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# Oxidative desulfurization of model fuel using ozone oxidation generated by dielectric barrier discharge plasma combined with $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$ catalysis

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## Abstract

Oxidative desulfurization (ODS) method is highly promising method for deep desulfurization. However, the oxidant used most often in ODS is hydrogen peroxide, which can decompose into water and form an oil–water biphasic system, which affects fuel quality and confer difficulty in recovering the oil phase. If a gas is used as an oxidizing agent in ODS, oil–water biphasic problems would not exist. In this study, we synthesized metal oxide  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$  as catalyst by two-solvent, impregnation, and adsorption method, produced ozone as oxidant by the dielectric barrier discharge (DBD) plasma technology, and prepared model fuel by dissolving representative sulfur compounds such as thiophene (T), benzothiophene (BT), dibenzothiophene (DBT) and 4,6-dimethyldibenzothiophene (4,6-DMDBT) in n-octane. Then, a novel room temperature catalytic oxidative desulfurization method through ozone oxidation combined with  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$  catalysis was developed. The method was suitable for the deep removal sulfur-containing compounds from model fuel. This desulfurization technology efficiently removed T, BT, DBT, and 4,6-DMDBT, and the sulfur removal of all sulfur compounds exceeded 99%.

## Keywords

Oxidative desulfurization; Model fuel; DBD plasma; Ozone;  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$

## 1. Introduction

Desulfurization from fuel oil is very important industrially. Fuel oil contains various kinds of sulfur compounds, such as thiol, sulfide, thiophene, benzothiophene, and its derivatives. Oil consumption accounted for more than 93% of total final energy consumed in the transportation sector.<sup>1</sup> Transportation fuels emit SO<sub>x</sub> when they are burned. SO<sub>x</sub> is a major source of air pollution and could damage human health,<sup>2,3</sup> SO<sub>x</sub> into the air can create acid rain, which corrodes buildings and destroys forests and crops.<sup>4-7</sup> As pollution worsens, people are becoming increasingly environmentally conscious and are paying an increasing amount of attention to the sulfur content in the oil in recent years. Governments worldwide are legislating stringent regulations to restrict sulfur concentration in transportation fuels to improve emission standards and reduce SO<sub>x</sub> emissions.<sup>8-14</sup> Europe and America have been regulating the use of “sulfur-free” diesel and gasoline fuels (≤10 ppm S) since 2009 and 2010, respectively.<sup>15, 16</sup> China had some disparities with the international convention and regulated that sulfur content in both gasoline and diesel was less than 50 ppm since 2010.<sup>17, 18</sup> Thus, lowering sulfur content and producing ultra-low sulfur fuels in China have been a difficult and challenging subject for researchers worldwide for quite some time.

Recently, compared to the conventional hydrodesulfurization (HDS), different types of non-hydrodesulfurization technologies, such as adsorptive desulfurization, extractive desulfurization, and ODS, have been significantly developed.<sup>19-21</sup> Although traditional HDS could effectively remove the majority of sulfur-containing compounds, this technique has several challenges, such as removing BT and its derivative, giving their larger steric hindrance. This difficult problem could be solved using the ODS method.<sup>22</sup> ODS technology is a process that converts organic sulfur into their related sulfone BTO and/or sulfoxide BTO<sub>2</sub> with stronger polarity than that of initial sulfur compounds and then removing it by extraction through strongly polar extractant according to the theory of “similarity and intermiscibility”.<sup>23</sup> Some different types of oxidizers were used in ODS process, including hydrogen peroxide, ozone, molecular oxygen, and

1 organic peroxide. The DBD plasma has been often used to produce fresh ozone in the presence of  
2 air or oxygen. Ozone is a very strong oxidant and easily oxidized the organic sulfur compounds.<sup>24, 25</sup>  
3 ILs are a series of strong polar compounds solely consisted of organic cations and organic or  
4 inorganic anions, so they can easier solvate and dissociate stronger polarity sulfone BTO and/or  
5 sulfoxide BTO<sub>2</sub>. Because of low vapor pressure, high thermal stability, easy to recycle, ILs received  
6 significant attraction in green chemistry as a new green solvent, and have been applied in  
7 desulfurization of fuel recently.<sup>26-28</sup>

8 Co<sub>3</sub>O<sub>4</sub> has a normal spinel structure, and is by far the most frequently used in a wide range of  
9 catalytic applications because it can be easily synthesized, as well as being chemically stable over a  
10 wide range of temperatures and highly reactive at room temperature.<sup>29, 30</sup> Many factors significantly  
11 affect catalytic activity and selectivity<sup>31</sup> of a supported catalyst in terms of dispersion of active  
12 components, the interaction between the carrier and active components, and so on. These include  
13 chemical nature, texture, and surface acidity of the support,<sup>32</sup> the composition of the metal  
14 precursor,<sup>33</sup> the preparation method<sup>34-36</sup> and the metal loading,<sup>37</sup> etc. Activated aluminum oxide  
15  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> is a porous and highly dispersed solid material with a large surface area, and its porous  
16 structure takes on an excellent adsorptive property, catalytic activity, and thermal stability.  
17 Therefore,  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> can be widely used as catalyst carrier for preparing metal/metal oxide  
18 nanoparticles.<sup>38-41</sup> Several synthetic methods for supported metal oxide catalysts are reported in the  
19 literature. The conventional procedures are based on impregnation and adsorption. Recently a novel  
20 method called a “two-solvent” technique for preparing metal oxide catalysts has attracted  
21 considerable attention.<sup>43</sup> This method is reported to allow the preparation of highly dispersed metal  
22 oxide nanoparticles.

23 In the present study, activated aluminum oxide  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> supported cobalt oxide Co<sub>3</sub>O<sub>4</sub> using  
24 Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O as the precursor with various Co-content, which were prepared by the  
25 impregnation, adsorption, and “two-solvent” technique. Then, the structures of prepared catalysts

1 were characterized using XRD, TEM and BET. The representative sulfur compounds such as T, BT,  
2 DBT, and 4,6-DMDBT were chosen to prepare the model fuel. Moreover, catalytic ODS  
3 performance of prepared catalysts were investigated using O<sub>3</sub> as oxidant combined with  
4 [BMIM]CH<sub>3</sub>COO ([BMIM]Ac) as the extractant at room temperature and pressure. A new  
5 desulfurization technology was established by O<sub>3</sub> oxidation – catalysts catalysis – IL extraction.

## 6 7 **2. Experimental**

### 8 *2.1 Material and methods*

9 T, BT, DBT, 4,6-DMDBT,  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O were purchased from Aldrich/J&K  
10 Chemical Ltd. IL, [BMIM]Ac were purchased from Lanzhou Zhongke Kaite Chemical New-tech  
11 Co., Ltd.. They were used without any further treatment. Model fuel was prepared by dissolving T  
12 (500 ppm sulfur content), BT (500 ppm sulfur content), DBT (100 or 500 ppm sulfur content) and  
13 4,6-DMDBT (100 or 200 ppm sulfur content) in n-octane to provide model fuel.

### 14 *2.2 Co<sub>3</sub>O<sub>4</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalysts preparation and characterization*

15 Supported cobalt oxide catalysts Co<sub>3</sub>O<sub>4</sub>/γ-Al<sub>2</sub>O<sub>3</sub> were prepared using the two-solvent method  
16 (TS), impregnation method (IM), and adsorption method (AD). The samples are recorded as Y-X-A,  
17 where Y represents TS or IM or AD, X represents the nominal Co-loading percentage, and A  
18 represents support γ-Al<sub>2</sub>O<sub>3</sub>. In all cases, Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O was used as the Co precursor. Detailed  
19 preparation methods have been reported elsewhere.<sup>39, 43, 44</sup> All samples were dried at 100 °C  
20 overnight, then calcined by heating in air at 2 °C·min<sup>-1</sup> and holding at 500 °C for 6 h.

21 The structural properties of the prepared catalysts were characterized using various  
22 characterization methods. The Co<sub>3</sub>O<sub>4</sub> content was measured by inductively coupled plasma-atomic  
23 emission spectrometry (ICP-AES) after digestion in HF/HNO<sub>3</sub>, prior to measurement all catalysts  
24 were digested with nitric acid and hydrofluoric acid. Wide-angle X-ray diffraction patterns were

1 obtained using a Bruker D8 Advance powder diffractometer (Bruker Company in Germany) in the  
2 scan range of  $2\theta$  between 10 and  $80^\circ$  with a monochromatic Cu  $K\alpha$  source radiation at 40 kV and  
3 40 mA. The data was collected with a step size of  $0.02^\circ$ .  $N_2$ -adsorption/desorption isotherms were  
4 determined using liquid nitrogen adsorption at approximately  $-196^\circ\text{C}$  by an ASAP 2020C surface  
5 area and porosity analyzer (Micromeritics Instrument Corporation, USA). The samples were  
6 outgassed at approximately  $150^\circ\text{C}$  for 6 h before analysis. Pore volume, specific areas, and the pore  
7 size distribution (PSD) (BJH method) were calculated using the BET equation. Transmission  
8 electron microscopy (TEM) was used to obtain detailed information on the micro-morphology of  
9 the  $\text{Co}_3\text{O}_4$ .

### 10 *2.3 Experimental apparatus of $\text{O}_3$ preparation and ODS process*

11 The schematic diagram of the experimental apparatus of  $\text{O}_3$  preparation is shown in Fig. 1. The  
12 whole setup consisted of a plasma power (CTP-2000K, Nanjing Suman electronic Co., Ltd), a DBD  
13 reactor, a mass flow controller, a variable-voltage transformer, and an oscilloscope (RIGOL  
14 DS1102E). And  $\text{O}_3$  was prepared used a wire-cylinder reactor through self-assembly.

15 The wire-cylinder reactor is a quartz glass tube 2 mm thick. A 3 mm thick steel rod attached to  
16 the AC high voltage (HV) electrode of plasma power is fixed in the axial center of reactor, and a  
17 layer of steel net 70 mm in length attached to the AC low electrode (LV) of plasma power is  
18 covered outside the reactor. The two electrodes are 4, 6 and 8 mm apart, respectively. Air is  
19 generated using an air compressor, and then introduced into the DBD reactor with a mass flow  
20 controller at a  $100\text{mL}\cdot\text{min}^{-1}$  flow rate. When the voltage applied to the two electrodes was 19.5 kV  
21 (with a frequency value of 14.3 kHz) and is higher than the breakdown voltage of air, the air is  
22 discharged by gas breakdown. Meanwhile, high-energy electrons and highly reactive oxygen-free  
23 radicals are generated in the reactor. Then, excess oxygen reacts rapidly with oxygen-free radicals  
24 to form fresh  $\text{O}_3$ . As an oxidant, the  $\text{O}_3$  product from the bottom of reactor was introduced into  
25 model oil to perform a desulfurization study. Ozone concentration was determined using

1 CJ/T3028.2–94 (the Chinese Standard). The process was conducted under normal atmospheric  
2 pressure and temperature.

### 3 *2.4 Catalytic Oxidative desulfurization procedure*

4 Fig. 1 shows that the catalytic oxidative desulfurization experiment was conducted in a 10 mL  
5 two-necked flask. At room temperature, a certain amount of model oil and  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$  catalyst  
6 was added into flask, and then the prepared  $\text{O}_3$  was fed into the mixture to oxidize sulfur  
7 compounds with a reflux condenser under magnetic stirring. After oxidation for a definite time, a  
8 certain quantity of IL [BMIM]Ac was used for an extraction experiment under a magnetic stirrer at  
9 room temperature. According to the desired extraction time, the supernatant oil phase was  
10 periodically taken after thorough standing, and the sulfur content was analyzed by microcoulometry  
11 (WK-2D, Jiangsu Jiangfen Electroanalytical Instrument Co., Ltd., China).

## 12 **3. Results and Discussion**

### 13 *3.1 Characterization of $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$ catalysts*

14 The  $\text{Co}_3\text{O}_4$  content of the prepared catalysts are summarized in Table 1. The  $\text{Co}_3\text{O}_4$  content  
15 differed from preparation methods to preparation methods. The actual  $\text{Co}_3\text{O}_4$  contents of IM-5%-A  
16 and TS-5%-A were closer to the nominal loading. However, the catalyst AD-5%-A showed lower  
17  $\text{Co}_3\text{O}_4$  content due to weak interactions between the  $\gamma\text{-Al}_2\text{O}_3$  support and the cobalt precursor. The  
18 actual loading amount of  $\text{Co}_3\text{O}_4$  in catalyst IM-5%-A before and after ODS had almost equal weight,  
19 demonstrating the superior stability of the  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$  catalyst.

20 Fig. 2 shows the wide-angle XRD patterns of  $\gamma\text{-Al}_2\text{O}_3$  supporter,  $\text{Co}_3\text{O}_4$  and  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$   
21 catalysts prepared through equal volume impregnation at various Co-loadings. The results showed  
22 that all Co-loading materials had the same crystal structures, and the main diffraction peaks  
23 matched exactly with the standard card of  $\text{Co}_3\text{O}_4$  (JCPDS 78-1970) with almost the same peak  
24 resolution. Thus, the prepared samples exhibited a pure  $\text{Co}_3\text{O}_4$  crystalline phase. When the loading

1 amount of  $\text{Co}_3\text{O}_4$  was 2.5% (mass percentage), the spinel structure of  $\text{Co}_3\text{O}_4$  was obvious. The  
2 intensity of the diffraction peak of  $\gamma\text{-Al}_2\text{O}_3$  decreased and the peak width broadened after  
3 Co-loading, which could be attributed to superposition of the characteristic peak of  $\gamma\text{-Al}_2\text{O}_3$  and  
4  $\text{Co}_3\text{O}_4$ , such as  $2\theta = 66^\circ$ . Moreover, the intensity of the diffraction peak of  $\text{Co}_3\text{O}_4$  sharpened, which  
5 could be attributed to reduction in the extent of the  $\gamma\text{-Al}_2\text{O}_3$ , such as  $2\theta = 36.978^\circ$ .  $\text{Co}_3\text{O}_4$  had a  
6 highly preferred orientation to the (311) face.

7 Fig. 3 gives the XRD patterns of  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$  catalysts prepared through different methods  
8 at 5 wt% Co-loading. Some characteristic peaks of  $\text{Co}_3\text{O}_4$  in the TS-5%-A and AD-5%-A catalysts  
9 were not obvious compared with  $\text{Co}_3\text{O}_4$  in IM-5%-A; both catalysts had two weak peaks at  $2\theta =$   
10  $31.38^\circ$  and  $2\theta = 59.58^\circ$ . Moreover, some essential characteristic peaks were not detected. Which  
11 could be attributed to the following reasons: (1) Base on the TEM image, the active components  
12  $\text{Co}_3\text{O}_4$  prepared using TS was dispersed in the channels of the mesoporous  $\gamma\text{-Al}_2\text{O}_3$ ; and (2) the  
13 actual loading amount of active components  $\text{Co}_3\text{O}_4$  prepared by AD was less than that by TS and  
14 IM according to Table 1.

15 The textural parameters of  $\gamma\text{-Al}_2\text{O}_3$  and all the Co-composites synthesized by IM, including  
16 BET surface area, total pore volume and average pore size, are summarized in Table 1. Compared  
17 with pure  $\gamma\text{-Al}_2\text{O}_3$ , the surface area of all the Co-composites showed a significant decreasing trend  
18 as  $\text{Co}_3\text{O}_4$  loading increased. When  $\text{Co}_3\text{O}_4$  loading was only 2.5 wt%, the surface area declined very  
19 slightly (from  $182.0 \text{ m}^2/\text{g}$  to  $178.4 \text{ m}^2/\text{g}$ ); but when  $\text{Co}_3\text{O}_4$  loading increased to 15 wt%, the surface  
20 area dropped to  $106.24 \text{ m}^2/\text{g}$  rapidly. The active ingredient  $\text{Co}_3\text{O}_4$  deposited on the surface of the  
21 supporter is the major reason for the falling surface. The average pore size of all the Co-composites  
22 slightly decreased as  $\text{Co}_3\text{O}_4$  loading increased, which indicates that the active components of  $\text{Co}_3\text{O}_4$   
23 were well dispersed in the channels and on the surfaces of the carrier.

24 Fig. 4 shows the  $\text{N}_2$  adsorption-desorption isotherms of the  $\gamma\text{-Al}_2\text{O}_3$  and all the Co-composites  
25 prepared using different methods. All the samples showed type IV isotherms with H3-type

1 hysteresis loops according to the IUPAC classification, which is typical for mesoporous materials.  
2 Fig. 4 shows that all the samples presented isotherms with identical shapes to that of  $\gamma$ - $\text{Al}_2\text{O}_3$  after  
3  $\text{Co}_3\text{O}_4$  was loaded, which is indicative of the preservation of the mesoporous structure for relatively  
4 low Co-loadings. However, the volume of adsorbed  $\text{N}_2$  decreased as Co-loading increased.  
5 Moreover the capillary condensation region shifted to a lower relative pressure compared to pure  
6  $\gamma$ - $\text{Al}_2\text{O}_3$ . These changes, together with reduction in the surface areas and pore volume of the  
7 Co-composites, were ascribed to the blockage of channel by cobalt species (Table 1).

8 The pore size distribution of  $\gamma$ - $\text{Al}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$  and Co-composites are shown in Fig. 5. The  
9 results show that  $\text{Co}_3\text{O}_4$  can be regarded as a solid with little pore. The pore structure of AD-5%-A  
10 had no significant differences compared to pure  $\gamma$ - $\text{Al}_2\text{O}_3$ , but the center of the peak slightly shifted  
11 to a lower pore width for TS-5%-A and IM-5%-A. Thus, the average pore size decreased after the  
12 formation of  $\text{Co}_3\text{O}_4$  inside the pores of the carrier. This result demonstrated that  $\text{Co}_3\text{O}_4$  was easier to  
13 deposit on the surface of the support prepared by TS and IM. From the pore volume and surface  
14 area,  $\text{Co}_3\text{O}_4$  was easier to enter into the pores of the support prepared using TS. In comparison to  
15 IM-5%-A, the centre of the peak of the sample IM-15%-A shifted to a lower pore width, illustrated  
16 that more  $\text{Co}_3\text{O}_4$  particles blocked the pores of the support.

17 Fig. 6 provides the TEM images of the catalysts IM-5%-A, TS-5%-A and the support  $\gamma$ - $\text{Al}_2\text{O}_3$ .  
18 For the catalysts IM-5%-A and TS-5%-A, the ordered hexagonal channels in the mesoporous  $\text{Al}_2\text{O}_3$   
19 were preserved after cobalt loading. This result was consistent with that obtained by XRD. Large  
20 patches were clearly observed on IM-5%-A catalyst, showing that  $\text{Co}_3\text{O}_4$  aggregation occurred. The  
21 patches diameter was larger than channels diameter of the support  $\gamma$ - $\text{Al}_2\text{O}_3$ . No aggregated particles  
22 were found on TS-5%-A, showing that  $\text{Co}_3\text{O}_4$  was highly dispersed in the channels of the  
23 mesoporous  $\gamma$ - $\text{Al}_2\text{O}_3$ .

### 24 3.2 Effect of the electrode distance between the two electrodes on ozone concentration

25 When discharge voltage is 19.5 kV, and the air flow rate is  $100 \text{ mL}\cdot\text{min}^{-1}$ , The ozone

1 generation rate histogram is shown in Fig. 7, in which the electrode distance between the two  
2 electrodes is 4mm, 6 mm and 8 mm apart, respectively. It can be seen from Fig. 7 that the electrode  
3 distance had a tremendous influence on ozone concentration. When the electrode distance between  
4 the two electrodes was shortened twice, the ozone concentration increased approximately 5 times.  
5 When the electrode distance was 8 mm, the ozone concentration was  $1.31 \text{ mg}\cdot\text{L}^{-1}$ . When the  
6 electrode distance was 4 mm, the ozone concentration was  $5.48 \text{ mg}\cdot\text{L}^{-1}$ . With the decreasing  
7 discharge distance, the amount of ozone increased because the probability of efficient collision was  
8 enhanced between the high-energy electrons generated by DBD and oxygen in a more narrow  
9 discharge space for the formation of more ozone. Later research found that the amount of ozone met  
10 the requirements of oxidative desulfurization experiments with a discharge distance of 8 mm. Thus,  
11 an electrode distance of 8 mm was selected for use in the late-stage ODS study.

### 12 3.3 Catalytic ODS test of $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$

#### 13 3.3.1 Desulfurization comparisons at different desulfurization system of $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$

14 In the hydrodesulfurization process, generally DBT was chosen as the representative sulfur  
15 compound in fuels. Therefore, model fuel with a sulfur content of 100 ppm that contains DBT were  
16 conducted to study the following catalytic ODS experiments. To evaluate the catalytic activities of  
17  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$  catalyst in different desulfurization systems (Table 2), we selected 0.05 g  
18 IM-10%-A as a catalyst and reacted for 30 min to investigate the desulfurization of different  
19 catalytic systems. Furthermore, the result was compared with the desulfurization activity of pure  $\text{O}_3$   
20 or pure  $\gamma\text{-Al}_2\text{O}_3$ . The results are listed in Table 2.

21 From the data listed in Table 2, it can be seen that IM-10%-A catalyst removed DBT with a  
22 sulfur content of 100 ppm from the model fuel entirely when  $\text{O}_3$  was used as oxidant. However,  
23 sulfur removal was only 43.3% when  $\text{O}_2$  was used as an oxidant. This result revealed that the  
24 oxidizability of  $\text{O}_2$  on DBT was far less than that of  $\text{O}_3$  used the same catalyst under identical

1 experimental conditions. In addition, if IM-10%-A or  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> was directly used for desulfurization  
2 without any oxidizing agent added, the DBT removal could reach approximately 35%. At this point,  
3 desulfurization method was turned into adsorption desulfurization. Compared to the ODS by O<sub>2</sub>,  
4 DBT removal had no significant differences, which further illustrated the weak oxidizing capacity  
5 of O<sub>2</sub> on DBT. Table 3 also shows that DBT was hardly oxidized by O<sub>3</sub> without Co<sub>3</sub>O<sub>4</sub>/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>  
6 existences.

### 7 *3.3.2 Effect of the catalyst loading amount on DBT removal*

8 The effect of the catalyst loading amount on DBT removal was investigated. The result is  
9 indicated in Fig. 8. As shown in Fig. 8, the desulfurization rate obviously increased with increasing  
10 amount of Co-loading. When DBT was oxidized for approximately 5 min, the DBT removal of  
11 IM-15-A exceeded 60%. When increased oxidative time was 20 min, the DBT removal of four  
12 different Co-loading catalysts reached over 95%, and IM-12.5-A and IM-15-A were 99.9%. When  
13 O<sub>3</sub> used to oxidize DBT for 30 min, the desulfurization rate of all Co<sub>3</sub>O<sub>4</sub>/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalysts with  
14 different supported Co<sub>3</sub>O<sub>4</sub> content reached 99.9%. From Fig. 8, the amount of Co-loading had a  
15 remarkable effect on DBT removal when oxidation time was less than 10 min. However, the  
16 amount of Co-loading had no obvious difference on DBT removal when oxidation time was more  
17 than 20 min.

### 18 *3.3.3 Desulfurization comparisons of Co<sub>3</sub>O<sub>4</sub>/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> prepared by different methods on DBT* 19 *removal*

20 At the same ODS condition, the catalytic activity of Co<sub>3</sub>O<sub>4</sub>/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> at 5% loading prepared by  
21 IM, TS, and AD was researched. The results are shown in Fig. 9. The catalytic performance of three  
22 Co<sub>3</sub>O<sub>4</sub>/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalysts rapidly increased with the extension of oxidation time and the sulfur  
23 removal all reached 99.9% at 30 min oxidization with O<sub>3</sub>. Moreover, TS-5%-A had excellent  
24 catalytic activity and a desulfurization efficiency of 95% was obtained after oxidizing for 5 min,

1 illustrated  $\text{Co}_3\text{O}_4$  particles diffused into the holes of  $\gamma\text{-Al}_2\text{O}_3$ . The result agrees with the discussion  
2 regarding pore-size distribution (Fig. 5) and TEM (Fig. 6).

### 3 *3.3.4 The influence of $\text{O}_3$ concentration on DBT removal*

4 The influence of  $\text{O}_3$  concentration on DBT removal was investigated, and the result is  
5 indicated in Fig. 10. In the preceding work of our project group,<sup>45</sup> the consistence of  $\text{O}_3$  could  
6 be adjusted by adjusting air flow rate, and increased with the decrease of the air flow rate. As shown  
7 in Fig. 10, the  $\text{O}_3$  concentration had remarkable effects on DBT removal. Only 93.8% DBT removal  
8 was reached when  $0.71 \text{ mg}\cdot\text{L}^{-1}$   $\text{O}_3$  was bubbled into the oxidation system. However, the  
9 desulfurization rate of DBT increased to 99.5% as the  $\text{O}_3$  concentration increased to  $1.19 \text{ mg}\cdot\text{L}^{-1}$ .  
10 As the  $\text{O}_3$  concentration was set to  $1.31 \text{ mg}\cdot\text{L}^{-1}$  [Air flow rate =  $100 \text{ mL}\cdot\text{min}^{-1}$ ], approximately  
11 99.9% DBT removal was reached.

### 12 *3.3.5 Desulfurization comparisons of different sulfur compounds by $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$*

13 In terms of its advantageous catalytic reaction performance, IM-15-A was selected as the most  
14 ideal for studying the effect of different substrates such as TS, BT, DBT, and 4, 6-DMDBT on ODS  
15 in the  $\text{O}_3 - \text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3 - [\text{BMIM}]\text{Ac}$  system under the same experimental conditions. Table 4  
16 exhibits that IM-15-A had excellent catalytic activity to four sulfur-containing compounds. For 500  
17 ppm T and BT, 100 DBT ppm and 4,6-DMDBT, and 200 ppm 4,6-DMDBT, the desulfurizing ratio  
18 reached to above 99.6%. However, for 500 ppm DBT, the desulfurizing ratio decreased to 93.1%.

### 19 *3.3.6 Reusability of the catalyst $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$*

20 The recyclability of the IM-15%-A catalyst was evaluated and the results are shown in Fig. 11.  
21 After the catalyst was oxidized, recovered by decantation, washed several times with methanol, and  
22 subsequently dried at  $100 \text{ }^\circ\text{C}$ . Then the fresh model oil and  $\text{O}_3$  were introduced for the next recycle  
23 under the same conditions. The data in Fig. 11 indicate that the catalyst was used up to five times

1 without significant change in its catalytic activity.

## 2 **4. Conclusions**

3 In this study, we synthesized metal oxide catalysts  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$ , and the  $\text{Co}_3\text{O}_4$  was  
4 accommodated inside the pores by the TS method. Moreover IL [BMIM]Ac was screened as an  
5 extracting agent and the model fuel was prepared using representative sulfur compounds such as T,  
6 BT, DBT, and 4,6-DMDBT in fuel oil. Then, the catalytic oxidation activities of prepared catalysts  
7 and extracting performance of screened IL for model fuel desulfurization were studied using ozone  
8 as an oxidant at room temperature and pressure. New desulfurization technology was established  
9 through  $\text{O}_3$  oxidation – catalysts catalysis – IL extraction. The results indicated that the oxidative  
10 desulfurization technology using  $\text{O}_3$  as oxidant in the presence of catalysts combined with IL  
11 extraction was very effective, and TS-5%-A had excellent catalytic activity. Moreover, the sulfur  
12 removal of T, BT, DBT, and 4,6-DMDBT all reached over 99% at ordinary temperatures and  
13 pressures, respectively. In addition, the oxidation step was the key step in the desulfurization  
14 process. Desulfurization was lower or ineffective if T, BT, DBT, or 4,6-DMDBT was not oxidized  
15 to the corresponding oxidization product. The IM-15%-A catalyst can be used repeatedly 5 times,  
16 and its catalytic activity was no significant change.

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## 22 **References**

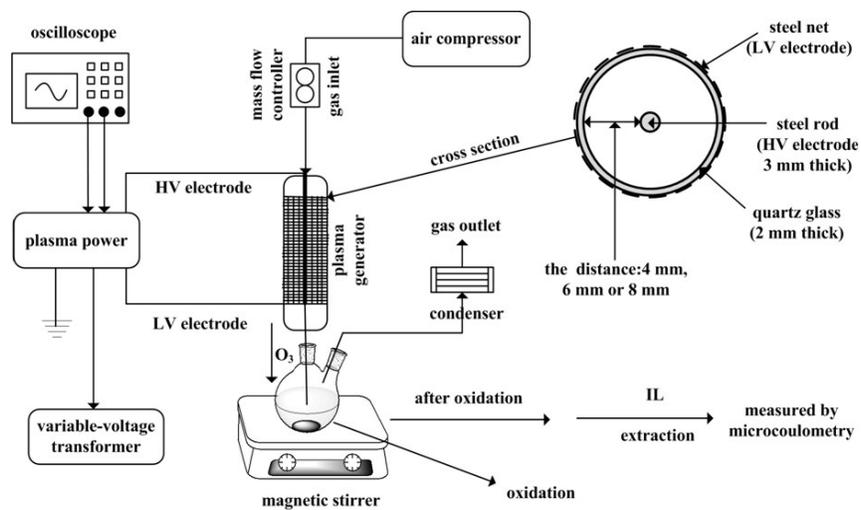
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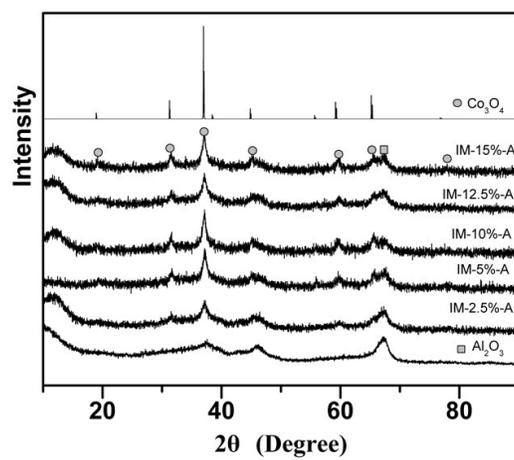
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**Figure Captions page**

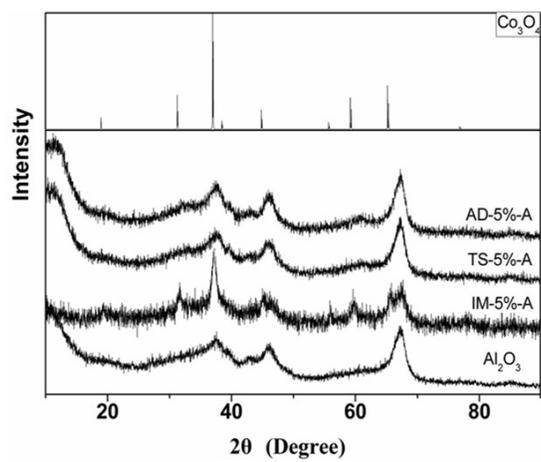
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- 2
- 3 **Fig. 1** The schematic of the experimental apparatus of O<sub>3</sub> preparation and ODS process
- 4 **Fig. 2** XRD patterns of Co<sub>3</sub>O<sub>4</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalysts by IM
- 5 **Fig. 3** XRD patterns of Co<sub>3</sub>O<sub>4</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalysts by IM, TS and AD
- 6 **Fig. 4** N<sub>2</sub> adsorption-desorption isotherms of γ-Al<sub>2</sub>O<sub>3</sub> and Co-composites
- 7 **Fig. 5** Pore size distribution of γ-Al<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub> and Co-composites
- 8 **Fig. 6** The TEM images of samples: (A) IM-5%-A; (B) TS-5%-A; (C) Al<sub>2</sub>O<sub>3</sub>
- 9 **Fig. 7** Effect of the electrode distance between the two electrodes on O<sub>3</sub> concentration
- 10 **Fig. 8** Effect of Co<sub>3</sub>O<sub>4</sub> loading on γ-Al<sub>2</sub>O<sub>3</sub> on DBT removal
- 11 **Fig. 9** Effect of preparation method of Co<sub>3</sub>O<sub>4</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalyst on DBT removal
- 12 **Fig. 10** Effect of O<sub>3</sub> concentration of DBT removal
- 13 **Fig. 11** Reusability of IM-15%-A for DBT removal
- 14
- 15 **Table 1** The actual content of Co<sub>3</sub>O<sub>4</sub> in Co<sub>3</sub>O<sub>4</sub>/γ-Al<sub>2</sub>O<sub>3</sub>
- 16 **Table 2** Surface area, average pore size and pore volume of samples
- 17 **Table 3** Desulfurization comparisons at different desulfurization system of Co<sub>3</sub>O<sub>4</sub>/γ-Al<sub>2</sub>O<sub>3</sub>
- 18 **Table 4** T, BT, DBT and DMDBT removal by Co<sub>3</sub>O<sub>4</sub>/γ-Al<sub>2</sub>O<sub>3</sub>
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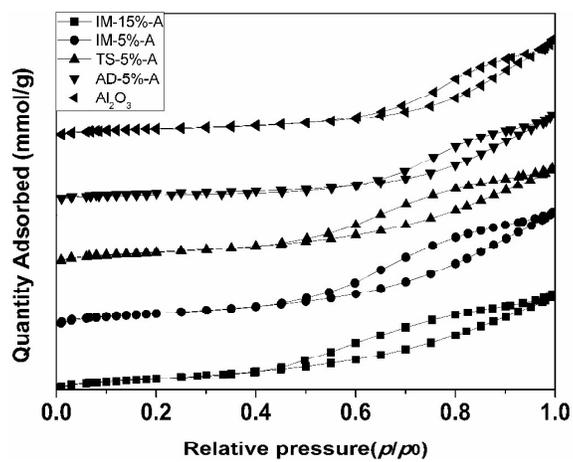
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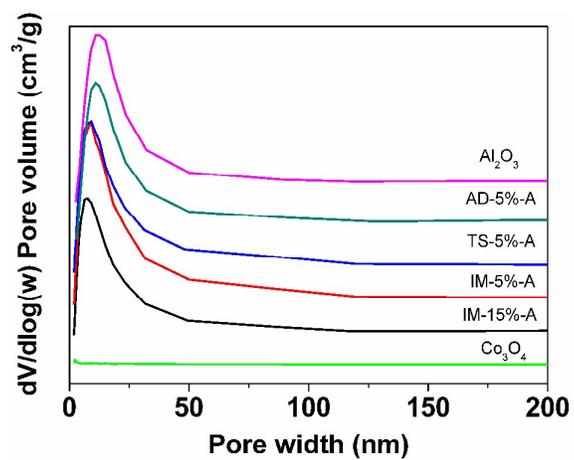
**Fig. 2** XRD patterns of  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$  catalysts by IM



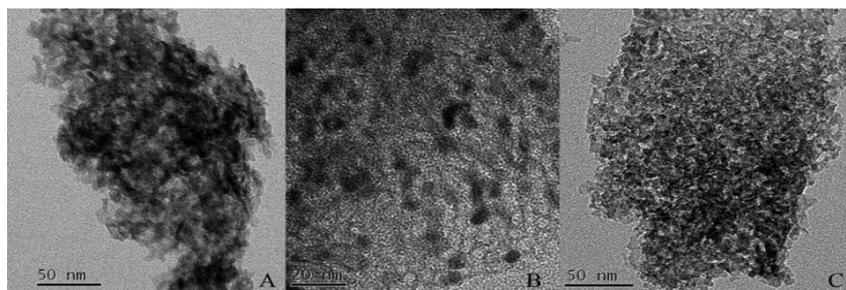
**Fig. 3** XRD patterns of Co<sub>3</sub>O<sub>4</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalysts by IM, TS and AD



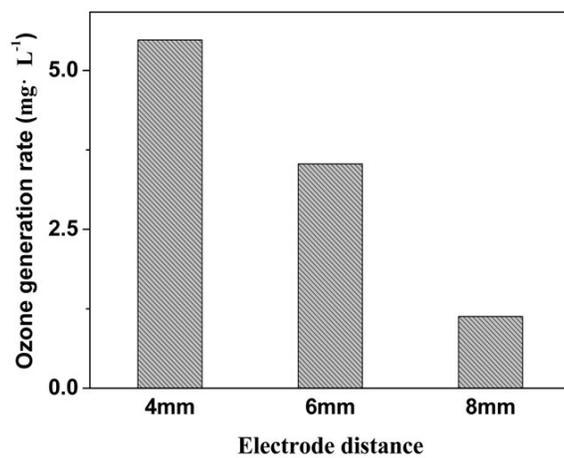
**Fig. 4** N<sub>2</sub> adsorption-desorption isotherms of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and Co-composites



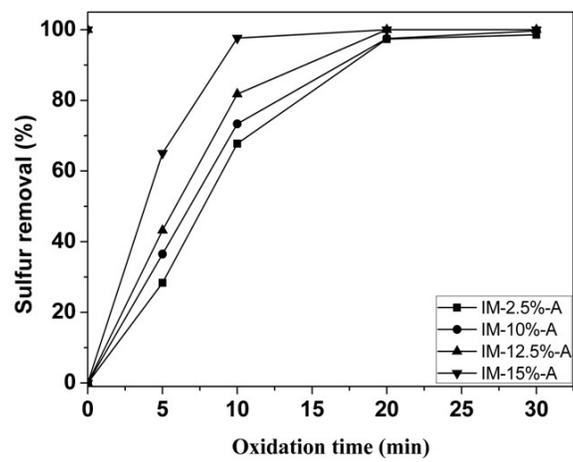
**Fig. 5** Pore size distribution of  $\gamma\text{-Al}_2\text{O}_3$ ,  $\text{Co}_3\text{O}_4$  and Co-composites



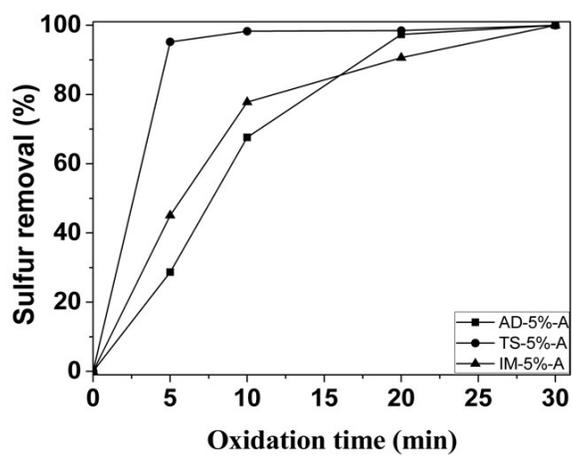
**Fig. 6.** The TEM images of samples: (A) IM-5%-A; (B) TS-5%-A; (C) Al<sub>2</sub>O<sub>3</sub>



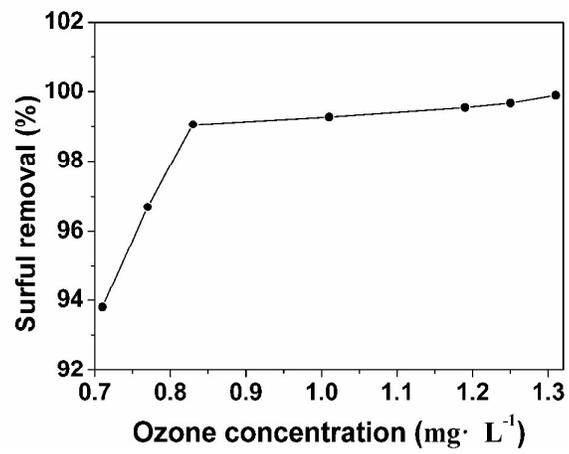
**Fig. 7** Effect of the electrode distance between the two electrodes on O<sub>3</sub> concentration



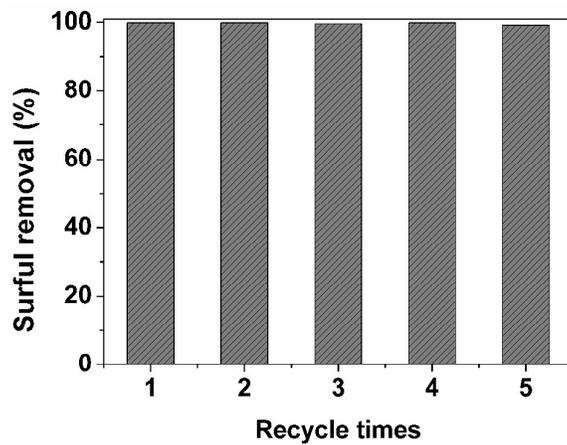
**Fig. 8** Effect of  $\text{Co}_3\text{O}_4$  loading on  $\gamma\text{-Al}_2\text{O}_3$  on DBT removal



**Fig. 9** Effect of preparation method of  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$  catalyst on DBT removal



**Fig. 10** Effect of O<sub>3</sub> concentration of DBT removal



**Fig. 11** Reusability of IM-15%-A for DBT removal

**Table 1** The actual content of  $\text{Co}_3\text{O}_4$  in  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$ 

Samples	Nominal $\text{Co}_3\text{O}_4$ content (wt%)	Actual $\text{Co}_3\text{O}_4$ content (wt%)
AD-5%-A	5	2.03
TS-5%-A	5	4.03
IM-5%-A	5	4.26
IM-5%-A (After ODS)	5	4.11

**Table 2** Surface area, average pore size and pore volume of samples

Samples	Surface area (m <sup>2</sup> /g)	Pore volume (cm <sup>3</sup> /g)	Average pore size (nm)
Al <sub>2</sub> O <sub>3</sub>	182.0	0.432	9.503
IM-2.5%-A	178.4	0.376	9.302
IM-5%-A	168.3	0.366	9.674
TS-5%-A	175.4	0.385	9.629
AD-5%-A	178.9	0.410	9.417
IM-10%-A	156.71	0.361	9.218
IM-12.5%-A	144.21	0.331	9.194
IM-15%-A	106.24	0.255	9.105

**Table 3** Desulfurization comparisons at different desulfurization system of  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$ 

	$\text{Co}_3\text{O}_4/\text{Al}_2\text{O}_3$	Sulfur-removal (%)
(1)	IM-10%-A + $\text{O}_3$	99.9
(2)	IM-10%-A + $\text{O}_2$	43.3
(3)	IM-10%-A	36.14
(4)	$\text{O}_3$	2.0
(5)	$\text{Al}_2\text{O}_3$	35.13

**Table 4** T, BT, DBT and DMDBT removal by  $\text{Co}_3\text{O}_4/\gamma\text{-Al}_2\text{O}_3$ 

Model fuel	Initial S-concentration (ppm)	Sulfur removal (%)
T	500	99.9
BT	500	99.6
DBT	100	99.9
	500	93.1
4,6-DMDBT	100	99.9
	200	99.7