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# Superhydrophobic surface on copper via a one-step solvent-free process and its application in oil spill collection

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**Abstract:** One-step and solvent-free process was developed to fabricate superhydrophobic surface on copper by high-temperature oxidation (300 °C) in the atmosphere of gasified 1-dodecanethiol (DT). The so-obtained superhydrophobic surface on copper mesh was used to build a miniature oil containment boom (MOCB) that was used for oil spill collection. It was found that the MOCB was efficient with a collection rate of over 89 % and durable with the negligible decrease in collection rate and the deterioration in superhydrophobicity even after 25 cycles of kerosene collection.

Keywords: superhydrophobicity; thermal treatment; environment-friendly

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## 1. Introduction

Superhydrophobic surfaces with high water contact angle (CA, above 150°) and low sliding angle (SA, below 10 °) have gained significant research attention because of its wide potential application in our daily life and industrial production [1-8]. Traditionally, superhydrophobic surfaces are fabricated using a two-step process: (1) creation of rough structures on different substrates; and (2) passivation by low-surface-energy molecules [9-10]. However, this two-step process is complex and has limited practical application due to the emission of waste solvent. Recently, a novel one-step process based on simultaneous surface roughening and passivation is proposed for superhydrophobic surfaces fabrication [11-17]. For instance, after simply immersed in ethanol solution of n-tetradecanoic acid for 3-5 days, superhydrophobic Cu(CH<sub>3</sub>(CH<sub>2</sub>)<sub>12</sub>COO)<sub>2</sub> coating was fabricated on copper [18]. Such a process is time-consuming. Electrodeposition in different electrolytic solution such as ethanol solution of stearic acid [19], ethanol solution of myristic acid / nickel chloride [20] and ethanol solution of myristic acid /cerium chloride [21] was used to reduce the deposition time.

These reported one-step processes [19-21] are simpler in comparison to the traditional two-step process. However, the used organic solvent such as ethanol can have adverse impacts on the environment. Consequently, an aqueous solution of silver nitrate / benzoic acid was used to fabricate superhydrophobic surfaces on copper substrate by galvanic silver deposition [16]. In this context, the aim of this study was to develop an even more environment-friendly strategy to fabricate superhydrophobic

copper by a one-step solvent-free process. The copper substrate was roughened by oxidation and passivated by the gasified 1-dodecanethiol (abridged as DT) molecules in a sealed jar (50 mL) with small amount of DT (10  $\mu$ L) at high temperature (300 °C). The environmental impact of this strategy is expected to be extremely low since there is no solvent emission in the fabrication process.

Additionally, the environment-friendly feature of the superhydrophobic surfaces on copper is incorporated in the potential application. Superhydrophobic surfaces have been used in wide range of environment and energy related applications such as self-cleaning, corrosion resistance, drag reduction, and ice retardation [19, 22, 23]. Furthermore, superhydrophobic surfaces showed excellent performance in the oil spill collection [24-29]. For example, Wang et al. [25-27] compared superhydrophobic surfaces based method against traditional methods of oil containment booms, skimmers, dispersants, bioremediation and in situ burning. The superhydrophobic surfaces - based oil / water separation or oil spill collection was found to be recyclable and free of secondary pollution. Inspired by these studies, miniature oil containment boom folded from the superhydrophobic copper mesh fabricated by such a one-step and solvent-free process was used to collect spilled oils including kerosene, toluene, gasoline, and diesel oil from water.

#### 2. Materials and methods

#### 2.1 Sample fabrication

The copper plate (99.7%, Sinopharm Chemical Reagent Co., Ltd) was ground with abrasive paper and cleaned successively for 10 min in acetone, ethanol and ultrapure water. Then, the cleaned copper substrate was introduced into a sealed jar (50 mL) containing 10  $\mu$ L 1-dodecanethiol (DT, 97%, Sigma-Aldrich), which was placed in an oven and heated to the preset temperature (200 °C, 300 °C or 400 °C) with the rate of 10 °C / min an maintained for different time (0.5 h ~ 2 h). After that, the samples were cooled down to room temperature naturally. The so-obtained superhydrophobic copper plate was coded as Cu-HT&DT.

Traditional two-step process to render superhydrophobicity was also carried out. Specifically, the cleaned copper plate was firstly sealed in a jar, which was placed in an oven and heated to 300 °C with the rate of 10 °C / min and maintained for 1 h. The so-obtained sample was coded as Cu-HT. Then, the Cu-HT sample was immersed into an an ethanol solution of DT (1.0 wt %) at room temperature for 1 h, followed by rinsing with ethanol thoroughly and drying with a stream of air. The so-obtained sample was coded as Cu-HT-DT.

Control sample coded as Cu-DT-HT was also fabricated. Firstly, the cleaned copper substrate was immersed into an ethanolic solution of DT (1.0 wt %) at room temperature for 1 h, followed by rinsing with ethanol thoroughly and drying with a stream of air. Then, the copper substrate was sealed in a jar at 300 °C for 1 h. After

that, the samples were cooled down to room temperature naturally. The macroscopic appearance, microscopic surface morphology, and surface wettability of the control samples of Cu-HT, Cu-HT-DT, and Cu-DT&HT, were shown in Fig. S1.

To fabricate superhydrophobic copper mesh (1200 #, Anhua Fardware Product Co., Ltd.), the substrate was firstly cleaned in HCl (0.1 M), acetone, ethanol, and ultrapure water successively. Then, it was introduced into a sealed jar (50 mL) containing 10  $\mu$ L DT at 300 °C for 1 h.

# 2.2 Characterization

Contact angle (CA) and sliding angle (SA) were measured on a contact angle meter (Easydrop, Krüss, Germany) equipped with a computer-controlled liquid dispensing system at room temperature. All the reported CA and SA were determined by averaging values measured with an ultrapure water droplet of 5  $\mu$ L at five different positions on each sample surface. The microscopic surface morphology and element composition were characterized on a field-emission scanning electron microscope (FE-SEM, Nova NanoSEM, FEI, USA) equipped with an energy-dispersive X-ray spectrometer (EDX, INCA 250, Oxford, UK) at an accelerating voltage of 15 kV. The crystallographic structure was characterized on an X-ray diffraction meter (XRD, Bruker-axs, D8ADVANCE, Germany) equipped with the graphite monochromatized Cu K  $\alpha$  radiation at a scanning speed of 4 ° / min in the range from 10 ° to 70 °

Miniature oil containment boom (2.0 cm  $\times$  3.5 cm  $\times$  0.5 cm) folded from the superhydrophobic copper mesh was used for the investigation of oil spill collection.

Kerosene (1 #, Datang Petroleum Industry Co. Ltd), toluene (Shanghai Chemical Reagent Co. Ltd.), gasoline (93 #, Datang Petroleum Industry Co. Ltd) and diesel oil (10 #, Datang Petroleum Industry Co. Ltd) were chosen to simulate the oil spill.

# 3. Results and Discussion



#### **3.1 Superhydrophobic surfaces on copper plate**

Fig. 1. Influence of treatment time (0.5 h, 1 h, 2 h) and treatment temperature (200 °C, 300 °C, 400 °C) on contact angle for the Cu-HT&DT sample. SA is the abbreviation of sliding angle.

In this one-step process, treatment temperature and time are the key factors that influence the surface wettability (Fig. 1). For the treatment temperature of 200 and  $300 \,^{\circ}$ C, CA increased gradually to above  $150 \,^{\circ}$  when the treatment time was increased from 0.5 to 2 h. The corresponding SA for the sample with CA above  $150 \,^{\circ}$  was quite different. Specifically, when the treatment temperature was increased from 200 to

300 °C, SA decreased from 90 to below 10 °. For the treatment temperature of 400 °C, CA decreased from approx. 80 ° (0.5 h) to approx. 52 ° (1 h) and finally to approx. 9 ° (2 h) with the increase in treatment time.

Field-emission scanning electron microscope (FE-SEM) images for the Cu-HT&DT samples treated for 1 h at different treatment temperature are shown in Fig. 2. Despite the different surface features, all samples were rough structured. For the Cu-HT&DT sample treated at 200 °C, micro-balls and micro-stripes were observed (Fig. 2a). The observation under higher magnification suggests that the micro-balls were also not smooth (Fig. 2b). For the Cu-HT&DT sample treated at 300 °C (Fig. 2d), relatively smaller micro-stripes and nano-cubes were formed, whereas the surfaces were covered by disordered micro- and nano-cubes for the sample treated at 400 °C (Fig. 2f). It was supposed that superhydrophobicity could be obtained on all these micro- / nano-structured surfaces if the samples were passivated properly [30]. However, only the sample treated at the temperature of 300 °C was superhydrophobic (Fig. 1). It is hypothesized that the failure to obtain superhydrophobicity can be attributed to the surface chemistry rather than the surface structures. To test this hypothesis, non-superhydrophobic samples were transferred into ethanolic solution of DT for 1 h to further passivate the surface, after which the samples turned into superhydrophobic. This is demonstrated by CA and SA being  $159.3 \pm 1.5^{\circ}$  and  $5.7 \pm 0.8^{\circ}$ , respectively for sample treated at 200 °C, while for sample treated at 400 °C, CA and SA turned to  $163.5 \pm 1.6$  ° and  $3.4 \pm 0.7$  °, respectively.



Fig. 2. Field-emission scanning electron microscope images of samples treated for 1 h at different temperature of 200 °C (a, b), 300 °C (c, d), and 400 °C (e, f). All surfaces are rough-structured. However, only the sample treated for 1 h at 300 °C is superhydrophobic among these samples (as shown in Fig. 1).

The role of surface chemistry on the superhydrophobicity was investigated based on EDX analyses (Table. 1). The sulfur element originated from the absorbed DT molecules was the highest for the Cu-HT&DT sample treated at 300 °C (11.44 weight % or 7.13 atomic %), while it was lower for the samples treated at 200 °C (1.22 weight % or 1.63 atomic %) and 400 °C (3.60 weight % or 4.60 atomic %). This can be attributed to the gasification temperature of DT, which is 266 ~ 283 °C, and stability of DT molecules at different temperatures [31-34]. Specifically, when the treatment temperature is 200 °C, DT molecules are not gasified and consequently the amount of the absorbed DT onto the solid substrate is small. When the treatment temperature is 400 °C, DT molecules are decomposed. Furthermore, as the treatment time increases, the decomposition is more thorough and the surface becomes more hydrophilic (for treatment time of 2 h, surface superhydrophilicity with CA of approx.

9 ° was obtained, Fig. 1).

Table. 1. Elemental composition obtained from the energy-dispersive X-ray spectrometer for the Cu-HT&DT samples treated for 1 h at different temperature.

Element	Weight %			Atomic %		
	200 °C	300 °C	400 °C	200 °C	300 °C	400 °C
С	5.40	37.76	4.07	19.18	62.79	19.90
0	8.28	15.10	11.45	22.08	18.85	29.33
S	1.22	11.44	3.6	1.63	7.13	4.60
Cu	85.09	35.70	80.88	57.11	11.22	52.17

From above discussions, it is apparent that the treatment temperature of 300 °C is effective to produce superhydrophobic surfaces. At this treatment temperature, the influence of treatment time on surface wettability was investigated. FE-SEM images of the Cu-HT&DT samples treated at 300 °C for 0.5 h and 2 h are shown in Fig. 3 (a). For 0.5 h, micro-balls and micro-stripes were formed on copper substrate and the morphological microstructures were similar to the sample treated at 200 °C for 1 h. The CA for the Cu-HT&DT sample treated at 300 °C for 0.5 h was approx. 140 ° (Fig. 1), which was also close to that for the Cu-HT&DT sample treated at 200 °C for 1 h. The similarity in surface morphology and wettability suggested that the reaction atmosphere for these two samples were quite similar, i.e. the gasified DT molecules

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under the conditions of 200 °C / 1 h and 300 °C / 0.5 h were inadequate due to the lower treatment temperature (200 °C) or shorter treatment time (0.5 h). Consequently, the so-prepared the Cu-HT&DT samples were hydrophobic with similar surface morphological micro-structures. As the treatment time increased to 1 h, more DT molecules were gasified and the amount of DT molecules that were attached to the substrate had increased. Consequently, the surface morphology and wettability had changed as shown in Fig. 1 and Fig. 2 (c) / 2 (d). When the treatment time was further increased to 2 h, rough surface structures of micro - / nano - balls were formed [Fig. 3 (a)] leading to formation of the surface superhydrophobicity (Fig. 1).



Fig. 3. (a) Field-emission scanning electron microscope images of the Cu-HT&DT samples treated at 300 °C for 0.5 and 2 h; (b) X-ray diffraction patterns of copper substrates (i), copper treated for 1 h at 300 °C without 1-dodecanethiol (ii), and copper treated for 1h at 300 °C with 10  $\mu$ L 1-dodecanethiol (iii). HT is the abbreviation of hot treatment; DT is the abbreviation of 1-dodecanethiol.

X-ray diffraction (XRD) patterns of different samples were shown in Fig. 3 (b). The bare copper substrate [Fig. 3 (b) - (i)] showed characteristic peaks of Cu (111) (2 theta = 43.30 °) and Cu (200) (2 theta = 50.42 °). For the Cu-HT&DT sample [Fig. 3 (b) - (iii)], new peaks with 2 theta values of 29.45 °, 36.35 °, 42.35 °, and 61.43 ° ascribed to Cu<sub>2</sub>O (110), Cu<sub>2</sub>O (111), Cu<sub>2</sub>O (200), and Cu<sub>2</sub>O (220), respectively, appeared [35]. This suggests that the copper was oxidized into Cu<sub>2</sub>O probably through the following reaction equations [36]:

$$2Cu + O_2 \rightarrow 2CuO \qquad \text{Eq. 1}$$
$$CuO + Cu \rightarrow Cu_2O \qquad \text{Eq. 2}$$

It was supposed that, at the beginning of reaction, copper is turned into CuO (Eq. 1), the growth of which decreased gradually on account of the consumption of oxygen when the reaction time increased. Meanwhile, CuO generated on the surface could be reduced into Cu<sub>2</sub>O by Cu (0) of the copper substrate (Eq. 2). The strongest peak for the Cu-HT&DT sample located at 2 theta =  $36.35 \circ$  was also observed for the sample of Cu-HT [Fig. 3 (b) - (ii)]. However, other weak peaks appeared in the XRD pattern of the Cu-HT&DT sample ascribed to Cu<sub>2</sub>O were not observed. This suggests that the gasified DT molecules can promote formation of Cu<sub>2</sub>O. The detailed mechanism for such promotion remains unknown. However, it is hypothesized that the reducibility of DT molecules cannot be neglected in the formation of Cu<sub>2</sub>O by the one step process. For example, as discovered by Fonder et al. [37], CuO was reduced to Cu<sub>2</sub>O by the thiol molecules. DT molecules would react with Cu<sub>2</sub>O to facilitate the surface attachment through the following reaction [38]:

$$2CH_3(CH_2)_{10}CH_2SH+Cu_2O \rightarrow 2CH_3(CH_2)_{10}CH_2SCu+H_2O$$
 Eq. 3

#### 3.2 Superhydrophobic surfaces on copper mesh

From the above discussions, it is concluded that the optimum temperature to fabricate superhydrophobic surfaces on copper plate was 300 °C and the optimum treatment time was 1 or 2 h. Superhydrophobic surfaces on copper plate fabricated at 300 °C for 1 h were found to be superoleophilic with CA of approximately 0 ° (Fig. S2) [39, 40]. For the copper mesh, after treated at 300 °C for 1 h, the surface turns into relatively rougher [Fig. 4 (a-i, a-ii)] in comparison to the pristine one (Fig. S3). Meanwhile, surface with superhydrophobicity (CA =  $162.8 \pm 2.2$  °, SA =  $3.5 \pm 0.8$  °) and superoleophilicity (CA of approx. 0 °) was obtained.

The special surface wettability, i.e., superhydrophobicity and superoleophilicity, of copper mesh for the oil spill collection was investigated. The primary factor influencing the use of the mesh in these potential applications is the stability of superhydrophobic surfaces [24-26, 38, 41], which was simply evaluated by measuring the variation of surface wettability for the superhydrophobic copper mesh immersed into water [Fig. 4 (a-iii)]. Before measuring, the superhydrophobic copper mesh was taken out from the water and dried using nitrogen stream. The experimental results showed that the mesh exhibited good water repellency after immersed for 12 days (CA =  $155.7 \pm 2.5$ °, SA =  $24.0 \pm 2.2$ °). The superhydrophobic copper mesh was also immersed into ethanol for 30 min under ultrasonication (the power and frequency for the ultrasonic cleaner is 100 W and 40 kHz). After that, the surface superhydrophobicity was still retained (CA =  $156.8 \pm 1.2$ °, SA =  $11.2 \pm 1.5$ °).

Miniature oil containment boom (MOCB, 2.0 cm  $\times$  3.5 cm  $\times$  0.5 cm) was folded from a sheet of superhydrophobic and superoleophilic copper mesh. The MOCB was found to be floating freely on the water surface [Fig. 4 (b-i)]. MOCB readily absorbed the kerosene when 10 mL of it was poured into the water [Fig. 4 (b-ii)]. The contained kerosene was continuously collected using a pump and the final kerosene volume collected was 9.1 mL [Fig. 4 (b-iii)]. As shown in Mov. S1, the time taken for the collection was less than 2 min. The oil collection rate (*k*) of the MOCB was calculated using the following formula

$$k = v/v_0 \times 100$$
 % Eq. 4

where  $v_0$  is initial volume of oil deliberately poured into the water surface and v is the volume of the collected oil. The collection rate of the MOCB for other oils such as toluene, gasoline, and diesel oil was also investigated [Fig. 4 (c-i)]. The *k* values were greater than 89 % for all cases after the first collection cycle, which were comparable with the reported data [24, 42-43]. Moreover, the repeated use of the MOCB was studied. After a cycle, the MOCB was contaminated by oil. The superhydrophobicity in contaminated MOCB was regenerated by cleaning it with the ethanol and then drying it at room temperature for 1 h. The regeneration facilitated the repeated use of the MOCB. As illustrated in Fig. 4 (c-ii), the collection rate *k* was greater than 89 % even after using the MOCB for 25 cycles in kerosene collection from the water surface. Additionally, CA was greater than 150 ° and SA was smaller than 10 °, which demonstrate its good reproducibility.



Fig. 4. Field-emission scanning electron microscope images of copper mesh treated for 1 h at 300 °C (a-i, a-ii). Evolution of contact angles and sliding angles for superhydrophobic surfaces immersed into water (a-iii). The miniature oil containment boom floating on water (b-i), the collecting of kerosene from water (b-ii, the volume of kerosene is 10 mL), and the collected kerosene (b-iii, the collected kerosene is 9.1 mL). Collection rate of the miniature oil containment boom for different oils in the first cycle (c-i). Effect of kerosene / water collection cycle on the collection rate and contact angles (c-ii).

# 4. Conclusion

An environmentally benign route was proposed to fabricate superhydrophobic surfaces on copper. The optimum treatment temperature for the fabrication route was 300 °C, which is close to the gasification temperature of DT and the optimum treatment time was 1 h or 2 h. The so-fabricated superhydrophobic surface was superoleophilic. The unique surface wettability, i.e., superhydrophobicity and superoleophilicity, facilitates the use for collecting oil spill from water surface. The MOCB was folded from a superhydrophobic and superoleophilic copper mesh and was efficient with a collection rate of over 89 % and durable with the negligible decrease in collection.

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