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## ARTICLE

## A novel Fe<sub>3</sub>C/graphitic carbon composite for electromagnetic wave absorption properties in C-band

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Electromagnetic (EM) wave absorber with the characteristic absorption in the millimeter wave range is very important for the EM industry. Especially, the absorption properties in microwave frequency range C-band (4-8 GHz) are necessary in the field of military aircraft. Herein, Fe<sub>3</sub>C/graphitic carbon (Fe<sub>3</sub>C/GC) composite has been synthesized through a low-cost and facile ion-exchanged route. The Fe<sub>3</sub>C/GC could exhibit excellent EM wave absorption properties in C-band with the frequency range of 4-8 GHz and also exhibits good dielectric loss, which could be attributed to the existence of lightweight GC in the composite. The reflection loss value of Fe<sub>3</sub>C/GC composite exceeds -10 dB in the frequency range of 4-8 GHz with a absorber thickness of 2-4 mm, implying its potential application of lightweight EM wave absorber in C-band. Moreover, the Fe<sub>3</sub>C/GC shows better electromagnetic wave absorption properties than other iron compound GC-based composites, such as Fe<sub>2</sub>N/GC and Fe/GC.

### Introduction

Electromagnetic (EM) absorbing materials have attracted interesting attention because of its potential applications in the EM industry, such as military aircraft, radar and wireless communications.<sup>1,2</sup> Considerable investigations have been focused on the effective EM wave absorption materials with the properties of wide frequency range, strong absorption, low density and high resistivity.<sup>3</sup> Metal oxides, such as Fe<sub>3</sub>O<sub>4</sub>,<sup>1</sup> ZnO,<sup>4</sup> MnO<sub>2</sub>,<sup>5</sup> BaTiO<sub>3</sub>,<sup>6</sup> and TiO<sub>2</sub>,<sup>7</sup> have been widely used in EM wave absorbing area. Although they have the advantages of low cost, easily preparation and non-toxicity, the nature of low efficient EM wave absorption properties would restrain their further applications.<sup>8</sup> In addition, magnetic particles and the magnetic particles coated with a nonmagnetic insulator have attracted particular interest, such as Fe/Ni,<sup>9</sup> carbonyl iron,<sup>10</sup> FeCuNbSiB,<sup>11</sup> hybrid structure of SiC/Co,<sup>12</sup> Fe/Y<sub>2</sub>O<sub>3</sub>,<sup>13</sup> and Fe/ZnO.<sup>14</sup> However, the high density and matching thick thickness of these materials would limit their applications in practice.

Recently, lightweight carbon-based materials have exhibited significant value in the EM wave absorbing material due to their good conductive, chemical inertness and high temperature resistance.<sup>15,16</sup> Among these, carbon-coated Ni or Fe nanocapsules are promising in the field of EM wave

absorption.<sup>17</sup> Moreover, carbon nanotubes (CNTs)-Fe (Co, Ni) composites have also been widely applied in EM wave-absorption area.<sup>18-20</sup> However, most of the research works are focused on the frequency range of Ku-band (12.4–18 GHz) and S-band (2.0–4.0 GHz).<sup>21</sup> It is still a challenge to obtain the materials which could exhibit good reflection loss with small matching thickness in C-band (4.0–8.0GHz). The absorption properties in microwave frequency C-band are essential in many fields, including satellite, aerospace and civil use. Hence, it is necessary to exploit new lightweight materials with excellent EM wave absorption properties in the C - band.

In this work, the Fe<sub>3</sub>C/graphitic carbon (Fe<sub>3</sub>C/GC) composite has been synthesized by our previous large-scale and facile ion-exchanged route.<sup>22</sup> The Fe<sub>3</sub>C/GC composite is investigated in terms of complex permittivity and permeability. Herein, it's the first time of the Fe<sub>3</sub>C/GC composite applied in EM wave absorption area, and the corresponding reflection loss value of the composite could exceed -10 dB in 4-8 GHz frequency range with the absorber thickness of 2-4 mm. We also compared the EM wave absorption properties of Fe<sub>3</sub>C/GC composite with other composites, including Fe<sub>2</sub>N/GC and Fe/GC.

### Experimental

#### Synthesis

The Fe<sub>3</sub>C/GC composite was synthesized by our previous ion-exchanged route.<sup>22</sup> In a typical synthesis, 0.12 mol/L FeCl<sub>2</sub> solution was exchanged with 9 g polyacrylic weak-acid cation-exchanged resin (AC) under stirring at room temperature for 16 h. After centrifugation, washing and drying, the AC-Fe<sup>2+</sup> precursor were formed. Finally, the precursor was heated at 800 °C for 1 h under nitrogen atmosphere with a heating rate of 5 °C/min to prepare Fe<sub>3</sub>C/GC composite. To investigate the wave-absorption

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performance of different iron-crystal, the Fe/GC composite was synthesized by carbonizing AC-Fe<sup>2+</sup> precursor at 1100 °C under nitrogen ambient. Also, the Fe<sub>2</sub>N/GC composite was synthesized by pyrolysis the AC-Fe<sup>2+</sup> precursor at 800 °C under the mixture of nitrogen and ammonia for comparison.

## Characterizations

X-ray powder diffraction (XRD) patterns were obtained by a Rigaku D/max-III B diffractometer using Cu K $\alpha$  radiation ( $\lambda = 1.5406 \text{ \AA}$ ). The transmission electron microscopy (TEM) experiment was performed on a JEM-2100 electron microscope (JEOL, Japan) with an acceleration voltage of 200 kV. Carbon coated copper grids were used as the sample holders. Thermogravimetric analysis was performed on a TG (TA, Q600) thermal analyzer under air with a heating rate of  $10 \text{ }^\circ\text{C}\cdot\text{min}^{-1}$ . Fourier-transform infrared spectra (FTIR) of the samples were acquired with a PE Spectrum One BIR spectrometer. Magnetization was measured at 300 K in a physical properties measurement system (PPMS, Quantum Design Inc.) up to a field of (20 kOe).

The composite samples used for the measurement of relative permittivity ( $\epsilon_r = \epsilon' + j\epsilon''$ ) and permeability ( $\mu_r = \mu' + j\mu''$ ) were prepared by mixing the products and paraffin wax in a mass ratio of 7:3. The complex permittivity and permeability of the mixtures in a frequency range of 2 to 18 GHz were evaluated using an Agilent N5244A vector network analyzer. The reflection loss (RL) was calculated according to the following equations.

$$\epsilon_r = \epsilon' + j\epsilon'' \quad (1)$$

$$\mu_r = \mu' + j\mu'' \quad (2)$$

$$Z_{in} = \sqrt{\frac{\mu_r}{\epsilon_r}} \tanh \left[ j \frac{2\pi f d \sqrt{\mu_r \epsilon_r}}{c} \right] \quad (3)$$

$$RL = 20 \log \left| \frac{Z_{in} - 1}{Z_{in} + 1} \right| \quad (4)$$

Where  $f$  is the frequency of the EM wave,  $d$  is the thickness of the absorber,  $c$  is the velocity of light;  $Z_{in}$  is the input impedance of the absorber.

## Results and discussion

The synthetic process of the Fe<sub>3</sub>C/graphitic carbon (Fe<sub>3</sub>C/GC) composite is shown in Fig. 1. Firstly, the AC resin exchanged with Fe<sup>2+</sup> ions to form AC-Fe<sup>2+</sup> precursor. After carbonization, the Fe<sub>3</sub>C/GC could be obtained. TEM is a useful tool to characterize the morphology of nanostructures. As shown in Fig. 2a, the synthetic Fe<sub>3</sub>C/GC composite is composed of Fe<sub>3</sub>C nanoparticles with the diameter between 50 and 200 nm dispersed on graphitic carbon surface. The dark spherical particles are attributed to the Fe<sub>3</sub>C phase. The magnified image in Fig. 2b further indicates the graphitic carbon in the composite existed in the form of nanosheets and

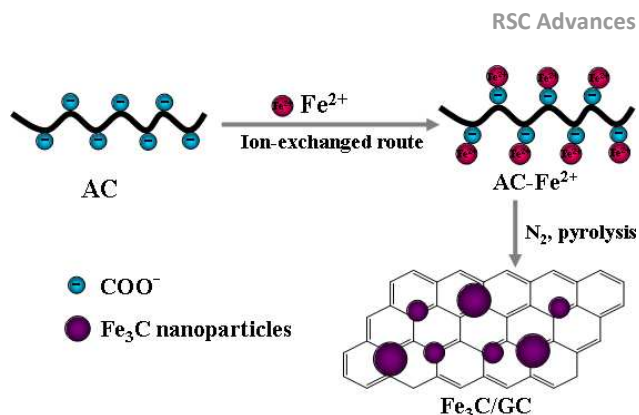


Fig. 1. The synthetic process of Fe<sub>3</sub>C/GC composite

nanobelts. It is better to observe the structure on a high resolution and Fourier transform (FT) images (Fig. 2c and 2d). The interlayer spacings of 0.21 and 0.34 nm are ascribed to the planes of Fe<sub>3</sub>C(211) and C(002), respectively.

The XRD pattern of the Fe<sub>3</sub>C/GC composite shows in Fig. 3a. The obvious diffraction peak at  $2\theta = 26.4^\circ$  is assigned to the (002) plane of graphitic carbon (JCPDS No. 41-1487). The other diffraction peaks at around  $2\theta = 37.8^\circ, 39.9^\circ, 40.7^\circ, 42.9^\circ, 43.7^\circ, 44.6^\circ, 45.1^\circ, 46.0^\circ, 48.7^\circ$  and  $49.1^\circ$  are attributed to the (210), (002), (201), (211), (102), (220), (031), (112), (131), and (221) planes of Fe<sub>3</sub>C phase (JCPDS No.89-2867), respectively. As compared, the composite with different iron phase was also synthesized, namely Fe/GC and Fe<sub>2</sub>N/GC composites (see experiment section). As shown in Fig. 3b and 3c, it can be seen that the Fe/GC and Fe<sub>2</sub>N/GC are composed of  $\alpha$ -Fe and graphitic carbon, Fe<sub>2</sub>N and graphitic carbon, respectively. Raman was used to further investigate the carbon phase in composite (Fig. S1, ESI). The Raman spectra of all the composites are characterized by three main featured peaks, namely 1366 (D-band), 1580 (G-band) and  $2730 \text{ cm}^{-1}$  (2D-band). The D-band is ascribed to the vibrations of carbon atoms with dangling bonds in

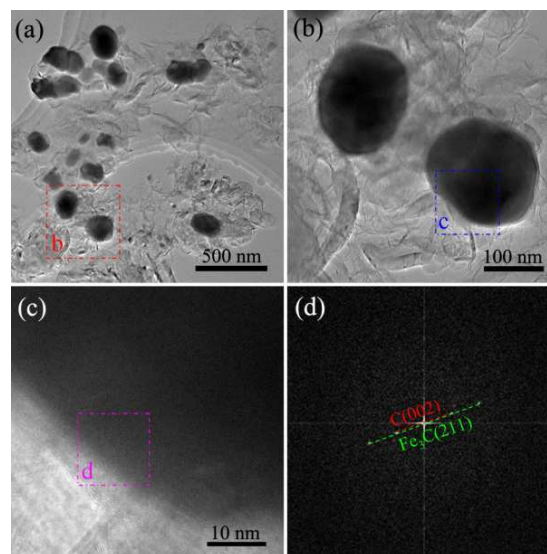


Fig. 2 (a-b) TEM and (c) HRTEM images of Fe<sub>3</sub>C/GC composite. (d) The Fourier transform (FT) image of (c).

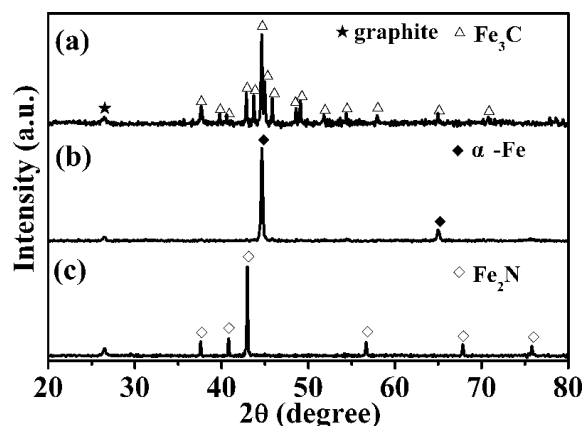


Fig. 3 XRD patterns of (a)  $\text{Fe}_3\text{C}/\text{GC}$ , (b)  $\text{Fe}/\text{GC}$  and (c)  $\text{Fe}_2\text{N}/\text{GC}$  composites.

disordered graphite planes and the defects incorporated into pentagon and heptagon graphite-like structures, while the G-band is attributed to the stretching modes of carbon  $\text{sp}^2$  bonds of the graphite ( $\text{E}_{2g}$  mode). The G peak is much higher in intensity and narrower in width compared to the D peak, implying the well crystalline of the graphitic carbon in the composites. The second-order 2D-band is typical of graphitic carbon. Moreover, the intensity ratio between G-band and D band ( $I_G/I_D$ ) is proportional to the graphitization degree of carbon.  $I_G/I_D$  values for  $\text{Fe}_3\text{C}/\text{GC}$ ,  $\text{Fe}/\text{GC}$  and  $\text{Fe}_2\text{N}/\text{GC}$  are about 3.52, 3.61 and 4.01, respectively, also indicating the well crystalline of the graphitic carbon in the synthetic composites.

The magnetization curves of the synthetic composites were investigated at 300 K and 20 kOe (Fig. S2, ESI). The saturation magnetization and coercivity of the  $\text{Fe}_3\text{C}/\text{GC}$  composite are about 17.72 and 0.5 emu/g, respectively. The  $\text{Fe}_3\text{C}/\text{GC}$  composite displays a very low coercivity of 100 Oe at room temperature and 20 kOe. The negligible coercivity and remanence demonstrate a superparamagnetic behavior of the  $\text{Fe}_3\text{C}/\text{GC}$  composite. The hysteresis loops for  $\text{Fe}/\text{GC}$  and  $\text{Fe}_2\text{N}/\text{GC}$  composites display zero coercivity with no remanence, indicating the superparamagnetic behaviour of the samples. The saturation magnetization of  $\text{Fe}_3\text{C}/\text{GC}$ ,  $\text{Fe}_2\text{N}/\text{GC}$  and  $\text{Fe}/\text{GC}$  composites are about 17.72, 40.30 and 54.19 emu/g, respectively.

To calculate the GC content of the three composites, TGA analyses under air have been performed in the revised manuscript (Fig. S3 and Table S1). The GC content in  $\text{Fe}_3\text{C}/\text{GC}$ ,  $\text{Fe}_2\text{N}/\text{GC}$  and  $\text{Fe}/\text{GC}$  composites are about 40.3 wt%, 38.1 wt% and 44.1 wt%, respectively, indicating the similar GC content in the three composites.

Graphitic carbon (GC) is a typical microwave absorbing material for dielectric loss, so the magnetic nanoparticles/GC composite has dual-loss characteristics. Moreover, the existence of GC in the magnetic composite greatly effect on the electronic and magnetic properties of materials. Therefore, the magnetic nanoparticles/GC composite may exhibit good EM absorption properties. To understand the possible microwave absorption mechanism, the real ( $\epsilon'$ ) and imaginary part ( $\epsilon''$ ) of the relative permittivity for the composites were investigated in the frequency range of 2~18 GHz. As shown in Fig. 4a and 4b, the real ( $\epsilon'$ ) and imaginary ( $\epsilon''$ ) part of

the relative permittivity of the  $\text{Fe}_3\text{C}/\text{GC}$  composite exhibits a decrease tendency in the frequency range of 2–18 GHz with a small fluctuation. However, the  $\epsilon'$  value of  $\text{Fe}_2\text{N}/\text{GC}$  composite is increase in the frequency range of 3–6.5 GHz, the  $\epsilon''$  value of  $\text{Fe}_2\text{N}/\text{GC}$  and  $\text{Fe}_3\text{C}/\text{GC}$  composite exhibits an increase tendency in

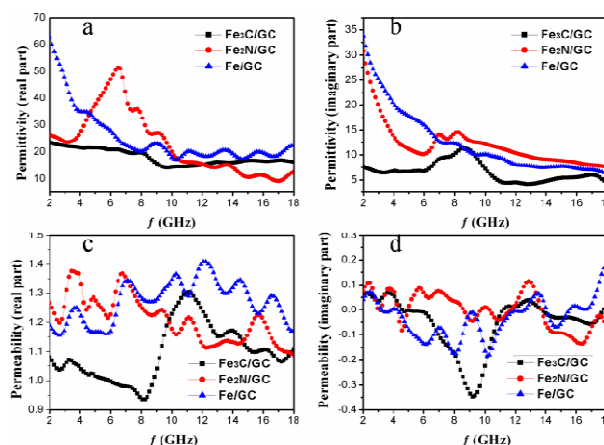


Fig. 4 (a) Real and (b) imaginary parts of relative permittivity; (c) Real and (d) imaginary parts of relative permeability for mixed paraffin wax with composite (weight fraction of 70%).

the frequency range of 3–6.5 GHz. According to the free electron theory,<sup>23</sup>  $\epsilon'' = 1/2\pi\epsilon_0\rho f$ , where  $\rho$  is the resistivity. The low  $\epsilon''$  value indicates a higher electric resistivity, which is attributed to the magnetic  $\text{Fe}_3\text{C}$  nanoparticles coated by GC in the composite. The  $\epsilon''$  value of the  $\text{Fe}_3\text{C}/\text{GC}$  composite in the range of 2 to 18 GHz is close to the reported carbon/ferrite composites<sup>24</sup> and (Fe, Ni)/C nanocapsules,<sup>25</sup> suggesting that the synthetic  $\text{Fe}_3\text{C}/\text{GC}$  composite exhibits strong dielectric loss against EM wave. Although the resistivity of the bulk graphite is about  $7.5 \times 10^{-6} \Omega\cdot\text{m}$ , which is close to that of metallic magnets ( $10^{-6}$ – $10^{-8} \Omega\cdot\text{m}$ ),<sup>26</sup> it is expected that the electrical resistivity may increase owing to the curving graphite shells with a thickness of several nanometers exhibits the special microstructure and defect properties.<sup>27</sup> Different magnetic materials may exhibit different dielectric loss performances. The magnetic  $\text{Fe}_3\text{C}$  nanoparticles in the cavities of GC may increase the electric resistivity, and the protective graphite shell plays a role as

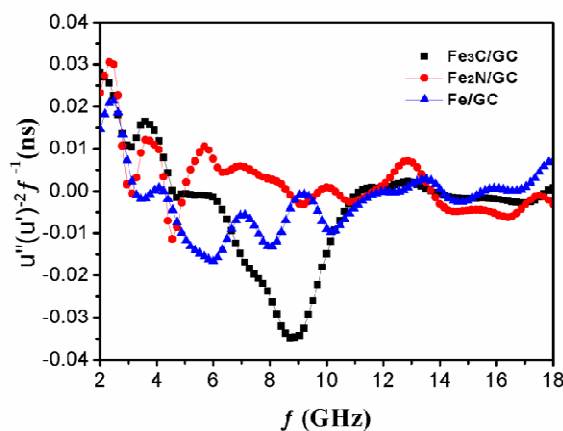


Fig. 5 Values of  $\mu''(\mu')^{-2}f^{-1}$  for the composites vs frequency.



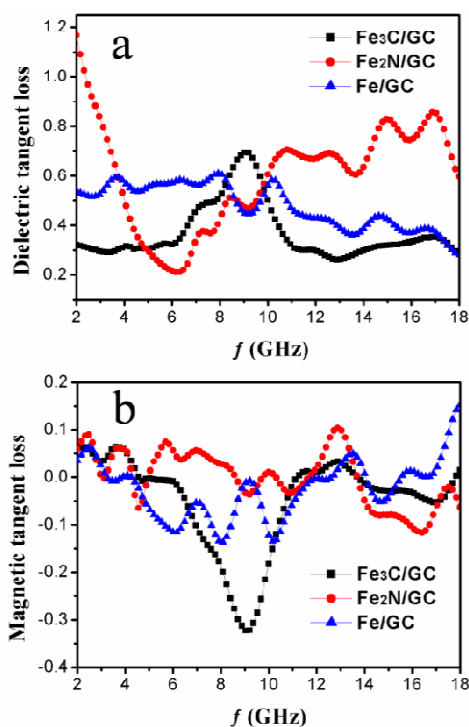


Fig. 6 (a) dielectric loss tangents and (b) Magnetic loss tangents of mixed paraffin wax with composite for weight fraction of 70 %.

an insulator in the composite. Compared with  $\text{Fe}_2\text{N}/\text{GC}$  and  $\text{Fe}/\text{GC}$  composites, the relatively lower  $\epsilon''$  values of the  $\text{Fe}_3\text{C}/\text{GC}$  is attributed to the performance of  $\text{Fe}_3\text{C}$  is different from that of  $\text{Fe}_2\text{N}$  and  $\text{Fe}$ .

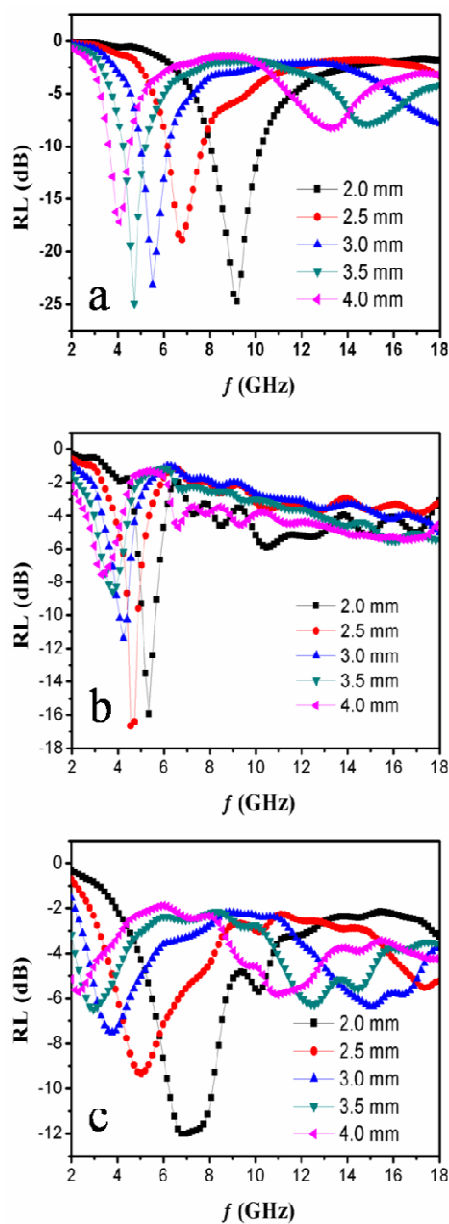
The frequency dependence of the real part ( $\mu'$ ) and imaginary part ( $\mu''$ ) of relative permeability of the composites are shown in Fig. 4c and 4d. It can be seen that the  $\mu'$  value of  $\text{Fe}_2\text{N}/\text{GC}$  and  $\text{Fe}/\text{GC}$  composites exhibit a decrease tendency in the frequency of 2–18 GHz with a small fluctuation. Only the  $\mu'$  value of the  $\text{Fe}_3\text{C}/\text{GC}$  composite is significantly increase in the range of 8–11 GHz. The  $\mu''$  values of the  $\text{Fe}_2\text{N}/\text{GC}$  and  $\text{Fe}/\text{GC}$  composites are fluctuates around zero, whereas the minimum  $\mu''$  value of  $\text{Fe}_3\text{C}/\text{GC}$  composite appears at 9.2 GHz. The maximum value of  $\mu''$  appeared at 3.6 GHz, implying the natural resonance occurred in the  $\text{Fe}_3\text{C}/\text{GC}$  composite. It has been shown that the electromagnetic transformation is associated with the energy transfer between vectors of electric and magnetic fields, and further gives rise to the resonance behavior when their energy states satisfy the matching with the frequency of the electromagnetic wave. The negative values of the imaginary part indicate that the loss associated with the magnetic vector is even smaller than those needed for the permeability in medium, probably aroused by the radiation and/or transfer of energy.<sup>28</sup> The natural resonance equation is as followed:  $2\pi f_r = \gamma H_a$ ,<sup>29</sup> where  $\gamma$  is the gyromagnetic ratio,  $H_a$  is the anisotropy field, and  $f$  is the resonance frequency. Therefore, the decrease of the relative permeability of  $\text{Fe}_3\text{C}/\text{GC}$  composite is attributed to the lower magnetization value of  $\text{Fe}_3\text{C}$  than that of  $\text{Fe}$  and the magnetic dilution of  $\text{GC}$ . In fact, the anisotropic energy of small-sized particles, especially in the nano-scale, could remarkably increase

because of the surface anisotropic field affected by the small size effect.<sup>9</sup>

The eddy current loss phenomenon is related to thickness ( $d$ ) and the electric conductivity ( $\sigma$ ) of the composites, which can be expressed by the followed equation:<sup>30</sup>

$$\mu''(\mu')^{-2} f^{-1} = 2\pi\mu_0 d^2 \sigma$$

where  $\mu_0$  is the vacuum permeability. Fig. 5 shows the calculated values of  $\mu''(\mu')^{-2} f^{-1}$  changed with the frequency. Generally, the magnetic loss of material mainly originates from natural resonance, exchange resonance and eddy current loss in the microwave region. If the magnetic loss is mainly determined by eddy current loss, the value of  $\mu''(\mu')^{-2} f^{-1}$  should be a constant. Based on the above, it



**Fig. 7** Reflection loss curves of composite at different thickness, consisting of mixed paraffin wax with composite for weight fraction of 70%. (a) Fe<sub>3</sub>C/GC (b) Fe<sub>2</sub>N/GC (c) Fe/GC.

can be concluded that the eddy current loss doesn't play a dominant role in the magnetic loss of the present composites. The low value of  $\mu''(\mu')^{-2}f^{-1}$  is attributed to the GC as a separator for suppressing the eddy current loss.<sup>20</sup>

There are two possible contributions for microwave absorption, namely, dielectric loss ( $\tan\delta_\epsilon = \epsilon''/\epsilon'$ ) and magnetic loss ( $\tan\delta_\mu = \mu''/\mu'$ ). The dielectric loss tangent values of the three composites are different as shown in Fig. 6a. The dielectric loss tangent value of Fe<sub>2</sub>N/GC composite is decreased in the frequency range of 2–6.5 GHz, and the loss tangent value of Fe<sub>3</sub>C/GC composite appears a characteristic peak at 9 GHz. However, the value of Fe/GC composite has no obvious change in the frequency range of 2–18 GHz.

The maximum magnetic loss tangent ( $\tan\delta_\mu = \mu''/\mu'$ ) value of Fe<sub>3</sub>C/GC is about 0.03, which is similar to the Fe/GC of 0.05 and Fe<sub>2</sub>N/GC of 0.10 (see Fig. 6b). However, all the three composites appear negative values of magnetic loss tangent at 2–18 GHz, which indicates the microwave absorption brings no magnetic loss. The results demonstrate that the dielectric loss plays a dominant role in the three composites. Therefore, the EM attenuation mechanism of the three composites is mainly dependent on the dielectric loss, which is different from the previous reports about the magnetic loss has been regarded as the reason of the main loss.<sup>12–14</sup> The magnetic loss tangent ( $\tan\delta_\mu = \mu''/\mu'$ ) value of Fe<sub>3</sub>C/GC is -0.33 at 9.2 GHz, indicating no magnetic loss contribution to the microwave absorption. However, the maximum dielectric loss tangent value of Fe<sub>3</sub>C/GC composite is 0.7 at 9.2 GHz, which endows the Fe<sub>3</sub>C/GC composite an outstanding microwave absorption property.

Fig. 7 shows the frequency dependence of reflection loss for the sample/paraffin wax composites in the frequency range of 2–18 GHz at different thickness. The three composites have excellent EM wave absorption properties in C-band (4–8 GHz). Especially, Fe<sub>3</sub>C/GC composite has the highest EM wave absorption properties. It can be observed that the minimum reflection loss of the Fe<sub>3</sub>C/GC composite is -26 dB at 9.2 GHz and the absorption range at -10 dB is from 8–10 GHz with a 2 mm thick layer. The frequency range is quite broader than that of the previously report for a single thickness.<sup>18</sup> Additionally, the minimum reflection loss obviously shifts to the low frequency range with the increase of layer thickness, and the optimum reflection loss of the different thickness layers is concentrated in the low frequency region. The Fe<sub>3</sub>C/GC composite exhibits much better microwave absorption properties in C-band than the reported magnetic composites, including Fe/SmO,<sup>12</sup> Fe/Y<sub>2</sub>O<sub>3</sub>,<sup>13</sup> Fe/CNTs<sup>18</sup> and CoFe<sub>2</sub>O<sub>4</sub>/CNTs.<sup>31</sup>

The magnetic loss tangents of three composites are almost the same, but the corresponding reflection loss values are different, which is may be related to their different dielectric loss tangent caused by different electric resistivity. The Fe<sub>3</sub>C/GC composite has the most excellent EM wave absorption properties in C-band (4–8 GHz), indicate that the absorbing performance is determined by the matching degree between dielectric loss ( $\tan\delta_\epsilon = \epsilon''/\epsilon'$ ) tangent and magnetic loss tangent ( $\tan\delta_\mu = \mu''/\mu'$ ). The excellent microwave absorption properties in C-band may be proper

combination of the complex permeability and permittivity resulting from the composite of magnetic nanoparticles and GC.

## Conclusions

The Fe<sub>3</sub>C/GC composite synthesized through a low-cost and scaled-up route exhibited better EM wave absorption properties in C-band (4–8 GHz) than that of the Fe<sub>2</sub>N/GC and Fe/GC composites. The minimum reflection loss of Fe<sub>3</sub>C/GC composite reaches -26 dB and its absorption range under -10 dB is between 4 to 8 GHz with a thickness layer of 2 mm. The excellent microwave absorption properties of Fe<sub>3</sub>C/GC composite could be attributed to the high dielectric loss of light weight graphitic carbon. The composite exhibited well performance of EM wave-absorption in C-band, which may have potential applications in military aircraft, radar and wireless communications.

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