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Preparation of cellulose-graft-polylactic acid via melt copolycondensation for use in 1 2 polylactic acid based composites: synthesis, characterization and properties 3 4 Sun Hua, Feng Chen, Zheng-ying Liu, Wei Yang, Ming-bo Yang\* 5 College of Polymer Science and Engineering, State Key Laboratory of Polymer Materials Engineering, 6 Sichuan University, Chengdu 610065, Sichuan, People's Republic of China 7 8 Abstract: In order to improve the melt strength of poly(lactic acid) (PLA), microcrystalline 9 cellulose-graft-polylactic acid (MCC-g-PLA) copolymer was prepared and introduced into PLA 10 matrix. The MCC-g-PLA copolymers were synthesized by melt copolycondensation of lactic acid 11 (LA) with microcrystalline cellulose (MCC) which was pretreated to improve accessibility. The 12 MCC-g-PLA copolymers with a molar substitution (MS) of PLA in range of 1.67-5.97 were synthesized by adjusting reaction temperature, molar ratio of LA monomer to MCC and washing 13 14 times in pretreatment process. Compared with MCC, the crystalline structures of MCC-g-PLA 15 copolymers were not perfect due to the existence of PLA side chains. A glass transition 16 temperature ( $T_{a}$ ) appeared in the copolymers, which had never been observed in unmodified MCC, 17 and decreased with the increase of MS. When MS was above 4.41, the thermal degradation of 18 PLA side chains emerged. When MCC-g-PLA copolymer was introduced into PLA matrix, well 19 dispersion of MCC-g-PLA was verified with SEM results. The extension rheology results showed 20 that the melt strength of PLA can be effectively enhanced with the addition of MCC-g-PLA,

especially at low elongation rate. Meanwhile, MCC-g-PLA also improved the crystallization
 ability of PLA in non-isothermal crystallization process.

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Keywords: Microcrystalline cellulose; Lactic acid; Melt copolycondensation; Graft copolymer;
 Extensional rheological

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# 27 1. Introduction

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29 Poly(lactic acid) (PLA), which holds the potential to replace traditional petroleum based polymer 30 materials because of its excellent mechanical properties, outstanding processing performance, 31 availability from renewable agricultural products and biodegradability, has gained enormous attention <sup>1-3</sup>. It has been widely used in academic researches and industrial applications <sup>4-7</sup>, for 32 example stretch-blown bottles<sup>8</sup>, scaffold materials<sup>9-11</sup> and so on. Except for these applications, it 33 is noteworthy that PLA should be used as plastic bags and plastic film due to the biodegradability 34 taking the environment problems into consideration <sup>12</sup>. Taking agricultural plastic film as an 35 example, the residue of agricultural plastic film in the field has already become an important 36 37 negative factor that affects agricultural environment, which destroys the soil structure and harms growth of crop, due to the non-degradable plastic film<sup>13</sup>. So it is of great value to use PLA film 38 instead of traditional plastic film for environment and demanding markets <sup>12</sup>. 39

Although PLA possesses many advantages, the drawbacks of the poor viscoelastic behavior, low melt strength, the inherent brittleness, and slow crystallization rate, have limited its large-scale commercialization especially as film materials <sup>14-16</sup>. As is known, blow molding, by which a bi-axial stress is imposed on the film bubble, is the most convenient and high-performance-price-ratio method to manufacture films. From such a process, impact

properties of the film are excellent and mechanical and optical properties can be controlled <sup>17</sup>. 1 2 However, polymer melt undergoes a complex three-dimensional deformation process during blow 3 molding, so to prepare blown film steadily and successfully, high melt strength is the basic 4 requirement for materials, such as the case for branched low density polyethylene (LDPE). 5 Unfortunately, the blow molding of PLA is quite difficult owing to its poor viscoelastic behavior 6 and low melt strength. The brittleness of PLA also prevents it from being used as plastic bags and 7 plastic film. Therefore, in order to improve the processability of PLA to be used as blown films 8 and to prepare PLA films with good properties, PLA needs to be modified to improve the melt strength, viscoelastic behavior and toughness <sup>16, 18</sup>. 9 Increasing the molecular weight and introducing long branched chains have been proved to be 10

11 effective methods to improve the melt strength of PLA, which can increase chain entanglement 12 and extend melt relaxation time of PLA chains. Although high molecular weight (Mw) PLA can be synthesized by ring-opening polymerization of lactide and chain extension in laboratory studies<sup>19</sup>, 13 <sup>20</sup>, Mw of commercial PLA is still not high enough to ensure the melt strength needed for blow 14 molding. Introducing the long branched chains is another effective method, which also has a great 15 influence on the viscoelastic behavior of polymer melt, and has been proved to be able to increase 16 the melt strength and chain entanglement <sup>21-23</sup>. So, if we can synthesized copolymer with long 17 branched chains of PLA, the existence of PLA branched chains can not only increase 18 entanglement of PLA chains and melt strength of PLA, but also improve the dispersion state of 19 20 the copolymer in PLA, thus making PLA easy to process.

Cellulose is the most abundant, biodegradable, and renewable natural polymer in the earth, and holds many attractive properties, such as low cost, nontoxic, good mechanical properties and low density <sup>24, 25</sup>. If we can graft long branched chains of PLA onto cellulose, the biodegradable property of products is guaranteed, simultaneously, the applications of PLA and cellulose are both widened.

Graft copolymerization is a common way to introduce other polymers onto cellulose or cellulose 26 derivatives <sup>26-32</sup>. Unfortunately, cellulose has strong intramolecular and intermolecular 27 28 hydrogen-bonding network and high crystallinity, which make it non-thermoplastic and insoluble 29 in common solvent. Most reaction reagents penetrate only into the amorphous regions of cellulose <sup>33</sup>, while a lot of hydroxyl groups are sealed in crystalline region, then it is difficult to access to 30 31 reagents and participate in reaction. These restrict the reaction activity of cellulose. In recent years, new solvents of cellulose have been discovered, such as lithium chloride/N.N-dimethylacetamide 32 and ionic liquid <sup>34-36</sup>. They had been used as reaction media to graft polymer chains onto cellulose 33  $^{37-42}$ , which could improve the accessibility and reactivity of cellulose. But the use of solvents 34 could bring some problems, such as toxicity, complicated preparation process, or degradability. 35

How can we improve the accessibility of cellulose in non-toxic solvent ? According to previous studies <sup>43-46</sup>, treating cellulose with aqueous sodium hydroxide (NaOH) solutions had a considerable effect on the hydrogen-bonding network and crystalline structure of cellulose, in this case the crystalline structure of cellulose can transform from cellulose I to cellulose II. In this process, the alkali can destroy the hydrogen bonds and infiltrate into the crystalline region, which could be utilized to improve the accessibility and activity of cellulose. Then the solvent can be exchanged. Thus, the reaction monomer could get inside of cellulose.

Because lactide is easy to decompose, lactic acid was chosen as reaction monomer. In this work,
 firstly we improved the accessibility of cellulose by solvent exchanged method. Then, melt

copolycondensation of lactic acid with microcrystalline cellulose (MCC) was carried out to obtain
 microcrystalline cellulose-graft-polylactic acid copolymers using Tin(II) chloride dehydrate
 catalyst. Finally, the synthesized copolymer was added into PLA matrix, and the properties of PLA
 composites were studied.

- 5 **2.** Experimental
- 6

# 7 2.1. Materials

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Microcrystalline cellulose (MCC) with a degree of polymerization (DP) of ca. 200 was purchased
from ChengDu KeLong Chemical Co., Ltd. China. Lactic acid (chemical grade, solute
concentration: 85wt%), sodium hydroxide (NaOH), Tin(II) chloride dihydrate (SnCl<sub>2</sub>), toluene,
dichloromethane, dimethyl sulfoxide (DMSO) and alcohol were reagent grade and purchased from
ChengDu HaiHong Chemical Co., Ltd. China. PLA (trade name REVODE110) with a
number-average molecular weight of 4×10<sup>4</sup> g·mol<sup>-1</sup> was purchased from Zhejiang Hisun
Biomaterials Co., Ltd. China.

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# 17 2.2. Introduction of lactic acid to the inside of microcrystalline cellulose

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A dissolving procedure of MCC in alkaline solution was performed as follows <sup>47</sup>. 2.5g NaOH was 19 dissolved in 26.9g water at room temperature. 1g MCC was then added into the mixture, resulting 20 21 in a suspension of MCC in an 8.5wt% NaOH solution. The suspension was put into refrigerator 22 until it became a frozen solid state. The frozen solid was then put into room temperature to thaw, 23 and 20.6g water was added to the thawed mixture with gentle stirring, and a clean solution was 24 obtained. The dissolved cellulose was precipitated with lactic acid and filtrated, and then the 25 precipitate was washed with LA for 4 times, dried in an oven at 60 °C, and was coded as MCC-L. 26 The weight of MCC-L was 26.2g.

As a contrast, using the same process, we used water to precipitate the dissolved cellulose and
wash the precipitate, then the product was dried in an oven at 60 °C, and was coded as MCC-W.
The weight of MCC-W was 0.9g.

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# 31 2.3. Synthesis of MCC-g-PLA copolymers

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33 The undried MCC-L and lactic acid monomer (molar ratio of LA/AHG was 36/1) were put into a 34 three-neck flask equipped with a mechanical stirrer and a thermometer. The system was heated in 35 an oil bath and dehydrated under vacuum condition at 100 °C, 110 °C and 120 °C for 2h, 36 respectively. After dehydration, the temperature was heat up to initial reaction temperature, and 37 then catalyst SnCl<sub>2</sub> was added into flask. Then the absolute pressure was reduced to 500-700Pa, 38 and the melt copolycondensation was carried out by heating the reaction system at a gradient style 39 to prevent the evaporation of LA molecules in early stage (specific reaction temperature and time 40 was in the order as follows: 130 °C, 2h; 140 °C, 2h; 150 °C, 2h; 160 °C, 2h). After the reaction 41 finished, 200ml dichloromethane was poured into the flask. The resultant polymer was 42 precipitated with alcohol, and then was extracted with toluene in a Soxhlet extraction apparatus 43 for 24h to remove the byproduct (homo-PLLA) formed in reaction. The purified product was 44 soaked with dichloromethane for hours, and was filtered until the filtrate became transparent and

no precipitate appeared when a few drops of filtrate were put into alcohol, which could confirm that no byproduct remained and the purification was sufficient. Finally the product, MCC-g-PLA, was dried in an oven at 60 °C for over 24h, and was coded as MP-C2W4-T160, in which C represented the content of LA, W represented the washing times with LA in pretreatment, and T represented the maximum reaction temperature. Using the same process and adjusting reaction conditions or molar ratios of LA monomer to anhydroglucose (AHG), a series of MCC-g-PLA copolymers were prepared. The reaction conditions, molar ratios of LA monomer to MCC and

- 8 reaction results were summarized in Table 1.
- 9

#### 10 2.4 Preparation of PLA/MCC-g-PLA composites

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12 Composites of PLA with MCC-g-PLA were prepared by solution mixing. PLA and MCC-g-PLA (sample MP-C2W1-T160 was used) were dissolved separately in DMSO before mixing. The 13 14 concentrations of PLA/DMSO and MCC-g-PLA/DMSO were 3g/100ml and 3g/100ml 15 respectively. The two solutions were then mixed and the mixture was ultrasonically treated for 16 30min. Subsequently, the mixture was precipitated in alcohol and dried to a constant weight at 60 17 °C in a vacuum oven, and finally the composites PLA/MCC-g-PLA were obtained. The 18 composites were coded as PLA-MP-X, in which X represented the weight of MCC-g-PLA in 100g PLA matrix and X was 2, 3, and 4, respectively. As a contrast, composites of PLA with 19 unmodified MCC were prepared using the same process, and were coded as PLA-MCC-X, in 20 21 which X represented the weight of MCC in 100g PLA matrix, and X was 2, 3, and 4, respectively.

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# 23 2.5. Characterization

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25 2.5.1. Fourier transforms infrared (FTIR) spectrometry

The molecular structure of MCC-g-PLA by melt copolycondensation was confirmed by Fourier Transform Infrared Spectroscopy (FTIR) using a Nicolet 6700 FTIR spectrometer (Nicolet Instrument Company, USA) at the wavelength range of 650-4000 cm<sup>-1</sup> with a resolution of 4 cm<sup>-1</sup> in the transmission mode. Samples of MCC and MCC-g-PLA copolymers were respectively mixed with KBr powders and pressed into a disk for FTIR measurement.

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32 2.5.2. <sup>1</sup>H nuclear magnetic resonance (<sup>1</sup>H NMR)

The contents of grafted PLA in MCC-g-PLA copolymers were characterized by <sup>1</sup>H nuclear magnetic resonance (NMR) spectroscopy. <sup>1</sup>H NMR spectra were recorded on a Bruker AV II-600 MHz spectrometer (Bruker Company, Switzerland) in dimethyl sulfoxide- $d_6$  (DMSO- $d_6$ ) solvent with tetramethysilane (TMS) as an internal standard. A drop of trifluoroacetic acid-*d* was added into the DMSO- $d_6$  to shift active hydrogen to lower field area, in order to reduce the influence of active hydroxyl and water on the subsequent calculation. Other measuring conditions were as follows: solute concentration, 6mg/ml; temperature: ambient temperature.

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41 2.5.3. Wide-angle X-ray diffraction (WAXD)

42 The crystalline structures of MCC, MCC-L, MCC-W and MCC-g-PLA copolymers were studied

43 by WAXD. WAXD patterns of the samples were obtained with a DX-1000 diffractometer

44 (Dandong Fangyuan Instrument Company, China) with Cu Ka radiation (wave length=0.154 nm)

1 under 40 kV and 25 mA at ambient temperature. Samples were scanned over the range of 2 diffraction angle  $2\theta = 5 \sim 40^{\circ}$  with a scan speed of 3 °/min at room temperature. 3 4 2.5.4. Differential scanning calorimetry (DSC) 5 To get the glass transition temperature  $(T_{\sigma})$  of MCC-g-PLA copolymers, differential scanning 6 calorimetry (DSC) analysis was implemented on a TA Instrument DSC Q20 (TA Instruments Inc., 7 USA) under nitrogen atmosphere. Before measurement, the samples of 5~7mg were dried at 60 °C 8 for 24h, and then were heated from -25 °C to 180 °C and kept at 180 °C for 5 min to eliminate the 9 thermal history. Finally they were cooled to -25 °C and reheated to 180 °C. The scanning rate was 10 10 °C/min. The second heating curves were recorded to determine the  $T_g$  of samples. 11 The thermal analysis of PLA/MCC-g-PLA composites was also performed by DSC. The samples 12 of 5~7mg were dried at 60 °C for 24h before measurement, and were heated from 25 °C to 200 °C at a heating rate of 10°C/min and kept at 200 °C for 3min to eliminate the thermal history, then 13 14 cooled to 25 °C at a rate of 5 °C/min, and finally were reheated to 200 °C at a rate of 10 °C/min 15 under nitrogen atmosphere. The cooling and second heating curves were recorded. 16 17 2.5.5. Thermogravimetric analysis (TGA) 18 To characterize the thermal stability of MCC-g-PLA copolymers, thermogravimetric analysis 19 (TGA) was performed on a thermogravimetric analyzer (TGA Q600, TA Instruments, USA) from 20 30 to 800 °C at a heating rate of 10 °C/min under nitrogen atmosphere. 21 22 2.5.6 Scanning electron microscope (SEM) 23 The dispersion of MCC-g-PLA in PLA matrix was examined using a scanning electron 24 microscopic (SEM) (JEOL JSM-5900LV, JEOL PTE Ltd., Tokyo, Japan) at an accelerating voltage 25 of 5kV. The samples for SEM observation were compression molded into 0.1mm thickness at 180 26 °C and 10 MPa, and then were fractured manually after immersion in liquid nitrogen for 1h. 27 Before observation the fracture surfaces were coated with a thin layer of gold. 28 29 2.5.7. Extensional rheology

Uniaxial extensional rheological behavior of PLA/MCC-g-PLA composites was conducted on an
ARES extensional rheometer with the extensional viscosity fixture (EVF, TA Instruments, USA) at
158.5 °C at extensional strain rates of 0.1s<sup>-1</sup> and 0.5s<sup>-1</sup>. The testing sheets of composites were
compression molded at 180 °C and 10 MPa into 17mm ×10mm ×1mm. The test was conducted
under nitrogen atmosphere.

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#### 36 3. Results and discussion

37

38 3.1. Synthesis and characterization of MCC-g-PLA copolymers



1 2

Figure 1. WAXD spectra of MCC, MCC-W and MCC-L

WAXD spectra of MCC, MCC-W and MCC-L were shown in Figure 1. Cellulose I and cellulose
II are the most commonly used cellulose, and in WAXD spectra cellulose I shows three
characteristic diffraction peaks at around 20=14.8, 16.3 and 22.6°, whereas cellulose II shows
three peaks at around 20=12.1, 19.8 and 22.0° <sup>43</sup>. From Figure 1, MCC was a typical cellulose I,
and MCC-W was a typical cellulose II. But MCC-L was neither cellulose I nor cellulose II, only
a dispersive broad peak at 20=20.0° was observed.

9 In cellulose, the hydrogen-bonding network makes molecular chains arrange regularly and form 10 crystal. Different from cellulose I with parallel chain structure, cellulose II was comprised of an array of antiparallel chain molecules, and the unit cell was monoclinic according to Kolpak and 11 Blackwell 44. When MCC was treated in NaOH solution, alkali reached to amorphous and 12 crystalline regions of MCC, and destroyed the hydrogen bonds in the crystalline regions, then 13 MCC was dissolved in NaOH solution <sup>47</sup>. When dissolved MCC was regenerated in water, the 14 conformation of hydroxymethyl group changed <sup>43-45</sup>, and cellulose I transformed to cellulose II 15 with an antiparallel chain structure. So MCC-W was cellulose II. But for cellulose II, the 16 17 hydrogen-bonding network and structure were also very dense, and the reaction reagents were still 18 difficult to penetrate into the inside of cellulose and react with cellulose. So, simple alkali 19 treatment could not improve the accessibility of cellulose. Therefore, if we wanted to introduce 20 reaction reagents into cellulose, we had to use the stage when hydrogen bonds were destroyed.

According to the above analysis, after MCC was dissolved in NaOH solution, hydrogen bonds in cellulose were destroyed by alkali. At this time, if the reaction reagents were added into the mixture, reaction reagents may enter into the cellulose before the hydrogen bond regenerated. For MCC-L, perfect crystalline structure was not observed, indicating that the crystal structure and hydrogen-bonding network had been disrupted. This may be owing to that adding lactic acid into

the dissolved MCC solution did make lactic acid enter into cellulose, and the lactic acid remained 1 in cellulose after drying at 60 °C. The boiling point of lactic acid was about 122 °C 48, and it was 2 not easy to evaporate at 60 °C. This was also confirmed by increase in the weight of MCC-L 3 4 compared with MCC-W. The remained LA molecules formed steric hindrance to hinder the 5 configuration change of C-O bond at C6 position and the formation of hydrogen bonds, and broke 6 the regularity of hydrogen-bonding network in cellulose, thus MCC-L cannot crystallize. That is, 7 lactic acid had reached into the crystalline region of cellulose, and had a possibility of reacting 8 with hydroxyl groups both in amorphous and crystalline region, and the accessibility of cellulose 9 to lactic acid was improved.

10



CH<sub>3</sub>

+ COOH—CH—OH Melt copolycondensation

7

 $H_2O$ 

R=H or

ÒR

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Scheme 1. Illustration of the melt copolycondensation of LA with MCC. 1 The structure of the copolymers was also investigated by <sup>1</sup>H NMR. An <sup>1</sup>H NMR spectrum 2 obtained for one MCC-g-PLA copolymer (MP-C0W4-T160) was displayed in Figure 3 and the 3 4 signal peaks were assigned as follows:  $\delta = 1.32$  ppm (methyl protons of terminal lactyl);  $\delta = 1.50$ 5 ppm (methyl protons of internal lactyl);  $\delta$ =4.23 ppm (methine protons of internal lactyl); 6  $\delta$ =5.07-5.29 ppm (methine protons of terminal lactyl);  $\delta$ =3-5.4 ppm (protons of anhydroglucose). 7 The appearance of proton signals of lactyl groups in this spectrum, further confirmed that 8 MCC-g-PLA copolymers were synthesized successfully. 9 The contents of grafted PLA in cellulose-g-PLA copolymers were calculated according to <sup>1</sup>H 10 NMR spectra. As shown in Figure 3, we designated the resonance peak area derived from methine 11 protons of internal lactyls in PLA side chains as A, and the resonance peak area from methine 12 protons of terminal lactyls as B. The resonance peak area derived from methyl protons of internal lactyls was labeled as C, and the area from methyl protons of terminal lactyls was labeled as D. 13 14 The integral of all protons of anhydroglucose (AHG) unit was designated as E. Then the average 15 degree of polymerization of a PLA side chain (DP<sub>s</sub>), the degree of lactyl substitution (DS, the 16 average number of hydroxyl groups substituted for lactyls per AHG of cellulose), and the molar 17 substitution (MS, the average number of introduced lactyl units per AHG of cellulose) were estimated by equations (1)- $(3)^{38,40}$ , respectively, and the results were summarized in Table 1. 18

- 22



- 23 24
- Figure 3. <sup>1</sup>H NMR spectrum of a MCC-g-PLA copolymer (MP-C0W4-T160)

According to Table1, the amount and length of PLA side chains can be controlled by adjusting
reaction conditions and molar ratios of LA monomer to MCC, and the relationship between them
will be discussed in detail subsequently.

From Table 1, the difference of the reaction conditions of samples MP-C0W4-TX (X=130, 140, 150, 160) was reaction temperature, where the average numbers of hydroxyl groups substituted for lactyls per AHG (DS values) were almost constant, ranging from 0.60 to 0.67 with increasing reaction temperature, meaning that the accessibility of LA monomer to cellulose kept the same.

Based on previous analysis, the accessibility of cellulose was mainly affected by solvent exchange 1 2 pretreatment process. So the influence of reaction temperature on DS was small. However DPs 3 values of the four samples increased with the increasing of reaction temperature. Lactic acid 4 melting polycondensation reaction was an equilibrium reaction, producing PLA and water, so removing water was beneficial to the conversion of lactic acid into PLA 50, 51. Under the same 5 vacuum condition, high temperature could accelerate the removal of water, including free water 6 7 and that formed in reaction process. Besides, elevated temperature could also increase the thermal 8 degradation rate. Therefore, the influence of temperature on reaction was a combination of these 9 factors. In the temperature range of our experiments, the DP<sub>s</sub> value increased with the temperature 10 rising.

11

12 Table 1. The reaction conditions, molar ratios of LA to AHG and <sup>1</sup>H NMR results of MCC-g-PLA

copolymers

13

		1 2				
Sample	Washing times	LA <sup>a</sup> /AHG (mol/mol)	T(°C)	DPs	DS	MS
MP-C0W4-T130	4	0	130 <sup>b</sup>	2.79	0.60	1.67
MP-C0W4-T140	4	0	140 <sup>c</sup>	3.40	0.60	2.04
MP-C0W4-T150	4	0	150 <sup>d</sup>	3.47	0.64	2.22
MP-C0W4-T160	4	0	160	4.67	0.67	3.13
MP-C1W4-T160	4	18/1	160	5.17	0.71	3.67
MP-C2W4-T160	4	36/1	160	4.60	0.64	2.94
MP-C2W3-T160	3	36/1	160	4.70	0.88	4.14
MP-C2W2-T160	2	36/1	160	5.90	0.88	5.19
MP-C2W1-T160	1	36/1	160	6.22	0.96	5.97

<sup>a</sup> indicates the amount added in melt copolycondensation process, which does not include the LA

15 remained in MCC-L;

<sup>b</sup> specific reaction temperature and time: 120 °C, 2h; 130 °C, 6h;

<sup>c</sup> specific reaction temperature and time: 120 °C, 2h; 130 °C, 2h; 140 °C, 4h;

<sup>d</sup> specific reaction temperature and time: 130 °C, 2h; 140 °C, 2h; 150 °C, 4h

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20 Samples MP-CXW4-T160 (X=0, 1, 2) were synthesized by adjusting the molar ratios of LA 21 monomer to MCC. According to Table 1, with increasing molar ratios of LA/AHG, DS and DPs 22 values of the copolymers showed no obvious changes, indicating that increasing the content of LA 23 monomer had almost no effect on the copolymers. Theoretically, increasing the content of reactant 24 was helpful to produce the product for an equilibrium reaction. But in our work, the melt 25 copolycondensation happened in a heterogeneous condition, and the steric hindrance influenced 26 the reaction, which made the added monomer not participate in the reaction completely, so the 27 influence of monomer content on graft copolymers was not so significant.

Except for the reaction process, the pretreatment process, in which we used solvent exchanged method to change the accessibility of cellulose, also influenced the formation of copolymers. The solvent exchanged process was related to the washing step with lactic acid in the pretreatment process, then we wondered whether the washing times with lactic acid had influenced on the graft copolymers. So we synthesized samples MP-C2WX-T160 (X=1,2,3,4) through the same reaction process, only changing the washing times with lactic acid in pretreatment process.

From Table 1, we observed the dependence of DS and  $DP_s$  on washing times. Obviously, DS and 1 2  $DP_s$  increased gradually when the number of washing times reduced, indicating that the 3 consumption of lactic acid can be reduced. During the process that the dissolved cellulose was 4 regenerated and washed with lactic acid, firstly, lactic acid entered into cellulose, and combined 5 with alkali, then the alkali was brought out of cellulose, at this time hydroxyl groups surrounded 6 by alkali were freed out. These free hydroxyl groups probably formed hydrogen bonds with other 7 free hydroxyl groups, or probably were surrounded by lactic acid again. If hydroxyl group 8 contacted with lactic acid, it had the possibility of reacting with LA. But, once it formed hydrogen 9 bond with other free hydrogen group, it was hard to take part in a reaction because the hydrogen 10 bonds were difficult to be broken again. So in each washing process, some hydroxyl groups which 11 were surrounded with alkali or lactic acid were freed out again and then formed hydrogen bonds, 12 thus losing the possibility of reaction. So with the increase of washing times, DS value decreased gradually. The hydrogen bonds also limited the diffusion of lactic acid in cellulose, which affected 13 14 the amount of lactic acid that could participate in reaction, causing the decrease of  $DP_{s}$ .



Figure 4. WAXD spectra of unmodified MCC and MP-C2W1-T160

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The crystalline structures of MCC and MP-C2W1-T160 were studied by WAXD and the results were shown in Figure 4 (Spectra of other copolymers were similar to MP-C2W1-T160 and not shown here for brevity). MCC was a typical cellulose I, as mentioned above. Different from WAXD spectrum of MCC, MP-C2W1-T160 showed two broad and small peaks at 19.8° and 22.0°, which were the characteristic diffraction peaks of cellulose II. The intensity of these two peaks was very weak, and the characteristic peak at 12.1° did not appear, indicating that MCC-g-PLA

copolymers presented an imperfect crystalline structure of cellulose II. According to Kolpak and
Blackwell <sup>44</sup>, for cellulose II intramolecular hydrogen bonds (O2'-H...O6) and intermolecular
hydrogen bonds (O6-H...O3, O6-H...O2) were in the 020 plane, and intermolecular hydrogen
bond (O2-H...O2') was in 110 plane. These hydrogen bonds made the molecular chains arrange
regularly and form a perfect crystal. Reaction between LA and hydroxyl group reduced the
amount of hydroxyl groups capable of forming hydrogen bonds. On the other hand, the existence

29 of PLA side chains generated steric hindrance, also affecting the formation of hydrogen bonds and

- 1 regular arrangement of molecular chains. So the hydrogen-bonding network was weakened and
- 2 MCC-g-PLA copolymers could not form perfect crystals. These result also proved that
- 3 copolycondensation reaction occurred both in amorphous and crystalline region. Therefore we had
- 4 improved the reactivity of cellulose by this method and synthesized MCC-g-PLA successfully.
- 5 6

# 3.2. Thermal properties of MCC-g-PLA copolymers



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# Figure 5. DSC curves of (a) MCC, (b) MP-C0W4-T130, (c) MP-C0W4-T160, and (d) MP-C2W1-T160.

10 The thermal properties of MCC-g-PLA copolymers were investigated by DSC and TG 11 measurements. Figure 5 displayed the DSC curves of MCC and MCC-g-PLA copolymers (MP-C0W4-T130, MP-C0W4-T160, MP-C2W1-T160) in the second heating scan, and  $T_g$  values 12 collected from second heating curves for all samples were listed in Table 2. From Figure 5, each 13 14 curve of MCC-g-PLA copolymers exhibited a baseline gap which reflected the glass transition temperature Tg. However in the standard heating scan unmodified cellulose did not show a glass 15 transition temperature, Batzer and Kreibich 52 reported a Tg at about 230 °C for cellulose by using 16 a more sensitive method. It can be seen that Tg varied with the copolymer composition,  $T_g$  of 17 18 MP-C0W4-T130 was the highest, and Tg of MP-C2W1-T160 was the lowest. Compared to the 19 unmodified MCC, the remarkable decrease in  $T_g$  for MCC-g-PLA copolymers suggested that the 20 existence of PLA side chains broke the hydrogen-bonding network, expanded the intermolecular 21 distance, and improved the chain mobility. This was also confirmed by WAXD result. That is, the 22 grafted PLA side chains played an important role of internal plasticizer to the semi-rigid cellulose.

23 24

Table 2. Thermal properties of MCC, PLA and MCC-g-PLA copolymers

C)

MP-C1W4-T160	5.17	0.71	3.67	58.56	257.7	321.5
MP-C2W4-T160	4.60	0.64	2.94	61.94	255.1	321.9
MP-C2W3-T160	4.70	0.88	4.14	62.79	242.3	285.7, 321.6
MP-C2W2-T160	5.90	0.88	5.19	59.99	239.4	277.1, 313.2
MP-C2W1-T160	6.22	0.96	5.97	57.42	216.4	256.7, 301.7
MCC					320.1	347.6

1

2





5

-30

100

200

300

Figure 6. (a) TG and (b) DTG curves of MCC, MP-C0W4-T160, MP-C2W4-T160 and MP-C2W1-T160

400

Temperature(°C)

500

600

700

800

6 TG measurement was used to evaluate the thermal stability of copolymers and the results were

displayed in Figure 6 and Table 2. Obviously, the onset decomposition temperature ( $T_{onset}$ ) and the

8 maximum decomposition temperature  $(T_{max})$  of MCC-g-PLA copolymers were lower than those of

MCC. It was owing to that the introduction of PLA side chains on the cellulose backbone destroyed the hydrogen-bonding network and crystalline structure of MCC to some extent, resulting in the decrease of thermal stability. This was also confirmed by DSC and WAXD results. On the derivative thermogravimetry (DTG) curves, there was only one peak for copolymers when MS<4.14, demonstrating that the thermal degradation of copolymers proceeded in one step. Because the content of PLA side chains was low, the decomposition peak of PLA chains did not emerge, and the peak in DTG curve was mainly caused by decomposition of cellulose backbone. However a shoulder peak appeared near the main peak in DTC curves of MP-C1W4-T160 and MP-C2W4-T160, showing that thermal decomposition process changed gradually. When MS<sub>24.14</sub>, two derivate thermogravimetry peaks appeared, indicating that thermal degradation of these samples proceeded in two steps. This should be attributed to the different decomposition temperatures of MCC backbone and PLA side chains, and the degradation occurring at low temperature was caused by PLA side chains, and that at high temperature was caused by cellulose backbone, which was also reported in literature <sup>40</sup>. 3.3. Structure and Properties of PLA/MCC-g-PLA composites a 10µm 10µn 10µm Figure 7. SEM micrograph of (a) PLA, (b) PLA-MP-2, (c) PLA-MP-3, (d) PLA-MP-4, (e) PLA-MCC-2, (f) PLA-MCC-3, and (g) PLA-MCC-4. According to above analysis, PLA had been successfully grafted onto the MCC, and then sample

MP-C2W1-T160, which had the longest PLA side chains, was chosen and compounded into PLA 1 2 matrix to explore the influence of MCC-g-PLA copolymer on the structure and properties of PLA. Improving the dispersion of cellulose in matrix is necessary to enhance the properties of such 3 composites <sup>53</sup>, and the dispersion state of MCC-g-PLA in PLA matrix was revealed by SEM 4 micrograph shown in Figure 7. For neat PLA, the micrograph showed a smooth and flat fracture 5 surface. But it was changed to an uneven fracture surface with the addition of MCC-g-PLA, which 6 7 indicated that a signification PLA matrix deformation occurred. As is known, the compatibility of 8 PLA and cellulose was poor due to the hydrophobic nature of PLA and hydrophilic characteristic 9 of cellulose <sup>38,54</sup>. So large-size aggregates of cellulose and void appeared in the fracture surfaces of PLA/MCC composites, which was indicated with arrows in Figure 7 (e-g). However, 10 11 MCC-g-PLA dispersed well in the matrix, and there was no obvious large-size agglomeration, 12 showing that the existence of PLA side chains can greatly improve the dispersion state of 13 MCC-g-PLA in PLA matrix and inhibit the agglomeration of MCC-g-PLA and improve the 14 compatibility with PLA.



15 16

Figure 8. Variation of elongation viscosity as a function of time for PLA and PLA/MCC-g-PLA composites at 158.5 °C with elongation rates of (a) 0.1s<sup>-1</sup> and (b) 0.5s<sup>-1</sup>.

17 18

In order to investigate the influence of MCC-g-PLA on the melt strength of PLA, the extensional 19 rheological properties of PLA and PLA/MCC-g-PLA composites were characterized by the 20 extensional rheology at the extensional strain rates of  $0.1s^{-1}$  and  $0.5s^{-1}$  in steady uniaxial extension, 21 22 and the results were shown in Figure 8. It was obvious that the elongational viscosity of neat PLA 23 kept almost constant at the full time of stretching, and the strain-hardening behavior could not be observed, which was the typical characteristic of linear polymer. The elongational viscosity was 24 improved with the addition of MCC-g-PLA at low extensional strain rate (0.1s<sup>-1</sup>), and the 25 26 increment increased with increasing content of MCC-g-PLA, which was attributed to the 27 entanglement between MCC-g-PLA and PLA matrix. According to the <sup>1</sup>H NMR analysis of 28 MCC-g-PLA, the average degree of polymerization of PLA side chain was 6.22, that is the average molecular weight was 425g/mol, however the critical molecular weight for entanglement 29 of PLA was near 9000g/mol<sup>55</sup>, the length of PLA side chains in MCC-g-PLA was not long 30 enough to form strong entanglement with PLA matrix. So the entanglement should be between 31 32 MCC-g-PLA filler particles and PLA matrix, but not between the PLA side chain and PLA matrix. However, at high extensional strain rate  $(0.5s^{-1})$ , when the content of filler was low (sample 33 PLA-MP-2 and PLA-MP-3), the elongational viscosity could not be improved and was 34 35 approximately equal to that of neat PLA; only PLA-MP-4 showed higher elongational viscosity

than neat PLA. According to the SEM results, MCC-g-PLA was well dispersed in the matrix, so 1 2 the higher the content of MCC-g-PLA, the more the entanglement in the composites. For 3 PLA-MP-2, due to the low entanglement, the elongational viscosity was almost equal to neat PLA 4 even at low extensional strain rate. For PLA-MP-3, the entanglement was increased, so the 5 elongational viscosity increased at low extensional strain rate. But at high extensional strain rate, 6 the elongational viscosity decreased because of disentanglement and was approximately equal to 7 neat PLA indicating hardly any entanglement between filler and matrix. For PLA-MP-4, the 8 elongational viscosity decreased with the increase of extensional strain rate, but was still higher 9 than neat PLA, showing that there was entanglement remained in spite of the existence of

10 disentanglement.



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12 13

Figure 9. DSC thermograms of pure PLA and PLA/MCC-g-PLA composites (a) for the first cooling process, (b) for the second heating process.

14 The effects of MCC-g-PLA on the non-isothermal crystallization and melting behaviors of PLA 15 matrix were also investigated by DSC. Cooling curves of different samples were shown in Figure 16 9(a). For pure PLA, there was no exothermic peak representing the crystallization of PLA in the 17 cooling curve due to the relatively rigid molecular chain and slow crystallization rate. However, an exothermic peak emerged when MCC-g-PLA was introduced, and the peak became stronger 18 19 with increasing content of MCC-g-PLA, except for sample PLA-MP-4. In the second heating process (Figure 9(b)), there was no cold crystallization peak, which was also observed in literature 20 <sup>56, 57</sup>, and melting peak for pure PLA. For PLA/MCC-g-PLA composites, we observed the 21 appearance of cold crystallization peak, and the cold crystallization temperature ( $T_{CC}$ ) shifted to 22 23 the lower temperature with increasing content of MCC-g-PLA, and returned to higher temperature 24 for PLA-MP-4. These results indicated that the addition of MCC-g-PLA acted as nucleation agent 25 and promoted the crystallization ability of PLA. At first, the nucleation ability of MCC-g-PLA was 26 enhanced with the increasing content of nucleation agent, thus making crystallization peak 27 become stronger and T<sub>CC</sub> shift to lower temperature. Then the content of MCC-g-PLA increased 28 further, the entanglement between PLA and MCC-g-PLA also increased, resulting in the hindered 29 mobility of PLA molecular chains. This was in agreement with the extensional rheology test. In 30 addition, the shape of melting peak also changed with the content of MCC-g-PLA. As shown in Figure 9 (b), there were double melting peaks in the second heating curves of PLA/MCC-g-PLA 31 composites, which was attributed to the melt/recrystallization behavior of PLA 58, 59. The melting 32 peak at lower temperature was caused by the melting of imperfect crystals and the melting peak at 33 34 higher temperature was caused by the melting of the relatively perfect crystal and recrystallized

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1 crystals. Taking PLA-MP-3 as an example, the crystallization ability was the strongest, and the

amount of relatively perfect crystal formed in crystallization process was more, so the higher
 temperature melting peak was intensified.

4

#### 5 4. Conclusions

6

7 A series of cellulose derivatives MCC-g-PLA copolymers with MS of PLA in a range of 1.67-5.97 8 were synthesized by melt copolycondensation of lactic acid with microcrystalline cellulose using 9 SnCl<sub>2</sub> as catalyst. The factors of reaction temperature and washing times in pretreatment process 10 had a great effect on the DS and DP<sub>s</sub> value of graft copolymers. The resultant copolymers had an imperfect crystalline structure of cellulose II due to the PLA side chains, which was comfirmed 11 12 by WAXD measurements. All MCC-g-PLA copolymers exhibited a single Tg in second heating 13 thermograms in DSC, and  $T_g$  varied from 77.50 °C to 57.77 °C in relation to the MS of PLA, 14 indicating that the existence of PLA side chains had played an important role as internal 15 plasticization. The thermal stability of MCC-g-PLA copolymer was lower than that of MCC, due 16 to the weakened hydrogen-bonding network and crystallinity. When  $MS \ge 4.14$ , the thermal 17 degradation of copolymers proceeded in two steps instead of one step, and the thermal 18 decomposition behavior of PLA side chains appeared.

19 MCC-g-PLA copolymer can be well dispersed in PLA matrix, and the melt strength of PLA can be 20 improved by the addition of MCC-g-PLA at low extensional strain rate, but the improvement 21 decreased at high extensional strain rate, due to the weak entanglement. MCC-g-PLA also acted as 22 nucleation agent to enhance the crystallization ability of PLA. The results in this work proved that 23 the performance of PLA can be improved by this method, but the length of PLA side chains was 24 short, if we improve its length over the critical entanglement length, the PLA side chain can also 25 form entanglement with matrix, thus making melt strength increase significantly, so the studies on 26 further improving the length of PLA side chains are now in progress.

27

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MCC-g-PLA copolymer can improve the elongational viscosity of PLA at elongation rates of  $0.1 \text{s}^{-1}$