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**Thermoxidative stability and char formation mechanism for the introduction of  
CNTs and MoS<sub>2</sub> into halogen-free flame retarding TPEE**

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**Abstract**

In this paper, we give an insight to the char formation mechanism for the addition of CNTs and MoS<sub>2</sub> into halogen-free flame retarding thermoplastic poly(ether ester) elastomer (TPEE). We used the real-time Fourier transform infrared spectroscopy (FTIR) to analyze the change of the characteristic peaks of formulations during the thermoxidative process. Thermoxidative stability of the samples was investigated by thermalgravimetric analysis (TGA) under air atmosphere at a heating rate of 10 °C min<sup>-1</sup>. The catalyzation of carbon nanotubes (CNTs) during the thermoxidative process was demonstrated. The pyrolysis products for different formulations were studied by Pyrolysis/gas chromatography/mass spectroscopy (Pyrolysis/GC/MS). The variation of composition of the volatile decomposition

product ( $M_n < 100$  g/mol) was discussed. The morphology and the graphite degree of the high temperature remained residues was studied by scanning electronic morphology (SEM) and Raman Spectra, respectively. We found that the Mo element can catalyze effectively the char forming process through the cycloaddition interaction of volatile decomposition products. TPEE/P-N/CNTs/MoS<sub>2</sub> has the best stable char structure for the combination of the bone structure of CNTs and the cycloaddition reaction of the pyrolysis gas products with the low molecular weight.

**Keywords:** Carbon nanotubes; Molybdenum disulfide; flame retardant;

## 1. Introduction

Thermoplastic poly(ether ester) elastomer (TPEE) is a potential polymer material which can replace the natural and synthetic rubber.<sup>1</sup> With the combination of advantages of flexibility of rubber, the strength of plastics, and the processibility of thermoplastics, TPEE has been widely used for various applications.<sup>2</sup> The development of multifunctional TPEE with excellent performance has been a hotspot research topic. Much efforts has been done to realize this goal such as the incorporation the functional groups in the main chain of TPEE,<sup>3-6</sup> the preparation of the TPEE alloy and TPEE nanocomposites.<sup>7-9</sup> Meanwhile TPEE is easily ignited and burned with serious melt dripping behavior and the release of combustible decomposition products<sup>10</sup> which limit its application in many fields. To enhance the flame retarding performance to meet the requirement of industrial application is urgent. The formation of a compacted char during the burning process has proven to

be an effective way to enhance the fire retardancy of polymer.<sup>11-13</sup> In recent years, the incorporation of nanofillers with a high aspect ratio can enhance the flame retardancy of the polymer obviously on account for the formation of a high-quality char during the burning process.<sup>14, 15</sup>

Carbon nanotubes (CNTs) have been attracted considerable interest due to their unique structure, electronic, thermal and mechanical properties<sup>16</sup> and, thus have been used in various applications, including drug delivery<sup>17, 18</sup>, chemical sensor<sup>19, 20</sup>, electronic sensor<sup>21, 22</sup> and reinforced fillers for polymer<sup>23, 24</sup>. CNTs have been a promising candidate for enhancing the flame retardancy of polymer materials since 2002.<sup>25</sup> The published literatures showed that the introduction of CNTs into the polymer can effectively improve the thermal stability and flame retardant of composite for it can provide the barrier effect for the matrix during the heating process<sup>26-29</sup>. Further, the combination of CNTs and other nanoadditives exhibited a synergistic effect in the formation of the char at the high temperature.<sup>30-33</sup>

Meanwhile, in recent years, molybdenum disulfide ( $\text{MoS}_2$ ), a type of two-dimensional (2D) layered materials, has attracted more and more attentions from various applications such as transistors<sup>34</sup>, catalysts<sup>35</sup>, composites<sup>36, 37</sup> due to its intrinsic structure and unique performances.  $\text{MoS}_2$  was called white graphite for the similar structure like graphite. Different layers were associated by van der Waals forces.<sup>38-40</sup> Recently,  $\text{MoS}_2$  was incorporated into polymer materials to enhance the fire resistance and thermal stability.<sup>41-44</sup>

The dominated synergistic flame retarding mechanism of CNTs and  $\text{MoS}_2$  is that

the formation of the three-dimensional (3D) network structure in matrix which can provide the physical nano-barrier effect and act as framework structure during the burning process resulted in the enhancement of the thermal stability and flame resistance of the nanocomposites. Nanofillers play the physical role during the char formation process.

However, the chemical interaction of the CNTs and MoS<sub>2</sub> the char formation process has not yet been reported so far. The aim of this study was to give an insight to the thermoxidative decomposition and the char forming mechanism for the introduction of the combination of CNTs and MoS<sub>2</sub> into halogen-free flame retarding TPEE. MoS<sub>2</sub> can eliminate the negative effect of CNTs on the chemical char forming process. The new flame retarding mechanism would provide guidance to develop the next generation of a binary synergist system.

## 2. Experimental

### 2.1 Materials

TPEE (H3303) was provided by Sunplas (China). P-N flame retardant consists of diethylphosphinate (AlPi) and melamine polyphosphate (MPP) were provided by Clariant (German), the mass ratio of AlPi and MPP is 2:1. Carbon nanotubes (CNTs, with purity >95%, length: 0.5-40 μm, diameter: 10-30 nm, Ni ~ 2.4%, Fe ~ 0.4%) and Molybdenum disulfide (MoS<sub>2</sub>, AP, particle size ~3 μm, the density: 5.06 g/ml) were purchased from Shenzhen Nanotech Port Co.,LTD and Sigma-Aldich, respectively. CNTs and MoS<sub>2</sub> were used as received without any chemical treatments. Table 1 showed the composition of the different formulations. All the formulations melted in a

twin-roll mill at 190 °C for 10 minutes with the screw speed of 60 rpm. All the materials were hot-pressed under 12 MPa for 5 min at about 190 °C for the sheet of the suitable thickness and size for analysis.

**(Here Table 1)**

## **2.2 Measurements**

### **2.2.1 Dripping behavior**

Samples were measured by UL 94 (ASTM D3801, Size of the sample: 130 mm×13 mm×1.6 mm.)

### **2.2.2 Residues Analysis**

High temperature remained residues are collected from the samples after heating treatment at 800 °C for 10 min., . The morphology of the residues were observed by using SEM (S-4800, Hitachi, Japan). The degree of the graphitization was calculated by the results of Laser Raman spectroscopy (LRS) measurements. Raman spectra were recorded at room temperature on an SPEX-1403 laser Raman spectrometer with a 200 mW argon-ion laser at an excitation wavelength of 514.5 nm.

### **2.2.3 Thermoxidative stability**

Thermogravimetry analysis (TGA) was measured by using a NETZSCH STA 409 PC/PG thermogravimetry analyzer in air atmosphere with a heating rate of 10 °C min<sup>-1</sup>.

### **2.2.4 FTIR spectroscopy**

The change of the characteristic peaks during the heating process was measured by Fourier transform infrared (FTIR) spectra with a heating device. Samples filmed

on a KBr disc were heated from room temperature to 400 °C with a heating rate of 10°C min<sup>-1</sup>.

### 2.2.5 Pyrolysis/GC/MS analysis

To investigate the volatile product during the burning test, formulation 1-4 were analyzed by pyrolysis/gas chromatogram/mass spectrometry (pyrolysis/GC/MS). The samples were pyrolyzed at 600 °C. The gas thermal decomposition products were identified by GC/MS (Agilent 6890/5073B). Mass range: 18~500 amu.

## 3. Result and discussion

### 3.1 Dripping behavior

#### (Here Table 2)

The results of UL 94 tests of all the formulations were shown in Table 2. As presented in our previous research, TPEE burned with heavily melt dripping phenomenon in the UL 94 test. Meanwhile, the P-N flame retardant can't form the compacted char with enough strength to protect the matrix to prevent the heat and mass transfer.<sup>10</sup> Melt dripping behavior was still existed by simply adding the P-N flame retardant into TPEE. With the addition of 3wt% CNTs into P-N flame retarding TPEE can't get the desirable fire resistance without melt dripping behavior. However, adding the combination of CNTs and MoS<sub>2</sub> into TPEE with P-N flame retardants got the V-0 ranking. The significant difference in UL 94 test between TPEE/P-N/CNTs and TPEE/P-N/CNTs/MoS<sub>2</sub> was highlighted in the result of the dripping behavior. TPEE/P-N/CNTs presented the melt dripping behavior during the first ignition process of UL 94 tests. TPEE/P-N/CNTs/MoS<sub>2</sub> leads to the best flame retardancy in

terms of anti-dripping behavior. The reason for the different results of UL 94 test for TPEE/P-N/CNTs and TPEE/P-N/CNTs/MoS<sub>2</sub> will be discussed in the following part.

### 3.2 Thermoxidative decomposition and chain formation mechanism

#### 3.2.1 Real time FTIR

Fig.1 showed the alternation of the intensity and wavenumber of characteristic peaks of the solid phase in FTIR spectra at a heating rate of 10 °C min<sup>-1</sup> in the air atmosphere. All the attributions of wavenumbers for the typical bands were presented in Table. 3. The changes of characteristic bands of TPEE during the decomposition process were given in Fig.1 (a). The intensities of band at 2956 and 2861 cm<sup>-1</sup> (-CH<sub>2</sub>) decreased rapidly at the high temperature mainly resulted from the chain scission of the  $\alpha$ -methylene group in the soft segment which was demonstrated in our previous work<sup>10</sup>. In Fig.1 (b), the characteristic band at 3413 cm<sup>-1</sup> is attributed to the action of the intermolecular hydrogen bond of MPP. As increased with the temperature, there are no peaks at 3300~3600 cm<sup>-1</sup> resulted in the release of the non-flammable gas like ammonium. During the heating process, the metal ions interacted with the decomposition products containing carbonyl acid groups. The typical absorption bands of carboxyl (C=O) (1715 cm<sup>-1</sup>) shifted to the lower wavenumbers (1683 cm<sup>-1</sup>) for the migration of electrons for the interaction with the metal ions for the introduction of flame retardant. P-N flame retardants changed into metal polyphosphate salt formed a brittle char with the different size holes on the surface of the matrix.<sup>10</sup>

However, the characteristic band of CNTs and MoS<sub>2</sub> is hard to be observed for

their low amount addition and the method of sample preparation for the FTIR test. The changes of typical peaks for Formulation 3 were shown in Fig.1 (c). With addition of 3wt% CNTs into TPEE/P-N composites, TPEE/P-N/CNTs failed in the UL 94 tests for the melt dripping behavior. The anti-dripping performance of TPEE/P-N/CNTs was even worse than that of TPEE/P-N for the appearance of melt dripping behavior at the first ignition process of UL 94 tests. As we all know, CNTs can effectively increase the viscosity with regarding to the formation network structure.<sup>45</sup>

The only typical band at  $1675\text{ cm}^{-1}$  was attributed for the electric charge on the metal ion to the carboxyl group. There might be two points to the change of the peak. The first one is the metal cation on the surface of the CNTs and the Aluminum ion ( $\text{Al}^{3+}$ ) acts as Lewis acid sites, providing the basis for a coordinative interaction with the carbonyl group of TPEE. The introduction of CNTs can strengthen the Lewis based-acid interaction between the additives and the decomposition products. The other point is that the barrier effect can decrease the release rate of the degradation products. Therefore, the Aluminum ion ( $\text{Al}^{3+}$ ) can react with the decomposition products containing the carbonyl group completely for the barrier effect provided by the network structure of CNTs. There is another interesting zone at  $2800\sim 3000\text{ cm}^{-1}$  in the meantime. The characteristic peaks of aliphatic groups completely disappeared at the high temperature, indicating the addition of CNTs accelerated the chain scission reaction resulted from the existence of the metal ion on the surface of CNTs which was corresponded to the composition of CNTs. However, the burning process is a

vigorous chemical and physical reaction with the release of heat and volatile gases. The barrier effect provided by the introduction of CNTs can enhance the thermal stability. Meanwhile, the catalyzation of the metal ions on the surface of CNTs can accelerate the chain scission reaction. As the result of UL 94 tests, we found that the catalyzation of CNTs is the main course of the melt dripping behavior. The introduction of CNTs also can't result in the formation of the compacted stable char to prevent the melt dripping behavior. Then, we moved on Formulation 4. The alternation of characteristic bands of TPEE/P-N/CNTs/MoS<sub>2</sub> during the heating process is presented in Fig.1 (d). There are two obvious distinctive regions in the spectra comparing with TPEE/P-N/CNTs. The intensity of typical bands at 2800~3000 cm<sup>-1</sup> of the aliphatic groups at 400 °C indicating the introduction of MoS<sub>2</sub> revealed the decomposition rate of aliphatic groups of TPEE resulted from the decomposition catalyzation for the addition of CNTs. The second different region was in 1600~1750 cm<sup>-1</sup>.

As presented in the Fig.1 (c), the characteristic peak of carboxyl group shifted to 1675 cm<sup>-1</sup> completely for the interaction between the metal ions and the carboxyl acid. The special structure of TPEE/P-N/CNTs/MoS<sub>2</sub> decreases the decomposition rate during the heating process. For the better nano-barrier effect providing by 1-Dimensional CNTs and 2-Dimensional MoS<sub>2</sub> layers, which can promote the interaction between the additive and the decomposition products of TPEE, the characteristic peak of the carbonyl group should shift to the lower wavenumbers. The introduction of MoS<sub>2</sub> can promote the char formation and improving the char residue

was reported by other searchers.<sup>41, 42</sup>

The mechanism has not been demonstrated. If the Mo element might promote the char formation through the Lewis based-acid interaction (Fig.2(a), the characteristic peak of the carbonyl group should shift to the 1675  $\text{cm}^{-1}$  completely. On the contrary, there are still two typical peaks in the 1630~1750  $\text{cm}^{-1}$  zone indicating that the char formation process might be changed after the introduction of  $\text{MoS}_2$ . The double-bonded products undergo cycloaddition interaction for the catalyzation of Mo element improving additional carbonaceous char at the high temperature. The mechanism was given in Fig.2 (b). Thus, TPEE/P-N/CNTs/  $\text{MoS}_2$  has best stability corresponded the result of TG. These results attributed to the introduction  $\text{MoS}_2$ : the better nano-barrier effect for the coexistence of the CNTs and  $\text{MoS}_2$  and the  $\text{MoS}_2$  can promote char formation to avoid the catalysis of decomposition for the impurity on the surface of CNTs. The network structure reduces the release rate of the volatile gases which can provide more time for the char formation process.

### 3.2.2 Pyrolysis/GC/MS analysis

The thermal decomposition of Fomulation 1-4 in solid phase was investigated by real-time FIIR. Different kinds of product having carboxylic acid, hydroxyl end groups such as benzoic acid, tetrahydrofuran and their derivative mainly resulted from the degradation step of neat TPEE is the ester-linkage breaking reaction are released at the high temperature.<sup>10</sup>

**(Here Fig.1)**

This paper mainly focused on the change of the volatile product for the introduction

of P-N flame retardant, CNTs and MoS<sub>2</sub>. In Fig.3, the introduction of the additives didn't change the decomposition pathway of TPEE by comparing the peaks in the GC spectra. All the various volatile products for the characteristic peaks was analyzed by using Wiley's library. The identifications of the volatile products were presented in Table 4. There are two characteristic peaks (7,9) were found for the introduction of nitrogen containing flame retardant which resulted from the gas flame retarding action of P-N flame retardant. The phosphorus containing products wasn't found demonstrating that phosphorus containing flame retardant play flame retarding action in solid phase. The characteristic mass peaks (Mn<100) and relative peak area of Formulation 1-4 was presented in Table.5. The relative peak areas of low molecular weight products were decreased after the introduction of additives. The value of relative peak area of benzoic acid of TPEE/P-N/CNTs is 4.9 resulted from the Lewis-based interaction between the benzoic acid and Ni<sup>2+</sup> on the surface of the CNTs corresponding the result of FITR. The value of relative peak area of 1,3-butadiene of TPEE/P-N/CNTs/MoS<sub>2</sub> was half that of neat TPEE which indicated more 1,3-butadiene remained in the solid phase. The combination of the CNTs and MoS<sub>2</sub> effectively decreased the released of the 2,3-dihydrofuran and tetrahydrofuran resulted from the chain scission of the  $\alpha$ -methylene group in the soft segment due to the nano-barrier effect of the 3-dimensional network.

**(Here Fig.2)**

The introduction of MoS<sub>2</sub> can decrease the release of the volatile product into gas phase for the special nanostructure and the double-bonded containing product

remained in condensed phase for the catalyzation of char forming process. Therefore, TPEE/P-N/CNTs/MoS<sub>2</sub> has the best thermal stability and fire resistance.

(Here Fig.3)

(Here Table 3-5)

### 3.3 Thermoxidative performance

The thermoxidative behaviors of all the formulations were investigated by TG in the air atmosphere at a heating rate of 10 °C min<sup>-1</sup>; the results are presented in Fig.4. As is showed in the picture, all the samples decomposed into two step thermal decomposition process, which means the additives didn't change the main decomposition pathway of TPEE. The thermoxidative behaviors of TPEE and TPEE/P-N were demonstrated in our previous research<sup>10</sup>.

TPEE has no remained residues at 700 °C for the completely decomposition process. A special shoulder peak was observed at 300-350 °C which resulted from the chain scission of the  $\alpha$ -methylene group of soft segments corresponding to the result of the real-time FTIR testing. The temperature of the shoulder peak, the first maximum decomposition temperature and the second maximum temperature all shifted to higher temperature than that of TPEE. The remained residue of TPEE/P-N increased to 8.5 wt%. The decomposition products of P-N flame retardant interact with the decomposition product of TPEE which effectively decreased the release of volatile products and enhance the thermal stability and remained residues at the high temperature.

Adding 3 wt% CNTs into P-N flame retarding TPEE, the initial decomposition temperature and the maximum decomposition temperature are higher than that of

TPEE/P-N which resulted from the barrier effect of CNTs. However, the residue of Formulation 3 at the end of the TG test decreases plainly to 6.81 wt%. Meanwhile, the mass loss rate obviously increased since the introduction of CNTs. The results suggested that the metal cation on the surface of CNTs catalyze the decomposition process of TPEE during the thermoxidative heating process. While, adding 1 wt% MoS<sub>2</sub> into TPEE/P-N/CNTs, the initial decomposition and the maximum decomposition temperature was shifted to higher temperature. The remained residue of Formulation 4 increased to also twice that of Formulation 3. The most interesting thing is that the mass loss rate decreased obviously by simply adding 1 wt% MoS<sub>2</sub>. The result suggested that the combination of CNTs and MoS<sub>2</sub> can enhance the network structure to improve the thermal stability of the nanocomposites for the excellent barrier effect<sup>45</sup>.

Besides, the increase of remained residue at the high temperature was attributed to the interaction of the pyrolysis products and MoS<sub>2</sub> during the heating process.

### 3.4 Characterization of Residues

We got the residue after burning the samples in a muffle furnace at 800 °C for 10 min. We found that there is no residue remained at a high temperature for neat TPEE. The result corresponds with the results of TG. Fig.5 presents SEM images of the residues of Formulation 2-4. The residue morphology of TPEE/P-N is given in Fig.5 (a). There are a lot of holes with different size presented in the image. The inner part of the char has many porous structures which could be destroyed easily. During the burning process, the release of the volatile products would be through the pathway of

the permeable holes and flaws. These brittle char can't protect the materials from the melt dripping behavior.

The residue morphology of TPEE/P-N/CNTs was presented in Fig.5 (b). We found that there is still different sized pores existed in the image. The char layer seems to be more compacted and integrated than that of TPEE/P-N. The introduction of CNTs into the composites resulted in the formation of network. The network structure can slow down the release rate of the composites for the barrier effect at the low temperature. At the high temperature, the CNTs can act as framework structure for building compacted char. Nevertheless, there are still many small holes in the char and the catalyzation of metal ions on the surface of CNTs resulted in the melt dripping behavior so as to reach V-2 ranking in the UL94 test.

The SEM images of the remained residue of TPEE/P-N/CNTs/MoS<sub>2</sub> are given in Fig.5(c). The introduction of MoS<sub>2</sub> has a clear improvement on the quality of the residue. The compacted structure can effectively stop the melt dripping behavior for it is strong enough to protect the matrix from the burning process. The results indicated that CNTs and MoS<sub>2</sub> had a good synergistic char formation effect since the formation of better network structure provide the excellent nano-barrier effect during the burning process.<sup>41</sup> The structure can decrease the release of volatile combustible products. And The CNTs can provide the framework structure and Mo element can catalyze the char forming process resulted in the compacted and dense char layer on the surface of the matrix.

As it is known to all, Laser Raman spectroscopy has been demonstrated as an

easy way to characterize the degree of graphitization of carbonaceous structure after burning process. As presented in the Fig.6, there are two bands existed for Formulation 2-4. The first one at  $1352\text{ cm}^{-1}$  called D resulting from the amorphous carbon band, and the second one at  $1600\text{ cm}^{-1}$  called G band resulting from the graphite crystalline. The degree of graphitization of the residual char could be calculated by the ratio of accumulated intensity of the D and G bands ( $I_D/I_G$ )<sup>42</sup>.

Where  $I_D$  and  $I_G$  are the integrated intensities of the D and G bands, respectively. The residue has the lower ratio of  $I_D/I_G$  indicating the higher degree of graphitization and the better compacted char. Residue char layer with high degree of graphitization can efficiently decrease the rate of releasing volatiles products for the integrated structure during the burning process. The compacted and stable char can effectively stop the heat and mass transfer resulted in protecting the materials under the char.

The  $I_D/I_G$  ratio follows the order of TPEE/P-N/CNTs/MoS<sub>2</sub> (1.76) < TPEE/P-N/CNTs (1.81) < TPEE/P-N (2.38), Formulation 4 has the highest  $I_D/I_G$  ratio value indicating it has the most thermally stable char structure. The result corresponds with the morphology of char residue. There is not much big difference in the  $I_D/I_G$  ratio value between Formulation 3 and Formulation 4 for that the Mo element catalyze the char forming process resulted in the production of more amorphous carbon on the surface than the graphited carbon in the inner part. Adding the CNTs can enhance the graphitization of the char for the network structure has the benefit for the inner pressure which is important to the graphitization process. The combination of CNTs and MoS<sub>2</sub> can build a new network structure which can

improve the degree of the graphitization. Meanwhile, the Mo element catalyzed the char forming process. The graphited carbon filled into the pore of the network structure and large amount of amorphous carbon dispersed on the surface of the layer to effectively prevent the melt dripping behavior.

#### 4. Conclusion

In this work, the melt dripping behavior was disappeared for adding the combination of CNTs and MoS<sub>2</sub> into P-N flame retarding TPEE during the burning process. The TGA results suggested the addition of CNTs obviously decreased the weight of char residues at the high temperature. Otherwise, the introduction of 1 wt% MoS<sub>2</sub> effectively increased the char residue. The FTIR indicated that the metal ions on the surface of the CNTs can catalyze the decomposition process of TPEE while Mo element can catalyze the cycloaddition interaction of the double-bonding product which can promote additional carbonaceous char at the high temperature. SEM images and Raman spectra presented that a compacted char was formed through the introduction the combination of CNTs and MoS<sub>2</sub> into P-N flame retarding TPEE. During the burning process, the Mo element catalyzes the cycloaddition process of volatile decomposition products which formed amorphous carbon to cover on the surface of CNTs. TPEE/P-N/CNTs/MoS<sub>2</sub> can effectively build the network to decrease the decomposition rate and the addition of MoS<sub>2</sub> can eliminate the harmful effect resulted from the introduction of CNTs. CNTs and MoS<sub>2</sub> had a synergistic effect on the char forming process and anti-dripping behavior.

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**Figure Captions**

Fig.1 FTIR spectra of the solid phase in TPEE(a), TPEE/P-N(b), TPEE/P-N/CNTs(c), TPEE/P-N/CNTs/MoS<sub>2</sub>(d) at different temperatures.

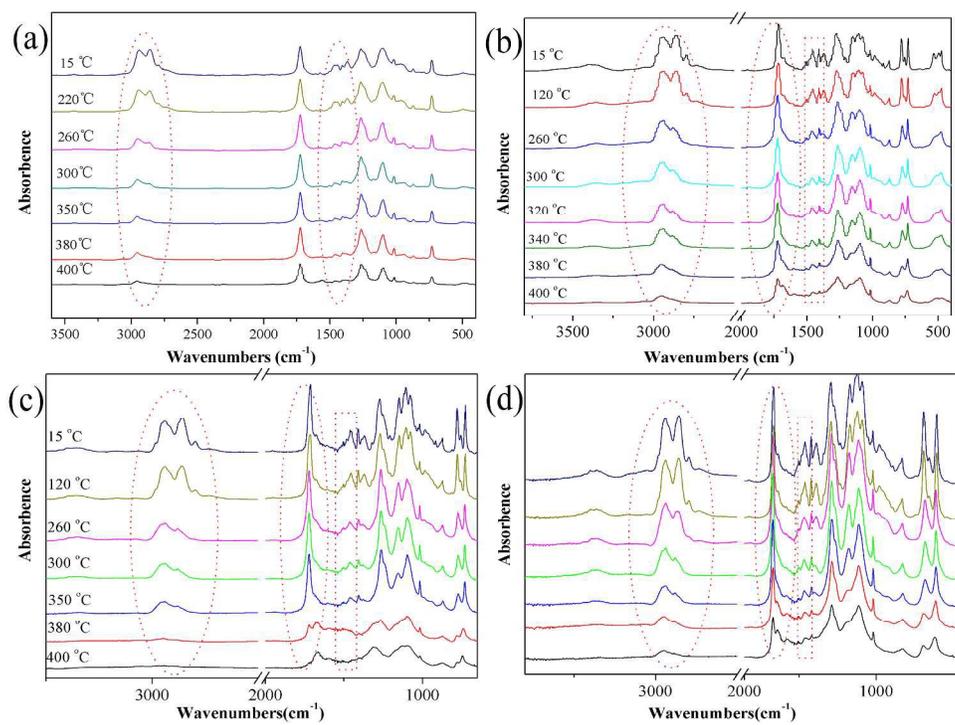
Fig.2 Mechanism of the Mo element catalyazation of char forming process

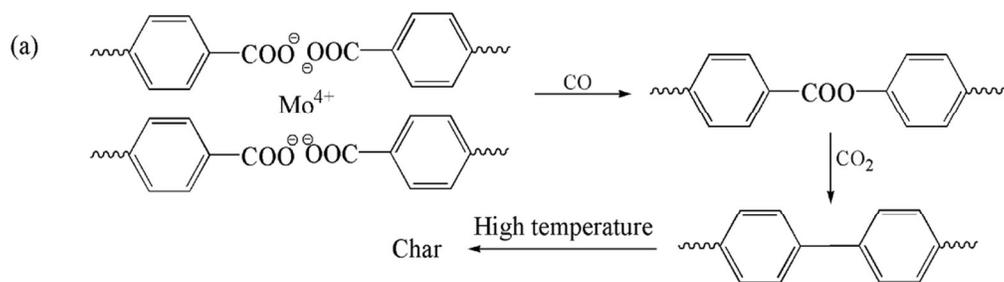
Fig.3 Gas chromatogram of the gaseous pyrolysis products of TPEE(a), TPEE/P-N(b), TPEE/P-N/CNTs(c), TPEE/P-N/CNTs/MoS<sub>2</sub>(d) obtained on heating at 600 °C.

Fig.4 Mass loss(a) and mass loss rate(b) curves of samples recorded under air atmosphere, heating rate 10 °C min<sup>-1</sup>.

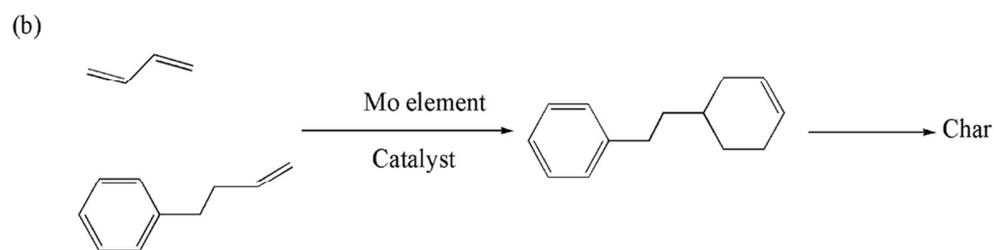
Fig.5 SEM images of the residue for TPEE/P-N(a), TPEE/P-N/CNTs(b), TPEE/P-N/CNTs/MoS<sub>2</sub>(c)

Fig.6 Raman curves of the char residues of TPEE/P-N, TPEE/P-N/CNTs, TPEE/P-N/CNTs/MoS<sub>2</sub> after calcinations at 800 °C for 10 min.



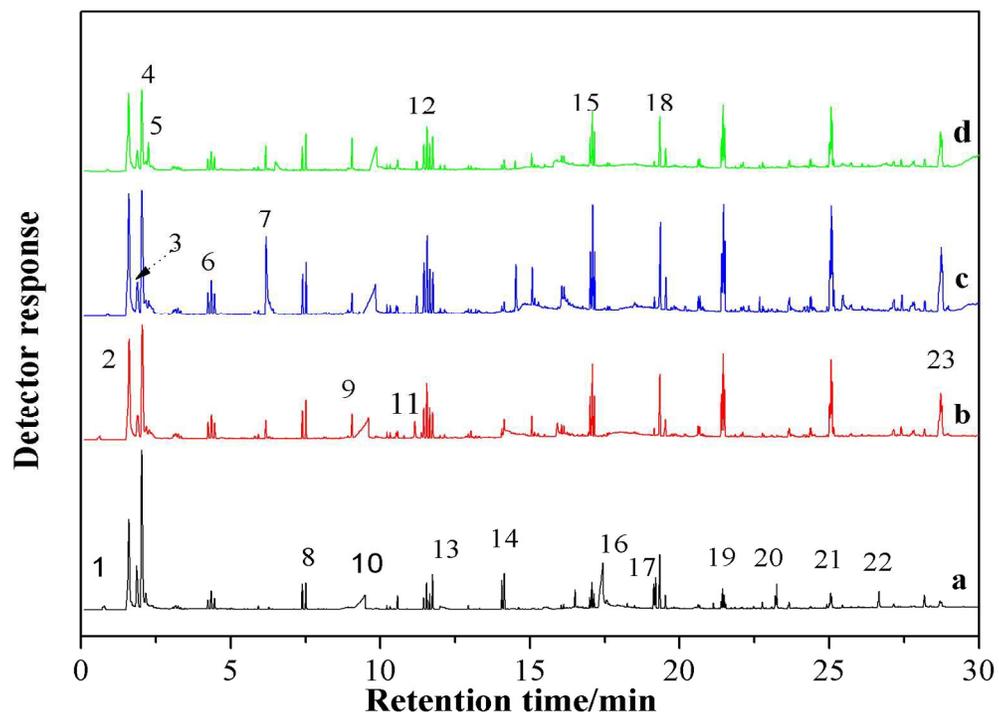


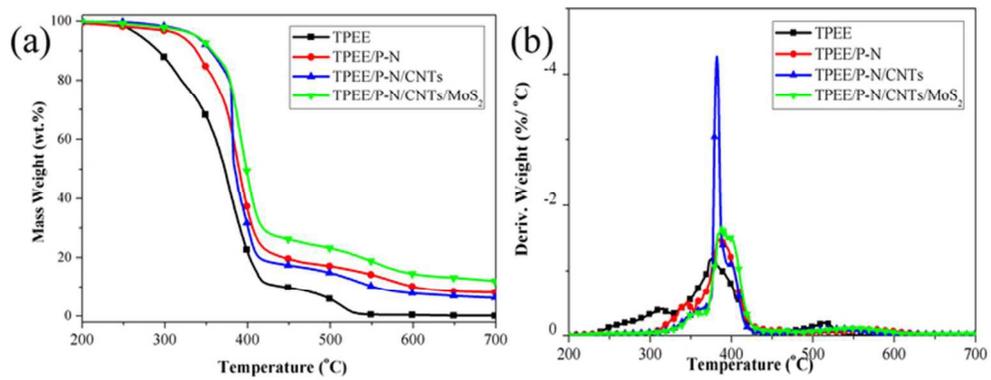
Lewis base-acid interaction



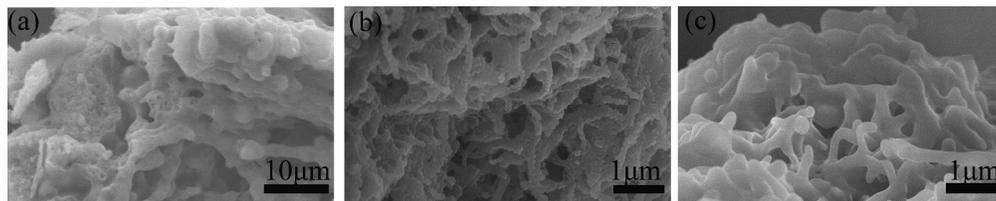
Cycloaddition interaction

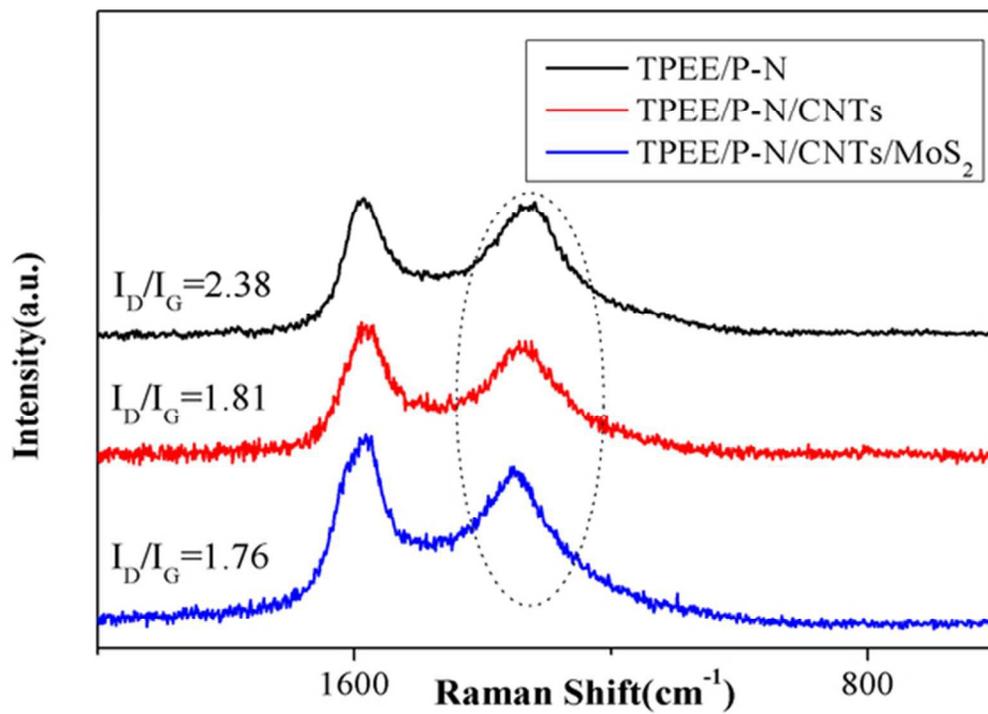
49x35mm (600 x 600 DPI)





64x25mm (300 x 300 DPI)





49x35mm (300 x 300 DPI)

Table 1. Composition of formulation in wt%

	<b>Material</b>	<b>TPEE</b>	<b>P-N</b>	<b>CNTs</b>	<b>MoS<sub>2</sub></b>
<b>1</b>	TPEE	100	–	–	–
<b>2</b>	TPEE/P-N	85	15	–	–
<b>3</b>	TPEE/P-N/CNTs	82	15	3	–
<b>4</b>	TPEE/P-N/ CNTs/MoS <sub>2</sub>	81	15	3	1

Table 2. Results of UL-94 tests of the investigated formulations

	<b>Material</b>	<b>Ranking</b>	<b>Dripping</b>
<b>1</b>	TPEE	No rating	– <sup>a</sup>
<b>2</b>	TPEE/P-N	V-2	No/yes <sup>b</sup>
<b>3</b>	TPEE/P-N/CNTs	V-2	Yes/yes
<b>4</b>	TPEE/P-N/CNTs/MoS	V-0	No/no

<sup>a</sup> the specimen burns out with dripping behavior

<sup>b</sup> No/yes corresponds to the first/second flame application.

Table 3. The attribution of wavenumbers of characteristic peaks obtained for the all formations [7,19]

Wavenumbers of Characteristic peaks ( $\text{cm}^{-1}$ )	Attribution
3413 $\text{cm}^{-1}$	-OH, MPP
2956 $\text{cm}^{-1}$ , 2861 $\text{cm}^{-1}$	-CH <sub>2</sub> , stretching vibration
1715 $\text{cm}^{-1}$	-C=O, stretching vibration
1458 $\text{cm}^{-1}$	-CH <sub>2</sub> , scission vibration
1411 $\text{cm}^{-1}$	aromatic ring
1270 $\text{cm}^{-1}$	-CO-O esters
1100 $\text{cm}^{-1}$	-CH <sub>2</sub> -O-CH <sub>2</sub> - ether
1150 $\text{cm}^{-1}$ , 1079 $\text{cm}^{-1}$ , 780 $\text{cm}^{-1}$	-P-O
1013 $\text{cm}^{-1}$	-PO <sub>4</sub> <sup>3-</sup>
727 $\text{cm}^{-1}$	-CH bending vibration of aromatic ring
531 $\text{cm}^{-1}$	O-P-O, MPP
474 $\text{cm}^{-1}$	O=P-O, AlPi

Table 4. The pyrolysis products of Formulation 1-4 at 600 °C.

No	Molecular mass (m/z)	Retention time (min)	Compound
1	44	0.785	CO <sub>2</sub>
2	54	1.602	1,3-butadiene
3	70	1.865	2,3-dihydrofuran
4	72	2.037	tetrahydro-furan
5	72	2.171	3-buten-1-ol
6	127	4.351	4-butoxy-1-butene
7	103	6.16	benzonitrile
8	100	7.514	2,3-dimethyl pentane
9	147	9.1	4-cyanobenzoic acid
10	128	9.49	benzoic acid
11	59	11.1	guanidine
12	202	11.6	1,4-butanediol diglycidyl ether
13	164	11.7	benzenebutanoic acid
14	186	14.1	heptan-2-yl butanoate
15	170	17.1	3-butoxy-2,4-dimethyl-1-pentene
16	250	17.4	2-hexan-3-yloxycarbonylbenzoic acid
17	100	19.2	cis-3-methylpent-3-ene-5-ol
18	278	19.4	dibutyl terephthalate
19	286	21.4	2,2,4-trimethyl-1,3-pentanediol diisobutyrate

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20	100	23.7	z-1-methoxy-2-pentene
21	396	25.1	bis(2-ethylhexyl) ester
22	206	26.7	3-hydroxy-2-methyl-1-phenyl-hexan-1-one
23	334	28.8	2-ethylhexyl-2-methylpropyl phthalate

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Table.5 Characteristic mass peaks ( $M_n < 100$ ) and relative peak area of Formulation 1-4.

<b>Products</b>	<b>Retention time</b>	<b>1(%)</b>	<b>2(%)</b>	<b>3(%)</b>	<b>4(%)</b>
<b>1,3-butadiene</b>	1.602	13.72	11.01	8.14	6.06
<b>2,3-dihydrofuran</b>	1.865	5.762	2.429	2.152	1.927
<b>Tetrahydro-furan</b>	2.037	17.48	9.315	6.3	6.285
<b>benzoic acid</b>	9.49	5.42	5.44	4.9	5.207