies<sup>185</sup> list 1022 1023 many systems for which diastereomeric salt resolution has proven successful. The utility of this 1024 method is demonstrated by its use in the production of large quantities of (S)-naproxen, (R)phenylglycine, and (R)-4-hydroxyphenylglycine.<sup>241</sup> Diastereomeric resolution can be used to 1025 resolve individual enantiomers of conglomerate-forming and racemate-forming compounds. 1026 Figure 9 represents the resolution of the S enantiomer of a conglomerate forming compound by 1027 addition of resolving agent  $S^{\dagger}$ . The apex represents pure solvent, while the lower left vertex is 1028 1029 pure S or  $SS^{\dagger}$  and the lower right vertex represents pure R. Using process analytical technology 1030 (PAT, discussed further in the process design section) one would observe the solution 1031 composition following the solid black curve from Point A to Point B, with movement up and to
- 1032 the right due to crystallization and movement left due to racemization.



- 1033
- 1034Figure 9. Isothermal ternary phase diagram for diastereomeric resolution. The phase equilibrium before1035addition of the resolving agent is symmetrical, shown by bold gray curves, while after addition the resulting1036diastereomer SS<sup>†</sup> phase equilibrium is asymmetric, shown by dashed gray curves, enabling crystallization of only1037the desired enantiomer. During the process, the solution moves from Point A (undersaturated) to B upon addition of
- 1038  $S^{\dagger}$  with concurrent racemization in solution.
- 1039 <u>Preferential crystallization</u> utilizes the addition of seed crystals to solutions of
- 1040 enantiomers in the metastable zone to initiate nucleation and subsequent growth of a single
- 1041 enantiomer from a racemic solution. The methodology is useful for conglomerate-forming
- 1042 systems. Seed crystals of the desired enantiomer are added, and the supersaturation is held within

1043 the metastable zone. The seed crystals grow and breed new crystals of the desired chirality while

- 1044 the undesired enantiomer remains in solution; primary nucleation must not occur as it would
- 1045 initiate crystallization of the undesired enantiomer. Simultaneously subjecting the solution to a
- 1046 racemization reaction enhances the yield of the seeded species. Yoshioka<sup>245</sup> summarized several
- 1047 examples of preferential crystallization of amino acids, both proteogenic and unnatural, with
- 1048 racemization by catalytic salicylaldehyde. Petrusevska-Seeback et al. give an example of
- 1049 combining preferential crystallization with enzymatic racemization .<sup>246</sup> Supersaturation may be
- 1050 generated by cooling, pH adjustment or other means. Figure 10 shows the preferential
- 1051 crystallization of S by acidification reactive crystallization, where  $pH_1 > pH_2 > pH_3$  and the
- 1052 solubility decreases with decreasing pH value.



1053

1054Figure 10. Ternary phase diagram for preferential crystallization of S by addition of S seed crystals.1055Supersaturation is generated by decreasing the pH from  $pH_1$  to  $pH_3$  while a racemization reaction converts excess R1056in solution to restore a 1:1 ratio of R:S in solution. Again, the bold black curve from Point A to Point B represents1057the solution composition observed by PAT, while the blue arrows represent movement due to crystallization and the1058red arrows movement due to racemization.

1059 Enantiomeric enrichment followed by crystallization is especially valuable if an 1060 enantiomerically pure product is to be recovered from a racemate-forming system. Enrichment in 1061 the present context means that the relative proportion of the desired enantiomer in solution is 1062 increased to an extent that crystallization of enriched pure enantiomer is feasible. Enrichment of a specific enantiomer can be accomplished in several ways. For example, Johnson et al.<sup>247</sup> used 1063 1064 an asymmetric palladium catalyst in route to an API, producing the desired enantiomer at a 1065 solution enantiomeric excess of 95%; crystallization was used to upgrade the enantiomeric excess of the solid to >99%. Encarnacion-Gomez *et al.*<sup>210</sup> used a chemo-enzymatic 1066

- 1067 stereoinversion reaction system to enrich the concentration of a desired enantiomer to
- 1068 appropriate concentrations for crystallization of the pure enantiomer. They demonstrated the
- 1069 process using racemic mixtures of phenylalanine and of methionine and recovered crystals of the
- 1070 desired pure enantiomer from each system. Harriehausen *et al.*<sup>248</sup> suggested several process
- 1071 configurations that combined enantioselective chromatography with enzymatic racemization to
- 1072 recover pure enantiomer with nearly complete extinction of the undesired enantiomer. Figure 11
- 1073 shows enantiomeric enrichment in a racemate forming system by reacting *R* to *S* followed by
- 1074 crystallization in a racemate-forming system. The middle cone-shaped region identifies
- 1075 conditions corresponding to equilibrium between crystals of the racemate and the solution. The
- 1076 objective of enantiomeric enrichment is to move from the central region to the yellow region,
- 1077 thereby facilitating crystallization of the desired enantiomer.



1078

1079Figure 11. The ternary phase diagram for enantiomeric enrichment in a racemate-forming system. The1080enantiomeric enriching reaction occurs under supersaturated conditions, but high conversion ensures only the1081desired enantiomer is crystallized. Again, the bold black curve from Point A to Point B represents the solution1082composition observed by PAT, while the blue arrow represents movement due to crystallization and the red arrow1083movement due to an enantioselective isomerization reaction.

1084 <u>Attrition-enhanced deracemization</u>, sometimes referred to as "Viedma ripening," was 1085 observed originally by Viedma<sup>249</sup> and explored further by Viedma<sup>250</sup> and Blackmond.<sup>251, 252</sup> The 1086 original observations were on aqueous solutions of sodium chlorate, a species that is achiral in 1087 solution but which, on crystallization, produces chiral crystals. Experiments included seeding 1088 with mixtures of *R* and *S* chiral crystals that had been subjected to attrition before being added to 1089 the system and which were subject to continuous attrition by the presence of glass beads that 1090 were added to the stirred system. After stirring for a sufficiently long period, the resulting 1091 crystals were found to be enantiomerically pure R or S. Later work found similar behavior for 1092 conglomerate-forming enantiomers that underwent rapid racemization reactions and, therefore, 1093 maintained the ratio of enantiomers in solution near 1:1. Examples of such systems include: an amino acid derivative N-(2-methylbenzylidene)-phenylglycine amide;<sup>253</sup> aspartic acid, one of 1094 two conglomerate forming proteogenic amino acids;<sup>250</sup> and an imine that is the key component in 1095 clopidogrel.<sup>254</sup> Spix et al.<sup>255</sup> converted the racemate-forming amino acids alanine and 1096 1097 phenylalanine to conglomerate-forming salts alanine 4-chlorobenzene sulfonic acid and 1098 phenylalanine 2,5-xylenesulfonic acid. After deracemization of the salts, the free amino acids 1099 were recovered by neutralizing the salts with alkali.

### 1100 **Reactive Crystallization Process Design**

Development of reactive crystallization processes for use at the industrial scale is a challenging multi-objective problem. The generation of a given product by reactive crystallization involves simultaneous fundamental thermodynamic and kinetic phenomena, including reaction, mass transfer, and crystal nucleation and growth, all coupled with the engineering aspects of reactor design, configuration, control, and product recovery. While each of these has been well-studied in the literature, decisions for process design, optimization, and control are often unique to the system of interest.

1108 Reactive crystallization processes generate supersaturation by synthesizing a product 1109 through a reaction, concomitantly increasing the concentration of the product and leading to 1110 crystallization. The rates of the reaction and crystallization steps guide strategies for reactor 1111 design and control. In cases where fixed operating conditions favor both reaction and 1112 crystallization, reactive crystallization can be performed in a single vessel. For example, many of 1113 the ionic reactions mentioned earlier produce a sparingly soluble compound in an instantaneous 1114 reaction and fall into this category. Other cases may require the steps to be temporally or 1115 spatially separated, several configurations of which are illustrated in Figure 12. Temporally 1116 separated processes include well-mixed batch or semi-batch designs in which synthesis reactions 1117 occur, followed by a shift in temperature or pH to promote subsequent crystallization of the 1118 product. Processes that are spatially separated utilize multiple vessels or different segments of a 1119 vessel—first performing the reaction to generate supersaturation and then feeding the mixture 1120 into a second vessel for crystallization. Process intensification in the form of combining both 1121 reaction and crystallization steps into a single vessel is likely to lead to savings in capital and

1124

- operating costs as the technology matures,<sup>256, 257</sup> but like many aspects of design problems, the
- 1123 potential benefit is system-dependent.



1125Figure 12. (a) Temporal separation of reaction and crystallization favoring conditions in a well-mixed1126batch reactor; (b) Spatial separation of reaction and crystallization favoring conditions in continuous well-mixed1127reactors (above) and tubular reactors (below).

1128 Key factors in process design for reactive crystallization include the presence of multiple components (sometimes with more than one crystallizing), effects of mixing on crystallization 1129 1130 kinetics, the necessity of maintaining mutually beneficial operating conditions for reaction and 1131 crystallization, and the need for producing crystals that can be readily separated from a reaction 1132 slurry. In instances where a heterogeneous catalyst is used to facilitate a desired reaction, 1133 separating the catalyst from product crystals represents an additional challenge. As crystal shape 1134 and size distributions are strongly influenced by supersaturation, process control is also a unique 1135 challenge due to the generation of supersaturation from a reaction rather than by temperature 1136 manipulations, evaporation, or anti-solvent addition. In the following discussion, challenges 1137 unique to reactive crystallization process design and control that focus on the aforementioned 1138 issues are discussed in more detail. 1139 *Reactor Design.* Design and implementation of reactive crystallization systems rely

heavily on reaction and crystallization kinetics. A strong distinction between the operation of a reactive crystallizer and a traditional crystallizer is that reactive crystallization conditions must 1142 satisfy *both* the reaction *and* the crystallization. For example, an enzymatic reaction usually 1143 requires benign temperatures (20 to 37 °C), aqueous conditions, and near-neutral pH values. If 1144 these conditions promote crystallization of the desired product, then reaction and crystallization 1145 may be conducted in the same vessel. If the conditions for reaction do not permit crystallization 1146 of the product, then using multiple vessels may need to be investigated. Alternatively, the conditions within the vessel may be varied over the time course of the reactive crystallization or 1147 across the volume of the reactor (specifically for tubular reactors). For example, Jiang et al.<sup>190</sup> 1148 1149 varied the temperature across a tubular reactor to allow for enhanced reaction kinetics in the 1150 upstream section and improved crystallization kinetics in the downstream section.

1151 Configurations of vessels in which reactive crystallizations are conducted usually are 1152 similar to those of non-reactive crystallizers. The perfectly mixed continuous crystallizer, which 1153 is often referred to as a mixed-suspension mixed-product removal (MSMPR) crystallizer,\* is an 1154 idealized version of a continuous stirred-tank crystallizer. A similar vessel may serve as a batch 1155 crystallizer with feed added at time zero and product removed at a designated endpoint. In a 1156 semi-batch (or fed-batch) unit, one or more feed streams is added during the course of a run and 1157 product removed at the designated endpoint. More details on these generic configurations, which often have to do with mixing, are available in general references on industrial crystallization.<sup>36</sup>, 1158 258 1159

Most applications of reactive crystallization described in the literature focus on batch or 1160 1161 semi-batch systems. While these are often relatively simple to design and operate, continuous 1162 reactive crystallization processes offer several benefits. Advantages of continuous systems have been outlined specifically for pharmaceuticals manufacturing by Lee et al.<sup>259</sup> and Acevedo et 1163 al.<sup>260</sup> Some of these benefits include higher process capacity and productivity, more efficient use 1164 1165 of raw materials and energy, production of fewer intermediate compounds, and more robust 1166 control. The design and use of various arrangements of reactive crystallization equipment for 1167 batch, semi-batch and continuous operation are covered in the following discussion.

<sup>\*</sup> The MSMPR crystallizer is a useful model for continuous stirred-tank crystallizers. The assumptions of perfect mixing and uniformity of residence time distributions of solvent and crystals of all sizes are approximations often approached in actual systems.

*Batch and semi-batch systems.* The use of a batch reactor allows for adjustment of process parameters during the time course of the reactive crystallization, such as decreasing the temperature or adjusting the pH value towards the end of a batch so as to crystallize more product and increase the overall process yield. For example, in the enzymatic synthesis of betalactam antibiotics shown in Figure 6, the solution pH value typically decreases as the reaction progresses due to the formation of acidic products. The lower pH value further decreases the solubility of the product, improving product crystallization and yield.<sup>4, 261</sup>

1175 Batch and semi-batch reactive crystallization processes are operated in well-mixed 1176 reactors that allow for implementation of on-line PATs, are robust, and are more resistant to 1177 clogging and encrustation issues than tubular reactors. Also, these well-mixed reactors are often 1178 highly modular, allowing for the inclusion of baffles, a draft tube,<sup>262</sup> or different impeller types to enhance mixing.<sup>263</sup> Cao et al.<sup>85</sup> used an airloop-lift reactor (ALR) to improve mixing for the 1179 1180 batch reactive crystallization of Ni(OH)<sub>2</sub> over traditional impeller stirring. Another alternative to traditional impeller-stirred reactors is the Taylor-Couette reactor used by Ferreira et al.,<sup>198</sup> which 1181 1182 uses a combination of inner rotating and outer stationary cylinders to gently mix the slurry of 1183 crystals and catalyst particles in the region between the cylinders (Figure 13). The design is used 1184 to protect the catalyst particles, which are susceptible to the shear stress induced by an impeller 1185 in a conventionally mixed reactor. Often, traditional impeller stirring may be adequate for a 1186 system, but for very fast reactions, the various parameters involving mixing and reactant addition 1187 rate or novel techniques of mixing may need to be investigated to achieve a desirable crystal size 1188 distribution.

1189 In the case of fast reactions in semi-batch systems, mixing and the method and rate of 1190 reactant addition significantly impacts the product size distribution. Åslund and Rasmuson<sup>264</sup> 1191 studied the effect of stirring rate, impeller type, reactant concentration, reactant feed rate, and 1192 feed position (e.g. surface level, bulk liquid, next to impeller feeds) on the size distribution of 1193 benzoic acid crystals formed via reactive crystallization. The rate of addition of the reactant 1194 hydrochloric acid, reactant concentration, and stirring rate significantly influenced the product 1195 size distribution. As the stirring rate was increased, the size of resulting crystals increased up to a 1196 maximum where crystal size began to decrease; the type of impeller and feed position had a 1197 lesser effect on the product size distribution, especially at higher stirring rates. Chen et al.<sup>114</sup> 1198 investigated mixing during reactive crystallization of barium sulfate. Three separate scales of

1199 mixing, Kolmogorov, turbulent, and convective, were proposed in a new mixing model 1200 composed of viscous deformation and molecular diffusion in a slab element. The model was 1201 used to give accurate predictions of the effect of stirring speed, feed location, and viscosity on particle sizes. Zauner and Jones<sup>265, 266</sup> investigated the effect of feed rate, feed concentration, 1202 1203 feed tube diameter, impeller type and stirring rate on particle size for the reactive crystallization 1204 of calcium oxalate and calcium carbonate. Overall, the results of the aforementioned mixing 1205 studies suggest that poor mixing conditions promote a higher rate of primary nucleation, leading 1206 to a larger number of nuclei and a size distribution of smaller final crystals.

1207Continuous systems. As in batch systems, the stirred tank is the most commonly-used1208vessel in continuous systems, but alternative geometries have also been proposed and1209implemented. Several examples of alternatives to the stirred-tank crystallizer are shown in

- 1210 Figure 13. These include Taylor-Couette, impinging jet, airlift loop, continuous flow inversion,
- 1211 and oscillatory baffled crystallizers. Examples (a), (b), and (c) in Figure 13 approximate
- 1212 MSMPRs, while (d) and (e) are used to provide near plug-flow behavior.



Figure 13. Summary of novel reactive crystallizers; (a) Taylor-Couette,<sup>198, 267</sup> (b) Impinging jet mixer,<sup>165</sup> (c)
 airlift loop,<sup>85</sup> (d) continuous flow inverter – Reprinted with permission from Kurt et al.<sup>268</sup> copyright 2017, Elsevier,
 (e) continuous oscillatory baffled.<sup>190</sup>

1213

1217 For reactions of short timescales, often a reactor that is nearly perfectly mixed is used due 1218 to its robust operation and the ease of implementing process analytical technologies (which are 1219 discussed later and may include in situ microscopy, Raman and IR spectroscopy, and particle 1220 size analysis). Well-mixed reactors such as an MSMPR are also used when high supersaturation 1221 is not desired, such as when high supersaturation promotes the formation of an undesired 1222 polymorph or a finer crystal size distribution. For reactions in which high reactant concentrations 1223 are preferred, a single well-mixed reactor may not be the best design because it operates at outlet 1224 conditions; that is, conditions throughout the vessel correspond to those at the outlet. However, the use of a plug-flow reactor may introduce clogging concerns.<sup>269</sup> To address this issue, Hu et 1225 al.<sup>270</sup> utilized multiple MSMPR reactors in series to approach plug-flow behavior for a second-1226 1227 order reaction in which high reactant concentration was needed to achieve high conversions.

1228 When the reaction proceeds much faster than crystallization (both nucleation and 1229 growth), techniques such as wet-milling or sonocrystallization can promote nucleation and more rapid consumption of supersaturation. Yang et al.<sup>271</sup> and Acevedo et al.<sup>272</sup> showed that wet 1230 1231 milling in a continuous crystallizer increased the yield, operating as a promoter of both primary 1232 and secondary nucleation for paracetamol in two different solvents. Use of wet-milling has also 1233 been shown to enable deracemization of conglomerates by combining the principles of preferential crystallization and Viedma ripening.<sup>273</sup> Sonocrystallization, or the application of 1234 ultrasound to a crystallizer, has been shown to hasten crystallization in batch.<sup>274</sup> Hatakka et al.<sup>180</sup> 1235 used sonocrystallization to selectively produce a single polymorph during the batch reactive 1236 1237 crystallization of L-glutamic acid while experiments without sonication resulted in a mixture of 1238 polymorphs. The authors concluded that the polymorphic purity results from reduced 1239 supersaturation due to enhanced nucleation by sonication. Wet-milling and sonocrystallization can both lead to narrower, finer size distributions as a result of increased nucleation.<sup>275, 276</sup> 1240

1241 Slower reactions may require the use of multiple vessels in series to achieve higher 1242 conversions. Mo and Jensen<sup>277</sup> demonstrated the use of a micro-CSTR cascade for two separate 1243 solid-forming reactions: (1) the reaction of glyoxal and cyclohexylamine to form the practically 1244 insoluble N,N'-dicyclohexylethylenediimine and (2) the sulfonylation of 2-octanol which 1245 produced the sparingly soluble side product triethylamine hydrochloride. For the first reaction, a 1246 six-unit CSTR cascade (15-minute total residence time) was needed to reach nearly 100% 1247 conversion while the second reaction only required three CSTRs to achieve 100% conversion. Effective control of process parameters such as temperature and pH, often important variables in determining the reaction and crystallization rates, is typically achieved in well-mixed reactors with the inclusion of probes, a thermal jacket, and addition of acid or base. Process control will be discussed in more detail below.

1252 Mixing intensity may be an issue in continuous reactive crystallization. Like batch 1253 crystallizers, if the reaction utilizes a catalyst that is susceptible to high shear, a Taylor-Couette 1254 style reactor may be operated with a feed and continuous product removal. Aggregation of 1255 mixing-induced nuclei may also be a concern, leading to a wide crystal size distribution (CSD). Liu *et al.*<sup>165</sup> found that incorporation of an impinging jet mixer in the continuous reactive 1256 1257 crystallization of the antibiotic sodium cefuroxime resulted in a narrower CSD and improved 1258 product stability compared to a traditional impeller-stirred reactor. Jung et al. found a similar 1259 decrease in the size distribution using a Taylor-Couette reactor for calcium hydroxide production because the more gentle mixing discouraged agglomeration.<sup>278</sup> 1260

1261 Continuous tubular reactors such as plug flow reactors (PFRs) are frequently used in the 1262 chemical industry. Higher overall concentrations of reactants across the length of the reactor lead 1263 to higher conversions for positive-order reactions. For reactive crystallization, unlike in a well-1264 mixed tank, temperature or pH value may be varied along the length of the reactor, allowing for the enhancement of reaction or crystallization kinetics in different sections. Jiang and Ni<sup>190</sup> 1265 1266 varied the temperature across a continuous oscillatory baffled crystallizer (COBC), a type of continuous tubular reactor designed to achieve plug flow at low fluid velocities, such that higher 1267 1268 temperatures in the initial segments favored the reaction and lower temperatures towards the outlet improved the rate of crystallization. Kurt et al.<sup>268</sup> achieved near plug-flow behavior of 1269 1270 slurry by designing and operating a coiled flow inverter (CFI) crystallizer for the reactive 1271 crystallization of calcium carbonate. The inverting flow and helically coiled tubing enhanced 1272 mixing via formation of Dean and Taylor vortices, which increased secondary flow 1273 perpendicular to the primary flow direction. Others have physically segmented plugs of slurry by injecting inert gas spacers.<sup>279</sup> All of these crystallizers enhance mixing and slurry suspension by 1274 1275 achieving a more plug-flow-like flow profile than conventional PFRs. Increased turbulence using 1276 these novel designs permits the use of reactors with larger diameters and shorter lengths to 1277 achieve the same residence times. In general, using small-diameter tubing to achieve adequate turbulence and slurry suspension is a concern in PFRs because of clogging. Polster et al.<sup>84</sup> 1278

attempted to design a continuous reactive crystallization process for a BACE inhibitor using a
 PFR, but eventually settled on an MSMPR due to clogging inside the reactor tubing. Oroskar and
 Turian<sup>280</sup> developed the following correlation to estimate the critical slurry velocity, which is
 defined as the velocity required to suspend particles and prevent their deposition in a tube or
 pipe:

$$\frac{v_c}{\sqrt{gd(s-1)}} = 1.85C^{0.15} \left(1-C\right)^{0.36} \left(\frac{d}{D}\right)^{-0.38} \left(\frac{D\rho_l \sqrt{gd(s-1)}}{\mu}\right)^{0.090} x^{0.30}$$
(23)

All dimensional variables are in SI units and  $v_c$  represents the critical velocity, *d* the equivalent spherical particle size, *C* the fractional slurry density, *D* the pipe diameter,  $\rho_l$  the liquid density,  $\mu$  the liquid viscosity, and *s* the ratio of the liquid-to-solid density. Here, *x* is a correlation factor estimated using the fraction of particles above the critical velocity generally approximated to be unity. This correlation may be used to estimate the minimum diameter of a PFR to avoid clogging keeping in mind that the minimum diameter, while providing the most turbulence, must be large enough to accommodate the largest crystals.

1292 Another downside of using continuous tubular reactors is that the composition of the 1293 suspension cannot be easily manipulated after the inlet. Thus, controlling the pH can be difficult 1294 (especially for reactions involving acids and bases), which may lead to unintended changes in 1295 reaction or crystallization kinetics across the reactor. Controlling pH is a special challenge in 1296 working with enzymes as biocatalysts typically work in very narrow, well-regulated pH environments. As a solution, Jiang and Ni<sup>190</sup> used multiple sampling ports across the length of a 1297 1298 tubular reactor to learn more about the slurry by off-line analysis. Another issue arises when a 1299 continuous tubular reactor requires seed crystals to initiate crystallization; either the reactor must 1300 be fed seed crystals or a recycle stream must be incorporated to introduce crystals at the inlet, 1301 complicating the design and operation of the reactor. In contrast, a well-mixed reactor (for 1302 example, an MSMPR unit) does not face this issue as it operates with a suspension of crystals 1303 that participate in secondary nucleation and foster crystal breeding during continuous operation.

Modelling, Monitoring, and Process Control. A control scheme for reactive
 crystallization processes depends on the nature of the species being produced and its desired
 characteristics. Various factors such as temperature,<sup>193</sup> pH,<sup>127</sup> and the presence of additives<sup>281</sup>
 can dictate the final crystal properties in specific processes. More generally, control of

1308 supersaturation and seeding have the greatest effect on crystal size distribution, crystal shape, 1309 and polymorphic form. Compared to crystallization alone, supersaturation may be more difficult 1310 to control in a reactive crystallization process because it can only be manipulated indirectly via 1311 adjusting the reaction rate. Extreme examples are near-instantaneous reaction rates, typical of 1312 ionic systems, where the only manipulation of the reaction rate is through the supply of reactants. 1313 Slow-reacting systems are also difficult to control as the solution stays near saturation (S  $\approx$  1.0). 1314 Reactive crystallization models that couple the kinetics of the three governing phenomena of 1315 chemical reaction, nucleation, and crystal growth are constructed to narrow an operating window that will provide a desired CSD, crystal shape, and polymorph.<sup>5, 113</sup> From models, the 1316 1317 development of process control algorithms for reactant flow rate or seed-crystal addition can be 1318 tuned to optimize robust production of the desired crystal properties.

1319 One of the earliest and most general models for semi-batch reactive crystallization 1320 processes focused on developing reactive phase equilibrium equations and diagrams based on reaction equilibria where the products are non-soluble and instantly form a solid.<sup>282</sup> While useful 1321 1322 for identifying reaction conditions and simulating reactor performances that generate only solid 1323 products, this model focused on hypothetical examples and did not include the kinetics of nucleation and growth that determine CSD and crystal shape. Kelkar and Ng<sup>283</sup> expanded this 1324 1325 model to include nucleation and growth kinetics for MSMPR crystallizers. Their model included 1326 the steps for reactions in solution generating supersaturation, nucleation, and linear growth rate 1327 of crystals from supersaturated product in solution. Applying their model for process design, 1328 they studied the reaction rate under different reactor throughput conditions, dissolution rates, and 1329 mass transfer rates. The effect of different reaction rates, nucleation rates, and growth rates on 1330 the product weight fraction distribution was also predicted.

1331 The previously discussed models primarily focus on using hypothetical kinetic 1332 parameters to simulate reactor performance, while only a few studies have been directed towards process optimization. Choong and Smith<sup>284</sup> further expanded semi-batch reactive crystallization 1333 1334 models by including a population balance to allow for the optimization of CSD. Assuming 1335 perfect mixing, the initial amount of reactants, feed addition time, and number of feeds were 1336 considered to be design variables for two optimization problems: (1) maximizing crystal size 1337 with a constraint of maximum coefficient of variation of the size distribution and (2) minimizing 1338 the coefficient of variation subject to a constraint of minimum average crystal size. A stochastic

1339 optimization framework was then used to circumvent traditional pitfalls such as nonconvergence

1340 or suboptimal solutions in highly nonlinear systems.<sup>284</sup> The model neglected secondary

1341 nucleation with the rate of nuclei generation being defined by Equation (9). Within that

1342 limitation, their model allowed for devising nonlinear control policies that could be implemented

1343 in a semi-batch reactive crystallization process.

1344 While the studies discussed above are not exhaustive, they have developed models that 1345 present the primary features of reactive crystallization processes and strategies for their 1346 optimization. Other reactive crystallization models include more specific studies on modelling and control of enantiomer and polymorph crystallization,<sup>285</sup> multi-objective optimization and 1347 generation of Pareto-optimal solutions for desired crystal properties,<sup>286</sup> incorporation of seeding 1348 1349 strategies,<sup>287</sup> resistances in double-film mass transfer models for gas-liquid systems,<sup>121</sup> and effects of macro- and micromixing regimes on crystal size distributions.<sup>114</sup> System-specific 1350 1351 models to predict control profiles for optimal mean crystal size and narrow CSD have also been developed for ampicillin,<sup>288</sup> barium carbonate,<sup>108</sup> aluminum hydroxide,<sup>115</sup> and 2,4,6 -triamino-1352 1353 1,3,5-trinitrobenzene.<sup>122</sup> Similar models for continuous reactive crystallization have also been developed but focus primarily on instantaneous reaction kinetics<sup>287</sup> or are specific to a given 1354 system<sup>5, 113</sup> and examples in the literature are still quite limited in the literature. 1355

1356 Reactive crystallization process modeling and process evaluation would not be robust 1357 without in-line monitoring using PAT and sensors to obtain qualitative and quantitative data on the evolution of the solution and crystal phases.<sup>289</sup> The use of PAT is important for process 1358 1359 monitoring, which in turn allows for analyses of reaction and crystallization mechanisms and 1360 process control. A summary of PATs common to reactive crystallization processes is shown in 1361 Figure 14. Attenuated total reflectance-Fourier transform infrared (ATR-FTIR) coupled with 1362 multivariate models is often used to analyze the liquid-phase composition during the process, as it has low solid-phase sensitivity.<sup>29, 290, 291</sup> Raman spectroscopy can be used to quantify solution 1363 1364 or crystal composition for molecules that can undergo large polarization changes and thus exhibit 1365 strong Raman scattering. Raman measurements are especially useful in systems with cocrystallization or multiple polymorphs to distinguish different solids.<sup>180, 237, 290, 291</sup> Focused beam 1366 1367 reflectance measurement (FBRM) estimates the evolution of chord-length distributions of 1368 crystals (a proxy for, but fundamentally different from, the crystal size distribution) in real time.<sup>84, 98, 146, 173, 270, 292</sup> Coupled with system-dependent algorithms, chord-length distributions 1369

1370 can be directly related to crystal size distributions; however, substantial work is required to 1371 transform chord-length distributions for comparison with size distributions obtained by laser diffraction or optical imaging.<sup>293, 294</sup> Particle vision and measurement (PVM) can provide *in situ* 1372 estimates of crystal size and shape by observing crystals in a crystallizer or a reactor as 1373 1374 transformations take place. PVM has been shown to be especially useful in observing polymorph shifts,<sup>295</sup> agglomeration,<sup>88, 296</sup> and crystal growth under different process conditions.<sup>292</sup> Other 1375 1376 monitoring techniques include HPLC for offline solution composition measurements and laser 1377 diffraction particle size analyzers coupled with image analysis to collect information about 1378 particle size and shape. Crystal structure can be further characterized offline with x-ray 1379 diffraction (XRD) and x-ray powder diffraction (PXRD). For products that undergo color 1380 changes upon degradation, a stability chamber and transmittance measurements using UV to 1381 obtain color-grade data can be used to evaluate purity of the final product. These methods are performed offline after crystal isolation but they do provide metrics for confirmation and 1382 calibration of online measurements or process stability.<sup>297</sup> PATs are often combined to give a 1383 1384 more complete view of the reaction and crystallization phenomena.



Figure 14. Common PAT used for characterizing composition and concentration of species in solution as well as crystal properties. Representative data outputs from each PAT are shown.

Control of final product properties can be achieved without modelling the system of interest but requires a detailed understanding of how different process parameters affect qualities of the solution and crystal phases. Polster *et al.*<sup>84</sup> developed a continuous reactive crystallization process for production of an API for clinical trials and studied experimentally how crystallizer residence time, temperature, solvent composition, and recycle configuration impacted size distribution, final blend flow function coefficients, yield, and tapped density. The control strategy then focused on feedback control of reactant flow rates and pH adjustments.

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1392 In any control application, model-free control is simpler and easier to implement 1393 compared to model-based optimal control, but the latter can provide superior performance if an 1394 accurate model is available. A representative example for how PAT can assist in modelling, 1395 monitoring, and optimal control during the development of a large-scale process is the reactive crystallization of glutamic acid from monosodium glutamate and sulfuric acid.<sup>298</sup> A common 1396 1397 control strategy in batch antisolvent or cooling crystallizations is to determine the optimal 1398 supersaturation trajectory for the process as a function of some manipulated variable such as 1399 temperature or anti-solvent flow rate and to design a feedback control system to maintain the optimal state using ATR-FTIR for direct measurement of solution concentrations.<sup>299, 300</sup> Direct 1400 1401 concentration control commonly used in antisolvent or cooling crystallizations is often difficult 1402 to employ in reactive crystallizations due to strong process nonlinearities that can arise from 1403 coupled reaction, dilution, and crystallization dynamics. For instance, the desired supersaturation 1404 trajectory in the reactive crystallization of glutamic acid is dome-shaped, and conventional 1405 concentration control cannot be used at many operating points because it would require a 1406 reduction in volume to hit the desired trajectory. However, volume is constantly increasing from 1407 the startup of the system due to the addition of reactants. A variation of direct concentration 1408 control known as Just-in-Time-Learning, JITL, can be employed to build a nonlinear model-1409 predictive control strategy based on extended predictive self-adaptive control that accounts for 1410 nonlinearities.<sup>301</sup> This method is used to identify a set of empirical state-space models along the desired process trajectory.<sup>177</sup> JITL has also been coupled with system models to include batch-to-1411 batch model predictive control strategies.<sup>302</sup> 1412

1413 Glutamic acid crystallization is further complicated by the existence of two polymorphs; 1414 the desired  $\alpha$  form is thermodynamically metastable and eventually transforms into the undesired 1415 but stable  $\beta$  form. Obtaining the metastable  $\alpha$  form requires a detailed monitoring and control process. Alatalo et al.<sup>290</sup> showed that ATR-FTIR measurements coupled with thermodynamic 1416 1417 modeling in a multivariate partial least squares model were effective in accurately measuring 1418 glutamic acid concentrations in solution over the course of the reaction. By using coupled ATR-FTIR and Raman spectroscopy measurements, Qu et al.<sup>291</sup> determined that formation of the 1419 1420 stable  $\beta$  polymorph was favored at high supersaturation. They speculated that this was due to the 1421  $\beta$  form having a higher barrier to nucleation than the  $\alpha$  form. The in-line monitoring techniques 1422 allowed discovery of the formation of the  $\beta$  polymorph at conditions of high global

supersaturation and in regions of poor mixing, especially those where feed was introduced above

1424 the liquid surface in the crystallizer. Alatalo *et al.*<sup>298, 303</sup> further extended this work to the design

1425 of a closed-loop feedback control algorithm based on the ATR-FTIR measured concentration of

1426 glutamic acid in solution and adjustment of the sulfuric acid feed rate with a PID controller. Such

1427 an arrangement allowed control of supersaturation and the formation of the  $\alpha$  polymorph in a 50-

1428 L reactor.

# 1429 Perspectives and Future Directions for Reactive Crystallization

1430 Reactive crystallization provides opportunities for process intensification and product improvements, which could be favorable to product economics. In this section the necessary 1431 1432 developments needed for reactive crystallization to advance to new applications are outlined, with emphasis on the need for more data, improved PAT, advanced crystallizer design, and 1433 1434 better understanding of reaction and crystallization mechanisms. Brief guidance for adaptation of 1435 existing processes or creation of new processes for reactive crystallization is given. Finally, 1436 possible future enhancements centered on reactive crystallization, primarily continuous 1437 manufacturing and hybrid systems, are outlined.

1438 *Kinetics: distinguishing reactive crystallization from other separation techniques.* 1439 Utilizing crystallization, and therefore reactive crystallization, in industrial processes presents 1440 unique challenges with respect to product quality: namely those associated with meeting criteria 1441 on crystal size, size distribution, purity and form. Such challenges must be met while also 1442 satisfying the usual process requirements of yield and economics. Advancing reactive 1443 crystallization to where it can increase the yield of a product, while at the same time meeting 1444 quality criteria, is a great challenge. Environmental and economic sustainability add urgency that 1445 new manufacturing processes are implemented and matured.

Some specific studies of how reactive crystallization can fit into a useful process have already been published.<sup>84, 113</sup> However, relating reactive crystallization to meet final product specifications including purity, size distribution, morphology (including polymorphic form and crystal shape), and more, remains a difficult task. For example, a few authors have undertaken the task of optimizing simulated reactive crystallization processes,<sup>79, 282, 284</sup> but bypassed the significant effort required to characterize the reaction kinetics and crystallization kinetics in the combined reactive crystallization environment. 1453 Several authors have shown that the kinetics of crystal growth and nucleation, which 1454 together with system configuration determine product crystal size distribution, can vary in the presence of other species such as reactants and byproducts.<sup>17, 75, 76</sup> Elucidating reaction and 1455 1456 crystallization kinetics in complex environments requires large volumes of data, which can come 1457 from either high-throughput or data-rich experiments. High-throughput experimentation involves 1458 measuring reaction and crystallization (that is, nucleation and growth) rates across a large 1459 sampling of process conditions and compositions to predict complex process features such as 1460 crystal size distribution. Data-rich experimentation, on the other hand, uses a smaller number of 1461 experiments, but with collection of high-dimensional data, such as crystal size distribution, 1462 which can be used to work backwards and determine reaction and crystallization kinetics. Both 1463 approaches enable the required level of description for designing new reactive crystallization 1464 processes, and substantial progress has been made towards both ends; however, each approach also comes with its own hurdles and challenges.<sup>304-306</sup> 1465

Reactive crystallizations typically take place in more complex solutions than cooling, 1466 1467 antisolvent, or evaporative crystallization; PAT tools that are effective in such complex solutions 1468 would enable more accurate modeling and precise control of reactive crystallization processes. 1469 Taking ATR-FTIR as an example, each dissolved species contributes to the overall IR spectrum, 1470 and through careful construction of calibration models the concentration of each species can be extracted from the overall spectrum.<sup>110, 307, 308</sup> However, the presence of uncharacterized species 1471 such as impurities, intermediates, byproducts, or catalysts, can break calibration models, and the 1472 1473 work required to characterize all species and their combination may be too laborious or even 1474 impossible (e.g. non-isolatable intermediates). Improved baselining algorithms and regression 1475 techniques may make calibration model construction more manageable, such as recent work by Maggioni et al.<sup>111</sup> based on blind source separation and independent component analysis 1476 1477 requiring only single point calibration with robustness against unknown species. The 1478 methodology was demonstrated on mixtures of simple oxyanions and did not perform as well 1479 when the anions' spectra overlapped. For many reactive crystallizations the reactants, 1480 intermediates, and products have similar functional groups and IR spectra; continued 1481 chemometric development is required for general solution phase monitoring by spectroscopic 1482 methods. Additionally, many species may only be present at low concentration compared to the 1483 reactants and products. In the production of terephthalic acid the intermediate 4-CBA has a

1484 maximum concentration of <10% of the total concentration of aromatics, leading to 1% 4-CBA 1485 in the final product. Using control to minimize the 4-CBA concentration is difficult as improved 1486 spectroscopic analysis would be needed to quantify the small amount of 4-CBA in such a complex solution (see Figure 5).<sup>193, 309</sup>Likewise, in the enzymatic production of beta-lactam 1487 1488 antibiotics the undesired byproduct phenylglycine (see Figure 6) may crystallize and contaminate 1489 the antibiotic slurry. Detecting the nucleation of phenylglycine amounts to detecting a change in 1490 phenylglycine concentration of <10 mmol/L in a solution with >100 mmol/L 6-APA and PGME, 1491 both of which have IR spectra with significant overlap with phenylglycine, and has proven to be very challenging with ATR-FTIR.<sup>310</sup> 1492

1493 Improvement in the characterization of solids will also benefit reactive crystallization 1494 process design and process control. In the case of beta-lactams the ability to distinguish between 1495 antibiotic crystals and byproduct crystals in situ could circumvent the challenges associated with 1496 solution-phase monitoring. FBRM has been used to indicate polymorph transformation in paracetamol<sup>311</sup> and in-situ microscopy with machine learning has been demonstrated for 1497 classifying individual crystals versus agglomerates.<sup>37</sup> Both FBRM and *in situ* microscopy are 1498 restricted to use in slurries of low solids concentration.<sup>312, 313</sup> Reactive crystallization would 1499 1500 benefit considerably from the development of techniques that can identify new particle types 1501 with minimal training data and calibration effort, especially since many systems involve solid reactants dissolving, reacting, and crystallizing.<sup>196, 206, 314, 315</sup> A promising development for these 1502 systems, where solution concentration cannot quantify reaction conversion, are composite PAT 1503 arrays and crystallization informatics.<sup>289</sup> An array of complimentary sensors combined with 1504 1505 process expertise has been shown to enable quantification of different solids concentrations in other solution-mediated solids transformations, such as polymorph transformations<sup>316</sup> and 1506 hydrate-to-anhydrate transformations;<sup>317</sup> application to a reactant-to-product transformation 1507 1508 follows naturally.

**Determining the applicability and utility of reactive crystallization.** Heuristics to identify when a reactive crystallization could enhance a process do not exist and should be created. It is often assumed that the product must be less soluble than the reactants, however fedbatch and continuous stirred-tank reactors (with independent solution and solids residence times) can enable reactive crystallization even when the product is more soluble. Use of co-formers can decrease the solubility of the product below that of the reactants, also enabling productive

- 1515 reactive crystallization. A brief guide to how reactive crystallization can improve a process is
- 1516 presented in Table 4, below.
- 1517Table 4. A list of useful heuristics for recognizing when reactive crystallization is advantageous and/or1518feasible.

Product Type	
Inorganic	Reactive crystallization almost always possible, preferable with
	sparingly soluble compounds, mixing control key to supersaturation
	control and size control
Organic Ionizable	Usually possible with appropriate counter-ion. Preferable for
	temperature-sensitive compounds and hydrates. Ideal for isolating
	intermediates, overcoming reaction equilibrium. Requires modest
	aqueous solubility in charged state
Organic Nonionic	Should be evaluated on a case by case basis. Examples of successful
	processes include covalent reactions eliminating charged groups in
	aqueous solution (e.g. amide bond formation) or creating charged
<u> </u>	groups in nonpolar solvents (e.g. hydrogenolysis)
Critical Quality and Pro	ocess Attributes
Yield, Productivity,	Reactive crystallization ideal for improving yields and selectivity by
Selectivity,	shifting equilibrium, isolating inhibitory products, protecting reactive
Sustainability	intermediates
Purity, Form, Solvate	Complex composition in reaction mixture can increase number of
	possible impurities, may change form preference from pure solution,
	reaction solvents may limit solvate options
Crystal Size	Fast reactions, i.e. neutralizations and acidifications, will create a
Distribution	fines-dominated CSD. Slow reactions and seeding typically give large
	crystals. Reaction rate modification by catalyst engineering can enable
	fine-tuning of CSD
Methods of Reactive C	rystallization
Neutralization	Reactive crystallization by neutralization ideal for intermediate
	process steps, e.g. isolating an intermediate as a calcium salt before
	dissolving salt for further processing. Limited by neutralizing agents,
	usually calcium, magnesium, and ammonium
Acidification	Ionizable compounds typically least soluble in protonated (neutrally
	charged) form, ideal for removing acids/bases from complex mixtures
	of nonionic species
Covalent reaction	System specific, often catalyst dependent. Least generalizable but
	most opportunity for process improvement. Requires that the catalyst
	be in a form that can easily be separated from the crystal product

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1520

Continuous manufacturing. The end-to-end integrated continuous manufacturing

- 1521 paradigm is becoming increasingly important in the pharmaceutical industry, due in large part to
- 1522 the potential benefits of lower costs, shorter supply chains, smaller footprints, and better quality

monitoring and controls with PAT.<sup>259, 318, 319</sup> In this relatively new paradigm in pharmaceutical manufacturing, reactive crystallization processes should be designed to be adapted to the whole process, rather than considered as an independent unit operation. For example, traditional batch operations may allow operational flexibility over a range of conditions, such that the reaction time can be shortened or extended based on the extent of reaction; such alterations are not easily made in continuous reactors.

1529 Control of raw materials to an integrated reactive crystallization is important, as: (1) raw 1530 materials often include insoluble particles requiring a clarification bypass system beforehand;<sup>320</sup> 1531 (2) variability in raw materials (like differences in purity or water content) could result in lower 1532 yield or higher impurity profile. Batch processes have more flexibility to handle raw material 1533 variability; different control strategies for continuous reactive crystallization may be more or less 1534 amenable to mitigating the risks of variability in raw material composition, based on the 1535 frequency and extent of the irregularity.

1536 *Novel reactive crystallization process designs.* Process intensification has been cited as 1537 one of the primary reasons for implementing a reactive crystallization process. Further intensification can be found with examples of evaporative reactive crystallization,<sup>202</sup> cooling 1538 reactive crystallization,<sup>321</sup> membrane-assisted reactive crystallization,<sup>322, 323</sup> liquid-liquid 1539 extraction reactive crystallization,<sup>181</sup> and chromatography-assisted reactive crystallization.<sup>241, 324</sup> 1540 1541 In each case multiple techniques may be applied simultaneously: for example, a reaction 1542 occurring in one liquid phase, crystallization occurring in a second liquid phase, and rapid mass transfer between phases;<sup>322</sup> or sequentially: for example, a reactive crystallization occurring at 1543 1544 high temperature with fast reaction kinetics followed by cooling to reduce solubility and generate supersaturation while sacrificing reaction speed.<sup>89</sup> 1545

1546 Most complex chemical processes require catalysts to control reactions and produce 1547 desired products. Using stoichiometric amounts of catalysts is often undesirable from the 1548 standpoints of process economics as well as purification. Catalysts must be recovered for 1549 sustainability and product purity. Separating solid catalysts from a crystal slurry can be 1550 prohibitively difficult; several examples of reactive crystallization followed by dissolution for the purpose of catalyst recovery have already been discussed.<sup>92, 198</sup> Alternatively a soluble 1551 1552 catalyst can be used and retained/recovered via ultrafiltration, which may work well for 1553 dissolved biocatalysts as bio-macromolecules can be separated from small molecules with

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ease.<sup>182, 325</sup> Nanofiltration, which has proven useful for removing impurities during
crystallization,<sup>326</sup> may be useful for recovery of non-biologic soluble catalysts. However,
membranes are subject to fouling and are not compatible with all solvents, substrates, and
catalysts, in which case the pursuit of solid-solid separations based on size, density, or other
properties may be preferable. Examples of such solid-solid crystal-catalyst separators include
hydrocyclones,<sup>141</sup> elutriation,<sup>327</sup> and sieves.<sup>198</sup>

Further research into the fundamentals of crystallization in complex environments, i.e.
with multiple solutes, solvents, and surfaces, will enable future synthesis and separation
processes with improved yield and sustainability.

### 1563 **Concluding remarks**

1564 As process designers continue to experiment with novel methods of increasing economic 1565 and environmental sustainability, reactive crystallization has become increasingly attractive as a 1566 means to those ends. Reactive crystallization is not particularly new, as ionic compounds have 1567 been synthesized by reactive crystallization since the beginning of the chemical industry. 1568 However, new applications of reactive crystallization promise to make possible new processes 1569 and improve existing ones. New applications of ionic reactive crystallization include capturing 1570 greenhouse gases as carbonates, recovering minerals from wastewater, and enabling fermentation 1571 routes to platform chemicals. Covalent reactive crystallization, while less developed, has more 1572 promise as a tool to enhance existing reactions or overcome the kinetic and equilibrium 1573 limitations of formerly untenable reactions. Biocatalytic processes could benefit the most, as 1574 those systems are most sensitive to accumulations of products and intermediates. Additionally, 1575 crystallization plays a dominant role in processes to separate enantiomers, where the 1576 combination of a racemization reaction and crystallization can lead to enantiomeric excess 1577 greater than 99%. The design of reactive crystallization systems follows closely the design of 1578 crystallizers in general. Crystallization is a highly nonlinear process; controlling crystallization 1579 coupled with a reaction is difficult but many control strategies and reactor designs have proven 1580 effective for specific cases. The future of reactive crystallization rests on collection of more data 1581 and generalization of findings from disparate case studies, which is the primary aim of this 1582 review. While this review may not be exhaustive, it should serve as a starting point for the design 1583 of reactive crystallization processes for any type of compound across many scales of industry.

## 1584 Conflicts of Interest

1585 The authors have no conflicts to declare.

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