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1 **Synthesis of levulinic acid-based polyol ester and its influence on**
2 **tribological behavior as potential lubricant**

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8 **Abstract**

9 Levulinic acid (LA) has been identified by the US Department of Energy
10 as a top platform chemical and regarded as one of the twelve most promising
11 molecules derived from biomass. In this study, it was used to prepare lubricant
12 base stocks by esterification with three different polyols including neopentyl
13 glycol (NPG), trimethylolpropane (TMP), and pentaerythritol (PE) in the
14 presence of sulfuric acid. The crude product was distilled to obtain target
15 product with a purity above 95%. These products of polyol ester were
16 characterized using ¹H NMR and mass spectral techniques. The lubricant
17 properties, such as kinematic viscosity, viscosity index, pour and flash points,
18 were evaluated using standard ASTM methods. Among the base stocks
19 prepared, TMP-tri-LA ester exhibited superior lubricant properties like good
20 kinematic viscosity at 40°C (87.28) and at 100°C (8.42), viscosity index (48),
21 low pour point (-25 °C), high flash point (238 °C), cloud point (-4 °C) , copper

1 strip corrosion (1a) and Volatility at 120°C (0.41%). Wear prevention
2 characteristics of this ester was tested and performed low coefficient of friction
3 and small wear scar diameters. It was found that this kind of polyol ester was
4 suitable for lubricant base stocks.

5 **Keywords:** Levulinic acid, Polyol esters, Biolubricant, Lubricant properties

6 **1. Introduction**

7 Biodegradable polyol esters, which served as biolubricant components,
8 have aroused more interest because of their excellent lubricity, biodegradability,
9 viscosity-temperature characteristics, and low volatility.¹ However, natural
10 triglycerides are thermally sensitive at high temperature. The main reason of
11 this phenomenon is the presence of hydrogen atoms on the β position of the
12 glycerol molecule backbone,² since this structural feature is prone to the partial
13 fragmentation of the molecule and the formation of unsaturated compounds.
14 The formed compounds under polymerization led to the increase of the liquid's
15 viscosity and resulted in the formation of precipitate particles.³ Thus, natural
16 triglycerides are generally not appropriate for the applications of lubricant that
17 require heat resistance. This problem could be easily solved by replacing
18 glycerol with another special polyhydric alcohol which does not contain β -
19 hydrogen atoms.^{4,5} In previous literatures, researchers used neopentyl polyols
20 such as neopentyl glycol (NPG), trimethylolpropane (TMP) and pentaerythritol
21 (PE) for this purpose.⁶⁻⁸ So far, the investigation of polyol esters biolubricant
22 preparation has been conducted using polyols with various fatty acids by

1 transesterification or esterification. Most of fatty acids reported in literature are
2 generally obtained from animal oils such as beef tallow, lard, mutton tallow as
3 well as vegetable oils, such as soybean oil, sunflower oil, rapeseed oil, castor
4 oil, olive oil, palm kernel oil and waste cooking oil.⁹⁻¹⁵ These high
5 monounsaturated oils have optimal performance as raw materials to generate
6 environment friendly lubricants with high performance. However, part of these
7 oils are edible, and their use for the production of lubricants will indirectly
8 influence the food demand. Hence, more attention is paid for the preparation of
9 non-edible oil-based polyol esters containing any unusual fatty acids.

10 Levulinic acid (LA), having five carbon atoms with carboxyl group and
11 ketone functional groups, can be easily produced from glucose, fructose, starch
12 and lignocellulosic residues.¹⁶ It has been identified by the US Department of
13 Energy as a top platform chemical and regarded as one of the twelve most
14 promising molecules derived from biomass, because it can be transformed into
15 a variety of other important compounds in the chemical industry.¹⁷⁻¹⁸ In the
16 1990s, there were some patents about the conversion of LA production from
17 lignocellulose by acid degradation at an elevated temperature and the
18 theoretical yield of LA could reach 55% (molar yield based on hexose polymer
19 content of wood feed) under the optimal condition.¹⁹⁻²⁰ Recent research
20 demonstrated that LA could be obtained from cellulose in the presence of
21 catalyst such as functionalized ionic liquids,²¹ dilute acid,²² alkaline-treated
22 zeolite,²³ and Fe/HY catalyst.²⁴ LA produced from cellulose has attracted
23 considerable attention and become one of the key steps for the biomass

1 refining.²¹ Meanwhile, the esterification of levulinic acid with polyols could
2 easily implemented and the polyol esters based on levulinic acid are expected
3 to have similar properties of lubricant compared to other polyol esters.
4 Therefore, there might be broader application prospects for it to produce
5 biolubricant compared to other vegetable oils.

6 Hence, this study was aimed at employing levulinic acid and polyols such
7 as NPG (dihydric), TMP (trihydric) and PE (tetrahydric) for the synthesis of
8 polyol esters. The potential of the synthesized esters as base stocks for
9 biodegradable lubricants was also evaluated.

10 **2. Materials and methods**

11 *2.1. Chemicals*

12 NPG, TMP and PE were obtained from Fuchen Chemical Co. Ltd.
13 (Tianjin, China); levulinic acid (LA) with the purity of 99% was purchased
14 from Adamas Reagent Co., Ltd.; the sulfuric acid with purity of 98% was
15 procured from Beijing Chemical Factory. The other solvents of analytical grade
16 were obtained from Beijing Chemical Factory; mineral oil with similar
17 viscosity of LA-based TMP ester was provided kindly by SINOPEC in Beijing.

18 *2.2. Analysis*

19 ¹H NMR spectra were obtained using a Bruker AR X 400 Spectrometer
20 (400, 200 MHz). Mass spectra were recorded on a VG Auto Spec-M
21 (Manchester, UK) and the compounds including LA, mono-, di- and
22 trisubstituted esters in the reaction mixture were quantified using a GC-2010

1 gas chromatography (Shimadzu, Japan) equipping with a DB-1ht capillary
2 column (30m × 0.25mm × 0.1µm; J&W Scientific, USA) and a flame ionizing
3 detector (FID). The column temperature was held at 110°C, then heated to
4 132°C at 12°C/min, and to 180°C at 30°C/min and finally to 300 °C at 20
5 °C/min and then maintained for 5min. The temperatures of the injector and
6 detector were both set at 300 °C.

7 *2.3. Viscosity*

8 Viscosity measurements were conducted at 40°C and 100°C using Cannon
9 Fenske viscometer tubes in a Cannon Constant Temperature Viscosity Bath
10 (Hunan Petrochemical Instrument CO., LTD.). Viscosity and the viscosity
11 index were calculated using ASTM methods D445 and D2270, respectively.
12 All viscosity measurements were carried out in triplicate, and the average value
13 was reported.

14 *2.4 Pour point*

15 Pour points were determined by ASTM method D97 with an accuracy of
16 ±3°C an using Automatic Pour Point Tester, manufactured by Hunan
17 Petrochemical Instrument CO., LTD.. All runs were carried out in duplicate.
18 Sample temperature was measured in 3°C increments at the top of the sample
19 until it stopped pouring.

20 *2.5 Flash point*

1 Flash point of the products was determined using a Flash Point Tester (Hunan
2 Petrochemical Instrument CO., LTD.) according to ASTM D93 method. The
3 lowest temperature for application of the test flame, which caused the vapor
4 above the surface of the liquid to ignite, was taken as the flash point of the
5 product at ambient barometric pressure.

6 *2.6 Cloud point*

7 Cloud points were determined by standard ASTM D2500 using Cloud Point
8 Apparatus (Beijing Timepower Measure and Control equipment CO., LTD.).

9 *2.7 Copper strip corrosion*

10 Copper strip corrosion was determined using Copper Strip Corrosion Tester
11 (Beijing Timepower Measure and Control equipment CO., LTD.). The
12 appearance of the Cu strip was assessed by comparison with Copper Strip
13 Corrosion Standards (ASTM D130).

14 *2.8 The volatility determination*

15 The volatility was determined in agreement with ASTM method D6184 in
16 an electrical stove using glass pans of 4 cm in diameter.

17 *2.9 Thermogravimetric analysis (TGA)*

18 Thermogravimetric analysis (TGA) is a measure to evaluate the thermal
19 stability of materials. A higher TGA onset temperature represents a higher
20 thermal stability of a material. Thermal behavior of the LA-based polyol esters
21 were studied using a PerkinElmer thermo gravimetric differential thermal

1 analyzer (TG/DTA) under a flow of nitrogen (flow rate of 40 ml/min) at a
2 constant heating rate of 10°C/min.

3 *2.10 HFRR (High frequency reciprocating rig) configuration*

4 The HFRR wear test was used to investigate the effect of ester under fluid
5 film lubrication as shown in Figure 1. The HFRR test (ASTM D6079) used in
6 this study involves a weighted cast iron pin cylinder (6 mm length) and a
7 stationary cast iron plat (15 mm*15 mm), which is completely submerged in a
8 10 ml of sample. The ball and disk is tested at room temperature and brought
9 into contact with each other and the entire apparatus is vibrated at 50 Hz for 75
10 min with the load 200g. The sliding stroke is maintained at 2 mm. Several
11 blends of LA-based TMP ester including 1%, 3%, 7%, 10%, 20% and 100%,
12 are tested and analyzed. Each test was carried out three times repeatedly to
13 observe any errors need to be analyzed.

14 *2.11 Synthesis methods*

15 *2.11.1 Preparation of NPG diester of LA (NPG-di-LA)*

16 Synthesis of NPG-di-LA was according to Figure 2 (A), and the catalyst
17 was sulfuric acid. The reaction was performed in a temperature controlled
18 reactor with mechanical stirring. The reaction mixture contained 500.00g
19 (4.30mol) LA and 149.15g (1.43mol) NPG. It was incubated for 2h at 95°C in
20 presence of 6.49g sulfuric acid (1% of total mixture). The process of the

1 reaction was monitored by GC, and after completion of the reaction, the crude
2 product was distilled by Rotary Film Molecular Distillation (VTA GMBH &
3 Co. KG, Germany) at 140°C and 1mbar to remove sulfuric acid and excess LA.
4 After that, the obtained product from the first distillation was distilled once
5 again at 170°C and 0.3mbar to get the final NPG-di-LA product with purity of
6 96.21%. The structure of the target product was characterized by ¹H NMR and
7 mass studies.

8 ¹H NMR (CDCl₃, δ ppm): 0.97 [s, 6H, 2×(-CH₃)], 2.21 [s, 6H, 2×(-CO-
9 CH₃)], 2.59-2.62 [m, 4H, 2×(-CO-CH₂-)], 2.76-2.79 [s, 4H, 2×(-CH₂-CO-)],
10 3.90 [s, 4H, 2×(-CO-CH₂-)]; ESI MS: m/z 323.15 [M+Na]⁺.

11 2. 11.2. Preparation of TMP triester of LA (TMP-tri-LA)

12 Synthesis of TMP-tri-LA was according to Figure 2 (B), and the catalyst
13 was sulfuric acid. The reaction was performed in a temperature controlled
14 reactor with mechanical stirring. The reaction mixture including 500.00g
15 (4.30mol) LA and 144.43g (1.08mol) TMP. It was incubated for 2h at 95°C in
16 presence of 6.44g sulfuric acid (1% of total mixture). The process of the
17 reaction was monitored by GC, and after completion of the reaction, the crude
18 product was distilled by Rotary Film Molecular Distillation (VTA GMBH &
19 Co. KG, Germany) at 140°C and 1mbar to remove sulfuric acid and excess

1 LA. Thereafter, the obtained product from the first distillation was distilled
2 once again at 230°C and 0.009mbar to get the final TMP-tri-LA with purity of
3 95.82%. The structure of the target product was characterized by ¹HNMR and
4 mass studies.

5 ¹H NMR (CDCl₃, δ ppm): 0.89-0.92 [s, 3H, (-CH₃)], 1.48-1.50 [s, 2H, (-
6 CH₂-CH₃)], 2.20 [s, 9H, 3×(-CO-CH₃)], 2.58-2.60 [s, 6H, 3×(-CO-CH₂-)],
7 2.76-2.79 [s, 6H, 3×(-CH₂-CO-)], 4.03 [s, 6H, 3×(-CO-CH₂-)]; ESI MS: m/z
8 451.20 [M+Na]⁺.

9 2. 11.3 Preparation of PE tetraester of LA (PE-tetra-LA)

10 Synthesis of PE-tetra-LA was according to Figure 2 (C), and the catalyst
11 was sulfuric acid. The reaction was performed in a temperature controlled
12 reactor with mechanical stirring. The reaction mixture contained 500.00g
13 (4.30mol) LA and 117.24g (0.86mol) TMP. It was incubated for 12h at 115°C
14 in presence of 6.17g sulfuric acid (1% of total mixture). The process of the
15 reaction was monitored by GC, and after completion of the reaction, the crude
16 product was distilled by Rotary Film Molecular Distillation (VTA GMBH &
17 Co. KG, Germany) at 140 °C and 1mbar to remove sulfuric acid and excess LA.
18 Afterward, the obtained product from the first distillation was distilled once
19 again at 290 °C and 0.0085mbar to get the final TMP-tri-LA product with

1 purity of 95.01%. The structure of the target product was characterized by
2 ^1H NMR and mass studies.

3 ^1H NMR (CDCl_3 , δ ppm): 2.19 [s, 12H, $4\times(-\text{CO}-\text{CH}_3)$], 2.57-2.60 [s, 8H,
4 $4\times(-\text{CO}-\text{CH}_2-)$], 2.75-2.78 [s, 8H, $4\times(-\text{CH}_2-\text{CO}-)$], 4.12 [s, 8H, $4\times(-\text{CO}-$
5 $\text{CH}_2-)$]; ESI MS: m/z 551.21 [$\text{M}+\text{Na}$] $^+$.

6 **3. Results and discussion**

7 *3.1 Characterization and physico-chemical properties of esters*

8 Polyol esters, derived from esterification or transesterification using plant
9 oils and animal oils with neopentyl polyols without hydrogen atoms on the β
10 carbon, have been widely used for lubricants. Due to their superior physico-
11 chemical properties and performances compared with mineral oils, its
12 applications have expanded largely. The present study was focused on the use
13 of non-edible levulinic acid, a promising platform chemical derived from
14 biomass, combined with dihydric, trihydric and tetrahydric alcohols named
15 NPG, TMP and PE respectively to produce LA-based polyol esters. The polyol
16 esters based on levulinic acid were expected to have similar properties of
17 lubricant compared with other polyol esters.

18 The purity of the levulinic acid-based polyol esters was determined by GC
19 analysis and found to exceed 95%. The structures of polyol esters were

1 confirmed using ^1H NMR (Figure 4) and ESI-MS (Figure 3) spectral studies.
2 The molecular ions 323.15 $[\text{M}+\text{Na}]^+$, 451.20 $[\text{M}+\text{Na}]^+$, 551.21 $[\text{M}+\text{Na}]^+$
3 correspond to compounds NPG-di-LA; (B) TMP-tri-LA; (C) PE-tetra-LA,
4 respectively. All the products were characterized for their physico-chemical
5 properties, such as viscosity at 40°C and 100°C, viscosity index (VI), pour
6 point, flash point, cloud point and copper strip corrosion (Table 1).

7 Kinematic viscosity is an important characteristic to exhibit the
8 relationship between viscosity and temperature. The property of the viscosity–
9 temperature directly represents lubricant’s performance and determines its
10 application. Table 1 showed the kinematic viscosities of different ester
11 products. The NPG-di-LA, TMP-tri-LA and PE-tetra-LA exhibited their
12 kinematic viscosity at 40 °C in the range of ISO VG10, reaching 17.29, 87.28
13 and 417.45, respectively. At 100°C their kinematic viscosities were 3.35, 8.42
14 and 19.14 cSt. Viscosity of the polyol ester base fluids generally increases with
15 the increase of the number of present acyl functionalities.²⁵ In this study, the
16 LA based esters prepared with NPG, TMP and PE exhibited similar trend with
17 the result of Gryglewicz’s and Padmaja’s in term of the relationship between
18 pour point and the number of branches in molecule.²⁵⁻²⁶

19 The viscosity index (VI) is an another parameter generally used for

1 evaluating the performance of a potential lubricant. By detecting the value of
2 viscosity index, variation of the kinematic viscosity with temperature can be
3 known. Generally, the higher its value, the lower variation of viscosity with the
4 temperature, and so the better performance of the lubricant. Table 2 also
5 showed the property of NPG-di-LA, TMP-tri-LA, PE-tetra-LA with viscosity
6 index 30, 48 and 15, respectively. As a high viscosity index means there was
7 little change over a wide temperature range. The performance of the three
8 synthesized esters need further improvement to become lubricant with high
9 viscosity index which was a desirable property for a lubricant by adding
10 additives in formulated lubricants. The low viscosity index can also be
11 overcome by increasing the molecular weight of the products and altering the
12 structure of their molecules, especially the introduction of double bond in their
13 composition.^{27,28} The reaction between LA and furfural, which is also a
14 platform chemical from lignocellulosic residues, can be easily implemented in
15 aq. NaOH.²⁹ The product, 6-furfurylidene levulinic acid, can be used to prepare
16 biolubricant base stocks by esterification with polyols. This kind of polyol
17 esters contains the double bond and the molecular weight is higher than
18 levulinic acid-based polyol esters. So the viscosity index could be improved
19 obviously.

1

2 Pour point is an another key parameter to assess the performance and
3 application of a potential lubricant. It is the temperature that a lubricant can't
4 flow when a jar is tilted during cooling environment. Lubricants with a low
5 pour point is conducive to the operation of the engine in cold temperature
6 climates. The pour point of ester products in this study was measured by
7 ASTM D97. Generally, pour points of polyol esters prepared from unsaturated
8 fatty acids were very low, and a similar trend was observed in term of the pour
9 points of NPG-di-LA (-34 °C), TMP-tri-LA(-25 °C) and PE-tetra-LA (-8 °C).
10 It was found that the pour point of NPG-di-LA with less number of acyl chains
11 was lower compared to other polyols, which could be due to more effective
12 disruption of molecules packing compared to PE and TMP esters. However, the
13 pour point of PE-tetra-LA was high. It suggested that the molecular
14 configuration of NPG and TMP esters was more effective at disrupting
15 molecule packing compared to PE ester. Such low pour points were useful for
16 applications in machine tool and hydraulic systems.³⁰ Compared with recent
17 researches which reported the pour points of other fat acid-based polyol esters,
18 the NPG-di-La and TMP-tri-LA ester exhibited competitive characteristic of
19 lower temperature, it's pour points lower than product (pour point -27 °C) from

1 castor oil and TMP¹² and that of the polyol ester (pour point -18 °C) from
2 rapeseed oil and TMP,³² and polyol ester (pour point -6 °C) from rubber seed
3 oil and TMP.³³

4 The flash point is defined as the minimum temperature at which the liquid
5 produces a sufficient concentration of vapor above it that it forms an ignitable
6 mixture with air. The lower flash point is, the greater fire hazard. The TMP-tri-
7 LA ester possessed excellent thermal stability with flash points at 228°C
8 followed by PE-tetra-LA ester at 210°C and NPG-di-LA at 185°C. The TMP-
9 tri-LA ester had higher thermal stability followed by NPG-di-LA and PE-tetra-
10 LA esters. This trend was different from other synthetic esters.³¹ Flash points of
11 all the polyol esters were found to be very high within the range of 185–228 °C,
12 and the esters with flash point $\geq 165^\circ\text{C}$ lie well within the range of hydraulic
13 oils.³⁴

14 Cloud point was the temperature at which liquid becomes cloudy in
15 appearance. A high cloud point could lead to filter plugging and poor
16 pumpability in cold weather applications. Among the new three kinds of esters
17 in this paper, NPG-di-LA had the lowest cloud point, which reached -11 oC
18 and even lower. The cloud point of TMP-tri-LA was -4 °C followed by 7 °C of
19 PE-tetra-LA.

1 Copper corrosion test was also conducted in order to measure the
2 tendency to cause metal deterioration. The result indicated that three kinds of
3 the levulinic acid-based polyol esters were class 1a (slight tarnish). The term
4 “class” represents the property of copper corrosion, and it is judged according
5 to the color of the copper strip. The lower the copper corrosion property the
6 lower the “class” of the oil. 1a was the lowest class in Copper Strip Corrosion
7 Standards (ASTM D130). Thus, all the esters in this study had low corrosion
8 on metal materials.

9 The volatility relates to the potential loss of lubricant and to the
10 environmental impact of the volatile components of the fluid. Both European
11 and U.S. OEM and industry organizations include volatility in their
12 specifications.³⁵ In this study, NPG-di-LA, TMP-tri-LA and PE-tetra-LA
13 exhibited very low volatility with only 0.57%, 0.41% and 0.33% of weight
14 loss at 120 °C, respectively. The loss of three kinds of the levulinic acid-based
15 polyol esters due to high-temperature volatility was found to decrease steadily
16 with an increase in carbon numbers. Therefore, in levulinic acid-based polyol
17 esters formulations, volatility is not a problem, which is due to higher
18 molecular weight associated with the structure of glycerol analogues.

19 TGA is a measure to evaluate the thermal stability of materials. Generally,

1 the higher T_{onset} of a material, the higher is its thermal stability. In previous
2 literatures, some researchers have used this method to measure the thermo-
3 oxidative stability of oils.³⁶⁻³⁷ According to the TGA analytical results as
4 shown in Figure 5, TGA curves of all samples had similar behavior. The
5 accurate analysis of TGA curves was summarized in Table 2. It was also
6 found that the three prepared levulinic acid-based polyol esters possessed
7 good thermal stability. NPG-di-LA, TMP-tri-LA, and PE-tetra-LA were
8 thermally stable with less than 4% mass weight loss below the temperature of
9 189°C, 255°C and 222°C, respectively. Besides, about 9-10% of weight loss
10 was observed for each sample within the temperature range of 203–205°C,
11 281–286°C and 252–259°C, respectively. The weight loss of the NPG-di-LA,
12 TMP-tri-LA, and PE-tetra-LA reached 97% when each of the temperature
13 achieved 579, 487 and 684°C, respectively. Then, there was no further loss of
14 weight with any increasing temperature. It is known that levulinic acid-based
15 polyol esters are not susceptible to undergo autoxidation reactions. While
16 these TGA measurements provided a preliminary estimate of the stability of a
17 lubricant, further chemical studies would be necessary to check for the
18 stability and functions in these lubricants.

19 Among the three levulinic acid-based polyol esters, TMP ester exhibited

1 superior properties such as pour point, viscosity index and oxidation stability
2 which were similar to that of TMP trioleate.³⁸ Due to its high viscosity index,
3 high thermal stability and low pour point, TMP-tri-LA ester could be
4 considered as a potential biodegradable lubricant base stock.

5 *3.2 Tribological properties of TMP-tri-LA*

6 *3.2.1 Coefficient of friction (COF)*

7 Figure 6. showed the friction coefficient plotted against the sliding time
8 for various percentages of TMP-tri-LA biolubricants. The results of the figure
9 depict that the value of friction coefficient ranged from 0.007 to 0.17. For
10 ordinary mineral oil (0% ester), it can be seen that the coefficient of friction
11 which is 0.15 on average is the highest within the operation time. For samples
12 of 3%, 7%, 10%, 20% TMP-tri-LA in mineral oil, the coefficient of friction
13 was higher at the beginning and then it fell down rapidly. The 100% TMP-tri-
14 LA kept constantly low coefficient of friction which was 0.09 on average
15 within the operation time. A considerable improvement of friction coefficient
16 was observed with addition of TMP-tri-LA ester in ordinary mineral oil. This
17 phenomena was consistent with Madankara's work which claimed that friction
18 coefficient was reduced significantly by adding hydroxy ester product to diesel
19 fuel.³⁹ The TMP-tri-LA component of biolubricants formed multi and mono

1 layer on the surface of the rubbing zone and make stable film to prevent the
2 contact between the surfaces.

3 3.2.2 Wear scar diameter (WSD)

4 The frictional wear results by the addition of different percentages of
5 TMP-tri-LA ester to mineral oil were studied using HFRR apparatus.
6 Microscope images of wear scar generated on the surface of a test sample were
7 showed in Figure 7 when different percentages of TMP-tri-LA in ordinary
8 mineral oil were used as lubricant contact fluids. It is evident in Figure 8, the
9 highest wear scar diameter of 300 μm was generated when 1% ester in ordinary
10 mineral oil. The ordinary mineral oil (0% ester) has generated a wear scar
11 diameter of 291 μm . There was a significant reduction in wear scar diameter
12 with a higher percentages of TMP-tri-LA in ordinary mineral oil. The
13 significance improvement in wear scar diameter of 132 μm was found for the
14 100% TMP-tri-LA product. It was reported in previous researches that TMP
15 esters of palm and palm kernel (*E.gue-neensis*) oil had resulted in wear scar
16 diameters of 200–350 μm and 200–400 μm , respectively.⁴⁰ Comparatively, the
17 TMP-tri-LA ester exhibited superior lubricity performance comparing with
18 other biolubricants.

19 The possible mechanism by which the friction was reduced was that the

1 uniform molecule structure of TMP-tri-LA ester formed a monolayer film in
2 the contact area with the addition of different percentages of ester to mineral
3 oil. of lubrication is the good monolayer film formed by the uniform molecule
4 structure of TMP-tri-LA ester in the contact area with the addition of different
5 percentages of ester to mineral oil. Basically, polyol esters are well known that
6 they can provide good lubricity because of its uniform molecule structure.^{41,42}
7 Fatty acids used to synthesize polyol esters have longer branched chains than
8 ordinary mineral oil. This kind of molecule structure offers formation of good
9 monolayer film on sliding surface. The second possible mechanism of
10 lubrication is the polarity of molecule of TMP-tri-LA ester that contributes to
11 better lubricity characteristic. The property of the molecular structure of the
12 polyol ester is a polar at one end and non-polarity at the other end. The reason
13 that friction was reduced as percentages of ester to mineral oil increased is that
14 molecular adsorption on the surface of metal was enhanced. The friction was
15 reduced as percentages of ester added to mineral oil increased was resulted
16 from the enhancement of molecular adsorption on the surface of metal. One
17 end of the molecular was attracted strongly to metal surface due to the polarity
18 and the other one end was extended out. This distribution of moleculars in the
19 mixture samples produced a strong barrier to avoid direct friction between two

1 surfaces.^{43,44,45} So, there is a significant reduction in wear scar diameter with
2 addition of TMP-tri-LA ester in ordinary mineral oil. This phenomena was
3 consistent with other researchers' results that wear scar diameter got smaller
4 and friction was reduced obviously when carboxylate group in ester and the
5 polarity increased in the ordinary mineral oil.^{46,47}

6 **4. Conclusions**

7 LA was a promising derivative derived from biomass. In this study, a new
8 kind of levulinic acid-based polyol esters was prepared by esterification of
9 levulinic acid with three different kinds of polyol. The crude product was
10 distilled to obtain target product with purity of above 95%. Among the three
11 polyol esters obtained in this study, TMP-tri-LA ester exhibited superior
12 properties of lubricant like good viscosity index, low pour point, high flash
13 point, low cloud point and copper strip corrosion, low volatility. The
14 biolubricity of TMP-tri-LA ester was tested on a High Frequency
15 Reciprocating Rig (HFRR) apparatus. The result exhibited that this kind of
16 biolubricant performed low coefficient of friction and wear scar diameters. It
17 suggested that this kind of polyol ester could be regarded as potential base
18 stocks for production of lubricant with high performance.

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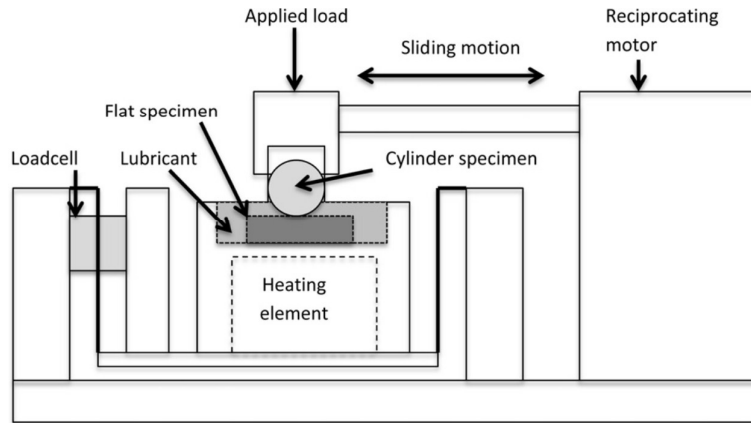


Fig. 1. The schematic diagram of HFRR wear test.

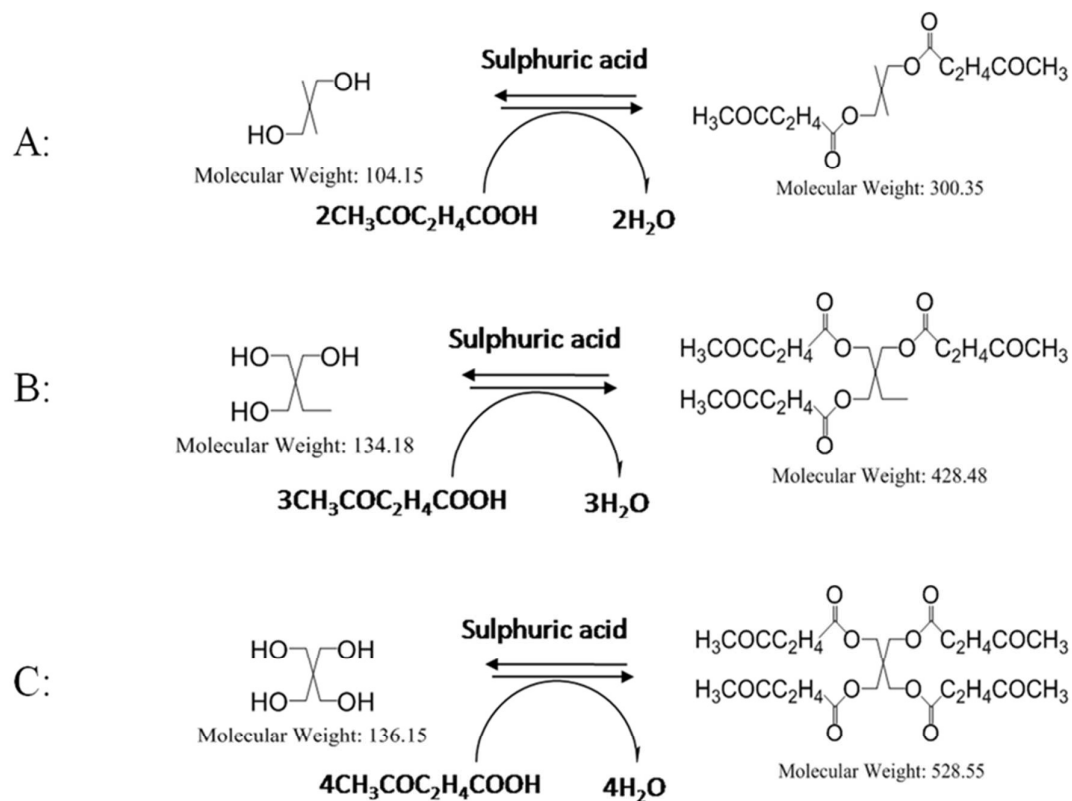
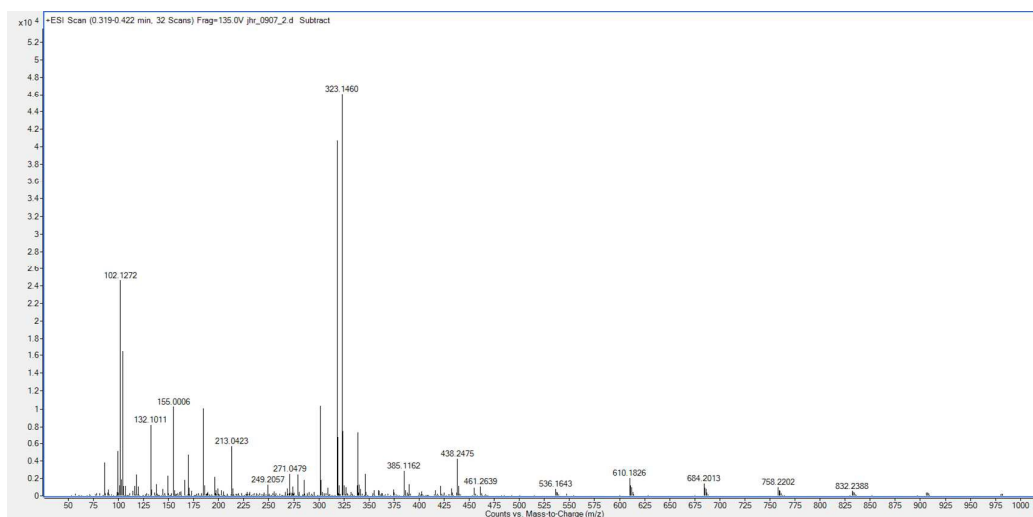
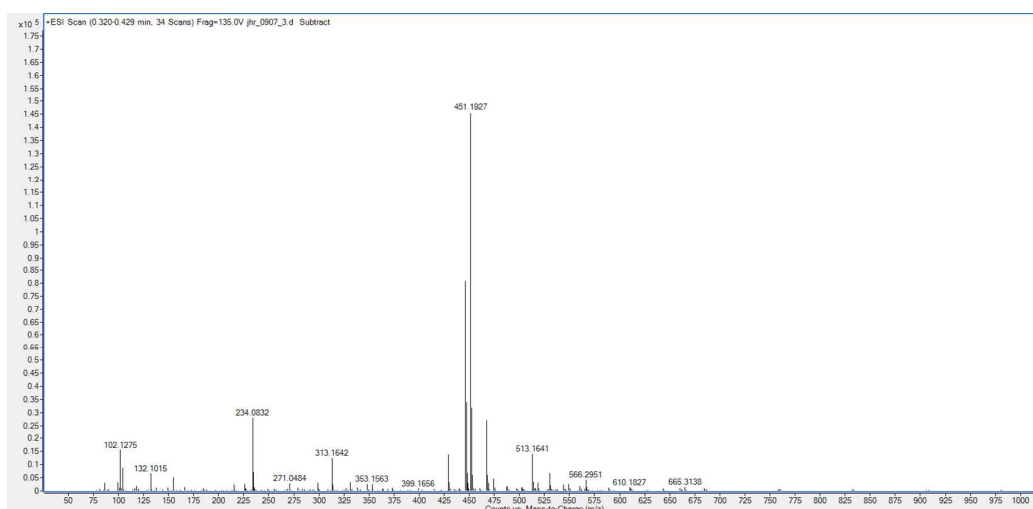


Fig. 2. Schematic representation of esterification reaction between LA and NPG, TMP, PE, respectively.

(A)



(B)



(C)

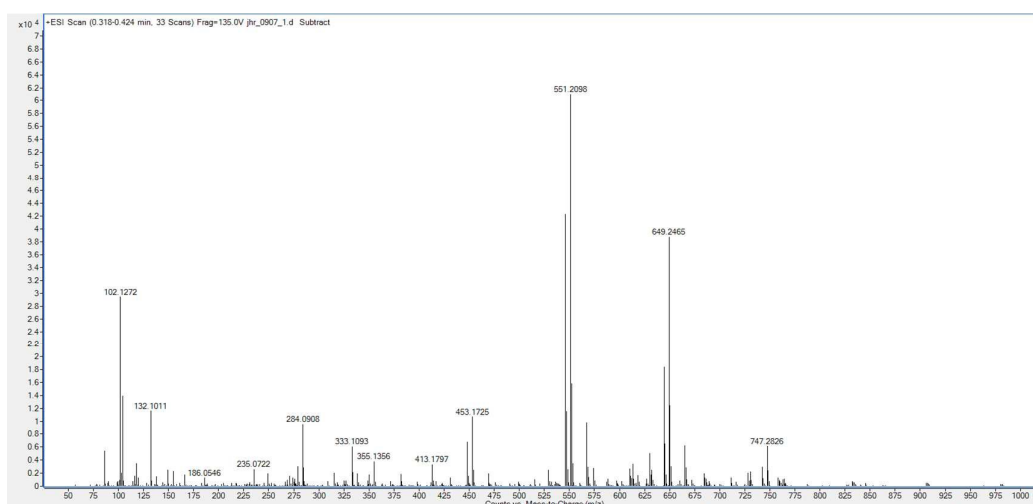


Fig. 3. Mass spectra of levulinic acid-based polyol esters : (A) NPG-di-LA; (B) TMP-tri-LA; (C) PE-tetra-LA.

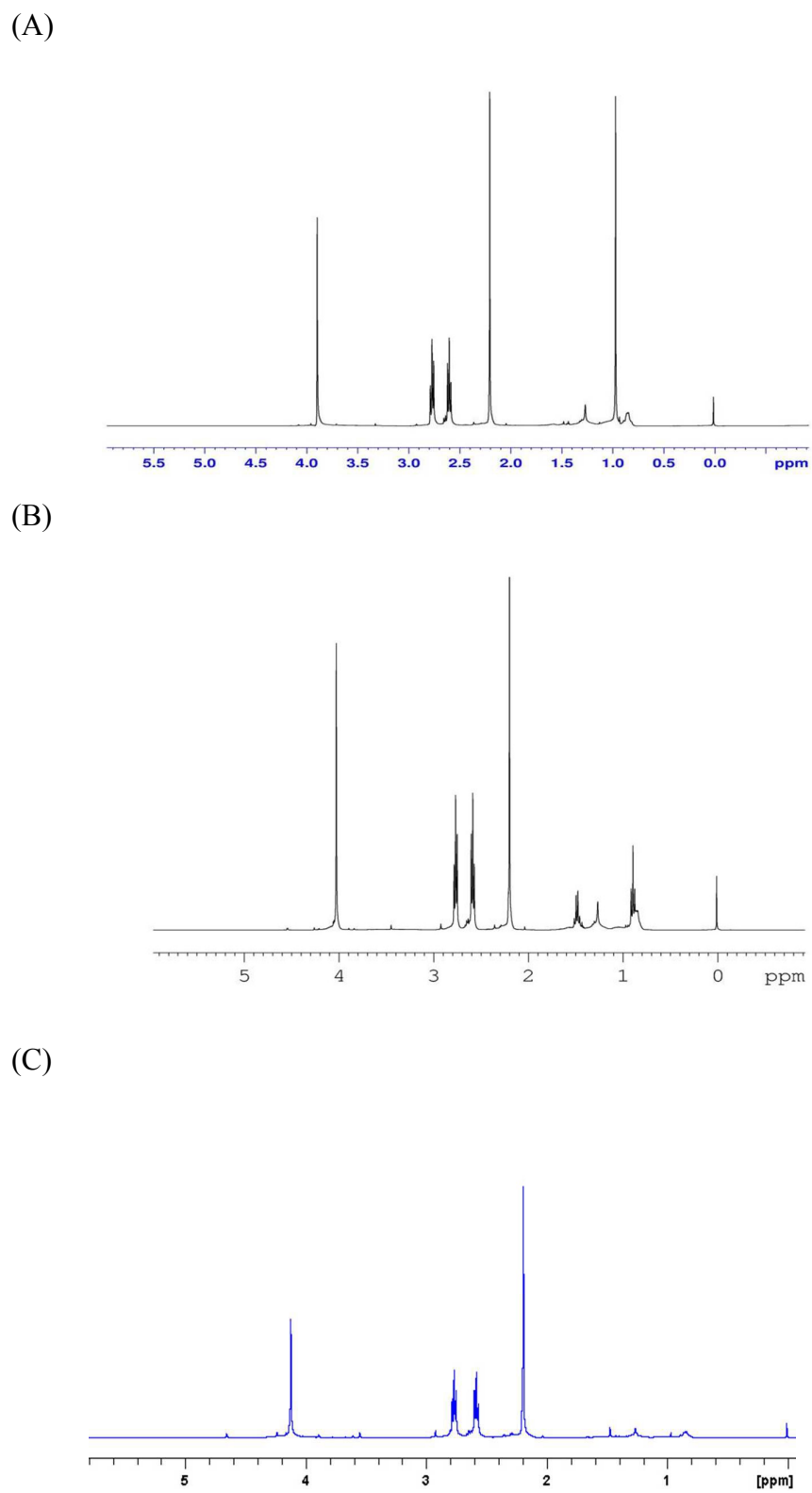


Fig. 4. ^1H NMR spectra of levulinic acid-based polyol esters : (A) NPG-di-LA; (B) TMP-tri-LA; (C)

PE-tetra-LA.

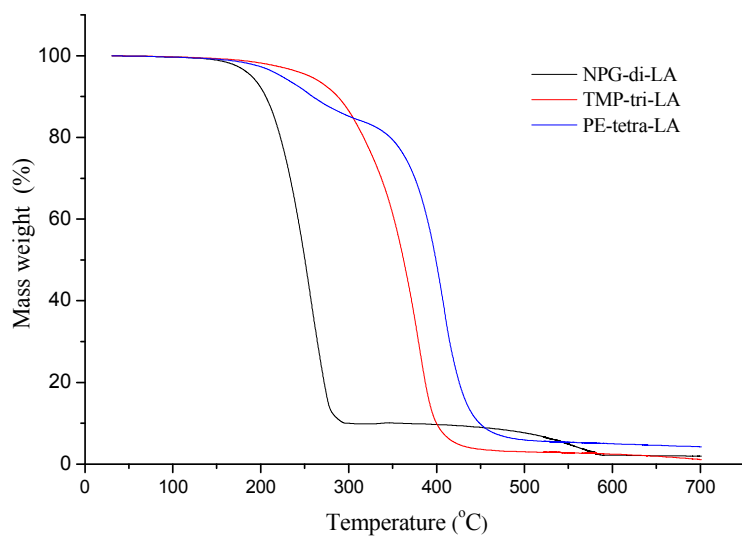


Fig. 5. The TGA curves of of LA-based polyol esters.

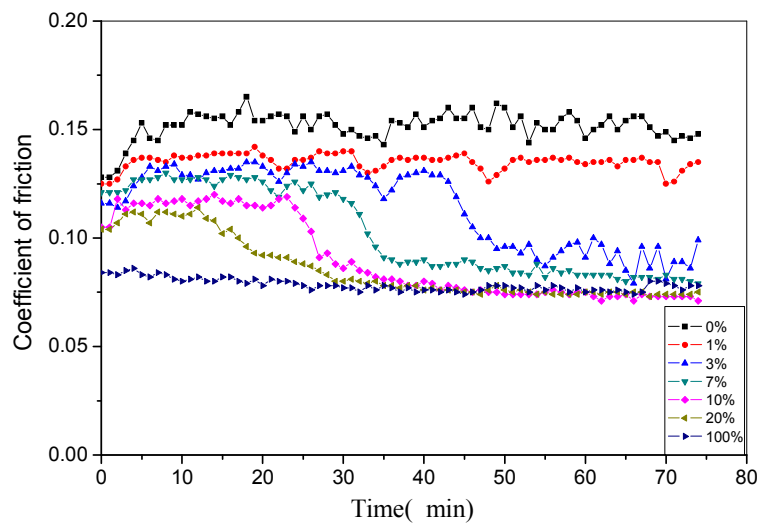


Fig. 6. Variation in coefficient of friction different percentages of TMP-tri-LA in ordinary mineral oil.

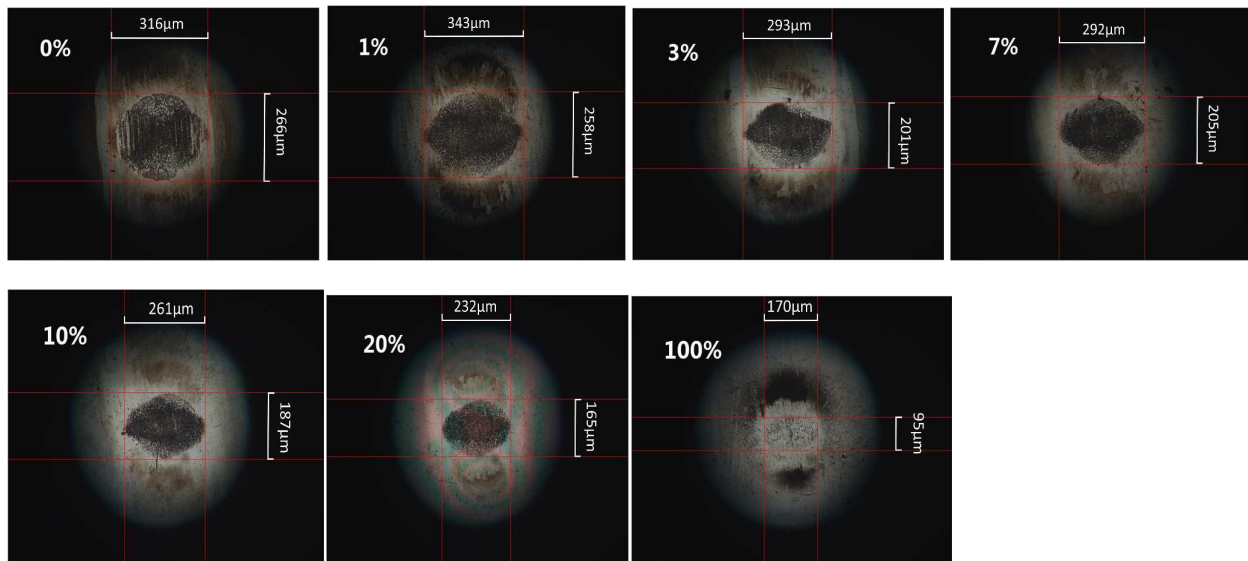


Fig. 7. Microscope of wear scar with different percentages of TMP-tri-LA in ordinary mineral oil.

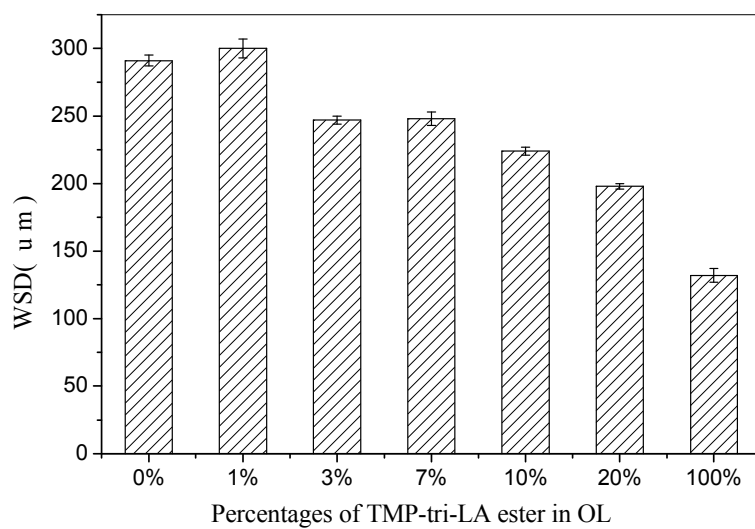


Fig. 8. Wear scar diameter of different percentages of TMP-tri-LA in ordinary mineral oil.

Table 1 Physico-chemical properties of LA-based polyol esters.

Property	NPG-di-LA	TMP-tri-LA	PE-tetra-LA
Viscosity at 40 °C, (mm ² /s)	17.29	87.28	417.45
Viscosity at 100 °C, (mm ² /s)	3.35	8.42	19.14
Viscosity index	30	48	15
Pour point (°C)	-34	-25	-8
Flash point (°C)	185	228	210
Cloud point (°C)	-11	-4	7
Copper strip corrosion	1a	1a	1a
Volatility at 120 °C (%)	0.57	0.41	0.33

Table 2 Thermal stability data of the ester products.

Product	T_{onset} (°C)	9–10% wt loss (°C)	97% wt loss (°C)
NPG-di-LA	189	203-205	579
TMP-tri-LA	255	281-286	487
PE-tetra-LA	222	252-259	684