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1 **Electrochemical degradation of perfluorooctanoic acid (PFOA) by Yb-doped**  
2 **Ti/SnO<sub>2</sub>-Sb/PbO<sub>2</sub> anodes and determination of the optimal conditions.**

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9 **ABSTRACT**

10 Model aqueous solutions of perfluorooctanoic acid (PFOA, 100 mg/L) were  
11 electro-oxidized in a homemade container. The electrocatalytic behavior and anodic  
12 performance of Ti/SnO<sub>2</sub>-Sb/Yb-PbO<sub>2</sub>, Ti/SnO<sub>2</sub>-Sb-PbO<sub>2</sub> and Ti/SnO<sub>2</sub>-Sb-Yb anodes  
13 in sodium electrolytes were compared. The SnO<sub>2</sub>-Sb/Yb-PbO<sub>2</sub> anode demonstrated  
14 better electrocatalytic performance compared with the SnO<sub>2</sub>-Sb-PbO<sub>2</sub> and  
15 SnO<sub>2</sub>-Sb-Yb electrodes in terms of both degradation and defluorination. Then a  
16 systematic experimental study was designed as follows to analyze the influencing  
17 factors: initial concentration of PFOA (10mg/L to 200 mg/L), current density (1  
18 mA/cm<sup>2</sup> to 40 mA/cm<sup>2</sup>), initial pH value (3 to 11) and electrode distance (5 mm to 20  
19 mm). After a 150 min electrolysis, the optimum reaction conditions were obtained and  
20 the degradation and defluorination ratios reached 95.11±3.9% and 75.7±2.8%,

21 respectively. Under the optimum conditions, the degradation of PFOA followed  
22 pseudo-first-order kinetics ( $0.0193 \text{ min}^{-1}$ ) and the degradation half-life was 35.9 min.  
23 The produced  $\text{F}^-$  was measured using a fluoride ion selective electrode, whereas the  
24 intermediate PFCAs with short-chain lengths were measured using HPLC-MS. A  
25 detailed degradation pathway was proposed in this study by analyzing the  
26 intermediates and the recovery of fluoride.

27 **Keywords:** Electro-chemical degradation; Ytterbium-doped; Perfluorooctanoic acid  
28 (PFOA); Optimal conditions; Mechanisms

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## 42 1. Introduction

43 Perfluorooctanoic acid compounds are considered important surfactants and  
44 emulsifiers because of their hydrophobic and oleophobic characteristics. Since the  
45 1960s, the electrochemical fluorination method has been applied to the production of  
46 perfluorinated compounds, perfluorooctanoic acid, and many other kinds of  
47 perfluorinated carboxylic acids (PFCAs) and salts that contain sulfonyl perfluorinated  
48 organic compounds. Over the recent decades a large number of these products have  
49 been developed for both industrial and domestic uses [1,2]. The extensive use of these  
50 products and the strong bond energy of the C-F bond (116 kcal/mol) [3] have driven  
51 the accumulation of these compounds in various environmental niches worldwide  
52 [4-6]. In fact, these compounds have also been observed in many animal [7] and  
53 human tissues [8, 9] because of the amplification of the food chain. Some reports  
54 suggested that this class of compounds are toxic to experimental animals and humans  
55 [10, 11]. Therefore, in the fourth session of the Stockholm Conference in 2009,  
56 perfluorinated compounds including perfluorooctane sulfonic acid, perfluorooctane  
57 sulfonate and perfluorooctanesulfonyl fluoride were included in the new list of  
58 persistent organic pollutants thereby establishing the harmfulness of such substances.  
59 Several methods for degrading perfluorinated acids under specific situations have  
60 been investigated. Among these methods, sonochemical degradation [12] and  
61 thermolysis [13] can achieve high decomposition ratios for PFOA, but these  
62 techniques require strict reaction conditions and high energy consumption. Although

63 the persulfate radical ( $S_2O_8^{2-}$ ) oxidation [14] and  $H_3PW_{12}O_{40}$  [15] methods can  
64 degrade PFOA under mild reaction conditions, the defluorination process is slow and  
65 inefficient. Membrane separation [16, 17], adsorption [18, 19] and ion exchange [20,  
66 21] have also been investigated, but these merely transfer the contaminants to a  
67 second phase. The effect of disposal of the generated waste disposal on the  
68 environment and the consumption of resources must also be managed.

69 Unlike the above methods, electrochemical oxidation can overcome the limited  
70 oxidizing abilities of conventional advanced oxidation processes because of its many  
71 advantages, such as high oxidation efficiency, fast reaction rate, easy operation,  
72 amenable to automation, and environmental compatibility. Previous studies have  
73 demonstrated the effectiveness of boron-doped diamond,  $SnO_2$  and  $PbO_2$  in the  
74 degradation and mineralization of perfluorocarboxylic and perfluorosulfonic acids in a  
75 model solution [22]. Some reports have also reported the strong ability of the lead  
76 dioxide electrode in producing hydroxyl radical [23-25]. Other researchers have  
77 incorporated materials, such as  $Nb^{5+}$ [27],  $Bi^{4+}$ [28],  $Ce^{4+}$ [29],  $Mn^{4+}$ [30], and carbon  
78 aerogel [31] into the  $PbO_2$  coating to enhance its catalytic activity for wastewater  
79 treatment [32].

80 In the previous report [32, 33], cerium was doped in the preparation of electrodes for  
81 degrading PFOA. Ytterbium and cesium, which both belong to Lanthanide, share the  
82 similar chemical properties. The configuration of Ytterbium is  $[Xe]4f^{14}6s^2$ , which is  
83 the most stable element among the rare earth (RE) element because of the saturation  
84 state. At the same time, the resistivity of Ytterbium is  $28 \mu\Omega / cm$ , which is the

85 smallest among the rare earth. The structural superiority above makes  $\text{Yb}^{3+}$  being  
86 studied extensively for many applications, such as the preparation of lithium ion  
87 batteries [34]. The the photoluminescence properties of Yb-doped Si oxide [35] have  
88 been investigated, but the performance of Yb-doped electrode in degrading PFOA by  
89 electrochemical method has been rarely examined.

90 In this study, we attempt to decompose PFOA using a novel Yb(III)-doped  $\text{PbO}_2$   
91 anode that is selected from three types of anodes (e.g.,  $\text{Ti/SnO}_2\text{-Sb/Yb-PbO}_2$ ,  
92  $\text{Ti/SnO}_2\text{-Sb-PbO}_2$  and  $\text{Ti/SnO}_2\text{-Sb-Yb}$ ) and propose a decomposition pathway. We  
93 prepared and doped the electrode, investigated the effects of different factors on the  
94 electrochemical decomposition and defluorination of PFOA and studied the  
95 decomposition kinetics and defluorination pathways of PFOA by measuring the  
96 degradation rate and identifying the intermediate products. The Yb-doped anode can  
97 be an effective technology for dealing with PFOA pollution in the future.

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## 105 2. Material and methods

### 106 2.1. Chemical reagents and Instruments.

107 SnCl<sub>4</sub>·5H<sub>2</sub>O (99%, Hushi, Shanghai), SbCl<sub>3</sub> (98%, Kemiou, Tianjin), HCl (36%, Tieta,  
108 Shandong), Pb(NO<sub>3</sub>)<sub>2</sub> (99%, Damao, Tianjin), iso-propanol (99.7%, Fuyu, Tianjin),  
109 HNO<sub>3</sub> (68%, Kangde, Laiyang), NaF (99% , Damao, Tianjin), Yb(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O (99%,  
110 Bailingwei, Beijing), Oxalic acid (99%, Xilong, Guangdong), NaOH (96%, Yongda),  
111 Na<sub>2</sub>SO<sub>4</sub> (99%, Tianda, Tianjin) and Ti sheet (99%, Taiye, Baoji) were used to prepare  
112 the electrodes and for the electrolysis procedures. Perfluorooctanoic acid (PFOA, 95%)  
113 was purchased from Wongjiang (China). Perfluoroproptanoic acid (PFPrA, 97%) was  
114 supplied by Aladdin (China). Perfluoroheptanoic acid (PFHpA, 98%),  
115 perfluorohexanoic acid (PFHxA, 98%), perfluoropentanoic acid (PFPeA, 97%),  
116 perfluorobutanoic acid (PFBA, 98%) and trifluoroacetic acid (TFA, 99%) were  
117 obtained from Bailingwei (China). Na<sub>3</sub>C<sub>6</sub>H<sub>5</sub>O<sub>7</sub>·2H<sub>2</sub>O (98%, Beichen, Tianjin) and  
118 NaNO<sub>3</sub> (98%, Aibi, Shanghai) were used when measuring the concentration of  
119 fluorine ion. The instruments involoved during the experiment as follows: ultrasonic  
120 instrument (KQ-250B, Kunshanyiqi), drying cabinet (101A-2, Shuangwujin), muffle  
121 furnace (XS1-25-1200, Zhongda), pH meter (PXS-215, Lieci), magnetic stirrer (79-1,  
122 Guohua), DC power supply (DYY-6B, Liuyi). All chemicals were used without  
123 further purification and deionized water was used in all of the experiments.

## 124 2.2. Electrode fabrication.

125 The titanium (Ti) sheet was cut to a rectangular shape (50 mm × 20 mm, with a  
126 thickness of 0.4 mm). After polishing with two grades of sandpaper (280-grid and  
127 600-grid), the sheets were placed in the ultrasonic instrument for 10 min to remove  
128 the particles on its surface. The sheet was then soaked in a NaOH solution (5%, m/m)  
129 at 95 °C for 1 h to remove grease. The Ti sheet was washed with distilled water and  
130 etched in boiling oxalic acid solution (10%, m/m) for about 2 h until gray pits were  
131 observed on its surface. The middle layers of the Ti/SnO<sub>2</sub>-Sb/Yb-PbO<sub>2</sub> and  
132 Ti/SnO<sub>2</sub>-Sb-PbO<sub>2</sub> anodes are the same, while that of the Ti/SnO<sub>2</sub>-Sb-Yb anode is  
133 different. The coating solution was prepared as follows using the sol-gel technique:  
134 SnCl<sub>4</sub>·5H<sub>2</sub>O and SbCl<sub>3</sub> were dissolved in 50 ml iso-propanol at a Sn:Sb atomic ratio  
135 of 95:5. Next, 15 mL of concentrated HCl solution was added, and the resulting  
136 solution was diluted to 100 mL using iso-propanol. This solution was marked as  
137 solution A. For the Ti/SnO<sub>2</sub>-Sb-Yb anode, we added trace ytterbium nitrate to the  
138 iso-propanol solution (which contained dissolved Sn and Sb) at a Sn: Sb: Yb atomic  
139 ratio of 95:5:0.5. This solution was marked as solution B and was used to make the  
140 Ti/SnO<sub>2</sub>-Sb-Yb electrode only. We prepared three identical Ti sheets, of which two  
141 (marked as sheets 1 and 2, respectively) were dipped in solution A, while the other  
142 sheet (sheet 3) was dipped in solution B for 5 min. The sheets were then dried at  
143 130°C for 10 min, and the organics were thermally decomposed at 490°C for 5 min.  
144 This dipping-annealing cycle was repeated 12 times. In the final stage, the coating  
145 was annealed for 1 h at 490°C. Sheet 3 was the Ti/SnO<sub>2</sub>-Sb-Yb electrode.



146 Electro-deposition was employed for the preparation of Ti/SnO<sub>2</sub>-Sb/Yb-PbO<sub>2</sub> and  
147 Ti/SnO<sub>2</sub>-Sb-PbO<sub>2</sub>. Sheet 1 was placed into an acidic (pH 1, adjusted with HNO<sub>3</sub>)  
148 electro-deposition solution, which contained 200 g/L Pb(NO<sub>3</sub>)<sub>2</sub>, 2 g/L NaF, and 2.36  
149 g/L Yb(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O at a constant anode current density of 20 mA/cm<sup>2</sup> for 90 min  
150 under room temperature (25°C). The anode was used as the Ti/SnO<sub>2</sub>-Sb/Yb-PbO<sub>2</sub>  
151 electrode. Sheet 2 was treated similarly as sheet 1 except without the addition of  
152 Yb(NO<sub>3</sub>)<sub>3</sub>. The preparation of Ti/SnO<sub>2</sub>-Sb-PbO<sub>2</sub> was thus completed.

### 153 **2.3. Electrochemical Experiments**

154 The 200 mL electrochemical reaction container was made of organic glass  
155 (Polymethyl Methacrylate). During the experiments, 200 ml PFOA (100 mg/L) was  
156 electrolyzed using 0.1 M Na<sub>2</sub>SO<sub>4</sub> as a supporting electrolyte. The prepared  
157 Ti/SnO<sub>2</sub>-Sb/Yb-PbO<sub>2</sub>, Ti/SnO<sub>2</sub>-Sb-PbO<sub>2</sub> and Ti/SnO<sub>2</sub>-Sb-Yb electrodes were used as  
158 the anodes, and a same size Ti sheet was used as the cathode. The effective  
159 electrolytic area was 10 cm<sup>2</sup>, and the stirring rate was 500 r/min. The distance  
160 between the two electrodes and the electrolysis current density can be changed. The  
161 reaction solution was sampled for analysis every 15 min or 30 min during the  
162 experiments. All experiments were performed triplicate and performed at room  
163 temperature.

### 164 **2.4. Instrumental Analysis**

165 The PFCA's concentration were measured by using a high-performance liquid  
166 chromatography-mass spectrometry (HPLC-MS, Dionex U3000, USA), which was

167 equipped with a Thermo C18 column (100 mm × 2.1 mm, 3 μm). A mixture of  
168 methanol (80%, volume percent) and distilled water (20%, containing 0.1%  
169 methanoic acid) was used as the mobile phase. The sample injection volume was 10  
170 μL at a flow rate of 0.2 mL min<sup>-1</sup>. Room temperature was regarded as the column  
171 temperature (25°C). Electrospray negative ionization mass spectrometry (Thermo  
172 LCQ Fleet, USA) was used to identify the intermediate products of PFOA. The  
173 capillary temperature was 320°C. The full scan range of the mass spectra ranged from  
174 100 m/z to 600 m/z. The gas flow rates of sheath, aux, and sweep were 30, 10 and 0  
175 units, respectively, and the spray voltage was -4 kV. Given that the sodium sulfate  
176 electrolyte could harm the mass spectrometer, solid-phase extraction was performed  
177 to remove the salt from all samples before measurement. The analyte-specific mass  
178 spectra and standard curves of the PFCAs are shown in Figure S1 and S2(a to g) in the  
179 supporting information section.

180 The concentration of F<sup>-</sup> was measured using a fluoride ion selective electrode. Given  
181 that the acidity of the electrolyzed solution (pH < 4) affects the determination of  
182 fluoride ion concentration, the total ion strength adjustment buffer (TISAB) should be  
183 added to the test solution. TISAB was prepared as follows: 58.8 g sodium citrate and  
184 85 g sodium nitrate were dissolved in a beaker, then the pH was adjusted between 5  
185 and 6 with HCl, and the solution was diluted to 1000 mL using distilled water. The  
186 concentration of fluoride ( $C_{F^-}$ ) and the defluorination ratio ( $R$ ) were calculated as  
187 follows:

$$188 \quad E = E_0 - \frac{2.303RT}{F} \lg C_{F^-} \quad (1)$$

$$R = \frac{C_{F^-}}{C_0 \times 15} \times 100\% \quad (2)$$

189 where  $E_0$  (mV) represents the steady electromotive force,  $E$  (mV) is the determined  
190 electromotive force,  $C_{F^-}$  is the concentration of fluoride ion (mg/L), and  $C_0$  is the  
191 initial concentration of PFOA in mg/L. The stoichiometric factor of 15 indicates to the  
192 number of fluorine atoms in a PFOA molecule. Under the condition that the total ion  
193 strength in the solution is constant and sufficient, the electromotive force ( $E$ ) has a  
194 linear relationship with  $\lg C_{F^-}$ , and  $-\frac{2.303RT}{F}$  represents the slope of this line. The  
195 concentration of  $F^-$  can be obtained from the standard curve of  $F^-$  (Fig. S3).  
196

$$ACE = \frac{(COD_0 - COD_t)FV}{8It} \times 100\% \quad (3)$$

197 The average current efficiency (ACE) is calculated by the formula as above. Where  
198  $COD_0$  and  $COD_t$  are the chemical oxygen demands (mg/L) at the initial and the final  
199 moments, respectively. The difference between  $COD_0$  and  $COD_t$  is COD removed.  $F$   
200 is the Faraday constant (96487C/mol),  $V$  is the volume of electrolyte (L), 8 is the  
201 equivalent mass of oxygen (g/mol),  $I$  is the current (A), and  $t$  means the electrolysis  
202 time (s).  
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### 211 3. Results

#### 212 3.1. Selection of the anode material.

213 As shown in Fig. 1, under the standard reaction conditions, the degradation ratios of  
214 PFOA were  $95.11\pm 3.9\%$ ,  $83.94\pm 1.6$ , and  $80.14\pm 3.8\%$  for the Ti/SnO<sub>2</sub>-Sb/Yb-PbO<sub>2</sub>,  
215 Ti/SnO<sub>2</sub>-Sb-PbO<sub>2</sub> and Ti/SnO<sub>2</sub>-Sb-Yb anodes, respectively. Kinetic behavior was  
216 observed and modeled as a probable pseudo-first-order reaction. The electrochemical  
217 degradation rate constants ( $k$ ,  $k = \ln C_0/C$ ) of the three anodes were 0.0193, 0.012 and  
218  $0.011 \text{ min}^{-1}$ , respectively, and their defluorination ratios of PFOA were  $76.7\pm 2.8\%$ ,  
219  $61.4\pm 1.1\%$  and  $52.8\pm 2.8\%$ , respectively, as shown in Fig. 1. According to the rate  
220 constants, the degradation h e the optimal reaction conditions. A 200 mL PFOA  
221 solution was used in the electrochemical experiments to examine the effects of current  
222 density ( $1 \text{ mA/cm}^2$  to  $40 \text{ mA/cm}^2$ ), initial concentration (10 mg/L to 200 mg/L),  
223 electrode distance (5 mm to 20 mm), and initial pH (3 to 7).

#### 224 3.2. Initial PFOA concentration

225 The effects of PFOA concentration are described in this section. Table 1 shows four  
226 samples with initial PFOA concentrations of 10, 50, 100 and 200 mg/L. The  
227 concentrations of PFOA for the three anodes were reduced by  $90.90\pm 0.1\%$ ,  
228  $93.75\pm 0.7\%$ ,  $95.11\pm 3.9\%$  and  $83.86\pm 2.8\%$ , respectively (Fig. 2(a)), indicating the  
229 excellent performance of the Ti/SnO<sub>2</sub>-Sb/Yb-PbO<sub>2</sub> electrode in degrading PFOA for  
230 low-concentration solutions (<100 mg/L).

231 Fig. 2(b), shows that with an increasing initial concentration of PFOA, the  
232 pseudo-first-order kinetic constant ( $k$ ) is reduced at first, eventually increases;  
233 correspondingly, the electrochemical reaction rates increased and then decreased. This  
234 phenomenon might be explained as follows. When the concentration of initial PFOA  
235 is low (<100 mg/L), the PFOA around the anode is degraded but cannot be  
236 replenished quickly. Given the turbulence in the electrolytic cell, the PFOA located far  
237 from the anode is degraded slowly, thereby affecting the degradation rate of PFOA. In  
238 contrast, higher concentrations of shorter-chain intermediates were produced under  
239 high concentrations of PFOA. The reaction of the intermediates would consume  
240  $\text{HO}\cdot$  and gather on the surface of the electrode to transfer electrons, which would  
241 restrain the degradation reaction of PFOA.

### 242 3.3. Effect of current density

243 By influencing the electron transfer capability and the hydroxyl radical production in  
244 electrolytic systems, the current density affects the degradation and defluorination  
245 rates of PFOA [30]. Fig. 3(a) shows the different current densities (1, 5, 10, 20, 30,  
246 and 40  $\text{mA}/\text{cm}^2$ ) used to investigate the degradation of 100 mg/L PFOA. The  
247 degradation rate is very low at a low current (1  $\text{mA}/\text{cm}^2$ ), where less than 60% of the  
248 PFOA can be degraded after 150 minutes of electrolysis. Compared with this result,  
249 the degradation rate gradually increased with the increasing of applied current density.  
250 When the current density increased from 20  $\text{mA}/\text{cm}^2$  to 40  $\text{mA}/\text{cm}^2$ , the rate of  
251 degradation remained above 95% and the  $k$  value increased greatly as well, to 0.0193

252  $\text{min}^{-1}$ ,  $0.0234 \text{ min}^{-1}$  and  $0.0306 \text{ min}^{-1}$  respectively.  
253 As we can see from Fig.3 (b), when the X coordinate is  $20 \text{ mA/cm}^2$ , the Yb-doped  
254 electrode has the highest average current efficiency (ACE). The degradation of  
255 COD is low ( $<250 \text{ mg/L}$ ) under a low current intensity ( $1, 5, 10 \text{ mA/cm}^2$ ). However,  
256 in spite of the high removal, a low ACE was obtained as well when the current  
257 intensity is higher than  $20 \text{ mA/cm}^2$  because of the high power consumption. This  
258 experiment also proved that the  $20 \text{ mA/cm}^2$  is the best degradation current density in  
259 this electro-chemical system. This finding may be attributed to two reasons. First, the  
260 mass transfer rate of PFOA molecules toward the anode is limited and the degradation  
261 is inadequate. Second, the oxidation reaction at the anode is gradually enhanced by  
262 the increasing applied current density. As a result, the current oversupply leads to a  
263 lower average current efficiency (ACE) [36, 37].

#### 264 **3.4. Effect of initial pH value**

265 The electrochemical degradation of PFOA was evaluated for five integral initial pH  
266 values ranging from 3 to 11. Fig. 4 shows the degradation rates and the fitted  
267 pseudo-zero-order kinetic curves after 150 minutes at different initial pH values.  
268 When the pH value was 5, the best degradation rate of  $95.11 \pm 3.9\%$  was achieved,  
269 which was 1.1 times higher than that in pH 3 and pH 7, 1.2 times higher than that in  
270 pH 9, and 1.5 times higher than that in pH 11. The PFOA solutions with a lower initial  
271 pH value had a higher oxidation rate than those with a higher initial pH value, thus  
272 indicating that the oxidation process was more favorable in acidic solutions. This  
273 conclusion also mentioned in previous literatures [38, 39]. However, low pH value  
274 will increase the concentration of  $\text{H}^+$  and hamper the positive direction to produce

275 HO·. Therefore, the trend in Fig. 4 was present. Thus, pH 5 was the most beneficial  
276 pH value for the degradation of PFOA.

### 277 3.5. Effect of gap distance between two plates

278 At the same current density, the effect of different electrode gap distances on  
279 degradation of PFOA is equivalent to that of electrode voltage. The degradation ratios  
280 of PFOA were  $95.11 \pm 3.9\%$ ,  $89.05 \pm 1.1\%$ ,  $85.23 \pm 1.4\%$ , and  $67.92 \pm 3.8\%$  for the plate  
281 distances of 5, 10, 15, and 20 mm, respectively (Fig. 5). As shown in Table 1, the  
282 highest k value ( $0.0193 \text{ min}^{-1}$ ) was obtained at 5 mm, the k values of 0.0151 and  
283  $0.0122 \text{ min}^{-1}$  were obtained at 10 and 15 mm, respectively; and the lowest k value  
284 ( $0.0193 \text{ min}^{-1}$ ) was obtained at 20 mm. The  $t_{1/2}$  value ranged between 35.9 min and  
285 87.7 min. These data indicate that within a certain distance, a shorter electrode space  
286 will lead to a higher degradation efficiency. However, the voltages between two  
287 electrodes were 2.4, 2.9, 3.2 and 3.8 V for the distances of 5, 10, 15, and 20 mm,  
288 respectively. The longer electrode distance, the more electrolysis time was required  
289 due to the longer diffusion distance. Unlike degradation, the defluorination of PFOA  
290 required higher potential to activate electron transfer. Energy-band theory argues that  
291 the electron transfer reaction can be activated [33] when the energy level of an  
292 unoccupied electron given by the anode is lower than that of the highest occupied  
293 molecular orbital of PFOA.

### 294 3.6. The production of intermediates.

295 To investigate the production of intermediates during the electrochemical process,

296 HPLC-MS was used to measure the concentration of PFCAs (C<sub>2</sub> to C<sub>7</sub>). As shown in  
297 Fig. 6(a), six different shorter-chain perfluoroalkyl groups (e.g., TFA, PFPA, PFBA,  
298 PFPeA, PFHxA, and PFHpA) were identified and quantified by using the mass  
299 spectra, which were produced during PFOA degradation as the intermediates. Fig. 6(a)  
300 also shows the formation of intermediates over the electrolysis time. As we can see  
301 from the diagram, during 150 min of degradation, the concentrations of PFHpA (C<sub>7</sub>)  
302 and PFPeA (C<sub>6</sub>) reached their maximum values at 30 min and 60 min, respectively,  
303 which decreased afterward. The concentrations of PFPeA (C<sub>5</sub>) and PFBA (C<sub>4</sub>)  
304 increased slightly since the beginning of electrochemical reaction but began to  
305 decrease after reaching their peaks at 90 and 120 min, respectively.  
306 The concentrations of PFPA (C<sub>3</sub>) and TFA (C<sub>2</sub>) slowly increased throughout the  
307 electrolysis time. The observed degradation process is similar to that seen by other  
308 researchers [30, 40]. In summary, the appearance of the maximum concentrations of  
309 the intermediates follows the order of the number of carbon atoms and PFCAs, with  
310 longer carbon chains showing higher concentrations. These phenomena indicate that  
311 the intermediates with longer chains are formed at the beginning of electrochemical  
312 reaction and are further decomposed into shorter chain intermediates as the reaction  
313 continues [33]. The incomplete degradation also indicates that some PFOA  
314 degradation products have not been fully decomposed.

$$315 \quad \eta = \sum_{i=0}^5 (3 + 2i) \times C_{\text{CF}_3(\text{CF}_2)_i\text{COO}^-} \quad (4)$$

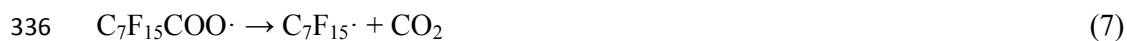
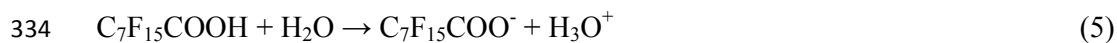
316 The mass balance of fluorine after 150 min electrolysis was investigated to analyze  
317 the electro-chemical degradation pathway of PFOA. Using Eq.(3), the mass balance



318 values of fluorine (i.e.,  $\{ F_{\text{in intermediate PFCAs, undegraded}}^- + F_{\text{in PFOA, undegraded}}^- + F_{\text{in solution}}^- \} /$   
319  $F_{\text{in PFOA initial}}^-$ ,  $F_{\text{in intermediate PFCA, undegraded}}^-$  were calculated to be 95.8%, 95.8%, 96.8%,  
320 95.3%, 93.6%, and 89.0% at different times, as shown in Fig 6(b). The recovery rates  
321 of fluoride were less than 100% (i.e.,  $F_{\text{unknown}}^-$ ), indicating that other intermediate  
322 products were quantified or detected in the solution. For example, volatile 1-C  
323 fluorocarbons may accumulate along with an increasing of electrolysis time [41].  
324 However, the high recovery rates of fluoride allow us to describe the main reaction  
325 mechanism of the PFOA degradation in an aqueous solution.

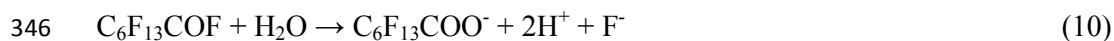
### 326 3.7. Degradation pathway of PFOA.

327 Based on the results presented above and in the previous literature, a possible pathway  
328 by electrochemical oxidation could be expressed as follows: PFOA was ionized when  
329 dissolved in the solution (Eq. (5)) [42, 43]. Using the electrochemical device, PFOA  
330 underwent direct electron transfer from the carboxyl group on the anode to form  
331 perfluorooctanoic acid carboxyl radical ( $C_7F_{15}COO\cdot$ ) (Eq. (6)). This radical was then  
332 decarboxylated to form the perfluoroheptyl radical ( $C_7F_{15}\cdot$ ), where the method of bond  
333 cleavage was similar to the Kolbe decarboxylation mechanism in Eq. (7) [44-46].

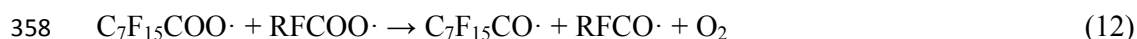


337 After the degradation process,  $C_7F_{15}\cdot$  followed two pathways. As shown in Eq. (8), the  
338 perfluoroheptyl radical was oxidized by radical species to form  $C_7F_{15}OH$  [47, 48],

339 which could be largely produced by the typical active electrode [23]. Given that  
 340  $C_7F_{15}OH$  was a terminally unstable alcohol [49], this radical underwent  
 341 intramolecular rearrangement to form  $C_6F_{13}COF$  and eliminate HF (Eq. (9)) [15, 50].  
 342 The  $C_6F_{13}OF$  was then hydrolyzed to form shorter-chain PFCAs by removing of  $CF_2$   
 343 units [15] and releasing fluoride ions into the aqueous solution (Eq. (10)).



347 In the previous literature, another reaction pathway was proposed after the Kolbe  
 348 decarboxylation. In Eq. (11), the  $C_7F_{15}\cdot$  reacted with the oxygen produced via water  
 349 electrolysis [46]. The existence of this pathway was proven by using oxygen isotope  
 350 tracers [40]. The produced  $C_7F_{15}COO\cdot$  was then combined with another  
 351 perfluorinated carboxylic acid radical ( $RFCOO\cdot$ ) to form  $C_7F_{15}CO\cdot$  and  $RFCO\cdot$  (Eq.  
 352 (12)) [29]. According to Eq. (13), the  $C_7F_{15}CO\cdot$  was decomposed to produce  
 353  $C_7F_{13}\cdot$  and  $COF_2$  [46]. The obtained carbonyl fluoride was hydrolyzed to produce  
 354 carbon dioxide and HF (Eq.14). In the degradation process, some volatile fluorinated  
 355 organic contaminants, such as  $CHF_3$ ,  $CF_4$  and  $C_2F_6$ , may be produced during the  
 356 electrolysis of the PFCs [13, 51].



361 In the two pathways above (Eq. (5-10), and Eq. (5-7, 11-14) ), PFOA was degraded to  
362 shorter-chain PFCAs by repeating the  $\text{CF}_2^-$  unzipping processes in a step-wise manner  
363 as time progressed, and PFOA was then entirely mineralized to  $\text{CO}_2$  and  $\text{F}^-$ .

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#### 383 4. Conclusion

384 Typical anodes, such as Ti/SnO<sub>2</sub>-Sb-PbO<sub>2</sub> and Ti/SnO<sub>2</sub>-Sb-Yb, can be used in the  
385 electrochemical degradation of PFOA, whereas the addition of the rare earth  
386 ytterbium (Ti/SnO<sub>2</sub>-Sb/Yb-PbO<sub>2</sub> anode) can increase the decomposition of PFOA  
387 from 83.94±1.6 and 80.14±3.8% to 95.11±3.9%. The reaction follows the  
388 pseudo-first-order kinetics, and the *k* values of PFOA follow the order of  
389 Ti/SnO<sub>2</sub>-Sb/Yb-PbO<sub>2</sub> (0.0193 min<sup>-1</sup>) > Ti/SnO<sub>2</sub>-Sb-PbO<sub>2</sub> (0.012 min<sup>-1</sup>) >  
390 Ti/SnO<sub>2</sub>-Sb-Yb (0.011 min<sup>-1</sup>). The degradation of PFOA showed a positive correlation  
391 with the increase of current density (1 mA/cm<sup>2</sup> to 40 mA/cm<sup>2</sup>), reduction of initial  
392 concentration (10 mg/L to 200 mg/L) and shorter electrode distance (5 mm to 20 mm).  
393 The degradation rate reached to the peak at pH 5, which was higher than the other  
394 tested pH values (3 to 11). The intermediate products of PFCAs (C<sub>2</sub> to C<sub>7</sub>) and  
395 fluoride ion were detected, and a possible pathway for the PFOA electrochemical  
396 degradation was proposed by analyzing the intermediate products. Compared with  
397 other metal-doped electrodes that have been recently used (between 2011 to 2015) in  
398 the decomposition of PFOA, the linear fit of the kinetic plot was *k* =0.0193 min<sup>-1</sup>,  
399 which was higher than that of the Mn-doped electrode (0.004 min<sup>-1</sup>) [30], but lower  
400 than that of the Ce-doped (0.037 min<sup>-1</sup>) electrode [29]. In addition, the degradation of  
401 the Yb-doped electrode was 95.1%, which was higher than the reduction of Bi-doped  
402 electrode (93.3%) [28]. These results indicate that electro-chemical oxidation with  
403 Yb-doped electrode is an efficient method for decomposing PFOA.

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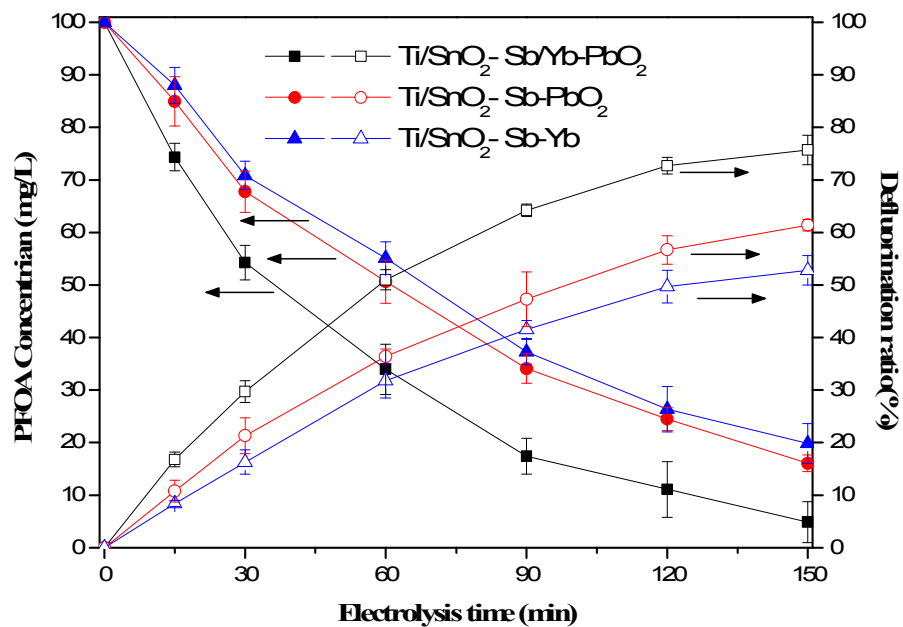
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**Fig. 1** Electrochemical degradation and defluorination ratio of PFOA at the reaction conditions including applied current density ( $20 \text{ mA/cm}^2$ ), initial concentration ( $100 \text{ mg/L}$ ), electrode distance ( $5 \text{ mm}$ ), initial pH ( $5$ ) and with a  $0.1 \text{ M}$  sodium sulfate supporting electrolyte solution during  $150 \text{ min}$ ,  $T=25 \text{ }^\circ\text{C}$ .

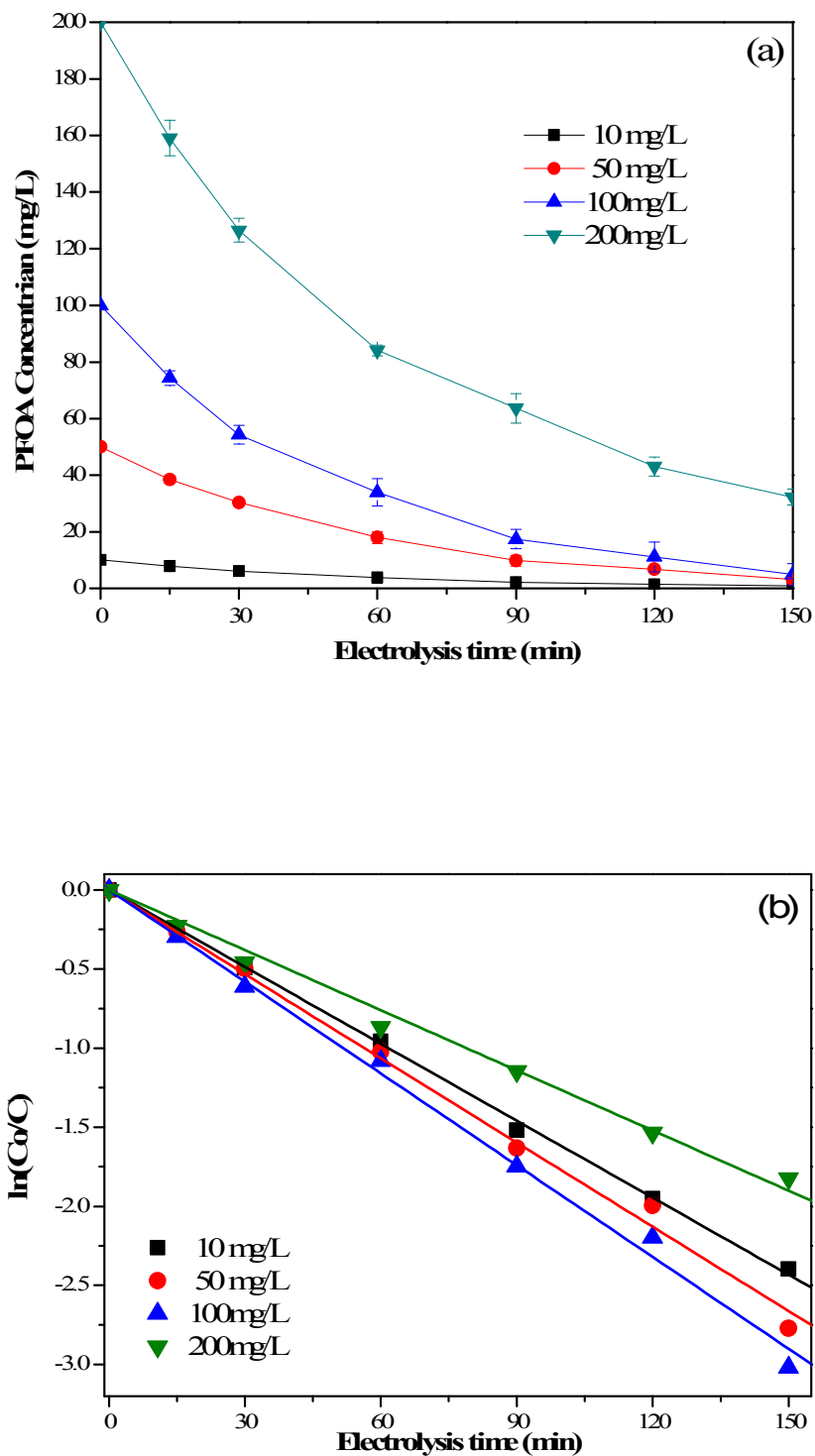


Fig. 2 (a) Effect of the initial PFOA concentration and (b) fitted pseudo-first-order kinetic curve. (Initial pH 5, plate distance 5 mm, current

density 20 mA/cm<sup>2</sup>, 0.1 M Na<sub>2</sub>SO<sub>4</sub>, T=25 °C)

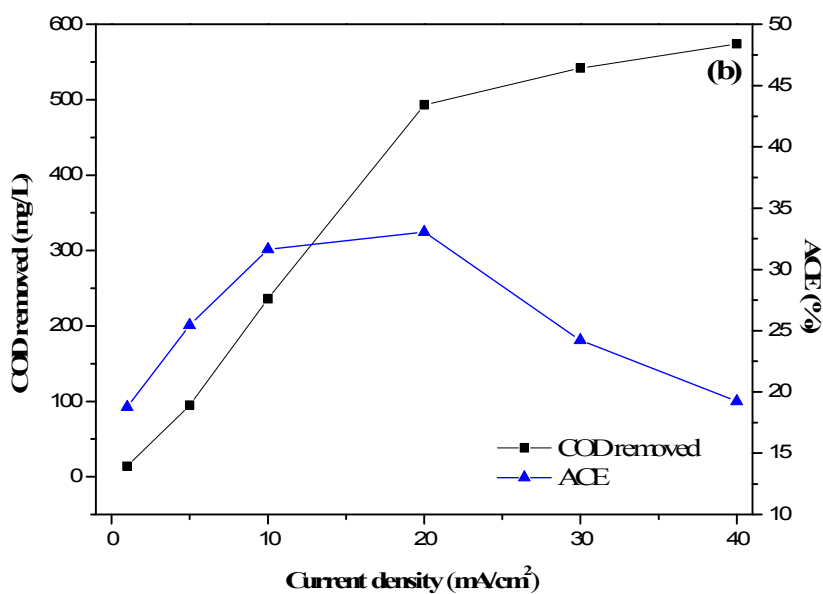
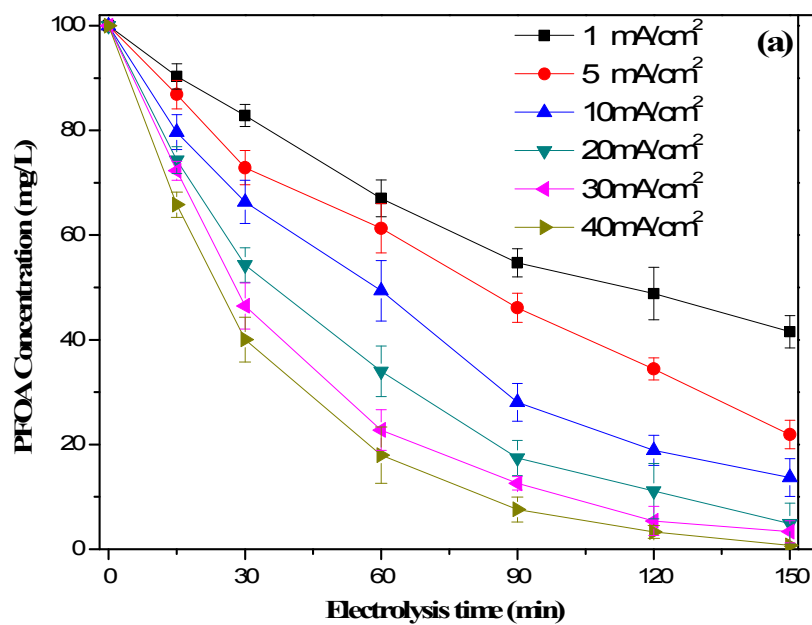


Fig. 3(a) PFOA concentration as a function of electrolysis time at current density

1, 5, 10, 20, 30, 40 mA/cm<sup>2</sup>. Initial pH 5, plate distance 5 mm, 0.1 M Na<sub>2</sub>SO<sub>4</sub>,



T=25°C. (b) COD removed and average current efficiency (ACE) as a function of current density.

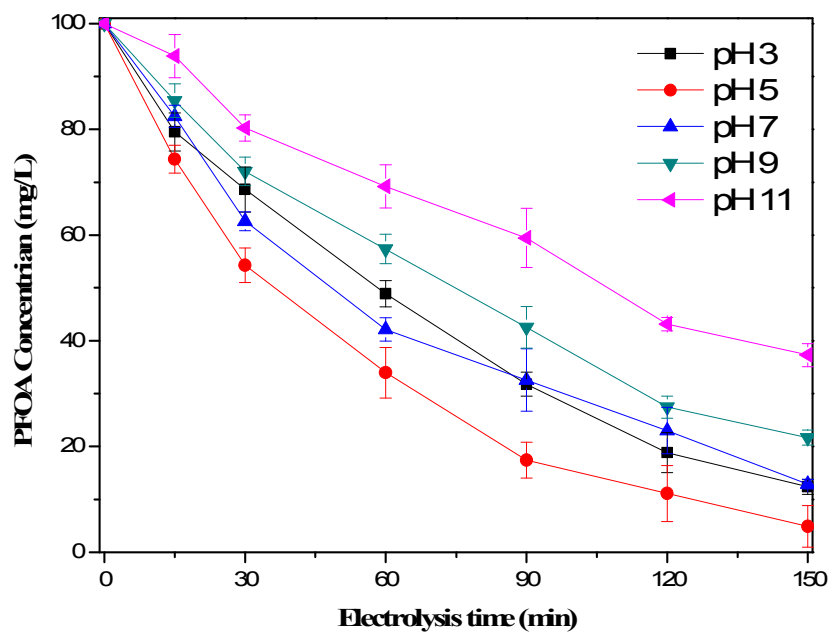
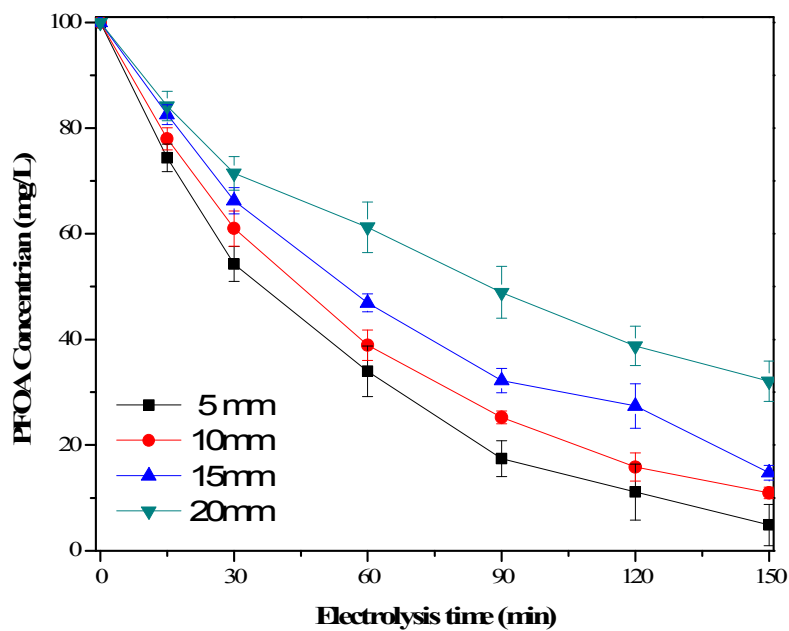
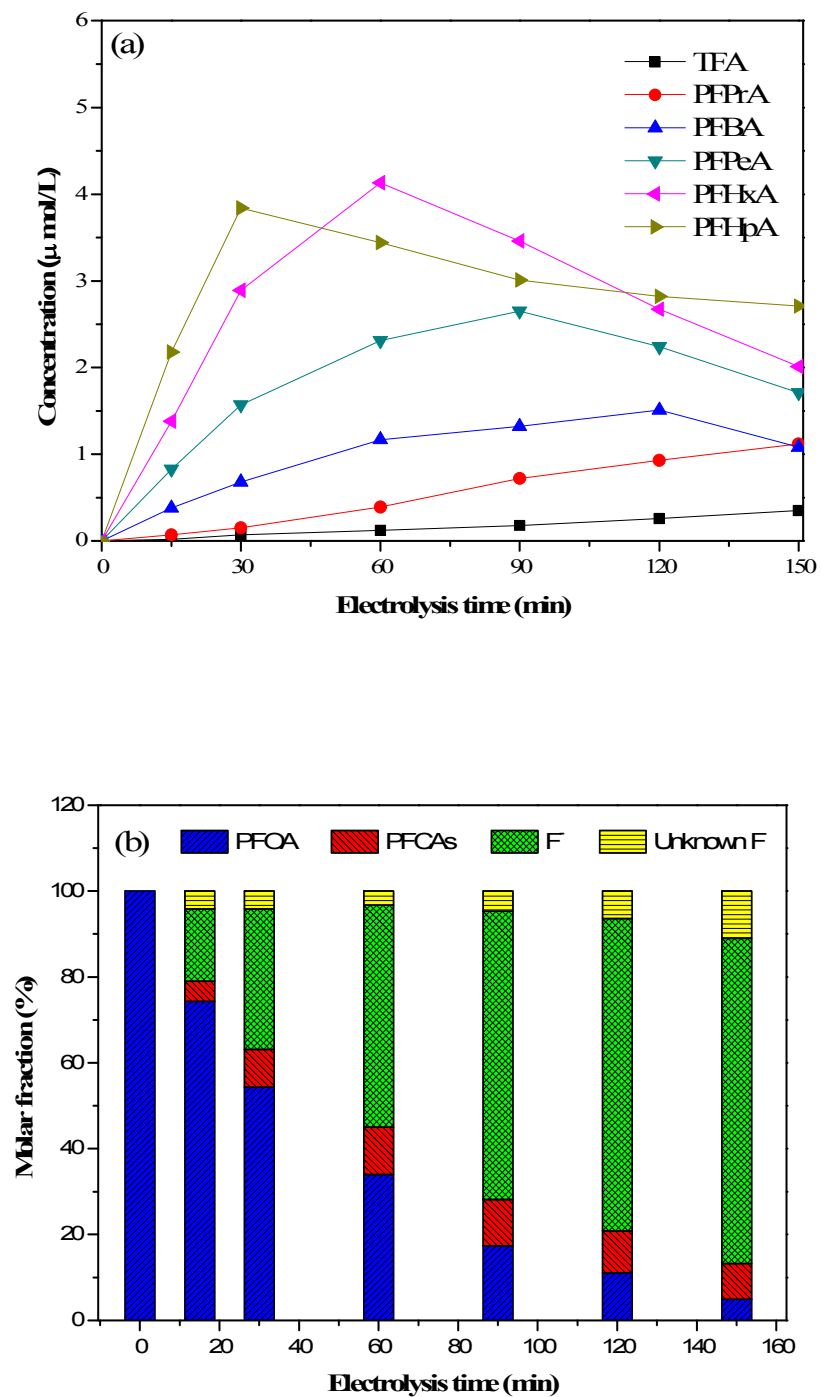


Fig. 4 Effect of initial pH value. Initial concentration 100mg/L, current density 20 mA/cm<sup>2</sup>, plate distance 5 mm, 0.1 M Na<sub>2</sub>SO<sub>4</sub>, T=25 °C.



**Fig. 5** PFOA concentration change as a function of electrolysis time at gap distance of 5, 10, 15, 20 mm. Initial pH 5, current density 20 mA/cm<sup>2</sup>, initial PFOA concentration 100 mg/L, 0.1 M Na<sub>2</sub>SO<sub>4</sub>, T=25 °C.



**Fig. 6 (a) Concentration of intermediates ( $\text{C}_2\text{-C}_7$ ) formed during electrochemical decomposition of PFOA and (b) fluorine element mass balance with the progress of reaction. The operation conditions are given in the caption of Fig. 1.**

**Table. 1 The efficiency and kinetics for PFOA degradation by Ti/SnO<sub>2</sub>-Sb/Yb-PbO<sub>2</sub> electrode. ( electrolysis time: 150 min)**

Parameters		$\eta^a$	$k^b$	$t_{1/2}^c$	$R^{2d}$
Current density (mA / cm <sup>2</sup> )	1	58.50±3.1%	0.0061	113.63	0.991
	5	78.10±2.7%	0.0094	113.63	0.984
	10	86.33±3.6%	0.0135	51.34	0.995
	20	95.11±3.9%	0.0193	35.91	0.995
	30	96.68±2.1%	0.0234	29.62	0.997
	40	99.30±0.2%	0.0306	22.65	0.987
Initial PFOA concentration (mg/L)	10	98.10±0.1%	0.0272	25.48	0.994
	50	97.19±0.7%	0.0230	30.14	0.996
	100	95.11±3.9%	0.0193	35.91	0.995
	200	83.86±2.8%	0.0127	54.58	0.991
Initial pH value	3	87.65±1.4%	0.0139	49.87	0.994
	5	95.11±3.9%	0.0193	35.91	0.995
	7	87.13±0.9%	0.0130	53.32	0.990
	9	78.34±1.4%	0.0103	67.30	0.994
	11	62.71±2.2%	0.0067	103.45	0.988
Gap distance (mm)	5	95.11±3.9%	0.0193	35.91	0.995
	10	89.05±1.1%	0.0151	45.90	0.998
	15	85.23±1.4%	0.0122	56.82	0.986
	20	67.92±3.8%	0.0079	87.74	0.985

Other operating conditions are same as Fig. 3 - 6.

a Degradation ratio of PFOA. (%)

b Pseudo-first-order rate constant of electrochemical degradation. (min<sup>-1</sup>)

c The time of half-left. (min)

d Goodness of fit.