

Environmental
Science
_{Water Research & Technology}

Impacts of Antiscalants on the Formation of Calcium Solids: Implication on Scaling Potential of Desalination Concentrate

Water Impact Statement

The management of desalination brine has become increasingly important and a costly issue, especially in inland areas. In particular, the presence of oversaturated calcium as scale-forming compounds in the brine is challenging to dispose. I nthis study, we established a quantitative relationship to predict the nucleation rate of three commonly observed scale-forming calcium minerals in desalination brine and three widely used antiscalants. The modeling of precipitation rate from this study provided crucial information on the relationship among the rate of precipitation, antiscalant dosage and critical saturation index in desalination concentrate.

14 **Abstract**

15 Brackish water desalination has become increasingly important in arid inland regions for 16 reliable water supplies, but the management of desalination brine waste is costly. In 17 particular, the presence of oversaturated calcium as scale-forming compounds in the brine 18 is challenging to disposal. This study investigated the effects of three widely used 19 antiscalants, *i.e.,* nitrilotri-methylenephosphonic acid (NTMP), ethylenediaminetetra-20 methylenephosphonic acid (EDTMP) and diethylenetriaminepentakis-methylphosphonic 21 acid (DTPMP) on the precipitation of calcium from solutions under chemical conditions 22 relevant to brackish desalination brine, with an emphasis on the nucleation and 23 precipitation of three calcium-containing solids including hydroxyapatite $Ca₅(PO₄)₃OH_(s)$, 24 gypsum $CaSO_{4(s)}$, and vaterite $CaCO_{3(s)}$. The nucleation rates and activation energy of 25 nucleation were investigated for the first time for hydroxyapatite relevant to a desalination 26 concentrate. Results showed that all three antiscalants exhibited uniquely time-dependent 27 effects on the inhibition of calcium solid formation. The precipitation kinetics exhibited a 28 three-phase behavior, with an induction phase, a rapid reaction phase, and a final 29 equilibrium phase. The effectiveness of antiscalant in delaying calcium precipitation and 30 slowing down the rate of precipitation followed the order of DTPMP > EDTMP > NTMP. 31 Antiscalants adsorb on the nuclei of calcium solids and inhibit the crystal growth process. 32 Activation energy of nucleation increased linearly with antiscalant dosage, but it decreased 33 as the regime changed from homogeneous to heterogeneous nucleation. This study 34 generated vital information on the precipitation kinetics of calcium solids in the presence 35 of phosphonate-containing antiscalants and advances the development of desalination 36 brine management strategies.

38 **Introduction**

39 As freshwater scarcity becomes more severe with increasing population and climate 40 change impacts, alternative water sources - in particular, brackish groundwater - have 41 become increasingly important for arid inland regions.^{1,2} Brackish groundwater is usually 42 formed as a result of geological salt deposition or long-term agricultural activities.³⁻⁵ It 43 typically contains total dissolved solids (TDS) levels between 1 and 10 g/L .⁶⁻⁸ In recent 44 years, membrane-based brackish water desalination has been increasingly implemented to 45 supply drinking water in inland areas worldwide, including Australia, the Middle East and 46 the United States.⁹⁻¹³ For example, the operational and planned brackish groundwater 47 desalination plants in California have a combined annual capacity of 260 million gallons 48 per day as of 2013^{14}

49 Another major challenge with desalination is scaling of the membranes themselves, a 50 phenomenon attributed to the inevitable precipitation of calcium-containing minerals 51 including calcium sulfate $CaSO_{4(s)}$, calcium carbonate $CaCO_{3(s)}$ and calcium phosphate $52 \text{ Ca}_5(\text{PO}_4)_3\text{OH}_{(s)}$ at the membrane surface.^{15,16} The efficiency of reverse osmosis based 53 brackish water desalination is inherently limited by membrane scaling. To control 54 membrane scaling, scale-inhibiting chemicals known as antiscalants are added to the feed 55 water.17-19 These chemicals interfere with the nucleation process of calcium solids and 56 retard the crystal growth.²⁰ The continuous application of antiscalants in the feed water 57 results in an oversaturation of dissolved calcium that coexists with antiscalants in the 58 brackish desalination concentrate (also known as brine).^{21,22} Meanwhile, the inhibiting 59 effects of antiscalants on the precipitation of calcium solids are time sensitive. For 60 example, in the Inland Empire of Southern California, a 70-mile brine pipeline system

61 carries inland brackish water desalination concentrate to a coastal disposal facility.²³ The 62 presence of antiscalants in the discharged brine prevents calcium precipitation at the entry 63 points along the brine line, but as the brine wastewater travels along the pipeline, a 64 substantial amount of additional solids are generated, creating problematic scaling issues 65 in the pipeline.24,25 Other studies similarly reported the delayed precipitation of solids in 66 membrane concentrate.26-28 This inadvertent solid formation and associated challenge with 67 scale formation during brine disposal make it urgent to understand the effects of 68 antiscalants on solid formation.

69 Furthermore, recovery of water from desalination brine is important to minimize brine 70 disposal cost. However, the presence of oversaturated scale-forming calcium in the brine 71 is undesirable to additional water recovery. In contrast, a tunable control on antiscalants 72 can potentially accelerate the precipitation of calcium solids. This decrease in scale-73 forming constituents can help achieve higher recovery of water from brine using secondary 74 membrane units. Therefore, it is critical to understand the nature and effects of antiscalants 75 on the chemical stability of calcium solids in the brine, which can lead to the development 76 of sustainable concentrate management for inland desalination.

77 Most antiscalants are organic phosphorus chemicals known as phosphonic acids. They 78 contain multiple phosphonate functional groups $(-PQ_3H_2)$ within a tertiary amine 79 structure.29,30 The phosphorus-carbon bond in antiscalants exhibits a good thermal 80 stability,³¹ and promotes their applications in desalination plants as well as cooling 81 towers.^{32,33} The concentration of phosphonic acids in desalination processes depend on the 82 composition of the feedwater. For brackish water desalination concentrate it is typically in 83 the range of 2-10 μ M.^{34,35} In particular, nitrilotri-methylenephosphonic acid (NTMP),

84 ethylenediaminetetra-methylenephosphonic acid (EDTMP) and 85 diethylenetriaminepentakis-methylphosphonic acid (DTPMP) are among the most widely 86 used antiscalants in water industry.³⁶⁻³⁹ Their molecular structures are shown in Figure S1 87 of the SI section.

88 Prior studies examined the impact of different antiscalants on the precipitation of calcite, 89 gypsum, silica, etc.^{29,40-42} Multiple studies have tried to quantify the dose response of 90 antiscalants with respect to the extent of supersaturation.^{19,43,44} Recent studies investigated 91 the cost associated with maximizing the water recovery in membrane desalination process 92 for brackish water with these scaling minerals.⁴⁵ Phosphonic antiscalants can also form 93 complexes with calcium and undergo multiple steps of deprotonation.⁴⁶⁻⁴⁸ However, the 94 effect of antiscalants on the nucleation and crystal growth process of calcium solids 95 remains unknown. Typically, the onset of solid precipitation is delayed in the presence of 96 antiscalants. This delayed period, known as induction time, is controlled by the activation 97 energy of the nucleation process.^{49,50} A better and quantitative understanding on how 98 antiscalants impact the induction time is critical to predict the effectiveness of antiscalants. 99 Furthermore, although the presence of antiscalants delays nucleation reaction, the nuclei 100 formation eventually takes place. Therefore, it is important to quantify the kinetics of solid 101 precipitation in the presence of antiscalants.

102 In recent years, membrane-based advanced reuse of domestic wastewater in agricultural 103 and industrial sectors have been increasingly implemented. Reclaimed wastewater is also 104 increasingly used for industry and landscaping. Sparingly soluble hydroxyapatite 105 Ca₅(PO₄)₃OH_(s) in the brine becomes a major limiting factor in these scenarios where the 106 reclaimed water is rich in phosphate.⁵¹⁻⁵⁴ While there are studies mainly focused on the 107 commonly observed scaling minerals such as $CaSO_{4(s)}$ and $CaCO_{3(s)}$ ⁵⁵⁻⁵⁸ To the our best of 108 knowledge, no study has looked into the impact of antiscalants on the precipitation 109 mechanisms and kinetics of hydroxyapatite nucleation. However, the nature of calcium 110 phosphate formation and the associated antiscalant effect remains to be understood.

111 The objectives of this study were to examine the impacts of three widely used antiscalants 112 (*i.e.*, NTMP, EDTMP and DTPMP) in brackish water concentrate on the nucleation process 113 of calcium-containing solids (*i.e.*, $Ca_5(PO_4)_3OH_{(s)}$, $CaSO_{4(s)}$, and $CaCO_{3(s)}$), quantify the 114 precipitation kinetics of calcium solid formation, and the nature of calcium phosphate 115 nucleation in presence of these antiscalants.

116 **Materials and methods**

117 The solution chemical matrix for the precipitation experiments was selected based on the 118 chemical composition of the brackish RO concentrate. A synthetic concentrate allowed us 119 to precisely control and vary the saturation indices of different calcium minerals. This 120 simplified setup also helped us to understand the fundamentals of nucleation of different 121 calcium minerals in presence of the antiscalants. All solutions were prepared with 122 analytical grade chemicals and deionized (DI) water (resistivity ≤ 18.2 M Ω /cm). To start a 123 precipitation experiment with $Ca₅(PO₄)₃OH_(s)$, stock solutions of 25-50 mM CaCl₂ and 1-124 3 mM Na₂HPO₄ were prepared and adjusted to pH 7.8 with droplets of 0.5 M NaOH and 125 0.5 M HClO₄ at a temperature of 20 °C. This pH level is typical of brackish water 126 desalination brine.⁵⁹ Initial ionic strength of the mixing solution was fixed at 0.1 M by 127 adding targeted amount of NaClO4.

128 A 150 mL solution containing CaCl₂ and a 100 mL solution containing $Na₂HPO₄$ were 129 adjusted to pH 7.8. Following that, 0-10 mM of NTMP, EDTMP or DTPMP prepared from 130 its respective sodium-based salt was added into $CaCl₂$ and $Na₂HPO₄$ solutions with equal 131 concentrations. Both solutions were then quickly mixed at a high stirring rate in a batch 132 reactor at 20 °C. This approach of mixing avoided possible interference due to localized 133 concentration spikes. The final mixed solution created a targeted antiscalant concentration 134 typical to a brackish water desalination brine, ranging between 0 and 11 µM, and a 135 saturation index between 14 and 15 with respect to $Ca₅(PO₄)₃OH_(s)$. The saturation index 136 of $Ca₅(PO₄)₃OH_(s)$ is defined as:

$$
SI_{Ca_5(PO_4)_3OH} = log \left(\frac{\alpha_{Ca^2}^5 \times \alpha_{PO_4^3}^3 - \times \alpha_{OH^-}}{K_{sp, Ca_5(PO_4)_3OH_{(s)}}} \right)
$$
 (1)

137 where $\alpha_{PQ_4^3}$ -, α_{OH} - and, $\alpha_{Ca^{2+}}$ are activities of PO₄³⁻, OH and Ca²⁺, respectively. 138 $K_{\text{sp, Ca}_5(\text{PO}_4)_3\text{OH}_{\text{(s)}}}$ is the solubility product of hydroxyapatite (10^{-44.33}). Equilibrium 139 calculations and stability constants were from the Visual MINTEQ software database.⁶⁰

140 The precipitation experiments with $CaSO_{4(s)}$ and $CaCO_{3(s)}$ were performed similarly to that 141 of $Ca₅(PO₄)₃(OH)_(s)$, except that phosphate was replaced by sulfate and carbonate salt, 142 respectively. The saturation index was controlled between 0.2 to 1.2 for $CaSO_{4(s)}$. The 143 saturation index for $CaCO_{3(s)}$ was varied between 1.3 and 1.8 by adjusting the alkalinity 144 from 10 to 36 mM as carbonate. The saturation index of each solid is defined as:

$$
SI_{CaSO_4} = \log \left(\frac{\alpha_{Ca^{2+}} \times \alpha_{SO_4^{2-}}}{K_{sp, CaSO_{4(s)}}} \right)
$$
 (2)

$$
SI_{CaCO_3} = \log \left(\frac{\alpha_{Ca^{2+}} \times \alpha_{CO_3^{2-}}}{K_{sp,\;CaCO_{3(s)}}} \right) \tag{3}
$$

145 Where $\alpha_{\text{SO}_4^2}$, $\alpha_{\text{CO}_3^2}$ and α_{Ca^2} are the activities of SO₄², CO₃² and Ca²⁺, respectively, 146 while $K_{\text{sp, CaSO}_4}$ and $K_{\text{sp, CaCO}_3}$ are the solubility products of calcium sulfate and calcium 147 carbonate, respectively $(K_{\text{sp, CaSO}_4} = 10^{-4.61}$, $K_{\text{sp, CaCO}_3} = 10^{-8.48}$.⁶¹

148 After the mixing of respective solutions, precipitation experiments were conducted in a 149 250 mL batch reactor completely mixed at 400 rpm with a magnetic stir bar. The solid 150 precipitation kinetics were monitored by measuring the change of turbidity at pre-151 determined time intervals using a HACH 2100N turbidimeter. The suspension pH was 152 maintained at 7.8 ± 0.05 with a requisite amount of tris(hydroxymethyl)aminomethane 153 (TRIS) buffer. The presence of TRIS buffer has a negligible impact on the calcium 154 precipitation reaction (Figure S2). The rate of precipitation was calculated by fitting the 155 turbidity-time profile to a Michaelis-Menten type model.⁶² The rate model and the fitting 156 are described in Text S1 and Figure S3. The concentration of antiscalants was confirmed 157 by UV oxidation with H_2O_2 followed by analysis of phosphate using the standard 158 molybdate blue spectrophotometric method.⁶³ Zeta potential of precipitated calcium solids 159 was measured using Zetasizer nano ZS90 analyzer (Malvern Panalytical, Inc.). The mineral 160 phases of precipitated solids were analyzed by X-ray diffraction (XRD) and three calcium 161 solids were confirmed (Figure S4).

162 **Results and discussions**

163 *Effect of antiscalant type on the precipitation of calcium solids*

164 Figure 1A shows the kinetics of hydroxyapatite precipitation reactions in the presence of 165 three antiscalants. The precipitation kinetics on the basis of the solution turbidity exhibited 166 three distinct phases: an initial lag phase, a rapid precipitation phase and a final equilibrium 167 phase. During the lag stage, hydroxyapatite nuclei underwent a constant formation and 168 dissolution until a critical radius (denoted as $r_{critical}$) was achieved. This initial phase was 169 followed by a rapid precipitation phase where crystals grew quickly until reaching 170 equilibrium and becoming stationary in the end.

171 In the presence of 1 µM NTMP, EDTMP or DTPMP, the induction time for hydroxyapatite 172 precipitation to occur ranged between 1 and 5 minutes (Figure 1A). Phosphonate 173 antiscalants can adsorb onto the incipient nuclei generated during the induction period, 174 resulting in a distortion of crystal growth pattern and a delay of nucleation.64-66 Antiscalants 175 can also act as an impurity on the surface of a growing crystal, which slows down its further 176 growth. The presence of antiscalants can increase the surface energy of the growing 177 crystals, which decreases the rate of nucleation and increases the induction time.⁶⁷

178 The induction time of hydroxyapatite precipitation without an antiscalant was only a few 179 seconds. It significantly increased in the presence of an antiscalant compared to the control 180 (Figure 1A). Calculations showed that a majority of calcium under the brine chemical 181 condition exists as the free ion form rather than aqueous calcium-antiscalant complexes in 182 the presence of antiscalants (Text S2 and Figure S5), indicating that the inhibitive effect 183 by antiscalants likely results from the adsorption of antiscalants onto the incipient nuclei 184 of hydroxyapatite.

185 In addition, the effectiveness of antiscalant in extending the induction time followed the 186 order of DTPMP > EDTMP > NTMP (solid lines in Figure 1B). The longer induction time

9

187 of hydroxyapatite nucleation in the presence of DTPMP compared to NTMP or EDTMP 188 is likely contributed by two factors. First, antiscalants differ from each other in the number 189 of amine functional groups in their backbone structure and the number of phosphonate 190 groups (Figure S1). High-molecular-weight antiscalants with a larger number of amine 191 groups (*e.g.*, DTPMP) have a bigger molecular structure compared to the relatively low-192 molecular-weight antiscalants (*e.g.*, NTMP). When antiscalants adsorb on the incipient 193 hydroxyapatite nuclei, the high-molecular-weight DTPMP molecules occupy a larger 194 surface area of the nuclei structure, thus extending the induction time considerably.^{31,68}

195 Second, different antiscalants possess different surface charges. Calculations showed that 196 DTPMP is the most negatively charged molecule among the three antiscalants (Text S3 197 and Figure S6). Meanwhile, the point of zero charge for hydroxyapatite in the brine 198 solution was measured as 8.21 (Figure S7A), consistent with prior literature.^{69,70} At pH 7.8, 199 the surface of hydroxyapatite nuclei is positively charged and promotes the electrostatic 200 adsorption of DTPMP. Consequently, it enhanced the effectiveness of DTPMP in delaying 201 the induction time. Experimental data also confirmed that the surface charge of 202 hydroxyapatite was reduced upon DTPMP adsorption (Figure S7B).

203 The mechanism of antiscalant inhibition on hydroxyapatite nucleation was further 204 investigated by quantifying the steady-state nucleation rates, which is calculated as:

$$
J_s = F \times \exp\left(\frac{-\beta \gamma_s^3 N_A f(\theta)}{(RT)^3 \text{SI}^2}\right) \tag{4}
$$

205 where *F* is the pre-exponential factor and has a theoretical value of 10^{33} nuclei L^{-3} s⁻¹, β is 206 the shape factor (16 π /3 for spherical nuclei), γ_s is the surface energy of crystallization

207 (J/m²), N_A is the Avogadro's number (mol⁻¹), $f(\theta)$ is the correction factor (value=1 for 208 homogeneous nucleation),⁵⁸ *R* is the gas constant (8.3 J·mol⁻¹·K⁻¹), *T* is the absolute 209 temperature (K), and SI is the saturation index. Results showed that the nucleation rate 210 dropped with an increasing antiscalant dosage (dashed lines in Figure 1B). This trend is 211 also consistent with the extension of induction time (solid lines Figure 1B). A decrease in 212 the nucleation rate consequentially increases the time required for the crystal to grow and 213 delays the onset of precipitation.

214 Furthermore, with the same saturation index of hydroxyapatite, the induction time 215 increased with the antiscalant dosage (Figure 2A). For instance, an increase of EDTMP 216 dosage from 0.5 to 3 μ M increased the duration of induction time from 1.5 to 5 minutes, 217 thus delaying the onset of homogeneous crystallization. A higher antiscalant concentration 218 in the solution resulted in a higher surface adsorption of the nuclei and less surface area 219 was available for the nucleation to take place. In addition, the effects of antiscalant on the 220 induction time also depends on the extent of calcium supersaturation. For example, a higher 221 saturation index of hydroxyapatite reduced the induction time at the same dosage of 222 EDTMP (Figure 2B).

223 Typically, as the dosage of antiscalant increased, it became more effective in delaying the 224 onset of hydroxyapatite precipitation with a more oversaturated solution, as shown by the 225 extension of induction time with an increasing antiscalant dosage at a fixed saturation index 226 (Figure 3). Furthermore, the three antiscalants exhibited different effectiveness in delaying 227 hydroxyapatite precipitation, which is evaluated based on the critical saturation index 228 (CSI). For a given antiscalant dosage, CSI is defined as the maximum saturation index 229 below which a decrease in the saturation index shows a significant increase in the induction

230 time. This was quantified by measuring the slope of induction time *vs*. the saturation index 231 (Figure 3) and the CSI was the saturation index below which the average slope shows more 232 than 40% change compared to its previous value. A higher CSI suggests a stronger 233 inhibiting effect by antiscalant in precipitation. For example, at a dosage of 0.5 μ M, NTMP 234 only became effective in delaying hydroxyapatite precipitation at a saturation index less 235 than 14.40 (Figure 3A), whereas EDTMP became effective with a saturation index less 236 than 14.55 (Figure 3B), and DTPMP was effective when saturation index was below 14.69 237 (Figure 3C). A similar trend was also observed for $CaSO_{4(s)}$ and $CaCO_{3(s)}$ precipitation, 238 respectively (Figure S8). These critical saturation indices are significant in defining the 239 inhibitive effects of antiscalants on scale formation in desalination concentrate. These 240 trends are also consistent with the observation that inhibition effects on calcium solids 241 precipitation follow the order of DTPMP > EDTMP > NTMP.

242 *Thermodynamics of calcium crystallization in the presence of antiscalants*

243 According to the theory of homogenous nucleation, the duration of induction time is 244 intrinsically associated with the thermodynamics of nucleation reaction and crystal growth 245 process. Specifically, the logarithm of induction time is linearly related to the square root 246 of the saturation index of the corresponding solid as described in the equation below: $71,72$

$$
\log(t_{\text{ind}}) = A T^{-3} (\text{SI})^{-2} + B \tag{5}
$$

247 where t_{ind} is the induction time (second), T is the solution temperature (Kelvin), SI is the 248 saturation index of the solution with respect to a calcium-containing solid (dimensionless), 249 and both *A* and *B* are fitting parameters. This linear relationship was observed during the 250 precipitation of $Ca₅(PO₄)₃OH_(s), CaCO_{3(s)}$ and $CaSO_{4(s)}$ (Figure S9).

- 251 The surface energy of crystallization, γ_s (J/m²), was calculated using the equation 6 below
- 252 using the value of *A* obtained from equation 5:

$$
\gamma_{\rm s} = \left(\frac{A (2.3R)^3}{\beta V_{\rm m}^2 N_{\rm A} f(\theta)}\right)^{1/3} \tag{6}
$$

253 where β is the geometry factor and has a value of $16\pi/3$ for a spherical nucleus, V_m is the 254 molecular volume of the crystal $(1.2 \times 10^{-28} \text{ m}^3/\text{molecule}$ for gypsum,⁷³ 6.1 \times 10⁻²⁹ 255 /molecule for vaterite,⁷⁴ and 2.6×10^{-28} m³/molecule for hydroxyapatite^{75,76}).

256 The Gibbs free energy of homogenous nucleation with respect to the radius of the nucleus 257 is calculated as:77-79

$$
\Delta G = -\frac{4\pi r^3 kT(SI)}{3V_m} + 4\pi r^2 \gamma \tag{7}
$$

258 where *k* is the Boltzmann constant $(1.38 \times 10^{-23} \text{ J} \cdot \text{K}^{-1})$. The first term in Equation 7 259 represents the change in the bulk free energy. The second term is the change in the surface 260 free energy that results from the formation of new interface between the new nuclei and 261 the aqueous phase.

262 When the Gibbs free energy of nucleation reaches a maximum, the radius of the nucleus is 263 defined as the critical radius of nucleation (r_{critical}), and the corresponding Gibbs free energy 264 is defined as the activation energy of nucleation $(\Delta G_{\text{critical}})$. r_{critical} is the minimal radius of 265 the nucleus that is required for the initiation of crystal growth and precipitation. A typical 266 calculated trend of the nucleation process is shown in Figure 4A. For Equation 7, when r $267 = r_{\text{critical}}$, $\left(\frac{d}{d}G}{dr}\right) = 0$. Therefore,

$$
r_{\text{critical}} = \frac{2\gamma V_{\text{m}}}{kT(SI)}\tag{8}
$$

268 Accordingly, a combination of Equations 7 and 8 results in the following expression:

$$
\Delta G_{\text{critical}} = \frac{16\pi\gamma^3 V_{\text{m}}^2}{3 k^2 T^2 S I^2}
$$
\n(9)

269 Calculations show that values of $\Delta G_{\text{critical}}$ and r_{critical} decreased with an increase in saturation 270 index (Figures S10-S11). A higher oversaturation level increases the probability of 271 collisions between nuclei, and exerts a stronger driving force for nucleation, therefore 272 decreasing the requirement on the size of subcritical nuclei reaching the *r*_{critical}.

273 To understand the effect of antiscalants on the precipitation thermodynamics, the effect of 274 antiscalant dosage on the activation energy of calcium solid nucleation was investigated. 275 Figure 4B shows a plot of relative changes in activation energy of nucleation $(\Delta G_{\text{critical}})$ as 276 a function of EDTMP dosage for different calcium solids. $CaCO_{3(s)}$ and $CaSO_{4(s)}$ showed 277 a linear increase in the activation energy with an increasing EDTMP dosage. 278 Ca₅(PO₄)₃OH_(s), however, only showed a similar trend at a low EDTMP dosage up to 1 279 µM, and its activation energy decreased with a further increase in the EDTMP dosage from 280 1 μ M to 4 μ M (open circles, Figure 4B).

281 The decrease in the activation energy of nucleation of $Ca₅(PO₄)₃OH_(s)$ at higher EDTMP 282 dosages can be attributed to a transition from homogenous to heterogeneous nucleation. 283 Plotting the log of induction time of hydroxyapatite in presence of EDTMP against the 284 saturation ratio exhibited two distinct linear correlations (Figure S9A), suggesting a 285 transition from homogenous to heterogenous nucleation when the saturation index 286 decrease. This effect was only observed with lower saturation indices and higher 287 antiscalant dosages. Similar findings were reported for the precipitation of calcium solids 288 changing from homogeneous to heterogenous nucleation at lower saturation indices.⁷² The 289 heterogeneous nucleation can take place due to the presence of freshly formed 290 hydroxyapatite acting as seeds for nucleation.⁸⁰ The free energy barrier is smaller for 291 heterogeneous nucleation compared to that for homogeneous nucleation.⁸¹ Thus, to 292 calculate the homogeneous activation energy of hydroxyapatite nucleation the results with 293 higher antiscalant dosage and lower saturation indices conditions were discarded. The 294 recalculated results showed a linear increase with EDTMP dosage (closed circles, Figure 295 4B).

296 *Effect of antiscalant on the kinetics of calcium solids precipitation*

297 The rate of hydroxyapatite precipitation depended on the antiscalant dosage and the 298 saturation index (Figure 5). In general, at a fixed level of oversaturation, the rate of 299 precipitation decreased with an increasing antiscalant dosage. Meanwhile, the rate of 300 precipitation increased with a higher saturation index for any given antiscalant dosage.

301 In addition, different antiscalants exhibited distinct dosage-response behaviors on the 302 precipitation rate. For example, NTMP showed a very strong dosage effect that highly 303 depends on the level of oversaturation (Figure 5A). At a fixed NTMP dosage, as the 304 saturation index increased beyond a critical value, the precipitation rate increased 305 significantly. On the contrary, the dosage effect of EDTMP on the precipitation rate was 306 moderate (Figure 5B), and that of DTPMP was insensitive to the saturation index (Figure 307 5C). The use of EDTMP or DTPMP at a low dosage of 0.5 µM is as effective as higher 308 dosages in slowing down the precipitation kinetics regardless of calcium saturation, but 309 NTMP at 0.5 μ M was only effective at a low calcium saturation level. These trends suggest 310 that EDTMP and DTPMP are more effective than NTMP in suppressing the rate of 311 hydroxyapatite precipitation. This difference likely resulted from a higher surface blockage 312 of nuclei by the larger antiscalant molecules of EDTMP and DTPMP, and the consequently 313 stronger inhibitive effects on the growth of calcium crystals.

314 **Conclusion**

315 These findings show that although all three of the antiscalants considered have active 316 phosphonate functional groups, they affect the precipitation kinetics of calcium solids 317 differently. Antiscalants are only effective in temporarily stabilizing the oversaturated 318 desalination brine and delay the scale-forming substances (in this case, calcium solids) 319 from precipitation. Results from this study established a quantitative relationship between 320 the nucleation rate of three most commonly observed calcium-scaling solids and three most 321 widely used antiscalants. Accordingly, it provided guidance on the threshold dosage of 322 these antiscalants that can hold a certain duration of time to prevent the oversaturated brine 323 waste from scale formation. Furthermore, with an ever-increasing dependence on 324 desalination, especially in inland areas, and more desalination facilities targeting a near 325 zero liquid discharge, brine demineralization (*i.e.*, TDS removal) is the key to increasing 326 water recovery and managing the concentrate waste. The modeling of precipitation rates 327 from this study provided crucial information on the relationships among the rate of 328 precipitation, the antiscalant dosage, and the critical saturation index; together these can 329 help to determine the targeted amount of antiscalant that needs to be removed to achieve a 330 high rate of demineralization. The optimization of an efficient demineralization technique 331 is crucial and will be further investigated in the future.

332 **Acknowledgement**

333 This research was supported by grants to H.L. from the National Science Foundation

334 (Grant #1611306) and to T.J. from the National Water Research Institute. We thank the

- 335 assistance of John Orta at UCR, Jesus Trujillo from San Bernardino Middle College High
- 336 School and Osvaldo Mireles from San Bernardino Valley College on participation.

337 **Supporting Information Section**

338 Additional description of molecular structures of the antiscalants, calculation procedure for 339 kinetic modeling, XRD spectra, free calcium ion calculations in each antiscalant system 340 and antiscalant molecular charge calculations, figures on induction time and activation 341 energy dependence on antiscalant concentration and saturation index are available in the 342 SI section.

343

344 Figure 1 (A) Comparison among three antiscalants on their effects on the kinetics of 346 hydroxyapatite precipitation. $[Ca^{2+}] = 10$ mM; $[PO_4^{3-}] = 26$ mg P/L; saturation index = 347 14.2; [antiscalant] = 1 μ M. pH = 7.8; ionic strength = 100 mM; [TRIS buffer] = 20 mM. 348 (B) Impact of different antiscalant dosage on the induction time (solid lines) and the 349 nucleation rate (dashed lines) of hydroxyapatite. $[Ca^{2+}] = 10 \text{ mM}$; $[PO_4^{3-}] = 30 \text{ mg } P/L$; 350 saturation index = 14.6; pH = 7.8; ionic strength = 100 mM; [TRIS buffer] = 20 mM.

353 **Figure 2** The effects of EDTMP dosage and saturation index on induction time of 354 precipitation of hydroxyapatite. (A) $\left[Ca^{2+}\right] = 10 \text{ mM}$; $\left[PO_4^{3-}\right] = 26 \text{ mg } P/L$; saturation index 355 = 14.2; EDTMP = 0-3 μ M; pH = 7.8; ionic strength = 100 mM; [TRIS buffer] = 20 mM. 356 (B) $[Ca^{2+}] = 10$ mM; $[PO_4^{3-}] = 22-25$ mg P/L; EDTMP = 2 µM; pH = 7.8; ionic strength = 357 100 mM; [TRIS buffer] = 20 mM.

358

359

360 **Figure 3** The effect of antiscalant dosage on induction time of precipitation of 361 hydroxyapatite. (A) $[Ca^{2+}] = 10$ mM; $[PO_4^{3-}] = 17-34$ mg-P/L; saturation index = 14.1-362 14.9; pH = 7.8; ionic strength = 100 mM; [TRIS buffer] = 20 mM. (B) $[Ca^{2+}] = 10$ mM; 363 $[PO_4^3] = 22-31$ mg-P/L; saturation index = 14.3-14.8; pH = 7.8; ionic strength = 100 mM;

364 [TRIS buffer] = 20 mM. (C) $[Ca^{2+}] = 10$ mM; $[PO_4^3] = 24-35$ mg P/L; saturation index =

365 14.5-14.9; pH = 7.8; ionic strength = 100 mM; [TRIS buffer] = 20 mM.

366

368 **Figure 4** (A) Gibbs free energy for homogeneous nucleation of $CaSO_{4(s)}$ at varying NTMP 369 dosages. $[Ca^{2+}] = 37$ mM; $[SO_4^2] = 564$ mM; Saturation index = 0.84; pH = 7.8. (B) Impact 370 of EDTMP dose on activation energy of different calcium solids; Experimental conditions 371 for CaCO_{3(s)}: $[Ca^{2+}] = 10$ mM; $[CO_3^2] = 10$ mM; $[EDTMP] = 0-21$ µM; saturation index $372 = 1.32$; pH = 7.8; ionic strength = 100 mM; [TRIS buffer] = 50 mM; Experimental 373 conditions for CaSO_{4(s)}: $[Ca^{2+}] = 37$ mM; $[SO_4^2] = 564$ mM; $[EDTMP] = 0-21 \mu M$; 374 saturation index = 7; $pH = 7.8$; ionic strength = 1M. Experimental conditions for 375 $Ca₅(PO₄)₃OH_(s)$: homogeneous nucleation (closed circles), heterogeneous nucleation (open 376 circles); $[Ca^{2+}] = 10 \text{ mM}$; $[PO_4^{3-}] = 0.6 \text{ mM}$; $[EDIMP] = 0.4 \mu\text{M}$; saturation index = 14.2; 377 pH = 7.8; ionic strength = 100 mM; [TRIS buffer] = 20 mM.

Figure 5 Impact of antiscalant dosage on rate of precipitation of hydroxyapatite in presence 382 of (A): NTMP (saturation index = 14.1-14.9); (B): EDTMP (saturation index = 14.3-14.8) 383 and (C): DTPMP (saturation index = 14.5-14.8). $[Ca^{2+}] = 10$ mM; pH = 7.8; ionic strength 384 = 100 mM; [TRIS buffer] = 20 mM.

386 **References**

- 1 Vörösmarty, C. J.; Green, P.; Salisbury, J.; Lammers, R. B. Global water resources: vulnerability from climate change and population growth. *Science* **2000**, 289 (5477), 284-288.
- 2 Trenberth, K. E. Changes in precipitation with climate change. *Climate Research* **2011**, 47, 123-138.
- 3 Seckin, G.; Yilmaz, T.; Sari, B.; Ersu, C. B. Groundwater hydrochemistry at the Mediterranean coastal plains—the case of Silifke, Turkey. *Desalination* **2010**, 253 (1), 164-169.
- 4 Giambastiani, B. M. S.; Colombani, N.; Mastrocicco, M.; Fidelibus, M. D. Characterization of the lowland coastal aquifer of Comacchio (Ferrara, Italy): hydrology, hydrochemistry and evolution of the system. *Journal of hydrology* **2013**, 501, 35-44.
- 5 Barlow, P. M.; Reichard, E. G. Saltwater intrusion in coastal regions of North America. *Hydrogeology Journal* **2010**, 18 (1), 247-260.
- 6 US Geological Survey. National Brackish Groundwater Assessment. USGS Water Availability and Use Science Program.

https://water.usgs.gov/ogw/gwrp/brackishgw/brackish.html (Access on 2/5/2019)

7 Ahmed, M.; Shayya, W. H.; Hoey, D.; Al-Handaly, J. Brine disposal from reverse osmosis desalination plants in Oman and the United Arab Emirates. *Desalination* **2001**, 133 (2), 135-147.

- 8 Ruiz-García, A.; Ruiz-Saavedra, E.; Feo-García, J. Start-up of brackish water desalination for agricultural irrigation in the Canary Islands (Spain). *Desalination and Water Treatment* **2016**, 57 (48-49), 22734-22742.
- 9 Shannon, M. A.; Bohn, P. W.; Elimelech, M.; Georgiadis, J. G.; Marinas, B. J.; Mayes, A. M. Science and technology for water purification in the coming decades. *Nature* **2008**, 452 (7185), 301-310.
- 10 CÙtÈ, P.; Siverns, S.; Monti, S. Comparison of membrane-based solutions for water reclamation and desalination. *Desalination* **2005**, 182 (1-3), 251-257.
- 11 Werber, J. R.; Osuji, C. O.; Elimelech, M. Materials for next-generation desalination and water purification membranes. *Nature Reviews Materials* **2016**, 1, 16018.
- 12 Famiglietti, J.; S. The global groundwater crisis. *Nature Climate Change*. **2014**,4, 945- 8.
- 13 El Saliby, I.; Okour, Y.; Shon, H. K.; Kandasamy, J.; Kim, I. S. Desalination plants in Australia, review and facts. *Desalination*. **2009**, 247, 1-4.
- 14 "Desalination (Brackish and Sea Water)." California Water Plan Update 2013. Retrieved November 28, 2018 from

http://www.water.ca.gov/waterplan/docs/cwpu2013/Final/Vol3_Ch10_Desalination.pd

f. (access on 2/5/2019)

- 15 Benecke, J.; Rozova, J.; Ernst, M. Anti-scale effects of select organic macromolecules on gypsum bulk and surface crystallization during reverse osmosis desalination. *Separation and Purification Technology* **2018**, 198, 68-78.
- 16 Shirazi, S.; Lin, C. J.; Chen, D. Inorganic fouling of pressure-driven membrane processes—a critical review. *Desalination* **2010**, 250 (1), 236-248.
- 17 Greenlee, L. F.; Lawler, D. F.; Freeman, B. D.; Marrot, B.; Moulin, P. Reverse osmosis desalination: water sources, technology, and today's challenges. *Water research* **2009**, 43 (9), 2317-2348.
- 18 Pramanik, B. K.; Gao, Y.; Fan, L.; Roddick, F. A.; Liu, Z. Antiscaling effect of polyaspartic acid and its derivative for RO membranes used for saline wastewater and brackish water desalination. *Desalination* **2017**, 404, 224-229.
- 19 Neveux, T.; Bretaud, M.; Chhim, N.; Shakourzadeh, K.; Rapenne, S. Pilot plant experiments and modeling of $CaCO₃$ growth inhibition by the use of antiscalant polymers in recirculating cooling circuits. *Desalination* **2016**, 397, 43-52.
- 20 Sheikhi, A.; Li, N.; van de Ven, T. G.; Kakkar, A. Macromolecule-based platforms for developing tailor-made formulations for scale inhibition. *Environmental Science: Water Research & Technology* **2016**, 2 (1), 71-84.
- 21 Ahmed, M.; Arakel, A.; Hoey, D.; Thumarukudy, M. R.; Goosen, M. F.; Al-Haddabi, M.; Al-Belushi, A. Feasibility of salt production from inland RO desalination plant reject brine: a case study. *Desalination* **2003**, 158 (1-3), 109-117.
- 22 Van der Bruggen, B.; Lejon, L.; Vandecasteele, C. Reuse, treatment, and discharge of the concentrate of pressure-driven membrane processes. *Environmental science & technology* **2003**, 37 (17), 3733-3738.
- 23 Santa Ana Watershed Project Authority Website; http://www.sawpa.org/brineline/what-is-it/ (access on 2/5/2019)
- 24 Owens-Bennett, E. L.; Trussell, B.; Monroy, I.; Trussell, R. Proposed solids formation recovery formula for the inland empire brine line; October 10, **2016**.
- 25 Benjamin, M. M.; Lawler, D. F.; Tobiason, J. E. Inland empire brine line expert panel; June 29-30, 2011.
- 26 Greenlee, L. F.; Testa, F.; Lawler, D. F.; Freeman, B. D.; Moulin, P. Effect of antiscalants on precipitation of an RO concentrate: metals precipitated and particle characteristics for several water compositions. *Water research* **2010**, 44 (8), 2672- 2684.
- 27 Greenlee, L. F.; Testa, F.; Lawler, D. F.; Freeman, B. D.; Moulin, P. The effect of antiscalant addition on calcium carbonate precipitation for a simplified synthetic brackish water reverse osmosis concentrate. *Water research* **2010**, 44 (9), 2957-2969.
- 28 Hasson, D.; Drak, A.; Semiat, R. Induction times induced in an RO system by antiscalants delaying CaSO4 precipitation. *Desalination* **2003**, 157 (1-3), 193-207.
- 29 Darton, E. G.; Scale inhibition techniques used in membrane systems. *Desalination* **1997**, 113 (2), 227-229.
- 30 Austin, A. E.; Miller, J. F.; Vaughan, D.A.; Kircher, J.F. Chemical additives for calcium sulfate scale control. *Desalination* **1975**, 16 (3), 345-357.
- 31 Ketrane, R.; Saidani, B.; Gil, O.; Leleyter, L.; Baraud, F. Efficiency of five scale inhibitors on calcium carbonate precipitation from hard water: effect of temperature and concentration. *Desalination* **2009**, 249 (3), 1397-1404.
- 32 Abd-El-Khalek, D. E.; Abd-El-Nabey, B. A. Evaluation of sodium hexametaphosphate as scale and corrosion inhibitor in cooling water using electrochemical techniques. *Desalination* **2013**, 311, 227-233.
- 33 He, F.; Sirkar, K. K.; Gilron, J. Effects of antiscalants to mitigate membrane scaling by direct contact membrane distillation. *Journal of Membrane Science* **2009**, 345 (1), 53-58.
- 34 Nowack, B. The behavior of phosphonates in wastewater treatment plants of Switzerland. *Water research* **1998**, 32 (4), 1271-1279.
- 35 Kumar, P.S.; Ejerssa, W.W.; Wegener, C.C.; Korving, L.; Dugulan, A.I.; Temmink, H.; van Loosdrecht, M.C.; Witkamp, G.J. Understanding and improving the reusability of phosphate adsorbents for wastewater effluent polishing. *Water research* **2018**, 145, 365-374.
- 36 Sweeney, F. M.; Cooper, S.D. The development of a novel scale inhibitor for severe water chemistries. In SPE *International Symposium on Oilfield Chemistry* **1993**. Society of Petroleum Engineers.
- 37 Carter Jr, R. P.; Carroll, R. L.; Irani, R. R. Nitrilotri (methylenephosphonic acid), ethyliminodi-(methylenephosphonic acid), and diethylaminomethylphosphonic acid: acidity and calcium (II) and magnesium (II) complexing. *Inorganic Chemistry* **1967**, 6 (5), 939-942.
- 38 Pairat, R.; Sumeath, C.; Browning, F. H.; Fogler, H. S. Precipitation and dissolution of f alcium – ATMP precipitates for the inhibition of scale formation in porous media. *Langmuir* **1997**, 13 (6), 1791-1798.
- 39 Knepper, T. P. Synthetic chelating agents and compounds exhibiting complexing properties in the aquatic environment. *TrAC Trends in Analytical Chemistry* **2003**, 22 (10), 708-724.
- 40 Yu, W.; Song, D.; Li, A.; Yang, H. Control of gypsum-dominated scaling in reverse osmosis system using carboxymethyl cellulose. *Journal of Membrane Science* **2019**, 577, 20-30.
- 41 Peters, E. M.; Chivavava, J.; Rodriguez-Pascual, M.; Lewis, A. E. Effect of a Phosphonate Antiscalant during Eutectic Freeze Crystallization of a Sodium Sulfate Aqueous Stream. *Industrial & Engineering Chemistry Research* **2016**, 55 (35), 9378- 9386.
- 42 Rosenberg, Y. O.; Reznik, I. J.; Zmora-Nahum, S.; Ganor, J. The effect of pH on the formation of a gypsum scale in the presence of a phosphonate antiscalant. *Desalination* **2012**, *284*, 207-220.
- 43 Greenlee, L. F.; Testa, F.; Lawler, D. F.; Freeman, B. D.; Moulin, P. The effect of antiscalant addition on calcium carbonate precipitation for a simplified synthetic brackish water reverse osmosis concentrate. *Water research* **2010**, 44 (9), 2957-2969.
- 44 Shih, W. Y.; Albrecht, K.; Glater, J.; Cohen, Y. A dual-probe approach for evaluation of gypsum crystallization in response to antiscalant treatment. *Desalination* **2004**, 169 (3), 213-221.
- 45 Ruiz-GarcÌa, A.; Feo-Garcia, J. Antiscalant cost and maximum water recovery in reverse osmosis for different inorganic composition of groundwater. *Desalination and Water Treatment* **2017**, 73, 46-53.
- 46 Duan, W.; Oota, H.; Sawada, K. Stability and structure of ethylenedinitrilopoly (methylphosphonate) complexes of the alkaline-earth metal ions in aqueous solution. *Journal of the Chemical Society, Dalton Transactions* **1999**, (17), 3075-3080.
- 47 Deluchat, V.; Bollinger, J. C.; Serpaud, B.; Caullet, C. Divalent cations speciation with three phosphonate ligands in the pH-range of natural waters. *Talanta* **1997**, 44 (5), 897-907.
- 48 Popov, K.; Rönkkömäki, H.; Lajunen, L.H. Critical evaluation of stability constants of phosphonic acids (IUPAC technical report). *Pure and applied chemistry* **2001**, 73 (10), 1641-1677.
- 49 Wang, F.; Davis, T. E.; Tarabara, V. V. Crystallization of calcium sulfate dihydrate in the presence of colloidal silica. *Industrial & Engineering Chemistry Research* **2010**, *49* (22), 11344-11350.
- 50 Söhnel, O.; Mullin, J.W. Interpretation of crystallization induction periods. *Journal of colloid and interface science* **1988**, 123 (1), 43-50.
- 51 Greenberg, G.; Hasson, D.; Semiat, R. Limits of RO recovery imposed by calcium phosphate precipitation. *Desalination* **2005**, 183 (1-3), 273-288.
- 52 Malki, M.; Abbas, V. Relationship between phosphate scales and silica fouling in wastewater RO membrane systems. *IDA Journal of Desalination and Water Reuse* **2013**, 5 (1), 15-24.
- 53 Ning, R. Y.; Troyer, T. L. Colloidal fouling of RO membranes following MF/UF in the reclamation of municipal wastewater. *Desalination* **2007**, 208 (1-3), 232-237.
- 54 Rathinam, K.; Oren, Y.; Petry, W.; Schwahn, D.; Kasher, R. Calcium phosphate scaling during wastewater desalination on oligoamide surfaces mimicking reverse osmosis and nanofiltration membranes. *Water research* **2018**, 128, 217-225.
- 55 Mitrouli, S. T.; Kostoglou, M.; Karabelas, A. J. Calcium carbonate scaling of desalination membranes: Assessment of scaling parameters from dead-end filtration experiments. *Journal of Membrane Science* **2016**, 510, 293-305.
- 56 Ray, J. R.; Wong, W.; Jun, Y. S. Antiscaling efficacy of $CaCO₃$ and $CaSO₄$ on polyethylene glycol (PEG)-modified reverse osmosis membranes in the presence of humic acid: interplay of membrane surface properties and water chemistry. *Physical Chemistry Chemical Physics* **2017**, 19(7), 5647-5657.
- 57 Hamdona, S. K.; Al Hadad, O. A. Influence of additives on the precipitation of gypsum in sodium chloride solutions. *Desalination* **2008**, 228 (1-3), 277-286.
- 58 Zhao, J.; Wang, M.; Lababidi, H.M.; Al-Adwani, H.; Gleason, K.K. A review of heterogeneous nucleation of calcium carbonate and control strategies for scale formation in multi-stage flash (MSF) desalination plants. *Desalination* **2018**, 442, 75- 88.
- 59 Jurenka, R. A.; Chapman-Wilbert, M. Maricopa Ground Water Treatment Study: Water Treatment Technology Program Report No. 15. US Department of the Interior, Bureau of Reclamation, Denver, CO. **1996**.
- 60 Visual MINTEQ ver. 3.1 (released 2014) J. P. Gustafsson
- 61 Benjamin, M. M. Water chemistry. Waveland Press **2014**.
- 62 Menten, L.; Michaelis, M. I. Die kinetik der invertinwirkung. *Biochem Z* **1913**, *49*, 333-369.
- 63 American Public Health Association, American Water Works Association, Water Pollution Control Federation and Water Environment Federation, *Standard methods*

for the examination of water and wastewater **1915**. American Public Health Association.

- 64 Rahardianto, A.; McCool, B. C.; Cohen, Y. Reverse osmosis desalting of inland brackish water of high gypsum scaling propensity: kinetics and mitigation of membrane mineral scaling. *Environmental science & technology* **2008**, 42 (12), 4292- 4297.
- 65 Zeiher, E. K.; Ho, B.; Williams, K. D. Novel antiscalant dosing control. *Desalination* **2003**, 157 (1-3), 209-216.
- 66 Klepetsanis, P. G.; Koutsoukos, P. G. Kinetics of calcium sulfate formation in aqueous media: effect of organophosphorus compounds. *Journal of crystal growth* **1998**, 193 (1-2), 156-163.
- 67 Oh, H. J.; Choung, Y. K.; Lee, S.; Choi, J. S.; Hwang, T. M.; Kim, J. H. Scale formation in reverse osmosis desalination: model development. *Desalination* **2009**, 238 (1-3), 333-346.
- 68 Li, F.; Zhang, B.; Wang, H.; Wu, Y. Ethylenediamine core, octamethylenephosphonic acid terminated, PAMAM dendrimer and its use as antiscalant. *U.S. Patent Application* **2014**, 13 (943), 672.
- 69 Janusz, W.; Skwarek, E. Study of sorption processes of strontium on the synthetic hydroxyapatite. *Adsorption* **2016**, 22 (4-6), 697-706.
- 70 Harding, I. S.; Rashid, N.; Hing, K. A. Surface charge and the effect of excess calcium ions on the hydroxyapatite surface. *Biomaterials* **2005**, 26 (34), 6818-6826.
- 71 He, S.; Oddo, J. E.; Tomson, M. B. The nucleation kinetics of calcium sulfate dihydrate in NaCl solutions up to 6 m and 90 C. *Journal of Colloid and Interface Science* **1994**, 162 (2), 297-303.
- 72 Lancia, A.; Musmarra, D.; Prisciandaro, M. Measuring induction period for calcium sulfate dihydrate precipitation. *AIChE Journal* **1999**, 45 (2), 390-397.
- 73 Mahmoud, M. H. H.; Rashad, M. M.; Ibrahim, I. A.; Abdel-Aal, E. A. Crystal modification of calcium sulfate dihydrate in the presence of some surface-active agents. *Journal of colloid and interface science* **2004**, 270 (1), 99-105.
- 74 Christoffersen, J.; Christoffersen, M.R. Kinetics of spiral growth of calcite crystals and determination of the absolute rate constant. *Journal of crystal growth* **1990**, 100 $(1-2)$, 203-211.
- 75 Wu, W.; Nancollas, G. H. Determination of interfacial tension from crystallization and dissolution data: a comparison with other methods. *Advances in colloid and interface science* **1999**, 79 (2-3), 229-279.
- 76 Boistelle, R.; Lopez-Valero, I. Growth units and nucleation: the case of calcium phosphates. *Journal of crystal growth* **1990**, 102 (3), 609-617.
- 77 Becker, R. V.; Döring, W. Kinetic treatment of the formation of nuclei in oversaturated steam. *Ann Phys* **1935**, 5 (24), 719-752.
- 78 Frenkel, J. A. A general theory of heterophase fluctuations and pretransition phenomena. *The Journal of Chemical Physics* **1939**, 7 (7), 538-547.
- 79 Markov, I.V. Crystal Growth for Beginners: Fundamentals of Nucleation, Crystal Growth and Epitaxy. **2003**: World Scientific.
- 80 Myerson, A. S.; Jacovs, J.; Jacovs, J. Handbook of industrial crystallization **1993**. *Massachusetts: Butterworth-Heinemann.*
- 81 Opalko, F. J.; Adair, J. H.; Khan, S. R. Heterogeneous nucleation of calcium oxalate trihydrate in artificial urine by constant composition. *Journal of crystal growth* **1997**, 181 (4), 410-417.

