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Complete List of Authors:	Ogihara, Hitoshi; Saitama University, Tajima, Hiroki; Saitama University Kurokawa, Hideki; Saitama University, Graduate School of Science & Engineering

## ARTICLE

## Pyrolysis of Mixtures of Methane and Ethane: Activation of Methane with the Aid of Radicals Generated from Ethane

Hitoshi Ogihara,\*<sup>a</sup> Hiroki Tajima<sup>a</sup> and Hideki Kurokawa<sup>a</sup>Received 00th January 20xx,  
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Direct chemical conversion of methane (CH<sub>4</sub>) has been actively researched in order to use natural gas as a chemical resource. However, the high stability of CH<sub>4</sub> molecules hinders the chemical conversion of CH<sub>4</sub>. In this study, we investigated pyrolysis of mixtures of CH<sub>4</sub> and ethane (C<sub>2</sub>H<sub>6</sub>) at 973~1073K. Even though CH<sub>4</sub> alone did not react in the temperature range, mixtures of CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> and of Ar/C<sub>2</sub>H<sub>6</sub> showed different pyrolysis behaviours; the co-existence of CH<sub>4</sub> significantly increased yields of propylene (C<sub>3</sub>H<sub>6</sub>), propane (C<sub>3</sub>H<sub>8</sub>) and toluene. Mass spectrometry analysis using <sup>13</sup>C-labeled CH<sub>4</sub> revealed that carbon contained in CH<sub>4</sub> was incorporated into the pyrolysis products. The results suggested that CH<sub>4</sub> was activated with the aid of C<sub>2</sub>H<sub>6</sub>. We assumed that CH<sub>4</sub> was attacked by radical species generated from pyrolysis of C<sub>2</sub>H<sub>6</sub> and was converted into methyl radicals. The CH<sub>4</sub>-derived methyl radicals were incorporated into pyrolysis products via radical reactions. This study clarified that CH<sub>4</sub> can be activated by radicals generated from co-existing molecules without the help of catalysts or extremely high temperature.

### Introduction

Innovations in shale gas extraction technology are boosting the use of natural gas in various fields. Natural gas is expected to play an active role as a raw material for the chemical industry. This is because petroleum, which is a fossil resource that plays a major role in the current chemical industry, is depleting rapidly. Methane (CH<sub>4</sub>), a main component of natural gas, is industrially used to produce synthesis gas via steam reforming. In addition, ethane (C<sub>2</sub>H<sub>6</sub>), a secondary component of natural gas, can be converted to ethylene (C<sub>2</sub>H<sub>4</sub>) via thermal cracking. Steam reforming and thermal cracking are typical examples of methods of chemical conversion of natural gas, however, although industrial interest in natural gas conversion has intensified, most natural gas is presently used as fuel for thermal power generation etc. In other words, natural gas plays a more limited role in the current chemical industry compared with petroleum.

The reason is attributed to the high stability of the CH<sub>4</sub> molecule; the high stability of CH<sub>4</sub> hampers the chemical conversion processes for natural gas<sup>1</sup>. Thus, the development of technology to convert natural gas into essential chemicals is being intensively researched. In particular, direct conversion processes of CH<sub>4</sub> such as coupling to produce lower olefins<sup>2-7</sup> and aromatization<sup>8,9</sup> are being rigorously explored.

In contrast, Periana et al. developed a catalyst for the selective oxidation of mixtures of CH<sub>4</sub>, C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub> to alcohol esters.<sup>10</sup> Such direct conversion of CH<sub>4</sub>-based hydrocarbon mixtures is interesting from the viewpoint of direct utilization of natural gas

because natural gas is a CH<sub>4</sub>-based hydrocarbon mixture (C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub> are present as secondary and tertiary components). In related works, dehydrogenative conversion of lower olefins containing CH<sub>4</sub> using zeolite-supported catalysts has also been investigated.<sup>10-15</sup>

However, the chemical conversion of CH<sub>4</sub>-based hydrocarbon mixtures is not easy because the reactivities of CH<sub>4</sub> and other hydrocarbons are quite different; in brief, CH<sub>4</sub> is much more stable than other hydrocarbons. Pyrolysis of CH<sub>4</sub> has been intensively investigated,<sup>16-20</sup> and among various hydrocarbons, CH<sub>4</sub> requires extreme high temperatures (> approx. 1473 K) for pyrolysis reactions.<sup>1,18</sup> However, such high temperatures are too severe for other hydrocarbons. For most hydrocarbons, coke should be formed by deep dehydrogenation under the conditions appropriate for pyrolysis of CH<sub>4</sub>. Conversely, reaction conditions suitable for pyrolysis of other hydrocarbons such as C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub> are too mild to activate CH<sub>4</sub> molecules, indicating CH<sub>4</sub> does not react.

So far, most studies have focused on catalysts that enable the direct activation of CH<sub>4</sub>. However, indirect activation routes would be feasible; for example, OH radicals generated from H<sub>2</sub>O on a molten salt catalyst activate CH<sub>4</sub> molecules and promote the coupling of CH<sub>4</sub>.<sup>21,22</sup> In addition, CH<sub>4</sub> activation by gas phase atomic clusters has been investigated.<sup>23</sup> Thus, if active radical species can be generated, CH<sub>4</sub> would be activated with the aid of the radicals. In this study, pyrolysis of mixtures of CH<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> was examined. We clarified that CH<sub>4</sub> was activated by C<sub>2</sub>H<sub>6</sub>-derived radicals; as a result, even under mild conditions where CH<sub>4</sub> alone did not react, CH<sub>4</sub> molecules played a role in the pyrolysis reaction and were incorporated into pyrolysis products.

<sup>a</sup> Graduate School of Science and Engineering, Saitama University, 255 Shimo-Okubo, Sakura-ku, Saitama 338-8570, Japan. E-mail: ogihara@mail.saitama-u.ac.jp

## Experimental

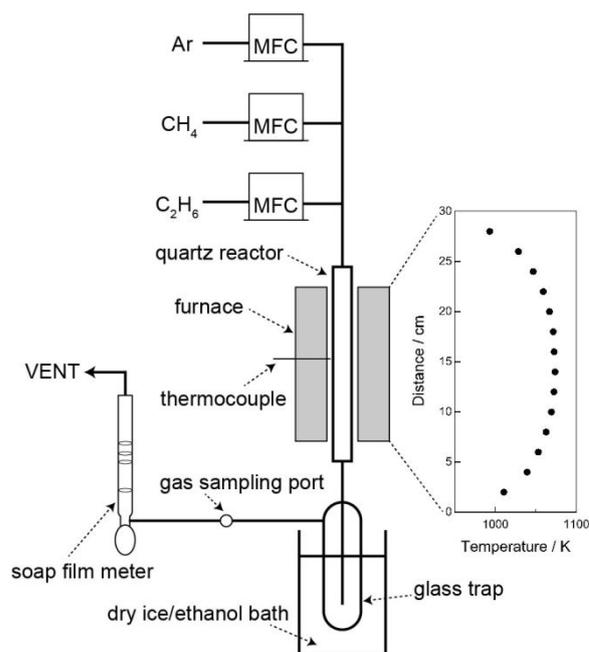
### Pyrolysis reactions

Schematic diagram of reactor system is shown in Fig. 1. Pyrolysis reactions were carried out with a quartz reactor (i.d. = 10 mm, o.d. = 12 mm) that was heated with an electric furnace. The temperature profile for the furnace is shown in Fig. 1. Flow rates of CH<sub>4</sub> (99.999%), C<sub>2</sub>H<sub>6</sub> (99.7%), and Ar (99.99%) were controlled by using mass flow controllers. The reactor was purged by flowing Ar for 10 min, and then heated to reaction temperature (973–1073 K). By introducing mixtures of CH<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> or of Ar and C<sub>2</sub>H<sub>6</sub>, pyrolysis was carried out for 1 h. Hereafter, mixtures of CH<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> and of Ar and C<sub>2</sub>H<sub>6</sub> will be denoted as CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> and Ar/C<sub>2</sub>H<sub>6</sub>, respectively. Volume fractions of C<sub>2</sub>H<sub>6</sub> in the gas mixtures were adjusted to 0.17, 0.25, and 0.50, and flow rates of the gas mixtures were controlled at 10, 30, and 50 mL min<sup>-1</sup>. The flow rates of the outlet gas were measured by a soap film flowmeter.

During the pyrolysis reaction, outlet gas of 0.5 mL was collected with a gas-tight syringe and injected into gas chromatographs every 15 min. For H<sub>2</sub>, CH<sub>4</sub>, and C<sub>2</sub>H<sub>6</sub>, a gas chromatograph (Shimadzu GC-8A, TCD) equipped with a packed column (Active carbon) was used at 473 K (injection/detector) and 443 K (column) under flowing Ar as a carrier gas. For C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>2</sub>, and C<sub>3</sub> hydrocarbons, a gas chromatograph (Shimadzu GC-8A, FID) equipped with a packed column (Unibeads 1S) was used at 453 K (injection/detector) and 383 K (column) under flowing N<sub>2</sub> as a carrier gas. To quantify gaseous products, calibration curves for all products were prepared by injecting different volume of the gases. The gases were collected from a gas cylinder (99.999% H<sub>2</sub>, 99.999% CH<sub>4</sub>, and 99.7% C<sub>2</sub>H<sub>6</sub>) or a gas can (GL Science Inc; 99.5 % C<sub>2</sub>H<sub>4</sub>, 0.100% C<sub>2</sub>H<sub>2</sub>, 99.5% C<sub>3</sub>H<sub>6</sub>, and 99.5% C<sub>3</sub>H<sub>8</sub>). Formation rates of the products were calculated based on the flow rates and the GC analysis.

Aromatics (benzene, toluene, styrene, and naphthalene) formed by the pyrolysis were collected in a glass trap cooled with a dry ice/ethanol bath. After the reaction, the trapped aromatics were dissolved in acetonitrile and then 30 mM butyl acetate in acetonitrile (1 or 2 mL) was added as an internal standard. The obtained solution was injected into a gas chromatograph (Shimadzu, GC-18A) equipped with a capillary column (Shinwa chemical industries Ltd., ULBON HR-1, 0.25 mm i.d., 30 m) under flowing N<sub>2</sub> as a carrier gas. Temperature for injection/detector was settled at 523 K and temperature for column was raised from 313 K to 473 K at 10 K min<sup>-1</sup>. To quantify the aromatics, solutions containing different amounts of benzene (99.5%, Kanto Chemical Co., Inc.), toluene (99.5%, Kanto Chemical Co., Inc.), styrene (99.0%, Kanto Chemical Co., Inc.), naphthalene (98.0%, Kanto Chemical Co., Inc.), and butyl acetate (99.0%, FUJIFILM Wako Pure Chemical Corporation) in acetonitrile (99.5%, Kanto Chemical Co., Inc.) were prepared and calibration curves were prepared by injecting the solutions into the GC.

Conversions of CH<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> were calculated based on gas composition analysed by GC and flow rates of mixture gas. Mass balance was calculated from ratios of carbon atoms for components of feed and outlet gases and trapped solutions.



**Fig. 1** Schematic diagram of reaction system and the temperature profile for the furnace.

Equilibrium conversion and standard free energy of formation for hydrocarbons ( $\Delta G_r^\ominus$ ) was calculated using HSC Chemistry (Outotec).

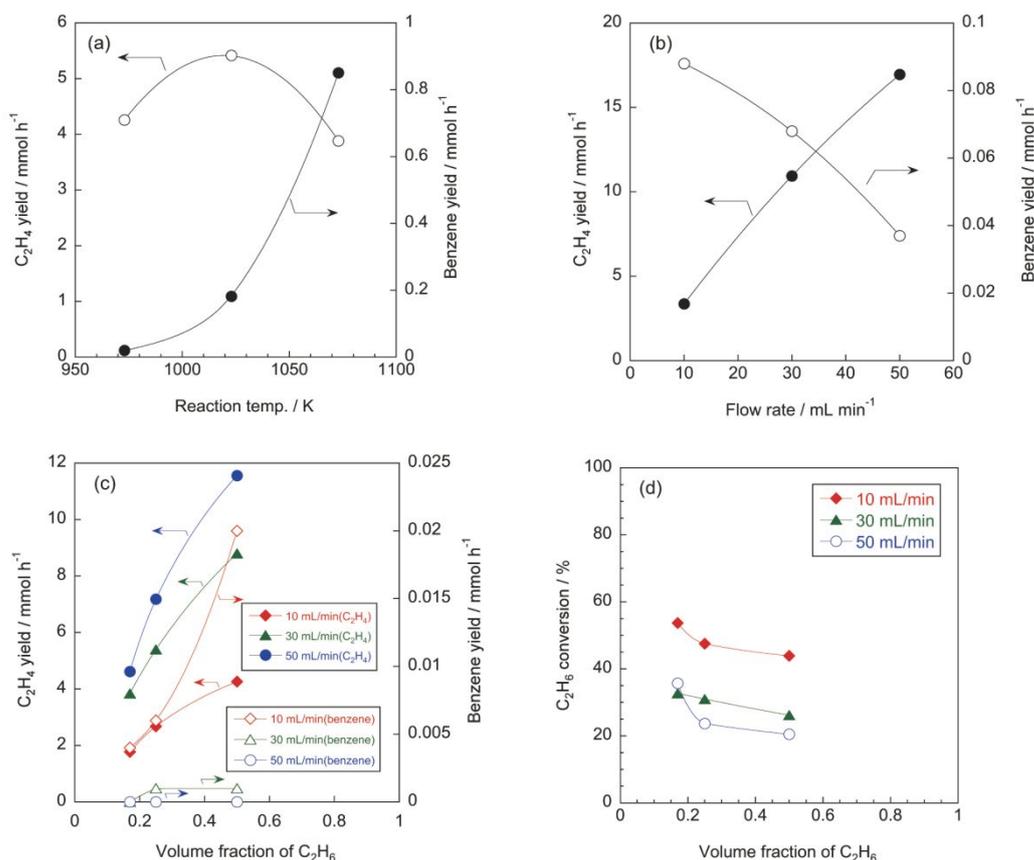
### Pyrolysis reactions using <sup>13</sup>C-labeled CH<sub>4</sub>

Pyrolysis reactions using <sup>13</sup>C-labeled CH<sub>4</sub> (<sup>13</sup>CH<sub>4</sub>; Watari Co. Ltd.) were carried out on a closed gas-circulation system (224 mL) equipped with an electric furnace. The closed gas-circulation system was mainly made of Pyrex glass and a reactor that was heated with an electric furnace was made of quartz glass. After evacuating the closed gas-circulation system, <sup>13</sup>CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> (20 kPa/20 kPa) or He/C<sub>2</sub>H<sub>6</sub> (20 kPa/20 kPa) were introduced. The reactor was heated to 1073 K under circulating the gas mixtures and maintained for 2 h. During the reaction, the aromatics were collected in a glass trap cooled with a dry ice/ethanol bath. After the reaction, the trapped aromatics were dissolved in acetonitrile and mass spectra of the aromatics were obtained with GC-MS (Bruker, SCION SQ) equipped with a capillary column (Bruker, BR-5ms, 0.25 mm i.d., 30 m).

**Table 1** All results of pyrolysis reactions in this study.

entry	reaction temp. / K	reactant gas	volume fraction of C <sub>2</sub> H <sub>6</sub>	flow rate / mL min <sup>-1</sup>	yield / μmol h <sup>-1</sup>											conv. <sup>b)</sup> / %		mass balance / %
					H <sub>2</sub>	CH <sub>4</sub> <sup>a)</sup>	C <sub>2</sub> H <sub>6</sub>	C <sub>2</sub> H <sub>4</sub>	C <sub>2</sub> H <sub>2</sub>	C <sub>3</sub> H <sub>8</sub>	C <sub>3</sub> H <sub>6</sub>	C <sub>6</sub> H <sub>6</sub>	C <sub>7</sub> H <sub>8</sub>	C <sub>8</sub> H <sub>8</sub>	C <sub>10</sub> H <sub>8</sub>	CH <sub>4</sub>	C <sub>2</sub> H <sub>6</sub>	
1	973	Ar/C <sub>2</sub> H <sub>6</sub>	0.5	10	5011	731	6978	4258	11	4	76	20	2	1	0.3	n/a	43.9	94.2
2	973	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.5	10	5138	13356	7444	4496	13	12	109	16	2	1	0.4	-1.7	42.3	96.7
3	1023	Ar/C <sub>2</sub> H <sub>6</sub>	0.5	10	7457	2010	3360	5418	28	7	121	182	14	14	12	n/a	73.1	85.1
4	1023	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.5	10	7900	15746	3607	5668	29	16	181	202	15	12	12	-20.1	72.0	93.2
5	1073	Ar/C <sub>2</sub> H <sub>6</sub>	0.5	10	8764	5831	1238	3882	57	3	60	508	20	31	62	n/a	90.1	80.5
6	1073	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.5	10	9648	18610	1524	4204	54	7	109	522	30	34	58	-44.7	88.0	89.8
7	973	Ar/C <sub>2</sub> H <sub>6</sub>	0.25	10	2898	319	3346	2678	11	1	32	6	0.4	n.d.	n.d.	n/a	47.5	97.9
8	973	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.25	10	2710	19680	3393	2481	12	8	63	5	0.4	n.d.	n.d.	2.1	46.8	96.0
9	1023	Ar/C <sub>2</sub> H <sub>6</sub>	0.25	10	4494	1559	1157	3364	26	2	52	88	5	6	7	n/a	79.6	89.5
10	1023	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.25	10	4590	20406	1485	3331	25	9	123	86	8	5	5	-1.2	76.8	94.2
11	1073	Ar/C <sub>2</sub> H <sub>6</sub>	0.25	10	5280	1819	311	2463	50	1	28	239	8	14	30	n/a	94.3	73.0
12	1073	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.25	10	6029	21788	612	2672	47	4	90	251	17	15	24	-8.4	90.4	92.7
13	973	Ar/C <sub>2</sub> H <sub>6</sub>	0.17	10	1916	165	1953	1771	10	0.4	15	4	0.3	n.d.	n.d.	n/a	53.7	91.1
14	973	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.17	10	1873	22490	2259	1619	9	6	47	2	0.3	n.d.	n.d.	1.2	46.1	97.2
15	1023	Ar/C <sub>2</sub> H <sub>6</sub>	0.17	10	3071	811	693	2238	24	1	25	60	2	2	4	n/a	83.5	85.3
16	1023	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.17	10	3404	23104	947	2382	26	6	103	47	6	4	3	-0.9	77.4	97.3
17	1073	Ar/C <sub>2</sub> H <sub>6</sub>	0.17	10	3599	1571	209	1667	47	0.2	14	129	3	6	14	n/a	95.0	75.7
18	1073	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.17	10	4568	23411	334	1984	48	3	81	154	12	9	16	-2.2	92.0	94.4
19	973	Ar/C <sub>2</sub> H <sub>6</sub>	0.5	30	9882	473	27007	8797	25	2	68	1	n.d.	n.d.	n.d.	n/a	26.2	98.7
20	973	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.5	30	10149	39915	26705	8386	25	16	103	1	n.d.	n.d.	n.d.	-1.5	27.3	97.9
21	1023	Ar/C <sub>2</sub> H <sub>6</sub>	0.5	30	20085	3170	13316	17459	80	17	332	132	5	3	3	n/a	61.7	96.0
22	1023	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.5	30	21066	41303	13881	16799	82	43	450	123	12	7	3	-5.9	61.3	94.8
23	1073	Ar/C <sub>2</sub> H <sub>6</sub>	0.5	30	27284	7769	5463	17287	209	13	314	756	17	24	34	n/a	84.9	81.9
24	1073	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.5	30	27551	47205	5678	18353	206	33	537	736	24	27	28	-20.6	84.1	92.1
25	973	Ar/C <sub>2</sub> H <sub>6</sub>	0.25	30	5687	227	12796	5395	24	1	28	n.d.	n.d.	n.d.	n.d.	n/a	31.0	98.8
26	973	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.25	30	5152	59286	13357	4871	24	16	68	n.d.	n.d.	n.d.	n.d.	1.9	30.1	97.7
27	1023	Ar/C <sub>2</sub> H <sub>6</sub>	0.25	30	12473	1368	6223	10941	74	5	133	68	7	5	2	n/a	65.7	101.4
28	1023	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.25	30	11930	59433	6637	9604	64	29	299	46	6	3	0.8	1.3	65.1	95.0
29	1073	Ar/C <sub>2</sub> H <sub>6</sub>	0.25	30	16412	4165	2047	10793	199	3	130	292	3	6	12	n/a	88.6	89.8
30	1073	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.25	30	17353	62212	2355	10650	185	18	385	252	7	7	19	-3.3	87.5	93.2
31	973	Ar/C <sub>2</sub> H <sub>6</sub>	0.17	30	3817	137	8570	3838	23	0.4	16	n.d.	n.d.	n.d.	n.d.	n/a	32.7	98.4
32	973	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.17	30	3214	64877	9227	3024	22	11	47	n.d.	n.d.	n.d.	n.d.	-0.4	27.8	99.4
33	1023	Ar/C <sub>2</sub> H <sub>6</sub>	0.17	30	8998	1045	3574	7723	68	3	23	46	3	3	1	n/a	76.8	88.8
34	1023	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.17	30	9164	64408	4536	7323	62	22	263	33	4	2	0.5	-0.8	68.9	98.3
35	1073	Ar/C <sub>2</sub> H <sub>6</sub>	0.17	30	11468	2966	987	7602	185	1	19	202	2	4	15	n/a	99.1	77.5
36	1073	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.17	30	13015	64175	876	8141	167	13	353	180	6	5	10	-0.7	94.3	94.0
37	973	Ar/C <sub>2</sub> H <sub>6</sub>	0.5	50	12156	415	50438	11555	41	1	53	n.d.	n.d.	n.d.	n.d.	n/a	20.5	98.4
38	973	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.5	50	12481	67289	50763	11319	38	20	84	n.d.	n.d.	n.d.	n.d.	-0.3	19.3	99.4
39	1023	Ar/C <sub>2</sub> H <sub>6</sub>	0.5	50	32276	2931	29434	28272	112	20	412	49	3	1	0.6	n/a	53.3	94.9
40	1023	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.5	50	33106	69008	29123	27750	112	70	596	49	2	1	0.6	-2.8	53.4	96.0
41	1073	Ar/C <sub>2</sub> H <sub>6</sub>	0.5	50	46302	8525	11065	34253	391	25	599	611	10	12	20	n/a	82.3	83.6
42	1073	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.5	50	48454	76300	12148	34998	390	64	972	594	14	14	20	-13.6	80.7	92.4
43	973	Ar/C <sub>2</sub> H <sub>6</sub>	0.25	50	7165	215	25122	7180	37	0.5	25	n.d.	n.d.	n.d.	n.d.	n/a	23.7	98.5
44	973	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.25	50	6892	98540	24831	5894	37	20	61	n.d.	n.d.	n.d.	n.d.	1.1	24.1	97.1
45	1023	Ar/C <sub>2</sub> H <sub>6</sub>	0.25	50	19571	1796	12678	16951	101	7	171	37	2	2	0.5	n/a	61.5	94.0
46	1023	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.25	50	18142	100294	14487	13050	85	46	333	20	2	1	n.d.	-0.6	55.8	94.9
47	1073	Ar/C <sub>2</sub> H <sub>6</sub>	0.25	50	27145	5836	4560	19518	315	7	239	278	2	4	11	n/a	86.1	86.6
48	1073	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.25	50	28294	103283	5319	19925	312	39	722	231	5	4	7	-5.4	83.3	98.0
49	973	Ar/C <sub>2</sub> H <sub>6</sub>	0.17	50	4429	148	14111	4620	36	0.2	12	n.d.	n.d.	n.d.	n.d.	n/a	32.2	90.4
50	973	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.17	50	3599	105133	16386	3948	34	15	95	n.d.	n.d.	n.d.	n.d.	2.7	23.7	96.4
51	1023	Ar/C <sub>2</sub> H <sub>6</sub>	0.17	50	12528	936	7243	10989	87	3	81	23	0.7	1	0.3	n/a	65.2	91.0
52	1023	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.17	50	11820	109066	9741	10206	73	37	305	8	0.3	n.d.	n.d.	-0.5	54.9	99.0
53	1073	Ar/C <sub>2</sub> H <sub>6</sub>	0.17	50	18047	3318	1941	13027	303	2	113	192	0.9	2	10	n/a	90.6	85.0
54	1073	CH <sub>4</sub> /C <sub>2</sub> H <sub>6</sub>	0.17	50	19563	109098	3235	13611	266	24	595	125	3	2	4	-0.7	85.0	96.2
55	1073	CH <sub>4</sub>	0	10	n.d. <sup>c)</sup>	n/a	3	1	n.d.	0.002 <sup>d)</sup>	n/a	102.0						

<sup>a)</sup> CH<sub>4</sub> yields for CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> conditions contained not only formed CH<sub>4</sub> but also feed CH<sub>4</sub>; <sup>b)</sup> average value in pyrolysis for 1h; <sup>c)</sup> although C<sub>2</sub>H<sub>6</sub> and C<sub>2</sub>H<sub>4</sub> was formed by dehydrogenation reactions, H<sub>2</sub> could not be detected because hydrocarbon was analysed by using GC-FID at the highest sensitivity but H<sub>2</sub> was analysed by using GC-TCD; <sup>d)</sup> the CH<sub>4</sub> conversion was calculated on the basis of the yields of C<sub>2</sub>H<sub>6</sub> and C<sub>2</sub>H<sub>4</sub>.



**Fig. 2** C<sub>2</sub>H<sub>4</sub> and benzene yields for Ar/C<sub>2</sub>H<sub>6</sub> condition at different (a) reaction temperatures, (b) flow rates and (c) volume fractions of C<sub>2</sub>H<sub>6</sub>. (d) C<sub>2</sub>H<sub>6</sub> conversion at different flow rates and volume fractions. (a) flow rate: 10 mL min<sup>-1</sup>, volume fraction of C<sub>2</sub>H<sub>6</sub>: 0.5; (b) reaction temperature: 1023 K, volume fraction of C<sub>2</sub>H<sub>6</sub>: 0.25; (c, d) reaction temperature: 973 K.

## Results and discussion

In this study, pyrolysis reactions of two different gas mixtures (i.e., CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> and Ar/C<sub>2</sub>H<sub>6</sub>) were carried out by controlling three reaction parameters: (1) reaction temperature, (2) gas flow rate, and (3) gas composition. Consequently, 55 experimental results were obtained and are summarized in Table 1. In these reactions, the pyrolysis products were hydrogen (H<sub>2</sub>), CH<sub>4</sub>, C<sub>2</sub>H<sub>4</sub>, acetylene (C<sub>2</sub>H<sub>2</sub>), propylene (C<sub>3</sub>H<sub>6</sub>), C<sub>3</sub>H<sub>8</sub>, benzene (C<sub>6</sub>H<sub>6</sub>), toluene (C<sub>7</sub>H<sub>8</sub>), styrene (C<sub>8</sub>H<sub>8</sub>), and naphthalene (C<sub>10</sub>H<sub>8</sub>). Coke was also produced depending on the reaction conditions. Note that CH<sub>4</sub> conversions under CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> conditions were calculated based on the amount of CH<sub>4</sub> in the inlet and the outlet gases, therefore, when CH<sub>4</sub> was formed from C<sub>2</sub>H<sub>6</sub> (Eqs. 1 and 2), the amount of CH<sub>4</sub> in the outlet gas increased so that the CH<sub>4</sub> conversion became negative.

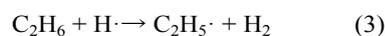


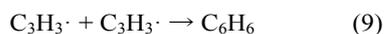
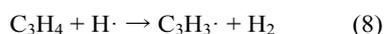
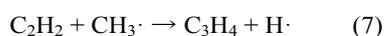
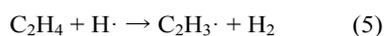
Before considering the main subject (i.e., activation of CH<sub>4</sub> with the aid of C<sub>2</sub>H<sub>6</sub>), the basic effects of the reaction parameters on the pyrolysis behaviour will be considered.

### Effect of reaction temperature

To discuss the effect of reaction temperature, we used several results of Ar/C<sub>2</sub>H<sub>6</sub> conditions as examples (entries 1, 3, 5 in Table 1). C<sub>2</sub>H<sub>6</sub> conversions increased to 44, 73, and 90% as reaction temperature increased to 973, 1023, and 1073 K, which is because the pyrolysis reactions are endothermic. Fig. 2a shows C<sub>2</sub>H<sub>4</sub> and benzene yields at different reaction temperatures. Because C<sub>2</sub>H<sub>4</sub> and benzene were the main products in the reaction, their yields may become higher with increasing C<sub>2</sub>H<sub>6</sub> conversion with the reaction temperatures. While the benzene yield increased with the reaction temperatures, the C<sub>2</sub>H<sub>4</sub> yield dropped at 1073 K. As for the formation of H<sub>2</sub>, dehydrogenation of C<sub>2</sub>H<sub>6</sub> to C<sub>2</sub>H<sub>4</sub> mainly contributed at 973 K. For example, in entry 1, the yields of C<sub>2</sub>H<sub>4</sub> and H<sub>2</sub> was 4258 and 5011 μmol h<sup>-1</sup>; the amounts C<sub>2</sub>H<sub>4</sub> and H<sub>2</sub> were similar. At higher temperature, the formation of benzene and coke also contributed to the formation of H<sub>2</sub>.

According to previous studies on CH<sub>4</sub> pyrolysis,<sup>24, 25</sup> benzene is formed by the recombination of propargyl radicals (C<sub>3</sub>H<sub>3</sub>·), which are generated via H abstraction reactions of C<sub>2</sub>H<sub>6</sub>.





In addition, there is another model that cyclopentadienyl radical is an important intermediate.<sup>26, 27</sup>

Considering that  $\text{C}_2\text{H}_4$  is the primary product in the pyrolysis of  $\text{C}_2\text{H}_6$ ,<sup>28</sup>  $\text{C}_2\text{H}_4$  concentration should increase at high reaction temperatures because  $\text{C}_2\text{H}_6$  conversion increased with the reaction temperature. Furthermore, as shown in Eqs. 3-9, benzene is formed via  $\text{C}_2\text{H}_4$ ; therefore, it is likely that benzene formation is enhanced with increasing  $\text{C}_2\text{H}_4$  concentration at high temperature. Consequently, the  $\text{C}_2\text{H}_4$  yield was suppressed apparently by consuming  $\text{C}_2\text{H}_4$  to form benzene. This is the reason why the  $\text{C}_2\text{H}_4$  yield dropped at 1073 K.

Mass balance for carbon atoms was shown in Table 1. At 973 K, the mass balance was approx. 100%, while the mass balance decreased as increasing reaction temperature. This is because the formation of coke, indeed, the wall of the quartz reactor became black after the pyrolysis reaction at high temperature.

#### Effect of gas flow rate

The effect of gas flow rate on the pyrolysis of Ar/ $\text{C}_2\text{H}_6$  was considered by using entries 9, 27, 45 in Table 1 as typical examples. As the flow rate of the reactant gas increased to 10, 30, and 50  $\text{mL min}^{-1}$ ,  $\text{C}_2\text{H}_6$  conversions decreased to 80, 66, and 62%, respectively. The high flow rate means a short residence time of reactant gases in the reactor, which should result in the decrease in  $\text{C}_2\text{H}_6$  conversion. Yields of lower hydrocarbons such as  $\text{C}_2$  and  $\text{C}_3$  increased when the flow rate was high, and conversely, yields of aromatics decreased. As typical examples, the effect of the flow rate on yields of  $\text{C}_2\text{H}_4$  and benzene is shown in Fig. 2b. With increasing gas flow rates, the  $\text{C}_2\text{H}_4$  yields increased and the benzene yields decreased. As described above, benzene is formed via the recombination of propargyl radicals that are successively formed by H abstraction reactions of  $\text{C}_2\text{H}_6$ . Such a successive reaction is likely to be affected by the residence time of reactant gases; long residence time is favourable for the formation of benzene. Therefore, high flow rate, that is, short residence time, resulted in increasing yield of the intermediate product, namely  $\text{C}_2\text{H}_4$ .

#### Effect of volume fraction of $\text{C}_2\text{H}_6$

The volume fraction of  $\text{C}_2\text{H}_6$ , that is the concentration of  $\text{C}_2\text{H}_6$ , is a reaction parameter in this study. As shown in Table 1, product yields became higher with higher  $\text{C}_2\text{H}_6$  concentrations, and product distributions were almost the same regardless of the  $\text{C}_2\text{H}_6$  concentration. Fig. 2c shows  $\text{C}_2\text{H}_4$  and benzene yields at

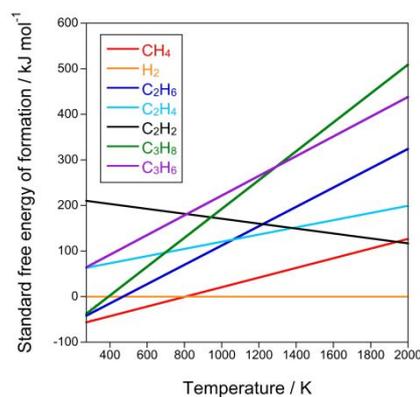


Fig. 3 Standard free energy of formation ( $\Delta G_f^\circ$ ) of hydrocarbons as a function of temperature.

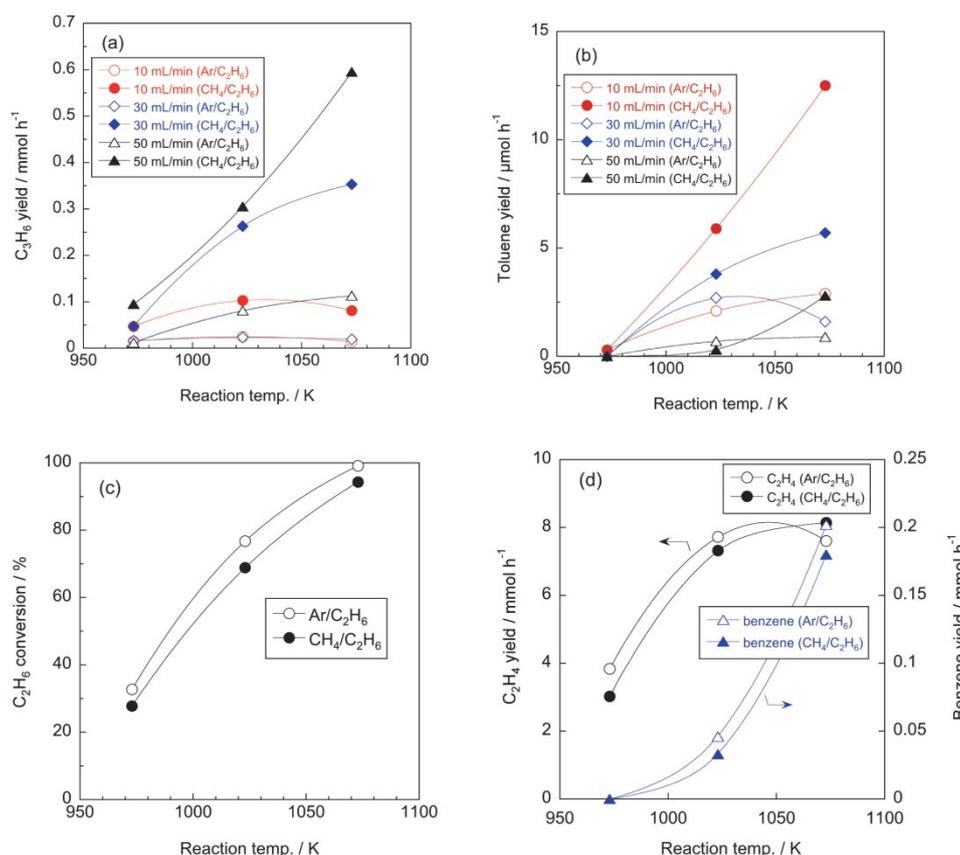
different volume fraction of  $\text{C}_2\text{H}_6$  and flow rates.  $\text{C}_2\text{H}_4$  and benzene yields tended to increase as a function of the volume fraction of  $\text{C}_2\text{H}_6$ . As described above, H abstraction from  $\text{C}_2\text{H}_6$  provides  $\text{C}_2\text{H}_4$  and benzene. Thus, it is reasonable that increase in volume fraction of  $\text{C}_2\text{H}_6$  contributed to the formation of  $\text{C}_2\text{H}_4$  and benzene. In addition, similar to Fig. 2b, as increasing flow rates,  $\text{C}_2\text{H}_4$  yield increased and benzene yield decreased regardless of volume fraction of  $\text{C}_2\text{H}_6$ .

Fig. 2d shows  $\text{C}_2\text{H}_6$  conversion at different volume fractions of  $\text{C}_2\text{H}_6$  in Ar.  $\text{C}_2\text{H}_6$  conversion was in inverse proportion to the volume fraction of  $\text{C}_2\text{H}_6$ . The dominant reaction in the pyrolysis of  $\text{C}_2\text{H}_6$  is the dehydrogenation of  $\text{C}_2\text{H}_6$  into  $\text{C}_2\text{H}_4$  ( $\text{C}_2\text{H}_6 \rightarrow \text{C}_2\text{H}_4 + \text{H}_2$ ). The equilibrium conversions for the reaction are as follows: 71, 67, and 62% for the volume fractions of 0.17, 0.25, and 0.5, respectively. This order is in accordance with the tendency of  $\text{C}_2\text{H}_6$  conversion shown in Fig. 2d.

#### Pyrolysis of $\text{CH}_4/\text{C}_2\text{H}_6$ mixtures

A  $\text{CH}_4$  molecule is so stable that  $\text{CH}_4$  alone did not react under the reaction conditions in this study. Even under the most severe condition (i.e., the highest temperature and the lowest flow rate), the  $\text{CH}_4$  conversion was approximately 0% (entry 55 in Table 1). Thermodynamic data also suggest that  $\text{CH}_4$  is much more stable than other hydrocarbons (Fig. 3). Thus, in this study,  $\text{CH}_4$  is expected to behave as an inert molecule, such as Ar and He. In other words, results in pyrolysis of  $\text{CH}_4/\text{C}_2\text{H}_6$  and Ar/ $\text{C}_2\text{H}_6$  are assumed to be the same, however, their pyrolysis results were quite different. Fig. 4a shows  $\text{C}_3\text{H}_6$  yields under  $\text{CH}_4/\text{C}_2\text{H}_6$  and Ar/ $\text{C}_2\text{H}_6$  conditions at different temperatures and flow rates. Interestingly, the  $\text{C}_3\text{H}_6$  yields were greatly increased in the presence of  $\text{CH}_4$ . For example, under the condition at 1073 K and 50  $\text{mL/min}$ ,  $\text{C}_3\text{H}_6$  yields for Ar/ $\text{C}_2\text{H}_6$  and  $\text{CH}_4/\text{C}_2\text{H}_6$  were 0.11 and 0.60  $\text{mmol h}^{-1}$ , respectively, indicating the co-existing  $\text{CH}_4$  promoted the  $\text{C}_3\text{H}_6$  formation by more than five times. The same trend was observed for  $\text{C}_3\text{H}_8$  formation.

Fig. 4b shows the effect of co-existing  $\text{CH}_4$  on toluene yields. Similar to the  $\text{C}_3$  hydrocarbons, co-existing  $\text{CH}_4$  significantly enhanced toluene formation. For example, under the condition at 1073 K and 10  $\text{mL/min}$ , toluene yield increased by more than four times (from 2.9 to 12.5  $\mu\text{mol h}^{-1}$ ).



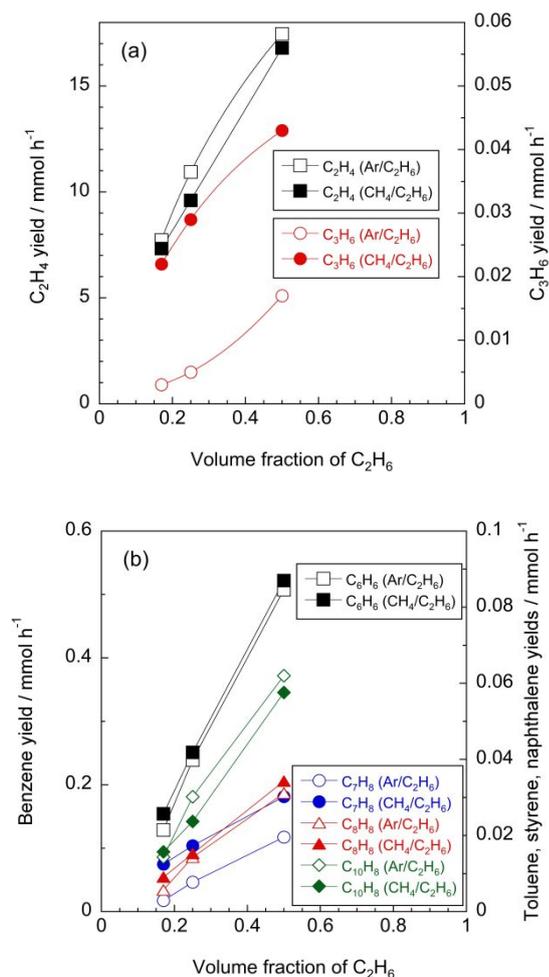
**Fig. 4** (a) C<sub>3</sub>H<sub>6</sub> yield, (b) toluene yield, (c) C<sub>2</sub>H<sub>6</sub> conversion, and (d) C<sub>2</sub>H<sub>4</sub> and benzene yields for CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> or Ar/C<sub>2</sub>H<sub>6</sub> condition at different reaction temperatures, different flow rates and C<sub>2</sub>H<sub>6</sub> volume fraction of 0.17. Flow rate for (c, d): 30 mL min<sup>-1</sup>.

From the perspective of the transition from petrochemical to natural gas chemistry, it is necessary to reconsider the production process of C<sub>3</sub>H<sub>6</sub>, which is an essential molecule in the chemical industry. In petrochemicals, C<sub>3</sub>H<sub>6</sub> (and benzene, toluene, xylene) are obtained as by-products of naphtha cracking to produce C<sub>2</sub>H<sub>4</sub>. In contrast, C<sub>2</sub>H<sub>4</sub> synthesis from C<sub>2</sub>H<sub>6</sub> in natural gas produces poor by-products. In this regard, the enhancement of C<sub>3</sub>H<sub>6</sub> formation by co-feed of CH<sub>4</sub> to C<sub>2</sub>H<sub>6</sub> would be worthwhile from the viewpoint of natural gas utilization.

Fig. 4c shows C<sub>2</sub>H<sub>6</sub> conversion for CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> and Ar/C<sub>2</sub>H<sub>6</sub> conditions. As described earlier, C<sub>2</sub>H<sub>6</sub> conversion increases with reaction temperatures, and the co-existence of CH<sub>4</sub> slightly suppressed the C<sub>2</sub>H<sub>6</sub> conversion. Probably, thermal cracking of C<sub>2</sub>H<sub>6</sub> to form CH<sub>4</sub> would be inhibited by the presence of CH<sub>4</sub>, which can be a reason why C<sub>2</sub>H<sub>6</sub> conversion slightly decreased under CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> conditions. In addition, the slight decrease in C<sub>2</sub>H<sub>6</sub> conversion in the presence of CH<sub>4</sub> indicates that the increase in C<sub>3</sub> hydrocarbons and toluene is irrelevant to C<sub>2</sub>H<sub>6</sub> conversion. Fig. 4d shows C<sub>2</sub>H<sub>4</sub> and benzene yields for CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> and Ar/C<sub>2</sub>H<sub>6</sub> conditions. As expected from Fig. 4c, C<sub>2</sub>H<sub>4</sub> and benzene were less formed under CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> conditions because C<sub>2</sub>H<sub>6</sub> conversion was suppressed in the presence of CH<sub>4</sub>. As described later, we considered that methyl radicals were generated from CH<sub>4</sub> with the aid of radicals formed from C<sub>2</sub>H<sub>6</sub>. Fig. 4 shows that while C<sub>2</sub>H<sub>4</sub> yield was hardly affected by CH<sub>4</sub>, the formation of C<sub>3</sub> hydrocarbon was enhanced in the presence

of CH<sub>4</sub>. From the results, we presumed that methyl radicals derived from CH<sub>4</sub> promoted the recombination reaction of C<sub>2</sub>H<sub>3</sub>· (or C<sub>2</sub>H<sub>5</sub>·) and CH<sub>3</sub>· to form C<sub>3</sub> hydrocarbons.

Fig. 5 shows the effect of volume fractions of C<sub>2</sub>H<sub>6</sub> on yields of lower olefins. Regardless of reaction conditions, all the product yields became higher with increasing C<sub>2</sub>H<sub>6</sub> concentration. Considering that products were mainly formed from the pyrolysis of C<sub>2</sub>H<sub>6</sub>, it is likely that the product yields were proportional to the concentration of C<sub>2</sub>H<sub>6</sub>. As shown in Fig. 5a, it appeared that the C<sub>2</sub>H<sub>4</sub> yields slightly decreased with the presence of CH<sub>4</sub>. The co-existence of CH<sub>4</sub> contributed to the decrease in C<sub>2</sub>H<sub>6</sub> conversion (Fig. 4c), thus, it is possible that the yield of the main product (i.e., C<sub>2</sub>H<sub>4</sub>) decreased with the presence of CH<sub>4</sub>. On the other hand, the C<sub>3</sub>H<sub>6</sub> yield was significantly increased by the co-existing CH<sub>4</sub> regardless of the C<sub>2</sub>H<sub>6</sub> concentration. This tendency is the same as shown in Fig. 4a. Fig. 5b shows yields of aromatics at various volume fractions of C<sub>2</sub>H<sub>6</sub>. Like the lower olefins, aromatics yields also increased with the concentration of C<sub>2</sub>H<sub>6</sub>. Comparing CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> and Ar/C<sub>2</sub>H<sub>6</sub> conditions, we can see that there were no significant effects of CH<sub>4</sub> on the benzene, styrene and naphthalene yields, while only the toluene yield increased with the CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> conditions, which is similar to the results shown in Fig. 4b. Based on the above results, the effects of co-existing CH<sub>4</sub> on the pyrolysis reactions are summarized as follows:

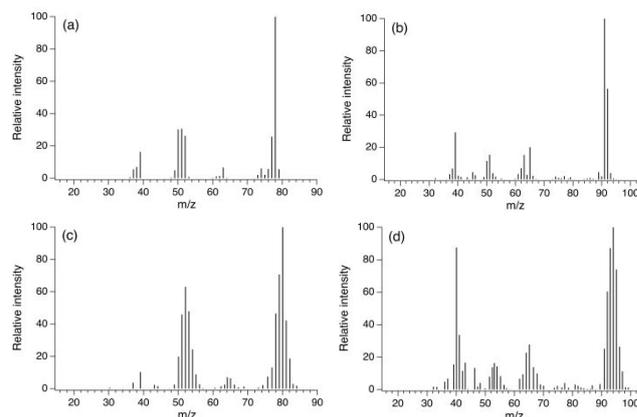


**Fig. 5** Products yield for  $\text{CH}_4/\text{C}_2\text{H}_6$  or  $\text{Ar}/\text{C}_2\text{H}_6$  condition at different volume fractions of  $\text{C}_2\text{H}_6$  in the mixture gases. (a) reaction temperature: 1023 K, flow rate: 30 mL  $\text{min}^{-1}$ , (b) reaction temperature: 1073 K, flow rate: 10 mL  $\text{min}^{-1}$ .

- $\text{C}_3\text{H}_6$ ,  $\text{C}_3\text{H}_8$  and toluene yields increased significantly in the presence of  $\text{CH}_4$ .
- $\text{C}_2\text{H}_6$  conversion was slightly lowered in the presence of  $\text{CH}_4$ .
- The influence of co-existing  $\text{CH}_4$  on main products (i.e.,  $\text{C}_2\text{H}_4$  and benzene) yields was small.

#### Mass spectrometry analysis using $^{13}\text{C}$ -labeled $\text{CH}_4$

It is well-known that  $\text{CH}_4$  molecules are significantly stable because of both their structural symmetry and strong C-H bond.<sup>1</sup> Indeed, pyrolysis of  $\text{CH}_4$  hardly took place when only  $\text{CH}_4$  was heated to 1073 K (entry 55 in Table 1). Thus, it is not surprising that  $\text{CH}_4$  molecules in  $\text{CH}_4/\text{C}_2\text{H}_6$  behaved the same as an inert gas, however,  $\text{CH}_4/\text{C}_2\text{H}_6$  showed different pyrolysis behaviour from  $\text{Ar}/\text{C}_2\text{H}_6$ . This result strongly suggests that  $\text{CH}_4$  molecules in  $\text{C}_2\text{H}_6$  played a role in the pyrolysis reaction. In order to understand the role of  $\text{CH}_4$ , pyrolysis using  $^{13}\text{CH}_4$  was carried out. If  $\text{CH}_4$  molecules were activated and converted into pyrolysis products, mass spectra of the pyrolysis products should be changed by incorporating  $^{13}\text{C}$  into them.



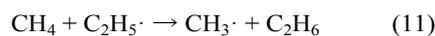
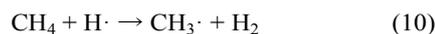
**Fig. 6** Mass spectra of (a, c) benzene and (b, d) toluene formed by dehydrogenation of (a, b)  $\text{He}/\text{C}_2\text{H}_6$  and (c, d)  $^{13}\text{CH}_4/\text{C}_2\text{H}_6$  at 1073 K.

Fig. 6 shows mass spectra of the aromatic compounds formed by pyrolysis of  $^{13}\text{CH}_4/\text{C}_2\text{H}_6$  or  $\text{He}/\text{C}_2\text{H}_6$  at 1073 K (mass spectra of  $\text{C}_2$  and  $\text{C}_3$  hydrocarbons could not be obtained due to the limitation of separation in the GC-MS system). It was no wonder that typical mass spectra of benzene and toluene were observed under the  $\text{He}/\text{C}_2\text{H}_6$  condition (Fig. 6a and 6b). On the other hand, it is interesting that mass spectra of benzene and toluene formed from  $^{13}\text{CH}_4/\text{C}_2\text{H}_6$  (Fig. 6c and 6d) were different from those of  $\text{He}/\text{CH}_4$ ; benzene and toluene from  $^{13}\text{CH}_4/\text{C}_2\text{H}_6$  had higher  $m/z$  values. The  $m/z$  values at the highest peaks were 78 (benzene from  $\text{He}/\text{CH}_4$ ), 80 (benzene from  $^{13}\text{CH}_4/\text{C}_2\text{H}_6$ ), 91 (toluene from  $\text{He}/\text{CH}_4$ ) and 94 (toluene from  $^{13}\text{CH}_4/\text{C}_2\text{H}_6$ ). The increase in  $m/z$  of benzene and toluene in the presence of  $^{13}\text{C}$  derived from  $\text{CH}_4$  strongly suggested that  $^{13}\text{C}$  derived from  $\text{CH}_4$  was incorporated into benzene and toluene during the pyrolysis reactions.

#### Reaction mechanism

The mass spectra shown in Fig. 6 indicated that  $\text{CH}_4$  was incorporated into the products in the presence of  $\text{C}_2\text{H}_6$  even though  $\text{CH}_4$  alone did not react, which implies  $\text{CH}_4$  molecules were activated with the aid of  $\text{C}_2\text{H}_6$ . Considering that no catalysts were used in this study, we assumed that radical species generated from  $\text{C}_2\text{H}_6$  would play a role to activate the stable  $\text{CH}_4$  molecules.

It is known that various radical species are formed from  $\text{C}_2\text{H}_6$  at above 773~873 K.<sup>29</sup> If the radicals abstract  $\text{H}\cdot$  from  $\text{CH}_4$  molecules,  $\text{CH}_4$  molecules generate radical species (mainly methyl radicals):



Consequently, the methyl radicals derived from  $\text{CH}_4$  molecules can convert into  $\text{C}_3\text{H}_6$  and  $\text{C}_3\text{H}_8$  by the following radical reactions:



In the above recombination reactions, CH<sub>4</sub> molecules are incorporated into C<sub>3</sub> hydrocarbons. For example, by combining Eqs. 5, 10, and 12, we know that a CH<sub>4</sub> molecule is consumed to form a C<sub>3</sub>H<sub>6</sub> molecule (CH<sub>4</sub> + C<sub>2</sub>H<sub>4</sub> + 2H $\cdot$  → C<sub>3</sub>H<sub>6</sub> + 2H<sub>2</sub>)

Also, when the methyl radical reacts with a phenyl radical, toluene is formed:



The significant increases in C<sub>3</sub> hydrocarbons and toluene yields under CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> conditions can be explained by the above mechanism; the increase in the concentration of methyl radicals promoted the formation of C<sub>3</sub> hydrocarbons and toluene. As shown in the mass spectra, CH<sub>4</sub>-derived carbon was also incorporated into benzene, which can be explained by the recombination of propargyl radicals that is formed from <sup>13</sup>CH<sub>3</sub> $\cdot$  and C<sub>2</sub>H<sub>2</sub> (Eq. 7-9).

Current strategies for CH<sub>4</sub> activation can roughly be categorized into (1) the development of catalysts that efficiently activate C-H bonds in CH<sub>4</sub> and (2) pyrolysis of CH<sub>4</sub>, where coupling of methyl radicals proceeds with the aid of extreme high temperature (> approx. 1473 K). In this study, an alternative route for the chemical conversion of CH<sub>4</sub> was proposed: radicals generated from co-existing molecules (in this study, C<sub>2</sub>H<sub>6</sub>) activate CH<sub>4</sub> molecules.

## Conclusions

Pyrolysis reactions of mixtures of CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> or Ar/C<sub>2</sub>H<sub>6</sub> were carried out at 973–1073 K. Even though CH<sub>4</sub> alone did not react in the temperature range, the pyrolysis behaviour was quite different in the presence of CH<sub>4</sub>; the formation of C<sub>3</sub> hydrocarbons and toluene was enhanced. In contrast, C<sub>2</sub>H<sub>4</sub> and benzene yields were not affected by the co-existing CH<sub>4</sub>. Mass spectrometry analysis using <sup>13</sup>C-labeled CH<sub>4</sub> revealed that CH<sub>4</sub>-derived carbon was incorporated into the pyrolysis products, indicating CH<sub>4</sub> molecules were activated and played a role in the pyrolysis reactions. Probably, radicals generated from C<sub>2</sub>H<sub>6</sub> abstracted H $\cdot$  from CH<sub>4</sub> so that CH<sub>4</sub>-derived methyl radicals would be formed. By reacting the methyl radicals with C<sub>2</sub>H<sub>3</sub> $\cdot$  and C<sub>6</sub>H<sub>5</sub> $\cdot$ , C<sub>3</sub>H<sub>6</sub> and toluene were formed. In other words, the increase in the concentration of methyl radicals enhanced the formation of C<sub>3</sub> hydrocarbons and toluene. This study clarified that CH<sub>4</sub> can be activated by radicals generated from co-existing molecules without the help of catalysts or extreme high temperature.

## Conflicts of interest

There are no conflicts to declare.

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Inert  $\text{CH}_4$  molecule can be activated and incorporated into pyrolysis products with the aid of radicals generated by pyrolysis of  $\text{C}_2\text{H}_6$ .

# CH<sub>4</sub> Activation with Radicals

