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Nanocomposites of Graphene/Polymers: A Review

Chee W.K.¹, Lim H. N.^{1,2,*}, Huang N.M.³, Harrison I.⁴

¹Department of Chemistry, Faculty of Science, Universiti Putra Malaysia, 43400 UPM
Serdang, Selangor, Malaysia

²Functional Device Laboratory, Institute of Advanced Technology, Universiti Putra Malaysia,
43400 UPM Serdang, Selangor, Malaysia

³Low Dimension Materials Research Centre, Department of Physics, Faculty of Science,
University of Malaya, Kuala Lumpur 50603, Malaysia

⁴Faculty of Engineering, The University of Nottingham Malaysia Campus, Jalan Broga,
43500 Semenyih, Selangor, Malaysia

*Corresponding author. Tel: +60 3 8946 7494

E-mail address: janet_limhn@yahoo.com

Abstract

This paper essentially reviews the types of graphene-based nanofillers and the fabrication of graphene/polymer nanocomposites. Routes to produce the graphene materials, along with the methods and modifications used to efficiently disperse the graphene nanofillers within the polymer matrices are discussed. In addition, the mechanical properties, morphological, structural, electrical conductivities, electrochemical activities, thermal stabilities, and gas barrier properties are evaluated, along with the direct relationships of these properties with the graphene-polymer interaction and their dispersion in the polymer matrix. Finally, a brief summary of the practical applications of polymeric-graphene materials along with the current

1 trends in the field is presented to progressively show future prospects for the development of
2 these materials.

3 Keywords: Graphene; graphene oxide; polymer nanocomposites; polymeric materials

4

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- 14 Summary and perspectives

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16

17 List of Abbreviations

Abbreviation	Character
ATRP	Atom transfer radical polymerization
LDPE	Low density poly(ethylene)
GO	Graphene oxide
CNT	Carbon nanotubes
PHA	Polyhydroxyalkanoates

PPy	Polypyrrole
PAC	Polyacetylene
PANI	Polyaniline
PEDOT	Poly(3,4-ethylenedioxythiophene)
PTFE	Polytetrafluoroethylene
DMF	N,N-dimethylformamide
GCE	Glassy carbon electrode
ITO	Indium-doped Tin oxide glass
RAFT	Reversible addition-fragmentation chain transfer polymerization
SET-LRP	Single-electron transfer living radical polymerization
NMRP	Nitroxide-mediated radical polymerization
PLA	Poly(lactic acid)
PDLA	Poly(D-lactide)
RGO	Reduced graphene oxide
PAN	Polyacrylonitrile
PVA	Polyvinylalcohol
Pt	Platinum
TEM	Transmission electrode microscope
COST/GO-n	Chitosan/oxidized starch/graphene oxide
DMAC	N,N-dimethylacetamide
LiCl	lithium chloride
GO-g-PDLA	Graphene oxide-grafted-PDLA
PLLA	Poly(L-lactide)
FT-IR	Fourier-transform infrared spectroscopy
PS	Polystyrene
SDS	Sodium dodecyl sulfate
UV-Vis	UV-visible spectroscopy
GNS	Graphene nanosheets
Ag/AgCl	Silver/ silver chloride reference electrode
H ₂ SO ₄	Sulphuric acid
VTES	Vinyl triethoxysilane
SA	stearic acid
SA-g-RGO	Stearic acid-grafted-RGO
PET	Poly(ethylene terephthalate)
PE	Poly(ethylene)
PNIPAM	Poly(N-isopropylacrylamide)
PMMA	Poly(methyl methacrylate)
CMG	Chemically reduced graphene oxide
NMR	Nuclear magnetic resonance spectroscopy
PGMA	Poly(glycidyl methacrylate)
TEM	Transmission electron microscope
OBD	Organic bistable device
PCL	Poly(caprolactone)
PVDF	Polyvinylidene fluoride
PU	Polyurethane
THF	Tetrahydrofuran
WPU	Waterborne polyurethane
FGS	Functionalized graphene nanosheets

GONS	GO nanosheets
HPU	Hyper-branched polyurethane
MEGO	Microwave-exfoliated graphite oxide
f-GO	Functionalized graphene oxide
PEO	Poly(ethylene oxide)
XRD	X-ray diffraction spectroscopy
AFM	Atomic force microscopy
PI	Polyimide
OTR	Oxygen transfer rate
WVTR	water-vapor transmission rate
DMSO	Dimethyl sulfoxide
PC	Polycarbonate
VASA	Vacuum-assisted self-assembly
CV	Cyclic Voltammetry
SSE	Silver/ silver sulfate electrode
PABS	Poly(3-aminobenzene sulfonic acid)
Wt%	Weight percentage

1

2 1. Introduction

3 Graphene and graphene oxide (GO) have been widely studied for use in a variety of
4 applications because of their excellent electrical conductivity and superb mechanical
5 properties¹. These properties arise from the two-dimensional crystallographic nature of
6 graphene: a one-atom thick sheet of sp² bonded carbon atoms packed in a honeycomb crystal
7 structure(see Figure 1a)². The theoretical tensile strength and Young's modulus of graphene
8 have been measured to be 130 GPa and 1.0 TPa, respectively³. The tensile strength of
9 graphene is therefore much higher than that of nano-sized steel or carbon nanotubes (CNT).
10 The measured electrical and thermal conductivities are approximately 7200 Sm⁻¹ and ⁴ 1800
11 W m⁻¹K⁻¹, respectively^{5,6}. Although individual CNT also possessed very high electrical and
12 thermal conductivity (1, 000 000Sm⁻¹ and 2500 W m⁻¹K⁻¹ specifically), the properties of bulk
13 material heavily depended on how the CNTs are organized⁷. The specific control over the
14 position of CNT is often difficult due to intrinsic difficulties in handling individual nanotubes.
15 Therefore, these properties along with the large specific area (2630 m²g⁻¹) and the ability to
16 modify the behavior of the underlying graphene by the use of polymer composites, have

1 integrated this material in energy storage systems, biological or physical sensors, and
2 biomedical applications ⁸.

3 Generally, graphene oxide is produced using the method of Brodie ⁹, Staudenmaier ¹⁰, or
4 Hummer¹¹. All three methods involve an oxidation reaction of graphite, followed by the
5 exfoliation. The exact chemical form of graphite oxide is unknown, but it is widely accepted
6 that graphite oxide has oxygen functional groups that are responsible for its hydrophilic
7 characteristics and allow it to be exfoliated to form graphene oxide (Figure 1b) in many polar
8 solvents. The formation of graphene platelets, or more exactly reduced graphene oxide,
9 requires a reduction process. Several methods have been reported in the literature, including
10 chemical reduction using reducing agents ^{12, 13}, thermal treatment ¹⁴⁻¹⁶, and electro-chemical
11 reduction ^{17, 18}. The oxygen function groups remaining on the graphene platelet after the
12 reduction step will have a significant effect on its properties. Consequently, the process of
13 forming graphene platelets is still an active research area.

14 Polymers are an important class of materials in today's society; they are relatively
15 cheap and easy to process ¹⁹. Common synthetic polymers include polyolefin (polyethylene,
16 polypropylene, etc.), polycarbonate, poly(methyl methacrylate), polyimide, poly(vinyl
17 alcohol), and polyurethane . However, their physical properties limit their application in some
18 areas. The incorporation of graphene into polymeric chains can improve the mechanical or
19 electronic properties. For example, graphene has been used to enhance the mechanical
20 strength ^{12, 20, 21} of polymers, as well as to impart electrical conductivities ^{16, 22, 23}, enhance
21 their thermal stabilities ^{24, 25}, improve their electrochemical activity ²⁶⁻²⁸, as well as impart gas
22 barrier properties ^{29, 30} whereby the significant impact of graphene addition was discussed in
23 detail in a very recent review article by Xu et al. ³¹. Although synthetic polymers are widely
24 used, they have a significant negative environmental impact because they are not
25 biodegradable, and often the base chemicals are derived from petroleum. For example, the

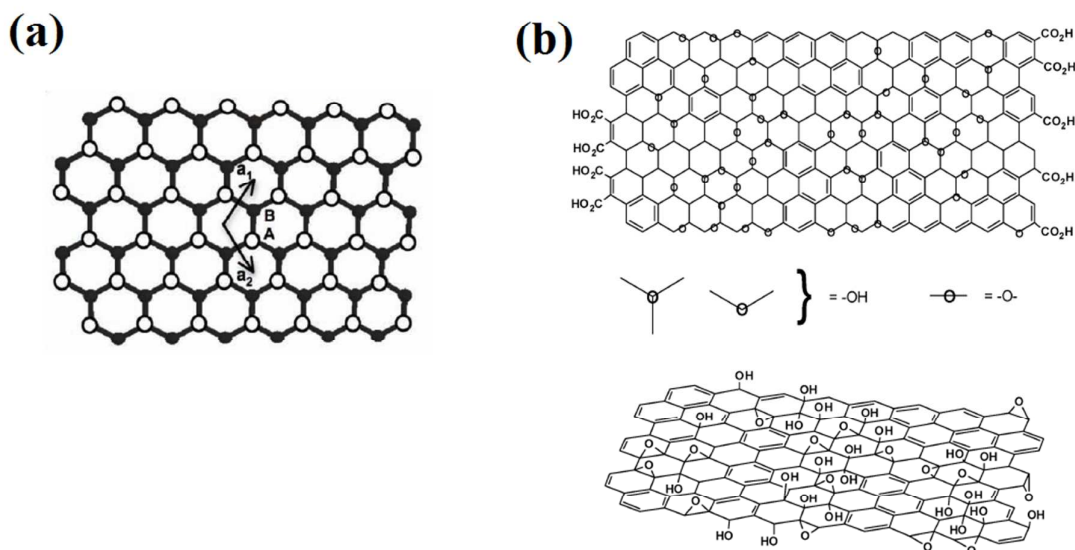
1 worldwide use of polyolefin has been reported to produce a total of approximately 140
2 million tons of industrial waste products each year ³². To overcome these environmental
3 concerns, natural polymers are now being investigated as replacements for synthetic non-
4 degradable plastics. The common matrices used to manufacture natural polymers are
5 polysaccharides, proteins, lipids such as fats and oils, polyesters from microorganisms (PHA),
6 chitosan, cellulose, lignin, and those derived from natural monomers such as poly(lactic acid)
7 ³³. However, these polymers often have inferior properties compared to synthetic polymers.
8 Thus, the inclusion of graphene is able to achieve enhanced performance of the main polymer
9 matrices.

10 The increased use of battery-operated appliances in both the commercial and
11 industrial fields has resulted in the search for more effective ways of harvesting energy from
12 the environment, storing energy for later use, delivering power, and improving energy
13 efficiency. Besides being used as a replacement for the semiconductor diode in a solar cell,
14 conducting polymers have specific applications in electrochemical cells, for both energy
15 storage (batteries) and power delivery (supercapacitors) ^{34,35}. Common types of conducting
16 polymers include polypyrrole (PPy), polyacetylene (PAC), polyaniline (PANI), and poly(3,4-
17 ethylenedioxythiophene) (PEDOT) ³⁶⁻⁴². Although these are conducting polymers, their
18 resistivity is too high for some applications. Graphene can be incorporated as an ideal
19 conductive additive into the polymer matrix to further boost the conductivity, in addition to
20 providing mechanical benefits towards the composite structure.

21 Furthermore, numerous articles also reported the incorporation of inorganic materials
22 (mainly metal oxides) or direct synthesis of graphene-based composites with functional
23 polymers and inorganic nanostructures. The development of such specific advanced
24 composites materials were targeted in application of energy storage system including Li-ion
25 batteries and supercapacitors, or even the energy system such as photovoltaic devices and

1 photocatalysis. These scopes were well-addressed in the review articles by Huang et al.⁴³ and
2 Chen et al.⁴⁴, respectively from the standpoint of electrochemistry. It significantly discussed
3 the up-to-date synthesis techniques, along with the electron transfer properties, involving the
4 electronic structure and electron transport within the graphene/ composites nanostructure.

5 Most of the literature published on polymer/graphene nanocomposites has reported
6 significant improvements in the mechanical, thermal, and electrical activities, as well as the
7 conductivities and gas barrier properties, compared to the neat polymer. This positive change
8 even occurs with a small amount of graphene filler^{21, 29, 45-48}. However, the improvement
9 relies heavily on the distribution of the graphene within the polymer matrix, as well as the
10 interfacial bonding between the graphene and the host matrix. The distribution of the
11 graphene within the polymer is significantly affected by the polarity of the polymeric
12 backbone. A hydrophilic polymer may cause the graphene layers to aggregate because of the
13 interactions between the graphene layers and the hydrophilic polymer chains. In contrast,
14 graphene oxide sheets, which have oxygen functional groups heavily bonded to the surface,
15 are more compatible with organic polymers⁴⁹⁻⁵². However, graphene oxide is not suitable for
16 electrical applications because of its electrical insulating properties. Consequently, to enhance
17 the electrical conductivity of polymers, surface modification of the graphene may be required
18 to ensure a homogeneous dispersion of individual graphene sheets in the polymer matrix.



1

2 Figure 1. (a) Schematic diagram of graphene crystal structure. Reproduced with permission
 3 from ref. 2 (Copyright (2010) Wiley) and (b) Lerf-Klinowski model of graphene oxide.

4 Reproduced with permission from ref. 1 (Copyright (2010) RSC)

5

6 2. Polymeric-based graphene/ graphene oxide nanocomposites

7 2.1 Preparation methods

8 2.1.1 Solution cast technique

9 Mainly because of its simplicity, the solution casting technique is one of the most commonly
 10 practiced methods used to manufacture uniformly dispersed nanocomposites. Prior to
 11 dissolving it in the polymer solution, the graphene is dispersed within a solvent by sonication.
 12 The solvent is then removed by evaporation at either an elevated or ambient temperature. The
 13 obtained nanocomposite film is washed with water to remove any residual solvent and further
 14 dried. The solvent chosen must be capable of dissolving the host polymer and be volatile to
 15 encourage fast evaporation. In the preparation of PLA/ graphene nanocomposite⁵³, the host

1 polymer matrix was dissolved in chloroform, while graphene was pre-dispersed in
2 chloroform using sonication technique. Both the polymer and dispersed graphene was mixed
3 via stirring and casted on polytetrafluoroethylene (PTFE) mold. Because of the volatility of
4 chloroform, the solvent was left evaporated at room temperature, followed by vacuum dried
5 at elevated temperature to remove any residual solvents. Additionally, other literatures which
6 utilized similar technique were further reported in this article^{13, 54-56}.

7

8 2.1.2 Melt blending technique

9 Melt blending is another fast and common option used to prepare nanocomposite film. This
10 technique relies heavily on the dis-entanglement of polymer structure during their molten
11 phase. Therefore, the polymer chains are free moving and completely mixed during the
12 melting phase of the polymer. However, the main shortcoming of this technique is on the
13 introduction of solid organic/ inorganic particles into the polymeric phase, particularly when
14 the solid materials having opposite surface characteristic to that of the main matrix. Therefore,
15 several attempts were focused on the surface functionalization (covalent/ non-covalent
16 bonding) towards the particles to achieve better compatibilization between the two-phase
17 system⁵⁷. For instance, the poor distribution of graphene layers within the polymer matrix,
18 caused by the strong force between graphene sheets and the high viscosity of polymers, is
19 overcome by functionalizing graphene sheets with oxygen and hydroxyl functionalities to
20 encourage better interactions between the components²³.

21

22 2.1.3 In-situ polymerization

23 Graphene/polymer nanocomposites are commonly synthesized using in-situ polymerization.

24 The monomer and graphene precursors are initially dissolved in a common solvent and

1 ultrasonicated to achieve a uniform dispersion. An initiator is then added to the mixture to
2 form the polymer. This particular technique can be expanded or varied to form a very wide
3 range of categories and classifications, depending on the type of desired end product, as well
4 as the selected synthesis routes. For instance, a free-radical initiator and reducing agent can
5 be added simultaneously to induce polymerization and at the same time reduce GO to
6 graphene, or achieve ordered layer structure of the desired composites⁵⁸⁻⁶⁰. On the other hand,
7 emulsion polymerization is another type of commonly applied in-situ polymerization
8 technique which differs only at the stage where the formation of the final desired product is in
9 an emulsion form. The advantages of this strategy include its ease of manipulation, simplicity,
10 scalability, low cost, and lower environmental concern⁶¹. Even though various types of
11 emulsion polymerization techniques have been reported and described elsewhere, the
12 common approach is a microemulsion technique in which the final product produces
13 thermodynamically stable polymer particles on the scale of tens of nanometers⁶².
14 Furthermore, additional additives such as surfactants are added to achieve enhanced
15 dispersion of the dispersed components in the continuous matrix or solution, hence creating a
16 fine and evenly dispersed graphene/ polymer particles to form a stable microemulsion.

17

18 2.1.4 Electrospinning

19 Electrospinning can be used to prepare fine composite nano-fibers with average diameters
20 from the nanometer to micrometer range⁶³. The preparation of the precursor mixture involves
21 dissolving the polymer matrices and graphene in a solvent (commonly N,N-
22 dimethylformamide, DMF). The mixture is then electrospun by applying a high positive
23 voltage (5–20 kV) on a syringe needle. During the typical process, the polymer solution held
24 by its surface tension at the end of the syringe needle is subjected to a high-voltage field,

1 whereby a charge is induced on the liquid surface as a result of the high voltage applied, and
2 the mutual charge repulsion induces a force directly opposite to the surface tension⁶⁴. As the
3 voltage increases, the hemispherical surface at the tip of the needle eventually elongates and
4 forms a Taylor cone⁶⁵. When a critical voltage value is reached, the repulsive force
5 overcomes the surface tension of the solution, and a charged jet of the solution is ejected
6 from the tip of the Taylor cone itself. The high-voltage application leads to the formation of
7 ultra-fine composite fibers with diameters in the micrometer to nanometer range⁶⁶, which are
8 electrospun as the solvent evaporates when the jet travels in air, leaving behind the polymer
9 fibers on the collector. The electrospun fibers present interesting properties such as a high
10 surface/volume ratio, leading to a low density and high pore volume, and outstanding
11 mechanical strength. However, the process parameters, as well as the choice of system,
12 including the type and molecular weight of the polymer, polymer viscosity, solvent used,
13 voltage applied, needle to collector distance, and the polymer flow rate often play crucial
14 roles in achieving the desired properties in the nanofibers produced^{67, 68}.

15

16 2.1.5 Electro-deposition

17 Electro-deposition is a simple and fast approach to prepare nanocomposites using
18 electrochemical reactions. The process involves the electro-polymerization of a
19 polymer/graphene composite from an aqueous precursor solution of the monomer, doping
20 agent (if needed), and graphene oxide. Usually the electro-deposition cell has three electrodes:
21 a working electrode onto which the layer is deposited, reference electrode, and counter
22 electrode, which is usually made of platinum. The working electrode consists of an electrical
23 conductive material or substrate (GCE or ITO glass). The electro-deposition of the polymer
24 occurs at a specific potential and stops when an appropriate amount of charge has passed. As
25 a result, a nanocomposite film is formed on the surface of the conductive material.

1 2.2 Modification techniques for graphene and graphene oxide

2 2.2.1 Grafting

3 In the preparation of graphene or graphene oxide-based nanocomposites, the interface of the
4 graphene material and host polymer matrix plays a significant role in determining the final
5 properties of the products formed. Therefore, grafting technique is commonly utilized to
6 introduce functional groups on the surface of the graphene and graphene oxide, which then
7 acted as a compatibilizing or anchoring agent to improve the interfacial adhesion of the
8 immiscible components, and consequently increase the compatibility and dispersion of the
9 graphene materials within the main matrix. Generally, numerous types of monomers have
10 been utilized in grafting technique^{52, 55, 69-71}, with the selection of monomers based solely on
11 the polarity and types of functional groups present on the surface of the polymer matrix.

12

13 2.2.2 Atom transfer radical polymerization (ATRP)

14 Specifically, ATRP is one of the most utilized grafting techniques to achieve purely surface
15 functionalization using a polymer-initiated technique. This is because the technique provides
16 good control of the overall polymer molecular weight, polydispersity, and composition. In
17 addition, the experiment is often straightforward⁷². Classified as one of the controlled radical
18 polymerization technique, it is an effective approach in achieving precise and well-controlled
19 modification of GO or graphene with polymeric chains⁷³. In the preparation of
20 polymer/graphene-based composites, the graphene material is pre-functionalized to provide
21 active sites for surface polymerization to occur. The modified graphene material is then
22 mixed with monomers, and the process is completed by stirring at room temperature for a
23 certain amount of time to obtain the final yield. The final product obtained is rather different

1 from that of a physical blending method, in which the mixed components cannot be
2 physically separated via filtration or washing ⁷⁴. However, this method is currently applied
3 only for small-scale synthesis (in milligrams on a graphene material basis).

4

5 2.2.3 Other radical polymerization techniques

6 Other controlled radical polymerization techniques include reversible addition-fragmentation
7 chain transfer polymerization (RAFT), single-electron transfer living radical polymerization
8 (SET-LRP) and nitroxide-mediated radical polymerization (NMRP). RAFT polymerization
9 technique relies mainly on the degenerative chain transfer, i.e. converting dormant chains to
10 active propagating radicals during a free-radical reaction which depends on the high transfer
11 coefficients of thiocarbonylthio compounds and trithiocarbonates ⁷³. This technique is
12 commonly utilized to functionalize GO with polymer chains via grafting-from approaches, at
13 which the GO is pre-modified with a RAFT initiator in the polymerization step ^{75, 76}. SET-
14 LRP is also referred to Cu(0)-mediated radical polymerization as the entire polymerization
15 process feature the disproportionation of Cu(I) in a suitable solvent, resulting in the formation
16 of Cu(0) and Cu(II). Cu(0) is responsible towards the activation process due to the effect of
17 reaction with alkyl halide, whereas deactivation occurs via reaction with Cu(II),. The high
18 end group fidelity generated is a huge advantage when utilizing SET-LRP to grow chains on
19 the GO surface ^{77, 78} as the polymerization process is complete with full monomer conversion
20 (high efficiency). Unlike others, NMRP technique is not frequently used in modification of
21 graphene / GO. It utilizes the use of free-radical initiator and a nitroxide to pre-synthesize
22 polymeric chains end-capped with nitroxide, which subsequently reacted with GO sheets
23 under elevated temperature and stirring. This causes the dissociation of alkoxyamine C-O
24 bonds and generates PMMA radicals towards the double bonds of GO sheets.

1

2 2.2.4 Condensation techniques

3 The condensation technique is one of the most common methods in the synthesis of
 4 polymeric chains. In the effort of GO functionalization, the choice of monomers is limited to
 5 the extent that a condensation reaction is possible to occur between the monomers and
 6 functional groups present on the surface of GO. In a mixture of GO/ monomers dispersion, an
 7 initiator is added at elevated temperature for propagation of polymeric chains along with
 8 consumption of monomers ⁷⁹. Simultaneously, part of the protonated polymeric chains are
 9 immobilized onto the GO sheets as the effect of condensation reactions occurred ⁸⁰. The
 10 growth of polymeric chains continue as long as the monomers are available in the mixture.

11

12 2.3 Summary of previous works

13 As discussed in the previous sections, there are a variety of methods used to deposit
 14 polymeric-based graphene nanocomposites. The previous results are summarized in Table 1.

15

16 Table 1 Summary of polymer types, nanofiller, and preparation methods for
 17 graphene/polymer-based nanocomposites

Matrix polymer	Filler type	Method	References
Natural polymers			
Cellulose	Graphene	Solution cast	81
Chitosan/oxide	GO	Solution cast	51, 82
Starch			
Starch	RGO	Solution mixing, filtration	83
Polysaccharide	GO, Keratin grafted GO	Solution cast	52
PLA	Graphene	Solution cast	53, 54
PLA	PDLA grafted GO	Solution cast	84
PLA	Graphene	Melt blending	21

Synthetic polymers	RGO	Electrospinning	85
PAN			
PAN	GO	Solution cast	86
PAN	GO	Electrospinning	49
PAN	GO	In-situ polymerization	59
PC	Graphene, functionalized	Melt compounding	57
PC	Graphene	Emulsion/solution cast	87
PC	Graphene	Melt compounding, foamed	88
PCL	Graphene	Solution cast	89
PCL	GO	Electrospinning	90
PI	GO	In-situ polymerization	91, 92
PI	Graphene	In-situ polymerization, spin casting	15
PI	GO	In-situ polymerization, thermal treatment	93, 94
PI	GO, RGO, Graphene	Solution cast, thermal imidization	12, 30, 95
PEO	Graphene	Melt blending	13, 96
PEO	Graphene	Solution cast	13
PU	MEGO	Melt blending	20
PU	Functionalized graphene	Solution cast	22, 97
PU	Functionalized graphene	Colloidal dispersion	98
PU	GO	In-situ polymerization, solution cast	99, 100
PU, epoxy	GO	In-situ polymerization	101, 102
PU/PVP	Graphene	Solution cast	16
PVDF	RGO	Solution cast	103
PVDF	GO	Solution cast	56
PVDF	Graphene	Solution cast, non- solvent diffusion	104
PMMA	RGO	In-situ polymerization, bulk polymerization	105
PMMA	RGO	Solution cast	106
PMMA	Graphene	Sandwiched	107
PMMA	GO	Solution cast,	108, 109
PMMA	Graphene, Modified graphene	In-situ polymerization	24, 110
PMMA	Amine-modified Graphene	Dispersion polymerization/ Core- shell	111
PNIPAM	Graphene	In-situ polymerization (frontal)	112

PNIPAM	Graphene	Polymer grafting	113
PET	EG	Melt compounding	114
PET	Graphene	Melt compounding	23, 115
PE	Graphene	In-situ polymerization	25
PE		Solution cast	29
PE	Functionalized RGO	Solution cast	116
PP	Graphene	Solution cast	47
PS	Graphene	Melt blending	117, 118
PS	Graphene	Solution cast	45, 117, 119
PS	Graphene	In-situ polymerization	62
PVA	Functionalized graphene	Solution cast	55
PVA	PVA- grafted/sulfonated graphene	Solution cast	46, 50, 120-122
PVA	GO	Solvent cast/ uniaxial drawing	123
Conductive polymer			
PPy	Graphene	In-situ polymerization	58, 124, 125
PPy	GO	In-situ polymerization, filtration	126, 127
PPy	GO	Interfacial polymerization	128
PPy	RGO	In-situ polymerization	129
PPy	GO/Graphene	Electro-deposition	18, 28, 48
PANI	Graphene	In-situ polymerization	27, 130
PANI	RGO	In-situ polymerization	129
PANI	RGO	Filtration	131
PANI	RGO	Micro-emulsion polymerization	132
PAC	Graphene	Solution cast	133
PAC	Graphene	In-situ nitrene reaction	134
PEDOT	GO	Electro-deposition	135, 136
PEDOT	Graphene	Chemical reduction/electro- deposition	26
PEDOT	Graphene	In-situ polymerization/ spin cast	60
PEDOT	RGO	In-situ polymerization	129
PABS	GO	Amidation/ chemical reduction	71

1

2 2.4 Interactions of Graphene Oxide and Graphene with Polymers

1 Commonly, the dispersion of fillers within the host polymer matrices is one of the
2 most crucial parameter in determining the effectiveness of the fillers added as well as the
3 final characteristics achieved ⁴⁶. Graphene oxide, which is best known for its oxygen-rich
4 functional groups (hydroxyl, carboxyl, epoxy, carbonyl) located on the basal plane and edges,
5 is able to be dispersed into individual sheets in water. Therefore, a molecular level dispersion
6 is able to be achieved, providing that a common solvent is used for both GO and the polymer
7 matrix. In contrast, the overall performance of graphene-based composites depends heavily
8 on the interfacial adhesion between graphene and the host matrix. While the most common
9 interactions of graphene or graphene oxide with the polymers rely mainly on the physical
10 bondings as the strongest possible interactions, various studies utilized the oxygen functional
11 groups which are responsible for hydrogen bonding formation to react with polymeric
12 molecules, as illustrated and summarized in Figure 2.

13

14 2.4.1 Interactions of graphene oxide in polymer matrices

15 In hydrophilic polymers (e.g. PVA), GO easily achieves molecular dispersion due to
16 the interactions of oxygen-containing functional groups towards the hydrophilic-based
17 polymer chains. Additionally, the hydrogen bonding achieved between GO and the host
18 matrix potentially enhanced the interfacial adhesion and the mechanical performance of the
19 nanocomposite ¹³⁷. Alternatively, the functional groups present on the surface of GO could be
20 utilized by chemical functionalization and grafting to achieved maximum adhesion and
21 compatibility by targeting towards a specific functional groups of the host polymer matrix.
22 For instance, GO has been functionalized with keratin for specific interactions between the
23 N-H groups from keratin and the O-H groups from chitosan ⁵².

24

1 Nevertheless, dispersion of GO within hydrophobic polymers often made impossible
2 due to the issue of polarity. Similar issues have been investigated in an attempt to disperse
3 GO in non-polar organic solvents ¹¹. The oxygenated groups tend to force GO layers to
4 agglomerate as a result of the repelling forces between the hydrophilic and hydrophobic
5 groups. Modifications have been attempted by introducing organic functional groups to
6 enhance the compatibility of GO in a hydrophobic condition, such as functionalization of GO
7 by introducing ethyl isocyanate via a ring opening mechanism of epoxy group on the surface
8 of GO⁹⁵, in which the modified GO readily dispersed in a DMF solvent upon
9 functionalization.

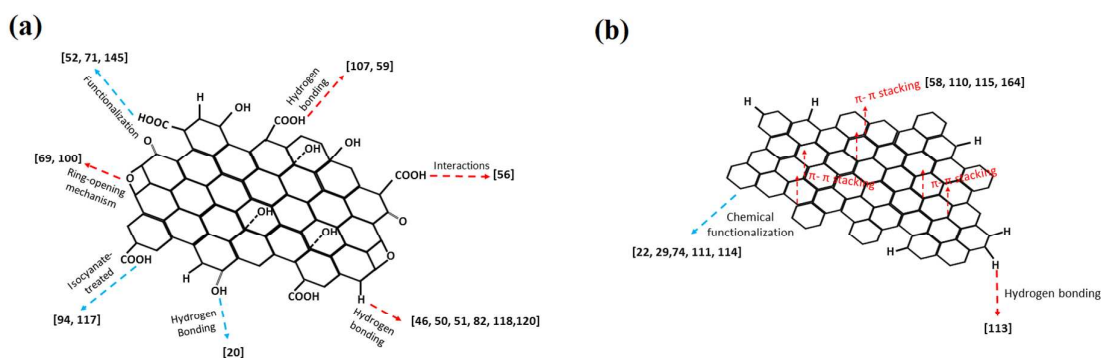
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11 2.4.2 Interactions of graphene in polymer matrices

12 Unlike graphene oxide, graphene is a carbon-based sheets arranged in hexagonal
13 planar rings without any functional groups present on the structure. The naturally
14 hydrophobic graphene readily disperses within a hydrophobic polymer matrix through π - π
15 stacking. Nevertheless, several polymers have unique surface characteristics which restrict
16 graphene from dispersing evenly within the matrix, causing agglomeration of graphene sheets
17 and subsequently gives rise to poor mechanical properties. The weak interactions of graphene
18 with the host matrix have made the low stress transfer between the immiscible components
19 even more pronounced, therefore often resulting in low tensile and elongation characteristics.
20 Often the modifications are initiated mainly by utilizing the functional groups of GO,
21 followed by the reduction of graphene oxide to form functionalized graphene. The lack of
22 functionalities on the surface of graphene sheets limits the possibilities of modifications
23 through chemical reactions.

24

1 The hydrophobic nature of graphene causes aggregation in most aqueous solvents due
 2 to the effect of π - π restacking of graphene layers. In order to fully utilize the potential of
 3 graphene in widespread applications, the limitation of inherent solubility of graphene has to
 4 be solved⁷⁴. Grafting of specific functionalities on graphene has been reported in various
 5 literatures with the aim to introduce functional groups on the surface of graphene in an effort
 6 to enhance its compatibility with various solvents, taking into account covalent or non-
 7 covalent functionalization with defects generated on the structure of graphene. While
 8 covalent bonding usually focuses on the formation and attachment of functional groups on
 9 the surface of graphene, a non-covalent approach relies heavily to the formation of π - π
 10 stacking of the group of interest to graphene. Besides that, hydrogen bonding and
 11 electrostatic forces^{138, 139} are alternatives that are commonly practiced to adhere target
 12 molecule to graphene surfaces.



13

14 Figure 2. Summary of possible interactions on the surface of (a) graphene oxide and (b)
 15 graphene.

16

17 2.5 Natural polymers

18 2.5.1 Chitosan/graphene/graphene oxide nanocomposites

19 The first report on the use of a graphene-chitosan composite involved a Pt-based glucose
 20 biosensor¹⁴⁰. The composite was deposited by electro-deposition. The electrochemical

1 sensing performance was investigated, and the detection limit for glucose was found to
2 0.6 μ M. However, the mechanical properties were not reported, with the exception of noting
3 the wrinkled nature of the graphene sheets in the TEM image. Subsequently, the mechanical
4 properties of chitosan/graphene composites have been investigated^{141, 142}. The tensile and
5 Young's modulus increased by 122 MPa and 64 MPa, respectively, when 6 wt% of graphene
6 was added, compared to the chitosan polymer reference¹⁴². There is evidence that only a
7 small amount of graphene (>0.1 wt%) is required to obtain these mechanical advantages¹⁴².
8 However, another study suggests that there is a maximum enhancement at 6 wt%⁸². The
9 differences could also be attributed to the different processing routes, whereby the first study used
10 graphene produced by direct current discharge, while the latter utilizes reduced graphene
11 oxide via chemical reduction of GO using hydrazine monohydrate. The later study also
12 investigated electrical properties and found that the electrical conductivity also reached a
13 maximum of 1.28 Sm⁻¹ when the amount of RGO was 6 wt%⁸².

14 Chitosan has also been blended with oxidized starch and graphene oxide using solution
15 casting to prepare chitosan/oxidized starch/graphene oxide (COST/GO-n) nanocomposites⁵¹.
16 Upon the addition of GO at 6wt%, the surface morphology had a rough surface caused by the
17 high loading of GO, which resulted in the aggregation of the nanosheets and reduced the
18 compatibility with the polymers. However, the fracture surface of chitosan/GO (4 wt%) and
19 COST/GO (4 wt%) appeared to be much smoother than that of polymer blends without GO.
20 The incorporation of GO could have formed a stronger interaction with the polymers and
21 dispersed more homogeneously in the matrix. The interactions between GO and the matrix
22 were also proven by the tensile strength result, where the COST/GO-n nanocomposites
23 recorded an increase from 13.66 to 21.54 MPa. These results suggested that the carboxyl
24 groups introduced to starch and the incorporation of GO effectively improved the properties

1 of the nanocomposites, which could be attributed to the hydrogen bonding formed between
2 the GO, CS, and oxide starch.

3

4 2.5.2 Cellulose/graphene/graphene oxide nanocomposites

5 Graphene was well-dispersed in a regenerated cellulose matrix synthesized using a solution
6 mixing technique in a mixture of N,N-dimethylacetamide (DMAC) and lithium chloride
7 (LiCl) ⁸¹. This observation indicates a strong interaction between the two components, and
8 the mechanical, thermal, and electrical properties of the composites were significantly
9 enhanced. Besides using the conventional approach of blending, graphene has been
10 chemically grafted on keratin to act as a functional filler to improve the compatibility
11 between the starch and GO components ⁵², resulting in a remarkable improvement (929%) in
12 the storage modulus (graphene 0.5 wt%). At higher temperatures, the inclusion of graphene-
13 grafted keratin further improves the storage modulus, while decreasing the rigidity of the
14 material.

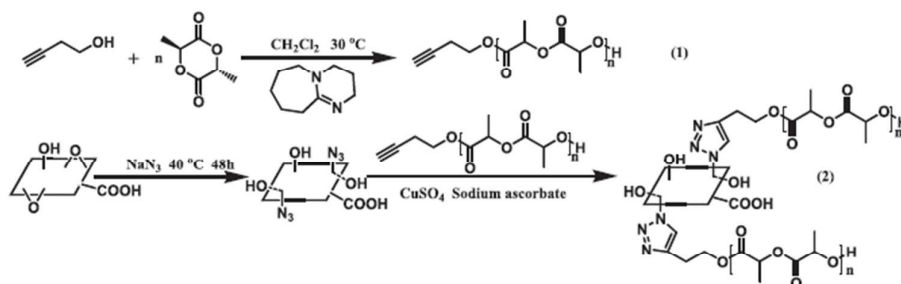
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16 2.5.3 Poly(lactic acid)/graphene/graphene oxide nanocomposites

17 In a modification approach for poly(lactic acid) (PLA) matrices, the pristine polymer was
18 blended with graphene via the solution casting method and achieved a homogeneous
19 distribution of graphene within the polymer matrix. The presence of graphene significantly
20 affects the crystallization of the PLA. For cold crystallization, the graphene acts purely as an
21 inert filler to decrease the cold crystallization rate of the PLA ⁵⁴. However, under melt
22 conditions, the graphene promotes crystallization. More recently, PLA has been mixed with
23 liquid phase exfoliated graphene via solution blending using chloroform as a solvent. The
24 incorporation of the graphene improved the thermal stability, and significantly increased the

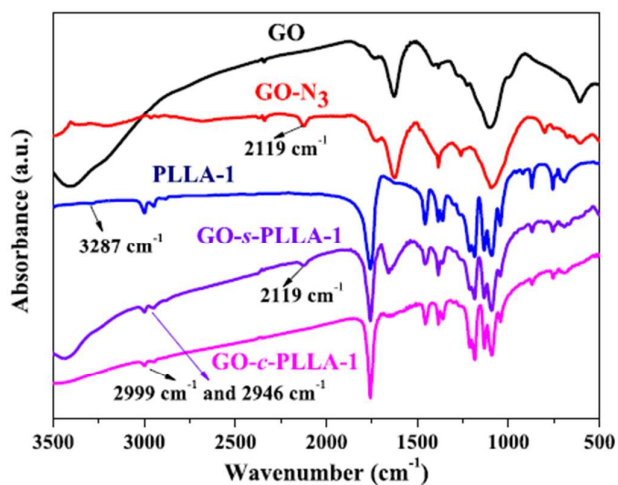
1 tensile strength up to 51.14 MPa with 1 wt% addition of graphene, that is approximately 40%
2 as compared to the pure PLA (36.64 MPa) ⁵³. Moreover, the optimization of the tensile
3 strength of PLA-based graphene nanocomposites was also evaluated in the literature and
4 revealed the optimum addition of graphene nanoplatelets in a PLA matrix ²¹. The parameters
5 involved in the processing included the graphene loading, blending temperature, blending
6 time, and rotor speed of the melt mixer. Based on the result achieved, the maximum tensile
7 strength of the PLA/graphene nanocomposite was recorded at 61.61 MPa, with the addition
8 of graphene at 0.1 wt%, processing at 160 °C, and 10 min of blending at a rotor speed of 25
9 rpm. Meanwhile, GO was grafted to the backbone of poly(D-lactide), forming GO-g-PDLA,
10 which was then blended with poly(L-lactide) before solution casting with GO using
11 chloroform as the solvent. The utilization of GO in the polymer resulted in a lower
12 crystallization activation energy, lower polymer chain mobility, and smaller crystal sizes. In
13 another approach, graphene oxide was initially modified by introducing azide groups using
14 the ring opening mechanism of sodium azide and the epoxide groups of GO ⁶⁹. The N₃
15 functionalized GO easily reacted with alkyne-terminated PLLA to form GO/PLLA
16 composites. A schematic diagram illustrating the synthesis of PLLA-grafted GO sheets is
17 shown in Figure 3. Both the FT-IR characterization peaks responsible for alkyne and azido
18 peaks diminished due to the successful grafting of PLLA chains onto the surface of GO
19 (Figure 4). However, the mechanical properties of the modified PLLA are not mentioned in
20 this paper. GO-N₃ was described as having a wrinkled structure due to the functionalization
21 effect, as compared to the GO sheets, which had sharp edges and a flat surface. The average
22 height of the GO sheets was said to be affected by the grafting ratio, with a higher grafting
23 ratio producing a higher average height for the GO nanosheets (Figure 5). An intercalated
24 structure for the GO/PLLA composites was achieved when the grafting ratio was low,
25 whereas an exfoliated structure was obtained at a high grafting ratio. It was concluded that

1 GO, with OH-, O-, and -COOH functional groups at the edges of the honeycomb graphene
 2 layer, is much easier to disperse within polar polymer matrices because of the interactions
 3 between the oxygen functional groups on the GO and the polar polymer backbone chains⁸⁴.



4
 5 Figure 3. Schematic illustration on the synthesis of PLLA grafted GO sheets: (1) synthesis of
 6 the alkyne-terminated PLLA; (2) synthesis of GO-N₃ and click reaction between GO-N₃ and
 7 alkyne-terminated PLLA. Adopted with permission from ref. 69. (Copyright (2014) Elsevier)

8



9

10 Figure 4. FT-IR spectroscopy of GO, GO-N₃, PLLA-1, GO-s-PLLA-1 and GO-c-PLLA-1.

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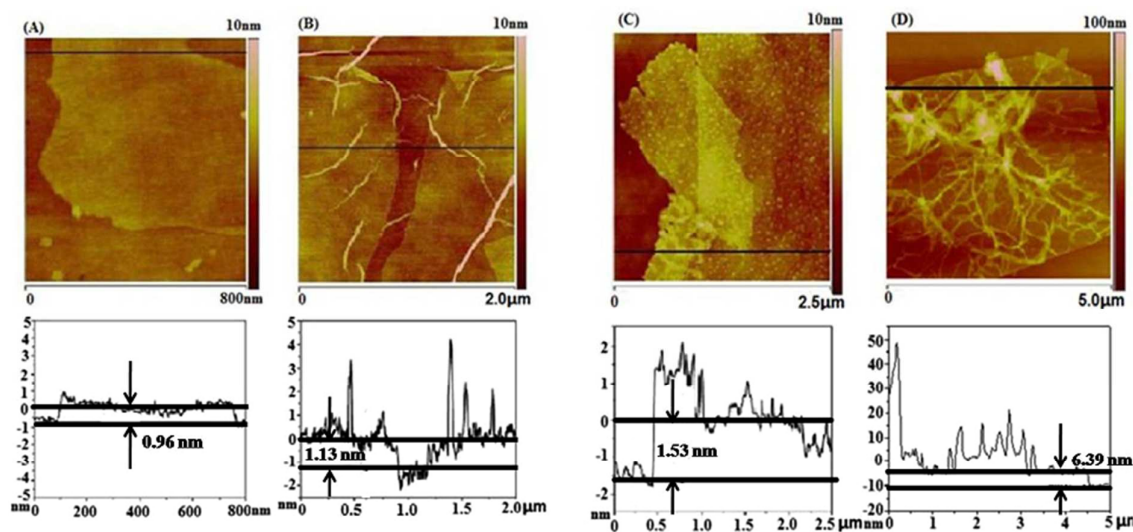


Figure 5. AFM images and height profiles of (A) GO; (B) GO-N₃; (C) GO-s-PLLA-1; (D) GO-c-PLLA-1. All the AFM samples were spin-coated on the silica surface. The concentrations of the samples were 0.1 mg/mL in DMF. Reprinted with permission from ref.

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2.5.4 Starch/graphene/graphene oxide nanocomposites

Graphene oxide was introduced in a starch matrix to prepare a graphene oxide/starch nanocomposite film by means of solution casting⁸³. The mechanical strength was improved even at a low weight content of GO (2 wt%). Moreover, the GO could be well dispersed within the polymer matrix at a low content, and aggregations were formed only at a higher loading. The improvements in the mechanical properties and morphology with the addition of GO were mainly attributed to the strong hydrogen bonding formed between the GO and the functional groups of the starch backbone. Nanocomposites of oxidized starch, chitosan, and GO have also been reported to have good miscibility and a better tensile strength (36.6%)⁵¹. Again, it is believed that the hydrogen bonding between the functional groups of GO and the polymer backbone plays a key role in the improvement of the nanocomposite properties.

1 2.3.5 Contributions and challenges

2 The non-environment friendly characteristic of synthetic polymers has created serious issues
3 in terms of biodegradability and impact on nature, therefore becoming one of the crucial goal
4 in synthesizing natural polymers to replace the currently dominating synthetic polymers in
5 various applications. Yet, the natural polymers commonly shared a mutual physical
6 boundaries by having low mechanical properties and adequate thermal stabilities, which
7 limited their actual potential in replacing the synthetic one. The fascinating mechanical and
8 thermal properties of graphene has successfully imparted into the polymeric backbones by
9 various preparation techniques, with further fine-tuning on the desired properties of the final
10 product could easily achieved by adjusting the ratio of graphene/ polymer matrix.
11 Nevertheless, the final main challenge is to tackle the issue of phase dispersion of graphene in
12 the polymer matrix, as well as the interactions occurred between functional groups presence
13 within the binary phase boundaries which heavily influenced the out coming characteristic of
14 the composites produced.

15

16 2.6 Synthetic polymers

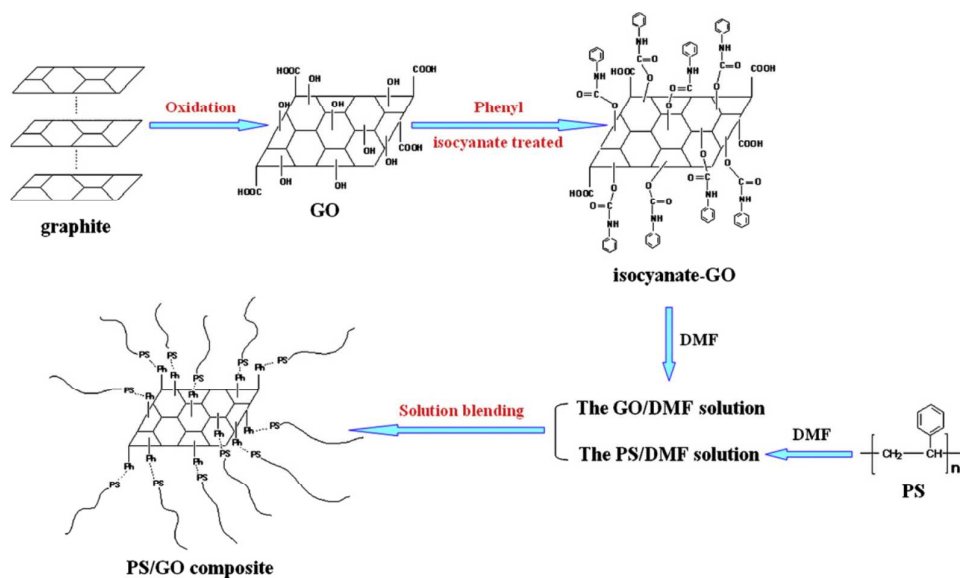
17 2.6.1 Polystyrene/graphene/graphene oxide nanocomposites

18 A comparison of graphene and carbon nanotube (CNT) polystyrene (PS) composites made
19 using the solution casting method was performed¹¹⁸, and polymers containing graphene were
20 found to form a conductive polymer more easily than CNT composites. In fact, only a small
21 amount of graphene (1 vol%) enhanced the conductivity of polystyrene to 3.49 Sm^{-1} , which is
22 approximately 4 orders of magnitude higher than that achieved using multi-walled carbon-
23 nanotube/ PS composites⁴⁵.

1 GO-polystyrene composites, formed using conventional solution blending, have also been
2 reported, as summarized in Figure 6 ¹¹⁹. GO as synthesized via oxidation of exfoliation of
3 graphite, was further treated with isocyanate monomers to obtain isocyanate-GO. Both
4 functionalized GO and PS were then solution blended to achieve PS/GO nanocomposite.
5 Most of the GO sheets are dispersed through the polymer as stacked layers. Only a small
6 amount of the GO is exfoliated into single layer graphene oxide suspended within the PS
7 matrix. This is attributed to the hydrophilic residual nature of the modified GO itself, which
8 influences the compatibility between the GO sheets and the host matrix. To overcome this
9 incompatibility, another facile approach using an in-situ micro-emulsion polymerization
10 technique has been introduced, as summarized in Figure 7 ⁶². Typically, the method utilizes
11 dispersion of graphene in the presence of SDS, forming micro-emulsion within the
12 suspension. Styrene monomers and initiators are then added into the mixture, forming PS
13 functionalized graphene nanoparticles, which will be applied as a filler to prepare the PS film.
14 The prepared graphene/styrene nanoparticles filler consists of thin, aggregated graphene
15 flakes randomly associated with each other, while PS nanoparticles cover the surface forming
16 a disordered solid. It appears that the emulsified monomer droplets increase the probability of
17 having a collision between a nanoparticle and graphene sheet, which provides more
18 anchoring sites for PS nanoparticles to attach to the graphene surface. A similar method was
19 also used to prepare PS/graphene/carbon nanotube (CNT) nanocomposites ¹⁴³.

20 PS/graphene nanocomposites formed via melt blending have also been investigated ¹¹⁷ since
21 melt blending enhances the interactions between the PS chains and graphene through the high
22 shear force applied during the melt blending process. The strong shear force stretches the PS
23 chains, which then diffuse into the interlayer gap of the graphene sheets to form a π - π stack,
24 effectively preventing the graphene sheets from aggregating (see Figure 8). Moreover, the
25 material obtained a homogeneous dispersion with enhanced electrical properties.

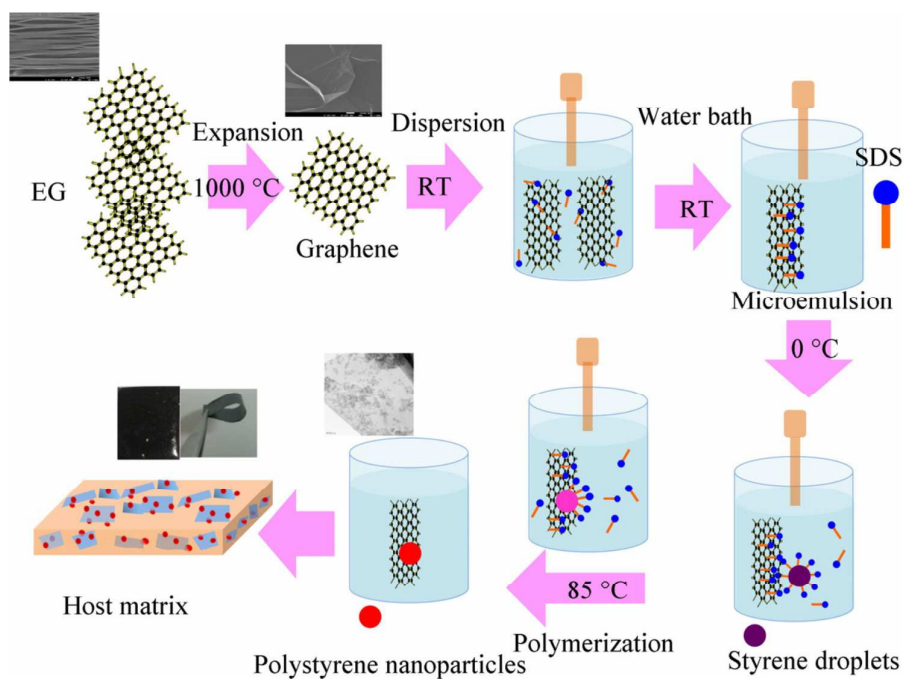
1 On the other hand, graphene nanosheets/polystyrene nanocomposites were prepared via a one
2 pot synthesis method (emulsion polymerization) ¹⁴⁴. For instance, sodium dodecyl sulfate
3 (SDS) was utilized to exfoliate the graphite with the aid of ultrasonication. UV-Vis indicated
4 that with a 0.3 wt% SDS dispersion, a strong peak was detected at 270 nm, denoting the
5 presence of sp² pristine graphene nanosheets, and indirectly showing that the exfoliation was
6 successful (see Figure 9 a). In addition, it has been explained that through ultrasonication for
7 60 min, the graphene nanoplatelets were dispersed evenly with an average length of 6-10 μm
8 (Figure 9 b), indicating that the graphite flakes were exfoliated close to the monolayer
9 graphene. In-situ polymerization with large surface area graphene sheets provided good
10 adhesion at the contact region between the graphene and PS matrix interface. Interestingly,
11 the characteristic peaks of PS still remained prominent even after the formation of the
12 nanocomposite. On the other hand, TEM revealed that the PS nanospheres formed were
13 directly coated on the graphene sheets (Figure 9 c). The conductivity of the GNS-PS
14 nanocomposite with 1.0 wt% of GNS was found to be $3.4 \times 10^{-4} \text{ Sm}^{-1}$, which was an
15 enhancement by a factor of 3×10^6 compared to pure PS (10^{-10} Sm^{-1}). To confirm the validity
16 of the result, cyclic voltammetry (CV) measurements were performed via a three-electrode
17 configuration. A glassy electrode (GCE) was used as the working electrode, Ag/AgCl as a
18 reference electrode, and platinum foil as a counter electrode in 0.1 M H₂SO₄. A larger current
19 density was achieved with the PS/GNS-modified GCE, compared to the bare GCE (Figure
20 10). The high electrochemical activities were credited to the dispersion of the conductive
21 graphene nanosheets in the polymer matrix. This contributed an essential impact toward the
22 modification of the insulating polymer to a conductive material by utilizing graphene.



1

2 Figure 6. Schematic diagram of preparation of polystyrene/GO composite via solution
 3 blending. Adopted with permission from ref. 119 (Copyright (2011) Elsevier)

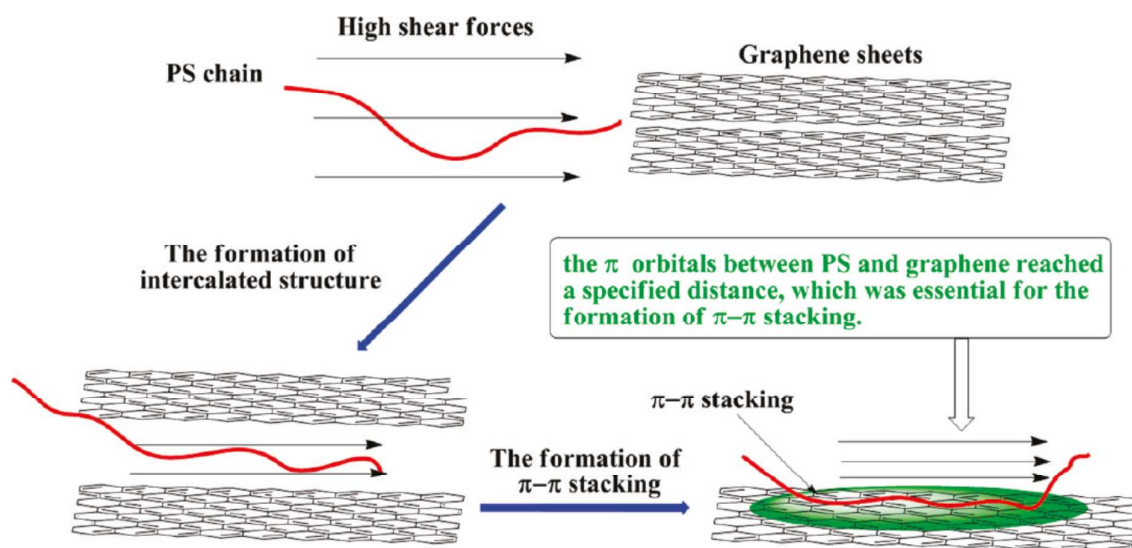
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6 Figure 7. In-situ microemulsion polymerization technique for polystyrene/graphene
 7 nanocomposites. Reprinted with permission from ref. 62 (Copyright (2010) Elsevier)

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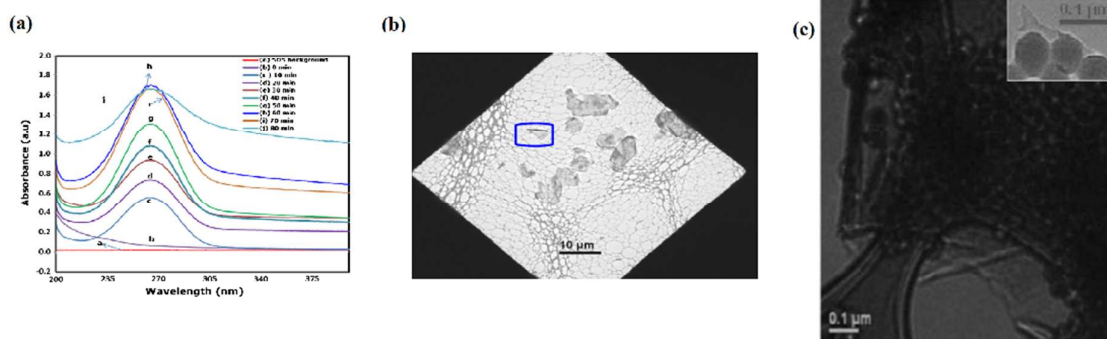
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3 Figure 8. Proposed mechanism of π - π stacking via melt blending. Adopted with permission

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7 Figure 9. UV-Vis spectra of aqueous dispersion phase dispersion of 0.1 wt% EG and 0.3%

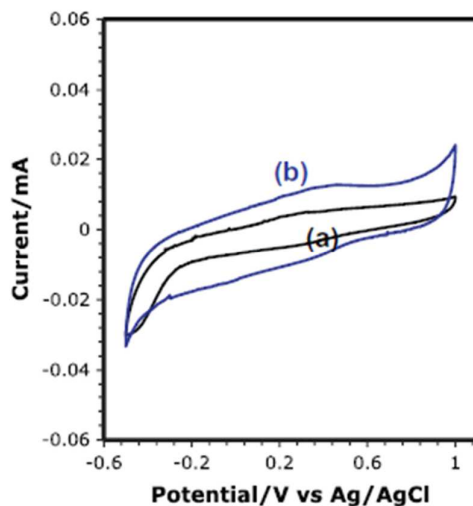
8 SDS as function of sonication time (a); TEM image of graphene sheets after 60 minutes

9 sonication (b); TEM image of PS nanospheres coated on 3-layer graphene (c) Adopted with

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11



1

2 Figure 10. CV profiles at 50 mV/s scan rate using: (a) bare GCE and (b) PS/graphene
3 modified GCE Adopted with permission from ref. 144 (Copyright (2013) Elsevier)

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5 2.6.2 Poly(vinyl alcohol)/graphene nanocomposites

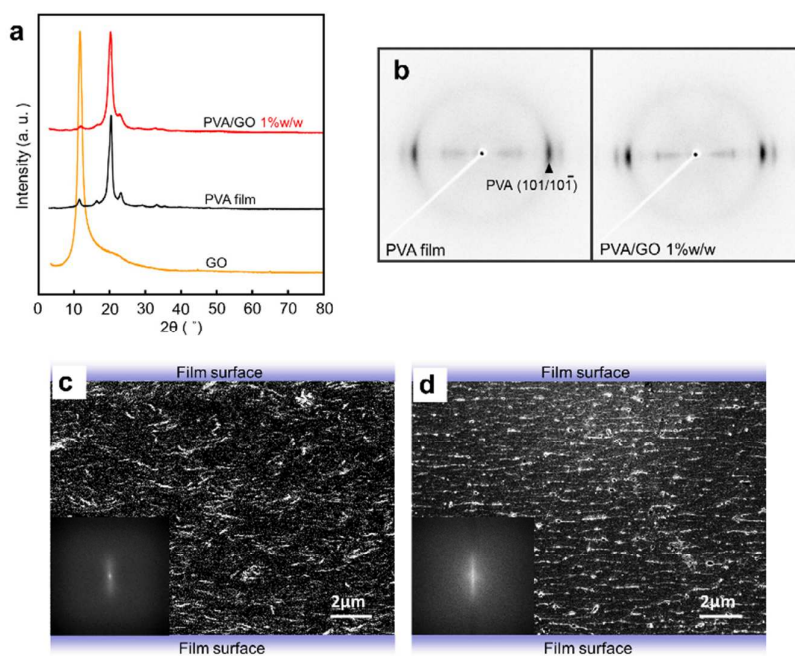
6 Nano-composites of polyvinyl alcohol (PVA) and graphene were prepared via simple
7 solution mixing of PVA/GO, along with a post treatment involving the addition of hydrazine
8 to the mixture to reduce the GO¹²². The resulting film was a strong and ductile material with
9 16% and 32% improvements in the modulus and tensile stress, respectively, at a graphene
10 content of 3.5wt%. The thermal stability of the material was also improved by the
11 incorporation of graphene. The enhancement was ascribed to the homogeneous dispersion of
12 graphene in the PVA matrix and the positive interactions between the components. Similarly,
13 a PVA/GO nanocomposite was reported to have improved the tensile strength and Young's
14 modulus by 76% and 62%, respectively, by the addition of only 0.7wt% of GO⁴⁶. The
15 significant enhancement in the mechanical properties is closely related to the dispersion of
16 GO in the main matrix, also attributed to the formation of strong hydrogen bonding at the
17 GO-PVA interface, which efficiently transfers the external stress loads across the

1 components. Similar explanations for the enhancement of mechanical properties have been
2 reported elsewhere^{50, 120}.

3 GO is able to form a better dispersion and exfoliation within a polymer matrix than graphene
4 due to the strong interactions between the PVA backbone chains and the oxygen functional
5 groups of GO, whereas graphene causes greater property enhancements, including those for
6 the mechanical strength, electric conductivity, and thermal stability, which are attributed to
7 the enhancement of the crystallinity upon mixing¹²¹. However, with the addition of an
8 amphiphilic copolymer, significant improvements have been observed in the
9 exfoliation/dispersion of the added graphene, because the ionic functional groups in the
10 polymer backbone bind the graphene to the hydrophilic portion of the PVA matrix⁵⁵.

11 A rather dissimilar attempt was utilized in PVA/GO nanocomposites via a uniaxial drawing
12 method¹²³. The PVA/GO nanocomposite was initially solvent cast, which was followed by a
13 uniaxial drawing technique with the drawing ratio fixed at three times. Increases in the
14 crystallinities of both the PVA matrix and PVA/GO nanocomposite were detected via XRD,
15 indicated by sharp peaks, as the effect of annealing (Figure 11 a). Equatorial arc patterns
16 were recorded via XRD images for PVA/GO nanocomposites (see Figure 11 b), which
17 indicated that the PVA crystallites were oriented parallel to the drawn direction. Based on the
18 FESEM analysis (Figure 11 c & d), the orientation was observed as bright lines across the
19 images. The GO platelets were observed to be almost fully aligned parallel to the film surface
20 in the overall structure of the uniaxial drawn nanocomposites. In the study of the mechanical
21 properties, Young's modulus of the PVA/GO nanocomposite increased with increasing GO
22 content, with values as much as 160% higher than that of the drawn PVA film using just 1%
23 w/w GO loading, as shown in Figure 12 a. However, in relation to the tensile strength (see
24 Figure 12 b), the highest value of 392 MPa was achieved at a slightly lower GO content (0.5%
25 w/w), which was 37 higher than that of the drawn PVA film. As expected for the filler effect,

1 the elongation at break of the drawn nanocomposite moderately decreased with an increase in
2 the GO content (Figure 11 c). The large improvements in the tensile strength and Young's
3 modulus of the drawn nanocomposites compared to those of the as-cast nanocomposites were
4 attributed to the highly oriented PVA crystallites and highly aligned GO as functions of the
5 drawing process. Additionally, the random alignment of the GO in the as-cast nanocomposite
6 affected the anisotropic morphology, therefore causing the large decrement in elongation at
7 break. This scenario remained stable for the drawn nanocomposite, whereby with 1% w/w
8 loading, the elongation at break was found to be higher than that of the as-cast nanocomposite.
9 The incorporation of GO largely suppressed the swelling ratio of the uniaxially drawn PVA
10 and PVA/GO nanocomposites. With only 1% w/w of GO added, the plateau swelling ratio
11 was greatly suppressed (by 42%). The aligned GO platelets effectively suppressed the
12 molecular motion of the PVA, and therefore retarded the swelling of the whole material itself.

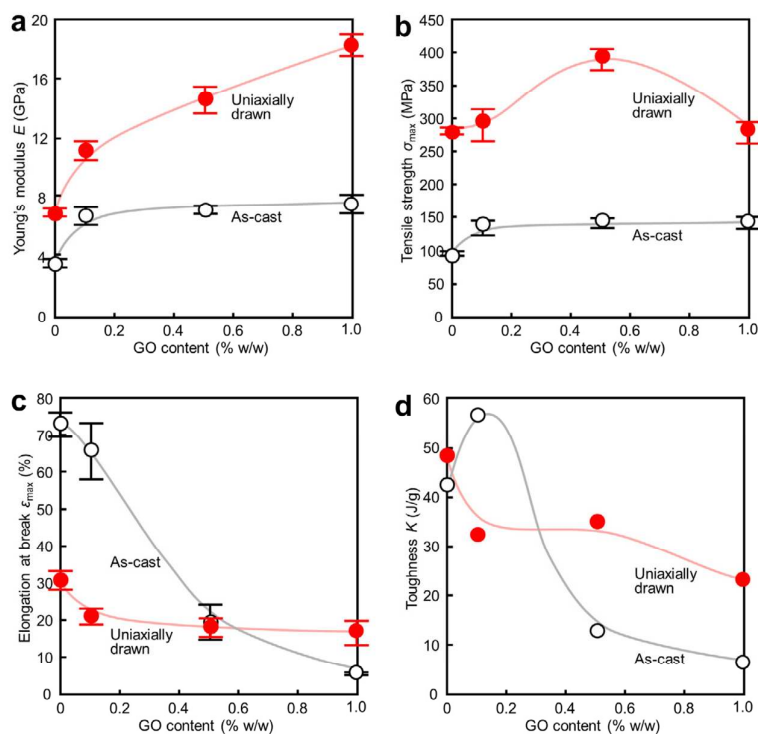


13
14 Figure 11. (a) Equatorial X-ray diffraction profiles of the uniaxially drawn PVA film,
15 PVA/GO nanocomposites and annealed GO (160 °C, 15 min); (b) X-ray diffraction images of
16 the uniaxially drawn PVA film and PVA/GO nanocomposite with 1% w/w loading; FE-SEM

1 image of cross section of (c) as-cast PVA/GO nanocomposite with 1% w/w loading and (d)
 2 uniaxially drawn PVA/GO nanocomposite with 1% w/w. Results for 2D fast Fourier
 3 transform are superimposed in lower left corners. Adopted with permission from ref. 123

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6

7 Figure 12. (a) Young's modulus (E), (b) tensile strength (σ_{max}), (c) elongation at break (ϵ_{max}) and (d) toughness (K) of the uniaxially drawn PVA/GO nanocomposites and the as-cast
 8 PVA/GO nanocomposites as a function of GO content. Reprinted with permission from ref.

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11
 12 2.6.3 LDPE/graphene/graphene oxide nanocomposites

1 The fracture surface of a low density polyethylene (LDPE)/graphene nanocomposite,
2 prepared via the in-situ polymerization method²⁵, remained a fibrous-like structure even with
3 the addition of 1.4 wt% of graphene, indicating that the polyethylene (PE) matrix was still
4 undergoing deformation upon breaking. When a higher amount of graphene was added, it
5 tended to agglomerate, which caused the weak interactions between the immiscible
6 components to be more pronounced as a result of the non-polar polymer matrix and graphene
7 surface, which lacked functionalities (Figure 13). Thus, a slight decrease in the tensile
8 strength of the composite was reported. The modification of graphene with vinyl
9 triethoxysilane (VTES) successfully overcomes the strong interlayer cohesive energy and
10 surface inertia of the material, resulting in a better compatibility between the polymer and
11 graphene²⁹. The strong physical bond between VTES-graphene and LDPE enhanced the
12 tensile strength of the nanocomposite up to 13.6 MPa, and the Young's modulus of the
13 material was recorded at 225.4 MPa (pure PLA recorded a tensile strength of 10.7 MPa and
14 Young's modulus of 116.9 MPa). In another attempt to enhance the lipophilicity of graphene,
15 stearic acid (SA) was utilized as an additive¹¹⁶. The graphene obtained as a function of the
16 thermal reduction of GO was modified by the reaction of the epoxy groups on the graphene
17 with SA. In addition, this method created only minimal damage to the pi-electronic structure
18 of the graphene basal plane. The SA-modified graphene (SA-g-RGO) was blended into the
19 LDPE matrix using a conventional solution casting method. Upon modification, the SA-g-
20 RGO recorded an increase in weight to 35.3 parts per 100 parts of pristine graphene (35.3
21 phr), as compared to the pure RGO, which was recorded at 11.1 phr. This increase in weight
22 was related to the reaction between the epoxy group of graphene and stearic acid, which
23 resulted in a functionalization effect. In addition, the FT-IR analysis supported that an
24 additional broad absorption band was recorded for SA-g-RGO at the region of 1690–1770
25 cm^{-1} , having a peak at 1744 cm^{-1} attributed to the ester C=O bond created by the reaction of

1 SA and the epoxy groups on graphene. An evaluation of the dispersion of the modified
2 graphene in the LDPE matrix was carried out by utilizing the morphology features of the
3 samples. As the amount of SA bonded on the graphene sheets increased, the number of black
4 particles (formed due to the nature of the agglomeration of graphene sheets toward each other)
5 decreased significantly, which indicated that a fine dispersion of graphene in LDPE was
6 achieved by the functionalization of the graphene surface with the SA addition. Moreover,
7 the modulus and yield strength of SA-g-RGO/LDPE were both significantly enhanced by the
8 reinforcing effect upon the addition of graphene, and the enhancement effect was further
9 intensified by the lipophilization of graphene. The enhancement was correlated to the
10 improved interfacial interaction, as well as the fine dispersion of the graphene in the LDPE
11 matrix. In addition, the necking effect was absent in the nanocomposites, whereby the
12 samples exhibited very low values for the elongation at break due to the molecular re-
13 arrangement of the LDPE that occurred during the deformation process, which was strictly
14 inhibited as a function of the dispersed graphene. Nevertheless, it was proven that the
15 intrinsic epoxy groups on graphene could be utilized for modifications in order to achieve the
16 characteristics of interest. Furthermore, the defects on graphene could be minimized by
17 applying modification via the intrinsic groups. The addition of graphene successfully had a
18 reinforcing effect in improving the tensile modulus and yield strength of the LDPE upon
19 mixing, courtesy of the fine dispersion of functionalized graphene.

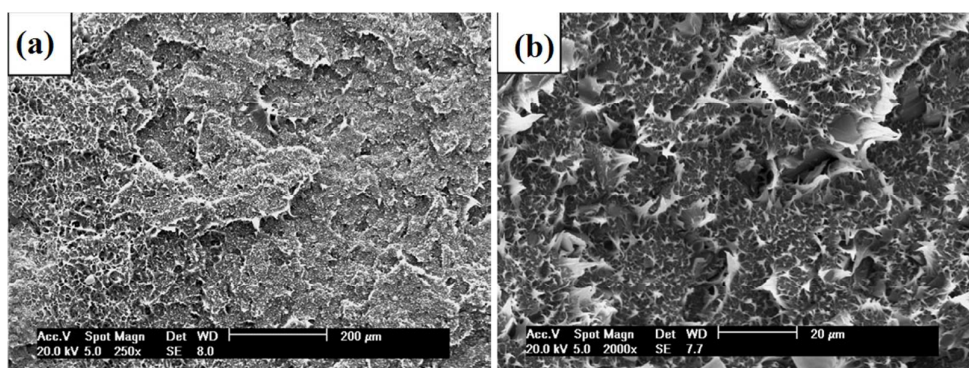
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21 2.6.4 Poly(ethylene terephthalate)/graphene/graphene oxide nanocomposites

22 Poly (ethylene terephthalate) (PET)/graphene nanocomposites prepared via the melt
23 compounding method²³ exhibited a uniform dispersion of graphene throughout the PET
24 matrix, with no large agglomerates forming. As expected, the electrical conductivity sharply

1 improved as a result of the graphene incorporation. A value of 2.11 Scm^{-1} was obtained at a
2 low graphene content of 3.0 vol%. Rather than using graphene directly, exfoliated graphite
3 has been used instead ¹¹⁴. No aggregates were observed for quantities up to 7 wt%, and the
4 thermal stability of the prepared composite was improved because of the well dispersed
5 exfoliated graphite within the PET matrix, which served as a barrier in preventing further
6 degradation of the polymer within. The prepared 7wt% exfoliated graphite/ PET composite
7 recorded a volume electrical resistivity of approximately 10^{-6} Scm^{-1} while that of pure PET
8 was $10^{-16} \text{ Scm}^{-1}$. Another approach to prepare PET/graphene nanocomposites is injection
9 molding ¹¹⁵. The graphene remains as platelets when dispersed within the PET matrix, with
10 an exfoliated layer of graphene sheets (shown by red arrow) being observed (Figure 14). The
11 addition of the graphene content up to 15 wt% improves the Young's modulus of the
12 nanocomposite to approximately 8 GPa, compared to the pure PET at around 2.8 GPa.
13 Additionally, micromechanical model (Halphin-Tsai and Hui-Shia) was utilized to determine
14 the theoretical elastic modulus of the PET and its nanocomposite. Unfortunately, the
15 improvement in elastic modulus of PET upon of graphene addition was purely theoretical
16 calculation.

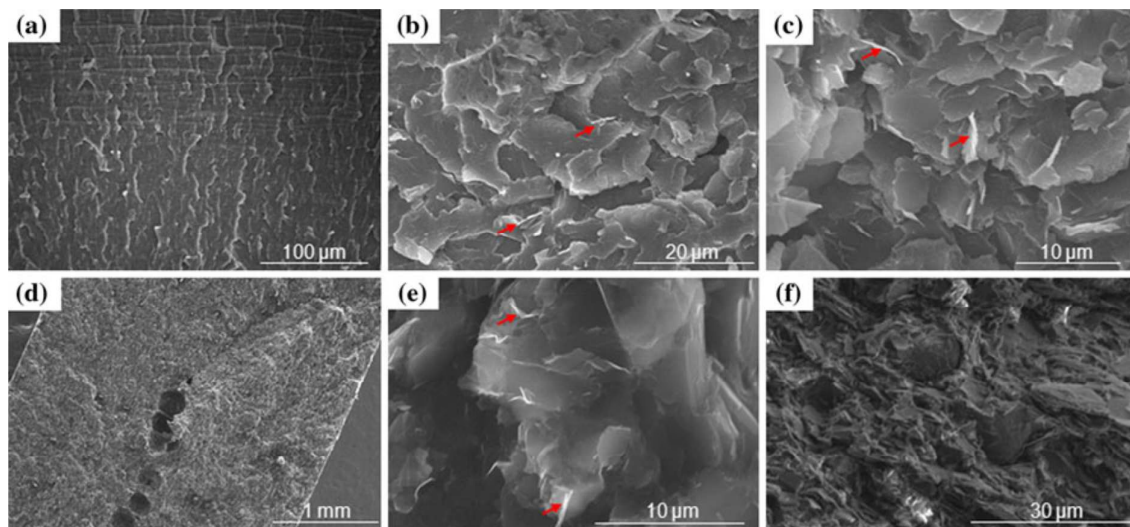
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19 Figure 13. SEM images of broken tensile section for PE/6.6% at magnifications of (a) 250X
20 and (b) 2000X. Reprinted with permission from ref. 25 (Copyright (2013) Wiley)

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Figure 14. SEM micrographs of (a) pristine PET and PET/
nanocomposites with volume contents of (b) 2wt%, (c) 5wt%, (d)10 wt%, (e) 10wt% at 5kX,
and (f) 15wt% Reprinted with permission from ref. 115 (Copyright (2012) Springer)

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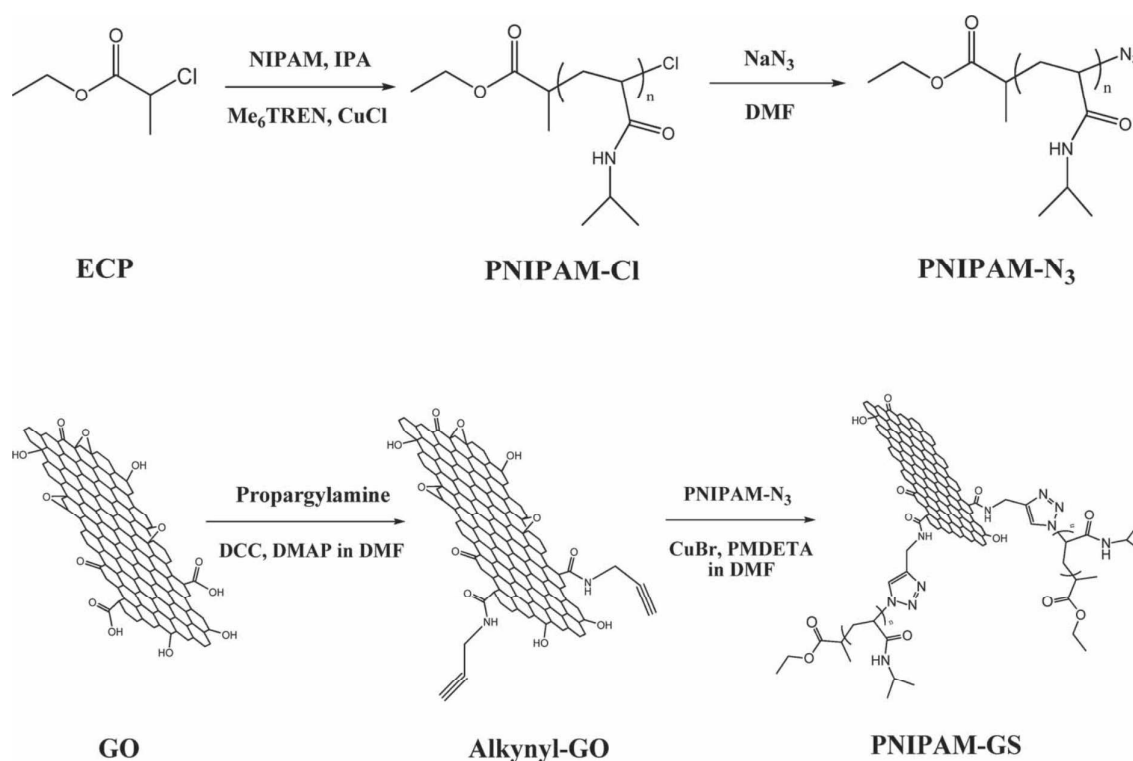
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2.6.5 Poly (*N*-isopropylacrylamide)/graphene/graphene oxide nanocomposites

The addition of graphene can also be used to tune the hydrophilic/phobic properties of a polymer. Graphene sheets have been covalently functionalized by grafting up to 50wt% onto the backbone chains of poly(*N*-isopropylacrylamide) (PNIPAM) (Figure 15)¹¹³, and the hydrophilic/phobic properties were tuned. The synthesis of functionalized graphene sheets involved three processes: (i) synthesis of the PNIPAM-N₃ homopolymer via the ATRP method through a series of steps, (ii) initial functionalization of GO sheets by propargyl amine through the acylation reaction, and (iii) grafting of the homopolymers onto GO sheets by the reaction between alkynyl-GO and the PNIPAM-N₃ homopolymer under room temperature. Upon the incorporation of PNIPAM, which was covalently bonded to the surface of the graphene, the graphene-g-PNIPAM was found to be easily dissolved in water

1 under the condition of phosphate-buffer saline and sonication. Although GO was also found
2 to be uniformly dispersed in water to form a stable dispersion over a long time, it could not
3 be well dispersed in PBS, and it precipitated after sonication was terminated. This change in
4 behavior was attributed to the successful interaction between the graphene sheets and the
5 PNIPAM polymer, whereby PNIPAM polymers were covalently bound on the surface of
6 graphene sheets. Moreover, the modified polymer was able to absorb camptothecin, a water-
7 insoluble anticancer drug, up to 15.6 wt%, as a result of the π - π stacking and hydrophobic
8 interactions between the graphene sheets and the polymer chains¹¹².



9

10 Figure 15. Synthesis route for PNIPAM/GS nanocomposites. Adopted with permission from
11 ref. 113 (Copyright (2011) Wiley)

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1 2.6.6 Poly(methyl methacrylate)/graphene/graphene oxide nanocomposites

2 Loading poly(methyl methacrylate) (PMMA) with 1 wt% of chemically reduced graphene
3 oxide (CMG) improves the elastic modulus by as much as 28%. The dispersion of CMG
4 within the polymer matrix was quantified using the Mori-Tanaka theory, suggesting that a
5 better dispersion was achieved at a lower loading of CMG. An NMR study showed there is
6 no change in the polymeric structure of a CMG polymer composite ²⁴, which suggests that
7 the CMG acts as an inert filler.

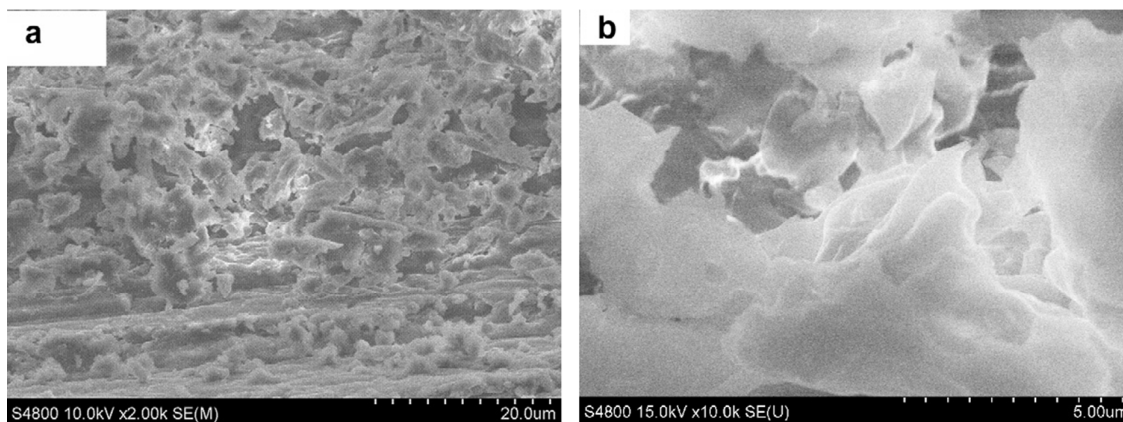
8 Using an in-situ polymerization technique, graphite oxide was dispersed at the nano-level
9 throughout the PMMA polymer matrices ¹¹⁰. Raman and FT-IR analyses showed that the
10 suspended phase consisted of graphite oxide with the possibility of graphene. Moreover, the
11 prepared nanocomposite also exhibited an improved storage modulus, with an electrical
12 conductivity recorded at 1.5 Scm^{-1} upon the addition of 3wt% graphite oxide.

13 A conventional solution blending approach was used to prepare PMMA/RGO
14 nanocomposites ¹⁰⁶. The electrical conductivity was increased to 3.7 Scm^{-1} with only 2 wt%
15 of RGO. As indicated by using SEM on the fracture surface of the material, a "pull out"
16 feature was observed and ascribed to the better interactions between the filler and polymer
17 matrix (Figure 16). The possible interaction involves the remaining oxygen-containing
18 groups of RGO forming strong hydrogen bonds with the carbonyl functional groups of
19 PMMA.

20 Another reported method for preparing PMMA/graphene oxide nanocomposites involved
21 mixing GO sheets and cationic PMMA emulsion particles ¹⁰⁹. The GO sheets, which adhered
22 tightly to the surface of the PMMA particles, were reduced using an in-situ chemical method
23 to produce graphene sheets without any aggregation. The SEM images (Figure 17 c & d)
24 show that the GO sheets were exfoliated and bonded onto PMMA particles. The measured

1 storage modulus of the material was enhanced by the addition of graphene. PMMA/GO
2 nanocomposites have also been prepared using a similar method, but with the application of
3 ultrasonication, rather than using surfactants¹⁰⁸. As shown by the SEM images (Figure 17 a
4 & b), the PMMA particles were still covered by the GO sheets when using ultrasonication
5 rather than a surfactant (as indicated by the arrows in Figure 16 b). The successfully
6 exfoliated GO was sonicated into a much smaller size, which promoted the efficient wrapping
7 of the hydrophobic particles. Furthermore, the GO sheets were flexible enough to bend and
8 wrap around the spherical surface.

9



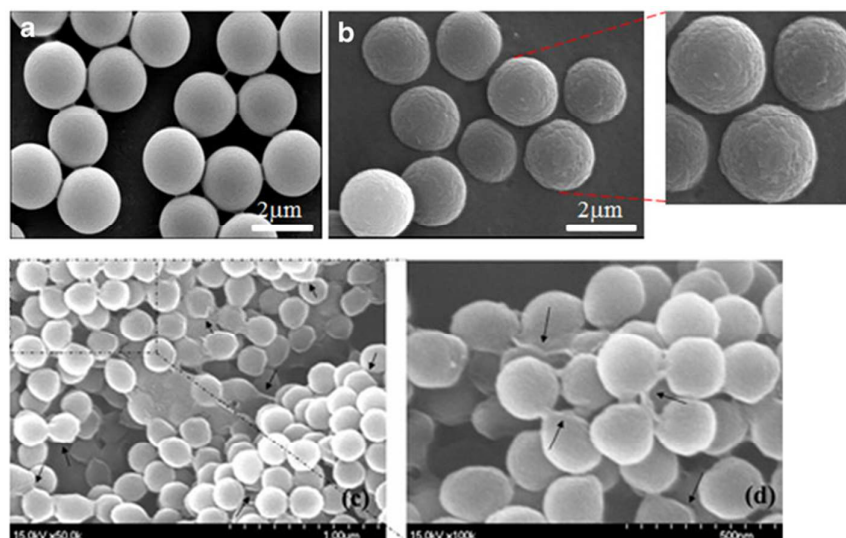
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11 Figure 16. SEM images of PMMA/RGO nanocomposites. Reprinted with permission from

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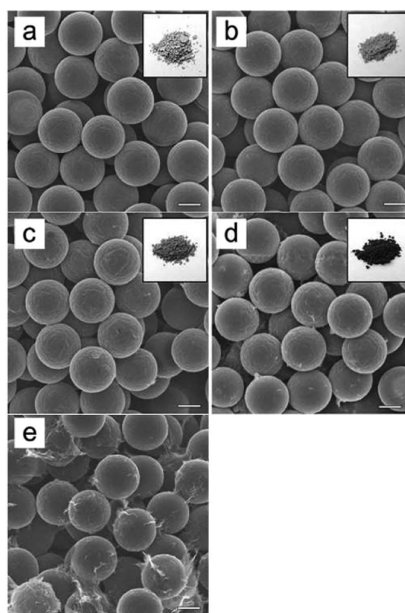
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2 Figure 17. Comparison of FESEM images of PMMA/GO (a & b) without surfactant and with
3 surfactant and without sonication (c & d) with surfactant and without sonication. Figure (a & b) adopted with
4 permission from ref. 108 (Copyright (2013 Springer), (c & d) reprinted with permission from
5 ref. 109 (Copyright (2012) Elsevier)

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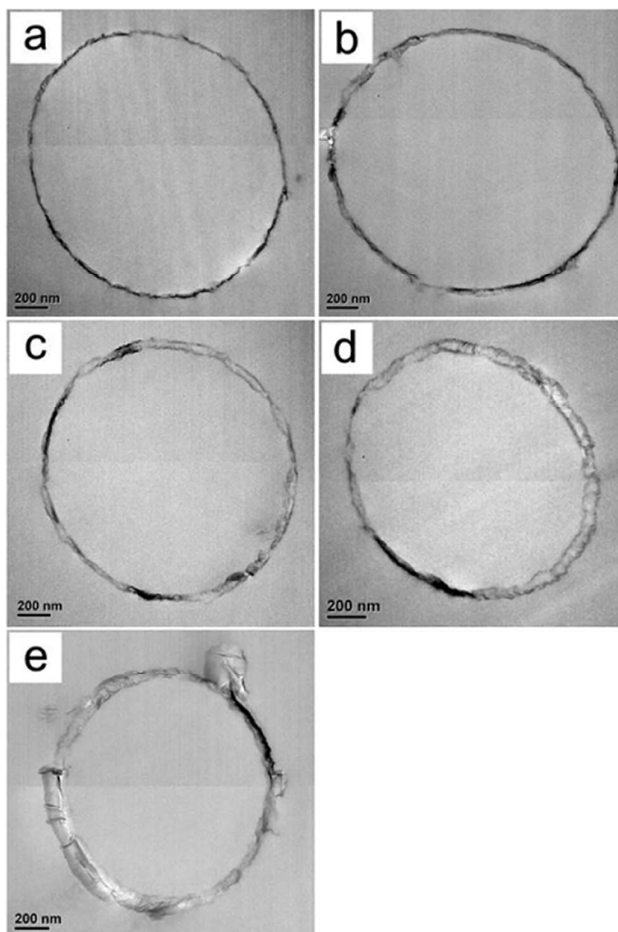
7 GO was blended with amine-functionalized poly(glycidyl methacrylate) (PGMA), which was
8 then utilized in the synthesis of a polymer core and graphene shell microspheres¹¹¹. PGMA
9 was initially dispersed polymerized and further modified with ethylene diamine, forming
10 amine-functionalized polymer microspheres (PGMA-ed). The pH of the mixture was found to
11 significantly influence the surface of the nanocomposites, where the surface roughness
12 increased as the pH decreased. Further, the fabrication process was initiated at pH 10, where
13 the surface charges of both GO and PGMA-ed remained the same, which indicated that the
14 reactions possibly occurred via reactions between the functional groups of GO and PMMA-
15 ed. The reactions via electrostatic attraction were less likely to occur. Digital images of the
16 RGO/PMMA powder showed that the color became darker as the pH decreased (inset of
17 Figure 18), suggesting that the layers of the RGO shell increased as the pH decreased because

1 the transmittance of the graphene layer was linearly reduced with an increase in the number
2 of layers. The RGO/PGMA-ed core-shell was uniform in size, without any aggregation
3 between particles, except for that synthesized at pH 2, as indicated by SEM images (Figure
4 18). This phenomenon explained why the self-assembly of GO sheets onto core particles was
5 not favored at exceedingly high acidic conditions (below pH 3), as the carboxylic acid groups
6 of the GO sheets were abruptly protonated, leading to instability. In addition, all of the
7 samples, regardless of pH, showed that the PGMA-ed microspheres were completely covered
8 with RGO shells without any voids noticed between the interfaces, as shown in TEM images
9 in Figure 19. The average shell thicknesses obtained at pH 10, 7, 5, 3, and 2 were
10 approximately 24, 37, 55, 70, and 100 nm, respectively. The maximum electrical conductivity
11 was recorded for the samples produced at pH 3, with the highest at 31.43 Sm^{-1} . An important
12 point worth mentioning is that the electrical conductivity of the samples could be easily
13 adjusted by varying the thickness of the shell.



14
15 Figure 18. SEM images of RGO/PGMA-ed core-shell microspheres produced at pH 10 (a), 7
16 (b), 5 (c), 3 (d), and 2 (e). The insets are the photograph images of powdered form of the
17 core-shell particles. Adopted from ref. 111 (Copyright (2014) RSC)

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3 Figure 19. Cross-sectional TEM images of RGO/PGMA-ed core-shell microspheres
4 produced at pH 10 (a), 7 (b), 5 (c), 3 (d), and 2 (e). Adopted from ref. 111 (Copyright (2014)

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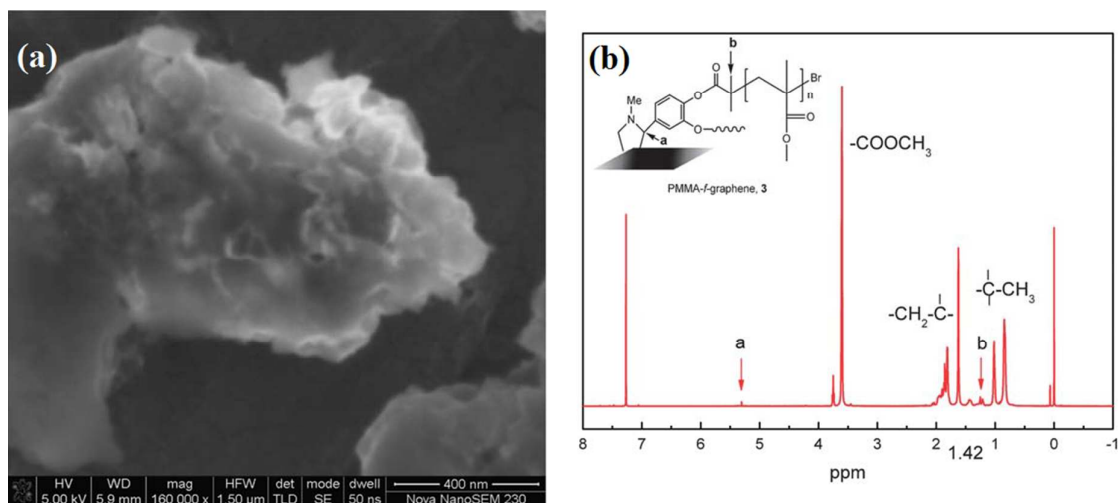
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7 In addition to depositing graphene nanosheets onto PMMA particles, research has also been
8 conducted on physically sandwiching graphene between two insulating PMMA layers to
9 prepare an organic bistable device (OBD)¹⁰⁷, which has potential applications for transparent
10 flexible non-volatile memory devices. The fabricated device demonstrated an electrical
11 bistable behavior, even after bending, indicating the memory stability of the material. For
12 comparison purposes, PMMA/RGO nanocomposites were prepared via three different

1 methods: the in-situ polymerization of MMA in the presence of RGO, bulk polymerization of
2 MMA in the presence of PMMA beads/RGO, and in-situ polymerization of MMA in the
3 presence of RGO followed by sheet casting ¹⁰⁵. Interestingly, the electric conductivity of the
4 prepared composites was critically dependent on the amount of RGO, as well as the method
5 of fabrication. At 2wt%, the electric conductivity of the material was increased by a factor of
6 10^7 by means of the in-situ polymerization of RGO/PMMA in the presence of PMMA beads,
7 whereas the conductivity was recorded at 10^8 for the composite at the same weight content
8 prepared via the casting method. Furthermore, the sheet casting method provided better
9 exfoliation of the RGO within the PMMA matrix among the three methods, thus providing a
10 better dispersion and adhesion of RGO toward the PMMA matrix, and significantly
11 improving the electrical conductivity. Along with the physical modification efforts, graphene
12 was also covalently functionalized ⁷⁴ with phenol groups, followed by the polymerization of
13 PMMA at room temperature. This process was carried out using N-methylglycine and 3,4-
14 dihydroxybenzaldehyde, whereby graphene was functionalized by two hydroxyl groups
15 without altering the electronic properties. Unlike physical blending, the two components of
16 the functionalized graphene/PMMA nanocomposites could not be separated from one another
17 even via extensive washing and filtration. As shown in Figure 20 a, the surface of the
18 graphene was heavily covered by PMMA. Additionally, the prepared functionalized
19 graphene/PMMA nanocomposites were readily soluble in organic solvents, which occurred
20 because the PMMA was covalently bonded onto the graphene surface. The functionalization
21 was also proven by the ¹H NMR spectrum shown in Figure 20 b.

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Figure 20. (a) FESEM image of the PMMA-functionalized Graphene and (b) ^1H NMR spectrum of PMMA-functionalized graphene in CdCl_3 . Adopted from ref. 74 (Copyright (2012) RSC)

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2.6.7 Poly(caprolactone)/graphene oxide biocomposites

Research conducted on the incorporation of GO in a poly(caprolactone) (PCL) matrix has not been widely reported. The initial results obtained from PCL/GO nanocomposites prepared via a typical electrospinning method⁹⁰ were encouraging, with dramatic increases (at 0.3 wt%) of the tensile strength, modulus, and energy at break of 95%, 66%, and 415%, respectively. Moreover, the porosity of electrospun nanocomposites was still retained at 94.1%, as compared to the neat PCL polymer (96.9%). The increase in the mechanical strength of the nanocomposites was directly related to the changes in the fiber morphology by the incorporation of GO. Thermally reduced graphene has also been incorporated in a PCL matrix via the conventional solution casting method⁸⁹. The prepared nanocomposites achieved a fine dispersion of graphene throughout the PCL matrix, with some graphene being embedded in the matrix, indicating a strong interfacial adhesion between the components. The addition of very small amounts of graphene (0.5 and 2.0 wt%) results in significant

1 improvements in the storage modulus of the nanocomposites by about 203% and 292%,
2 respectively, at -80 °C, as compared with the neat PCL.

3

4 2.6.8 Polyvinylidene fluoride/graphene/graphene oxide nanocomposites

5 Like most fluorinated hydrocarbons, polyvinylidene fluoride (PVDF) is hydrophilic, but the
6 dense skin-layers of PVDF membranes make it difficult to manufacture super-hydrophilic
7 surfaces¹⁰⁴. The addition of graphene, which is also hydrophilic, to the PVDF should make it
8 possible to tune the physical properties of the polymercomposite. Indeed, super-hydrophilic
9 surfaces based on PVDF/graphene nanocomposites have been reported in the literature¹⁰⁴.
10 Nano-composites were formed by the diffusion of a non-solvent vapor, either methanol or
11 water, into a PVDF/graphene/DMF suspension, followed by freeze drying, to form porous
12 materials¹⁰⁴. The addition of graphene influences the crystallization of the PVDF, resulting in
13 a surface roughness on the nanometer scale and a surface that is super-hydrophobic.

14 PVDF/GO nanocomposites, fabricated via solution mixing followed by either hot press
15 molding or solution casting, have also been reported⁵⁶. The strong interaction between the
16 carboxyl functional groups on the surface of the GO and the fluorine group on the PDVF
17 backbone ensures a homogeneous dispersion of GO nano-sheets within the PVDF matrix. At
18 the percolation threshold, the electrical conductivity of the polymer is expected to increase.
19 For the PVDF/GO material, this occurs between 0.1 wt% and 0.5 wt% of GO, which appears
20 to be lower than previously reported measurements on graphene/PVDF nanocomposites¹⁴⁵,
21¹⁴⁶. A comparison of the PVDF/GO synthesis routes using FTIR shows that solution casting
22 is more efficient at inducing the α -PVDF to β -PVDF phase transition than hot press molding.
23 This observation could be significant technologically since β -PVDF is a common
24 piezoelectric material, while α -PVDF is non-piezoelectric. There have been multiple reports

1 about adding graphene-related materials to PVDF to enhance its piezoelectric performance
2 ¹⁰³and thus improve the performance of devices, like energy harvesters, based on this material.

3 However, adding too much graphene/rGO to the nanocomposites obstructs the formation of
4 the piezoelectric β -phase crystals, because the space for β elongation becomes smaller.

5

6 2.6.9 Polyurethane/graphene/graphene oxide nanocomposites

7 The enhancement of the mechanical properties of polyurethane (PU) nanocomposite films as
8 a function of graphene and graphene oxide has been investigated, and the results were similar
9 to those for other polymer composites ¹⁰⁰. Namely, there was an exponential increase in
10 Young's modulus, but an exponential decrease in toughness with the graphene content. In
11 this study, a nanocomposite was synthesized by first dispersing the graphene in DMF,
12 followed by mixing with Pu-dissolved tetrahydrofuran (THF). The mixture was then drop-
13 cast to prepare the free-standing PU/graphene nanocomposite film. As previously mentioned,
14 there is an exponential increase in the Young's modulus with the amount of graphene.
15 However, above 50wt% of graphene, there is no longer any increase, and the
16 Young's modulus saturates at 1GPa. There is also a corresponding saturation in the stress at a
17 3% strain (25 MPa).

18 The electrical conduction of a polymer/graphene nanocomposite can be significantly
19 increased (by approximately 6 orders of magnitude) by the inclusion of graphene ¹⁶.

20 Waterborne polyurethane (WPU)/graphene nanocomposites were prepared by initially mixing
21 a graphene suspension and monomers, followed by chemical polymerization ¹⁶. The mixed
22 graphene solution and WPU emulsion was dried to obtain the composite film. The electrical
23 conductivity of the composite increased exponentially when the amount of graphene in the
24 composite was below 1 wt%. Above this amount of graphene, the rate of increase in the

1 electrical conductivity was significantly smaller, and there is evidence from the published
2 figures that the conductivity could saturate. The maximum conductivity of $8.30 \times 10^{-4} \text{ S cm}^{-1}$
3 occurred at a graphene content of 4 wt%. No information on the mechanical properties was
4 given in the paper. A very much similar study was performed by Sang et al.⁹⁸ to prepare
5 graphene/ waterbone polyurethane nanocomposites, however dissimilar method of colloidal
6 dispersion mixtures. The tensile strength and elongation at break recorded a decrease with
7 increasing functionalized graphene nanosheets (FGS) due to inhibiting effects of molecular
8 arrangements of PU as a function of FGS addition. Nevertheless, the conductivity was
9 recorded at $1.04 \text{ e}^{-7} \text{ Scm}^{-1}$ with 2 wt% content of FGS within the nanocomposite matrix that is
10 approximately 10^3 folds as compared to the nanocomposite with 1 wt% FGS content. It can
11 be concluded that the FGS could be finely dispersed within the polymer matrix via physical
12 mixing of colloidal dispersion of FGS and a colloidal dispersion of a polymer.

13 PU/epoxy/GO nanosheet composites were reported to have a uniform morphology, indicating
14 that the GO nanosheets (GONS) were well-dispersed throughout the polymer matrix as a
15 result of the effective chemical bonding between the PU/epoxy and functional groups on the
16 GONS surface¹⁰¹. The mechanical strength of the polymer increased (218 to 257 MPa), but
17 not to the same extent as graphene in pure PU. In addition, the elongation at break increased
18 by more than 52%. The enhancing mechanism is illustrated in Figure 21, where the urethane
19 bonds(-NH-CO-) could form to serve as covalent bonds, which resulted from the reaction
20 between the hydroxyl groups on the GO surface and the -NCO groups of the PU chains,
21 respectively. Additionally, the ability of epoxy to intercalates into the layered structure of GO
22 was also reported in literature¹⁰².

23 Significant improvements in mechanical properties have also been reported in hyper-
24 branched polyurethane (HPU)/GO nanocomposites⁹⁹. The HPU was initially chemically
25 polymerized¹⁴⁷ and mixed with graphene to form a dispersed solution. This mixture was then

1 solution cast on an inert substrate to obtain the desired nanocomposites. The tensile strength
2 increased from 7 to 16 MPa, and the elongation at break increased from 695 % to 810 %
3 when 2 wt% of GO was added. Furthermore, the (HPU)/ GO nanocomposites exhibited
4 excellent shape memory behavior, at which the photographs of the nanocomposite film prior
5 and after stretching force applied are illustrated in Figure 22 a. This is because of the increase
6 in stored energy caused by the π - π interaction between the GO sheets and the hard backbone
7 chains of the HPU as shown in Figure 22 b. GO created high quantity of stored elastic strain
8 energy which aids the nanocomposites to gain high recovery stress. Moreover, addition of
9 GO increased the degree of crystallinity of the nanocomposite, which improved the shape
10 recovery.

11 Other methods for synthesizing PU/graphene nanocomposites obtained similar results. For
12 example, Rana et al.²² functionalized graphene sheets and incorporated them into a PU
13 matrix to act as cross-linkers. In this experiment, ultra-sonicated graphene nano-sheets were
14 added to a pre-loaded mixture of 4,4-methylene bis(phenyl isocyanate) and poly(ϵ -
15 caprolactone) diol. Upon completion of the reaction, the mixture was cast onto a Petri dish
16 and dried to obtain the nanocomposite film. Covalent cross-linking effectively controlled the
17 re-stacking of graphene sheets within the polymer matrix, thereby creating a uniform
18 morphology. The mechanical properties of the nanocomposites were again enhanced.
19 Interestingly, at 4 wt%, the enhancement of Young's modulus and the shape recovery of the
20 graphene nanocomposite was larger than that for a sample containing carbon nanotubes.
21 Blending microwave-exfoliated graphite oxide (MEGO) into the polyurethane matrix via
22 injection molding also achieved a nanocomposite with a uniform morphology, whereby the
23 MEGO layers were uniformly dispersed throughout the matrix²⁰. The strong interactions
24 between MEGO and polyurethane are related to the formation of hydrogen bonding between
25 the N-H group of PU and the oxygen functional groups of the MEGO layers (Figure 23). The

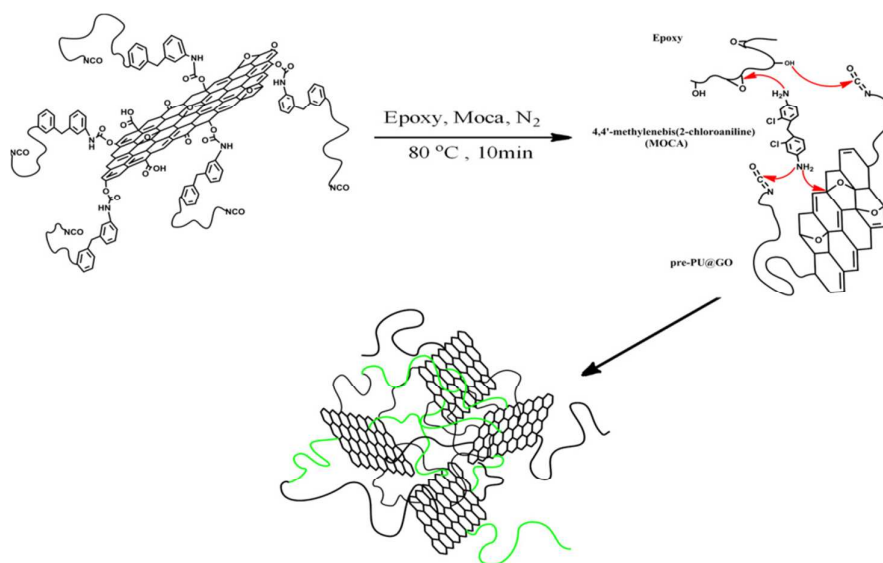
1 mechanical strength of the nanocomposites did not increase as much as with the other
2 methods discussed earlier. However, the enhancement of the electrical conductivity was
3 similar to the work discussed earlier. A conductivity of 10^{-4}Scm^{-1} was achieved at 4.0 wt% of
4 MEGO. Similar results were obtained for nanocomposites synthesized by introducing
5 functionalized graphene sheets (FGS) into waterborne polyurethane (WPS) using a chemical
6 polymerization method.

7 Finally, it should be noted that the reports of an exponential increase in the mechanical
8 strength of PU/graphene nanocomposites were obtained at very high levels of graphene
9 inclusion (20–60 wt%). This could explain the differences in the mechanical enhancements of
10 the different studies.

11 To improve the interfacial adhesion within the RGO/PU nanocomposite, the RGO was
12 functionalized with PCL by the esterification functionalization of GO, followed by a
13 reduction process¹⁴⁸. The PCL-modified RGO (PCL-RGO) was blended with PU in a DMF
14 solution and subjected to electrospinning. FT-IR indicated a peak shift in the carbonyl group
15 from 1724 to 1720 cm^{-1} , which was assigned to the change that occurred to the carboxylic
16 acid of the ester group (Figure 24). In addition, the peak of the C-H stretching was prominent,
17 as the effect of grafting long-chain C-C groups of PCL onto GO. Generally, the addition of
18 GO, f-GO, and r-GO increased the breaking stress of PU nanocomposites (Table 2). The
19 addition of 0.1 wt% of f-GO improved the breaking stress up to 9.3 MPa, which was 1.2
20 times higher than that of the pure PU nanofiber itself (7.8 MPa). Moreover, the modulus also
21 increased to 41.4 MPa by the addition of 1 wt% of f-GO (pure PU nanofibers recorded a
22 modulus of 31.5 MPa). Interestingly, the f-GO nanofibers had an improved breaking stress
23 and modulus compared to those of the GO and rGO-loaded nanofibers at the same loading.
24 The improvement was closely related to the improved dispersion of functionalized graphene
25 in the PU polymer matrix compared to GO and r-GO. Nevertheless, the elongation at break

1 values of the GO, f-GO, and r-GO composite nanofibers were also higher than that of the
2 pure PU nanofibers. However, the increase in the elasto-plastic behavior of graphene requires
3 additional characterizations because the addition of fillers commonly tends to cause a
4 decrease in the elastic behavior of the main matrix itself. The crucial shape memory
5 properties of PU were also discussed in this study. PU/graphene nanofibers recorded shape
6 recoveries higher than 90% in the first cycle, while the pure PU nanofiber web was 88.3%, as
7 plotted in Figure 25. However, the trend decreased with increasing cycles, although the
8 values achieved remained higher than 80%. Particularly, the shape recovery time decreased
9 significantly when graphene was incorporated into the nanofibers matrix, similar to the GO,
10 f-GO, and RGO samples. The properties were ascribed to the increase in graphene content,
11 which significantly disrupted the polymer flexibility, therefore resulting in the decrease in
12 shape recovery. The overall shape retention results are listed in Table 3.

13



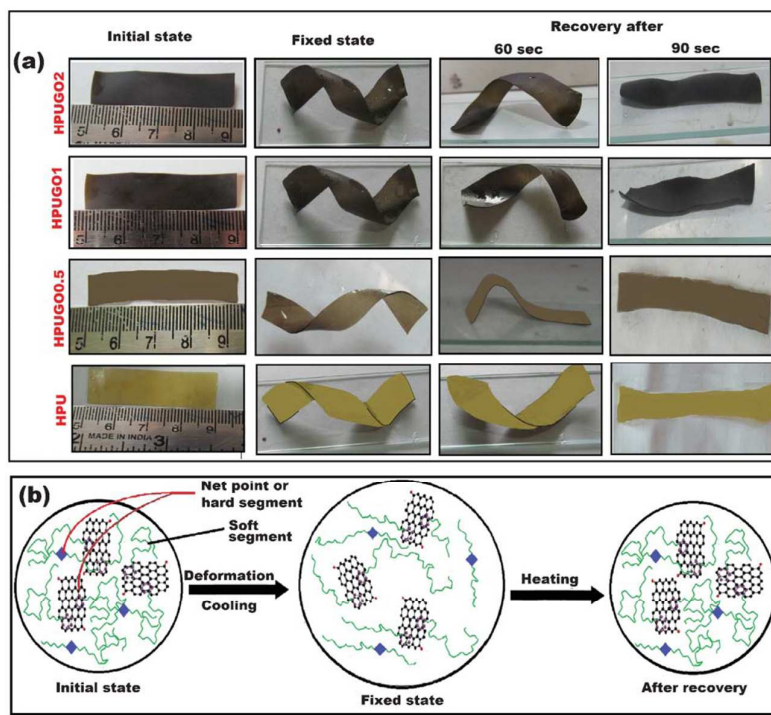
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15 Figure 21. Solidification mechanism for PU/GO/EP nanocomposites. Reprinted with

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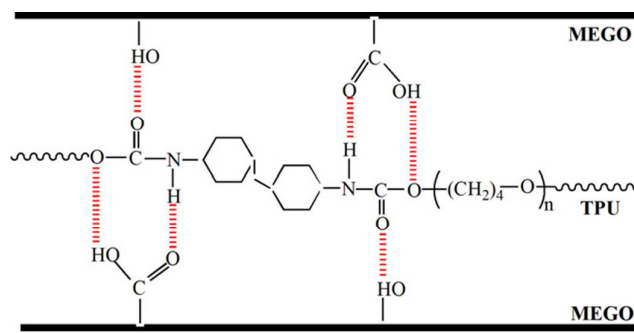


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3 Figure 22. (a) Shape memory performance of HPU and HPU/GO nanocomposites and (b)
 4 possible mechanisms of graphene-enhanced shape memory. Reprinted with permission from

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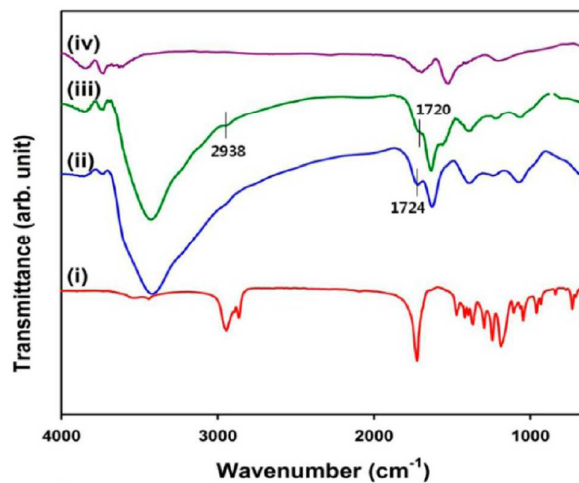
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8 Figure 23. Predicted interactions between polyurethane and MEGO layers. Reprinted with
 9 permission from ref. 20 (Copyright (2013) Elsevier)

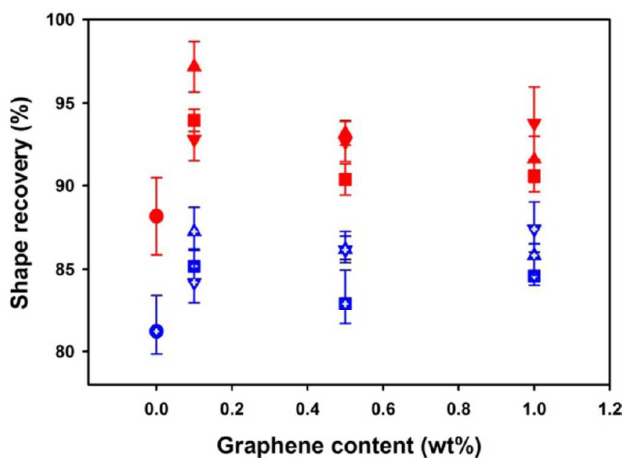
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3 Figure 24. FT-IR Spectra of (i) PCL, (ii) GO, (iii) f-GO and (iv) RGO. Reprinted with
4 permission from ref. 148 (Copyright (2014) American Chemical Society)

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7 Figure 25. Shape recovery of the pure PU and PU/graphene nanofiber webs with different
8 cycles (red and solid symbols, first cycle; blue and open symbols, fifth cycles; ●, PU; ■,
9 PU/GO; ▲, PU/f-GO; and ▼, PU/r-GO). Reprinted with permission from ref. 148

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1 Table 2. Tensile Properties of PU/Graphene Nanofiber Webs. Adopted with permission from
2 ref. 148 (Copyright (2014) American Chemical Society)

samples	graphene content (wt %)	tensile strength (MPa)	modulus (MPa)	elongation-at-break (%)
PU	0	7.8	31.5	406.7
PU/ GO	0.1	7.4	32.9	299.5
	0.5	8.3	33.7	412.9
	1.0	7.9	35.7	422.8
PU/f- GO	0.1	9.3	35.9	429.2
	0.5	8.5	36.9	515.4
	1.0	8.9	41.4	515.6
PU/r- GO	0.1	8.6	31.3	350.6
	0.5	9.1	33.1	553.6
	1.0	8.0	32.4	450.6

3

4 Table 3. Shape Retention (%) of PU/Graphene Nanofiber Webs. Adopted with permission
5 from ref. 148 (Copyright (2014) American Chemical Society)

cycle	PU	PU/GO			PU/fGO			PU/r-GO		
		0.1	0.5	1.0	0.1	0.5	1.0	0.1	0.5	1.0
1st	98.1	99.8	97.8	96.2	95.1	97.1	99.4	94.9	96.8	95.0
2nd	99.9	99.2	96.8	96.7	96.1	97.0	98.0	95.1	96.8	97.5
3rd	97.8	98.5	99.6	97.2	95.1	98.1	99.9	97.7	96.2	96.7
4th	97.3	98.3	98.9	97.9	98.2	97.5	98.7	96.9	95.9	96.9
5th	98.9	99.3	97.0	97.6	96.9	97.1	98.7	95.9	96.6	97.3

6

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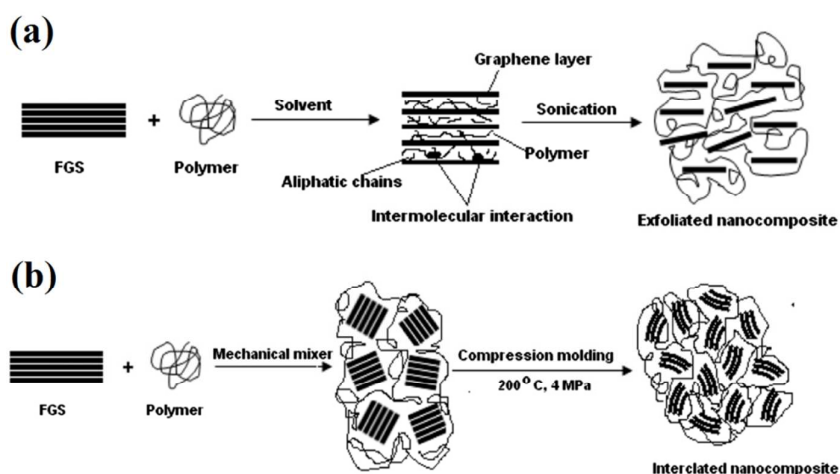
8 2.6.10 Poly(ethylene oxide) (PEO)/graphene/graphene oxide nanocomposites

9 The reinforcement effects of graphene in a PEO nanocomposite matrix have been
10 demonstrated using ¹³ two types of blending methods. Solution casting method showed a
11 parallel distribution of graphene compared to the nanocomposite surface, while the graphene
12 platelets were randomly distributed in melt blended nanocomposites (Figure 26). The two
13 different synthesis routes alter the thickness of the foliated graphene sheets. In the solution

1 casting method, the graphene sheets consist of two layers (thickness ~ 0.7 nm), while the melt
2 blended possessed 4 layers (thickness ~ 1.4 nm). There is also a difference in the
3 transparency of the solvent casted films compared to those manufactured using the melt
4 blended method, in which the former exhibited a higher transparency (87.6%) compared to
5 the latter (66%). This observation can be explained by the different arrangements of the
6 graphene sheets. In the melt blended sample, the graphene sheets are randomly oriented,
7 which causes the light to be randomly scattered, and thus reducing the transparency. There
8 was also a significant improvement in the mechanical properties. The performance
9 improvement was again the greatest for the solution casting method. The improvement in
10 Young's modulus at 2 vol% graphene was approximately 400% over the pristine polymer.
11 This compares with 100% for the melt blended sample. The large increase in the mechanical
12 properties was attributed to the well-dispersed state of the graphene sheets in the
13 nanocomposites, and a strong interfacial interaction between the graphene and PEO matrix
14 due to the high aspect ratio of graphene ¹⁴⁹. The inclusion of graphene also increased the
15 conductivity of the sample, and the percolation limits for both the solution and melt blended
16 samples were approximately 0.4 vol% and 1 vol% of graphene, respectively. This result
17 could be explained by the orientation of graphene sheets in the two nano-composites: in the
18 solution casting sample, the graphene sheets are aligned with the surface, whereas for the
19 melt blended sample they are randomly oriented. Another approach for the formation of a
20 PEO/graphene nanocomposite is to cause the PEO polymer chains to penetrate into the
21 interlayers of graphene by heating blends of the two materials at a weight ratio of 20:80 (PEO:
22 graphene) ⁹⁶. After heating for 12 h at 100 °C, the XRD peak attributed to crystalline PEO
23 almost disappeared, suggesting that many chains of the PEO polymer were constrained to
24 such an extent that crystallization was no longer possible. Moreover, an AFM analysis of the
25 sample surface confirmed that only parts of the PEO chains were absorbed onto the graphene

1 surface. Therefore, both XRD and AFM findings support the conclusion that only small
2 amounts of the PEO chains were absorbed on the surface of the graphene surfaces, while the
3 remaining larger portions penetrated into the graphene nanosheets. However, the effect on
4 the electrical and mechanical properties of the film cannot be determined since the paper did
5 not present any results.

6



7

8 Figure 26. Schematic diagram of graphene sheets incorporated into polymer by (a) solvent
9 blending method and (b) melt blending method. Reprinted with permission from ref. 13

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11

12 2.6.11 Polyimide/graphene/graphene oxide nanocomposites

13 High-performance polyimide (PI) is widely used in aerospace, optics, and microelectronics
14 because of its excellent properties, including a high mechanical strength, high thermal
15 resistance, and good chemical resistance. However, pristine PI is generally electrically
16 insulating in nature. Therefore, there is significant potential for the build-up of an
17 electrostatic charge on the surface of the material, which can cause damage to the component

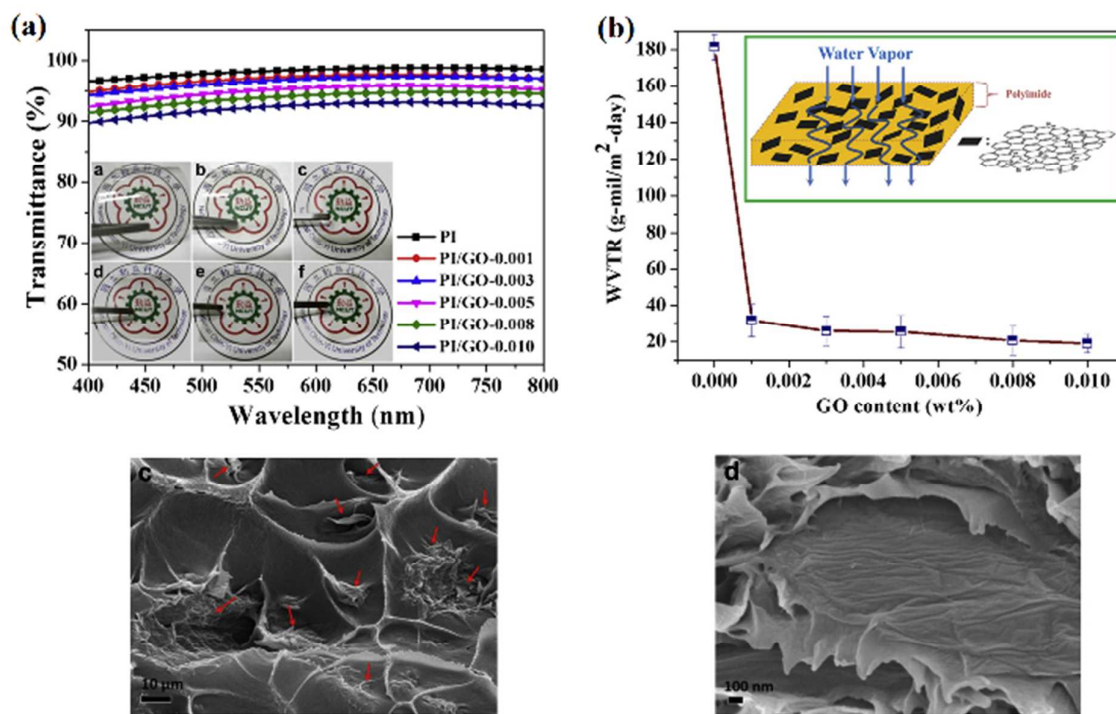
1 containing the film. To overcome this imperfection, GO can be introduced into the PI matrix
2 as a filler to improve the electrical conductivity, which the additional benefit of improving
3 the mechanical properties ⁹⁵. In this study, nanocomposites were fabricated by initially
4 modifying GO with ethyl isocyanate, which was then dispersed in a DMF solvent before the
5 nanocomposites were formed by in-situ polymerization. The electrical conductivities of the
6 0.3 wt% and 0.75 wt% graphene films were over 8 orders of magnitude higher than the neat
7 PI film. The 0.75 wt% graphene film had the highest conductivity of $8.9 \times 10^{-5} \text{ Sm}^{-1}$. The
8 Young's modulus and tensile strength of the composite film appeared to also slightly improve,
9 but the errors in the measured parameters make a definitive statement difficult.

10 As well as increasing the electrical conductivity, the addition of graphene also improves the
11 thermal conductivity but not by the same amount as the electrical conductivity. In this work,
12 the film made using 2.5 wt% of graphene had a thermal conductivity 25 % greater than a PI
13 film ¹⁵. However, the films were characterized using different methods. Graphene was
14 initially prepared via a thermal treatment of GO at 1000 °C in an inert atmosphere. An
15 appropriate amount of graphene (5–2.5 wt%) was dispersed in an N-Methyl-2-pyrrolidone
16 solution, following by PI. The prepared mixture was subjected to spin casting to obtain the
17 composite sheet.

18 The nanocomposites of PI/GO, prepared via in-situ polymerization, were used to improve
19 the friction and wear of the PI films ⁹⁴. The addition of graphene resulted in a 25 % reduction
20 in the coefficient of friction to ~ 0.29 and was not dependent, within the experimental error,
21 on the amount of graphene in the sample (over the range of 1–5 wt%). There is also strong
22 evidence that the wear rate was reduced by 23 % when the amount of GO added was 3.0
23 wt% . This reduction was attributed to the efficient formation of a graphene/PI film (transfer
24 film) on the metal “rubbing” contact. The GO-filled nanocomposite transfer films were more
25 uniform than the PI films, resulting in additional protection.

1 Ultra-low weight content GO (0.001 wt%)/ PI nanocomposites, prepared by solution mixing,
2 exhibited superior moisture barrier properties (an approximately 83 % improvement) over a
3 pure PI film, while retaining the visible light transmission of the film (Figure 27 a & b)³⁰.
4 Even at these small amounts of GO, there was significant improvement in the mechanical
5 properties: the storage modulus of PI/GO was recorded as high as 2474 MPa, with a 60 %
6 improvement compared to pristine PI with an addition of only 0.01 wt% of GO. The
7 improvement was attributed to the fine dispersion and high orientation of GO within the PI
8 matrix (Figure 27 c & d), which resulted in an increase in the reinforcement effect efficiency.
9 Furthermore, the wide distribution of GO with a high aspect ratio and high specific area
10 effectively extended the path the water vapor needed to take to pass through the film. This
11 seems to disagree with the results discussed earlier for films fabricated using isocyanated GO,
12 but the synthesis route was significantly different.

13 As a comparison, PI/RGO was prepared by using an in-situ polymerization technique, and the
14 investigation included the electrical and gas barrier properties of the nanocomposites⁹¹. As
15 expected, the incorporation of RGO greatly improved the electrical properties of the
16 nanocomposites as a result of the electrical percolation networks of RGO within the PI matrix.
17 The conductivity of the RGO/PI film(70:30) prepared using the in-situ polymerization
18 technique was approximately 10^{14} times higher ($1.1 \times 10^1 \text{ S m}^{-1}$) than that of a pure PI film
19 and even larger than the GO/PI composite prepared via the isocyanate route discussed earlier.
20 Furthermore, the oxygen transfer rate (OTR) was reduced by ~93 % ($375 \text{ cm}^3 \text{ m}^{-2} \text{ 24h}^{-1} \text{ atm}^{-1}$)
21 compared to the pristine one ($25 \text{ cm}^3 \text{ m}^{-2} \text{ 24h}^{-1} \text{ atm}^{-1}$). However, it had a higher weight
22 content of RGO (30 wt%) compared to the previous literature.



1

2 Figure 27 (a) UV-Vis spectra in visible light region of pure PI and PI/GO nanocomposite
 3 films, (b) effect of GO content on water-vapor transmission rate (WVTR) of pure PI and
 4 PI/GO films, FESEM images of (c) cross section of PI/GO-0.01 nanocomposites film (arrow
 5 indicates dispersed GO in matrix, and (d) magnified image of cross section shown in (c).

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8 2.6.12 Polyacrylonitrile/graphene/graphene oxide composites

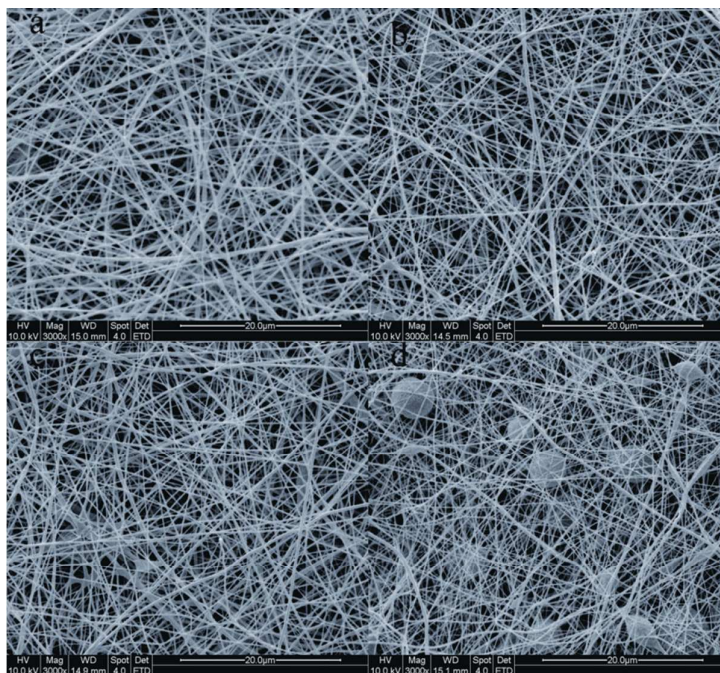
9 Polyacrylonitrile (PAN) is used as a precursor in the manufacture of carbon fiber, which is
 10 extensively used in the aerospace industry. Therefore, the effect of adding GO to PAN on the
 11 yield of carbon fiber has been investigated⁵⁹. In this study, the GO was prepared using the
 12 method of Hummers and Offman, and the polymerization was performed using an aqueous
 13 mixture of acrylonitrile, acrylamide, and GO at 60 °C for 3 h in a nitrogen atmosphere.
 14 Several samples with different GO weight contents (0, 0.05, 0.5, and 2.5 wt%) were prepared

1 and squeezed into thin membranes. As indicated by an FT-IR analysis, the GO sheets were
2 interconnected with the PAN matrix by means of hydrogen bonds. However, the addition of
3 GO slightly decreased the molecular weight. For the sample with the highest GO content (2.5
4 wt%), this decrease was approximately 12%. Below 300 °C, the GO/PAN composites were
5 stable, while the PAN sample saw a 5 % drop in weight. However, above this temperature,
6 the sample with 2.5 wt% showed a higher weight loss than the 0.5 wt% sample. By 350 °C,
7 the weight loss of the 2.5 wt% sample was very similar to that of the pure PAN sample.
8 However, the weight loss of the 0.5 wt% sample was always less than either the pure PAN
9 sample or the 2.5 wt% sample, even up to 900°C. Further evidence for this improved stability
10 was the observation of a 5 % increase in the carbon fiber yield for this sample.

11 In a similar attempt, nanofibers of a GO/PAN composite were prepared using a compounding
12 and electrospinning process⁴⁹. The precursor for the electrospinning solution was prepared
13 by initially dispersing the GO powder in an N,N-dimethylformamide (DMF) solution using
14 sonication, followed by the PAN powder. The structure of the electrospun PAN/GO
15 nanofibers was significantly affected by the addition of GO; the average diameter of the
16 composite nano-fibers decreased as the GO loading increased (Figure 28), and the nanofibers
17 were uniform in diameter. However, a beaded structure was found upon GO loading (see
18 Figure 28 d), which was due to the poor dispersion of GO in the DMF, causing an instability
19 in the liquid jet formed during the electrospinning process. The smooth surface and clear
20 fibril structure with the wrinkled morphology of pure PAN was altered to a coarser and
21 irregular morphology with an increase in the GO content (Figure 29). Interestingly, it was
22 also reported that at a low GO content (0.1 and 0.5 wt%), the nanofibers became “adhesive”
23 and would collapse into each other at the meeting point. The FT-IR spectra of the samples
24 showed no significant new peaks, indicating there was no chemical bonds between the PAN
25 chains and GO.

1 In another study ⁸⁵, electrospun PAN/GO nanofibers were prepared using a
2 dimethylformamide solvent, carbonized at 1200 °C, and then activated under air at 325 °C to
3 produce a textured and porous structure. Interestingly, the samples containing GO at 10 wt%
4 or less had a narrow diameter (140–165 nm) and a relatively smooth surface (Figure 30 a,b,d,
5 & e). However, at 15 wt% of GO, the diameter was larger (235 nm), with a rough surface
6 morphology (Figure 30 c & f). These observations provide evidence that excess GO in the
7 fiber will lead to a rougher surface and larger diameter as a result of the entanglement and
8 protrusion of GO. However, further work needs to be performed to verify this conclusion. It
9 is worth noting that electrochemical capacitors made using the 15 wt% GO sample had the
10 highest specific surface area and specific capacitance of 613 m²/g and 191.2 Fg⁻¹,
11 respectively, of all the samples made in this study.

12 A PAN/RGO composite was prepared via a conventional solution casting method with
13 dimethyl sulfoxide (DMSO) as the solvent ⁸⁶. The prepared composite recorded a significant
14 increase in electrical conductivity, attributed to the incorporation of partially reduced GO as a
15 conducting filler within the matrix.



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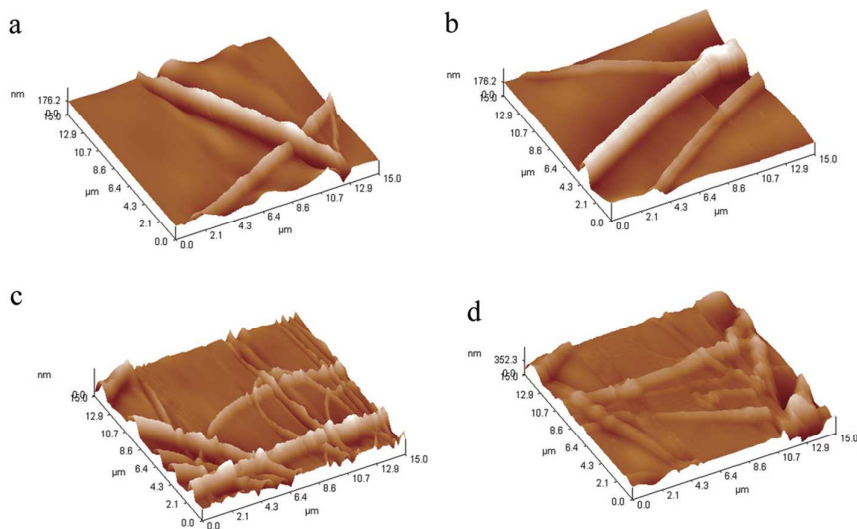
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Figure 28. SEM images of (a) PAN, (b) PAN/GO-0.05, (c) PAN/GO-0.1, and (d) PAN/GO

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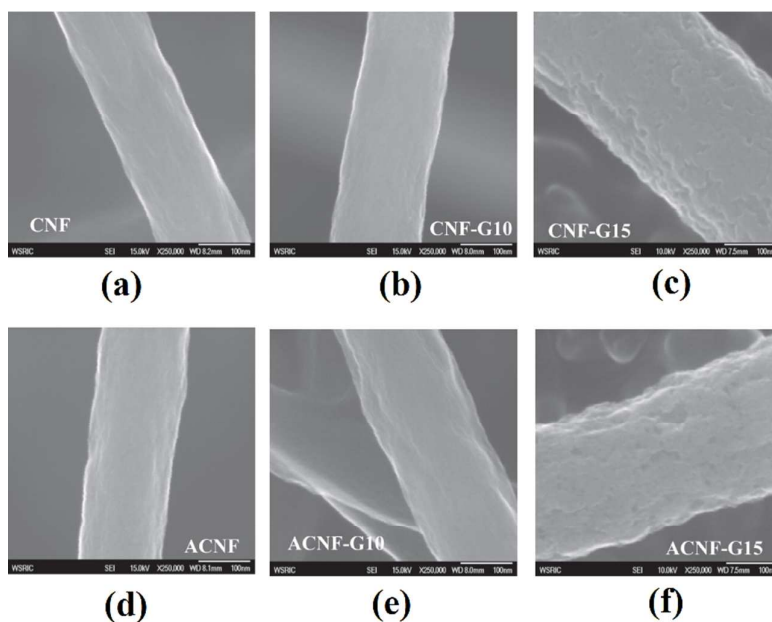
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Figure 29. AFM images of (a) PAN, (b) PAN/GO-0.05, (c) PAN/GO-0.1, and (d) PAN/GO

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2

3 Figure 30. SEM images of morphology of nanofibers electrospun from PAN before (a-c) and
4 after activation at 300°C. The GO contents of the samples were 0 wt% GO for (a and d), 10
5 wt% for (b and e), and 15 wt% for (c and f). Reproduced with permission from ref. 85

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8 2.6.13 Polycarbonate/graphene/graphene oxide nanocomposites

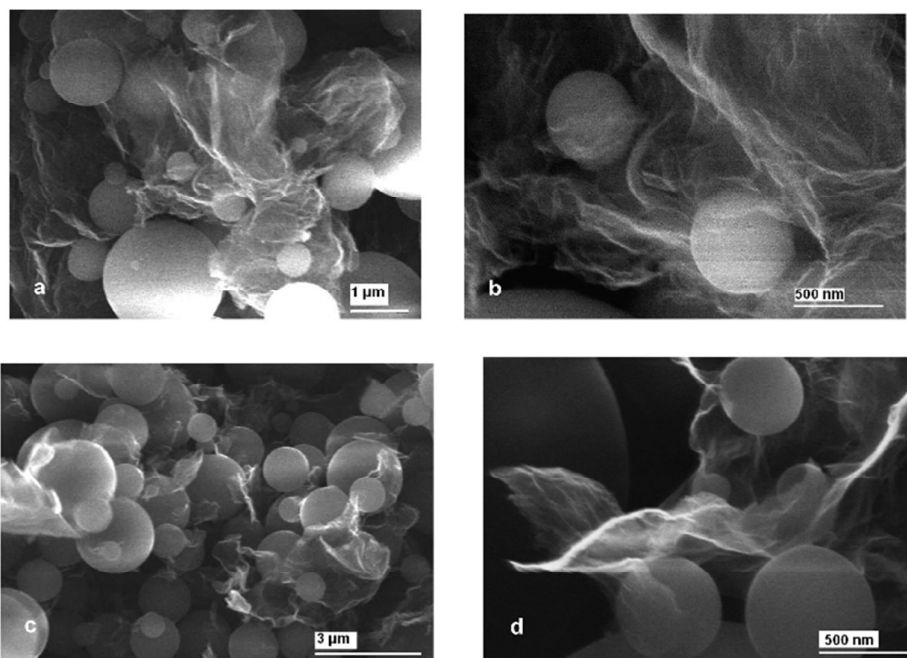
9 Polycarbonate (PC) was reinforced with thermally treated graphene oxide (GO) by using a
10 melt compounding technique⁵⁷. A comparison of the TEM micrographs of the platelets edge
11 on and face on indicates that the GO platelets were exfoliated after the melt process. Unlike
12 many other polymer/graphene composites discussed earlier, the incorporation of the GO did
13 not improve the tensile modulus, whereas the use of graphite did. However, there was an
14 improvement in the gas barrier properties of the nanocomposite. The gas permeability of He
15 on pure PC was reduced from 12.5 Barrer to 8.8 Barrer at 3 wt% of GO. Similarly, for N₂ gas,

1 the value also decreased from 0.36 Barrer to 0.20 Barrer. The percolation threshold, where
2 the electrical conductivity increases drastically, was approximately 0.1 wt% GO.

3 Another study of the electrical conductivity of PC/graphene nanocomposites was undertaken
4 by Yoonessi and Gaier⁸⁷. In their study, PC/graphene nanocomposites were prepared by the
5 emulsion mixing and solution blending methods, and the nanocomposites bearing 1.1 and 2.2
6 vol% of graphene recorded high conductivities. Samples bearing 2.2 vol% of GO prepared by
7 emulsion and solution mixing recorded conductivities of 0.512 and 0.226 S/cm, respectively.
8 The morphologies of these samples were slightly different; conductive graphene nanosheets
9 were wrapped around the PC microspheres (Figure 31), providing a conductive path for
10 electron transport. Furthermore, the graphene sheets had a wrinkling and irregular lateral
11 shape.

12 The thermal stabilities of both solid and foamed PC/graphene nanocomposites have been
13 evaluated at a fixed graphene content (5 wt%)⁸⁸. A nanocomposite was prepared via melt
14 compounding of PC and graphene, and to make the PC/graphene foam a one-step foaming
15 process with CO₂ was used. Both the foamed and solid nanocomposites were subjected to
16 thermogravimetric analysis. For the solid sample, the maximum degradation temperature
17 (T_{max}) of the composite increased compared to the sample containing only PC, indicating that
18 the presence of graphene platelets within the PC matrix aids the thermal stability. In addition,
19 the diffusion barrier effects of well-dispersed graphene nanofillers delay the escape of
20 volatile degradation products from the regions below the surface, thus improving the thermal
21 stability of PC/graphene nanocomposites¹⁵⁰. A very similar three-stage degradation was also
22 observed for the foam PC/graphene nanocomposites. However, there was a slight
23 improvement in thermal stability. The cellular structure of the foam composite decreased the
24 thermal conductivity, and so the inner parts of the sample were slightly cooler than the
25 outside.

1



2

3 Figure 31. SEM images of 0.55 vol % (a & b) and 1.1 vol % emulsion blended PC-G
4 microspheres covered with graphene. Reprinted with permission from ref. 87 (Copyright
5 (2010) ACS)

6

7 2.6.14 Contributions and challenges

8 Unlike natural polymers, most of the synthetic polymers possessed decent properties such as
9 high mechanical strength with high thermal stability. The addition of graphene successfully
10 imparted additional characteristic including electrical conductivity, high gas and moisture
11 barrier effect. Moreover, high mechanical strength and thermal stability of graphene still
12 contributed into the main matrix as an extra benefit towards the final properties of the end
13 products. Similarly for a polymer/ additive system, the characteristic of the binary system
14 could easily fine-tuned by tackling the ratio of each components, taking into accounts the
15 possible interactions within the dual phase system. Various literatures have reported in

1 graphene functionalization so as to achieve a better dispersion/ mixing of graphene in the
2 main matrix, which eventually could be the most promising way in achieving an efficient
3 graphene/ polymer system.

4

5 2.7 Conductive polymers

6 The findings in relation to conductive polymers have made possible the substitution of non-
7 metallic components for the metallic components used for conductors and semiconductors,
8 and extensive efforts have been made by numerous research groups to produce polymers with
9 various electrical, mechanical, and optical properties ^{151, 152}. Generally, a conductive polymer
10 possesses the unique properties of being able to conduct electricity in its solid state, high
11 processability, and low cost to synthesize compared to other conductive inorganic materials.
12 It also has high mechanical flexibility ¹⁵³. Often, these conductive polymers were added with
13 additives to increase its electrical conductivity in order to achieve a benchmark for specific
14 applications. The use of graphene to enhance the electrical properties of conducting polymers
15 is an obvious choice because graphene has good chemical stability ¹⁵⁴, high electric
16 conductivity ¹⁵⁵, and a large specific surface area ³⁴. The driving force to develop conducting
17 polymer fibers is the optimization of super-capacitors. These devices supplement advanced Li
18 ion batteries, which have high energy storage but poor power delivery ¹⁵⁶.

19

20 2.7.1 Polypyrrole/graphene/graphene oxide nanocomposites

21 Polypyrrole (PPy) is the most common conductive polymer, especially in energy storage
22 applications, because of its ease of synthesis, high conductivity, and, when used in a super-
23 capacitor, its relatively high capacitance¹²⁷. However, the main drawback of PPy is the poor
24 cycling stability caused by a mechanical rupture of the polymer fibers as a direct result of

1 their swelling and shrinkage during capacitor charging/ discharging^{157, 158}. Evidence from
2 other polymer/graphene polymers indicates that the presence of graphene nanosheets in the
3 polymer matrix leads to a significant improvement in the mechanical properties. Therefore,
4 by synthesizing PPy/graphene composites, the mechanical rupturing of the polymer should be
5 reduced, resulting in an improvement in the cycling stability. Therefore, a combination of
6 PPy with GO or graphene has been reported in various articles^{17, 159, 160}.

7 Polypyrrole/graphene nanocomposites were prepared via the in-situ polymerization of
8 graphite oxide (GO) and a pyrrole monomer, followed by the chemical reduction of GO to
9 graphene using hydrazine monohydrate⁵⁸. The GO sheets were surrounded by PPy in a
10 typical curved, layer-like orientation. However, upon reduction, the graphene sheets appeared
11 to have a wrinkled form. The magnitude of the conductivity of GO/PPy nanocomposites was
12 increased compared to the pure PPy sample, and this has been attributed to the π - π stacking
13 between the layers of GO and PPy. The conductivity increased even further after the
14 chemical reduction was performed, as a consequence of the large specific surface area and
15 the excellent conductive structure provided by graphene. A similar attempt was carried out to
16 prepare PPy/GO nanocomposites, without further chemical reduction of the GO¹²⁷. The
17 electrical conductivity of the nanocomposite film increased from 41.2 Scm^{-1} to 75.8 Scm^{-1}
18 with an increase in GO from 5 to 10 wt%, much higher than that of pure PPy film (1.18 Scm^{-1}).
19 Previous attempts to use PPy coating on carbon nanotubes (PPy-MWCNT) only managed
20 to achieve a conductivity of 2.40 Scm^{-1} , even with a loading of 50 wt% MWCNT¹⁶¹.
21 Similarly, in the previous report on the synthesis of PPy/functionalized MWCNT
22 nanocomposites via interfacial polymerization, the electrical conductivity recorded was
23 approximately 10 Scm^{-1} ¹⁶². In another attempt to improve the conductivity of PPy-MWCNT,
24 the nanocomposite was coated with Fe_3O_4 nanoparticles¹⁶³. The addition of 2.4 wt% of the
25 nanoparticles boosted the conductivity to 68 Scm^{-1} , which was still slightly lower than the

1 value achieved by PPy/rGO composites. Therefore, this finding significantly illustrates the
2 excellent conductivity imparted by graphene. It was also reported that the specific
3 capacitance increased to 421.42 F/g at a GO loading of 10 wt%, which indicated that the
4 presence of GO in the PPy matrix efficiently facilitates the formation of a charged
5 electrostatic interface layer responsible for the capacitance. Similar improvements in
6 electrical conductivity have been observed with significantly less graphene (1 wt%) using a
7 different synthesis method ¹²⁴. The in-situ polymerization of PPy/graphene was modified by
8 cationic polystyrenesulfonate (PSS). By the addition of only 1 wt% of graphene and 0.4 wt%
9 of PSS, the nanocomposite film exhibited a conductivity as high as 32.55 Scm⁻¹. This
10 significant improvement was attributed to PSS, which served as a dopant incorporated into
11 the PPy structure and efficiently improved the conductivity of the fabricated nanocomposites.

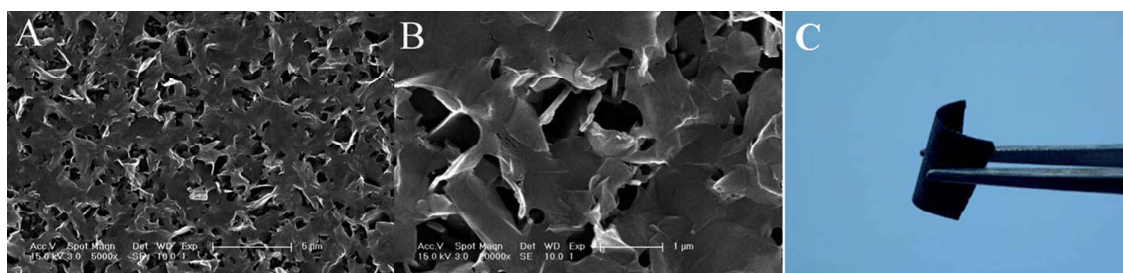
12 In another approach, polypyrrole/graphene nanosheets were synthesized via an in-situ
13 polymerization method with a pyrrole monomer and graphene nanosheets in an acidic
14 condition ¹²⁵. Graphene was initially prepared via the chemical reduction of graphene oxide
15 with hydrazine hydrate. The nanocomposites were then prepared by polymerizing the pyrrole
16 monomer in the presence of the graphene suspension. The PPy molecules surrounded the
17 graphene in an entangled structure, probably bonding via the hydrogen bonding interaction
18 and π - π stacking. The nanocomposites had a better capacitive performance and a better
19 cycling stability even when the amount of graphene was low (6.7 wt%). The inference of the
20 latter observation is that the addition of the graphene improved the mechanical properties of
21 the fibers, preventing them from breaking during the charging and discharging.

22 Nanocomposites of PPy/GO have also been prepared using an electrochemical method ^{18, 28},
23 where the PPy was electro-oxidized in a suspension containing GO, and the anionic GO
24 flakes were incorporated into the PPy/GO nanocomposites during growth. During this
25 process, the GO was reduced electrochemically to form the PPy/RGO composite. The

1 electrodeposited PPy/GO nanocomposites were highly porous, with a uniform PPy coating on
2 the surface of two-dimensional GO sheets (Figure 32 a & b). The nanocomposites obtained
3 by this method were flexible and freestanding (Figure 32 c). The films exhibited good
4 electrochemical performance as well as improved cycle stability.

5 The commercial adoption of this technology in supercapacitors will require the films to be
6 economically viable but also in a form that can be easily used in a manufacturing process.
7 The manufacture of a PPy/GO free standing nanocomposite paper^{18,28} addressed these issues
8¹²⁶. A precursor solution containing 0.1g of GO and 1mmol of pyrrole monomer were
9 ultrasonicated and then oxidized by the addition of ammonium persulfate. The resultant
10 mixture was filtered through a millipore filter and subjected to washing and drying to form
11 the nanocomposite paper. The free-standing paper had a high specific capacitance (330 F/g)
12 measured with a high scan rate of 100 mV/s. Furthermore, the nanocomposite paper showed
13 only a 9% decrease in capacitance after 700 cycles at 100 mV/s, indicating a superior
14 electrochemical stability. For comparison purposes, a PPy/GO nanocomposite (20 wt%)
15 prepared by liquid/liquid interfacial polymerization had a specific capacitance, at a 100 mV/s
16 scan rate, of only 92.2 F/g, with a high weight content of 20 wt%. Morphological analysis
17 showed that the GO sheets were uniformly dispersed within the PPy matrix¹²⁸.

18



1 Figure 32. (a & b) FESEM images of PPy/RGO nanocomposites, (c) photograph of free-
2 standing flexible PPy/GO nanocomposites. Reproduced with permission from ref. 18

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4 2.7.2 Polyaniline/graphene/graphene oxide nanocomposites

5 PANI is one of the common yet unique conductive polymers mainly due to its electronic ¹⁶⁴,
6 thermoelectronic and good optical properties. However, less thermal stability and the
7 stiffness of its polymer backbone limits its application in industrial field ^{165, 166}. Thus,
8 numerous approach had been conducted in order to alter its characteristic. As reported in
9 literature, a PANI/chemically converted graphene (CCG) composite film was prepared using
10 a simple vacuum filtration method for a mixed suspension containing PANI nanofibers (PNF)
11 and CCG ¹³¹. The prepared nanocomposite film possessed a layered sandwich morphology,
12 with the PANI nanofibers sandwiched between the CCG layers. The unique arrangement was
13 probably caused by the flow assembly of graphene sheets during the filtration process (Figure
14 33 a & b). As a result, the layered structure provided additional surface area, which is crucial
15 for super-capacitor applications. Moreover, the fabricated PANI/CCG nanocomposite films
16 possessed a free-standing property and were highly flexible, as shown in Figure 33 e. The
17 electrochemical characterization on CCG/PNF30 wt% (PNF₃₀) showed a conductivity of 5.5
18 $\times 10^2 \text{ Sm}^{-1}$, which was one order higher than pristine PANI nanofibers. Additionally, this
19 value was much higher than previously reported literature which utilized carbon black (CB)
20 nanoparticles/PANI nanocomposites ¹⁶⁷. The electrical conductivity achieved was only up to
21 1.38 Scm^{-1} even with loading of CB (23 wt%). Similarly, the electrical conductivity of
22 multiwalled carbon nanotube (MWCNT)/PANI nanocomposite was only $1.75 \times 10^{-2} \text{ Sm}^{-1}$
23 even with reinforcement of metallic components ¹⁶⁸. Meanwhile, non-covalent coating of
24 MWCNT with PANI nanosphere achieved 2.63 Scm^{-1} but with very high amount of CNT
25 added (30 wt%) ¹⁶⁹. Using the films as electrodes in a double electrode supercapacitor cell,

1 the measured specific capacitance was 210 F/g at a current density of 0.3 A/g. Even after 800
2 charging/discharging cycles, the capacitance value remained at 155 F/g.

3 Another approach was attempted to prepare PANI/graphene nanocomposites by the oxidative
4 polymerization of aniline monomers using ammonium peroxydisulfate as the solvent¹³⁰. The
5 nanocomposite surface achieved an inter-penetrating network structure of PANI/graphene. At
6 the aniline to graphene ratio of 1:2, the specific capacitance was recorded to be between 300
7 and 500 F/g, with good cycling stability when measured over 100 cycles. These
8 measurements were made at a lower current density of 0.1 A/g compared to the work
9 discussed in the previous paragraph.

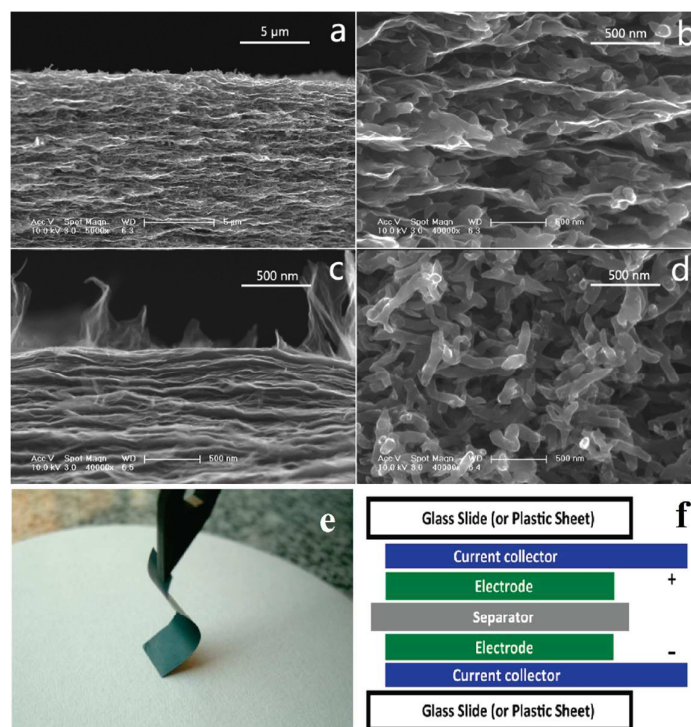
10 RGO sheets directly coated with PANI using an in-situ polymerization technique were
11 reported to have a worm-like morphology, with the paper and wrinkle structure of RGO but
12 thickened as a result of the PANI coating on the surface¹²⁹. The specific capacitance was
13 measured to be as high as 361 F/g at a current density of 0.3 A/g, with the capacitance falling
14 to 82 % of its original value after 1000 cycles.

15 Layered graphene spray dried into porous microspheres was used as a substrate for the
16 growth of polyaniline nanowire arrays using in-situ polymerization²⁷. The crucial point of
17 this technique was the formation of graphene microspheres within the nanocomposites, which
18 were interconnected with few structural defects. These microspheres formed a highly
19 conductive network that facilitated the electrical conductivity of the PANI. The PANI
20 attached to the graphene sheets had a nanowire-like morphology; the diameter and length
21 depended on the concentration of the aniline monomer (Figure 34 a & b). Furthermore, the
22 specific capacitance only decreased to 87.4 % of its original value after 10,000 cycles at a
23 current density of 3 A/g (Figure 34 c & d).

1 The post in-situ reduction of graphene oxide/PANI nanocomposites was achieved and
2 reported ¹³². PANI was synthesized via micro-emulsion polymerization, where nanosphere-
3 scaled PANI was obtained. By utilizing the electrostatic attraction between the oppositely
4 charged species (PANI was positively charged and GO was negatively charged), the species
5 were attracted to each other. The resulting layer-by-layer PANI nanosphere coating on the
6 GO was confirmed by SEM images, with porous channels observed within the nanostructure
7 (Figure 35). The composition of the nanocomposites was fixed by controlling the volume of
8 the suspensions added. It was reported that the best composition of GO:PANI was 60/40,
9 whereby the nanocomposites possessed both desirable morphological and electrochemical
10 properties. The GO/PANI nanocomposites were further treated with hydrogen iodide (HI) to
11 reduce the graphene oxide to graphene. As expected, the UV-Vis spectra indicated the major
12 characteristic peaks of PANI. However, a new characteristic peak was detected at 268 nm,
13 which corresponded to graphene. In addition, the absorption peaks of the nanocomposite
14 were also reported to be broader, smaller, and recorded at higher wavelengths, therefore
15 confirming the strong π - π conjugation between PANI and graphene ¹⁷⁰. The unique
16 morphology acquired was related to the vacuum-assisted self-assembly (VASA) and in-situ
17 reduction process applied. In order to relate the porous nanostructure to the capability of
18 allowing penetration of electrolyte ions into the interior, an electrochemical performance test
19 was conducted using the PANI/graphene nanocomposite as an electrode material. Both PANI
20 and PANI/graphene showed typical pseudo-capacitance behaviors in the CV profiles (Figure
21 36). However, the higher current density achieved for the nanocomposites indicated a higher
22 specific capacitance. Similarly, the specific capacitance calculated for the PANI/graphene via
23 the discharge curves at 0.5 A/g was 448 F/g, which was much higher than that of a graphene
24 film (133 F/g) and PANI film on an SSE electrode (241 F/g). The capacitance retention
25 remained at 81% even after 5000 cycles of the charging/discharging process. This was

1 attributed to the protection of the PANI nanospheres by sandwiching them between the
2 graphene layers, which was realized through a layer-by-layer approach. This improved the
3 mechanical properties and increased the cycling performance of the as-synthesized material.

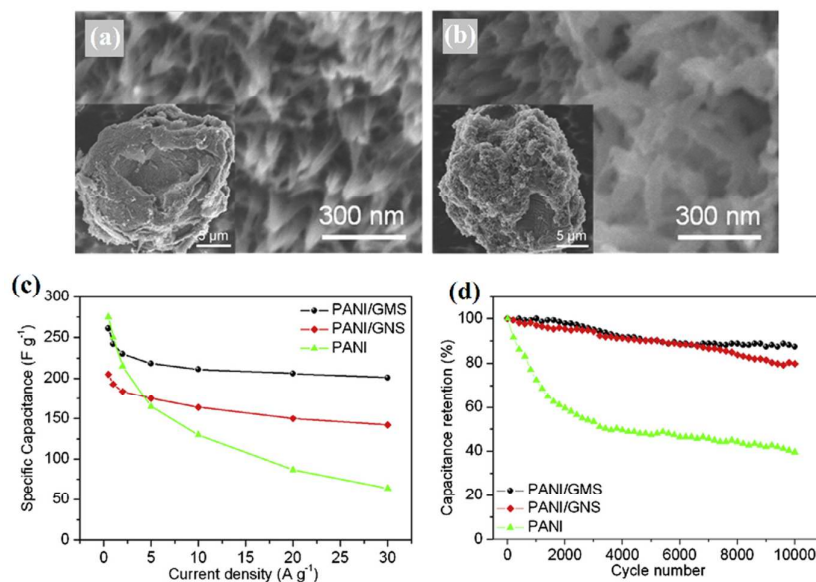
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6 Figure 33. Cross sectional SEM images of (a & b) CCG/PNF₃₀, (c) pure CCG, (d) PANI-NF
7 film; (e) photograph of flexible CCG/PNF₃₀ film; (f) two-electrode configuration. Reprinted
8 with permission from ref. 131 (Copyright (2010) American Chemical Society)

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1

2 Figure 34. SEM images of PANI/GMS nanocomposites at different aniline concentrations of

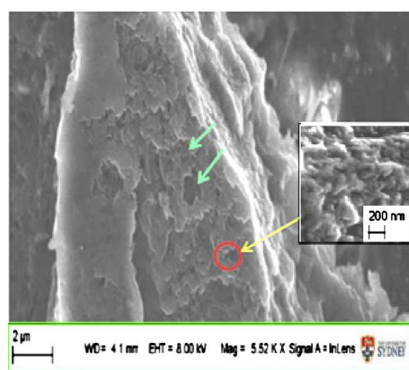
3 (a) 0.05M, (b), 0.06M; (c) graphs of specific capacitances of PANI, PANI,GNS, and

4 PANI/GMS measured at different current densities; and (d) cycling profiles of PANI,

5 PANI/GNS, and PANI/GMS measured at current density of 3 A/g. Reproduced with

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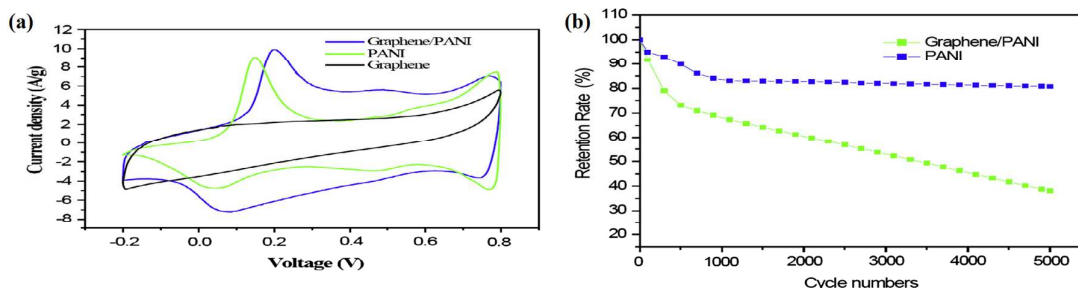


8

9 Figure 35. SEM image of graphene/ PANI film. The green arrow illustrates the porous
10 structure of graphene/ PANI film and the agglomerated PANI spheres on graphene sheets

11 (red circle). Reprinted with permission from ref. 132 (Copyright (2014) Elsevier)

1



2

3 Figure 36. CV profiles of graphene/ PANI, PANI on SSE and graphene (a); and cyclic
4 stability of Graphene/PANI and PANI measured at 2 A/g. Reprinted with permission from
5 ref. 132 (Copyright (2014) Elsevier)

6

7 2.7.3 Polyacetylene/graphene/graphene oxide nanocomposites

8 Graphene was covalently functionalized with polyacetylene (PAC) through a simple nitrene
9 chemistry reaction¹³⁴. The reaction took place between reactive azido groups of the PAC
10 backbone chains and graphene. The prepared PAC/graphene nanocomposites became soluble
11 in different organic solvents, therefore providing a new alternative way to make graphene
12 soluble in organic solvents. Another method to prepare water soluble graphene sheets¹³³ was
13 initiating the chemical reduction of GO in the presence of polyacetylene and a quaternary
14 ammonium pendant (Pac) at a ratio of 1:3 (Pac/GO). The adsorption of Pac onto the graphene
15 sheet was attributed to the π - π interaction and electrostatic interactions between the materials,
16 resulting in an enhanced solubility of Pac/Go in water.

17

18

1 2.7.4 Poly(3,4-ethylenedioxythiophene) /graphene/graphene oxide nanocomposites

2 Poly(3,4-ethylenedioxythiophene)(PEDOT) is another popular type of conductive polymer

3 due to its high flexibility, processability, and lower production cost compared to other

4 conventional conductive inorganic materials. However, the application of this material in

5 electronic devices is limited by its relatively low conductivity and poor mechanical features.

6 Various methods have been tried to enhance the electrical properties such as in-situ

7 polymerization¹⁷¹⁻¹⁷³ and vapor phase polymerization^{174, 175}. Both methods improve the

8 electrical conductivity. However, they fail to enhance the mechanical strength. In a recent

9 attempt, graphene sheets were incorporated into a PEDOT matrix using the spin-coating

10 method⁶⁰. The graphene was obtained by the reduction of a GO precursor using hydrazine

11 hydrate. PEDOT was then spin-coated onto the graphene layer to produce a two-layer

12 PEDOT/graphene composite film. For a three-layer graphene/PEDOT/graphene film, GO

13 was initially spin-coated on a substrate, followed by a reduction process using hydrazine

14 hydrate. The consecutively layer of PEDOT was spin-coated, whereby the surface of the

15 PEDOT layer was treated with ozone to introduce hydrophilicity. Lastly, another layer of GO

16 was spin-coated again before the reduction process in hydrazine vapor (Figure 37). The two-

17 layer composite film exhibited a smoother morphology than the initial PEDOT film, which

18 consisted of many protruding surfaces with irregular shapes (Figure 38). The formation of a

19 uniform surface was attributed to the hydrophobicity of the graphene sheets. Interestingly, the

20 morphology of the graphene/PEDOT/graphene composite was more uniform than the two-

21 layer composite due to the stacking of graphene sheets onto the PEDOT layer. Furthermore,

22 the conductivity of the graphene/PEDOT film was measured to be as high as 13 Scm^{-1} , which

23 is an improvement of over 100% compared to the conductivity of a pristine PEDOT film (6

24 Scm^{-1}) (Figure 39 a). This value was also among the highest in electrical conductivity

25 achieved for PEDOT, where previous works in modifying PEDOT achieved the conductivity

1 of only 2.93 Scm^{-1} with addition of 27% of MWCNT¹⁷⁶. However, the three-layer film
2 recorded a slightly lower conductivity of 12 Scm^{-1} , which was caused by the insulating layer
3 of GO found underneath the reduced graphene. The reduction process for the GO only
4 occurred on the top side of the graphene layer. Mechanically, the double-layer composite film
5 recorded a stress of 60 MPa at a 1.0 % strain, whereas the three-layer film showed a stress of
6 65 MPa at a 1.0 % strain (Figure 39 b).

7 An alternative route for the fabrication of PEDOT/graphene oxide films for electrochemical
8 sensing was attempted via electrodeposition from an aqueous solution containing a dispersion
9 of GO and EDOT monomer¹³⁶. The electrochemical deposition was performed by cyclic
10 voltammetry (CV) with the potential scanning fixed between -0.2 and 1.2 V vs. an Ag/ AgCl
11 electrode at a scan rate of 100 mVs^{-1} , under the conditions of magnetic stirring and
12 continuous nitrogen gas bubbling. The deposited film was described as uniformly deposited
13 on the surface of the glassy carbon electrode (GCE), showing high roughness and a loose
14 structure formed by wrinkle-like sheets. The composite film exhibited good electrical
15 performance, with a much lower charge transfer resistance (R_{ct}). This was attributed to the
16 higher specific surface area, which facilitated the electron transfer between the solution and
17 electrode interface.

18 The effect of varying the process parameters has been studied for a PEDOT/GO composite
19 films synthesized by electrochemical reduction reactions¹³⁵. A two-step process was
20 performed. First, a PEDOT/GO film was electrodeposited on GCE or tin-oxide glass (TO
21 glass) from an aqueous mixture of GO/EDOT at constant potentials of 0.94, 0.97, and 1.05 V.
22 Then, an electrochemical reduction was carried under an inert atmosphere in 0.1M KCl
23 solution at a fixed potential of -0.85V vs. an Ag/ AgCl electrode for 10, 20, or 30 min. The
24 negative surface charges on the GO were able to serve as the counter ions in the
25 electropolymerization of the PEDOT. As shown in Figure 40 a & c, the surface morphology

1 of the PEDOT/GO film became more wrinkled, and there was an increase in surface
2 roughness as the reduction reaction time increased (Figure 40 e & f). In addition, the cross-
3 sectional views of the composite films indicated that they exhibited a layered structure in a
4 compact and well-ordered form (Figure 40 b & d). Although XPS analysis confirmed that the
5 reduction reaction removed the epoxy and hydroxyl groups from the GO surface, the
6 electrical conductivity of the polymer matrix increased only marginally from 9.8×10^{-5}
7 Scm^{-1} to $1.0 \times 10^{-4}\text{Scm}^{-1}$ when the reduction time of the PEDOT/GO on TO was increased
8 from 0 to 30 min.

9 Electrochemical polymerization has also been utilized to fabricate PEDOT/ modified
10 graphene composites for energy storage applications ²⁶. Prior to electro-polymerization, the
11 graphene was chemically functionalized in a sulphuric/ nitric acid mixture (3:1) and sonicated
12 for 6 h. The suspension was filtered on a carbon cloth to form a graphene paper layer
13 (GP/CC). The GP/CC was used as a substrate for the electro-deposition to occur, at a fixed
14 potential of 1.2 V versus Ag/AgCl electrode in acetonitrile. The prepared composites were
15 immersed in Pt solution for 24 h. After coating the CC with the graphene layer, a sheet-like
16 structure with wrinkles was observed. PEDOT particulates on the GP/CC were observed, and
17 they had a higher density than the PEDOT deposited on CC. Interestingly, the capacitive
18 performance of the PEDOT/GP/CC measured in a three-electrode configuration using a
19 Ag/AgCl reference cell was as high as 714.93 F/g, which is approximately 6 orders of
20 magnitude higher than that of PEDOT/CC. This effect was attributed to the high specific
21 surface area of graphene.

22

23 2.7.5 Poly(3-aminobenzene sulfonic acid)/ graphene nanocomposites

1 The application of Poly(3-aminobenzene sulfonic acid) (PABS) conducting polymers in
2 electronic fields has rarely been reported elsewhere in the literature. However, Pham et al.
3 reported on the fabrication of water-dispersible GNS functionalized with PABS to induce
4 hydrophilicity⁷¹. The modification was performed via the covalent bonding of PABS on GO,
5 based on the amidation reaction between the acyl chloride groups present on the GO surface
6 after modification with the amino group present on the polymers, as shown in the illustration
7 in Figure 41 a. The GO eventually reduced to graphene via a chemical reduction method
8 using sodium borohydride (NaBH₄). The presence of sulfur and nitrogen elements on PABS-
9 grafted-GNS (PABS-g-GNS) was confirmed via an EDX spectrum, which showed the
10 successful chemical grafting of PABS on the GNS surface through amide bonds. Furthermore,
11 the molar ratio of O to C decreased from 0.387 to 0.197, indicating that the reduction process
12 converted GO to graphene. Moreover, the surface modification was observed and confirmed
13 via FESEM, as shown in Figure 41 b & c. The electrical conductivity of PABS-g-GNS was
14 recorded at 29.4 S m⁻¹, which was better than that of pristine GO (3.1 × 10⁻⁶ Sm⁻¹). However,
15 the result was not sufficient to prove the improvement by the hybrid functionalization, as the
16 increase in conductivity might be due to the reduction of graphene oxide species to graphene.
17 In order to examine the hydrophilicity, the prepared PABS-g-GNS (0.5 mgml⁻¹) was
18 dispersed into distilled water, followed by ultrasonication for 30 min. The dispersibility of the
19 PABS-functionalized GNS dramatically increased compared to graphene oxide, as shown in
20 Figure 42, indicating the presence of covalently bonded PABS, which served as hydrophilic
21 groups.

22

23

24

1 2.7.6 Contributions and challenges

2 Electronically conductive polymers have received so much attention mainly because they

3 generally conduct electricity, as well as highly desirable polymer properties such as

4 flexibility, low density and ease of structural modifications. The introduction of graphene has

5 successfully contributed a large area, highly conductive template with beneficial tensile

6 strength towards the overall composites structure. Especially in the field of energy storage/

7 conversion system, graphene provides mechanical strength which stabilize the composites

8 structure, allowing continuous infuse/ outflow of electrolytes ions without suffering

9 mechanical degradation/ rupture. Additionally, the high conductivity of graphene template

10 indirectly minimize the resistance occurred throughout the transfer of electrons between the

11 electrode/ electrolyte boundaries. Despite all the advantages, the critical challenge relies on

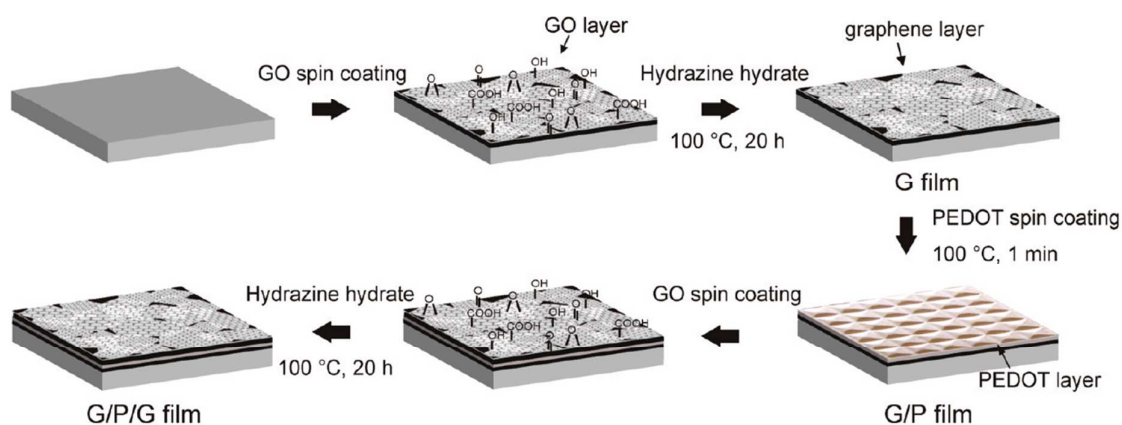
12 designing an efficient composite structure with proper spacing of individual graphene layers.

13 The appropriate graphene spacing effectively prevents restacking and retaining high surface

14 area of graphene, while providing empty spaces for molecules or ions to intercalate. These

15 issues encourage more future works worth for uptake as the current potential of graphene in

16 conductive polymers is highly promising.

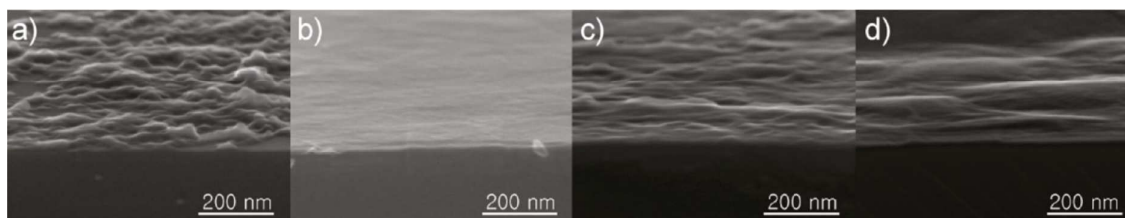


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18 Figure 37. Schematic diagram of fabrication process for graphene/PEDOT/graphene

19 composite film. Adopted with permission from ref. 60 (Copyright (2010) ACS)

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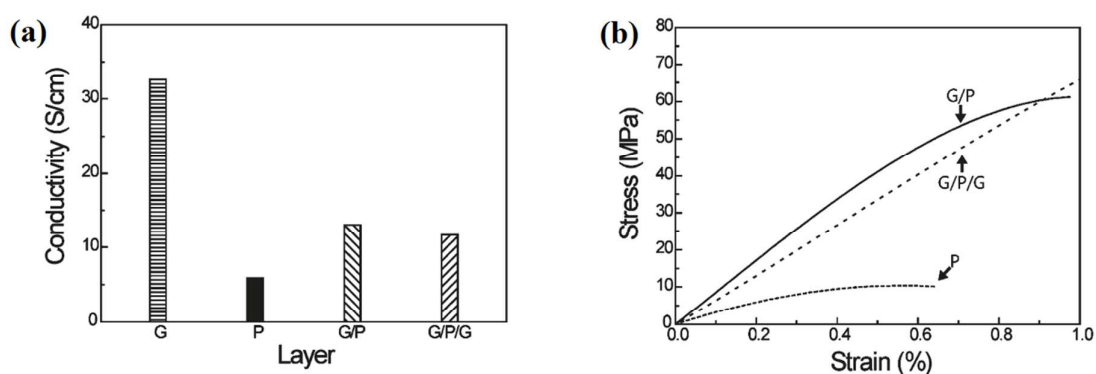
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3 Figure 38. SEM images of (a) pristine PEDOT, (b) graphene, (c) graphene/PEDOT film, and
 4 (d) graphene/PEDOT/graphene film. Adopted with permission from ref. 60 (Copyright (2010)

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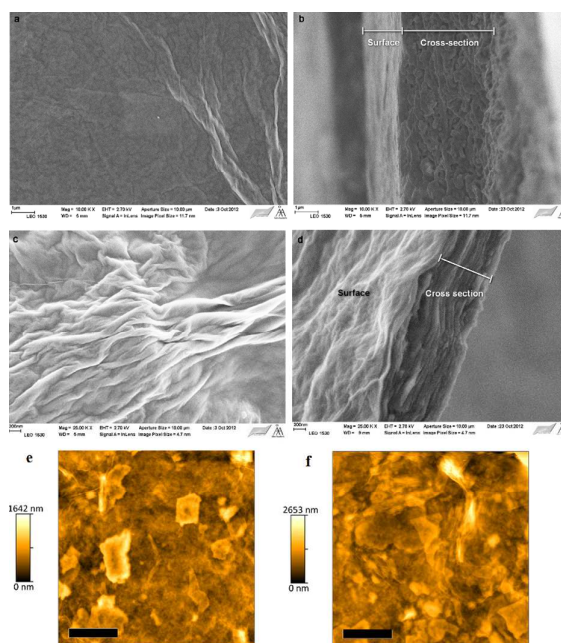
8 Figure 39. Graphs of (a) conductivity and (b) stress–strain curves of pristine PEDOT,

9 graphene/PEDOT, and graphene/PEDOT/graphene composite films. Adopted with

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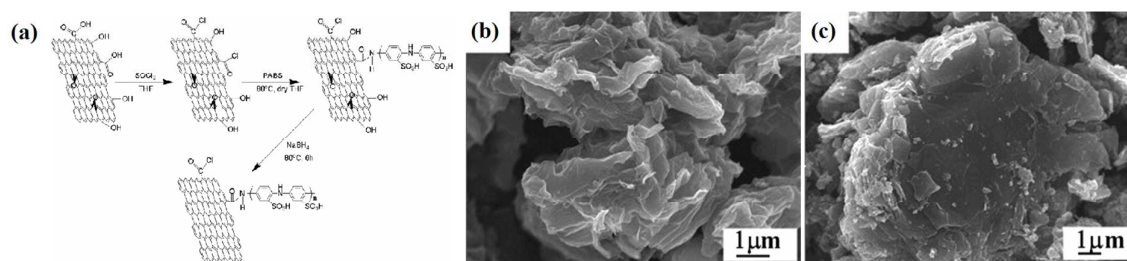
2 Figure 40. SEM micrographs of PEDOT/GO films electrochemically reduced at -0.85 V for

3 (a & b) 0 min and (c & d) 20 min, where (b) and (d) show cross sections. AFM images of

4 PEDOT-GO films reduced at -0.85 V for (e) 0 min and (f) 20 min. Reproduced with

5 permission from ref. 135 (Copyright (2013) Elsevier)

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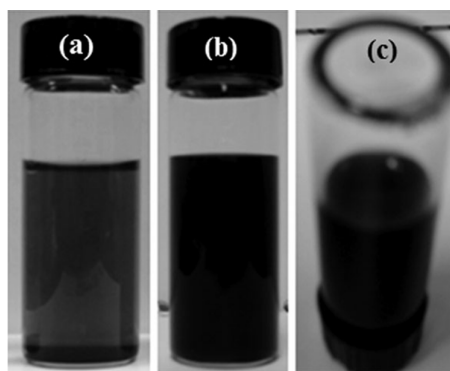
8 Figure 41. The schematic illustration in functionalization of graphene oxide by PABS and

9 FESEM images of (b) GO and (c) PABS-g-GNS. Reproduced with permission from ref. 71

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1

2 Figure 42. Digital images of dispersed states in distilled water of GO (a) and PABS-g-GNS

3 (b). The image of dispersed state of PABS-g-GNS(c) shows a negligible aggregation at the

4 bottom of vial. The images were taken after 2 weeks of storage at room temperature. Adopted

5 with permission from ref. 71 (Copyright (2012) Elsevier)

6

7 **Summary and perspectives**

8 There is no doubt that polymeric-based graphene nanocomposites are some of the

9 most scientifically promising advancements in graphene-based materials and polymeric

10 components. Despite the rapid developments, there are still numerous challenges that must be

11 tackled and considered in order to unleash their full performance. For example, although it

12 has been reported that pristine graphene is capable of being homogeneously dispersed within

13 the polymer matrix of some organic polymers, the π - π stacking interactions often result in the

14 agglomeration of graphene sheets within the polymer matrix, which results in non-

15 homogeneous morphologies and inferior properties. In order to improve the properties, the

16 dispersion of graphene within the polymer components needs to be enhanced, which has been

17 attempted by the surface modification of graphene sheets with functional groups. The surface

18 modification of graphene involves a wide range of techniques that have been carried out by

19 numerous researchers with various modifying agents, including amphiphilic copolymers⁵⁵,

1 organo-modifying agents such as phenylisocyanate ⁷⁰, and polyacetylene ^{133, 134}, for which it
2 was reported that the functionalized graphene sheets were soluble in water. The solvent
3 dispersible properties of graphene play an important role in facilitating the preparation of
4 polymer-based graphene composites.

5 The preparation methods, characterizations, and properties of polymer composites filled with
6 different graphene-based nanofillers were discussed thoroughly in this review. Generally, the
7 majority of the properties of polymer/graphene nanocomposites were shown to be much
8 greater than the pristine matrix. These improvements were obtained mainly at a minute
9 amount of graphene loading (approx. 1–5 wt%) ^{22, 53, 91, 101, 105, 148}, while higher graphene
10 loading (>20 wt%) ⁹¹ mostly resulted in adverse effects. However, the input amount of the
11 graphene is closely related to the final properties of the polymer matrix. The following
12 enhancements in the properties of polymer-based graphene composites were discussed:

13 (i) Graphene/polymer nanocomposites exhibited significant enhancements in mechanical
14 properties compared to the pristine polymer. However, different preparation methods
15 eventually affected the properties achieved. For example, PEO/graphene nanocomposites
16 ¹³prepared by solution casting recorded a remarkable enhancement in tensile strength as high
17 as 189 % compared to 104 % for melt blending, which was attributed to the high aspect ratio
18 of graphene and its better dispersion throughout the polymer matrix by solution mixing.

19 (ii) Thermal stability enhancement is another interesting feature offered by using a graphene
20 nanofiller in the preparation of thermally stable nanocomposites. Graphene/polymer
21 nanocomposites often showed better thermal stability than that of the neat polymer matrix. In
22 some cases, the material showed a 30 °C improvement in the onset degradation temperature
23 with the addition of only 1.4wt% of graphene. This distinctive feature of a graphene nanofiller
24 was attributed to the large specific area of the graphene sheets, which covered and hindered

1 the escape of volatile components within the polymer matrix, therefore increasing the thermal
2 degradation temperature.

3 (iii) The electrical conductivity of graphene-filled polymer nanocomposites was enhanced by
4 several orders of magnitude compared to the neat polymer. The remarkable enhancement in
5 electrical conductivity was due to the formation of a conducting network by graphene sheets
6 within the polymer matrix. However, the conductivities highly depended on the type of host
7 polymer matrix, the dispersion of the filler within the matrix, and the type of graphene-based
8 filler added. Most of the several-fold conductivity enhancements could be achieved even at a
9 low graphene content (<5 wt%)^{12, 20, 22}.

10 (iv) A homogenous distribution of graphene within the polymer matrix also enhanced the gas
11 barrier properties. The vapor permeation rate decreased significantly (up to six fold)
12 compared to the neat polymer³⁰ due to the high specific area of graphene within the polymer
13 matrix, which effectively extended the path of the water vapor passing through the film.

14 (v) The addition of graphene significantly enhanced the electrochemical activity of
15 conductive polymers. Both PANI/graphene¹³⁰ and PPy/graphene films²⁸ showed remarkable
16 enhancements in the capacitance performance (by up to several times).

17 This review of conductive polymer/graphene nanocomposites emphasized their potential
18 applications in energy storage and electrical devices in the future, including electrodes for
19 supercapacitors, fuel-cells, and lithium-ion batteries. Furthermore, the implementation of
20 graphene nanofillers in conductive polymer matrices has opened up a whole new area of
21 research on the fabrication of low-cost, lightweight, and excellent-performance
22 nanocomposite materials for a wide range of applications.

1 An excellent combination of graphene and polymer depended heavily on the dispersion of the
2 two components within the composite structure. Numerous efforts had been reported in
3 literatures, each trying to achieve improved interfacial by focusing on functional groups
4 interactions between graphene and polymeric chains. Furthermore, graphene
5 functionalization had been proven to effectively improve the dispersion of graphene within
6 the polymer matrices by displaying significant enhancement in the properties of the prepared
7 composites. Nevertheless, the main challenge is to ensure the effective separation of graphene
8 layers, in which proper spacing dimension is ensured to maximize the surface area of
9 graphene while maintaining nano-engineered space for polymeric chains to intercalate
10 effectively.

11

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